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## stereo amplifiers

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PHILIPS RH521
PHILIPS RH590
PHILIPS RH580
PIONEER SA500A.
PIONEER SA600.
PIONEER SA800.
pioneer sa900
PIONEER SA1000 ........................
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QA 800 Quadraphonic
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ELETON GT202

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TUNERAMP IMERS
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Recorder .......................
AKAI AA 850
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AKAI 6300.
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VR 5521 L AR 5501 AM/FM
4VR 5414 Quadraphonic
LEAK Delta 75
PHILIPS RH 790 .

| CARTRIDGES - contimued | Rec. Retall |
| :--- | :--- | ---: | ---: |
| Price | Comet |
| Price |  |


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| $5^{\prime \prime}$ L.P. 900 | 1.41 | 0.85 |
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GRUNDIG TK 141 4-track
GRUNDIG TK 141 4-track 4 -track Aut
GRUNDIG TK 147 4-track Auto
GRUNDIG TK 147 4-track Auto ${ }^{\text {GR }}$
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4307 4 -track
4308 De luxe 4-track
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corder.
PHILIPS 4416 4-track stereo re-
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$131 \cdot 85$
$141 \cdot 10$
$39 \cdot 46$
$50 \cdot 00$
$59 \cdot 00$
$89 \cdot 25$
$108 \cdot 50$
$120 \cdot 00$
$145 \cdot 00$
$200 \cdot 00$
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Ask the chap who's got one, there's lots of them!
NOTE: These CODAR Receivers meet the B.R.E.M.A. specification for Communication Receivers and are FREE of Purchase Tax. Some portable receivers being advertised as Communication Receivers do not meet these requirements.

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## THE HY41

The HY41 supersedes the popular HY40 introduced by ILP last year. This highly improved module achieves true High Fidelity with a dramatic reduction in distortion (typically $0.05 \%$ at 1 KHz into 8 ohms!) and is electronically and mechanically compatible with the HY 40 .

With this important improvement the HY41 retains all of the quality characteristics found in the earlier version and.P.C. board, Resistor, Capacitors, Hardware Mountings and comprehensive manual are included in the basic kit. No further components are required to construct a complete power amplifier of extremely high performance sufficiently versatile to provide power not merely for Hi -Fi but also for public address systems and industry.

The free manual gives a full circuit diagram of the HY41 and its various applications including a complete stereo amplifier.

Like its predecessor the HY41 is based on conventional and proven circuit techniques developed over recent years.
OUTPUT POWER: British Rating 40 WATTS PEAK, 20 watts
R.M.S. continuous.

LOAD IMPEDANCE: 4-16 ohms.
INPUT IMPEDANCE: 30 K ohms at 1 KHz .
VOLTAGE GAIN: 30 db at 1 KHz
TOTAL HARMONIC DISTORTION: less than 0.15\% (typical 0.05\%)
at 1 KHz .
FREQUENCY RESPONSE: $5 \mathrm{~Hz}-50 \mathrm{KHz} \pm 1 \mathrm{db}$.
SUPPLY VOLTAGE: $t 22.5$ volis D.C.
SUPPLY CURRENT: 0.8 amps maximum.
PFICE: inc. comprehensive manual, P.C. board, five extra components and P. \& P.
MONO: $£ 4.90$

## UNIQUE HYBRID PRE-AMPLIFIER

The HY5 has rapidly established a position in the WORLD as the sole hybrid pre-amplifier to contain all feedback and equalization networks within an integrated pre-amplifier circuit.

Supplied with the HY5 are two stabilizing capacitors and by the addition of volume, treble and bass potentiometers it is ready for use

Internally the HY5 provides equalization for almost every conceivable input, the desired function is achieved by use af a multi-way switch or by direct interconnection,

Two distinctive features of the HY5 are its inbuilt stabilization circuit, allowing it to be run off any unregulated power supply from 16-25 Volts and a balance circuit which, when linked by a balance control to e second HY5, forms a complete stereo preamplifier.

Specifically and critically designed to meet exacting Hi-Fi standards, the HY5 combines extremely low noise with a high overload capability. When used in conjunction with the HY41 and PSU45 forms a completely intergrated system.

Magnetic Pick-up (within $\pm$ 1db RIAA curve) 2 mV .47 K
Tape Replay fexternal components to suit head). $4 \mathrm{mV} .47 \mathrm{~K} \Omega$
Microphone (flat) $10 \mathrm{mV} .47 \mathrm{~K} \Omega$
Ceramic Pick-up lequalized and compen-
satabie) $20-2000 \mathrm{mV}$. variable.
Tuner (flat) $250 \mathrm{mV} .100 \mathrm{~K} \Omega$
Auxiliary 1250 mV . $47 \mathrm{~K} \Omega$
Auxiliary $22-20 \mathrm{mV}$. $100 \mathrm{~K} \Omega$

OUTPUTS
Main Preamp output 500 mV .
Direct tape output 120 mV .
ACTIVE TONE CONTROLS (Baxendall)
Treble $\pm 12 \mathrm{db}$.
Bass +72 db .
INTERNAL STABILIZATION
Enables the HY5 to share an unregulated supply with the Power Amplifier.
SUPPLY VOLTAGE
16-25 volts
PRICE: MONO: $£ 3.60$

## POWER SUPPLY PSU45

The versatile P.S.U. 45 is designed to supply your HY41's +HY5's in stereo or mono for mat.

## Specification

Input: 200-240 Volts.
Output: $\pm 22.5$ Volts at 2 amps .
Overall Dimensions: L. $7^{\prime \prime}$; D. 3.8"'; H. $31^{1+}$
PRICE: $\mathbf{£ 4 . 5 0}$ inc. P. \& P.


## MINIATURE POWER DRILLS

Capable of Drilling Mild Steel
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20-Watt Full Range Speaker Completely replaces the conventional cone speaker Super-thin construction permits new installation ideas.
Power capability: 40 watts peak. Frequency range: $40 \mathrm{~Hz}-20 \mathrm{KHz}$ Sensitivity: $85 \mathrm{~dB} / \mathrm{M}$ for 1 watt electrical input. Input impedance: 8 ohms. Operating temperature range: $-20^{\circ} \mathrm{F}$ to $+175^{\circ} \mathrm{F}$. Size
(W×DxL) $1 \cdot 7 / 16^{\prime \prime} \times 11 \cdot 3 / 4^{\prime \prime} \times 14 \cdot 11 / 16^{\prime \prime}$. Weight: 19 .
£6.50 each Stereo pair $£ 12.50$ post free
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RELAXATRON
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| 384 | 40 | 6C6 25 | 6L6G |  | 10F18 60 | 25Z5GT | 55 | 80180 | DK92 | 55 | ECH83 | 45 | EZ41 | 50 | PCF84 | 60 | R2 | 75 | UCL83 | 60 |
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| 1 T 4 | -14 | 30 PL 1. | $\cdot 58$ | ECC82 | $\cdot 18$ | EF184 | . 27 | PCF86 | . 44 | PY801 | . 80 |
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| 6SN7GT | -28 | DL96 | -36 | ECL86 | . 82 | KT66 | .75 | PFL200 | . 48 | UCL 82 | . 80 |
| 12AU7 | 18 | DY86 | $\cdot 21$ | EF39 | . 38 | N78 | . 85 | PL36 | . 45 | UF41 | - 49 |
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${ }_{A}^{A C 188 K}$
ACY17
ACY18
ACY19
ACY19
$A C Y 19$
$A C Y 20$
ACY 21
ACY 22
ACY 27
ACY27
ACY 28
4CY28
4 CY 29.
ACY30
ACY 31
ACY 34
CY 34
ACY 55
CXY
ACY36
ACY40
ACY40
ACY41
$A C Y 41$
$A C Y 44$
$A C Y 44$
AD130
AD140
AD 130
AD140
AD142
AD143
AD149
AD161



0.45 BF188

45 BF188 BF19 BF194
BF195
$0.40 \quad 0 \mathrm{Cl} 19$


$\begin{array}{ll}80 & \text { BF197 } \\ 60 & \text { BF200 }\end{array}$
BF200
BF222
BF257
BF258
BF259




$\qquad$ 2N3054
2N 3055
2N3391
2N $3391 A$
2N3392
2N3393
2N3394
2N3395
2N3402
2N3403
2N3404
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0 0.17
0.17
0.17

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| U29 | 101 Amo SCR's TO-5 can, up to 600 PIV CRSi/25-600 | . 0 |
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& 3 \text { AF } 117 \text { type transistors } \\
& 3 \text { OC } 171 \text { H.F. type transistor }
\end{aligned}
$$

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& \text { OU } 17 \text { B.F. type transistors. ..... } \\
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\text { Q16 } 2 \underset{\text { GETR coloura }}{\text { mixed }} \text {. .......................... }
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\begin{aligned}
& \text { transistors. } \\
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## Q21 4 AC127 NPN Germanium transistor

 Q22 20 NKT transistors A.F. R.F. coded.. Q23 10 OA 20:2 gilicon dionlea sub-min.Q24 8 OA 81 dionesQ26 8 OA45 Germantun diodes sub-minQ27 4 10A PIV siliton rectifers IS 425 K .
Q28 2 Silicon power rectifer BYZ13 .. $0 \cdot 50$
Q29 4 Silicon transistors $2 \times 2 \times 2 \times 13$...

Q3i 6 Silicn
Q32 3 PNPSilicon0.50
Q34 7 Sllicon NP transistors $2 \mathrm{~N} 1711 \ldots$500 MHF (cole PYa7)
 ..... 0.50
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witch）．SPEC．： 2101
240 V a．c． 50 Hz operation；switch rating $250 \mathrm{~V}, 3 \mathrm{~A}$ Complete with instructions，COMPLETE WITH KNOBS．FEATURES：－MAINS OPERATION I2－HOURALARM AUTO ＇SLEEP＂SWITCH HOURS，MINUTES AND SECONDS READ－OFF FORWARD AND BACKWARD TIME ADJUSTMENT －SILENT OPERATION SHOCK AND VIBRATION PROOF BUILT IN ALARM BUZZER
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This small versatile，easy to handle，power tool is doal for handymen，and professionals． drill rout cut erc．Perfect for delicare work drim，rout，cut erc．Perfect for delicate work．T MODEL 600K 37 piece Kit contains：
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## 

 Bronches
## Happy Anniversaries

F you have been orbiting in space, trekking across the Gobi Desert or drifting down the Amazon for the past few months, it is possible that the news of the great event about to be celebrated has not filtered through. Otherwise, you will be aware that this month the BBC notches up the 50th Anniversary of broadcasting in the UK.

Special programmes are being broadcast on radio and television, exhibitions are being mounted by the BBC and others, the Post Office has issued a special set of postage stamps, the IEE is staging a series of lectures. After such a welter of words, pictures and sounds, what is there left to say? Not a lot, really, except for Practical Wireless to add its tribute to all those on the engineering, programme and administrative sides, who over the past 50 years have made a contribution towards what is still (despite its lovable faults) the best broadcasting service in the world.

But while we are indulging in flag-waving, let us not forget the unsung heroes who have also played a part in the development of broadcasting-the component makers, the set makers, the performers, the backroom boys and those overlooked but staunch martyrs, the listeners themselves!

There is yet another group who, collectively, deserve a modest pat on the back-our colleagues, past and present, who presumably through some inherited defect (or sheer masochism) decided to devote their life to the career of technical journalism! In the early days of broadcasting, and even before it, the technical journals generated and sustained the interest in the subject. The famous magazines of the day, such as Popular Wireless, Wireless Magazine and Amateur Wireless have long been but memories, but three of the pioneer publications are still with us-Wireless World, Practical Wireless and Television (which started life as Practical Television as early as 1934).

At the risk of being dubbed chauvinistic, this seems to be the right occasion to mention (with a becoming blush) that during the BBC festive season of celebrating their 50th Anniversary, readers may like to raise a flag or two in recognition of the fact that this year Practical Wireless is a contender in the Anniversary Stakes, having now reached its 40th birthday-a period of time during which, like the famous Windmill, we never closed!
W. N. STEVENS-Editor.

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[^1]
# NEWS... 

## Bristol '73

The Bristol Group of the R.S.G.B. are now privileged to announce their plans for participation in the 1973 anniversary celebrations of the granting of the Royal Charter to the City and County of Bristol.

One aspect will be the operation of an amateur radio exhibition station on the S.S. Great Britain, now being restored in dry dock at Bristol.

The Ministry of Posts and Telecommunications, as the licensing authority, has agreed to the special call sign "GB2GB" for a station to be operated from the vessel and will permit the station to be operated by persons holding current Amateur (Sound) Licences A who visit the vessel during the month of August, 1973.

The general public will hear contacts being made with amateur radio stations, both local and long distance, and information will be available from the operators on the hobby of amateur radio and the role it plays in promoting international understanding.

With the co-operation of the S.S. Great Britain Project, receiving tests already carried out from the vessel have indicared that the site is suitable for reception and therefore transmission is not considered to present any problems.

It is anticipated that the station will make contacts with stations in other Bristols and the cities of Hanover and Bordeaux. Contact will also be attempted with amateur radio stations in the Falkland Islands where the vessel lay in Sparrow Cove for many years.

Specially designed cards depicting the S.S. Great Britain will be sent to amateur radio stations contacting GB2GB and these are being donated by a famous firm of Bristol wine merchants who have also agreed to present cases of sherry as awards in a Bristol Amateur Radio Activity Contest to be held in 1973, details of which will be announced in a few months' time.

As 1973 is also the Diamond Jubilee of the Radio Society of Great Britain, local members are pleased to announce that a convention will be held at a local hotel. This is to be on the 26th May, 1973, and details are now being planned.

It is hoped that these eventsGB2GB on the S.S. Great Britain, and radio contest, and the convention, will make 1973 a memorable year for Bristol and radio amateurs.

Further gen from G. Mather G3GKA, 8 Hills Close, Keynsham, Bristol.

## The "Elif"



West Hyde announce the Contil "ELF". Only 6in. x 4in. x 4in., they are offered at five cases for $\pm 6$ including postage and packing. (£1.25 ea. +10 p p.p.)

Glass polyester dough moulded in grey or blue, the price includes a chromium plated handle, an aluminium chassis, a protectively coated aluminium front panel and four fitted feet.

Two printed circuit boards can be fitted in the slots provided internally, making the case ideal for the increasing number of applications requiring miniature cases, in step with the firm's well known policy this tough smart little case is available by return of post. West Hyde Developments Ltd., Ryefield Crescent, Northwood Hills, Northwood, Middx.

## Portable rechargeable soldering iron

Soldering with the new 8 in. long portable, lightweight. soldering iron-which is rechargeable and can be used far from a power source-launched by the Van Dusen Aircraft Supplies Company in the UK and Europe. The "IsoTip" soldering iron, weighing less than 6 ounces, has been designed to handle, with speed and efficiency, every industrial or domestic soldering requirement. Price of unit and stand is $£ 8 \cdot 75$. Van Dusen Aircraft Supplies Co., Oxford Airport, Kidlington, Oxford.

Picture shows the iron in use.


## Pictures on the phone

EMI has entered the facsimile communications market with a document transceiver for sending clear, accurate copies of documents in minutes to anywhere in the world. Known as the EMIfax HF146, this compact, desk-top system transmits and receives any type of document up to A4 size ( $220 \times 305 \mathrm{~mm}$ ), including invoices, lists, graphs, sketches and handwritten notes, over public or private telephone networks.

A unique cost-saving advantage of the EMIfax machine is that normal office stationery is used for reproducing transmitted copies, eliminating the need for expensive coated papers which create both cost and supply problems. The document transceiver is priced at $£ 900$. Leasing and rental facilities are also available.


## A quick NIP

NIP Electronics, mentioned in our October News . . . pages have asked us to say that two of the readers who have written to them asking for information on NIP-E-BOARDS omitted to give their full addresses.

If they would please communicate with NIP again, giving their full addresses, they will be pleased to supply the items they require.

The readers are: Mr. A. M. Coppin, 128 Fernside Avenue and Mr . Christopher Jones of Coventry.

NIP Electronics, P.O. Box 11, St. Albans, Hertfordshire.

## Texan Reprints

Reprints of the "Texan" $20+20 \mathrm{~W}$ Stereo Amplifier are now available.

They may be obtained by sending 35 p ( $30 p+5$ p postage/packing) to Practical Wireless Editorial, Fleetway House, Farringdon Street, London, EC4A $4 A D$

## Paramo Handyvice

Latest addition to the Paramo range of tools is a new design of vice. The vice is manufactured from die cast high strength aluminium alloy, designed to give comparable strength to the standard cast iron product, but with considerable savings in weight.

The vice is available in three forms, a 3in. fixed base mechanics vice (HV1), a 3 in. swivel base mechanics vice (HV2), a 3in. swivel base mechanics vice with table clamp (HV3).

The vice is finished in hammer blue enamel with chrome plated moving parts. It is supplied with hardened file cut steel jaws and a steel anvil for light metal forming. On the swivel base versions a simple single handed locking lever enables the vices to be swivelled through $360^{\circ}$.

Prices are: HV1, £2.45; HV2, £2.95; HV3 (illustrated), £3.45.F. Parramore \& Sons (1924) Ltd., Caledonian Works, Chapeltown, Sheffield, Yorkshire.


## Disc car aerial



A new car radio aerial is being introduced by Valan Electricals to complement their wide range of conventional aeríals.

Named the Valan Disc Aerial, it combines the function of an aerial with that of the road tax licence holder or a club card holder, and is fitted on the windscreen.

It can be fitted in minutes by anyone. The fitting instructions are simple and are on the reverse of the pack. It works equally well in all makes of car and commer* cial vehicles.

The recommended retail price is $£ 1 \cdot 20$. The Valan Disc Aerial is available from Halfords and leading garage and accessory shops. Valan Electricals, 1034 Yardley Wood Road, Birmingham B14 $4 B W$.

## QSL from the BBC

This month there will be an opportunity for listeners to the BBC World Service programme, World Radio Club, to possess one of the BBC's QSL cards verifying reception of the Club's 50th Anniversary Edition.

There are 12,000 members of the Club, spread all over the world. The programme is broadcast on Thursdays at 1330 , Fridays at 2345 , and Sundays at 0815 GMT in the World Service. Any member who reports accurately on reception of the Anniversary Edition on November 9th, 10 th or 12th will be able to receive this QSL.

If you are not a member, write to World Radio Club, BBC, Bush House, London.

# AMAIIUR BANSS REEEIVER <br> 1.8-30MHz•AM-CW-SSB•BANDSWITCHED•EASYCALIBRATION PART 1 <br> <br> F. G. RAYER G30GR 

 <br> <br> F. G. RAYER G30GR}

THIS receiver possesses high stability coupled with excellent sensitivity, selectivity and adequate bandspread covering the Amateur bands from 10 to 160 metres. On all bands, except 80 m , the receiver employs double conversion with a crystal controlled first oscillator. It is easy to tune and to hold a.m., c.w. or s.s.b. signals on all bands.
Those who may not be familiar with the method of operation of this type of receiver should find the block diagram of Fig. 1 helpful in conjunction with the description that follows.

## CIRCUIT

Referring to Fig. 1 stage (1) is an r.f. amplifier followed by the first mixer (2) both working on all bands except 80 m . Each Amateur band, except 80 m , employs a crystal (3) chosen so that the output of the mixer (2) falls in the range $3 \cdot 5$ to 4 MHz whatever the band in use. This tuning range 3.5 to 4 MHz is covered by the tunable r.f./i.f. amplifier (4) and is followed by the second mixer and tunable oscillator (5) forming the tunable i.f. part of the receiver on all bands, except 80 m . On 80 m signals fall in the range $3 \cdot 5$ to 4 MHz and are switched to stage (4).
The output frequency of the second mixer (5) is 455 kHz which goes to the crystal filter (6) which is a bandpass filter with 2 kHz crystal separation. When using a single filter for a.m., c.w. and s.s.b. this is about the highest degree of selectivity which can be tolerated without excessive cutting of the sidebands of a.m. signals.

Stages (7) and (8) are 455 kHz i.f. amplifiers followed by the a.m. diode detector (9), its output going to the a.f. amplifier and output stages (10) and (11) and thence to the speaker. For c.w. and s.s.b. reception the beat frequency oscillator (12) and product detector (13) are switched into circuit. Both tunable oscillators (5) and (12) are fed from a voltage regulated source (14).

As the first i.f. is $3 \cdot 5$ to 4 MHz the second channel interference, which can be troublesome on the h.f. bands with a lower i.f., is virtually eliminated. The
use of a crystal controlled oscillator also gives an enormous improvement in overall stability.
The tuning coverage of each band is a constant 500 kHz with fixed 100 kHz calibration points which completely eliminates any calibration problems on the h.f. bands. One disadvantage is that because the 10 m band is so wide only a small portion of it can be covered butt this can be overcome by providing two or more 500 kHz sections with very little extra circuitry, as explained later.

## CONVERSION FREQUENCIES

As stated the tunable i.f. covers $3 \cdot 5$ to 4 MHz and is calibrated at 100 kHz intervals. The crystal frequency for the 160 m band is $5 \cdot 5 \mathrm{MHz}$ the difference or signal frequency selected by stages (1) and (2) thus extending from $1 \cdot 5$ to $2 \mathrm{MHz}(5 \cdot 5-3 \cdot 5$ and $5 \cdot 5-4$ ). In this case the oscillator frequency is on the high side of the tunable i.f.

| Band | Crystal | Calibration MHz |  |  |  |  |  |
| ---: | :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 80 | None | $3 \cdot 5$ | $3 \cdot 6$ | $3 \cdot 7$ | $3 \cdot 8$ | $3 \cdot 9$ | $4 \cdot 0$ |
| 160 | $5 \cdot 5$ | $2 \cdot 0$ | $1 \cdot 9$ | $1 \cdot 8$ | $1 \cdot 7$ | $1 \cdot 6$ | $1 \cdot 5$ |
| 40 | 11 | $7 \cdot 5$ | $7 \cdot 4$ | $7 \cdot 3$ | $7 \cdot 2$ | $7 \cdot 1$ | $7 \cdot 0$ |
| 20 | $10 \cdot 5$ | $14 \cdot 0$ | $14 \cdot 1$ | $14 \cdot 2$ | $14 \cdot 3$ | $14 \cdot 4$ | $14 \cdot 5$ |
| 15 | $17 \cdot 5$ | $21 \cdot 0$ | $21 \cdot 1$ | $21 \cdot 2$ | $21 \cdot 3$ | $21 \cdot 4$ | $21 \cdot 5$ |
| 10 | $24 \cdot 5$ | $28 \cdot 0$ | $28 \cdot 1$ | $28 \cdot 2$ | $28 \cdot 3$ | $28 \cdot 4$ | $28 \cdot 5$ |

For 40 m an 11 MHz crystal is used giving coverage of 7 to $7 \cdot 5 \mathrm{MHz}$ the crystal again being on the high side. Crystal frequencies for the remaining bands are shown in the accompanying table and it will be noted that they are all below the signal frequency. Calibration points are shown, the direction being reversed on 160 and 40 m because these crystals are above the signal frequency.
Since stages (1) and (2) cover 28 to 30 MHz three 500 kHz segments can be obtained by simply selecting the appropriate crystal with a three way switch, crystals on 25 and 25.5 MHz adding bands 28.5 to 29 MHz and 29 to $29 \cdot 5 \mathrm{MHz}$.


Fig. 1 : Block diagram to illustrate the function of each stage in a double conversion communications receiver.

## PROGRESSIVE CONSTRUCTION

The constructional work involved is naturally not simple but it can be carried out and tested in sections. This method has much to recommend it as the location of a wiring fault or error is then much easier. The audio stages together with the power supply can be wired and tested with a pick-up or audio oscillator as a signal source. Stages (4) and (5) with one i.f. stage and the a.m. detector can be added thus forming a complete 80 m receiver.

Next the additional i.f. stage and filter together with the b.f.o. and product detector will provide additional selectivity and c.w. and s.s.b. facilities. Stages (1) and (2) should then be wired for one additional band and checked after which the other bands can be added one by one. This general plan will be followed in the articles that follow.

## AF/POWER SUPPLY

In Fig. 2D showing this part of the circuit VR1 is the usual audio volume control, followed by a 2-stage amplifier, the output section of the ECL86 providing about 3 watts of audio. An output jack connected to the secondary of the speaker transformer Tl permits the use of phones or an external speaker automatically silencing the phones. This facility can be useful when operating the receiver with a transmitter.
The mains transformer T2 and rectifiers D1 and D2 supply 250 V for the triode anode, pentode screen grid and earlier stages of the receiver. The OA2 voltage regulator provides a stabilised 150 V supply for the tunable i.f. oscillator and beat frequency oscillator.

If T2 is not as listed, the h.t. voltage may be


Rear view of the completed receiver with the tunable If ampliffer in its own screened box on top of the chassis with the five crystals for the first mixer stage to the right. The two crystals at the bottom right are part of the fixed IF amplifier.

different. This has little effect on most stages of the receiver, but if it is found that the OA2 is extinguished or nearly so, with the receiver on any band other than 80 m and with no aerial connected and the r.f. gain control at maximum gain, then the h.t. is too low. It is then in order to reduce R7 or R8, or both, to obtain about 250 V .
Leads to VR1 run against the chassis and need not be screened but R5 should be soldered directly to pin 8 of the ECL86. A 250 mA fuse is placed in a holder on the inside of the chassis, and is in the h.t. circuit from T2 to earth.

The heaters require about 3 A and are run from the 6.3 V 4 A winding of T 2 . If a transformer is fitted which has two 6.3 V windings, rated at less than 3A, use one heater winding to supply some heaters and a separate circuit from the other heater winding to the remaining heaters.

The a.f. amplifier and power supply can be checked by connecting a pick-up, audio signal generator or other source of a.f. to the top of VRI. A $3 \Omega$ speaker is connected to or plugged into J1.

## IF STAGES

Fig. 2C is the circuit of this section of the receiver which operates at 455 kHz . IFTl is an intermediate frequency transformer with a centre-tapped secondary the centre tap being earthed. Balanced output in opposite phase, from pins 4 and 6 , go to the two crystals X6 and X7, which have a frequency separation of about 2 kHz . This pass-band can readily be modified, as described later. It is, however, a reasonable degree of fixed selectivity for all general amateur band purposes and avoids the need for an adjustable phasing capacitor.

Valves V1 and V2 are the two i.f. stages at 455 kHz both receiving bias from the a.g.c. line (which also passes to some earlier stages). The manual gain control VRI adjusts the cathode bias of the first i.f. stage.

Diode Dl provides bias for the a.g.c. line and also operates as the a.m. detector.
Switch Sla is one pole of a 3-way switch, and when in the "AM" position feeds audio via C 9 to the volume control.

When Sla is in the "CW/SSB" position, audio signals are fed from the product detector, Fig. 2E. The central position of Sl is for "Standby" when h.t. is removed from several stages.

## S-METER

Incoming i.f. signals produce negative bias at diode D1, Fig. 2C, fed through R10 and the secondary of i.f.t. 2 to V2 control grid. This moves negative with increased signal strength, the current through R7 and R6 falls, so that the screen of V2 becomes more positive, and the cathode more negative. With no signal, potentiometer VR2 allows the circuit to be balanced so that no voltage is present across the S-Meter. Incoming signals cause the meter reading to rise in proportion to the signal strength. R5 reduces the meter sensitivity to a suitable level.
If a steady signal is present, from a transmission or a signal generator, all i.f.t. or other adjustments can be directed towards obtaining the best meter reading. This also applies to any external adjustments, such as to an aerial tuner or to the aerial: earth system.

## CRYSTAL FILTER

With the i.f.t.'s aligned at 455 kHz , crystal X6 was 454 kHz and X 7 was 456 kHz but it is not necessary that X 6 and X 7 have exactly 2 kHz separation. The specified i.f.t.'s are 465 kHz types but they tune easily to 455 kHz .
If one crystal only is used, and the other replaced by a 15 pF variable phasing capacitor, a sharply resonant peak can be obtained together with a rejection notch which can be moved across the i.f. passband. A filter of this type was described in the December 1971 issue of Practical Wireless and is excellent for c.w. in particular.

The lead from the mixer pin 6, Fig. 2B, to pin 3 of i.f.t.l is screened right up to the i.f.t., otherwise stray coupling round the filter will degrade results.
If an accurately calibrated signal generator is available, set it midway between the crystal frequencies and inject at pin 1 of V2, Fig. 2C, adjusting the


Fig. 2E: Circuit of the b.f.o.l product detector, the addition of this unit to the receiver permitting the reception of c.w. and s.s.b. signals. The frequency of the b.f.o. is variable from the front panel to accommodate upper or lower sideband signals.

## components list

1ST. RF, MIXER/OSCILLATOR (FIG. 2A)
Resistors
R1 $47 \mathrm{k} \Omega 1 \mathrm{~W}$ R3 $33 \mathrm{k} \Omega 1 \mathrm{~W}$ R5 $100 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$
R2 $68 \Omega \frac{1}{2} W$. R4 $39 k \Omega 1 W$ R6 $270 \Omega \frac{1}{4} W$

## Capacitors

C1 $0.01 \mu$ F Disc 350 VW C7 $0.01 \mu$ F Disc 350 VW
$\begin{array}{llll}\text { C2 } & 0.01 \mu \mathrm{FF} \text { Disc } 350 \mathrm{VW} & \mathrm{C8} & 100 \mathrm{pF} \text { SM } \\ \text { C3 } & 470 \mathrm{pF} \text { Mica } & \text { C9 } & 22 \mathrm{pF} \text { SM }\end{array}$
C4 $0.01 \mu$ F Disc 350VW C10 10pF SM
C5 $0.01 \mu$ F Disc 350 VW C11 5pF SM
C6 $0 \cdot 01 \mu \mathrm{FD}$ Disc 350 VW TCI 30 pF trimmer
VC1-2 $2 \times 180 \mathrm{pF}$ (Jackson L2)
VC3 25 pF midget variable (Jackson CB04)
Valves
V1 6BA6 V2 ECH81
Miscellaneous
Valveholders B76 (1) skirted, B9A (1) skirted. Formers (7) see text, Crystals X1-5 Type HC6U (see text) with holders, Bandswitch sections A-H; comprising 4 wafers each 2 pole 6 way. Universal chassis flanged members, $6 \times 2 \mathrm{in}$. (1), $5 \times 2 \mathrm{in}$. (2) (Home Radio).

TUNABLE IF AMPLIFIER (FIG, 2B)
Resistors


Capacitors


VC1-2-3 $3 \times 25 \mathrm{pF}$ (Jackson 003)
Valves
V1 6BA6 V2 ECH81
Inductors
L1 Blue Range 3 L2 Yellow Range 3 L3 Red Range 3 (All Denco, miniature, valve type)
Miscellaneous
Universal chassis flanged members, $5 \times 2 \mathrm{n}$. (2), $4 \times 2 \mathrm{in}$. (2), flat plate $5 \times 4 \mathrm{in}$, (1) (Home Radio). Cabinet $15 \times 9 \times 8 \mathrm{in}$. Type $W$, chassis $13 \times 8 \times 21 \mathrm{in}$. Type K, brackets $4 \times 4 \mathrm{in}$. Type C (2) (H. L. Smith). Dial and drive, Type DL6 and ball drive Type 4511 (Home Radio). If not avallable use combined Jackson dial and drive Type 4103/A.

## FIXED IF AMPLIFIER (FIG. 2C)

Resistors

| R1 $100 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ | R5 3300 $\frac{1}{2} \mathbf{W}$ | R9 1MS ${ }^{\text {c }}$ W |
| :---: | :---: | :---: |
| R2 47ks.1W | R6 22 ks 1 W | R10 1Mn ${ }^{\text {W }} \mathrm{W}$ |
| R3 $68 \Omega \frac{1}{2} \mathrm{~W}$ | R7 100 ${ }^{1} \mathbf{1}$ W | VR1 $2 \mathrm{k} \Omega$ linear WW |
| R4 47kR 1 W | R8 100k ${ }^{1} \frac{1}{2} \mathrm{~W}$ | VR2 500 N WW pre- |

## Capacitors

| C1 | $0 \cdot 25 \mu \mathrm{~F} 350 \mathrm{VW}$ | C6 | $0.05 \mu \mathrm{~F}$ |
| :--- | :--- | :--- | :--- |
| C | $0.1 \mu \mathrm{~F} 350 \mathrm{VW}$ | C | 100 pF mica |
| C3 | $0.05 \mu \mathrm{~F} 350 \mathrm{VW}$ | C8 | 100 pF mica |
| C4 | $0.1 \mu \mathrm{~F} 350 \mathrm{VW}$ | C9 | $0.01 \mu \mathrm{~F} 350 \mathrm{VW}$ |
| C5 | $0.1 \mu \mathrm{~F} 350 \mathrm{VW}$ |  |  |

Valves V1 6BA6 V2 6BA6

## Inductors

IFT1 IFT/11/465CT IFT2 IFT/[1/465
"IFT3 IFT/11/465 (All Denco)

## Miscellaneous

Crystals X6/7 Type HC6U with holders (see text),
Valveholders B7G (2) skirted. Diode D1, OAB1.
Switch $\$ 1 a-d, 4$ pole 3 way wafer switch. $\$$ meter, 1 mA f.s.d.

## AUDIO AMPLIFIER/POWER SUPPLY (FIG. 2D)

Resistors


VR1 $500 \mathrm{k} \Omega \log$. pot. with switch, S1

## Capacitors

| C1 $60 \mu F 6 \mathrm{VW}$ | C5 $0.01 \mu \mathrm{~F} 350 \mathrm{VW}$ |
| :--- | :--- |
| C2 $0.01 \mu \mathrm{~F} 350 \mathrm{VW}$ | C6. $32 \mu \mathrm{FF} 450 \mathrm{VW}$ |
| C3 $32 \mu \mathrm{~F} 350 \mathrm{VW}$ | C7 $8 \mu \mathrm{~F} 450 \mathrm{VW}$ |

C4 $100 \mu \mathrm{~F} 5 \mathrm{VVW}$
Valves
V1 ECL 86 V2 OA2 (150V)

## Miscellaneous

Valveholders B7G (1), B9A (1), Dt-2 silicon rectifiers 800 p.i.v. 1A. Closed circuit jack. Fuse 250 mA and holder. T1, output transformer Type TO46 (Home Radio). T2, mains transformer Parmeko P2931 or similar (Home Radio) see text.

BFOIPRODUCT DETECTOR (FIG. 2E)
Resistors

| R1 | $1 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ | R4 | $1 \mathrm{k} \Omega \mathrm{L} \mathrm{W}$ | R7 | 22kS ${ }^{\text {a }}$ W |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R2 | $47 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ | R5 | 33 ka - 1 W | R8 | 100k $\Omega \frac{1}{2} \mathrm{~W}$ |
| R3 | 100k ${ }^{\frac{1}{2} \mathrm{~W}} \mathrm{~W}$ | R6 | 47kR ${ }^{\text {d }} \mathrm{W}$ | R9 | 7 k |

## Capacitors

C1 100pF
C2 100pF SM
C6 470pF mica
C3 150 pF SM
C4 $0.05 \mu \mathrm{~F} 350 \mathrm{VW}$
C5 $8 \mu \mathrm{~F} 350 \mathrm{VW}$
C7 470pF mica
C9 47pF SM
VC1 15pF variable
Valves
V1 6C4
V2 12AU7

## Miscellaneous

L1, b.f.o: coil (Denco BFO2/465). Valveholders B7G (1), B9A (1).
cores of i.f.t. 3 for best output. Repeat with i.f.t.2, with the signal applied at pin 1 of V1 The signal can then be taken to the second mixer grid and i.f.t. 1 aligned.

Assuming no generator is available, tune in any strong, stable signal. It will probably be found that
there are two responses, one is relatively broad and arises from the i.f.t.'s while the other is sharper and may be much weaker if the i.f.t.'s are not tuned near to the crystal frequencies. Tune the signal in at the sharper response position which places it in the continued on page 738

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From Heath (Gloucester) Ltd has come an excitingly new line of high-performance stereo equipment - the Heathkit 1214 series. You get advanced specifications, fabulous sound reproduction and immaculate design concepts at reasonable prices.
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Kit K/AR-1214 AM/FM Stereo Tuner Amplifier $£ 69.80$. Carr.: 80p.
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> CIRCUIT DIAGRAMS. R1155, B.F.L.N. with values, 50p. R1392, R1475, 30p ea. CT38 50p, Scopes CD518 (CT316), 13a, 1035 Mk. $1 \cdot 2$ \& 3,1049 Mk3 all 50 p ea. Sig Gens TF144G 50 p, TF801a 75p. R4187 Rx circ parts list \& block diagram £1.

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## A. LESTER-RANDS

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The loudhailer with siren described in this article has an output power of 3 to 4 watts on speech and is battery operated by eight 1.5 V cells (U11 or equivalent) providing a total of 12 V . The siren sound can be produced at about the same power output and is pitched at around 250 Hz to achieve maximum carrying range. The loudhailer can be hand held by its pistol grip type handle or can be self standing for use with a detachable microphone (see right). The main hailer on-off button is a rocker type switch mounted on the front of the pistol grip handle. This permits easy intermittent operation when the hailer is hand held but can be used in a continuous 'on' position when the hailer is used self-standing.

## The circuit

This is shown in Fig. 1 and consists of a microphone preamplifier Trl, which drives the PC5+ power amplifier via S1 and the volume control VR1. The siren generator $\operatorname{Tr} 2 / \operatorname{Tr} 3$ is simply a multivibrator


The loudhailer need not be hand held and can be rested as shown with the speaker adjusted to face forwards.
with a charge up circuit (C9/R11) that supplies a slowly increasing potential to the base of Tr3. This introduces a slight rise of pitch as the siren is switched on, resulting in a somewhat distinctive sound. The output of the siren is taken to the PC5 + power amplifier via $S 1$.

The power amplifier provides some 3 to 4 watts of power output to an $8 \Omega$ speaker and is a printed circuit assembly made by Newmarket Transistors. It was chosen because of its small dimensions which,
in turn, permitted the use of a case for the hailer of only $6 \times 4 \times$ 3ins but yet still large enough to accommodate the microphone preamplifier, the siren generator, the battery cells and the power amplifier itself.

Note that the 12V supply has both an on-off switch and the rocker switch (hailer control button) in series to the negative supply rail to the amplifier. The on-off switch is optional but could be used merely as a safety precaution against the rocker switch being left


## components list



Mic/Siren Switch
Siren Switch
Case

Sundries

Newmarket type PC5 +
Eagle type HDA5
Eagle type CM10 (lapel)
Eagle type PJM3
Home Radio WS201/Bulgin SIB825
Miniature slide type
Small toggle type
Home Radio Universal Chassis Parts: CU157(2); CU144 (2); CU146 (2)

Plain circuit board; Aluminium angle; 16 or 18 s .witg. aluminium for pistol grip; Stand-off pillars.
on. The siren button may be a small toggle switch on a press (self release) button type switch. (See components list regarding suitable rocker switch and self release button switch).

## Construction

The $6 \times 4 \times$ 3inch case was constructed from Home Radio Universal Chassis parts (see components list). The loudspeaker is an Eagle type PA speaker

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type HDA5 which is supplied complete with fixing bracket and is mounted on the front end of the case as in Fig. 2a. The rear end of the case is fitted with two aluminium angle pieces as in Fig. 2b which allow the unit to stand evenly when used self-standing. The pistol grip is hollow, being made from aluminium to the dimensions given in Fig. 2a and $b$ and which, in turn, is secured centrally to the underside of the case. The hailer control rocker switch is mounted on the front of the pistol grip as in Fig. 2a.


One of the side panels unscrewed. The components board can be seen clearly while at the extreme fottom is the main amplifier module. One of the battery holders can also be seen; there is another on the other side panel.

The mic/siren switch S1 and the siren control button (or switch) is mounted on the right hand panel of the case (looking from the rear end) whilst the volume control (with integral on-off switch) and


Fig. 4 : The component layout and wiring. The connections to the module are shown on the right.


For operation as a loudhaller, the microphone is fitted to the small clip shown.
microphone socket, are mounted on the left hand panel (looking from rear end). The positions of these components are shown in Figs. 2a and 2c. The microphone used for the prototype was an Eagle lapel type CM10 which is fitted with a screened lead and miniature jack plug and also has a small clip on the back. It can therefore, be clipped onto the rear of the hailer as shown in Fig. 2b. The support for the microphone clip is simply a small brass strip about ${ }^{1}{ }_{4} \mathrm{in}$. wide bolted onto the rear panel but raised about $1_{8}$ in. by spacers. Any small crystal microphone can be used with the loudhailer.

The loudspeaker leads are taken into the case and thence to the amplifier through a hole in the front panel. Before attaching the pistol grip, fit a pair of wires to the rocker switch long enough to go through into the case and thence to a) the on-off switch and b) to tag D on the $\mathrm{PC} 5+$ power amplifier.

The position of the microphone preamplifier and siren generator circuit board is shown in Fig. 3. It is mounted slightly off centre within the case to be clear of the battery boxes when they are in situ. The PC5 + amplifier is mounted as shown in Fig. 3 centrally and at the bottom of the case but is raised up on stand-off pillars by about ${ }^{1}{ }_{2}$ in.

The battery boxes (Eagle type BH411) are mounted one on each side panel (see photograph) and in the positions shown so as to be clear of both the circuit board and power amplifier when the panels are fitted. Changing batteries means only removing each side panel.

Layout and wiring of the circuit board containing the microphone preamplifier and the siren generator is shown in Fig. 4. The plain $0 \cdot 15 \mathrm{in}$. matrix circuit board is mounted on a piece of aluminium angle which, in turn, is secured to the upper panel of the case. Connections to the mic/siren switch S1, the mic socket, the volume control (VR1) and to the power amplifier etc., are all shown in Fig. 4.

## Checking out

Current consumption should be about 10 to 12 mA with no signals and can be checked with a meter in series with the 12 V negative lead from the battery. With the hailer switched to 'mic', adjust the volume control so that no feedback occurs i.e., no howling due to sound from the speaker coming back to the microphone. The supply current should rise to about 100 mA or a little over on speech peaks. With the switch S1 to 'siren', operate the siren button (or switch). The sound should rise slightly in pitch once it starts but if left on will stay at constant pitch. Intermittent use of the siren button should produce a sound with a slight 'whoop' pitched at about 250 Hz (around middle C). The current consumption of the hailer will rise to around 100 mA when the siren is operated.

These tests should be made with the side panels open to ensure that operation is satisfactory. Make sure that when the side panels are fitted (with the battery boxes now inside) that no short circuits occur which is quite possible as there is little space between the circuit board and battery containers etc.

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| $\begin{aligned} & \text { TP } 100 \mathrm{~W} \\ & \text { f14.28 } \\ & \text { Carr. } 45 \text { p } \end{aligned}$ | (illus) 170 W wave into $8 \Omega$. |  | sq. |
| :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { TP } 50 \mathrm{~W} \\ & 69.31 \\ & \text { Carr. } 40 \mathrm{p} \end{aligned}$ | $\begin{aligned} & 90 \mathrm{~W} \\ & \text { into } 8 \Omega \text {. } \end{aligned}$ | sq. | wave |
| $\begin{aligned} & \text { TP } 25 \mathrm{~W} \\ & 67.25 \\ & \text { Carr. } 40 \mathrm{p} \end{aligned}$ | $\begin{aligned} & 40 \mathrm{~W} \text { r.m.s. } \\ & \text { into } 8 \Omega \text {. } \end{aligned}$ | sq. | wave |

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THERE has been no shortage, in recent years, of designs for transistorised transmitters. In the majority of cases, however, the transmitters have been running at inputs of maybe a fraction of a watt. In some cases, modulation appears to have been something of an afterthought. Often, emitter or base modulation has been used in a desperate attempt to obtain the magical $100 \%$ modulation-the reason being, one suspects, that the more familiar high-level modulation has not been found to give the desired results.
The purpose of this article is to try to clear away some of the misconceptions surrounding the transistor power amplifier stage, and to outline the way in which amplitude modulation may most effectively be achieved.

## THE BASIC CIRCUIT

Fig. 1 shows the basic circuit arrangement for valve and transistor p.a. stages. Superficially, the circuits look very similar, but there are some important differences. First, one must remember that, unlike valves, transistors are current-operated devices. This means that there is no point at all in feeding a huge signal into the base of a p.a. transistor in an attempt to run it at high power. All that one is likely to achieve is the destruction of the transistor as the result of excessive reverse base-emitter potential.

What the base really requires is current, and this can only be achieved if the driver stage can supply adequate power at the correct impedance to match into the p.a. This brings us to the second important difference between valve and transistor p.a.'s. Being current devices, the latter operate at much lower input and output impedances, typically under 20 ohms . One must therefore pay careful attention to the problem of matching the transistor accurately to the load it is to feed.

## CLASS C OPERATION

In any Class C p.a. stage, we are basically trying to switch the stage into conduction for only a brief portion (typically $140^{\circ}$ ) of the signal cycle. The resulting burst of current causes the p.a. tank circuit to ring at a frequency determined by the LC of the tuned circuit, the oscillations being fed to the aerial via either a link coupling or some form of pi-network.

In a valve p.a. it is necessary to provide a negative bias on the grid in order to restrict conduction to the desired $140^{\circ}$, but the situation with transistors is (for once!) much simpler as a transistor will not conduct at all in the absence of an input signal. This immediately provides Class $\mathbf{B}$ operation, but there
is a further bonus in that owing to the existence of the base-emitter diode the input signal has to exceed a certain minimum value (approximately 0.6 V for silicon transistors) before conduction begins at all. This is ideal, as it means that Class C operation can be achieved with transistors with no special bias arrangements whatsoever. All we need to do is feed a signal with a positive excursion something in excess of 0.6 V between base and emitter of the p.a., from a driver stage capable of supplying adequate base current to give the desired mean collector current.

As a guide, a well-designed p.a. stage will provide a power gain of up to 17 dB (approximately 15 times). Thus, a 10 watt transmitter running at $70 \%$ efficiency will require a drive power of at least half a watt.


Fig. 1: Circuits Illustrating the similarity in valve and transistor p.a. stages.

## MATCHING

With valve transmitters, it has become almost standard practice to use a pi-network to match the p.a. to a $750 h m$ aerial system. The same principles apply to transistor p.a.'s but owing to the lower impedances involved component values can become somewhat inconvenient at the lower frequencies. For this reason, a tapped p.a. tank coil is often used, as a worked example will illustrate.

Assuming a p.a. efficiency of $70 \%$, the approximate p.a. output impedance can be calculated from:

$$
\mathrm{R}_{\mathrm{pa}}=\frac{\mathrm{V}_{\mathrm{c}}}{2 \mathrm{I}_{\mathrm{c}}} \text { ohms }
$$

where $V_{c}$ is the collector voltage and $I_{c}$ is the collector current.

Thus, a p.a. with a collector voltage of 20 V and a d.c. input of 0.5 A will present an output impedance of

$$
\frac{20}{2 \times 0.5}=20 \mathrm{ohms}
$$

The problem is now one of matching the 200 hm p.a. to the $750 h m$ aerial system. As mentioned earlier, the most suitable technique consists of initially converting the low p.a. impedance to a more convenient value by means of a tapped p.a. coil, and then transforming down to aerial impedance by means of a link coupling. In this way, a reasonable working $Q$ can be obtained with components of a more sensible value than would have been necessary for a pinetwork.


Fig. 2: Typical transistor p.a. stage and the matching problems involved.

The general arrangement is shown in Fig. 2. To establish a starting point in our calculations, we begin by assuming a convenient. value for the tuning capacitor $C$. The value of $L$ is then given in the normal way by:

$$
\mathrm{L}(\mu \mathrm{H})=\frac{25,000}{f^{2} \times \bar{C}}
$$

where $f$ is frequency ( MHz ) and $C$ is tuning capacitance ( pF ).

We next decide on the required operating $Q$. As with valve p.a.'s, this is usually somewhere between 5 and 15 as a compromise between harmonic suppression and tuned circuit loss. Now, $Q$ is given by:

$$
\mathrm{Q}=\frac{\pi \times \mathrm{f} \times \mathrm{C} \times \mathrm{R}}{500,000}
$$

where $R$ is the effective shunt resistance across the tuned circuit. From this, we can obtain an expression for $R$ :

$$
\mathrm{R}=\frac{500,000 \times \mathrm{Q}}{\pi \times \mathrm{f} \times \mathrm{C}} \mathrm{ohms}
$$

Thus, in order to obtain the required operating conditions, the p.a. output resistance must be transformed to look like this shunt resistance $R$.
Example: Suppose our p.a. is to work at 2 MHz and we choose $C=500 \mathrm{pF}$ as a convenient value for the tuning capacitance. Hence,

$$
\mathrm{L}(\mu \mathrm{H})=\frac{25,000}{2^{2} \times 500}=12.5 \mu \mathrm{H}
$$

If we now choose an operating $Q$ of 10 , the effective shunt resistance $R$ will need to be:

$$
\frac{500,000 \times \mathrm{Q}}{\pi \times \mathrm{f} \times \mathrm{C}}=\frac{500,000 \times 10}{\pi \times 2 \times 500}=1,590 \mathrm{ohms}
$$

It is now necessary to determine the turns ratio for the tapped p.a. coil. This is given by:

$$
\frac{\mathrm{n}_{1}}{\mathrm{n}_{2}}=\sqrt{\frac{\mathrm{R}}{\mathrm{R}_{\mathrm{pa}}}}
$$

Thus if in our example 30 turns were required to give the required inductance of $12 \cdot 5 \mu \mathrm{H}, \mathrm{n}_{2}$ could be obtained from:

$$
\frac{30}{\mathrm{n}^{2}}=\sqrt{\frac{1590}{20}}
$$

from which $n_{2}=$ Approx. $3 \mathrm{I}_{2}$ turns.
The number of turns required for the aerial link coupling can now be calculated in a similar manner from:

$$
\frac{\mathrm{n}_{1}}{\mathrm{n}_{3}}=\sqrt{\frac{\mathrm{R}}{\mathrm{R}_{\mathrm{ae}}}}
$$

For a $750 h m$ aerial system, the above example would therefore require a value for $n_{3}$ given by:

$$
\frac{30}{\mathrm{n}_{3}}=\sqrt{\frac{1590}{75}}
$$

from which $n_{3}=$ Approx. $6^{1}$ turns.
It is vital that the p.a. stage be adequately decoupled. This can be accomplished by means of an r.f. choke and decoupling capacitor as shown. The impedance of the choke should be no more than ten to fifteen times the p.a. output impedance, to discourage low frequency parasitics.

## MODULATION

Undoubtedly the best way to modulate a transistor transmitter is by collector modulation of the p.a. and driver stages. The audio power required will be equal to half the p.a. input power; that is, 5 watts for a 10 watt p.a.
'Efficiency' modulation systems modulating emitter or base of the p.a. with only a few milliwatts of audio can give satisfactory results if carefully set up, but even at their best will never have the 'talk-power' of a high-level modulated system. This is a matter of fundamental fact, not of design.

## MODULATOR MATCHING

In order to effectively modulate any p.a., it is essential that it be correctly matched to the modulator. The calculations are very simple. A transistor p.a. with a collector voltage of $V_{0}$ volts and a collector current of $I_{c}$ amperes will present a load to the modulator of $\frac{V_{c}}{I_{c}}$ ohms. If we call this load impedance $R_{p}$ it can be correctly matched to a modulator of output impedance $R_{m}$ by means of a modulation transformer with a turns ratio:

$$
\frac{\mathrm{N}_{1}}{\mathrm{~N}_{2}}=\sqrt{\frac{\mathrm{R}_{\mathrm{p}}}{\mathrm{R}_{\mathrm{m}}}}
$$

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[^2]Example:-Suppose we wish to modulate a p.a. having a collector voltage of 20 volts and a collector current of 0.5 amperes by means of a modulator with an output impedance of 1000 ohms . From the formula, the modulator load $\mathrm{R}_{\mathrm{p}}$ will be

$$
\frac{20}{0 \cdot 5}=40 \mathrm{ohms}
$$

To match this to a modulator output impedance of 1000 ohms , we shall require a modulation transformer with a turns ratio:

$$
\frac{\mathbf{N}_{1}}{\mathbf{N}_{2}}=\sqrt{\frac{40}{1000}}=\frac{1}{5}
$$

i.e. a step-up ratio of $1: 5$ between the p.a. and the modulator. The general arrangement is shown in Fig. 3.


Fig. 3: Circuit showing how the use of formulae given in the text can ensure correct matching between the p.a. and the modulator.

It is not possible, because of internal feedback, to fully modulate a transistor transmitter by means of collector modulation of the p.a. alone. For this reason, it has become established practice for the driver stage also to be collector modulated to a depth best determined by practical tests.

## CHOICE OF TRANSISTORS

This article would not be complete without a brief survey of suitable p.a. transistors available for amateur use at a reasonable cost.

When selecting a type of transistor to meet a particular requirement, there are a number of important parameters to bear in mind.

The first of these is transition frequency $f_{T}$. This is the frequency at which the forward current gain in common emitter mode $\mathrm{h}_{\mathrm{FE}}$ (also known as $\beta$ ) has dropped to unity. But more important, it is also the gain-bandwidth product for the transistor: a transistor with an $f_{T}$ of 200 MHz will have a gain of 100 at 2 MHz and 50 at 4 MHz .

From this one might conclude that one should aim for as high an $f_{T}$ as possible, but in practice this can result in excessive low-frequency gain and consequent instability. It is therefore best to select a transistor with an $f_{T}$ no more than ten to fifteen times higher than the proposed operating frequency.

Another important transistor parameter is its total dissipation $P_{\text {tot. }}$ A Class $C$ p.a. stage is generally no more than 70 per cent efficient, the remaining 30 per cent of input power is wasted as heat which must be adequately dissipated by the transistor and its heat sink if the device is to remain within the temperature limits stipulated by the manufacturer.

Finally, it tends to be expensive to pay too little attention to the manufacturer's 'absolute maximum' voltage and current ratings (the writer speaks from rueful experience!). A p.a. fed from a 12 volt supply will have a peak r.f. voltage on its collector of up to 24 volts on c.w. and up to 48 volts on a.m. A valve p.a. will withstand a fair degree of overload without complaining, but the risk is not worth taking with transistors. It is therefore good sense to choose a transistor with a collector-emitter voltage rating at least three times the proposed supply voltage for c.w. and at least six times the proposed supply voltage for a.m.

A list of readily available transistors suitable for amateur p.a. use is given in the accompanying table.

| $\begin{aligned} & P_{\text {tot }} \\ & (\mathrm{W}) \end{aligned}$ |  | $\stackrel{f_{\top}}{(M H z)}$ | $\begin{aligned} & V_{\text {Свм }} \\ & (V) \end{aligned}$ | $\begin{aligned} & V_{\text {CEM }} \\ & (V) \end{aligned}$ | $\begin{aligned} & I_{C M} \\ & (A) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 2N1893 <br> 2N1613 <br> 2N1711 | $\begin{aligned} & 50 \\ & 60 \\ & 70 \end{aligned}$ | $\begin{array}{r} 120 \\ 75 \\ 75 \end{array}$ | $\begin{aligned} & 80 \\ & 30 \\ & 30 \end{aligned}$ | 0.5 0.5 0.5 |
| 4 | 2N4030 2N4031 2N4032 2N4033 | $\begin{aligned} & 100 \\ & 100 \\ & 150 \\ & 150 \end{aligned}$ | $\begin{aligned} & -60 \\ & -80 \\ & -60 \\ & -80 \end{aligned}$ | $\begin{aligned} & -60 \\ & -80 \\ & -60 \\ & -80 \end{aligned}$ | 1.0 1.0 1.0 1.0 |
| 5 | 2N3053 BSY81 BSY83 BSY85 BSY84 BSY82 BSY86 2N3866 | $\begin{aligned} & 100 \\ & 100 \\ & 100 \\ & 110 \\ & 120 \\ & 120 \\ & 130 \\ & 700 \end{aligned}$ | $\begin{array}{r} 60 \\ 40 \\ 80 \\ 120 \\ 80 \\ 40 \\ 120 \\ 55 \end{array}$ | $\begin{aligned} & 40 \\ & 18 \\ & 35 \\ & 64 \\ & 35 \\ & 18 \\ & 64 \\ & 30 \end{aligned}$ | $\begin{aligned} & 0.7 \\ & 1.0 \\ & 1.0 \\ & 1.0 \\ & 1.0 \\ & 1.0 \\ & 1.0 \\ & 0.4 \end{aligned}$ |
| 11-5 | BD106A <br> BD106B <br> BD106C <br> BD106D | $\begin{aligned} & 100 \\ & 100 \\ & 100 \\ & 100 \end{aligned}$ | $\begin{aligned} & 36 \\ & 36 \\ & 64 \\ & 64 \end{aligned}$ | $\begin{aligned} & 36 \\ & 36 \\ & 64 \\ & 64 \end{aligned}$ | $\begin{aligned} & 2 \cdot 5 \\ & 2.5 \\ & 2.5 \\ & 2.5 \end{aligned}$ |
| 15 | BD124 | 60 | 70 | 45 | $4 \cdot 0$ |
| 45 | $\begin{aligned} & \text { BD123 } \\ & \text { BD121 } \end{aligned}$ | $\begin{aligned} & 85 \\ & 95 \end{aligned}$ | $\begin{aligned} & 90 \\ & 60 \end{aligned}$ | $\begin{aligned} & 60 \\ & 35 \end{aligned}$ | $\begin{aligned} & 5.0 \\ & 5.0 \end{aligned}$ |

## CONCLUSIONS

The writer concludes with a few recommendations which are the outcome of considerable experimentation and not a few traumatic experiences.

DO... bring up the voltage and drive to a transistor p.a. gradually to avoid any possible overloads.
DO . . . use single point earthing.
DO . . . keep leads short. There are high circulating currents in a transistor p.a. and stray inductance from over-long leads can ruin performance.
DO NOT . . . over-drive a transistor p.a. with voltage.
DO NOT . . . forget to decouple the stage properly.
DO NOT . . . run the p.a. even slightly off-tune or without a proper load.

## A series of simple transistor projects, each using less than twenty components and costing less than one pound to build.

THERE are several occasions when audio signals have to be mixed; public address systems frequently have several sources such as a microphone, tape recorder and record player and of course pop groups need an audio mixing facility to bring all the sources together before feeding the main amplifier. Some audio mixers are very complex and sophisticated in that they will handle signals varying from the tiny output from a tape head to more than half a volt produced by a crystal pickup and, as well as providing a mixing system, they equalise the inputs. It is more common however that the signals needing to be added together are of roughly the same level and to mix these is fairly simple as can be seen from the circuit in Fig. 1.

This circuit has facilities for three inputs, two medium level and one high level. One important feature of a mixer is that the level of each of the sources can be controlled individually and so a potentiometer is needed for each. If we simply connected the sliders of the pots together there would be considerable interaction between them. For instance, if one of the pots was set at minimum the slider would be at virtually chassis potential and thus the wanted signals would also be shorted. This interaction can be reduced to negligible proportions by inserting a resistor in series with each slider before taking them all to a common point; in our circuit these are represented by R2, R3 and R4.

The adding of the signals in this way does, however, cut down the level considerably, so much so that the combined signals need amplifying to recover the level and so Tr 1 is necessary. In fact this not only recovers the gain but amplifies the signal by about 20 times.

The high level input is that marked in Fig. 1 as $\mathbf{A}$ and this will handle signals of more than 1 V without causing distortion. The signal available across VR1 is only one seventh that of the input using the $68 \mathrm{k} \Omega$ resistor shown but the value of R 1 can be altered to suit the particular requirements. Inputs $\mathbf{B}$ and $\mathbf{C}$ do not have any initial attenuation and will handle signals up to about 150 mV without trouble. For this input the output is nearly 3 V which is more than sufficient and in most cases will be far too much; few amplifiers need more than 600 mV . Working backwards, we shall then find that this amplifier stage will give 600 mV out for inputs of 30 mV . There is no minimum level at which it will work and signals of 1 mV could be mixed, though of course the output would then be only about 20 mV .

Three inputs have been shown but the final number is up to the constructor. Only two may be required, in which case one can be left out but several more can be added simply by duplicating Input $A$ or or one of the others.

No separate power supply is shown as the mixer will usually be powered from the main amplifier


Fig. 1 : Circuit of the audio mixer providing for three inputs.


Fig. 2: A suggested component layout; no breaks in the conductor strips are necessary.

## components list

Prices are those recently advertised and may have changed. No allowance is made for minimum order costs or for postage and packing and these points should be checked carefully before ordering:
but it will work from a 9 V battery and, since the current drain is tiny, a PP3 type may be used.

The components may be built in any convenient form but for those using Veroboard a layout diagram is shown in Fig. 2; no breaks are necessary in the conductor strips.

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Convenient to use? Just connect a capacitor, select the right scale and press the button.
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## ALL IN THE JANUARY ISSUE ON SALE 1st. DECEMBER



Full size pattern of the p.c. board layout. This drawing may be cut out for those wishing to make their own boards; as this page backs onto details of next month's features, your copy will not be spoilt.


THE Music Maker electronic organ was originally conceived as a toy for the author's young daughter but, after the rigours of field trials of the kind that young children seem to be so well endowed to inflict, it was realised that the organ was more than just a toy.

It turned out to be a very robust and reliable musical instrument, very simple to construct and economic in both manufacture and battery consumption.

The complete instrument is housed in a plastic sandwich box, measuring $6^{7}{ }^{7}$ in. $\times 4^{5}{ }_{8} \mathrm{in}$. $\times 1^{5}{ }_{8} \mathrm{in}$. of the type offered for sale in most large chain stores for just a few pence. For those who are unable to obtain this, special arrangements have been made for the supply of this; see overleaf.

The organ is monophonic and played with a probe on a printed circuit keyboard laid out in conventional manner. The keyboard covers two full octaves, centred around middle C, including sharps and flats and gives sufficient notation to play almost any tune.

The notes, although not exactly the correct frequencies are close enough to pass the scrutiny of all but the trained musical ear. The accuracy of the notes was checked on a frequency meter and errors of no more than 10 Hz were found in the worst case.

The organ may be built without the tremolo circuit, if even greater simplicity is desired, but it is a very worthwhile addition.

## circuit description

The circuit diagram is shown in Fig. 1. The notes are generated by a relaxation oscillator $\operatorname{Tr} 1$ which is a unijunction transistor. The frequency of the notes is determined by C1 and R7 to R30. Tr2 is a simple audio amplifier feeding the output pair $\operatorname{Tr} 3$ and $\operatorname{Tr} 4$.

## * components list



The output stage has not been designed for quality but cross-over distortion is not important. The prime consideration here is low battery consumption. The quiescent current is only a few milliamps, giving long battery life.
The circuit diagram for the tremolo oscillator is shown enclosed on the circuit diagram. It consists of a simple oscillator working on the principle that a $180^{\circ}$ phase change occurs through the feedback capacitors C8 to C10, applying positive feedback from the collector to the base of Tr5, thus forming a low frequency oscillator.

The output of the tremolo circuit is mixed with the output of the note generator at the base of $\operatorname{Tr} 2$ when the switch SW2 is made.

The output power is quite sufficient to allow the organ to be heard in an average sized room and no volume control was considered necessary.

## circuit board construction

The printed circuit board is shown full-size on page 716. (For those not wishing to make their own boards, arrangements have been made for the supply of these.) Firstly, the board is cut to size and the corners shaped to fit the case. After checking that the board will fit the case easily, it is then etched and drilled. The components are then soldered in, starting from R1, C1 and Tr1 and progressively through each component shown on the circuit diagram as far as the loudspeaker.

Many small transistor speakers have a 6BA tapped hole in the permanent magnet keep at the back of the cone. The speaker may be fixed to the printed circuit board by a 6BA bolt, screwed into this hole. If the speaker does not have this hole, the magnet
can be glued to the board.
At this stage the circuit may be tested by injecting an audio frequency signal at C 4 (to prove the output stage) and C3 (to prove the audio amp.). If everything is satisfactory, the audio signal will be heard clearly from the speaker.

The relaxation oscillator may be tested by temporarily connecting a $15 \mathrm{k} \Omega$ resistor from the ' e ' of $\operatorname{Tr} 1$ to the positive rail and a note should be heard from the speaker. The keyboard components R7 to R30 and VR1 may then be fitted and the scales tried.
It should be mentioned at this stage that the values of some of the resistors R7 to R29 are not normal 10 per cent preferred values, but are 5 per cent or better types and the closer one adheres to the values stated, the closer the notes will be to the desired frequency. Since some of these values fall in the less common E24 series, special arrangements have been made to supply a kit of the scale resistors.
It was found, on the prototype, that the keyboard


Fig. 2: The component layout on the p.c. board. This is viewed from the components side.


A vew of the completed prototype.
must be polished with metal polish before playing because once the surface becomes tarnished the notes change, due to the increased resistance of the copper oxide coating. Several alternatives are possible, either the keyboard may be silver plated or, if the constructor is a soldering expert, the keyboard may be tinned. The ready-made p.c. board which is available is already tinned.

## case construction

Next the case is cut as shown in Fig. 3. The best method of cutting the case is with the tip of a hot soldering iron, keeping well within the actual line of cut to allow for the shrinking effect as the plastic melts. After cutting, the edges should be cleaned up with a sharp penknife and finally sandpapered to a clean edge.

It is recommended that the speaker hole be cut first so that the constructor may get some practice before attempting the more difficult keyboard slot.

The printed circuit board fixing bolts are put through the case next, and held by means of nuts inside. The speaker hole can be covered with cloth fret and the case may be covered with Vinyl or similar decorative covering. The printed circuit board is then placed inside and fitted on the mounting screws.
The switches SW1 and SW2 may then be fixed



Inside of the case showing the hole for one of the switches and the mount/ng screws for the p.c. board.


The case used for the prototype-the black escutcheon can be made from cardboard covered with black, self-adhesive plastic.
and the probe lead passed through the hole in the case and the probe connected. The author used a telephone jack plug for the probe, but it may be made from a variety of items.

Finally the battery is fitted and the probe is held on. middle C. VR1 should then be adjusted until the note corresponds to the correct sound; the rest of the notes should then be correct. If R7 to R29 are replaced by skeleton presets, then all the notes will have to be tuned individually, starting with the highest one because the tuning of the higher notes will upset the ones below it.

# practicially Wireess commentary by IELIII 

HAVE you ever suffered from mice in your bottom drawer, moths in the cambric and half the local pigeon population perching on your aerial?

You have my sympathy. You can even have my telephone number if you require a quick consultancy service in getting rid of birdies on the f.m. band, rumbles on your autochanger or the depredations of the dreaded alum-worm in your electrolytics.

Some things never age. And Henry is convinced by recent experiences that the problems and vicissitudes of servicing will never change, whatever the 'tomorrow men' may predict about modules, and multi-chips, or 'potent ethos determinants'. I do not need to invent these terms. The foregoing is a quote from Jonothan Benthall's review of Science and Technology in Art Today, by Brian Porter.

I remember the intense castigation I received when, as a humble field engineer, I dared to contribute to print the criticism of the first ever 'module-type' television receiver. The several printed circuit boards, according to the maker, would be supplied as immediate replacement spares, and no on-the-spot servicing would be needed.

Henry predicted that engineers would soon circumvent the system


Mice in your bottom drawer.
by their innate curiosity. They would find that certain components caused common faults and find it as easy to change these as nip back to the workshop for a new PC board. Which, in the event, is precisely as happened. In no time at all, the prevalence of common faults had caused a shortage of those printed circuit panels where the troubles most often took effect. And most of the problems we had with that particular set and its immediate successors were not with the printed circuit boards at all, but externals like volume controls.

Henry cannot share Mr. Benthall's regard of computer technology as art, but begins to see what he means when he describes the relevance of error factors. So much art is accidental: so much science is an inspired leap of one step after a determined plod up five hundred. So many of the radio receivers we have seen come off the production lines-computer controlled?-bear the marks of artistic error. Servicing them calls for some of the inspiration of the artist.

The psychology of service comes into it when you have to tackle those strange innovations under the critical gaze of the owner. A discreet tap with the hammer is not to be recommended, and a fierce tug in unstrategic places can result in two separate halves with a. mass of disconnected wires. Instead, one holds it wisely to one's ear, give a twiddle to any visible knobs, shakes it gently, frowns and declares: 'Rather tricky I'm afraid. This is a bench job.'

Depending on his previous experience and the snobbery of modern tech-owning, the reception by the owner of this advice will either be a glow of selfimportance or the suspicion of price-rigging. Trouble is, these contretemps are inevitable. No service engineer can keep up with


A fierce tug in strategic places...
all the models, nor even all the advances in general trends of technology. And as for the horror of having to order spares-this is where the psychology of service really sorts the professional from the chap round the corner who dabbles in wireless-and who will probably, eventually, do a much better job.

Here, again, the computer has taken over. The philosophy of the pro is to replace C195 with part number XV5600071008 as recommended in the service manual. He is not concerned that C195 is a 1 KpF ceramic, available from umpteen makers and a dozen surplus factors under a multitude of names. Superset Ltd., say item XYZ , so that is what he orders, and the receiver sits on the shelf while the part is airlifted from Japan.

But computers are almost human. In fact, take a quote from Benthall's last few lines in the computer section of his book:
'So far, the constraints of working with the computer so dominate anything done with it that they actually appear to oppose the advances of the artist. It is as if the computer were some creature of great sexual attractiveness whose actual anatomy remains elusive, frigid and unexplored.' Henry felt that way when they invented tights. But that's another story . . . !

## Organised by Practical Wireless and Heath (Gloucester) Ltd.

In this free competition you have two opportunities of winning a Heathkit 3in. portable oscilloscope kit! Our exciting competition will be repeated in the January issue of Practical Wireless, so save this month's coupon until next month's appears and post your two different attempts in the same envelope.
The Heathkit General Purpose Oscilloscope Kit K/OS-2 is a dependable, well-rated design, ideal for the hobby constructor. The small size and light weight make it ideal for the 'shack' while the wide range of facilities make it extremely versatile.
The low price of $£ 29 \cdot 50$ for the kit plus 80 p postage and packing (when ordered direct from the Gloucester factory) is an added attraction and of course, coming from Heathkit, the instructions for both assembly and operation are clear and precise, leaving nothing to chance. Even if you already own a 'scope, the OS-2 makes an excellent portable, back-up unit. Just consider the specification: $Y$ Bandwidth from 2 Hz to 3 MHz ; Time base $20 \mathrm{~Hz}-200 \mathrm{kHz}$ Automatic sync; P.C. board construction; small size, 12in $\times 7 \frac{3}{3}$ in $x$ 5in; Switched ext/int Y plate connections; Sensitivity 250 mV peak-to-peak per cm .

## HON TO ENTER:

Listed below are eight important features of the Heathkit OS-2 oscilloscope. All you have to do is place them in what you consider to be their order of importance to the average Practical Wireless reader. For example, if you think Portability is most important of all, write D in the box marked 1st on your entry coupon. The key letter of your second choice goes into the box marked 2nd, and so on for all eight. Complete the coupon, all in ink or ball-point pen, with your full name and address, then post in a sealed envelope to: PRACTICAL WIRELESS 'SCOPE COMPETITION, 16 GARRICK STREET, LONDON WC2E $9 P R$ to arrive not later than Wednesday, February 14th, 1973, the closing date. REMEMBER : The competition will be repeated next month, so you can keep the first coupon until then, if you wish, and send both attempts together.


## Scopes

 to be Won!
## RULES



There is no entry fee, but each attempt must be fully completed in ink on the proper printed coupon cut from Practical Wireless, and bear the entrant's own full name and address.
Every accepted entry will be examined and the prizes, as described, will be awarded to the ten entrants who, in the opinion of an expert panel of judges, and in any one attempt, have shown the most skill and judgment in listing the eight features in order of importance.
In the event of a tie or ties for any of the prizes, a further eliminating test will be conducted by post between the tying competitors to determine such winners.

Any entry which does not comply with the printed instructions or is received after the closing date will be disqualified, as wIII any received mutilated or illegible, incomplete, bearing alterations, or with more than one key letter in each space. No responsibility will be accepted for entries lost or delayed in the post or otherwise.
The judges' decision, and that of the Editor of Practical Wireless in all other matters affecting the competition, is final and legally binding. No correspondence can be entered into.

The competition is open to all readers in Great Britain, Northern Ireland, and the Channel Isles except employees (and their families) of IPC'Magazines, the printers of Practical Wireless, and Heath (Gloucester) Ltd., all of whom are ineligible.

The winners will be notified, and the result announced in the earliest possible issue of this magazine.



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IN general, anyone whose interest in electronics begins with radio and communications is inclined to think primarily in those terms, maybe extended a little to cover audio and data processing. All else tends to be dismissed as electrical engineering. It is similar with integrated circuits. Application to radio, TV and computers is just about the limit. It comes as something of a surprise, then, to be dealing with an integrated circuit-even if it is a thick film hybrid-designed for power control at ratings of up to 2.5 kW ., and operating off the mains. That, however, happens to be our topic for this month, the Hyreg type AR1 power regulator, manufactured by Westinghouse and available from Best Electronics (Slough) Ltd., of Michaelmas House, Salt Hill, Bath Road, Slough, Bucks.

## Applications

Applications may be domestic-to regulate an electric heater or keep a kettle just on the boil; to dim the lights for an evening at home or for the local hall when films are on, or a show is presented; to set the speed of an electric drill; anywhere, in fact, where it would be an advantage to control a high powered device with the same convenience as the volume of a radio. It will by now be clear that silicon controlled rectifiers are involved, or to be more precise, a triac, consisting of two s.c.r.'s with a common gate for triggering conduction, and capable of use on a.c. circuits.
It will be remembered by those who have followed this column for a long time that the application of triacs was discussed once before, when the very useful G.E.(USA.) range of triggering circuits was


A potentiometer is all that is required for full power control.
featured. In the present case, however, the triac itself, together with the triggering components, is incorporated in the hybrid assembly. All these items are then bonded to a ceramic substrate of high thermal conductivity and electrical resistivity. The assembly is potted in epoxy, with the ceramic in good thermal contact with a metal base plate.
In use, only three external components are required, and if the load is purely resistive, such as tungsten lighting or a kettle or bar-type electric heater, this can be reduced to one, a variable resistor, as shown. The unit is mounted on a heat sink with thermal contact established with the metal base plate of the regulator. Due to the properties of the ceramic, however, this plate and the attached heat sink are fuily insulated and protected.

It is suggested, however, that the variable resistor should be of the type with a plastic operating spindle, or a solid plastic knob used, for safety in the case of component failure, or accidental reversal of the connections to the mains. The fraction of the power dissipated in the load compared with that drawn directly from the mains is linearly dependent on the setting of the variable resistor. For zero resistance, the power delivered to the load is $100 \%$ dropping to zero when the resistance rises to some $800 \mathrm{k} \Omega$. It is clear, therefore, that if the application is for lighting, for example, a $1 \mathrm{M} \Omega$ linear variable resistance will control the illumination, from total darkness to full power.

One cautionary note must be sounded, however, about devices employing small a.c. motors. Most such motors, including those generally used to drive cooling fans, are of the induction or squirrel cage type. Such synchronous motors operate at a single speed or not at all. It follows therefore that it is impossible to regulate the speed of such motors with a triac device. Rather, at a particular point such a motor simply stops; and as the operating temperature of the motor, or of other components, if it is driving a fan, will then rapidly rise, damage may result. If it is intended to use this device in a system incorporatting an electric motor, first check that the motor is of the type using brushes, i.e. non-synchronous. If used with a fan heater, for example, ensure that the fan receives the full mains voltage at all times, while the regulator controls only the power dissipated in the heating element.

The AR1/250-10 (250V r.m.s. 10A r.m.s.) costs $£ 5 \cdot 87$ inc. $p / p$ with present delivery of 6 to 8 weeks.

HAVE you ever wanted to find out the value of an unmarked capacitor or wondered which was the primary and secondary of a transformer?
The value of a resistor can often be found easily by using a multimeter but how many of us possess one which can accurately measure $1 \Omega$ or, at the other extreme, $2 \mathrm{M} \Omega$ ? Capacitors are less easy to measure and an a.c. source is usually required and, the world being the way it is, capacitors tend to have their values erased more easily than most components. Inductors present another problem;

## UNIVERSAL BAIDGE

HALVOR MOORSHEAD
granted that this facility is rarely required for most of us but when you have to know, what do you do?
The Wheatstone Bridge is the answer; it will rapidly give answers to all the above. In the circuit used here, the values of the components can be read directly off the scale.

## THE THEORY

Look at the circuit arrangement in Fig. 1. An audio note (at any reasonable level and frequency, it doesn't affect the operation) is applied across the network made up from VR1, Ca and Cb with headphones connected between the slider of VR1 and the common junction of the capacitors.

Assume that Ca and Cb are of the same value; they will then each have the same reactarice at the audio frequency and therefore the signal level between E and F will be half that between E and D .

If the slider of VR1 is at its central position, then the resistance A-B will equal that between B-C and half the applied voltage will appear at the slider. Thus the signal level at B and F are the same: what will be heard in the phones? Nothing of course; since there is no voltage difference across them, no current can flow and so they remain silent. In this state, the Bridge, for that is what this network is called, is in balance and the null position has been achieved.
If the slider of VR1 is at any other position there will be a voltage difference and an audio note will be heard in the phones.


Fig. 1: The Wheatstone Bridge which forms the basis of this project. A full explanation of the theory is given in the text.


Now if Cb is one tenth the value of Ca , its reactance will be ten times greater and we shall only get a null when the resistance B-C is ten times greater than A-B. If we make Ca a standard, we shall obviously be able to find out the value of Cb as long as we know the relationship between the two parts of the track of VR1.

We have dealt with capacitors but the same applies to resistors and inductors with only one difference. The reactance of both of these is directly proportional to their values-in other words the higher their value, the more resistance they exhibit. With capacitors the reverse is true, the higher the value, the lower the reactance and so two scales are needed for the pot, one a mirror image of the other.

## THE CIRCUIT

To operate the bridge we require an audio source, a set of standards and also something to detect the null. Headphones are pretty good but they have to be quite sensitive to detect the setting of VR1 which corresponds to the maximum null and so an amplifier is used. In addition to feeding headphones, a cheap meter is also used which will give a visual rather than an audible indication.

The complete circuit is shown in Fig. 2. The audio frequency generator to drive the bridge is represented by Trl and the associated components. This is a phase-shift oscillator which provides a pretty good sine wave. R1 and R2 provide the base bias while C2, C3 and C4 together with R3 and R4 take part of the signal from the collector and invert it by $180^{\circ}$, converting it from a negative to a positive feedback and thus sustaining oscillation. As we have already mentioned, the actual frequency of operation is not important but the values given operate at about 700 Hz . This frequency can be altered slightly by modifying the value of R4 but only by plus or minus 50 per cent $(4 \cdot 7 \mathrm{k} \Omega$ to $15 \mathrm{k} \Omega)$. A transformer is included in the collector of Trl; this is a transistor output transformer type LT700 which is widely available. This has a tap on the primary but this is not required for our purposes. The metal case of the transformer should be connected to the negative line. The secondary of $T 1$ drives the bridge and it will be seen that this part of the circuit is isolated


Fig. 2 : Complete circuit of the Universal Bridge; the accuracy of the finished unit will depend on the tolerance of the standards and the care taken in calibration.

## TEST VOLTAGES

|  | Emitter | Base | Collector |
| :---: | :---: | :---: | :---: |
|  | Tr1 | 0 V | 0.5 V |
| Tr2 | 0 V | 0.25 V | 7.5 V |
| Tr3 | 1 V | 1.2 V | 3.2 V |

Note: Measured on Avo 8 ( 20,000 ohms per volt) on 10 V range, battery voltage on load reading 8.5 V . The above voltages should only be regarded as a guide.
from the audio oscillator. Two low value resistors are shown wired in series with the secondary; these do not really affect the circuit but prevent a complete short-circuit of the secondary if very low value resistance components need to be compared. If the secondary is short-circuited, the oscillator may cease to function.

The bridge potentiometer is represented by VRI which has its slider taken to the negative line. This pot should be a high quality component and should of course have a linear track. A wire-wound component is to be preferred although not essential (the prototype shown uses a staridard carbon track pot).

The standard components in the bridge circuit are represented by R7-R10, C5-C8 and L1, L2; these are selected by SW1. SW1 is also able to select an external pair of terminals (marked $Y$ ) for matching purposes.

The component to be measured on the bridge is connected across the terminals marked X.

The audio signal, indicating an imbalance in the bridge, will appear between chassis and the junction of the standard and unknown component and a d.c. blocking capacitor C9 takes this output to the amplifier. R11 is included to minimise the loading that the amplifier presents to the bridge. Cl0 bypasses any high frequencies to chassis and is necessary to prevent r.f. pickup since the amplifier has a very high gain.

The amplifier stage is made up from $\operatorname{Tr} 2$ and $\operatorname{Tr} 3$ with their associated components and is a fairly conventional arrangement. The use of BC109 transistors ensures considerable amplification of the input. The bias for $\operatorname{Tr} 2$ base is provided from the emitter of Tr3; this helps to stabilise the circuit and also takes up any variation in the parameters of the

## components list

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## transistors.

The amplified audio signal appears at the collector of $\operatorname{Tr} 3$ and is connected via C12 to the headphone socket. Any type of phones can be connected to this
point-even the low $8 \Omega$ types that are now common; the effect on the meter part of the circuit is marginal. The output is also connected to the meter circuit through C13 which rectifies the a.f. and applies it to the meter. D1 provides the d.c bias necessary for correct operation of D2. Since the variation of signal strength applied to this circuit is far more than any meter could sensibly handle, a sensitivity control is fitted. This is simply a variable resistor in series with the meter M1.

When the audio signal is at minimum, the meter will be showing the minimum reading and since we are not interested in calibration, only in noting the minimum deffection, a very simple and inexpensive meter may be used here. The most suitable type is a recording level meter; these come in a variety of shapes and sizes but most have a sensitivity of about $200 \mu \mathrm{~A}$ and cost between 50 p and $£ 1$. Suitable types are listed in the catalogues of the large mail order component suppliers.

The current drain of the prototype was measured at about 10 mA and a PP3 or PP6 type battery may be used; the low consumption should ensure a long battery life.

SW2 is a separate on-off switch and C1 decouples the positive line. The table shows the transistor voltages measured on the prototype; these may be of help if difficulty is experienced in getting the circuit to operate.

## CONSTRUCTION

The circuit can, of course, be built into any type of case but the one chosen for the prototype is a very convenient size and looks very attractive. The main body of the case is made from thick plastic and the front panel from aluminium with mounting screws provided. An internal chassis is also provided but this is not required for our purposes. Bearing in mind the attractive appearance of the case the price, $£ 1 \cdot 25$, is not expensive; details of the supplier are given in the components list. All the components are fitted to the front panel and the drilling and cutting of this is shown in Fig. 3. The front panel is supplied


Fig. 3: The front panel, which is supplied with the case, should be drilled and cut as shown.


Fig. 4: The majority of the components are mounted on a small piece of Veroboard as shown. Certain of the conductor strips should be broken.
with a protective plastic sheet and this is best left on while the marking is done to prevent scratching but it should be removed before the actual drilling starts. The meter cut out is shown for the type used in the prototype but other types may vary and so this dimension may have to be worked out separately. The holes are of two diameters, ${ }_{8}$ in and ${ }^{1} 4$ in. Two holes are not shown on this diagram: these are for the component board mounting bracket. These are best sited to suit the type of bracket used; they will lie to the right of the VR1 hole.

The majority of the components are fitted to a piece of Veroboard with a 0.15 in . matrix. The layout for this is shown in Fig. 4. Three chassis and two positive lines are used, these are connected by link


All the components are mounted on the front panel. The wiring, especially around VR1, should be short and straight.
wires as shown. The transformer T1 is fitted with two tabs which are rather larger than the holes in the board, but by slightly enlarging these with a drill the tabs may be pushed through the board and on one side bent over and soldered to the adjacent strip. The upper tag should be soldered to the upper strip. It is important that both sides are soldered to the correct strip as the upper strip must be at chassis potential for the connection for Cl . Take-off pins are connected at various points, these are marked A-G and correspond with similar letters in Fig. 5.

Several breaks are necessary in the copper conductor strip but these are clearly shown in the diagram.

Figure 5 shows the remaining wiring. The component board should be fitted to an ahminium angle bracket which in turn should be fitted to the front panel. A solder tag can be fitted under one of these mounting screws to act as the main chassis connection.
The standard components are wired directly to the switch SW1 and a common wire connects one side of these together; the photograph should make this clear.
To minimise the capacity of the wiring, all connections from and to SW1 and VR1 should be as short as possible and good stout wire should be used; it may look less attractive but will improve the performance of the unit.
The only component not on the front panel is the battery. This fits into the main body of the case and should be held in some form of clip to prevent it moving around.


Using the recommended case, and taking care over the labelling of the controls, the finished unit can look quite professional.

## CHOIGE OF STANDARDS

The accuracy of the unit depends on two factors: the quality of the standards and the care taken in calibration. One per cent resistors are available although they are hard to find. Two per cent types are not all that expensive and should be quite adequate; Home Radio list these in their catalogue at 5 p each. One per cent capacitors are available from a number of suppliers including Electrovalue Ltd., though C9, $10 \mu \mathrm{~F}$, costs a small fortune in this tolerance. However, it is highly unlikely that high accuracy is needed on this range.


Close-up of the reference components showing how these are wired directly to the switch.


Fig. 5: Wiring of the controls. The letters match up with those on the main component board.


Fig. 6: This scale may be cut out and calibrated as described in the text.

The inductors chosen for the circuit are a matter of choice. The author only included two in the prototype, a 10 mH and a $100 \mu \mathrm{H}$. Arrangements have been made with Repanco Ltd., for the supply of these 5 per cent tolerance inductors, details are given in the components list. This will allow measurement within reasonable accuracy of inductors lying within the range 1 mH to $10 \mu \mathrm{H}$. Lower inductances can be measured but the accuracy below this must be suspect because of strays in the circuit.

The matter of standards must be left up to the reader. Many people may be content using 5 per cent components throughout and certainly little usefulness will be lost.

## CALIBRATION

A blank calibration scale is shown in Fig. 6. This can be cut out and stuck onto the front panel, the null position is already marked. For calibration a source of close tolerance components is required and the remarks made above apply. However, as we are only interested in one set of markings, this can be done using the cheapest components-resistors. The best range on which to calibrate is probably the $1 \mathrm{k} \Omega$ one and a set of resistors with their values ranging between $100 \Omega$ and $10 \mathrm{k} \Omega$ will be needed. Points can be obtained by interpolation if only a few components are used. Alternatively, if a highly accurate test meter is available (one with an individually calibrated scale) a variable resistor can be adjusted on this and then used for the calibration. There are several ways of approaching this problem and the above points are only a guide. However, once calibrated, the scale will hold good for all values of resistance, capacitance and inductance as long as the standards are accurate.

For matching two components the internal standards are not used. The two components are fitted to X and Y and their similarity compared, if they are the same the null will appear at the $1: 1$ setting right at the top.

"I think it needs a plug change and its valves ground in!"


SOMETIME back, comment was made in this column about miniature lasers. Some will have wondered about the applications of these devices while others, perhaps, even doubted the existence of such midget marvels.

It will be of interest, therefore, that small lasers are available in this country from a company in Edgware. These are colourfully described as "Hip Pocket He-Ne Lasers". Ratings of one, three and 10 mW are available and the power supply allows operation from 230 V a.c. or 12 V d.c. Dare our imagination picture a man from Mars reaching for the "sky" on the commands of a Space Sheriff on whose hip hangs a 45MW laser? Jesse James would turn in his grave!

Before anyone ridicules the laser as just a novelty, they should consider the latest application by the Dutch electronics giant Philips. The Eindhoven laboratories use one in their latest system of video recording.
The reflection from a minute spot of light generated by a miniature laser is used to obtain a signal from a video LP. A 45 minute colour television programme can be recorded on a normal LP sized disc. This amounts to something like recording 50,000 separate frames or individual pictures.

Since there is no direct physical contact with the pick-up head, wear is almost non existent. However, one sees scratches as a problem and, more importantly, dust and/or dirt in the groove will throw up as noise in the system.

New electronic products flood the market every week. From amongst the current list is an interesting new IC. It is believed to be the first IC timer commercially available. Designated the 555 its applications include a timer which will cover intervals from fractions of a second to one hour, frequency divider, frequency modulator and missing pulse detector.

Another interesting newcomer is the range of epoxy-coated inductors. This IR-4 Series extends from $0.015 \mu \mathrm{H}$ to $240 \mu \mathrm{H}$ which is a very useful coverage. The devices are small, wire-ended and colour coded. The smaller ones in the range might be mistaken for resistors by the unwary. Selfresonant frequencies go from $5 \cdot 9 \mathrm{MHz}$ to 525 MHz . Weight is only 0.65 grammes maximum and size of the largest is 0.45 in . by 0.2 in . with an overall length of almost 3 in . (including the length of the wire end leads). Looks as though it won't be long before nobody bothers to wind coils. Old timers in radio wil be saddened and doubtless harbour fond nostalgic memories of winding 100 turns of 24 s.w.g. on a cardboard toilet roll former in order to receive 2LO.


## PART TWO

CONNECTIONS to each of the panel mounted components are given in Fig. 11. Note that the slider control connections are numbered as follows- 1 is the earth connection, 2 is the slider and 3 is the signal input. They must be wired this way to obtain the logarithmic performance of the potentiometer.
The layout and wiring of the circuit board is shown in Fig. 12. Note also that the leads coupling the spring line unit to the circuit board have to be screened and connected to the unit itself by means of phono plugs.
Construction of the power supply is shown in Fig. 13 in which details are also given regarding the size of the chassis etc. The capacitor C13 and the bridge rectifier BR1 are mounted on a small piece of circuit board elevated from the chassis on stand-off pillars.

## Checking out and Performance

The overall performance of the finished reverb unit is given in the specification table given last month.

The supply rail current at the negative 18 V point (see circuit) should be approximately 15 mA with no
signal and with the reverb control off. The no-signal current of the reverb driver amplifier only should, if possible, be checked by connecting a meter in series with the negative supply rail at the starred point shown in Fig. 2. The pre-set PRI should be adjusted until the standing current is about 10 mA . Otherwise set PR1 to mid position.

With signals, and with the reverb control VR3 at max, the current to the driver amplifier should rise to not more than 100 mA on speech peaks. A higher current indicates overload.

## The Overload Meter

The overload meter will read only with reverb on and on strong signals may show full scale deflection. This is well beyond the point of overload at which distortion from the reverb amplifier circuit will be high. The meter used in the prototype is an Eagle type MR2P with a $50 \mu \mathrm{~A}$ movement and calibrated $0-10$. For the prototype reverb unit the figures on the meter scale were erased leaving only the scale itself. The overload point is marked (in red ink) at what was division 8 as shown in Fig. 14. In normal use the input signal should always be adjusted so that with full reverb the overload meter never quite reads to the overload mark.

Fig. 11: The wiring of the front panel components.



A view of the prototype. The main component board and power supply sub-chassis can be



Fig. 14 : The overload meter can be marked as shown. The plastic cover can easily be removed to do this.


Fig. 15: The overall frequency response of the reverb unit from either input but with no reverb included.

## Frequency Response

The overall frequency response for through signals (i.e., with reverb 'Off'), is shown in Fig. 15. The frequency responses of the spring line driver amplifier and its output amplifier can be checked against the responses shown in Figs. 3 and 4 respectively. For checking the response of the line driver amplifier, connect an audio signal generator at the junction of R14 and VR3 and set VR3 at maximum. Input signal should be not greater than about 20 mV . Check the response at the output with an audio voltmeter between C19/R36 and chassis and with the line unit disconnected. Check the response of the spring line output amplifier $\operatorname{Tr} 9$ with an audio signal generator connected to C22 and with line unit output plug connected. Input signal should not be greater than about 5 mV . Check the response with an audio voltmeter connected between C9/R15 and chassis.

## Reverb Mute

The socket marked "Reverb Mute" (external remote switch) as in Fig. 2, is optional but can be used for remote control by means of a switch on the end of a screened lead. When the switch is closed signals feeding the reverb driver amplifier are short circuited to chassis.

GEOFFREY DRIVER who lives in Woodham, Surrey has been active on the medium waves and he reports reception of Tenerife, Canary Islands on 620 kHz after 2300 hrs ; Radio Andorra 701 kHz in both French and Spanish from 2030 hrs until midnight; Radio Portugal 755 kHz in English at 2300 hrs with "DX Magazine" on the last Monday of the month; Algiers 890 kHz in English at 0300 hrs ; Bissau, Portuguese Guinea with a good signal on 1070 kHz after midnight.
During the winter months North American medium wave stations are often heard in the U.K. before midnight and sometimes they are audible as early as 2300 hrs . This is the hour when a number of Europeans close down for the night leaving a few spaces for the DX to be heard. North Americans operate on channels spaced 10 kHz apart and all of them are allocated identifying call letters which they use frequently. Listen on 710 kHz at 2305 hrs after Cairo 2 signs-off, for CJOX which is located in Grand Bank, Newfoundland. This is a commercially owned station and it carries the "CJON Radio Service" programme. On 1070 kHz , Paris closes down at $2300-$ hrs leaving the frequency clear for CBA, a 50 kW outlet of the Canadian Broadcasting Corporation situated in Moncton, New Brunswick. CBA relays the CBC Radio Network and it identifies locally on the hour and the half hour. Propagation is variable on the North American path but when conditions are favourable CJOX and CBA should be heard by 2330 hrs . Others to listen for between 2330 hrs and midnight, are WHDH Boston on 850 kHz ; CJON St John's, Newfoundland on 930 kHz ; CBM Montreal on 940 kHz ; CHER Sydney, Nova Scotia 950 kHz ; WINS New York City on 1010 kHz ; WNEW 1130kHz also in NYC; CKEC 1320 kHz in New Glasgow, Nova Scotia.

A list of North American loggings made in the UK since 1962 and covering nearly 400 different stations, is currently being distributed by the Medium Wave Circle to its members. This club, which is now in its 19th year, deals exclusively with DXing on the medium waves. Its bulletin "Medium Wave News" appears 8 times a year and contains up-to-date information about the medium waves, loggings of DX, a verification section and articles on MW DXing. Further information about the MWC is obtainable from Ken Brownless, 7 The Avenue, Clifton, York YO3 6AS.
S. N. Gaythorpe of Cranbrook, Kent asks if it is possible to hear Bermuda on the medium waves. Bermuda has 3 medium wave stations; ZFBI on 960 kHz ; ZBM1 on 1230 kHz and ZBM2 on 1340 kHz and all have been heard in the UK. There is no short wave broadcasting in Bermuda and consequently this is a "medium waves only" DX country. Try on 1230 kHz after midnight for ZBM1, and log this rare DX country.

Please send logs and information about the medium waves to the author at 132 Segars Lane, Southport PR8 3JG.

## AUTON EMER 250 V SUPPI <br> Within the last two years there have been two electricity supply emergencies and, at the time of going to press, there is a possibility of another. This unit will save you the indignity of spending yet another spell 'blacked-out’. <br> S.SOAR <br> 

THE unit described here was developed during the power crisis of February 1972 and was primarily intended as a standby emergency lighting unit, although since the restoration of normal power the device has had considerable use, both as a battery charger and as a portable power supply in garage and caravan. The power output is sufficient to operate a small electric drill or an inspection lamp.

Specification


## Circuit Description

The unit has two modes of operation, with a 12 V accumulator and 240 V mains connected, the unit is a charger capable of delivering up to 12 A , this charge rate falls to approximately $1 \cdot 5 \mathrm{~A}$ with the battery fully charged. An auxiliary socket on the unit provides a 240 V mains output.
In the event of the mains supply being interrupted, the unit automatically switches over and power is taken from the battery and by inverter action is delivered to the auxiliary socket at 240 V thus maintaining the supply. When the mains supply is restored, the unit again switches automatically to its charging condi-


Fig. 1 : The complete circuit on the combined charger/inverter. This will give up to 150 W at $240 \mathrm{~V}, 50 \mathrm{~Hz}$. See text for a description of the operation.
tion and the battery is restored to its fully charged state.

Since the inverter output is a square wave, it is not ideally suitable as a supply for equipment such as a television receiver, however, satisfactory performance has been achieved with slightly reduced picture size and tolerable interference on sound.

## As a Charger

With the mains supply connected, relays RLI and RL2 are energised, transistor bases are isolated and mains supply is connected directly to the auxiliary socket and to the output transformer secondary via choke L1. Rectifiers D3 and D4 supply full wave rectified current to charge the battery. Ballast choke L1 limits the charging current to a safe maximum of around 12A with a flat battery, this charge rate decreasing as the battery potential rises.

## As an Inverter

With the mains supply interrupted, the relays deenergise, the transistor bases are connected and the output socket is connected directly to the secondary of the output transformer. The unit now operates as an inverter.

Referring to Fig. 1, assume Trl to be conducting, then transformer action (T1) holds $\operatorname{Tr} 2$ off ( + ve on base) and Trl on (-ve on base) magnetic flux in the transformer core (T1) increases uniformly and current is substantially constant. However, as the flux density in the core approaches saturation, current increases rapidly in an attempt to maintain the rate of flux increase constant. Base drive on Trl is limited by RI and the gain of the transistor falls with increased collector current, these two factors result in Tr 1 coming out of its saturated state and collector current can increase no further, flux cannot increase

## components list

## Resistors

| R1 | $5 \Omega$ | R4 | 4 5 |  |
| :---: | :---: | :---: | :---: | :---: |
| R2 |  | R5 | - $82 \Omega$ | 1W |
| R3 | $470 \Omega \frac{1}{2} W$ |  |  |  |
| Sem | ductors |  |  |  |
| Tr1 | MP2200A | D3. 2 | 20 A 100 V (e.g. 21PT | p.i.v. rectifier T20) |
| Tr2 | MP2200A | D4 2 | 20 A 100 V | p.i.v. rectifier |
|  |  |  | (e.g. 21P |  |
| D1 | 1N4001 | ZD1 | 45V 1W | zener, e.g. 153045 |
| D2 | 1N4001 | ZD2 | 45 V 1 W | zener, e.g. 153045 |

$\mathrm{Tr}_{1}$ and $\mathrm{T}_{\mathrm{r}} 2$ are available from Jermyn industries, Vestry Estate, Sevenoaks, Kent. D3 and D4, 21PT20, are International Rectifier types. ZD1 and ZD2 are available from Quarndon Electronics, Slack Lane, Derby.

Transformers, Coils and Relays
RL. 12 -pole changeover with 240 V a.c. coil
RL2 2 -pole changeover with 240 V a.c. coil
T1. Driver transformer type P/1286
$T 2$ Output transformer type P/1293
L1 Ballast Choke type P/1294
T1, T2 and L1 are avallable from Magtor Limited, 68 Dale Street, Manchester; a complete kit of these costs $£ 6.65$ plus 50 p postage.

## Miscellaneous

C1, C2, $0.01 \mu \mathrm{~F} 600 \mathrm{~V}$; M1, Ammeter with centre zero, 20-0-20A or similar (Car types are suitable).
and base drive falls causing a further reduction in collector current. Falling flux causes Tr2 to become biased on and the collector current increases rapidly and $\operatorname{Tr} 2$ is switched hard on, this completes one cycle.

Frequency of operation is determined by the time taken for the transformer core to saturate, suitable choice of core and windings results in an operating frequency of approximately 50 Hz .

The transistors are protected against reverse bias by diodes D1 and D2, and ZD1 and ZD2 clip voltage switching transients to a safe level.

## Construction

Since the power transistors are connected in common collector, these devices should be fixed directly to the chassis, 16 s.w.g. aluminium was used on the prototype. Transformers, relay and choke are also bolted directly to the chassis, and if rectifiers with anode studs are used, these can also be fixed directly to chassis. Other components should be mounted on insulated tag strips. It is advisable to have all low voltage components on one side of the output transformer (i.e. primary winding side) and all mains voltage components on the other side (i.e. secondary side).

## TELEVISION

## DECEMBER ISSUE

## EHT SYSTEMS FOR TV SETS

A lot of confusion seems to be present about the nature of the e.h.t. pulse, the stabilisation of the e.h.t. voltage and the different characteristics of half-wave and multiplier systems. This month we are taking a close look at this department, for both monochrome and colour set use.

## UHF PREAMPLIFIER

Full constructional details of a simple u.h.f. aerial preamplifier which has given excellent results for both fringe area and DX use. Several prototypes have been tried out and the stability is so good that they can be cascaded.

## SERVICING THE PYE 368 CHASSIS

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## TRANSISTOR CIRCUITRY formeginners PART 13 H.W. HELLYER \& MICHAEL HOLLIER

## Minimum noise

We have already stated that our principal aim is as good a signal swing as we can afford provided that we do not thereby increase the noise in the circuit. With any transistor type, some noise is generated, but this can be aggravated tremendously by collector currents and also by the source resistance seen by the transistor-and, as might be expected, the optimum conditions alter with frequency.
A digression here, for colleague Mike feels strongly on this subject, having been too often caught with unsuitable replacements. Transistors with the same code number but made by different firms can have widely odd noise performances, as we have found when using them for laboratory equipment.
To find the optimum operating conditions under which our chosen transistor is to be used, we must turn to the graphs of noise figures quoted by the maker. These indicate a typical noise level expected at a selected collector current, with a selected source resistance 'seen' by the transistor base. But the quotes are at one single frequency. In practice we find conditions vary widely-a whole family of curves is really needed for optimum choice-and is seldom available, even from our old friends Mullard, who kindly acknowledged our quotes while pointing out an omission, in a letter from L. W. Owers in the October issue of $P W$. Very few firms, including Mullard, give figures that allow us to optimise for the whole audio band-in fact, they seem to think the world ceases revolving below 100 Hz , giving data at 1 kHz and 10 kHz , generally. More noise is generated at low frequencies than high, and the higher the operating current, the higher the noise level.

We have decided upon a collector current of 80 microamps for $\operatorname{Tr} 1$ and the graphs, such as are available, would indicate that a source resistance of between 5 and $20 \mathrm{k} \Omega$ would be best for low noise. We shall aim at the lower figure.

The base of Trl will 'see' the resistance formed by the virtual earth (see Fig. 62) shunted by the series input resistor plus whatever the impedance
may be of the device that is feeding the circuit. The inset of Fig. 64 should give us some idea.

The virtual earth resistance can be calculated from $R_{v}=\frac{\mathbf{R}_{b}}{G_{\mathrm{o}}}$ so $\mathbf{R}_{\mathrm{b}}$ becomes $500 \mathrm{k} \Omega$, or, in practice, a $470 \mathrm{k} \Omega, 5 \%$ component. The voltage across this resistor is the $\operatorname{Tr} 2$ emitter voltage less the base voltage of Trl, or $9 \cdot 303 \mathrm{~V}$ and the current through this resistor will be around $19 \cdot 8$ microamps (remember we are ignoring the very small Ibl).
The current through R2 will, of course, be the same. So we come to a preferred value of $39 \mathrm{k} \Omega$. I shall not insult you with the details of the workings after 11 plodding articles of preparation...

We now have a working circuit with a low input resistance of around $5 \mathrm{k} \Omega$. And we insert R3 into the base 'feed' circuit of Trl. This does two things: first, it raises the input resistance-that is, the resistance the source will 'see'; second, it gives us some control of the gain of this circuit. Remember, closed loop gain is equal to $\mathrm{R}_{\mathrm{b}}$ dividend by $\mathbf{R}$, which is, in this particular configuration, $\mathrm{Rl}+\mathrm{R} 3$. To get a theoretical gain of 20 , for example, R3 would have to be $23 \cdot 5 \mathrm{k} \Omega$ (preferred value, $22 \mathrm{k} \Omega$ ).

$$
\mathrm{G}_{\mathrm{c}}=\frac{\mathrm{R} 1}{\mathrm{R} 3}=\frac{470 \mathrm{k} \Omega}{22 \mathrm{k} \Omega}=21.3613
$$

## Coupling

As for that input and output coupling. We found, in practice, great care had to be taken. In fact, we built the circuit and had some very strange figures before remembering that the feedback was both a.c. and d.c. conscious. So the input capacitor serves a double function; that of blocking the d.c. from previous stages (and to previous stages) and coupling the signal to the stage which we are designing.
Now the problem is that it must be of a sufficiently large value to present a short-circuit, or as near this as may be, to the frequencies over which our amplifier has to work. In the practical case, something like $200 \mu \mathrm{~F}$ is in order. One reason that

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| 1A | 8p | 8 p | 10 p | 11］ | 10 p | 150 | 20p | － |
| 3A | 159 | 17p | 20p | 881 | 25p | 275 | 80 p | 85 p |
| 6 A |  | － | 25p | 80 p | $32+5$ | 85 |  |  |
| 10A | 808 | $85 p$ | 40p | 47D | 66 p | 669 | 75 | $\underline{-}$ |
| 15A | 36p | 450 | 48p | 55 | $65 p$ | 751 | 870 | － |
| 35A | 70p | $80 p$ | 901 | 81.00 | 81.40 | 8170 | 88.75 | － |
| 1 amp and 3 amp are plastic encspssulation． |  |  |  |  |  |  |  |  |

DIODES \＆RECTIFIERS

| IN34A | 10p | AA119 | 7 p | BAX16 | 12ıp | FST3／4 | 2815 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| IN914 | 7 p | AA129 | 151 | BAY18 | 173 | OAS | 170 |
| IN916 | 70 | AAZI3 | 127 | BAY31 | 7p | 0 AlO | 809 |
| IN4007 | 20p | AAZ15 | 12p | BAY88 | 850 | 0 O99 | 10p |
| 1844 | 7 p | AAZ17 | 10 p | BY100 | 15p | OA47 | 8 p |
| 15113 | 15p | Pal00 | 15 p | BY103 | 22p | OA70 | 78 |
| 18120 | 129 | BA102 | 259 | BY122 | 471 P | OA73 | 10p |
| 18121 | 14p | BA170 | 25 | BY124 | 139 | 0 Of7 | 7 |
| IS130 | 8p | BA114 | 15p | BY126 | 15p | 0 OA81 | 80 |
| IS131 | 10p | BA115 | 7p | BY127 | 17p | OA82 | 109 |
| IS132 | 12p | BA14I | 17 y | BY164 | 67 p | OA90 | 78 |
| I8980 | 7 p | BA142 | 178 | BYX10 | 285 | OA91 | 78 |
| I8922 | 8p | BA144 | 120 | BY710 | $35 p$ | 0 A 95 | 7 |
| IS923 | 18p | BA145 | $17 p$ | BYZ11 | 32p | OA200 | 75 |
| IS940 | 5 p | BA154 | 120 | BYZ12 | $30 p$ | OA202 | 100 |
|  |  | BAX13 | 5p | BYZ13 | 25p | TIV307 | 60\％ |


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|  | 0.15 | 0.1 |
| :---: | :---: | :---: |
|  | Matrix | Watrix |
| $27 \times 3{ }^{3} \mathrm{in}$ | 175 | 23p |
| $2{ }^{2} \times 5$ in | 250 | 250 |
| $3 \frac{1}{4} \times 39$ in | 859 | 25p |
| $31 \times 5 i n$ | 30 p | 297 |
| $5 \times 17 \mathrm{in}$（Plain） | 88p |  |

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 0.15,
0.47
0.68
1.15
$1 \cdot 5 \mu \mathrm{~F}$
$2.2 \mu \mathrm{~F}$ $8 p$
119
149

WIRE－WOUND EESISTORS
2.5 watt $5 \%$（up to 270 ohms
only）， 7 p （up to $8.2 \mathrm{k} \Omega$ only）， 9 p

5 watt $5 \%$（up to $8.2 \mathrm{k} \Omega$ only），op
$10 \mathrm{watt} 5 \%$（up to $26 \mathrm{k} \Omega$ only），
10 p

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$\begin{array}{lll}0.1 \text { Watt } 6 p & \text { VERTICAL } \\ 0.2 \text { Watt } & 6 \mathrm{p} & 0 R\end{array}$
$\begin{array}{lll}\text { 0．2 Watt } & \text { 6p } \\ 0.3 \text { Watt } & \text { OR } \\ \text { moRIZONTAL }\end{array}$
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| THGO14P PREAMP |
| $21-20$ |

care is needed here is again to reduce that bothernoise. If we make short-circuit and open-circuit input tests while measuring the residual noise at the output, we find there are some amazingly variant readings. A practical tip, for those who get fun from building their own hook-ups, is to load the circuit, at the actual input point, with the input impedance you want the circuit to 'see'. You may be surprised at the difference from abstract theory which your eventual readings reveal!

## Measurement

We have talked glibly about open-loop gain, $\mathrm{G}_{0}$, but given no clues as to its measurement. This is no easy task-you see, if you disconnect the feedback to measure open-loop gain the first transistor bias goes adrift, and the measurements mean nothing.

We must take into account the a.c. feedback as well as the d.c., and here there is a gag which is worth recounting. A network can be made up temporarily, and inserted in place of the feedback resistor, which maintains the essential d.c. conditions, but effectively ties the a.c. feedback down to chassis. Fig. 65(a) shows a simple, three resistor


Fig. 65, (a) Substituting the feedback resistor with a decoupled network enables the gain to be measured more accurately. (b) Input for a variable gain pre-amplifier. An emitter follower, shown dotted, may be needed to effect matching. (c) Mixing facilities. (d) Microphone pre-amplifier.
and one-capacitor network, chosen so that the resistive values are approximately as R1 in Fig 64, but the large electrolytic capacitor acts as a complete shunt to any a.c. in which we might be interested. As Mike says, this may be of academic interest, but is worth a mention.

Of greater than academic interest is the capacitor shown dotted across the feedback resistor in Fig. 64. It has been said too often-which does not stop me from saying it again-that the wider one opens the window, the more the dirt blows in. Being interpreted, the wider our bandwidth, the more likelihood is there of our little amplifier getting upset by extraneous influences, like Aunty switching on the vacuum cleaner.

Without joining the argument that can set the hi-fi world by its ears; one group of contenders arguing for an almost infinite bandwidth and the inclusion of filters, the other for a 'tailored bandwidth', we can say here that the ease of making our frequency response roll off in a controlled manner at the top end appeals to us. Without that capacitor, our frequency response of the built amplifier (made up in a Norman Rose AB9 box with co-axial terminations, for complete screening) was within $+0-3 \mathrm{~dB}$ at 78 kHz and at 150 kHz , we were still only $8 \cdot 2 \mathrm{~dB}$ down.

At the bottom end, incidentally, we were $-0.1 d B$ at 40 Hz and -0.8 dB at 15 Hz , which is negligible.

Shunting the feedback resistor with 22 pF gave us -3 dB points at 20 kHz and -6 dB points (complying with DIN 45500 , in case anyone wanted to argue!) at 31 kHz . Under these conditions, the broadband residual noise was 0.13 mV with an open-circuited input, 990 microvolts with a short-circuited input. As clipping took us to slightly over 6 volts (for a 410 mV input), our signal-to-noise ratio, unweighted, could be said to be $20 \log 10^{-6}: 0 \cdot 0001$, taking a figure of $0 \cdot 1 \mathrm{mV}$ as a typical residual noise measurement. A rather impressive (who said impossible?) $95 \cdot 5 \mathrm{~dB}$.

Effective input noise is the output noise with input short-circuited divided by the gain. Our measured gain at a typical 10 mV input was only $14 \cdot 7$, not as much as we had expected, but accounted for most likely by component spreads and the second transistor, which happened to be an odd type we had handy. You can always select with great care for precision, as we said earlier, but it is great fun to 'suck it and see'. So in the practical instance, we can say our effective input noise is 68 microvolts. This now becomes the limiting factor for any use to which we are going to put such a device. I think you will agree that in the present case the limitation is hardly exclusive.

## Application

A few of the possible applications were hinted at previously. Without wasting any more space on design data, take a look at the three sub-circuits of Fig. 65 (b), (c) and (d). First we see a way of altering the input resistor, precisely, by presets, so that we get a variable gain pre-amplifier, as might be useful for an oscilloscope. The problem here may be an alteration of input impedance, and it is a good idea to precede the virtual earth pre-amplifier with an emitter follower stage, which gives, you will remember, a reasonably high input impedance and a low output impedance (providing the necessary low source our device wants to 'see'.)

Let's suppose we want to use the virtual earth pre-amplifier as an input stage for a mixer, where there are several odd sources that may be used separately or simultaneously, and where the action of one must not interfere with that of another. As any amateur disc-jockey will tell you, a very practical problem. In Fig. 65(c) we get the inputs from the sources taken to low value potentiometers and from there we can feed up to three R3 resistors to the virtual earth point, this time using our coupling capacitor to follow the resistors, for effective isolation. By juggling resistor values, with a little experiment, we can again get our levels somewhere the same, and use a master gain control later in the circuit, where its operation at a higher signal level will not introduce unwanted noise, etc.

Of course, there is always the microphone preamplifier, as in (d), where we want a bit more gain prior to a mixer stage. The transformer is a low/ high or medium/high type and is best mounted in the overall screened box that houses the virtual earth amplifier.

## Power supply

Finally, this month, having again not kept my promise to lead us on to tone controls, although a careful perusal of the foregoing will have seen the trend our thoughts are taking, we have a brief look at the proposed power supply for this and other projects. This was knocked up easily in an hour and needs no particular layout finesse, nor screening. It uses any convenient transformer that can give between 24 and 33 volts-not really safe to exceed $33 \cdot 6 \mathrm{~V}$-and the rectifiers are easily obtained types with minimum requirements of peak-inverse voltage


Fig. 66. A practical power supply, suitable for use with the circuits described.

50 V and handling capacity 200 mA . We used a REC 60 because it happened to be there, but four 1N4001's would have done. The particular requirement is the zener diode, which must be a 24 volt type, such as shown, and components can be halfwatt types, with the biggest problem the mounting of the two large capacitors. Note that this zener operates in the reverse to the breakdown mode, i.e., it is set to regulate, with cathode to positive. This 24 volt output, with the $2 \mathrm{k} \Omega$ resistor (or $2 \cdot 2 \mathrm{k} \Omega$, if you have no $2 \mathrm{k} \Omega$ version available) drops to the needed 20 volts for our amplifier.

## AMATEUR BANDS RECEIVER

-continued from page 698
crystal pass-band. Adjustment of any of the i.f.t. cores should then bring about a great increase in signal strength as they are shifted into the crystal pass-band. The i.f.t.'s are all finally peaked in this way, signal strength being reduced by VR1 as necessary.

When the i.f. amplifier is aligned in this way, a very steep sided response should be obtained. If X 6 and X 7 are removed and a 100 pF capacitor plugged into one holder, general selectivity will still be very good, but there should be a very noticeable reduction in sharpness of tuning and noise will increase due to the broader pass-band.

## MODIFICATIONS

As the idea of construction in stages is to obtain fully working circuits as quickly and easily as possible, the i.f. section can be simplified initially then modified to the full circuit.

The S-Meter circuit can be omitted completely at first and fitted later.

IFT1 and V1, Fig. 2C may be omitted and mixer pin 6 taken to pin 3 on i.f.t. 2 or Vl and i.f.t. 2 may be omitted and the crystals or secondary of i.f.t.l may be temporarily connected to pin 1 of V2.

When the tunable first i.f. section is constructed, the receiver can be employed for the $3 \cdot 5 \cdot 4 \mathrm{MHz}$ band only. The receiver cannot be used on other bands until the crystal controlled first conversion section is completed.

With some valves i.f. instability occurred with VR1 at maximum gain. This was cured by placing a $2 \cdot 2 \mathrm{k} \Omega$ resistor between pin 2 of i.f.t.l and h.t., with a $0.25 \mu \mathrm{~F}$ capacitor from pin 2 to chassis.

## TUNABLE FIRST IF AMPLIFIER

This has two stages, Fig. 2B, and is constructed in a screened box to minimise pick-up of unwanted signals. Coverage is 3.5 MHz to 4 MHz , with a little to spare at the extreme positions of the 3 -gang capacitor VC1, VC2 and VC3.

V1 operates as an r.f. amplifier on the $3 \cdot 5 \cdot 3 \cdot 8 \mathrm{MHz}$ band and as first i.f. on the other ranges. The gain of this stage is also controlled by VR1. AGC bias is applied to both stages via R1 and R4 (it is not good practice to apply a.g.c. to a frequency changer of this type-Ed).
The oscillator section of the mixer-oscillator V2 is run from the 150 V stabilised h.t. supply. Input to Ll is via a screened lead and a similar screened lead runs from V2 to the 455 kHz i.f. amplifier.

The box is $5 \times 4 \times 2 \mathrm{in}$. deep, with the valves on top and all other parts, including $\mathrm{VCl} / 2 / 3$, inside. This box is made from a $5 \times 4 \mathrm{in}$. flat plate, to which are bolted two $4 \times 2 \mathrm{in}$. and two $5 \times 2 \mathrm{in}$. "universal chassis" flanged members. It is easier to leave the sides and back off the box until wiring is completed.

## TO BE CONTINUED

Next month we shall cover the construction and alignment of the tunable IF amplifier and give full information on the BFO/Product Detector and RF/1st Mixer stages to enable the receiver to be completed.

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| H9 | 2 | OCP7! Light Sensitive Photo Transistor | 0 p |
| H40 | 20 | SFY50/2, 2N686, 2N1613 <br> NPN silicon uncoded TO-5 | 0p |
| H28 | 20 | $\begin{aligned} & \text { OC20011/2/3 PNP silicon } \\ & \text { uncoded TO-5 } \mathrm{can} \\ & \hline \end{aligned}$ | 50 p |
| H30 | 20 | Watt Zaner Diodes. Mixed Voleages 6.8-43V. | 0p |
| ${ }^{3} \mathrm{HS}$ | 100 | $\begin{aligned} & \text { Mixed Diodes. Germ. Gold } \\ & \text { Bonded, etc. Marked and } \\ & \text { Unmarked. } \end{aligned}$ | 50p |
| H38 | 30 | Short lead Transissors, NPN Silicon Planar types. | 50p |
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$16 \times 6 \mathrm{in} .28 \mathrm{p} ; 14 \times 9 \mathrm{in} .84 \mathrm{p} \div 12 \times 12 \mathrm{in} 40 \mathrm{p} \cdot 16 \times 10 \mathrm{in} 50 \mathrm{p}$ $16 \times 6 \mathrm{in}$. $28 \mathrm{p} ; 14 \times 9 \mathrm{in} .84 \mathrm{p} ; 12 \times 12 \mathrm{in} .40 \mathrm{p} ; 16 \times 10 \mathrm{in} 50 \mathrm{p}$.


4
30-14,500 c.p.s., $12 i n$ double cone, wooter and with a BABER coramil magnet assembly havin a fux density of 14,00 gauss and a wals 145,000 mexwells. Bas resonance 40 e.p.s. Rate 3 or 8 or 15 ohms. Post Free Module kit, $30-17,000$ c.p.8 with eweeter, crossover baflle and instructions. BAKER "BIG-SOUND" SPEAKERS
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"Group 35"
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 8 or 8 or 15 ohm 3 or 8 or 15 ohm 8 or 15 ohm TEAK HI-FI SPEAKER CABINETS. Fluted wood front For 12 in , or 10 in . dia. speaker $20 \times 12 \times 9 \mathrm{in}$. 29 , Post 25 p For $10 \times 6 \mathrm{in}$. or Gin. speaker $16 \times 8 \times 6 \mathrm{in}$. 84 . Post 25 p LOUDSPEAKER CABTNET WADDING18in. wide,15pft.

GOODMANS $6 \frac{1}{2}$ in. HI-FI WOOFER 8 ohm, 10 watt. Large ceramie magnet. pecial Cambric cone surround. Frequency Hi-Fí Enclosures Systems, ete. 54


## ELAC CONE TWEETER

The moving coil diaphragm gives a good radiation pattern to the higher frequencies and a smooth extension of total response from $1,000 \mathrm{cps}$ to $18,000 \mathrm{cps}$. Size $3 \frac{1}{7} \times$ $3 \frac{1}{x} \times 2 i n$ : deep. Rating 10 watts .8 ohm or 15 ohm models. $\$ 1.90$

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LOUDSPEAKERS P.M. 3 OHMS. $7 \times 4 \mathrm{in}$. $21-25$; $6 \frac{1}{2} \mathrm{in}$. $21 \cdot 50$; $8 \times 5 \mathrm{in}$. $£ 1 \cdot 60 ; 8 \times 2 \mathrm{in}$. $\mathbf{5 1} \cdot 508 \mathrm{in} .21 \cdot 75 ; 10 \times 6 \mathrm{in}$. $£ 1.90$. RICEARD ALLAN TWIN CONE LOUDSPEAKERS. or 8 or 15 ohm models $£ 2 \cdot 20$ each. Post $15 p$
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Push-Pull Ready built, with volume control. 97 . 4.50
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## MONTHLY

## NEWS FOR

 OX LISTENERSALTHOUGH a great deal of pleasure can be obtained from simply listening to Broadcast stations many listeners take the hobby a step further and collect QSL cards from all over the world:

A QSL card is a verification from the station that the listener did, in fact, hear their broadcast. QSJ, cards are issued as a reply to reception reports from the listener after the details have been checked against the station log.

The majority of stations are very glad to receive reports from listeners as a well prepared report tells the station how well its transmissions are getting through. The subject for this month is the preparation of reception reports which are helpful to the station.

The first essential of a good reception report is the name and address of the reporter, without this the station does not know where the reception occurred and is unable to send a reply. The technical information should be given in the following manner:-

## RECEPTION REPORT

I received your broadcast on ........... (date), on a frequency of $\ldots \ldots . . . . . \mathrm{kHz}$, and listened to it from
$\qquad$
$\qquad$
$\qquad$ hours G.M.T.
The receiver used was a ......... (TRF/Superhet etc.) with ......... (Number) Valves/Transistors, made by ............ model number $\qquad$
The aerial was an interior/exterior one, metres high and ......... metres long of the type.
Reception was ......... in the SINPO code, i.e.: "S" Signal Strength ......, "I" Interference ....... " N " Noise ......" "P" Propagation ......, "O" Overall Merit ...... The broadcast was in the ............ language and the programme details were as follows

I hope that this report is of use to your Engineers and trust that you will be able to verify that my report is correct. If so, will you please send me your QSL card, or verification letter, in reply to this report. I enclose an International Reply Coupon to cover your postage costs.
I hope that I shall have the pleasure of hearing your station in the future and look forward to sending you further reports on your transmission.

Yours sincerely,

The SINPO code mentioned in the above specimen report may be new to some readers so I will give details of this method of assessing reception.
The "P" in the SINPO code stands for Propagation but is probably easier to understand if we refer to it as Fading.

# THE BROADCAST BANDS Malcolm Connah 

| Rating <br> $S$ | 1 <br> Barely | 2 | 3 | 4 | 5 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Poor |  |  |  | Fair | Good | Excellent

Reception of BBC Radio One on 247 metres in the medium wave band can usually be rated as 55555 but the transmissions are sometimes affected by slight interference which reduces the rating to 54554. Radio Luxembourg on 208 metres is usually subject to severe fading and slight interference giving a rating of 54522 .

The overall Merit figure is a very subjective rating and takes into account the other four figures, it would however be unusual to have an overall merit figure which is greater than the lowest of the other four. To use the above example some listeners would rate Radio Luxembourg as 54523 , others would take the average of the first four figures as the "O" rating. In this case Luxembourg would rate 54524, which is incorrect since reception with severe fading cannot be classed as good.

The first log this month comes from Michael Berry of Dewsbury in Yorkshire who used his Eddystone EB35 receiver and 20 foot horizontal wire in the loft to hear :
3227 ELWA, Liberia, vernacular at 2010.
4890 R. Diff. Venezuela, Spanish at 0100.
11795 ETLF, Ethiopia in Malagache at 0330.
15105 R. Rural, Brazil, Portuguese at 2125.
15155 R. Diff. de Sao Paulo, Portuguese, 2235.
15170 ELW A, Liberia in French at 2000.
15445 R. Nacional be Brazilia, English at 2130.
Nigel Knowlman of Cullompton in Devon has sent in another log using his Lafayette HA-600A with an inverted ' $L$ ' antenna to hear:
11720 Radio Tashkent, USSR, at 1405.
11815 TWR, Bonaire noted at 0040.
11850 Radio Vilnius, USSR at 2245 .,
15185 WINB, USA in English at 2215.
15195 R. Ankara, Turkey in English at 2200.
17855 NHK, Japan, news in English at 0705.
17920 Radio Cairo in English at 1415.
A. P. Turner of Eastbourne, Sussex has a PetoScott H-25, 5-valve domestic superhet receiver and a 65 foot long wire which enabled him to hear:
6040 VOA with news at 1917.
7100 R. Tirana, Albania in English at 2223.
7245. R. Austria, news in English at 0907.

11805 R. Pakistan in English at 1830.
15245 RSA, South Africa in English at 1608.
17810 R. Kuwait, news in English at 1738.
Reports should arrive by the 15 th. of the month and be addressed to me at 59 Windrush, Highworth, Swindon, Wiltshire. Please note the new address.


DOUBTLESS many will not be pursuing the noble art of Amateur Radio on November 5 but will usefully employ the time to honour (?) Guy Fawkes for his near miss. However, that does leave another twenty nine days in which to make up for lost time.

One thought is the topband transatlantics. Quite a few signals have been received, not merely from across the pond but from other countries/continents also. A session around 0600 hours might be worth a try although most 160 metre stalwarts are just as liable to be putting out a slow $C Q$ in c.w. in the evenings too. Many d.x. stations are trying their hands at topband using s.s.b. and this band should make an interesting playground for the more seriously minded s.w.l. during the long winter evenings ahead.

Intruders in the Amateur bands are pests who have no moral or legal right to be there. The R.S.G.B. keep an intruder watch and this relies heavily upon reports received. Any s.w.l. with reasonable equipment is welcome to assist, but reports must be accurate. If you have a single conversion superhet, for example, you must ensure that it is not an image signal you are hearing which is, in fact, outside the band.

It's funny callsign time again. Queries flood in about those using a letter followed by two numbers. Not a postal code for Hong Kong, just a new prefix time-again! Bangladesh is apparently active and the call sign here begins S21 (sounds like the washroom in a Government building). Just in case you think I've picked out an odd one, how about C21 for Nauru. Don't be fooled though, the latter have also been known to use a C29 prefix too.

Paul Genner (Liverpool) writes in with news of activity from Vietnam which must surely be a rare one for anyone to bag. Callsign is XV5AC and no band given but 20 and/or 15 would be a safe bet. Paul also mentions that anyone wanting to add Willis Island to their list should look out for VK9ZB who will set sail in December from Willis. Quick, while there is yet time.

John Tirrall (Bognor) tells the amazing tale of a W7 reported to be putting up a 40 (forty) element beam for 28 MHz and will feed the brute on generous helpings of r.f.-a kilowatt no less. Those who hear nothing on ten metres could make it a red letter day. (Perhaps a red aerial day with all that power coming in).

Talking of ten metres, with the decline of the sunspot activity count this band is perhaps one of the most interesting. Readers might consider erecting a simple ground plane antenna especially for this band. The elements are only just over 8 feet in length and even a vertical dipole might be dangled down the side of the house. Feed in the centre with $75 \Omega$ coax as for a horizontal dipole and your in business. Watch that your receiver isn't one which is to be nurtured on $300 \Omega$ feed though or you'll have a mismatch.

# THE AMATEUR BANDS David Gibson, G3JDG Frequencies in kHz - Times in GMT 

Times to listen are always a dangerous thing to predict with any degree of dogma since some bright soul always hears half the world at the very opposite times to those you have predicted. However, according to the JDG crystal ball, afternoons and evenings appear favourite for 21 and 14 MHz which are still the most popular listening bands if logs received are any indication. Hopefully, adventurous s.w.1s will venture forth into regions such as $3 \cdot 5 \mathrm{MHz}$ and 7 MHz during the coming months as conditions improve.

Alan Smith (Nelson), JR310, a.t.u. and 60ft. end fed is one who braved $3 \cdot 5 \mathrm{MHz}$ to get s.s.b. scalps from; HK1NR, KZ5JF, K3JH, PY1HA, SP9FMA, VE1ARH, VE1IE, VE1XI, VO1BT, VO1CV, W1PSK, W3MFW, XE1HJ, YN1FI, ZL2BT, ZM4PG, 6Y5AR.

Up on 21 MHz Alan bagged; CR6QA, CR7LE, CR8BF, DU1BOB, DU2EL, EP2JW, ET3USA, FP8DH, HS4AGN, HS4AGZ, JA1HIV, JA2DX, JA3BLC, JA4FDZ, JA6FBQ, JA7MFA, JA8QX, JA9EFQ, JA0GRR, KA6MH, KH6KHD, KP4DDO, LU1ACO, SV0WW, SV1GP, TJ1DF, VE1AM, VE3AUM, VS6AD, W8EX, W9ADW, XV5AC, ZS1J, ZS2MI, ZS3AK, ZS4LW, ZS5OE, ZS60F, 4S7AB, 4S7PB, 4Z4EF, 4Z4LK, 5B4KP, 5N2ESH, 6W8YL, 6Y5GB.

Paul Russell (High Wycombe), went to West Norfolk for a holiday. With him went a Sentinal converter, UR-1A receiver as a tuneable i.f. ( $4-6 \mathrm{MHz}$ ) and a 5 -element yagi which posed transport problems on the way there, especially on the London Underground. Rewards for these sterling efforts included 144 MHz signals from; F5VA, F6AGV, F6NM, G2AKQ, G3BN, G3CZA, G3DAH, G3OXV, G3PMH/P, G3POI, G3SRT/A, G3TTV, G3UJK, G3WW, G3XIX, G3ZYC, G4ARD/P, G8DYK, GW4ABR/P, P0HVA, PA0VJ, PA0VZL.

William Fereday (Aston-on-Trent) uses an R107 and bent 50 ft long wire ( Oh -bold). Twenty metre tweets from; JA1QZY, JA2PJC, VK3AHI, VK3RZ, VK5FH, W6BMP, W6BT, YN3NPF, 9V1QT.

Roger Dixon (Skipton), PR30, CX203 receiver and 100 ft . long wire end fed sent in a log for ten metres (bless you). Stations bagged incluude; CE3AGU, LU4DCO, TU2DO and 9J2KY. Who says there's nothing up there?

Glyn Fisher (Oakham) landed a number of EU stations on 7 MHz . Among these were signals of the s.s.b. type from VK2AVA, VK5PB and VK7GK. Gear is a Westminster radiogram and a 50 ft . endfed.

Well worth a listen is the $1 \cdot 8 \mathrm{MHz}$ contest on November 11-12. There is also a Czechoslovakian contest on the 12th. The Czech stations are often in evidence on topband but if you want to log stations from further afield, try the CQ WW d.x. c.w. contest on November 25-26.

> Logs, in alphabetical order please to arrive by the 15 th of the month to 12 Cross Way, Harpenden, Herts.


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are illustrated. It costs only 70 pence, including post and packing, and each copy contains 10 vouchers worth 5p each.

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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AC107 | 15p | AL102 | 58 p | BD130 | 46 p | 0071 | 12p | 2N097 | 180 | 406336 | D |  |  | 95p |
| AC126 | 11 p | AL103 | 9 p | BD131 | 68p | OC72 | 1 p | 2nliai | 245 |  |  |  |  |  |
| AC127 | 11 p | AU103 | 85 p | BF194 | 15p | OC81 | 13 T | 2N1364 | 25 T |  |  |  |  |  |
| AC128 | 11p | AU111 | 95 p | BFY50 | 15p | OC81D | 13 p | 2N1305 | 25 n |  |  | SU | R LOW |  |
| $2 \mathrm{Cl17}$ | 255 | ${ }^{\text {HeIV7 }}$ | 8 p | BFY51 | 12p | $0 \mathrm{C83}$ | 200 | ${ }^{2 N 2 N} 268$ | 47n |  |  | PRI | LIN |  |
| $A^{\text {Cl4 }}$ | 20 p | 3che8 | 8 D | BSY95A | 15 p | ${ }^{0} \mathrm{Cl} 70$ | 24p | 2N2926 | 10 n | DIODES |  |  |  |  |
| ACl42K | $20 p$ | BC109 | 8p | ME0402 | 18p | OC200 | 25p | 2N3053 | 200 | IN4001 | 4p | 301A | ${ }^{T} 099$ | 9p |
| AD14 | 40p | BC154 | 20 p | ME0404 | 14p | OC201 | 25 p | 2N3055 | ${ }^{49}$ | IN4002 | 4 t | 301A | D1L |  |
| AD150 | 44p | EC168 | 10p | ME4401 | 10 p | OC25 | 25 p | 2N3702 | 12 p | IN4003 | 5 p | ${ }^{709 C}$ | To99 | 28p |
| ${ }^{\text {AD161 }} \mathrm{M}$ | 55p | ${ }^{\text {BC169 }}$ | ${ }^{13 p}$ | ME4102 | 12p | OC29 | 30p | 2Na703 | ${ }_{12 \mathrm{p}}^{12}$ | IN4004 | ${ }_{6 p} 7$ | ${ }_{723 \mathrm{C}}^{709 \mathrm{C}}$ | To99 | 30 p 87 p |
| ${ }_{\text {AD182 }}$ | 15p | ${ }_{\text {BC182 }}$ | 88 | ME6002 ME6101 | 14p | ${ }_{0}^{0 \mathrm{C} 29}$ | 35 p <br> $\mathbf{2 5 p}$ | ${ }^{2} \mathrm{~N} 9 \mathrm{~T} 05$ | 120 | ${ }_{0} \mathrm{OA} 91$ | ${ }_{8 \mathrm{p}}^{6 \mathrm{p}}$ | ${ }_{723 \mathrm{C}}$ | DIL | 90 p |
| AF115 | 15p | BC184L | 89 | ME6102 | 15p | OC36 | 36p | 2N3706 | 10. | Oaze0 | 10 p | 741 C | To99 | 35 p |
| AF116 | 15 p | HC212L | 8 s | MP8111 | 32p | TIP29A | 48p | 2N3707 | 10, | OA202 | 8 p | 7410 | DIL | 34 p |
| AF117 | 15p | BC214L | 8 | MP8511 | 34p | TIP30A | 55 p | 2N3708 | $\theta^{9}$ | IS44 | 10p | 741 C | 8 p in DIL | 34 p |
| capac |  |  |  | ${ }_{\text {OC41 }}^{\text {MP8513 }}$ | 45p | TIP31A | $\begin{aligned} & 58 p \\ & 69 p \end{aligned}$ | 2N3709 2N8710 | ${ }_{10 \mathrm{p}}^{10 \mathrm{p}}$ | ${ }_{\text {W02 }}$ IN4149 | 32p | ${ }_{748 \mathrm{C}}^{747 \mathrm{C}}$ | DIL | 489 380 |

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```


## SUPER PACKS

| $\underset{\substack{\text { Pack of } 10 \\ \text { (unmarked) } \\ \text { but tested }}}{50 \mathrm{p}}$ | $\begin{gathered} \text { Pack of } 25 \\ \text { IN4148 } \\ 50 \mathrm{p} \end{gathered}$ |
| :---: | :---: |
| $\begin{aligned} & \text { 2N2646 } \\ & \text { (unmarked) } \\ & \text { 30p each } \end{aligned}$ | BC108 50p |
|  | BC107 50p |
|  | (Plastic can) |
|  | 2 |
|  |  |
|  | $1-9 \quad 54 \mathrm{p}$ |
| $\left\lvert\, \begin{array}{cc} 10 \text { plus } & \mathbf{1 1 p} \\ 100 \text { plus } & \mathbf{p p} \end{array}\right.$ | 10 plus 48 p |
|  | $\underset{\text { BCi07-BC108 }}{ }$ |
| $\begin{gathered} \text { Pack of } 10 \\ 2 \mathrm{~N} 2926 \mathrm{G} \\ \text { unbranded but } \\ \text { tested } \end{gathered}$ | 1-9 BCI09 8p |
|  | $10-99$ |
|  | 100 plus $\quad 60$ |
|  | BC 182L:-3-4-212-4 |
| $\begin{gathered} \text { Unmarked but fully } \\ \text { tested } \\ 2 \mathrm{~N} 3055 \end{gathered}$ | $\begin{array}{ll}1-9 & 8 p \\ 10 & \text { plus } \\ & 7\end{array}$ |
|  | 10 plus |
|  | ck |
| $1-9 \quad 30 \mathrm{p}$ | Plastic BCl09 |
| 10 plus $25 p$ | 50 p |

## FELSTEAD ELECTRONICS (PW 63)

## LONGLEY LANE, GATLEY, CHEADLE, CHES. SK8 4EE

gelection from our List, sent free for stamped addressed envelope. (Free overseas.) Cash With order only-No C.O.D. or Caller service. Charges (Min. 6p) in brackets after all items apply to G.B. and Eire only. Regret orders under 25p plus charges unacceptable. S.A.E. pleabe for enquiries or cannot be replied to. Overseas Orders welcomed 86p; $5 \xi^{\prime \prime} 900 \mathrm{ft}$. $50 \mathrm{p} ; 7^{\prime \prime} 1200 \mathrm{ft} .56 \mathrm{p}$; LONG PLAY $5^{\prime \prime} 900 \mathrm{ft}$. $50 \mathrm{p} ; 5 \mathrm{~F}^{\prime \prime} 1200 \mathrm{ft}$. $56 \mathrm{p} ; 7^{* \prime} 1800 \mathrm{ft}$. 90p. (Charges for $5^{\prime \prime}$ and $5 z^{2}$, singles $8 p$, two to four 7 p each; fve and over 30 p the lot. For $7^{\prime \prime}$, one or two 10 p each reel, 3,4 and 5 reels 30 p the lot. 6 reels and over 35 p the lot.) Other sizes and accessories in list. CASSETTES in lib. cases for min. 5 cassettes, C60 28p, C90 38p, Cl20 48p, each ( 15 p per $5,6-1020 \mathrm{p}, 11$ and over 25 p .) Under 5 cassettes 33p, 45p and 55 p each respectively ( 1 to $4,10 \mathrm{p}$ ).
OARTRLDGES all with standard fittings and stylii. Stereo-compatible Mono GP91/SC £1-10; STEREO GP93 £1-40; Stereo Ceramic GP94 £1-95. (All at 6p each.) Comparatives (6p). DIAMOND STYLII: single tip types: Acos GP37, GP59, GP65/67, GPT1, BSR TC8/LP/ST: COLLARG O.P. and DC284, GARRARD GC2, GC8, GCS10, GCE12, RONETTE BF40, O.P. and T. PHILIPS. 3301 (3060, 3066, 3302, 3304), 3010/12/13/16, SONOTONE $19 \mathrm{~T} / 20 \mathrm{~T}$ ALL AT 40p each (6p). SAPPHIRE 17 $\frac{1}{2} \mathrm{p}$ ( 6 p ). DOUBLE TIP TURNOVER TYPES (78 sap, on other side). For ACOS GP73, GP91 (for cartridges GP93, GP94 etc) GP918C (for stereo compat. types) GP104 BSR ST4 (ST3, ST5), ST9 (ST8), ST12/14/15, SONOTONE 8TA, 9TA, 9TAHC. PHILIPS 3306 3310, 3224, 3228/22, GP2S0. GARRARD GCM21, and 22, GCS23, GKS25 and 26, GCM21T and 22T, GCM24T, GCS23. GKS25T and 26 , GCM31, GCS30, GCS35, GCS38, KS40A, KS41B ETC. ALL AT 75p (6p). SAPPHIRE 35p (6p). DOUBLE DAMOND STYLII: (same dia. tip each side: no ${ }^{\text {PICK-UP }}$ WIRE: super thin twin flex screened, sheathed, 6 p per yard (up to 6 yds., 6p. Over, charges paid. MCROPHONES: CRYSTAL: LAPEL 1 变, clip/hand, lead $3 . \bar{j} \mathrm{~mm}$
 "YLANEI" Metal, tapered with neck cord, adaptor for stand 51.50 ( 10 p ); "MIC 91 " hanildesk 81p ( $\mathrm{H}_{\mathrm{p}}$ ); "MIC 45" Curved metal hand grip $\mathbf{5 1 - 0 0}$ (10p) ALI, with leads. DYKAME: 209 Gardioh lball. $50 \mathrm{~K} / 600 \Omega$ built in volume control, on/ofi switch, special 20ft. ketal, the best value anywhere at $£ 600$ (30p); 50130 , umi-dir mesh ball $50 \mathrm{~K} / 600 \Omega$ juk plus, cable, adaptor, $£ 4 \cdot 80$ (20p); DM160, cmit-1ir, Ball mesh, 50 K, cable adaptor, jack plur, $83-90$ ( 30 p each). SPEAKERS: Very popular $12^{*}$ ROUND, fitted tweeter, 3,8 or 15 ohns (otate which) $\$ 1-87 \frac{1}{2}$ ( 30 p ) or pair for stereo $84-25$, charges paid. SMALL 21, $3 \Omega, 8 \Omega$ or $64 \Omega 2$ (state which) 40 p ( 8 p ). More speakers in List, HEADPHONES: High resistance 2000 S , widustable 81.00 (10p), EARPIECES: with lead and min. 2.5 mm or (up to 6 for 8 p any size). SOLDERING IRON: Slim, modern, British high speed, $8 \frac{1}{2}$, all parts replaceable, highest quality, fully giaranticd fillit (10p). TRANSFORMERS:
 for Gp. CONNEGTMG WIRE: Packs of 5 coils, cach coil 5yds. Asstd. cols. SOLID CORE 14p (6p). FLLXIBLS CORE 16p (8p). SUPLS THIN Hexible for transistor wiring, etc. 16p (6p). RETIACTABLE FLEXIBLE LEADS (CURLTES): With phono plug, each end, 6 fi. 24p, 12 ft . 40 p . With phono plup/phono socket other end $6 \mathrm{ft} .26 \mathrm{p}, 12 \mathrm{ft}$. 45p ( 6 p lead any typr). VIBRATORS: I $2 \mathrm{y} / 4$ pin non-synch $121 \mathrm{HD4}$, $29^{n}$ ex. pins, 30p. SAME but
 NEONS, Hy leals 10p. NEON SOREWDRIVER (pocket tester) 176 c ( 6 p either). MAINS BATMERY ELIMINATOR. Tmput $240 v$-AC. Output $3,4 \frac{1}{2}$. $6,7 \frac{1}{2}, 9$ and 12 volt D.C. by switeh selector. On/ofi switeh, pilot lamp, leads, plug to suit most cassette recorders, Our TiST
Our LIST (sue heading or sent free on request with all orders) contains, in adation to many mote of several of the above types of items, Cartridge and Stylii comparisons, Battery amplifiers (inc. steree) Condensers, Eliminators, Dials, F.M. Tuners, Indicator lamps, Intercom, Telephone amplifier and telephone pick-ups, Meters, Mike inserto, Testers, Vol. controls, Microphone and other cable, etc., etc.


Kit and wiring instrs. for 12 V windscreen wiper speed control; metal box $3 \frac{1}{4}^{\prime \prime} \times 34^{\prime \prime} \times 1 \frac{3}{4}$ " with fixing strap, relay and all compts £1-50 (post 20p).
$\frac{1}{2} \mathrm{lb}$ (min. 100) high stab resistors $\frac{1}{8} \mathrm{~W}$ to 1 W up to 2.5 M 50 p (10p post) ; $\frac{1}{2}$ lb mixed tag strips 2 to 12 way approx. 75 for £1 (10p post); spring back telephone cable, $10^{\prime \prime}$ coil ext. to 6 ft 4-core 15p (10p post) or 7 for £1 post pd.; AUDIO CONNEC. TORS, PLUGS 2-pin speaker 10p; 3-pin DIN 14p; 5-pin 17p; phono 5 p ; ${ }^{\prime \prime}$ " jack $12 \frac{1}{2} \mathrm{p} ; 2 \cdot 5 \mathrm{~mm}$ \& $3 \cdot 5 \mathrm{~mm} 6 \mathrm{p}$; METAL phono 12p $\frac{1}{4} / 12 \frac{1}{2} p ; 2 \cdot 5 \mathrm{~mm} 10 \mathrm{p} ; 3 \cdot 5 \mathrm{~mm} 12 \mathrm{p}$; SOCKETS 2-pin speaker 10p; 3 \& 5 pin DIN 9p; phono single 5p; double $7 \frac{1}{2} p$; treble 10p 4-way $12 \frac{1}{2} p$; 5-way 15p; $\frac{1}{4}$ " jack open 15p; moulded 20p; stereo open 20p; moulded 25p; LINE SOCKETS speaker, 3-pin \& 5-pin DIN 17 $\frac{1}{2}$; phono metal 12p; co-ax. T.V. plug 8p; car radio plug 6p; either socket 8p. Post 10p. any order.

MAINS TRANSFORMERS ( $240-250 \mathrm{v}$. input); postage in brackets. A. 100 v . at $100 \mathrm{ma} 35 \mathrm{p}\left(20 \mathrm{p}\right.$ ) ; B. charger 12v. $1 \frac{1}{2} \mathrm{~A}$. 60 p (20p) ; C. 200v. at 50 ma \& $6 \cdot 3 \mathrm{v}$. at 1 A . 35p (20p); D. 22v at 1A. $6 \cdot 3 \mathrm{v}$. at $2 \mathrm{~A} . \& 250 \mathrm{v}$ at 50 ma ., 75 p (25p) ; E. 250 v . at 50 ma \& 6.3 v . at $1 \frac{1}{2}$ A. 50 p (20p) ; F. $19 \mathrm{~V} \frac{1}{4}$ A. 30p (15p) ; G. 19V 2A. 75p. (20p). Deduct $10 \%$ from total bill for more than 1 trans.

Miniature A.M. transistor tuning gang, $250+250 \mathrm{pf} ; 2 \times 6$ b.a. fixings. Size $1 \frac{1}{2} \times 1 \frac{1}{4} \times$ tin.; gearing 3:1 to $\frac{9}{16}$ in. dia. moulded bush. Plastic dust cover
Plessey.
25p (post 5p).
GLADSTONE RADIO
66 ELMS ROAD, ALDERSHOT, Hants (Closed Wednesday)

## In the post

As a purchaser, in a small way of components advertised in P.W. 1 have sometimes been amazed at the varying rates of postage charged for parcels to N.Z. I therefore wrote to the Post Office, I.ondon to find out the reason.

I enclose copies of my letter and the reply.

I am sure that the advertisers are trying to act in our best interests. It is no advantage to them to pay out extra postage, but it's our money they're using!--C. J. Christie (Whangarei, New Zealand).

## LETTER TO GPO:

I should be grateful for your advice in the following problem.

I am a hobbyist meddler in things electronic and from time to time I make purchases of equipment from England.

Postage on parcels varies so much-for example: (1) Six hearing-aid inserts ( 1 oz.) Liversedge, $5 p$. (2) One integrated circuit (1 oz.) Sevenoaks, $61{ }^{2}$ p. (3) Resistance wire ( 7 ozs.) Croydon, $7^{1}{ }_{2} p$. (4) Loudspeakers (3 lb.) Liversedge, £1•23. (5) Five tape cassettes from London, 75p.

All these goods have been marked "surface mail"-not registered.
I don't object to waiting a couple of months for goods sent sea-mail but $I^{*}$ must confess to being mystified by the postages quoted.

Can you advise the most economical rate in general terms for the sort of equipment $I$ am buying please?

## REPLY FROM POST OFFICE:

We were interested to see the rates that were charged on the packets you have been receiving. Items 1 and 2, the hearing aids and integrated circuit, weighing one ounce each, should have been sent by the Letter Post at the Commonwealth Rate of 2 new pence ( $3 p$ from 1 July 1971). There was no service operating in March 1971, surface or air, by which the charges you mention of $5 p$ and $61^{1}{ }_{2} p$ could have been correctly made for these items. Although they were sent a long time ago, if you still have their
wrappings we will gladly investigate how the charges were raised. Item 3 was sent by the Small Packet service, and although you have not given us a date for the packet, the charge of $1 s 6 d$ was almost certainly correct. Item 4, the radio speakers weighing 3 lb would have been sent by the Surface Parcel Post Service for £1-15p.

The most economical service available for the sort of goods you have been receiving, including the tape cassettes, is undoubtedly the Small Packet service. This provides a cheap rate for lightweight goods (up to 2 lbs in the case of New Zealand). Small packets must be packed so that they can be easily examined without breaking any seal, and should not contain any letters or personal correspondence, although an invoice is permissible. The words 'Small Packet' should be marked on the top left hand corner. In this service a packet of cassettes weighing, say, 14 oz can be sent for $15 p$.

I enclose various leaflets showing our current charges and a photocopy of the Small Packet regulations taken from the current edition of the Post Office Guide. I am sure you will find the Small Packet service meets your needs.

## Radio fags



I enclose the photo of a packet which once held ESS-O-ESS cigarettes as I thought you might like to reproduce it in your magazine.

Whereas countless cigarette brand designs are based on ideas to do with the sea there must be few that have anything to do with radio. The only item apart from this that I know of is Wireless Mixture tobacco.

I do not know when the packet was introduced but this brand was on sale in 1939 at 3 d for 6, also 12 for 6 d and 3 for $1^{1}{ }_{2} \mathrm{~d}$. It was to disappear during the next ten years as it is not included in the 1949 retail price lists. Gallaher Ltd. are now the proprietors of Cope's brands.

One of my achievements is getting something into the Guinness Book of Records concerning wireless. I sent them an obituary from a newspaper called "the forgotten inventor." This resulted in the inclusion of details of the world's first advertised broadcast by Sir Aubrey Fessenden.-W. Humphries (Suffolk).

## She saw the light

One day a dear old lady came into our shop and asked if we could sell her a light bulb for her "loo". Upon asking what wattage she wanted she replied that she had not any idea. I then asked her to bring her old bulb into the shop so that I might try to read the wattage. At this suggestion she stepped back in surprise and flatly refused to do this. When asked the reason for her attitude she replied, "Young man, if I take the old bulb out without putting a new one in straight away, all the electricity will fall out of the socket and I'll have a big bill to pay next quarter".

It took me several minutes to explain to her that this was not the case and she went away with a new 25 W bulb in her bag which we gave her as a prize for being our 'customer of the month'.-C. Scott, (Edinburgh).

We are glad to hear that the lady went away a happy customer. If any readers have amusing stories like this, we'll be glad to consider them for our "Letters" pages-Editor.


FIFTY years ago British broadcasting was born in an ex-army hut near Chelmsford in Essex, when on 14th February 1922 a group of Marconi engineers began a series of regular experimental transmissions. Every Tuesday evening from a rigged-up transmitter, call sign 2 MT Writtle, or more affectionately to its listeners, Two Emma Tock, they transmitted programmes whose original purpose was entirely technical. Shortly afterwards, in May, another transmitter, later to be even better known, was opened up by the company at Marconi House in the Strand in London. This was the famous 2LO station that provided the foundation from which the British Broadcasting Company grew after its formation on 14th November of the same year.

Two Emma Tock provided the first regular broadcast service in this country, and incidentally broadcasting's first audience, an audience which in its enthusiasm for the pioneering programmes, generated the original demand for public service broadcasting. The 2 MT transmitter was set up for use in a series of experiments designed to establish the effective range of a wireless telephony transmitter. At the same time a number of radio amateurs were appearing, largely young ex-service men who had learnt about radio during the 1914-18 war, who had put together their own receiving sets, and who wanted transmissions to receive. Earlier experiments with entertainment, as when Dame Nellie Melba and later Lauritz Melchior, the Danish tenor, had broadcast from a makeshift studio in Chelmsford in 1920, had shown that there was a potential for wireless telephony outside official communication and naviga-


The $2 M T$ transmitter at Writtle from which the first regular broadcast transmissions in this country began on Feb. 14th, 1922.


A B.T.H. crystal receiver of 1923 vintage.
tion usage, but the official attitude had been discouraging, and the duty of granting licences for transmitters was the preserve of the Postmaster General. Government was unwilling to consider licences for more than a token number of even technical transmissions.

2MT was finally granted an experimental licence to transmit early in 1922, though the permission was hedged about with many restrictions. But for half an hour on Tuesday evenings, experiments were to be allowed, though even then with three-minute breaks in every ten, to ensure that no interference with "legitimate services" was being perpetrated.

2 MT opened regular broadcasts officially on behalf of the amateurs who needed a source against which they could calibrate their receivers, and to begin with its programmes were not very much more interesting than early 1920 transmissions made before the government clamp-down, when W. T. Ditcham read from Bradshaw's railway timetable, but the enthusiasm and gaiety of the young Marconi engineers who ran it very soon turned it into a half-hour's entertainment in its own right. The names of those men read like a roll-call of some of the great names in broadcasting. In charge of the project was Captain P. P. Eckersley, who later went to the new British Broadcasting Company as its first chief engineer. It was his infectious and spontaneous humour which gave 2MT its unique flavour; he was

## PICTURES TO BRING BACK MEMORIES



Marconi House" main entrance from the Strand (taken 1912).


The "Television Toppers" view a 23in screen. The largest at the 1953 Radio Show.


The "Roving Eye", taken in 1954


Jean Metcalf, compère of "Family Favourites"( 1954).

not only the first engineer in charge, he was also the first of the true radio entertainers, with a gift for ad-libbing that constantly alarmed those of a less adventurous disposition who worked with and around him. Others in the team were Noel Ashbridge, later Sir Noel, who was the BBC's first technical director, till his retirement in 1952, R. T. B. Wynn, a later chief engineer of the BBC and B. N. MacLarty, who became head of the BBC's Design and Installation team before he returned to Marconi's in 1947 as Engineer in Chief.

By contrast, Marconi's 2LO station, granted its licence in May, began a rather staid existence, a happy coincidence for the pioneers of 2 MT , as it gave them an opportunity to provide skits and lampoons which were much appreciated by their listeners. 2LO operated on conditions of restricted timing, at first even no music, and low power, beginning with 100 watts, later raised to $1_{2} \mathrm{~kW}$. Its programmes had each to be individually licensed by the PMG, and were limited to private occasions often for charity, at which Marconi engineers installed the receiving apparatus and operated it. Each programme was notified to listeners by postcard by means of a special mailing list kept by The Marconi Company, and most of them consisted of polite light music.

The 2LO station transmitter was designed by Captain H. J. Round, installed by C. S. Franklin and run by A. R. Burrows who eventually became the much-loved Uncle Arthur of the BBC. Among the many papers in the Marconi archives which tell the story of the birth of British Broadcasting, not the least interesting is Arthur Burrows' letter requesting permission to recruit a young man of particular quality to compere the station's programmes, a young man with "technical tendencies . . . . . grace of manner . . . . . and an excellent telephone voice." Many of Burrows' requirements were couched in terser terms and it was his organisational skill and foresight that shaped the studio techniques which are still the basis of modern broadcasting.
By this time many wireless societies had been formed and more and more the demand for radio receivers was being felt. In the United States. since 1919 "wireless" had become fashionable, but with no constitutional control of the use of wavelengths, chaos reigned in a commercially sponsored free-forall. The British Government, seeking a way from the dilemma posed by popular demand on the one hand and a justifiable reluctance to allow free access to the air on the other, set up the Wireless SubCommittee of the Imperial Communications Committee in April of 1922. After consideration, their recommendation to set up a single broadcasting company was accepted and in November 1922 the British Broadcasting Company' was formed from six commercially interested companies with $£ 100,000$ share capital.

The six companies were The Marconi Company, the Metropolitan Vickers Co., the Western Electric Co., the British Thomson-Houston Co., the Radio Communication Co., and the General Electric Co., and on its formation on 14th November a Broadcasting Committee of the founder members took over the responsibility of running 2 LO .

2MT Writtle continued to transmit until the following January, when it finally closed down.


Our favourite "dumb blonde"-Sabrina shown during rehearsals for Arthur Askey's "Before Your Very Eyes" show (1955).

We would like to thank the Marconi Company, the BBC, the Science Museum and readers whose help in compiling this article has really been appreciated.

CARIP ORT ABLE RADIO. October 1972
Readers experiencing difficulty in obtaining the oscillator coll L3 (Osmor PW/01) can use the Denco coil Type TOC1 using the following connections:Pin 1 to C3 and R3, Pin 2 to the positive line, Pin 3 to S1b, Pin 4 to IFT1, Pin 5 to Tr1 collector and Pin 6 to Tr1 emitter. (Denco Ltd, 357 Old Road, Clacton-onSea, Essex).

INTERCOMM: CALLING SYSTEM. October 1972
There is an error regarding the wiling around the secondary of T2, The loudspeaker is connected in series with the wire from pin 5 of SW1 fo the positlve The; the speakeris noticornected directly to the top of the secondary of 72

DXers AFF PROCESSING UNIT. July 1972
In Fig: 4 a break in the conductor strip should be shown at $30-9$.
1.C. AUTO PARKING LIGHT. September 1972

It has been brought to our attention that a single parking light is no longer sufficient; all four parking lights are necessary, This does not of course invalidate the circuit.

## 

## INTEGRATED CIRCUITS

Why buy alternatives when you can buy the genuine article trom us at
competitive prices from stock. BRANDED FROM TEXAS I.T.T FAIR.

## COMP官



Trpe 1/1112/2420/99

## SN7400

SN7460
SN7401
sN7402
GN7403
SN7404
SN7405
BN7406
GN7407
SN7408
SN7409
SN7409
SN7410
$\begin{array}{ll}\text { SN7411 } \\ \text { 8N7412 } \\ & 0\end{array}$
8N7412
gN7413
\&N7416
EN7416
GN7417
SN7420
SN7422
SN7423
GN7425
8N
SN7427
BN7428
SN7430
SN7
8N7432
8N7433
SN7433
SN7437
SN7438
SN7440
$\begin{array}{lllll} & \\ \text { BN7442 } & 0-74 & 0.72 & 0.70 \\ \text { BN } & 0.75 & 0.72 & 0.70\end{array}$
$\begin{array}{llll}\text { SN7443 } & 1.00 & 0.05 & 0.00 \\ \text { SN7445 } & 2.00 & 1.75 & 1.80\end{array}$
$\begin{array}{llll}\text { SN7446 } & 2.00 & 1 \cdot 75 & 1.60\end{array}$

| SN7448 | 1.75 | 1.60 | $1-45$ | SN74141 | 1.00 | 0.95 | 0.90 | SN74199 | 4.60 | $3 \cdot 70$ | 3.35 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

## Type 1/11 12/24 25/90

## 99 Typ

 $\begin{array}{lll}p & 0.18 & 0.16 \\ 0 & 80 & 0.18 \\ 0\end{array}$ $\begin{array}{lll}.20 & 0.18 & 0.16 \\ .20 & 0.18 & 0.16 \\ .20 & 0.18 & 0.16 \\ .20 & 0.18 & 0.16 \\ .20 & 0.18 & 0.16 \\ .30 & 0.27 & 0.25 \\ .30 & 0.27 & 0.25 \\ .20 & 0.19 & 0.18 \\ .45 & 0.42 & 0.85 \\ .20 & 0.18 & 0.18 \\ .23 & 0.28 & 0.20 \\ .42 & 0.40 & 0.85 \\ .30 & 0.27 & 0.25 \\ .30 & 0.27 & 0.25 \\ .30 & 0.27 & 0.25 \\ .20 & 0.18 & 0.16 \\ 48 & 0.44 & 0.40 \\ .48 & 0.44 & 0.40 \\ .48 & 0.40 & 0.35 \\ .42 & 0.39 & 0.35 \\ 50 & 0.45 & 0.42 \\ 20 & 0.18 & 0.16 \\ 42 & 0.39 & 0.35 \\ 70 & 0.61 & 0.44 \\ 65 & 0.60 & 0.50 \\ 65 & 0.60 & 0.30 \\ 20 & 0.18 & 0.16 \\ 74 & 0.72 & 0.70 \\ 75 & 0.72 & 0.70 \\ 00 & 0.96 & 0.90 \\ 00 & 1.75 & 1.60 \\ 00 & 1.75 & 1.60 \\ 76 & 1.60 & 1.45 \\ 75 & 1.60 & 1.45\end{array}$
## rovorin

1/1112/2425/99 \begin{tabular}{llll}
\& gN7450 \& 0.20 \& 0.18 <br>
\hline

 

\& SN \& P \& 9 <br>
SN74145 \& $1 \cdot 50$ \& $1 \cdot 40$ \& $1 \cdot 30$ <br>
SN74150 \& $8 \cdot 36$ \& $2 \cdot 95$ \& $2 \cdot 16$ <br>
SN74151 \& $1 \cdot 10$ \& 0.95 \& 0.90 <br>
SN74153 \& $1 \cdot 36$ \& 1.27 \& $1 \cdot 20$
\end{tabular}

PLESSEY INTEGRATED CIRCJIT
8 Wats Amplifer SL409D 8 Watt AmpliAer SL408
Complete with S-page Complete with 8-p
Dooklet, circuits booklet, el
and dsta and dsta
5.50 TRIACS
STUD WITH
TRIACS
STUD WITH ACCESSORIES $\begin{array}{lrr}\text { Type } & \text { Volts } & \text { Price } \\ \text { P.I.F. } & \text { 1-11 }\end{array}$

| $\begin{array}{llr}\text { Type } & \text { Volts } \\ \text { P.I.V. } & \text { Price } \\ & \text { 1.11 }\end{array}$ |  |  |
| :---: | :---: | :---: |
| 3 AMP RANGE |  |  |
| SC35A | 100 75p |  |
| 8C35B | 200 79\% |  |
| EC35D | $400 \quad 85 \mathrm{p}$ |  |
| 6 AMP RANGE (2048) |  |  |
| SCA0A | 100 85p | 3 |
| SCl0B | 200 00p |  |
| $8 \mathrm{SC40D}$ | 400 \$1.00 | 3 Amp |
| SC40E | 500 81.20 | 1048 |
| 10 AMP RANGE (TO48) T048 |  |  |
| 8C45A. | 100 95p |  |
| $8 \mathrm{C45} \mathrm{~B}$ | 200 \$1.00 |  |
| SC45D | $400 \quad 21.25$ |  |
| 8C45E | 500 \$1.45 |  |
| 15 AMP RAMGE (T048) |  |  |
| EC50A | 100 \$1.25 |  |
| AC5OB | 200 \$1-35 |  |
| 8C50D | 400 \&1.65 |  |
| SC50E <br> DIAC D32 | $500 \quad 21.85$ |  |
|  | DIAC D32 25p |  |
| TRIACS- |  |  |
| Additional | Types |  |
| 40430 | (TOB6) 85p | 15 Amp |
| 40669 | (Plastie) | Amp |
| 40486 | (TOS) $\begin{array}{r}81.00 \\ 80 p\end{array}$ | T048 |

## NEW BRIDGE RECTIFIERS SMALL SIZE AND LOW COST

## DIODES

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BZY 88 Range
All voltages
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LOW PROFILE PLATED PINS
(16 Lead
D.T.L.) 7400 SERIES ARE CALCULATED ON THE
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HIGH POWER SN 74 HOO, Now in stock-send
LOW POWER SM 74 LOO $\}$ for list No. 36
ALCTION SKOM STOCK
$\begin{array}{ccc}\text { 17p } & \text { D.I.L.) } & \text { (8 Lead } \\ \text { D.I.L.) } \\ \text { 15p } & \text { 15p }\end{array}$

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## SPECIAL OFFERS

MEL12 50p LM301A 90p $\begin{array}{lrr}\text { EM401 } & \text { 8p } & 2 N 5459\end{array}$ MA741 34p 2 N 3643

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UA709 31p UA748
IM. MTrimpots
" Stereo.
Complete kit of Semiconductor 66.30
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SIGNETICS NES55V Timer
first time offered to constructors. Features
*Timing from microseconds through I Hr.

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| SEMICONDUCTORS |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AAII9 | 9 p | BCl36 | 20p | BF161 | 45p | OABI | 0 p |
| AAYII | 10p | BC137 | 20p | BF178 | 25p | OA85 | 12p |
| AAY30 | 10p | BC139 | 25p | BF179 | 30p | OA90 | 8p |
| AAZI3 | 10 p | BC142 | $21 p$ | BF180 | 35 p | OA91 | 7 P |
| AC107 | 34p | BC143 | 23 p | BFI84 | 20p | OA95 | 7p |
| ACl 26 | 25p | BC147 | 12 p | BFI85 | 20p | OA200 | 7p |
| AC127 | 25p | BC148 | 10 p | BF194 | 15p | OA202 | 10 p |
| ACl28 | 25 p | BC149 | 120 | BF195 | 15p | OAZ223 | 45p |
| AC141K | 25p | BC152 | 20 p | BF196 | 15p | OAZ230 | 45p |
| AC142K | 18p | BC153 | 20p | BF197 | 15p | $\bigcirc{ }^{\circ} 28$ | 65p |
| AC153 | 25p | BC157 | 15p | BF200 | 35p | $\bigcirc{ }^{\circ} \mathrm{C} 35$ | 50p |
| AC153K | 22p | BC158 | 12p | BF222 | 30p | OC36 | 65p |
| AC175K | 36p | BC159 | 15p | BF224] | $15 p$ | OC44 | 15p |
| AC176 | 25p | BC170 | 15 p | BF256L | 30p | OC45 | 15p |
| AC176K | 20p | BC171 | 15p | BF256LC | 34 p | OC70 | 15p |
| AC187 | 25p | BCI71A | 17p | BFS 36A | 37p | OC71 | $11 p$ |
| ACligk | 25p | BC177 | 20p | BFW17A | ¢1.22 | 0 O 74 | 25p |
| AC188K | 25p | BC177B | 23p | BFX37 | 30p | OC75 | 23p |
| AC193K | 25p | BC178B | 16p | BFX84 | 23p | 0 OCl 70 | 23p |
| AC194K | 27p | BC179 | 20p | BFX85 | 25p | R2008 | ¢3.5 |
| ACY20 | 20p | BC182L | 10p | BFY50 | 20p | R2009 | E2.5 |
| ${ }^{\text {ACM }}$ A 1 | ${ }^{20} \mathrm{p}$ | $\mathrm{BC}_{\mathrm{BC} 182 \mathrm{LB}}$ | 10 p | BFY51 | 20 p | R2010 | E2.5 |
| ACY22 | 12p | $8 C 183$ $\mathrm{BC1} 18$. | ${ }_{10 p}^{10 p}$ | BFY52 | ${ }^{20}{ }^{59}$ | ${ }_{\text {SP8385 }}^{\text {TAA }}$ | ¢1. $\pm 2.4$ |
| ADI61 | 35p | BC183LB | 10 p | BS $\times 20$ | 15p | TAD100 | $\pm 1.3$ |
| AD162 | 35p | BC184LC | 12 p | BSX60 | 50p | TBA500 | E2.0 |
| AFll 5 | 25p | BC186 | 25p | BS $\times 61$ | 35p | TBA510 | E2.0 |
| AF117 | 20p | BC187 | 25p | BT106 | 85p | TBA520 | E2. 5 |
| AF121 | 30p | BC208A | 14p | BU105/02 | 62 | TBA520Q | ¢2. 5 |
| AF124 | 25p | BC212 | 10 p | BY126 | 15p | TBA530 | ¢1.8 |
| AF126 | ${ }^{20} \mathrm{p}$ | BC212L | 12p | BY127 | 15p | TBA530Q | ¢1.8 |
| AF 127 | ${ }^{20} 9$ | $\mathrm{BC2}^{\text {B } 2 \mathrm{LA}}$ | 13 p | BY147 | 61.04 | T8A540 | ¢2.0 |
| AF139 | ${ }^{30} \mathrm{p}$ | BC213L | 12p | BY164 | 35p | TBA550 | E3.0 |
| AFi79 | 25p | BC214 | 15p | BZY88 ser | 9.5 p | TBA5500 | ¢3.0 |
| AF178 | 55p | BC214L | 15p | BZY94 ser |  | TBA570Q | c1. 2 |
| AF170 | 60 p | ${ }^{\text {BC2 } 250 B}$ | 14p | BR100 | 26p | TBA750 | ¢1.4 |
| AF239 | 40 p | BC261 | 16p | BRC4443 | ${ }^{90}$ | TBA750Q | 61.4 |
| AsZ17 | 50p | BC268 | 11 p | BRY39 | 30p | TIC46 | 40 p |
| BA102 | 30p | BC308A | 17p | E1222 | 40 p | TIP29A | ${ }^{50} \mathrm{p}$ |
| BA145 | 15p | BC317 | 20p | E5024 | 40 p | TISSOM/6 |  |
| BA148 | 15p | BCY21 | 96p | GET102 | 39 p | T1561 | 20p |
| BA154 | 9 p | BCY31 | 40p | GET103 | 25p | Tis91 | 17p |
| BA155 | 10p | BCY42 | 30p | IS921 | 8p | 2 N 404 | 15 p |
| BA163 | 90 p | BCY70 | 15p | IS923 | 12 p | 2N697 | $12 p$ |
| BAX12 | 12p | BCY71 | 20p | ME0404 | $11 p$ | 2N706 | 9 p |
| BAW63 | 36p | $\mathrm{BCY}^{\text {Cl }}$ | 15p | ME0412 | 15p | 2 N 708 | 12 p |
| BAW65 | ${ }^{36 p}$ | BCY89 | ${ }^{975}$ | ME0413 | 12 p | 2N753 | 10 p |
| BAW67 | 35p | BDII 5 | 75p | ME0462 | 19p | 2 N 919 | 45p |
| BB105 | 37p | BD124 | 80 p | ME2002 | 8 pp | 2 N 920 | 42p |
| BBY20 | ${ }^{37} \mathrm{P}$ | 8Di31 | 75p | ME4003 | 12 p | 2 N 1302 | 17 p |
| ${ }^{\text {BC }} 107$ | 10 p | BD 32 | ${ }^{80 p}$ | ME4102 | 10 p | 2N1304 | $21 p$ |
| BC1078 | 12 P | 8D135 | 75p | ME4104 | 8 p | 2 N 1306 | 24p |
| BC108 | 10 p | 8Dis | 44 p | ME6002 | 12 p | 2N1307 | $24 p$ |
| BC108A | ${ }^{10} \mathrm{p}$ | BD181 | ${ }^{90}$ | ME6101 | 12 p | 2N1308 | 24 p |
| BC108C | 15p | BD184 | ¢1.3 | ME6102 | 13 p | 2N1309 | 24 p |
| BC109 | 12 p | BFI21 | ${ }^{25}$ p | ME8001 | 12 p | 2N3053 | 20p |
| $\mathrm{BC}^{8} 13$ | 15 p | BF 123 | 30p | ME8003 | 13 p | 2N3054 | 50p |
| BC116 | $20 p$ | BF 25 | 25p | MEF104 | $34 p$ | 2N3055 | 55p |
| BC117 | ${ }^{20} \mathrm{p}$ | BF 127 | 30p | MELI | ${ }^{30} \mathrm{p}$ | IN914 | 6p |
| BC 119 BC 121 | 30p | BF/53 BFI54 S | $20 p$ $20 p$ | MP8112 MP813 | 34 p 40 | IN9:6 | \%pp |
| BC\|25B | 25p | BF160 | 25p | OA47 | 10p | IN4148 | 6 p |

TERMS. Retail mail order subject to $£ 1.00$ minimum order. Cash with order only. Trade and educational establishments M/AC On application (minimum 65 ). Postage 10 p inland, 25 E Europe. GUARANTEE. All goods carry full manufacturer's war
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TRANSISTORISED F.M. tuner head with A.M. gang; slow motion drive. 88-108Mcs, with circuit diagram. $£ 2$ 10p.
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SPECIAL OFFERS of Unmarked Tested Power Transistors. 2N3055 Silicon NPN 30p each 4 for Ef:
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1 off 6 transistors single wave band
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Encapsulated bridge rectifier (itt usd 3 3mdh) 100 PIV 2 amps. 50p each.

Transistor F.M. Stereo Multiplex Decoder. Size: $5 \frac{1}{1} \times 2 \frac{1}{7} \times 1 \frac{1}{2}$. As used in well known British stereo units with circuit. £3 75.
GARRARD SP25 MK. II less Cartridge. $\mathbf{x 1 0} 50$.
10 VOLUME CONTROLS consisting of 2 off each.
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10 COMPUTER PANELS packed with conaponents including one panel with 2 Power Transistors. £1 00.

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## TAPE HEADS

We are gradually obtaining more information about the Truvox tape heads we have, we are told that these have been wound in a very
ingenious way so that winding may be coupled efther in parallel or in series depending whether high or low impedance is required. We also have matching erase heads and now offer these in pairs. 1 record and 1 erase head. Price of the 2 track 45 p per pair. 4 track 75 p per pair. Pair mounted on plate 45p extra.

I R.P.M. MOTOR
Made by the famous smiths Company. 240v. 50 cycle mains working. Ideal motor to drive clock mechanisms. Price 81 each or 10 for 29 . DRILL NTROLLER
 NEW IKW MODEL Electronically changes speed from approxi-
mately 10 revs. to mately 10 revs. to maximum. Full power at all speeds by finger-lip
control. Kit includes and parts, case, everything and 13 p post and insurance. Made up model also avail-
able. 42.25 pius 13 p post $\&$ p. MAINS OPERATED CONTACTOR $220 / 240 \mathrm{v} .50$ cycle solenoid with operation. Closes 4 circrits each rated at 10 amps. Extremely well made by a German Electrical Company. Overal size $2 \frac{1}{2} \times 2 \times 2 \mathrm{in}, 21.50$ each.
HIGH ACCURACY THERMOSTAT Uses differential comparator 1.C. with thermister as probe. Designer claims temperature control to within $1 / 7$ th of a degree. Complete kit with power pack $\mathbf{6 5} 50$. AUTO-ELECTRIC CAR AERIAL B with dashboard control switch-fully extendable to 40 in or fully
retractable. Su itable for 12 y positive retractable. Suitable for $12 v$ positive
or gegative earth. Supplied complete with fitting instructions and ready wired dashboard switch. $85 \cdot 75$ plus 25p post and insurance.


WATERPROOF HEATING 26 yards length $70 w$. Self-regulating
temperature control. 50 p post free.

MULTI-SPEED MOTOR Replacement in many well-known food mixers. Six speeds are available 500,850 and $1,100 \mathrm{r} . \mathrm{p} . \mathrm{m}$. from (where the beaters of the food (Where the beaters of the food
mixer normally go) and 8,000 , mixer $\& 15,000$ go from the main drive shaft. This drive shaft is $\frac{i n}{}$. diameter and approximately 1 in . long. A further point about this motor is that being $230 / 240 \mathrm{v}$. AC-DC series wound its speed may be further controlled with the use of our Thyrister controller. This is a very powerful and useful
motor size approx. 2 in. dia. $\times 5$ in. lonr, mains motor size approx. 2 in. dia. $\times 5$ in. long, mains
$230 / 240 \mathrm{v}$. Price 88 p plus 23 p postage and insurance, 12 or more post free.

## I5A ELECTRICAL PROGRAMMER



Learn in your sleep: Have radio playing and kettle boiling as you awake-switch
on lights to ward off intruders on lights to ward off intruders come home to. All these any many other things you can do if you invest in an electrical programmer. Clock by famous maker with 15 amp. on/off switch. Switch on time can be set anywhere to stay on up to 6 hours. Independent 60 minute $20 \mathrm{p} p$ \& $p$ or with glass front chrome bezel 75 p extra.

0-8 AMMETER 2in. square full vision for flush
mounting. Moving iron instrument. Ideal for charger. Price 60 p each 10 for $85 \cdot 40$.

## NUMICATOR TUBES

For digital instruments, counters, timers, clocks, etc. Hi-va
each. 10 for $£ 13$.

I2 WAY SUB-MINIATURE MULTI-CORE CABLE 7.0076 copper cores each core P.V.C. insulated and of difierent colour. Pick. Price 20 p per yard


LIGHT CELL
Almost zero resistant in sunlight increases to 10 K ohms light increases to 10 K ohms
in dark or dull light, epoxy resin sealed. Size approx. Rated at 500 MW , wire ended. 43 p with circuit Also ORP 12 light cell 45p.

BAKELITE INSTRUMENT CASE
Size approx. $6 \frac{1}{n}^{\prime \prime} \times 3 \frac{7}{4}^{\prime \prime} \times 2^{n}$
deep with bras inserts in deep with brass inserts in panel. This is a very strong case suitable to house instruments and special rigs, etc. Price 45p each.

## MULLARD $4+4$ UNILEX AMPLIFIER



We demonstrate these daily and almost always a sale results; it really is a crackjng amplifier. Only Mullard with their know how could have made it possible at this low price. SPEC.: Mains operated. 4 watts music or speech per channel. Double wired power supply eliminates 16 Khz . Input suitable for pick-up tuner or microphone. 6 month guarantee. Only $88.85+30 \mathrm{p}$ postage and insurance.

## THYRISTOR I.IGHT DIMMER

For any lamp up to 200 w . Mounted on switch plate to fit
in place of standerd switch. Virtually no radio interferences. in plese i2.95, plus 20 p post and insurance.

## TANGENTIAL HEATER UNIT'S



This heater unit is the very latest type, most efficient, and quiet running. Is a s fitted in Hoover and blower heaters costing $£ 15$ and more. We have a few only Comprises motor, impeller, 2 kW . element and 1 kW . element a llowing switching 1 , 2 and 3 KW . and with thermal safety cut-out. Can be fitted into any metal line


## DISTRIBUTION PANELS



Just what you need for work bench or lab.
$4 \times 13 \mathrm{amp}$ sockets in metal box to taike
tandard 13 amp fused plugs and on/off switch with neon warning light. Supplied tandard 13 amp fused plugs and on/ofn switch with to work, $22 \cdot 25$ plus $23 \mathrm{p} \mathbf{P}$. \& I THIS MOTe with 6 feet of flex cable. WIH'S SNIP

## BATTERY MOTORS

A bargain parcel of 7 motors for $\$ 1$. Some not as large as a postage stamp and only $\frac{3}{8}{ }^{\prime \prime}$ thick, largest is $1 \frac{1}{z^{\prime \prime}} \times 1 \frac{i^{\prime \prime}}{}$ dia. Some work off $1 \frac{1}{2} v$. some as high as 18 v . These motors are used in racing cars, power toys, etc. The This is a 4 pole motor, optimum working $16 \cdot 5 \mathrm{v}$, but very powerful even as low as $4 \pm \mathrm{v}$.
as low as $4 \dot{t} v$.
Don't miss this wonderful snip.


REPEATING TIME SWITCH
1 or 2 on, off per 24 hours. Repeats until re-programmed. Switches up to 15 amp . Switching time completely adjustable through 24 hours. Precision made with 24 hour dial. Minia-ture-will fit into 2ins. cube. Mains operated clock but switch may be isolated for switching battery sets. Ideal
for: shop window lighting, anti-thief devices, central for: shop window ighting, antior automatic processes heating contro and many other automatic processe
STANDARD WAFER SWITCHES
Standard size $1 \frac{1}{2}{ }^{\prime \prime}$ wafer-silver-plated 5 -amp contact
standard sas" spindle $2^{\prime \prime}$ long-with locking washer and nut.


| No. of Poles | 2 way |
| :---: | :---: |
| 1 pole | 40p |
| 2 poles | 40p |
| 3 poles | 40p |
| 4 poles | 40p |
| 5 poles | 40 y |
| 6 poles | 40p |
| 7 poles | 70 p |
| 8 poles | $70 p$ |
| 9 poles. | 70p |
| 10 poles | 70 p |
| 11 poles | 70 p |
| 12 poles | 70p |


| ay 4 way 5 |  |
| :--- | :--- |
| 40 p | 40 p |
| 40 p | 40 p |
| 40 p | 40 p |
| 40 p | 40 p |
| 40 p | 70 p |
| 70 p | 70 p |
| 70 p | 70 p |
| 70 p | 70 p |
| 70 p | 95 p |
| 70 p | 95 p |
| 85 p | 95 p |
| 95 p | 95 p |


|  |  |  |
| :---: | :---: | :---: |
| P | 40 p | 40p |
| D | 40p | 40 |
| p | 40p | 70 |
|  | 70 p | 700 |
|  | 70p | 95 |
|  | 70 | 95 D |
|  | 95p | 21-20 |
|  | 95p | £1.20 |
|  | 95 p | 81-45 |
|  | 81.20 | \$1.45 |
|  | 81.20 | E1.70 |
|  | \&1 | \$1.7 |

$W a y$
40 p
40 p
70 p
70 p
95 p
$9 . \mathrm{p}$
5120
51.20
51.45
51.45
5170
51.70

 40 p
70 p
$95 p$
81.20
81.45
81.70
.1 .95
42.20
82.45
32.70
22.85
83.20


MULLARD AUDIO AMPLIFIERS All in module form, each ready built complete
with heat sinks and connection tags, data supwith
Model 1163500 m watt power output 75 p .
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Model EP9000 4 watt power output $\mathbf{8 1} \cdot \mathbf{4 5}$.
$10 \%$ discount if 10 or more ordered

## Square, panel mounting type. $£ 2$

## INTEGRATED CIRCUIT DIAGRAM

A parcel of integrated circuits made by the famous Plessey Company. A once-An-arlifetime offer of Micro electronic devices well below cost of manufacture. The parcel contains 5 ICs all new and perfect, first-grade device, definitely not sub-standard or seconds. 4 of the ICs are single silicon chip GP amplifiers. The סth is a monolithic NPN matched pair. Regular price of parcel well over 25. Full circuit detalls of the IC's are included and in addition you will receive a list of many different IC's available at bargain prices $25 p$ upwards with circuits THIS TERRIFIC BARGATN.

MULLARD I.F. MODULE
This is a fully screened intermediate frequency module
for amplification and detection of f.m. signals at 10.7 MHz


5 A changeover contacts. 9 p 10 p each or $\$ 1.05 \mathrm{doz}$.

NEED A SPECIAL SWITCH?
Double Leal Contact. Very slight pressure closes each, 60p doz. Plastic pushrod suitable for operating 5p each, 45 p doz.

## PRESSURE SWITCH

Containing a 15 amp, change over switch operated by a diaphragm which in turn is operated by air Dressure. The operating pressure is
adjustable but is set to operate in
 approx. 10 in. of water. These are quite low pressure devices and can in lact be operated simply by blowing into the inlet tube. Original when tub has reached correct level but no doabt has many other appliontions has many ot

SWITCHES ? ? ? We could fill this whole page with all the you want send for our switch list.

TMED "OX" SWITCEES
Made by Smiths for washing machines, etc. Centre spindle closes double pole 15 amp switch directly it is turned. A full $360^{\circ}$ turn or only a part turn winds the clockwork mechanism and to the "off" position. A dial theretore could be fitted to indicate hours and minutes and the switch on period could be set quite accurately 3 models a vailable- 90 minutes, 120 minutes and 360 minutes. Price 950 each. Metal clad pointer knob 15p. Suitable relay to make the switch on" instead of "off" 35p.

## LEVER SWITCH-Ref. H52/4

Ideal for intercom or similar. Pressing the lever down operates 6 pairs of change-over contacts, pressing the lever up operates 4 pairs of change over contacts. The switch is spring loaded and Size approximately $1 \frac{1}{2}^{\prime \prime}$ long $\times 2 \frac{1^{\prime \prime}}{}$ deep $\times \frac{\frac{1}{2}^{\prime \prime}}{}$ thick. 40p each.
5 PUSH BUTTON SWITCEES
Mains, suitable for audio or R.F. Each switch rated at $250 \mathrm{v}, 15 \mathrm{amps}$. 1st (black push button) closes 2 circuits, 2nd (White push button) operates one change-over, 4 th (white Dush button) open one circuit. Note; all depressed buttons remain down until cleared by the 5 th (red button) Further note: It is a relatively easy job to alter the position of the tags thus making the switche suit your circuit. Fitted with 3 white, 1 red and

PUSH OPERATED MICROSWITCH
Change over contacts, spring return when plunger released. Also fitted with lamp holder to take Lilliput lamp in plunger: flxing is by locknut through si" hole. Price 25p each or 10 for 22.25 22-POSITION SOLENOID OPERATED STUD SWITCH
Mains operated, each current pulse to switch solenoid moves switch arm through one position on to the next contact stud-current to release solenoid brigs back but in good working These are ex-quiprould be replaced. Price 50p

SNAP ACTION SLIDE SWITC
Rated 5 a. 240v. Made by Arrow.
Type fitted in the handles of electric drilis, vach.
and a.m. signals at 470 kHz . The Cist stage
i.f. amplifier for f.m. and a self oscillating mixer for a.m. 85 each. 10 tor $£ 7.85$. 100 for $£ 62 \cdot 50 \mathrm{p}$. With connection dig.

[^3]
## Sinclair Project 60



Built and tested post free £5.98

The value of an efficient filtering system cannot be over emphasized in these days of very high quality reproduction since there are so often occasions where its use can mean the difference between comfortable and uncomfortable listening. On the low pass side the Sinclair A.F.U. will effectively reduce hiss from radio or tape, cut out heterodyne whistles on A.M. reception, greatly reduce record surface noise and other imperfections ; on the high-pass side it will cut out motor rumble and other spurious low frequency intrusion. The unit is for use between pre-amp (including tape pre-amps) and power amplifiers, and operates in two sections, both stereo. The cut-off frequencies are continuously variable, and since attenuation in the rejection band is rapid ( $12 \mathrm{~dB} /$ octave) there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is as easy to mount as the stereo 60 pre-amp/control unit which it matches in styling, along with the Stereo FM Tuner.

## SPECIFICATIONS

The A.F.U. employs two Sallen and Key type active fiter stages, one rumble (high pass) and one scratch (low pass). The two stages use complementary transistors to minimise distortion.
Supply voltage: 15 to 35 volts. Current 3 mA maximum.
Gain at $1 \mathbf{k H z}$; Filters flat $0.98(-0.2 \mathrm{~dB})$
HF cut off: ( -3 dB ) variable from 28 kHz to 5 kHz at $12 \mathrm{~dB} /$ octave.
LF cut off: ( -3 dB ) variable from 25 Hz to 100 Hz at $12 \mathrm{~dB} /$ octave.
Distortion: at 7 kHz ( 35 voit supply) $0.02 \%$ at fated output.


Having introduced Integrated Circuits to hr-fi constructors with the IC.10, the first time an IC had ever been made available for such purposes. we have followed it with an even more efficient version, the Super IC. 12 , a most exciting advance over our original unit. This needs very few external resistors and capacitors to make an astontshingly good high fidel.ty amplifier for use with pick-up. F.M. radio or small P.A. set up. etc. The free 40 page manual supplied, details many other applications which this remarkable IC. make possible. It is the equivalent of a 22 tran
sistor circuit contanned within a 16 lead DIL package, and the finned heat Sink is sufficient for all requirements. The Super IC. 12 is compatible with Project 60 modules which wauld be used with the $Z .50$ and $Z .30$ amplifiers. Complete with free manual and printed circuit board

## SPECIFICATIONS

Output power: 6 watts RMS continuous ( 12 watts peak). $6-8 \Omega$. Frequency Response: 5 Hz to $100 \mathrm{KHz} \pm 1 \mathrm{~dB}$. Total Harmonic Distortion: Less than $1 \%$. (Typical $0.1 \%$ ) at alf output powers and frequencies in the audio band (28V) Load Impedance: 3 to 15 ohms. Input ImLoad Impedance: 3 to 15 ohms. Input lmpedance: 250 Kohms nominal. Power Gain
90 dB ( 1.000 .000 .000 times) after feedback Supply Voltage: 6 to 28 V . Quiescent current: 8 mA at 28 V . Size: $22 \times 45 \times 28 \mathrm{~mm}$ including pins and heat sınk..
Manual available separately 15 p post free.
With FREE printed circuit board and 40 page manual.
f2.98
Post free

## Project 605

The easy way to buy and build


Project 60
Project 605 is one pack containing: one PZ5. two Z30's, one Stereo 60 and one Masterlink. This new module contains all the input sockets and output components needed together with all necessary leads cut to length and fitted with neat little clips to plug straight on to the modules Thus all soldering and hunting for the odd part is eliminated. You will be able to add further Project 60 modules as they become available adapted to the Project 605 method of connecting.
Complete Project 605 pack with
comprehensive manual, post free
and $£ 29.95$ comprehensive manual, post free
Everything you need to assemble a superb 30 watt high fidelity stereo amplifier without having to solder.

# the world's most advanced high fidelity modules 

## Z.30 \& Z.50 power amplifiers

The $Z .30$ and $Z .50$ are of advanced design using silicon epitaxial planar transistors to provide unsurpassed standards of performance. Total harmonic distortion is an incredibly low $0.02 \%$ at 15 w ( $8 \Omega$ ) and all lower outputs. Whether you use $Z .30$ or $Z .50$ amplifiers in your Project 60 system will depend on personal preference, but they are the same size and are intended for use principally with other units in the Project 60 range. Their performance and design are such, however, that $Z .50$ s and $Z .30$ may be used in a far wider range of applications.
SPECIFICATIONS ( 2.50 units are interchangeable with $Z .30 \mathrm{~s}$ in al/ applications).- Power Outputs: Z. 3015 watts R.M.S. into 8 ohms using 35 volts: 20 watts R.M. S. into 3 ohms using 30 voits. Z. 5040 watts R.M.S. into 3 ohms using 40 volts. 30 watts R.M.S. Into 8 ohms using 50 volts.

Frequency response: 30 to $300.000 \mathrm{~Hz}+1 \mathrm{~dB}$. Distortion: $0.02 \%$ nnto 8 ohms . Signal to noise ratio: better than 70 dB unwerghted. Input sensitivity: 250 mV into 100 Kohms (for 15 w into $8 \Omega$ ). For speakers from 3 to 15

## ohms impedance. Size: $14 \times 80 \times 57 \mathrm{~mm}$.

## Stereo 60 Pre-amp/control unit

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Designed specifically for use on Project 60 systems, the Stereo 60 is equally suitable for use with any high quality power amplifier. Since silicon epitaxial planar transistors are used throughout, a really high signal-to-noise ratio and excellen: tracking between channels is achteved. Input selection is by means of press buttons, with accurate equalisation on all input channels. The Stereo 60 is particularly easy to mount
SPECIFICATIONS-Input sensitivities: Radio - up to 3 mV . Mag. p.u. 3 mV : correct to R.l.A.A. curve $+1 \mathrm{~dB}: 20$ to $25,000 \mathrm{~Hz}$. Ceramic $p u$. $-u p$ to 3 mV . Aux - up to 3 mV . Output: 250 mV . Signal to noise ratio: better than 70 dB Channel matching: within 1 dB . Tone controis: TREBLE +12 to -12 dB at 10 KHz . BASS 12 to -12 dB at 100 Hz Front panel: brushed alumnnum with black knobs and controls. Size: $66 \times 40 \times 207 \mathrm{~mm}$.


## Project 60 Stereo F.M. Tuner

The phase lock loop principle was used for recesving signals from space craft because of its vastly improved signal to notse ratio. Now. Sinclatr have applied the principle to an F.M. tuner with fantastically good results. Other advanced features include varicap diode tuning, printed circuit colls, an I.C. in the speclally designed stero decoder and switchable squeich circuit for silent tuning between stations. In terms of high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically. a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with most other high fidelity systems.
SPECIFICATIONS-Number of transistors: 16 plus 20 in $1 . \mathrm{C}$. Tuning range: 87.5 to 108 MHz Sensitivity: $7 \mu V$ for lock-in over full deviation. Squelch level: Typically $20 \mu \mathrm{~V}$ signal to noise ratio: $>65 \mathrm{~dB}$. Audio frequency response: $10 \mathrm{~Hz}-15 \mathrm{KHz}$ ( $\pm 1 \mathrm{~dB}$ ). Total harmonic distortion: $0.15 \%$ for $30 \%$ modulation. Stereo decoder operating level: $2 \mu \mathrm{~V}$. Cross talk: 40 dB . Output voltage: $2 \times 150 \mathrm{mV}$ R.M S. maximum


## Power Supply Units

Designed specifically for use with the Project 60 system of your choice. Use. PZ. 5 for normal Z.30 assemblies and PZ. 6 or PZ. 8 where a stabilised supply is essential.
Typical Project 60 applications

| System | The Units to use | together with | Units cost |
| :---: | :---: | :---: | :---: |
| Simple battery record player | 2.30 | Crystal P.U., 12 V battery volume control, etc. | £4.48 |
| Mains powered record player | 2.30.PZ.5 | Crystal or ceramic P.U. volume control, etc. | £9.45 |
| 12 W . RMS continuous sine wave stereo amp. for average needs | $\begin{aligned} & 2 \times 2.30 \text { s, Stereo } \\ & 60: \text { PZ.5 } \end{aligned}$ | Crystal, ceramic or mag. P.U., F.M. Tuner, etc. | £23.90 |
| 25W. RMS continuous sine wave stereo amp. using low efficiency (high performance) speakers | $\begin{aligned} & 2 \times 2.30 \mathrm{~s} \text {, Stereo } \\ & 60 ; \text { PZ. } \end{aligned}$ | High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc, | £26.90 |
| 80W. (3 ohms) RMS continuous sine wave de luxe stereo amplifier. (60W. RMS into 8 ohms) | $2 \times 2.50 \mathrm{~s}$, Stereo 60; PZ.8, mains transformer | As above | £34.88. |
| Indoor P.A. | Z.50, PZ.8, mains transformer | Mic., guitar, speakers, etc., controls | £19.43 |

[^4]PZ. 530 voits unstabilised $\mathbf{£ 4 . 9 8}$ P2.5 30 voits unstabilised $£ 4.98$
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$\mathbf{E} 7.98$ PZ. 845 volts stabilised (lessmans transformer) $£ 7.98$ $\mathbf{P Z . 8}$ mains transformer $\mathbf{£ 5 . 9 8}$

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1 mA
5 mA
$\begin{aligned} & 10 \mathrm{~mA} \\ & 50 \mathrm{~mA}\end{aligned}$
$\begin{aligned} & 50 \mathrm{~mA} . \\ & 100 \mathrm{~mA}\end{aligned}$
500 mA
$\begin{aligned} & 1 \mathrm{amp} . \\ & 5 \mathrm{amp} .\end{aligned}$



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