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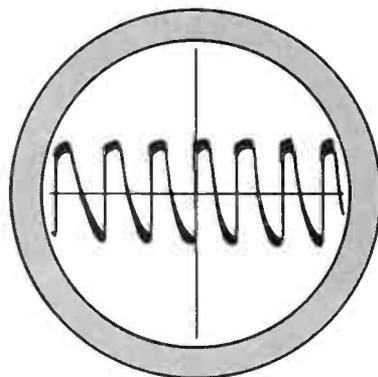
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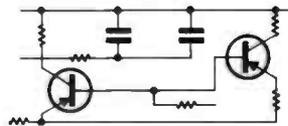
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PRACTICAL WIRELESS

VOL. 49 NO. 12

ISSUE 806

APRIL 1974

BRITAIN'S PREMIER MAGAZINE FOR THE DO-IT-YOURSELF RADIO AND ELECTRONICS CONSTRUCTOR

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We regret that we are unable to supply back numbers of Practical Wireless. Readers are recommended to enquire at a public library to see copies. Requests for specific back numbers of *Practical Wireless* and *Television* only can be published in our CQ Column.

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We regret that we cannot answer technical queries by telephone nor can we provide information or advice on manufacturers' products other than that given in the magazine. We will endeavour to assist readers who have queries relating to articles published but we cannot offer advice on modifications to our published designs. All correspondents expecting a reply should enclose a stamped addressed envelope.

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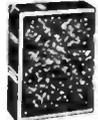
AUDIOTRINE STEREO 20 AMPLIFIER. GARRARD TURNTABLE with Sonotone Carr. ridge wired on Plinth with cover. PAIR DIPLOMAT 10W SPEAKERS. Teak Veneer finish.

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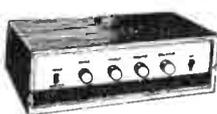
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RSC

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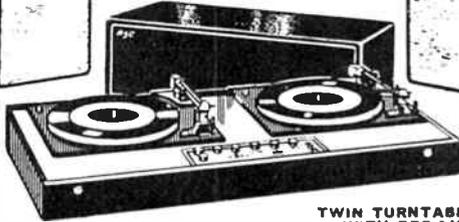
50 WATT SPEAKER

100 WATT AMPLIFIER

50 WATT SPEAKER



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8/15Ω | 15" 60 Watt
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8/15Ω | 12" 50 Watt
13,000 gauss
15Ω |
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1A6GT	.50	81K7A	.50	6Q7G(M)	.55	19G6	.50	150R2	.75	EB92	.50	EP92	.30	HN309	1.40	PI.81	.44	AC128	.22	BC116	.28	OA90	.14	
1A7GT	.65	81K7	.95	6R7G	.60	20D4	.70	2158C	.50	EB93	.50	EP97	.70	HVR2	.58	PL81A	.55	UF89	.38	AC132	.22	BC116	.28	
1B30T	.52	81R8	.85	6R7M	.75	20P2	.75	20T	.80	EB98	.30	EP98	.80	HVR2A	.58	PI.82	.37	UL41	.65	AC154	.28	BC118	.25	
1H6GT	.65	81B7	1.40	68A7	.44	20L1	.88	5702	.80	EB99	.50	EP18	.29	KT2	.50	PI.83	.39	UL44	.38	AC156	.22	BC110	.60	
1N4	.14	68B7C	.65	687GT	.33	25Z3	.30	5763	2.00	EBF89	.30	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
1R4	.38	68Z6	.49	68H17	.44	20P5	1.30	AC/PEN	.98	EC86	.59	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
1R6	.38	68C6A	.40	68K7C	.44	25A6G	.38	AC/PEN	.98	EC88	.59	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
1U4	.65	6C4	.28	68Q7GT	.38	25L6G	.50	DD	.98	EC92	.45	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
1U6	.90	6C9	1.25	6V6G	.17	25Y6G	.70	AC6PRN	.38	EC93	1.50	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
2B21	.48	6C106G	.80	6V6GT	.38	25Z4A	.38	ACTH1	.81	EC95	1.20	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
20K6	.53	6C10A	.75	6X4	.30	25Z3	.30	AL60	1.00	EC94	1.00	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
BA4	.42	6C116	.60	6X3GT	.28	25Z4A	.70	AT1	1.40	EC95	1.20	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
BD6	.19	6C16	.55	7B6	.75	20D7	1.00	AZ1	.60	EC98	.28	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
3Q4	.49	6C17	.75	7B7	.50	30A5	.65	AZ31	.60	EC98	.28	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
3Q5GT	.55	6C17G	.75	7B7	.75	30C16	.75	AZ41	.65	EC98	.28	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
3R4	.33	6C17A	.70	7B7	1.50	30C17	.90	CL33	1.50	EC98	.28	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
40R6	.55	6D7	.75	7Y4	.65	30C18	.73	CY1C	1.00	EC98	.28	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
40R8	.60	6D7A	.75	7Z4	.80	30P5	.33	CY31	.45	EM10A	.42	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
5R4G	.70	6E16	.75	9D7	.65	30P1	.75	DAF91	.30	EC189	.55	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
5U40	.30	6E5	1.00	10C2	.65	30F12	.75	DAF96	.44	EC80A	.60	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
5V40	.54	6F1	.70	10DE7	.55	30F12.10	.60	DF91	.30	EC804	.60	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
6Y30T	.38	6F61	.50	10F1	.50	30F13	.55	DF96	.44	ECF80	.34	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
5Z3	.53	6F13	.55	10F9	.65	30F14	.85	DH63	.50	ECF82	.34	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
6Z40	.35	6F14	.75	10F18	.55	30L15	.75	DH76	.45	ECF86	.75	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
6Z40T	.35	6F18	.55	10F11	.70	30L17	.70	DH40	.70	ECF80	.60	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55	
6Z80L2	.60	6F23	.85	10P13	.70	30P4MR	.80	DR92	.70	2.10	EZ40	.55	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55
6AR0	1.25	6P24	.85	10P14	2.00	1.00	DK96	.55	ECH21	1.50	EZ41	.50	EP184	.32	KT41	.98	PI.84	.38	UM80	.44	AC157	.28	BC112	.55
6AC7	.49	6P22	1.00	12AG	1.00	30P12	.80	DL92	.33	ECH35	.65	EZ80	.24	.55	UCC86	.75	2N3709	.22	BA130	.11	OA70	.17		
6AG5	.27	6P28	.70	12AG	.60	30P19	.75	DL96	.44	ECH42	.70	EZ81	.25	.65	PCL96	1.47	UCF80	.65	2N3988	.55				
6AH6	.50	6F32	.65	12AD6	.65	30P14	.75	DM70	.44	ECH81	.30	GY501	.75	.25	PI800	1.44	UCF21	.65	2N323	.55				
6AJ3	.75	6H19A	.75	12AE6	.65	30P11	.88	DM71	2.00	ECH83	.44	GZ32	.54	.65	PN445	.80	UCH43	.65	AA119	.17				
6AK5	.34	6H26	.65	12AF6	.35	30P17	.75	DY87	.20	EC26	.44	GZ33	1.00	.65	PN446	.30	UCH81	.35	AA130	.17				
6AL6	.60	6H17	.75	12AG	.45	30P14	.80	DY82	.33	ECH80	.40	GZ34	.57	.65	PN453DD	UCF82	.88	AA129	.17					
6AM8A	.65	6H6GT	.18	12AV6	.40	30P15	.85	EB00C1	1.65	ECL82	.34	GZ37	.67	2.00	UC183	.60	AAZ13	.20						
6AN8	.49	6J5GT	.32	12BAG	.30	35A3	.85	EB00P	1.20	ECL83	.57													
6AQ6	.40	6J6	.25	12BEG	.38	35C5	.75	EB3F	1.20	ECL84	.60													
6AR5	.55	6J7	.30	12BH7	.27	35L6G	.55	EB80C	.80	ECL85	.60													
6AN7	1.00	6J7A	.75	12E1	3.00	35W4	.33	EB92C	1.00	ECL86	.40													
6AT6	.35	6K7G	.19	12JGT	.55	35Z4T	.45	EB10V	1.00	EP22	1.50													
6AU6	.30	6K8	.85	12K5	.65	35Z54T1	.60	EB2CC1	.60	EF40	.40													
6AV6	.33	6L1	2.00	12K7GT	.38	50B5	.85	EB148	.53	EF41	.70													
6AW8A	.65	6L8GT	.58	12Q7GT	.45	50C5	.45	EA50	.27	EF42	.55													
6AX4	.55	6L7	2.00	12MGT	.50	50C16D	1.25	E476	1.00	EP73	1.50													
6BR0	.30	6L18	.49	12MGT	.38	60E16	.55	E4HC00	.30	EP80	.28													
6HA6	.28	6L19	2.00	12H17	.35	60L6GT	.65	E4C91	.75	EP93	.40													

VALVES ALSO REQUIRED FOR CASH. LOOSE OR BOXED, BUT MUST BE NEW. OFFERS MADE BY RETURN.
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ERNIE



MINICOMP 100



MINICOMP 1000

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NEW! SUPERBLY IMPROVED

Build something completely out of the ordinary: Build the fascinating MINICOMP the miniaturised ERNIE.

The MINICOMP employs sophisticated LOGIC techniques and brilliant NIXIE tubes to display truly RANDOM NUMBERS. At the mere touch of a button the neon numbers "WHIP" round spectacularly at high speed, before a random number within a pre-set range is selected and displayed.

MINICOMP 100
Includes four range selections within 00-99.
* DICE: 1-6 * ROULETTE: 00-36 * POOLS: 00-99 * BINGO: 00-99
Kit includes 7 latest LOGIC I.C.'s, 3 transistors, 2 NIXIES, fibreglass P.C. board, the power supply and various other components.

MINICOMP 1000
After tremendous popularity of MINICOMP 100 we are now pleased to introduce MINICOMP 1000, which has all the original features of MINICOMP 100 but in addition it provides two higher ranges:
* QUARTO: 000-399 * KILO: 000-999
Kit includes 9 latest LOGIC I.C.'s, 3 transistors, 3 NIXIES, 2 P.C. boards, the power supply and various other components.

The MINICOMP is extremely easy to build as the P.C. boards are supplied with I.C.'s fully assembled and tested. The illustrated instructions include an introduction to the LOGIC techniques employed in the MINICOMP. Attractive blue or red NYLON coated and elegantly sized case, approx. 7", 4", 3" and silk aluminium panel.

APPLICATIONS: The MINICOMP simulates electronically all phenomena in nature or activity in daily life with random occurrence. RANDOM PULSE TRAINS are found useful in medical and statistical research. Digital LOGIC makes possible a modern and exciting means of playing any number of NUMBER GAMES the human mind can conjure up.
A PROFOUND ATTRACTION FOR PARTY GAMES, FETES, RAFFLE AND POOLS DRAWS. A purely random selection of the draws could well contribute to your winning combination.

U.K. PRICES: Overseas and quantity prices on request.
240V, 50 HZ. OR 110V, 60 HZ. mains operated
MINICOMP100, KIT: £39.50 Built & Guaranteed Units: £42.50 | All prices in-
MINICOMP1000, KIT: £49.50 : £53.50 | clude V.A.T.
TERMS: C.W.O. or C.O.D., MAIL ORDER ONLY. : and P&P.
* Patent applied for.

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THE AVON AUDIO SYSTEM



The uncabineted system is ideal as an economical replacement for an outdated chassis. Stereo Amplifier for Stereo/Mono record reproduction. Tuner with medium, long and short wavebands provides Worldwide coverage, even the weakest continental stations can be received with superb clarity. Push button band selection, 10 watts total output. Frequency response 25-18000 Hz.

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TWIN ELLIPTICAL SPEAKERS These low impedance, permanent magnet units have been specially selected to provide the fullest range of audio reproduction.

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ALL EQUIPMENT COVERED BY OUR 12 MONTHS FULL GUARANTEE

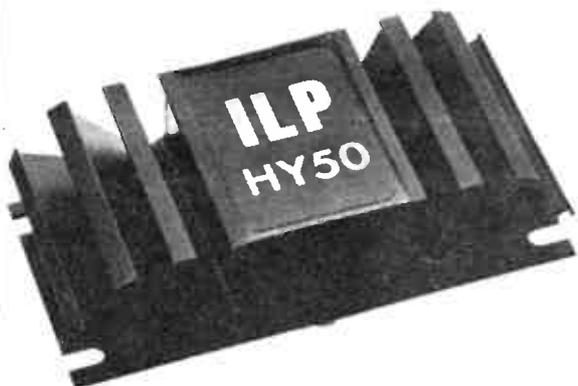
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I.L.P. (Electronics) Ltd

SECOND GENERATION 25 WATT HYBRID



A brand new hybrid fabrication technique, recently perfected in our laboratories, has enabled us to achieve our latest range of completely integrated devices. We have now finally reduced the modular amplifier to a simple input/output device requiring only the addition of a basic unstabilized (split line) power supply. The HY50 takes medium power modules to their logical conclusion by incorporating with it a heatsink, which is designed in special high conductivity alloy, sufficient for normal audio use without additional chassis sinking. All this without significantly increasing the size of the module comparable in size to a packet of 'King-size' cigarettes.

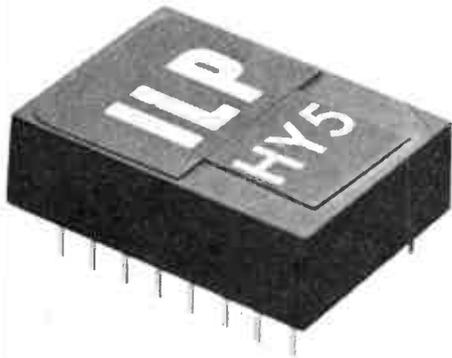
Consistent with modern thinking a triple rated output circuit with a load fuse allows for peak transient response without distortion but ensures the necessary protection.

OUTPUT POWER:	SPEC.
LOAD IMPEDANCE:	25 watts RMS, 50 watts peak music power
INPUT SENSITIVITY:	4-16 Ω into 8 Ω
INPUT IMPEDANCE:	0db (0-775 volts RMS)
TOTAL HARMONIC DISTORTION:	47K Ω
SIGNAL/NOISE RATIO:	Less than 0-1% at 25 watts typically 0-05 better than 75db
FREQUENCY RESPONSE:	10Hz-50KHz \pm 1db
SUPPLY VOLTAGE:	\pm 25 volts
SIZE:	105 x 50 x 25 mm

Price £5-80 mono, £11-60 stereo

Price inclusive of VAT & P & P

NEW HY5 PRE-AMPLIFIER



Unchallenged for two years, the HY5, our unique multifunction preamplifier/tone hybrid, has been brought into line with the advancements in our power hybrids. Like the HY50, the new HY5 has no external components & has been redesigned to run off a split power-line with improvements in signal/noise, overload, capability & reduced distortion. The output has been increased to match the power module (Odb), and to share the same power supply. Overall size is reduced by the use of a new thin film circuitry while the device still retains all the functions of the earlier device.

When combined with the HY50 & power supply only potentiometers are required to complete a simple mono amplifier with input & output facilities expected to be found on HI-FI amplifiers. The combination of two HY5's two HY50's sharing a common power supply (PSU50) are linked by a balance control to form a complete stereo system.

INPUTS	SPEC.
Magnetic Pick-up 3mV (within 1db RIAA curve)	
Ceramic Pick-up up to 3mV	
Microphone 10mV	
Tuner 250mV	
Auxiliary 3-100mV	
Input impedance 47k Ω 1kHz	

OUTPUTS
Tape 100mV.
Main output, 0db (0-775volts)

ACTIVE TONE CONTROLS

Treble \pm 12db at 10kHz

Bass \pm 12db at 100Hz

OVERLOAD CAPABILITY (equalization stage) 40db on most sensitive input

OUTPUT NOISE LEVEL (below 10mV magnetic input) 68db

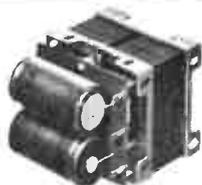
DISTORTION 0-05% at 1kHz

SUPPLY VOLTAGE \pm 16-25 volts

SUPPLY CURRENT 15mA

Price £4-85 mono, £9-70 stereo

Price inclusive of VAT & P & P



POWER SUPPLY PSU50

The new PSU50 has a low profile look being only 2½ inches high and can be used for either mono or stereo systems.

SPEC.
OUTPUT VOLTAGE \pm 25 volts
INPUT VOLTAGE 210-240 volts
SIZE L. 70, D. 90, H. 60 mm

Price £5-23

Price inclusive of VAT & P & P

CROSSLAND HOUSE · NACKINGTON · CANTERBURY · KENT

CANTERBURY 63218

Please note we reserve the right to substitute at our discretion updated versions of advertised designs where applicable.

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PANEL METERS · TRANSFORMERS · CONTROLS · RELAYS
 IRONS · TOOLS · VALVES · POT CORES MOST TYPES OF COMPONENTS
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UK's
**LARGEST RANGE
 OF KITS &
 GADGETS**



TEST EQUIPMENT

MULTIMETERS

- (carr. etc. 30p)
- M210 (Case £1.25) 20K/Volt Slimline 6 75
 - TLH33D 2K/Volt Robust 7 50
 - U437 10K/Volt Steel case. AC up to 40 KHz 4 95
 - U4324 20K/Volt with AC current ranges 8 90
 - AF105 (Case £1.90) 50K/Volt 11 95
 - U4313 20K/Volt AC current. Steel case 10 50
 - U4341 Plus Built in translator tester 10 50
 - Model 500 (Case £1.95) 30K/Volt 9 95

OTHER EQUIPMENT

- SE250B Pocket Signal Injector 2-10 carr. 15p
- SE500 Pocket Signal Tracer 1 70 carr. 15p
- TE15 Grid Dip meter 440kHz-280MHz 15-00 carr. 30p
- TE40 AC Millivoltmeter 1-2mHz 19 75 carr. 35p
- TE65 28 Range valve voltmeter 22 50 carr. 40p
- TE20D 120kHz-500mHz RF Generator 18 95 carr. 40p
- TE22D 20Hz-200kHz Audio Generator 19 95 carr. 40p
- SE350A Deluxe Signal Tracer 12 50 carr. 20p
- SE400 Volts/ohms/R-C aub./RF field/RF gen. 14 75 carr. 20p

New Revolutionary Supertester 680R

- | 680R Multi-Tester | Accessories |
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| £18 50 | Transistor tester 11 00 |
| | Electronic voltmeter 18 00 |
| | Amp clamp 11 95 |
| | Temperature probe 11 95 |
| | Gauss meter 11 95 |
| | Signal Injector 5 95 |
| | Phase Sequence 5 95 |
| | EHT Probe 3 95 |
| | Shunts 25/50/100A 4 50 |

A SELECTION OF INTERESTING ITEMS

- C3025 Compact transistor tester 8 50 p & p 15p
- C4002 Photoelectric System 13 70
- E1310 Stereo mag. cart. preamp. 4 80 p & p 25p
- Eaaphone D1201 telephone amplifier 7 50 p & p 25p
- D1203 Tcleamp. with PU coil 4 95 p & p 20p
- LL1 Door Intercomm. and chima 8 40 p & p 25p
- 1 Kw Dimmer/controller 3 00 p & p 10p
- 9" Twin spring unit For 3 30 p & p 15p
- 15" Twin spring unit Reverb 8 85 p & p 25p
- US50 Ultrasonic Switch Transmitter/Receiver 312 75
- C3041 1-250 MHz 42 25
- C3043 5CH 1-300 MHz 43 75
- VHF 105 Aircraft Band Converter 4 50 p & p 15p
- B2005 4 Ch. mic. mixer 4 20 p & p 15p
- B2004 2 ch. Stereo mixer 8 75 p & p 15p
- PK3 Kit. Etch your own printed circuits 41 95 p & p 20p

EXCLUSIVE: SPECIAL OFFERS

- MW/LW CAR RADIO AKAI GX40 + or - Earth with speaker Stereo cassette recorder, and fixings. £8 50 carr./pack, 50p. Pair Akai ADM microphones. £8 95 carr./pack, 20p.
- 8 TRACK CAR STEREO (- Earth) with speakers in Pods & fixings. £12 50 carr./pack, 40p.
- Portable Battery Cassette Tape Player £7 25.
- Car Lighter Plug and adaptor for all cassette and radio 6 7 1/2 volt output (state width) £1 95 each
- Rotel Stereophones RM630 £4 50 RM700 £8 75 RM430 £3 30
- Rotel RA310 15+15 watt Stereo Amplifier (List £52 00) £34 52.
- Weln W500 Battery/Mainst Cassette Recorder £12 75
- AKAI GX40 Stereo cassette recorder. £58 95 carr./pack, 50p.
- Pair Akai ADM microphones. £8 95 carr./pack, 20p.
- PORTABLE CASSETTE TAPE PLAYER— for car or carry around. £7 25 carr./pack, 20p.
- HANIMAX BC808 POCKET CALCULATOR WITH % KEY. £28 95.
- HANIMAX BC811M MEMORY VERSION £37 50
- MAINS UNIT for BC808, BC811M £2 85 (state model)
- HANIMAX H101 STEREO COMPACT RECORD PLAYER 2 x 7 watts Complete with Speakers (List £54 50) Price £39 95 Plus free pair of stereo phones.

SPECIAL PURCHASES

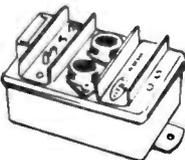
UHF TV TUNERS CHANNELS 21 TO 64

Brand new transistorised geared tuners for 625 Line Receiver IF output. £2 50. Post 20p.



EASY TO BUILD KITS BY AMTRON— EVERYTHING SUPPLIED

- | Model No. | Description | Price |
|-----------|---|-------|
| 310 | Radio control receiver | 2 98 |
| 300 | 4-channel R/C transmitter | 5 95 |
| 345 | Superhet R/C receiver | 5 95 |
| 455 | AM signal generator | 12 33 |
| 65 | Simple transistor tester | 1 40 |
| 115 | 8 watt Amplifier | 3 90 |
| 120 | 12 watt amplifier | 4 70 |
| 125 | Stereo control unit | 5 70 |
| 130 | Mono control unit | 3 60 |
| 605 | Power supply for 115 | 4 55 |
| 610 | Power supply for 120 | 4 55 |
| 615 | Power supply for 2 x 120 | 5 73 |
| 230 | AM/FM aerial amplifier | 2 83 |
| 240 | Auto packing light | 5 90 |
| 275 | Mic. preamplifier | 6 08 |
| 575 | LF generator 10Hz-1mHz | 15 80 |
| 575 | Sq. wave generator 20Hz-20KHz | 14 50 |
| 590 | SWR meter | 12 85 |
| 620 | NI-CAD Charger 1-2-12v | 8 00 |
| 630 | STAB Power supply 6-12v 0 25-0 1A | 8 15 |
| 690 | DC motor speed Gov. | 2 87 |
| 700 | Electronic Chaffinch | 7 00 |
| 705 | Windscreen wiper timer | 10 75 |
| 760 | Acoustic switch | 10 75 |
| 780 | Metal Detector (electronics only) | 9 65 |
| 790 | Capacitive Burglar alarm | 6 85 |
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| 795 | Electronic continuity tester | 4 30 |
| 860 | Photo timer | 7 15 |
| 871 | Slide projector auto feed control | 13 25 |
| 235 | Acoustic Alarm for driver | 14 60 |
| 465 | Quartz XTAL checker | 8 75 |
| 220 | Signal injector | 2 30 |
| 390 | VOX | 15 50 |
| 432 | Teatalk | 18 30 |
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ALL KITS OFFERED SUBJECT TO STOCK AVAILABILITY

Prices correct at time of preparation. Subject to change without notice.

BUILD THIS TUNER

MW/LW Radio Turner to use with any amplifier. Features Mullard RF/IF module Ferrita aerial, built in battery. Excellent results. Size 7" x 2 1/2" x 3 1/2". All parts £4 85. carr. 15p.

MULTI-USE & RADIONIC KITS

- | | | |
|-------|------------------------|-------|
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| 50-1 | 10 Projects | 6 00 |
| 150-1 | 150 Projects | 13 20 |
| | Telephone Communicator | 7 28 |
| X20 | 20 (Etc.) Projects | 4 95 |
| X40 | 40 (radio) Projects | 8 45 |
- (carr./packing 40p)

BUILD THIS RADIO

Portable MW / LW radio kit using Mullard RF/IF module. Features MW — bandspread for extra selectivity. Slow motion tuning. Fibre glass PVC cabinet. 600MW output. All parts £7 99 (battery 22p). carr. etc. 32p.



GARRARD BATTERY TAPE DECK

GARRARD 2 speed 9 volt tape decks. Fitted record/play and oscillator/Eraser heads. Wind and rewind controls. Takes up to 4" spools. Brand new complete with head circuits. £9 50 carr. 30p

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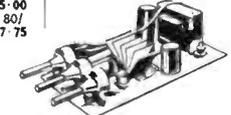
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8N7405AN	0.44	0.44	0.38	8N7473N	0.44	0.41	0.37	8N74165N	1.15	1.15	1.00
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8N7411N	0.25	0.23	0.21	8N7485N	1.87	1.87	1.63	8N74164N	2.01	2.01	1.76
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8N7422N	0.28	0.28	0.25	8N7494N	0.85	0.80	0.75	8N74174N	1.80	1.80	1.57
8N7422AN	0.38	0.38	0.33	8N7495N	0.85	0.80	0.75	8N74176N	1.29	1.29	1.13
8N7423N	0.37	0.34	0.32	8N7496N	1.00	0.90	0.83	8N74177N	1.44	1.44	1.26
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8N7432N	0.37	0.37	0.32	8N74110N	0.57	0.57	0.50	8N74184N	2.16	2.16	1.89
8N7433N	0.43	0.43	0.38	8N74111N	0.86	0.86	0.75	8N74185AN			
8N7433AN	0.57	0.57	0.50	8N74116N	2.16	2.16	1.89				
8N7437N	0.43	0.42	0.37	8N74188N	1.00	0.90	0.83	8N74188N	4.48	4.48	3.87
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8N7442N	0.85	0.79	0.73	8N74123N	1.44	1.44	1.26	8N74194N	1.72	1.72	1.51
8N7443N	1.50	1.27	1.13	8N74125N	0.60	0.60	0.60	8N74195N	1.44	1.44	1.26
8N7444AN	1.50	1.27	1.13	8N74126N	0.60	0.60	0.60	8N74196N	1.58	1.58	1.38
8N7445N	2.16	2.16	1.89	8N74132N	0.72	0.72	0.63	8N74197N	1.58	1.58	1.38
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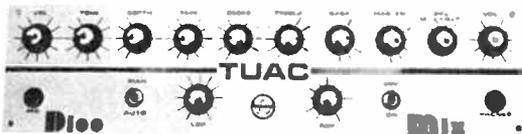
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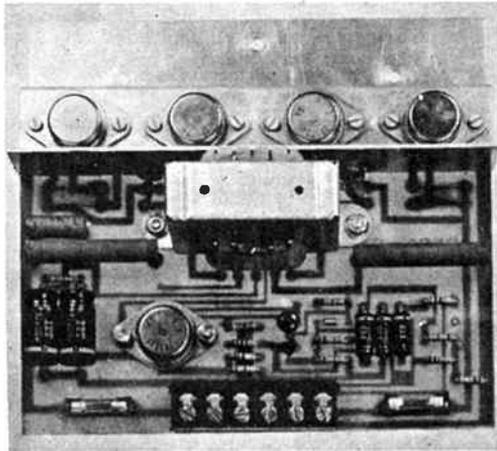
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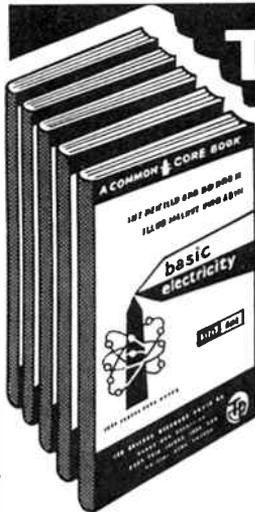
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£11-50 | <ul style="list-style-type: none"> ★ 100 Watts RMS sine wave ★ 2 RCA 15 Amp output transistors ★ Rugged transformer driver ★ Full thermal overload protection ★ Compact size: 5 x 5 x 3in. |
| TL60
£9-75 | <ul style="list-style-type: none"> ★ 60 Watts RMS sine wave ★ RCA 115 Watt output transistors ★ Only six connections to make ★ Same size as TL100 |
| TL30
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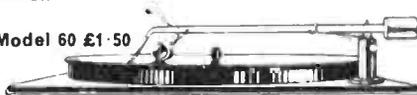
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1021 For model G240 1/8" 38p
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51 For model X25 1/8" 38p
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C 9	3	Micro Switches	0.55
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PS 40 Jack 3.5mm Switched 0-10
PS 41 Jack 1" Switched 0-17
PS 42 Jack Stereo Switched 0-28
PS 43 Phono Single 0-06
PS 44 Phono Double 0-10
PS 45 Car Aerial 0-09
PS 46 Co-Axial Surface 0-09
PS 47 Co-Axial Flush 0-14

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PS 25 Jack 2.5mm Plastic 0-10
PS 26 Jack 3.5mm Plastic 0-12
PS 27 Jack 1" Plastic 0-24
PS 28 Jack 1" Screened 0-28
PS 29 Jack Stereo Plastic 0-22
PS 30 Jack Stereo Screened 0-28
PS 31 Phono Screened 0-14
PS 32 Car Aerial 0-16
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PS 3 D.I.N. 4 Pin 0-15
PS 4 D.I.N. 5 Pin 180° 0-14
PS 5 D.I.N. 5 Pin 240° 0-15
PS 6 D.I.N. 6 Pin 0-15
PS 7 S.I.N. 7 Pin 0-15
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Holds 12. 10" x 2½" x 5". Lock & Handle. £1.90

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Holds 14. 13" x 5" x 6". Lock & Handle £1.95
Holds 24. 13½" x 8" x 5½". Lock & Handle £2.70

COLOURS: Red, Black and Tan—Please state preference.

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240v. Primary. Secondary voltages available from selected tappings 4v, 7v, 8v, 10v, 14v, 16v, 17v, 19v, 21v, 25v, 31v, 33v, 40, 60 and 25v-0-25v.

Type	Amps.	Price	P & P
MT50/1	1	£1.98	30p
MT50/1	1	£2.42	35p
MT50/2	2	£3.30	40p

CARTRIDGES

ACOS GP91-18C. 200mV at 1-2cm/sec £1.16
ACOS GP93-1. 280mV at 1cm/sec £1.85
ACOS GP96-1. 100mV at 1cm/sec £2.65
TTC J-2005. Crystal/Hi Output 95p
TTC J-20 10C Crystal/Hi Output Compatible £1.10
TTC J-200 CS Stereo/Hi Output £1.60
TTC J-2105 Ceramic/Med. Output £1.84

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The E12 Range of Carbon Film Resistors, 1/8th watt available in PAKS of 50 pieces, assorted into the following groups:—

R1	50	Mixed 100 ohms-820 ohms	40p
R2	50	Mixed 1K ohms-8.2K ohms	40p
R3	50	Mixed 10K ohms-82K ohms	40p
R4	50	Mixed 100K ohms-1 Meg. ohms	40p

THESE ARE UNREPEATABLE PRICES—LESS THAN 1p EACH INCL. V.A.T.

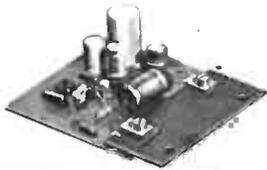
BI-PAK SUPERIOR QUALITY LOW-NOISE CASSETTES

C60, 32p C90, 41p C120, 52p

-the lowest prices!

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AL10/AL20/AL30 AUDIO AMPLIFIER MODULES



The AL10, AL20 and AL30 units are similar in their appearance and in their general specification. However, careful selection of the plastic power devices has resulted in a range of output powers from 3 to 10 watts R.M.S.
The versatility of their design makes them ideal for use in record players, tape recorders, stereo amplifiers and cassette and cartridge tape players in the car and at home.

Parameter	Conditions	Performance
HARMONIC DISTORTION	Po = 3 WATTS f = 1KHz	0.25%
LOAD IMPEDANCE	—	8 - 16 Ω
INPUT IMPEDANCE	f = 1KHz	100 k Ω
FREQUENCY RESPONSE @ 3dB	Po = 2 WATTS	50 Hz - 25KHz
SENSITIVITY FOR RATED O/P	Vs = 25V, RI = 8 Ω f = 1KHz	75mV, RMS
DIMENSIONS		3" x 2 1/2" x 1"

The above table relates to the AL10, AL20 and AL30 modules. The following table outlines the differences in their working conditions.

Parameter	AL10	AL20	AL30
Maximum Supply Voltage	25	30	30
Power output for 2% T.H.D. (RL = 8 Ω f = 1 KHz)	3 watts RMS Min.	5 watts RMS Min.	10 watts RMS Min.

AUDIO AMPLIFIER MODULES

AL10. 3 watts RMS £2 19
AL20. 5 watts RMS £2 59
AL30. 10 watts RMS £3 01

POWER SUPPLIES

PS 12. (Use with AL10 & AL20) 89p
SPM 80. (Use with also AL30 & AL50) £3 25
FRONT PANELS SP 12 with Knobs £1 10

PRE-AMPLIFIERS

PA 12. (Use with AL10 & AL20) £4 35
PA 100. (Use with AL30 & AL50) £13 15

TRANSFORMERS

T461 (Use with AL10) £1 38 P & P 15p
T538 (Use with AL20) £1 93 P & P 15p
BMT80 (Use with AL30 & AL50) £2 15 P & P 25p

PA 12. PRE-AMPLIFIER SPECIFICATION

The PA 12 pre-amplifier has been designed to match into most budget stereo systems. It is compatible with the AL 10, AL 20 and AL 30 audio power amplifiers and it can be supplied from their associated power supplies. There are two stereo inputs, one has been designed for use with ceramic cartridges while the auxiliary input will suit most magnetic cartridges. Full details are given in the specification table. The four controls are, from left to right: Volume and on/off switch, balance, bass and treble. Size 152mm x 84mm x 35mm.

Frequency response—
20Hz - 50KHz (± 3dB)
Bass control—
± 12dB at 60Hz
Treble control—
± 14dB at 14KHz
*Input 1. Impedance
1 Meg. ohm
Sensitivity 300mV
†Input 2. Impedance
30 K ohms
Sensitivity 4mV

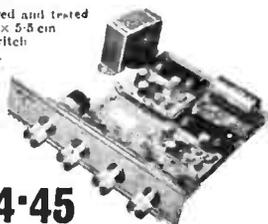
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ALL PRICES INCLUDE V.A.T.

The STEREO 20

The 'Stereo 20' amplifier is mounted, ready wired and tested on a one-piece chassis measuring 20 cm x 14 cm x 5.5 cm. This compact unit comes complete with on/off switch, volume control, balance, bass and treble controls, Transformer, Power supply and Power amps. Attractively printed front panel and matching control knobs. The 'Stereo 20' has been designed to fit into most turntable plinths without interfering with the mechanism or, alternatively, into a separate cabinet. Output power 20w peak. Input 1 (Cer.) 300mV into 1M. Freq. res. 25Hz-25KHz. Input 2 (Aux.) 4mV into 30K. Harmonic distortion—Bass control ± 12dB at 60Hz typically 0.25% at 1 watt. Treble con. ± 14dB at 14kHz



£14.45

50W pk 25w (RMS)

0.1% DISTORTION!
HI-FI AUDIO AMPLIFIER

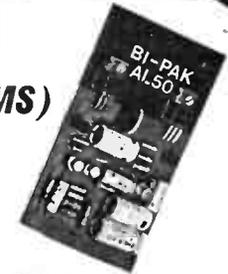
THE AL50

★ Frequency Response 15Hz to 100,000—1dB.

★ Load—3, 4, 8 or 16 ohms.

★ Distortion—better than 0.1% at 1 KHz.

★ Signal to noise ratio 80dB.



ONLY
£3.58 each

★ Supply voltage 10-35 Volts.

★ Overall size 63mm 105mm x 13mm.

Tailor made to the most stringent specifications using top quality components and incorporating the latest solid state circuitry and AL50 was conceived to fill the need for all your A.F. amplification needs.
FULLY BUILT TESTED GUARANTEED.



STABILISED POWER MODULE SPM80

SPM80 is especially designed to power 2 of the AL50 Amplifiers, up to 15 watt (r.m.s.) per channel simultaneously. This module embodies the latest component and circuit techniques incorporating complete short circuit protection. With the addition of the Mains Transformer MT80, the unit will provide outputs of up to 1.2 amps at 35 volts. Size: 63mm x 105mm x 30mm.
These units enable you to build Audio Systems of the highest quality at a hitherto unobtainable price. Also ideal for many other applications including—Disc Systems, Public Address-Intercom Units, etc. Handbook available 10p PRICE £3.25

TRANSFORMER BMT80 £2.15 p. & p. 28p

STEREO PRE-AMPLIFIER TYPE PA100

Built to a specification and NOT a price, and yet still the greatest value on the market the PA100 stereo pre-amplifier has been conceived from the latest circuit technique. Designed for use with the AL50 power amplifier system, this quality made unit incorporates no less than eight silicon planar transistors, two of these are specially selected low noise NPN devices for use in the input stages.
Three switched stereo inputs, and rumble and scratch filters are features of the PA100 which also has a STEREO/MONO switch, volume, balance and continuously variable bass and treble controls.



SPECIFICATION

Frequency Response 20Hz - 20KHz ± 1dB
Harmonic Distortion better than 0.1%
Inputs: 1. Tape Head 1.25 mV into 50K Ω
2. Radio, Tuner 35 mV into 50K Ω
3. Magnetic P.U. 1.5 mV into 50K Ω
All input voltages are for an output of 250mV. Tape and P.U. input equalised to RIAA curve within ± 1dB, from 20Hz to 20KHz.
Bass Control ± 15dB at 20Hz
Treble Control ± 15dB at 20 KHz
Filters: Rumble (High Pass) 100Hz
Scratch (Low Pass) 8KHz
Signal/Noise Ratio better than -65dB
Input overload ± 26dB
Supply ± 35 volts at 20mA
Dimension 292mm x 82mm x 35mm

SPECIAL COMPLETE KIT COMPRISING 2 AL50's, 1 SPM80, 1 BMT80 & 1 PA100 ONLY £25.30 FREE p. & p.

Giro No. 388-7006

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Minimum order 55p. Cash with order please.

Guaranteed Satisfaction or Money Back

TRANSFORMERS

SAFETY MAINS ISOLATING TRANSFORMERS

120 240 V Sec. 120 240 V Centre Tapped and Screened

Ref. No.	VA (Watts)	Weight lb oz	Size cm.	£	P & P
07	20	1 8	7.0 x 6.0 x 6.0	2.32	30
149	60	3 12	9.9 x 7.7 x 8.6	3.45	36
150	100	5 8	9.9 x 8.9 x 8.6	3.79	52
151	200	8 0	12.1 x 9.3 x 10.2	6.45	52
152	250	13 2	12.1 x 11.9 x 10.2	8.41	67
153	350	15 0	14.0 x 10.8 x 11.8	11.22	82
154	500	19 8	14.0 x 13.4 x 11.8	16.25	—
155	750	29 0	17.2 x 14.0 x 14.0	22.10	—
156	1000	38 0	17.2 x 16.6 x 14.0	29.87	—
158	2000	60 0	21.6 x 15.3 x 18.1	49.25	—

PLEASE NOTE
NEW ADDRESS
AS BEFORE

AUTO TRANSFORMERS

Ref. No.	VA (Watts)	Weight lb oz	Size cm.	Auto Taps	£	P & P
113	20	1 0	5.8 x 5.1 x 4.5	0-115-210-240	1.22	22
64	75	2 4	7.4 x 6.7 x 6.1	0-115-210-240	2.40	30
4	150	3 4	8.9 x 7.7 x 7.7	0-115-200-220-240	2.89	36
66	300	6 4	9.9 x 9.6 x 8.6	5.63	52
67	500	12 8	12.1 x 11.2 x 10.2	8.36	67
84	1000	19 8	14.0 x 13.4 x 14.3	15.19	82
93	1500	30 4	14.0 x 15.9 x 14.3	21.99	—
95	2000	32 0	17.2 x 16.6 x 14.0	28.70	—
73	3000	40 0	21.6 x 13.4 x 18.1	39.17	—

CASED AUTO TRANSFORMERS

115V 500W enclosed transformer, with mains lead and two 115V outlet sockets. £9.49, P & P 67p. 20 Watt version £2.02 P & P 7p

TRANSFORMERS

PRIMARY 240 250 VOLTS 12 AND OR 24 VOLT RANGE

Ref. No.	12V 24V	Amps.	Weight lb oz	Size cm.	Secondary Windings	£	P & P
111	0.5	0.25	1 4	4.8 x 2.9 x 3.5	0-12V at 0.25A x 2	1.22	22
213	1.0	0.5	1 4	6.1 x 5.8 x 4.8	0-12V at 0.5A x 2	1.44	22
71	2	1	1 12	7.0 x 6.4 x 6.1	0-12V at 1A x 2	1.90	22
18	4	2	2 12	8.3 x 7.7 x 7.0	0-12V at 2A x 2	2.68	30
70	6	3	3 8	8.9 x 8.0 x 7.7	0-12V at 3A x 2	3.20	42
108	8	4	5 8	9.9 x 8.9 x 8.6	0-12V at 4A x 2	3.60	52
72	10	5	6 4	9.9 x 9.6 x 8.6	0-12V at 5A x 2	4.25	52
112	12	6	6 12	12.1 x 10.2 x 9.6	0-12V at 6A x 2	5.10	52
17	0	0	8 12	12.1 x 9.9 x 10.2	0-12V at 8A x 2	6.56	52
115	20	10	11 8	14.0 x 9.6 x 11.8	0-12V at 10A x 2	8.36	67
187	30	15	15 8	14.0 x 12.1 x 11.8	0-12V at 15A x 2	15.40	82
226	60	30	32 0	17.2 x 15.3 x 14.0	0-12V at 30A x 2	28.44	*

30 VOLT RANGE

Ref. No.	Amps.	Weight lb oz	Size cm.	Secondary Taps	£	P & P
112	0.5	1 4	6.1 x 5.8 x 4.8	0-12-15-20-24-30V	1.42	22
79	1.0	2 4	7.0 x 6.7 x 6.1	1.92	36
3	2.0	3 4	8.9 x 7.7 x 7.7	2.90	36
20	3.0	4 8	9.9 x 8.3 x 8.6	3.58	42
21	4.0	6 4	9.9 x 9.6 x 8.6	4.25	52
51	5.0	6 12	12.1 x 8.6 x 10.2	5.30	52
117	6.0	8 0	12.1 x 9.3 x 10.2	6.31	52
88	8.0	12 0	12.1 x 11.8 x 10.2	8.18	67
89	19.0	13 12	14.0 x 10.2 x 11.8	10.33	67

50 VOLT RANGE

Ref. No.	Amps.	Weight lb oz	Size cm.	Secondary Taps	£	P & P
102	0.5	1 12	7.0 x 6.4 x 6.1	0-19-25-33-40-50V	1.90	30
103	1.0	2 12	8.3 x 7.4 x 7.0	2.80	36
104	2.0	5 8	9.9 x 8.9 x 8.6	3.87	42
105	3.0	6 12	9.9 x 10.2 x 8.6	5.26	52
106	4.0	10 0	12.1 x 10.5 x 10.2	6.99	52
107	6.0	18 0	12.1 x 10.2 x 11.8	10.35	67
118	8.0	18 0	14.0 x 12.7 x 11.8	12.51	97
119	10.0	25 0	17.2 x 12.7 x 14.0	16.93	*

60 VOLT RANGE

Ref. No.	Amps.	Weight lb oz	Size cm.	Secondary Taps	£	P & P
124	0.5	2 4	7.0 x 6.7 x 6.1	0-24-30-40-428-69C	1.93	36
126	1.0	3 4	8.9 x 7.7 x 7.7	2.70	36
127	2.0	6 4	9.9 x 9.6 x 8.6	4.25	42
125	3.0	8 12	12.1 x 9.9 x 10.2	6.46	52
123	0	13 12	12.1 x 11.8 x 10.2	8.36	67
40	5.0	12 00	14.0 x 10.2 x 11.8	9.85	87
120	6.0	15 8	14.0 x 12.1 x 11.8	12.14	82
121	8.0	25 00	14.0 x 14.7 x 11.8	13.65	*
122	10.0	25 0	17.2 x 12.7 x 14.0	20.09	*
189	12.0	29 00	17.2 x 14.0 x 14.0	22.49	*

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Ref. No.	MA.	Weight lb oz	Size cm.	VOLTS	£	P & P
238	200	1 4	2.8 x 2.6 x 2.0	3-0-3	1.31	10
212	1A, 1A	1 4	6.1 x 5.8 x 4.8	0-6-0-6	1.52	22
13	100	1 4	3.9 x 2.6 x 2.9	0-9-0	1.12	10
235	330, 330	4 4	4.8 x 2.9 x 3.5	0-9, 0-9	1.52	10
207	500, 500	1 00	6.1 x 5.4 x 4.8	0-8.9-0-8.9	2.03	22
208	1A, 1A	1 12	7.0 x 6.4 x 6.1	0-8.9-0-8.9	2.73	30
226	200, 200	4 4	4.8 x 2.9 x 3.5	0-15, 0-15	1.52	10
214	300, 300	1 4	6.1 x 5.8 x 4.8	0-20-0-20	1.60	22
231	700 (D.C.)	1 8	7.0 x 6.1 x 6.1	20-15-0-12-20	1.41	30
206	1A, 1A	2 12	8.3 x 7.7 x 7.0	0-15-20, 0-15-20	3.08	36
203	500, 500	2 4	8.3 x 7.0 x 7.0	0-15-27, 0-15-27	2.82	38
204	1A, 1A	3 4	8.9 x 7.7 x 7.7	0-15-27, 0-15-27	2.86	38

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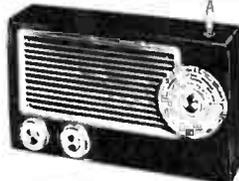
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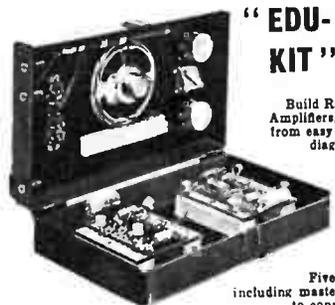


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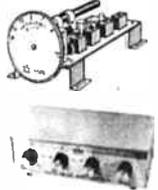


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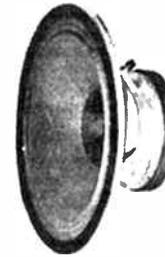


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MODERN TELEPHONES type 706. Two-tone grey, £3.75 each. Two-tone green £3.75 each. Black £2.75 each. P. & P. 25p ea. Also **TOPAZ YELLOW** £4.50 each, P. & P. 25p.

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AND G. W. SMITH & CO. (RADIO).**

LB3 TRANSISTOR TESTER
Tests ICO and B. PNP/NPN. Operates from 9V battery. Instructions supplied.
OUR PRICE
£3.95 P&P 20p



KAMODEN HM350 TRANSISTOR TESTER
High quality instrument to test reverse leak current and DC current. Amplification factor of PNP, PNP, diodes, transistors, SCR's etc. 4" square clear scale meter. Operates from internal batteries. Complete with instructions, leads carrying handle.
OUR PRICE £12.50 P&P 30p



S100TR MULTIMETER TRANSISTOR TESTER
100,000 opv. Mirror scale. Overload protection. 0/12/ 0.6/3/12/30/120/ 600V DC. 0/5/10/50/100/200/300/3000 ohms. Decibels: -5 to +10dB. Battery operated. Size: 210 x 115 x 90mm. Supplied in carrying case complete with leads.
OUR PRICE £15.00 P&P 20p



Model HT100B4 MULTIMETER
Overload protected, shock proof circuits. 9.5uA Meter with mirror scale. Sensitivity 100kV. Polarity change switch. Ranges: 0.5/2.5/1.5/50/500/1000V DC. 0.25/ 0.5/1/5/10/50/100/175A AC. Resistance: 0.5/10/100/200 ohms/1/3/30/300k ohms. Decibels: -5 to +10dB. Battery operated. Size: 210 x 115 x 90mm. Supplied in carrying case complete with leads.
OUR PRICE £15.00 P&P 20p



TE16A TRANSISTORISED SIGNAL GENERATOR
5 ranges, 400kHz to 30 MHz. An indispensable instrument for the handy-man. Operates on 9V battery. Wide easy to read scale. 800kHz modulation. Size: 145 x 149 x 82mm. Complete with instructions and leads.
OUR PRICE £8.97 P&P 25p



MODEL TE20 RF SIGNAL GENERATOR
Six bands. 120kHz-250MHz. Dual output RF terminals. Separate variable audio output. Accuracy ± 2%. Audio output to 8V. Power requirements: 105-125V 220-240V AC. Size: 193 x 95 x 150mm. Complete with test leads etc.
OUR PRICE £17.50 P&P 40p



ARF 300 AF/RF SIGNAL GENERATOR
All transistorised. Complete with fully portable AF sine-wave 18Hz to 200 kHz. AF square wave 18Hz to 100 kHz. Output Square/Sine wave 10V. P-P RF 100kHz to 200MHz. Output 1V maximum. 220/240V AC operation. Complete with instructions and leads.
OUR PRICE £29.95 P&P 50p



AT201 Decade ATTENUATOR
Frequency range 0-200kHz. Attenuator 0-111dB. 0.1dB steps. Impedance 600 ohms input power maximum 30dBm. Size: 180 x 90 x 65mm.
OUR PRICE £12.50 P&P 37p



MCA220 Automatic Voltage Stabiliser
Input 88-125V AC. Output 120V AC or 240V AC 200V/A rating. P&P 50p.
OUR PRICE £11.97



PS100B Regulated POWER SUPPLY UNIT
Solid state. Output 6, 9 or 12V DC up to 3 Amp. Meter to monitor current. Input 220/240V AC. Size: 100 x 82 x 159mm.
OUR PRICE £11.97 P&P 25p



PS200 Regulated POWER SUPPLY UNIT
Solid state. Variable output 5-20V DC up to 2 Amp. Indes pendant meters to monitor voltage and current. Output 220/240V AC. Size: 190 x 136 x 98mm.
OUR PRICE £19.95 P&P 25p



AUDIOTRONIC Model ATM1
Top value 1,000 opv pocket multi-meter. Ranges: 0/10/50/250/1,000 volt AC and DC. DC current 0-1mA/100mA. Resistance: 0/150k ohms. Decibels: -10 to +22dB. Size 90 x 60 x 28mm. Complete with test leads.
OUR PRICE £2.95 P&P 15p



AUDIOTRONIC Model ATM5
Jewel movement, attractively moulded case with edgewise ohms adjustment. Ranges: 0-31/15/50/300/1200V AC. (2500 opv). 0-6/30/300/600V DC. (5000 opv). 0-300 uA/0-300mA DC. Resistance: x 10 & x 100. -10 to +16dB. Supplied with battery test leads and data booklet. Size: 121 x 73 x 28mm.
OUR PRICE £3.75 P&P 15p



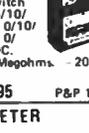
MODEL C1092 MULTIMETER
Features 5,000 opv jewel movement and a good selection of range functions. Edgewise ohms adjustment. Ranges: 0-3/15/50/300/1,200V AC (2,500 opv). 0-6/30/300/600V DC (5,000 opv). DC current: 0-30kA/300mA. Resistance: R x 10, R x 1,000. -10 to +16dB. Complete with battery, test leads and data booklet. Size: 120 x 73 x 28mm.
OUR PRICE £3.75 P&P 35p



MODEL U437 MULTIMETER
10,000 opv. A first class instrument manufactured in USSR to the highest standards. Ranges: 2.5/10/50/250/500/1000V DC. 2.5/10/50/250/500/1000V AC. DC current 100uA/1/10/100mA/1A. Resistance 300 ohms/3/30/300k/3 Meg. ohms. Complete with batteries, test leads, instructions and a sturdy steel carrying case.
OUR PRICE £4.95 P&P 25p



MODEL TH12
20,000 opv. Overload protection. Slide switch selector. 0/0.25/1.5/10/50/150/1000V DC. 0/10/50/250/1000V AC. 0/50uA/0.25/250mA DC. 0/3k/30k/300k/3 Megohms. -20 to +50dB.
OUR PRICE £5.95 P&P 15p



U4233 MULTIMETER
20,000 opv. Simple unit with audio/IF oscillator. Suitable for general receiver tuning. Ranges: 0.5/2.5/10/50/250/500/1000V DC. 0.5/2.5/10/50/250/500/1000V AC. DC Resistance 5/10/100k ohms/1Meg. Battery operated. Size: 160 x 97 x 40mm. Supplied in carrying case complete with test leads.
OUR PRICE £7.00 P&P 20p



MODEL TE300
30,000 opv. Mirror scale. Overload protection. 0/0.5/1.5/10/50/300/1200V DC. 0/6/30/120/600/1200V AC. 0/30uA. 6mA/60mA/300mA. 600mA. 0/8k/80k/800k/8 Meg ohms -20 to +63dB.
OUR PRICE £7.50 P&P 15p



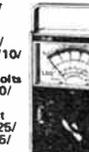
HIOKI Model 720X VOM
A versatile, accurate measuring instrument. 20,000 opv. 0/5/25/100/500/1000V DC. 0/10/50/250/1000V AC. 0-50uA/250mA. 0-20k/2 Megohms.
OUR PRICE £5.97 P&P 20p



U4324 MULTIMETER
High sensitivity, overload protected. 20,000 opv. Ranges: 0.5/1.5/10/50/100/200V DC. 3/6/15/50/150/300/600/900V AC. Current: 0.05/0.5/6/60/600mA/3A DC. 0.3/3/30/300mA/3A AC. Resistance: 25/500 ohms/0.5/5/50/500k ohms/5 Mohms. Decibels: -10 to +12dB. Size 167 x 98 x 63mm. Supplied complete with test leads, spare diode and instructions.
OUR PRICE £8.00 P&P 20p



TMK MODEL TW50K
40k ranges, mirror scale. 50kV DC. 50kV/AC. DC Volts: 0.125/ 0.25/1.25/2.5/5/10/25/50/125/250/500/1000. AC Volts 1.5/3/15/125/250/500/1000. Resistance: 10k/100k/1 Meg/10 Meg ohms. -20 to +81.5dB.
OUR PRICE £8.50 P&P 17p



U435 MULTIMETER
20,000 opv. Overload protected. Ranges: 75mV/2.5/10/25/100/250/500/1000V DC. 2.5/10/25/100/250/500/1000V AC. Current: 50uA/1/5/2.5 A DC. 5/25/100mA. 0.5/2.5 A AC. Resistance: 0.3/3/30k/300k ohms. Size: 205 x 110 x 84mm. Supplied complete with leads, crocodile clips and test carrying case.
OUR PRICE £8.75 P&P 20p



U4312 MULTIMETER
20,000 opv. Handy instrument for general electrical use. 667 opv. Ranges: 0/0.3/1.5/5/30/60/150/300/600/900V DC & 75mV. 0/0.3/1.5/7.5/30/60/150/300/600/900V AC. 0/300mA/1/1.5/6A DC. 0/1.5/15/150/300/600mA/1/1.5/6A AC. 0/200/3k/30k ohms. DC accuracy 1%. AC 1.5%. Knife edge pointer, mirror scale. Complete with test leads, carrying case, leads and instructions.
OUR PRICE £9.75 P&P 25p



KAMODEN 360 MULTIMETER
High sensitivity. DC 10k ohm/V. AC 10k ohm/V. 5" mirror scale, overload protected. Ranges: 0.5/ 2.5/10/50/250/1000V DC. 5/10/50/250/1000V AC. Current: 0.01mA/0.5/5/50/500mA/10A. Resistance: 0.1/1/10/100 ohms. 0/100k ohms. 0/100M ohms. Decibels: -20 to +62dB. Battery operated. Size 180 x 140 x 80mm. Supplied complete with test leads etc.
OUR PRICE £13.95 P&P 25p



U91 Clamp VOLT AMMETER
For measuring AC voltage and current without break circuit. Ranges: 300/800V AC. Current: 10/25/100/250/500A. Accuracy 4%. Size 28 x 94 x 38mm. Complete with carrying case, leads and fuses.
OUR PRICE £10.50 P&P 20p



MODEL 500
30,000 opv with overload protection. Mirror scale. 0/0.5/2.5/10/25/100/250/500/1000V DC. 0/2.5/10/25/100/250/500/1000V AC. 0/50uA/5/50/500mA. 12A DC. 0/6k/60 meg/10k megohms.
OUR PRICE £10.95 Carr. paid Leather case for above £1.75



HIOKI 750X VOLT-Ohm-MILLIAMMETER
43 ranges: 0-0.3/0.6/1.5/3/6/12/30/60/150/300/600/1200V DC. 0-3/6/15/30/60/120/300/600/1200V AC. Current: 0-30/60uA/1.5/3/15/30/150/300 mA/8/12A. Resistance: 0-3/30k/3/30k ohms. Decibels: -10 to +17dB. Output -0.3/6/15/30/60/120/300V. Accuracy ± 2%. DC, 4% AC. Sensitivity: 50,000 opv DC, 5,000 opv AC. 5 inch meter. Built in protection. Size: 57 x 102 x 153mm.
OUR PRICE £11.95 P&P 40p



KAMODEN HM720B FET VOM
Input impedance 10 Megohms. Ranges: 0/0.25/1.25/10/50/100V DC. 0/2.5/10/50/100V AC. Resistance: 0/25uA/2.5/25/250 mA DC. 0/5k/50k/500k/5 M 50k Megohms.
OUR PRICE £14.95 P&P 30p



370WTR MULTIMETER
Features AC current ranges, 20,000 opv. 0/0.5/2.5/10/50/250/500/1000V DC. 0/2.5/10/50/250/500/1000V AC. 0/50uA/1/10/100 mA/1/10A DC. 0/0.75/150/300/500k/5 Meg/50 Meg. Decibels: -20 to +62dB.
OUR PRICE £17.50 P&P 25p



TE40 HIGH SENSITIVITY AC VOLT METER
10 ranges: 0.001/ 0.010/ 0.1/ 0.3/ 1/ 3/ 10/ 30/ 100/ 300V RMS. 5cps. ± 2MHz. -40 to +50dB. Supplied complete with leads and instructions.
OUR PRICE £17.50 P&P 25p



MODEL U4311 Sub-standard Multi-range Volt-Ammeter
Sensitivity 330 Ohms/Volt AC and DC. Accuracy 0.5% DC. 1% AC. Scale length: 165mm. 0/300/750uA. 1.5/3/7.5/15/30/75/150/300/750mA/1.5/3/7.5 A DC. 0/3/7.5/15/30/75/150/300/750mA/1.5/3/7.5 A AC. 0/0.75/150/300/750mV/1.5/3/7.5/15/30/75/150/300/750V DC. 0/750mV/1.5/3/7.5/15/30/75/150/300/750V AC. Automatic cut out device. Supplied complete with test leads, manual and test certificates.
OUR PRICE £49.00 P&P 50p



U4317 MULTIMETER
High sensitivity instrument for field and laboratory work. Knife edge pointer, 86mm. mirror scale. Ranges: 100V/V. 0.5/2.5/10/25/50/100/250/500/1000V DC. 0.5/2.5/10/25/50/100/250/500/1000V AC. Current: 50uA/0.5/1/5/10/50/250mA/175A AC. Resistance: 0.5/10/100/200 ohms/1/3/30/300k ohms. Decibels: -5 to +10dB. Battery operated. Size: 210 x 115 x 90mm. Supplied in carrying case complete with leads.
OUR PRICE £15.00 P&P 20p



Model HT100B4 MULTIMETER
Overload protected, shock proof circuits. 9.5uA Meter with mirror scale. Sensitivity 100kV. Polarity change switch. Ranges: 0.5/2.5/1.5/50/500/1000V DC. 0.25/ 0.5/1/5/10/50/100/175A AC. Resistance: 0.5/10/100/200 ohms/1/3/30/300k ohms. Decibels: -5 to +10dB. Battery operated. Size: 210 x 115 x 90mm. Supplied in carrying case complete with leads.
OUR PRICE £17.50 P&P 40p



TE85 VALVE VOLTMETER
28 ranges. DC volts 1.5-1500V. AC volts 1.5-1500V. Resistance up to 1000 Megohms. 200/240V AC operation. Complete with probe and instructions.
OUR PRICE £17.50 P&P 30p



C15 PULSE OSCILLOSCOPE
For display of pulsed and periodic waveforms in electronic circuits. VERT. AMP Bandwidth: 10MHz. Sensitivity at 100kHz VRMS/mm: 0.1-25. HOR. AMP. Bandwidth: 500kHz. Sensitivity at 100kHz VRMS/mm: 0.3-25. Preset triggered sweep 1-3000usc. Free running 20-200 kHz in nine ranges. Calibrator pips. 220 x 380 x 430mm. 115-230V AC.
OUR PRICE £39.00 Carr. paid



RUSSIAN C116 Double Beam OSCILLOSCOPE
5 MHz case band. Separate Y1 and Y2 amplifiers. Rectangular 5" x 4" CRT. Calibrated triggered sweep from 0.2usc to 100 milli-sec/cm. Free running time base. 50Hz-1MHz. Build time base. Calibrator and amplitude Calibrator. Supplied complete with all accessories and instruction manual.
OUR PRICE £87.00 Carr. paid



LB4 TRANSISTOR TESTER
Tests PNP or NPN transistors. Audio indication. Operates on two 1.5V batteries. Complete with instructions etc.
OUR PRICE £4.50 P&P 20p



U4341 Multimeter & Transistor Tester
27 ranges. 16,700 opv. Overload protected. Ranges: 0.3/1.5/3/30/60/150/300/900V DC. 1.5/7.5/30/150/300/750V AC. Current: 0.05/0.5/5/6/6/60/800mA DC. 0.3/30/300mA AC. Resistance: 0/0.8/8/20/60/200k ohms/2 Mohms. Battery operated. Supplied complete with probes, leads and steel carrying case. Size: 115 x 215 x 90mm.
OUR PRICE £10.50 P&P 20p



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CLEAR PLASTIC PANEL METERS

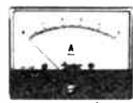
USED EXTENSIVELY BY INDUSTRY, GOVERNMENT DEPARTMENTS, EDUCATIONAL AUTHORITIES ETC.

Over 200 ranges in stock—other ranges to order. Quantity discounts available. Send for fully illustrated brochure.

CLEAR PLASTIC MODEL S0640

Size: 85 x 64mm

50uA	£3.35
100uA	£3.30
200uA	£3.30
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50-0-500uA	£3.35
100-0-1000uA	£3.30
1mA	£3.20
5mA	£3.20
10mA	£3.20
50mA	£3.20
100mA	£3.20
500mA	£3.20
1A DC	£3.20
5A DC	£3.20
10A DC	£3.20
5V DC	£3.20



20V DC .. £3.20
50V DC .. £3.20
100V DC .. £3.20
15V AC .. £3.30
300V AC .. £3.30
VU Meter .. £3.45

CLEAR PLASTIC MODEL SW100

Size: 100 x 80mm

50uA	£4.55
100uA	£4.35
500uA	£4.10
50-0-500uA	£4.35
100-0-1000uA	£4.30
1mA	£3.95
1A DC	£3.95
5A DC	£3.95
20V DC	£3.95
50V DC	£3.95
300V DC	£3.95



CLEAR PLASTIC MODEL 45P

Size: 50 x 50mm

50uA	£3.00
100uA	£2.85
200uA	£2.75
500uA	£2.70
50-0-500uA	£2.75
100-0-1000uA	£2.90
1mA	£2.65
5mA	£2.65
10mA	£2.65
50mA	£2.65
100mA	£2.65
500mA	£2.65
1A DC	£2.65
5A DC	£2.65
10V DC	£2.65
20V DC	£2.65
50V DC	£2.65
300V DC	£2.65
15V AC	£2.70

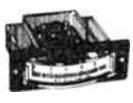


300V AC .. £2.70
S Meter 1mA .. £2.75
VU Meter .. £3.00
1A AC .. £2.65
5A AC .. £2.65
10A AC .. £2.65
20A AC .. £2.65
30A AC .. £2.65

EDGEWISE MODEL PE70

Size: 90 x 34mm

50uA	£4.15
100uA	£3.95
200uA	£3.75
500uA	£3.50
50-0-500uA	£3.95
100-0-1000uA	£3.85
1mA	£3.50
300V AC	£3.50
VU Meter	£4.25



MODEL E0107 EDUCATIONAL METER

Size: 100 x 90 x 150mm including terminals

A range of high quality moving coil instruments ideal for school experiments and other bench applications. 3" mirror scale. The meter movement is easily accessible to demonstrate internal working.



50uA	£7.60
100uA	£7.05
50-0-500uA	£7.70
1A DC	£6.55
5A DC	£6.55
10V DC	£6.55
15V DC	£6.55
20V DC	£6.55
50V DC	£6.55

300V DC ..	£6.55
500mA/5A DC	£6.55
5V/50V DC ..	£7.70
5V/15V DC ..	£7.70
1A/15A DC ..	£7.70

CLEAR PLASTIC MODEL 85P

Size: 120 x 110mm

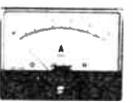
50uA	£4.85
100uA	£4.70
200uA	£4.45
500uA	£4.30
50-0-500uA	£4.70
100-0-1000uA	£4.65
500-0-5000uA	£4.30
1mA	£4.30
1-0-1mA	£4.30
10mA	£4.30
50mA	£4.30
100mA	£4.30
500mA	£4.30
1A DC	£4.30
5A DC	£4.30
15A DC	£4.30
30A DC	£4.30
10V DC	£4.30
20V DC	£4.30
50V DC	£4.30



CLEAR PLASTIC MODEL S0460

Size: 59 x 46mm

50uA	£3.10
100uA	£3.05
200uA	£3.00
500uA	£2.80
50-0-500uA	£3.10
100-0-1000uA	£3.05
1mA	£2.85
5mA	£2.85
10mA	£2.85
50mA	£2.85
100mA	£2.85
500mA	£2.85
1A DC	£2.85
5A DC	£2.85
10A DC	£2.85
15A DC	£2.85
20A DC	£2.85
3V DC	£2.85
10V DC	£2.85



15V DC .. £2.50
20V DC .. £2.50
50V DC .. £2.50
100V DC .. £2.50
300V DC .. £2.50
300V AC .. £2.55
S Meter 1mA .. £2.55
VU Meter .. £2.90

POWER RHEOSTATS

High quality ceramic construction. Windings embedded in vitreous enamel. Heat duty brush wiper. Continuous rating. Wide range available ex-stock. Single hole fixing. X" diameter shafts. Bulk quantities available.



25 WATT	10/25/50/100/250/500/1000 Ohms	£1.15	P&P 10p
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100 WATT	15/10/25/50/100/250/500/1000/2500 Ohms	£2.34	P&P 15p

AUTO TRANSFORMERS

0/115/250V. Step up or step down.

80 WATTS	£2.75	P&P 18p
150 WATTS	£3.50	P&P 18p
300 WATTS	£4.50	P&P 23p
500 WATTS	£6.95	P&P 33p
1000 WATTS	£9.50	P&P 38p
1500 WATTS	£12.50	P&P 43p
2250 WATTS	£20.95	P&P 50p
5000 WATTS	£44.95	P&P £1

CP110 CHASSIS PUNCH SET



Carefully machined top grade steel. Contains 1/2", 5/8", 3/4", 1" and 1 1/8" punches complete with gripper and accessories.

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Excellent quality at low cost. Input: 230V 50/60Hz. Output 0-260V. MODEL S260 BENCH MOUNTING

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5A	£17.50	37p
8A	£30.35	50p
10A	£37.75	75p
12A	£42.50	75p
20A	£85.00	125p
25A	£95.00	130p
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MODEL S260B PANEL MOUNTING

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BVD5 Vernier TUNING DIAL

App. 7:1 ratio planetary drive vernier dial. Log scale 0-180 degrees. Blank scales 1-5. Size 128 x 76mm. Overall size 190 x 117 x 41mm. Deep including knob and coupling. K" diam. shaft

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No Soldering required. All connect-made with spring clips. Kit includes all parts and wire including ear-piece. Will receive all normal broadcasts on Medium Wave 535-1805kHz. Operates from standard 9V battery or Solar Cell included.

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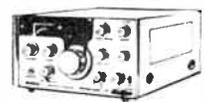
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Handy SWR meter for transmitter antenna alignment, with built-in field strength meter. Accuracy 5%, Impedance 52 Ohm. 100uA DC. Full scale 5 section collapsible antenna. Size 145 x 50 x 60mm.

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SUPER VALUE TOP QUALITY TRIO equipment

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Nine wave-bands covering 1.8-29.7 MHz. 140-146MHz and 10MHz WWV SSB, CW, AM and FM. AF output is more than 1 watt. S Meter. Squelch control. BFO. Variable AF and RF controls. 4-16 ohm output and jack for phono. Power requirement 100/240V AC, 12/14V DC. Size: 270 x 140 x 310mm.

Our Price £132.50 CARR. PAIO

TRIO 9R500S RECEIVER



Four bands covering 550kHz to 30 MHz continuous and electrical band spread on 10, 15, 20, 40, and 80 mtrs. 8 valve plus 7 diode circuit. 4 to 8 ohm output and phone jack. SSB-CW, ANL, variable BFO. S Meter and separate band spread dial. IF frequency 445kHz, audio output 1 1/2 watt. Variable RF and AF gain controls. 115/250V AC, with instructions.

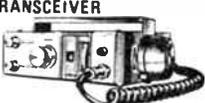
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TRIO TR2200 TRANSCEIVER

Fully transistorised portable VHF transceiver. Will transmit and receive on six channels between 144-146MHz. 1 watt transmitter. 12V DC internal or external supply. Built-in charger for Ni-Cad cells. Power/volume switch, squelch control, channel selector, mic, socket, earphone/external speaker socket. Complete with microphone and 144.48, 144.72 & 145.32 crystals. Size: 134 x 58 x 180mm.

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BELTEK W5400 CAR TRANSCEIVER



Solid state mobile transceiver for 12 volt DC car. Transmits and receives on any 12 of 28 channels between 144 and 146MHz. Power output 10W and 1W switchable. Controls: On/off/volume, squelch and channel selector. Internal 3" speaker. Complete with dynamic mic. P.T.T switch, three sets crystals for 144.48, 144.6, 144.6 and 145MHz, mounting bracket and instructions. Size: 150 x 70 x 220mm.

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SK YFON 100mw
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P302 Two Channel 300mW
OUR PRICE £52.50 per pair
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OUR PRICE £71.25 per pair
P&P 50p per pair
NB. Licence required for use in UK

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- 34 LILLE ST. WC2 01-437 9155
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- 193 EDGWARE RD. W2 01-723 6211
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- 311 EDGWARE RD. W2 01-262 0387
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TE1018 Deluxe Mono High Impedance Headset.

Sensitive magnetic headset with soft ear pads. Impedance 2,500 ohms (600 ohms DC) Frequency response 200-4,000Hz.
OUR PRICE £2.25



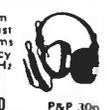
HO2S STEREO HEADPHONES

Wonderful value and excellent performance combined. Adjustable head band. Impedance 8 ohms 20-12,000Hz. Complete with lead and plug.
OUR PRICE £2.25



TE1035 Stereo HEADPHONES

Low cost with excellent response. Foam rubber earcups. Adjustable headband. 8 ohms impedance. Frequency response 25Hz-18kHz. Complete with cable and stereo jack plug.
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SH80V MONO/STEREO HEADPHONES

Volume control for each channel. 4/16 ohms impedance. Frequency response 20Hz-18kHz. Complete with 10ft. coiled lead and jack plug.
OUR PRICE £4.97



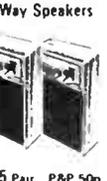
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Moving coil. Ideal for language teaching, communications etc. Headphone impedance 16 ohms. Microphone impedance 200 ohms.
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SPECIAL BARGAIN!! PHONIC 10 Two Way Speakers

Matched pair of compact bookshelf speakers of unique design incorporating a 2" high frequency unit & 6" woofer. 8 ohms impedance. Size: 348 x 228 x 110mm.
OUR PRICE £8.85 pair



SPECIAL BARGAIN !! STEREO SOUND SPEAKERS

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High quality three way speaker system offering a performance better than more expensive units. Teak finished with dark fronts. Frequency response: 40Hz-20kHz. 8 ohms impedance. Maximum power 20 watts. Size: 476 x 232 x 232mm.
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All kits are complete with comprehensive easy to follow instructions and covered by full guarantee. Post and Packing 15p per kit.

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- GP312 Circuit board..... £11.45
- GU330 Tremolo unit..... £7.45
- HF61 Diode detector..... £3.32
- HF65 FM transmitter..... £2.70
- HF75 FM receiver..... £2.87
- HF310 FM tuner..... £15.81
- HF325 Deluxe FM tuner..... £24.12
- HF330 Decoder (HF310/325)..... £9.96
- HF380 lw/hf aerial amplifier..... £4.94
- HF395 broadband serial amp..... £1.77
- LF380 Quadraphonic device..... £11.36
- M160 Multi-vibrator..... £1.71
- M191 VU Meter..... £4.55
- M192 Stereo balance meter..... £4.97
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- NT10 Stabilised power supply 100mA 9V..... £5.15
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Amateur Electronics by Josty-Kit, the professional book for the amateur - covers the subject from basic principles to advanced electronic techniques. Complete with circuit board for AE1 to AE10 above.
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High quality 2 way speaker systems. 25 Watts. 4-8 ohms. 40Hz-18kHz. Size: 560 x 340 x 255mm. approx. Wood grain finish with black fronts.
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Built-in driver unit. Impedance 16 ohms. Power rating 10W. Response 380-7000Hz. Size approx. 6" x 6" x 5". Weather and UV shock protected.
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- 710..... £22.70
- 810..... £28.30
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- MP60/ADC K8..... £11.50
- MP60/TPD..... £14.20
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- 40M 85p £4.00 £7.50
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Model 350 13 x 8" with single tweeter/crossover 20-20,000Hz. 15 watts RMS. Available 8 or 15 ohms.
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Model 450 13 x 8" with twin tweeters/crossover 55-13,000Hz. 8 watts RMS. Available 8 or 15 ohms.
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SINCLAIR CAMBRIDGE CALCULATOR

To build yourself. Complete kit of parts with step by step instructions to build a full specification pocket sized calculator.



OUR PRICE £24.95 P&P free
ALSO AVAILABLE READY BUILT Recommended Price £29.95

OUR PRICE £27.20 P&P 25p

Also available - **SINCLAIR EXECUTIVE** Recommended Price £39.00

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SINCLAIR EXECUTIVE with MEMORY Recommended Price £49.00

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- Z40 Power Amplifier..... £5.45
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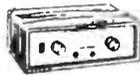
SINCLAIR Project 80 Packages

- 2 x Z40/Stereo 80/P25..... £25.00
- 2 x Z40/Stereo 80/P26..... £27.75
- 2 x Z60/Stereo 80/P28..... £30.45

POST & PACKING 35p each.

AUDIOTRONIC AH401 Stereo Headphone Amplifier

All silicon. transistor amplifier operates from magnetic, ceramic or tuner inputs with twin stereo headphone outputs and separate volume controls for each channel. Operates from 9V battery. INPUTS: 5mV and 100mV. OUTPUT: 50mV per channel.
OUR PRICE £8.50 P&P 20p



1021 Stereo Listening Station

For balancing and gain selection of loudspeakers with additional facility for stereo headphone switching. Two gain controls. On-off slide switch, stereo headphone socket.
OUR PRICE £2.25 P&P 15p



MP7 MIXER-PREAMPLIFIER

5 Microphone inputs each with individual gain controls enabling complete mixing facilities. Battery operated Size 235 x 127 x 26mm. Inputs: Mic. 3 x 3mV 50k; 2 x 3mV 600 ohms. Phono. Mag. 4mV 50k; Phono Ceramic 100mV 1 Meg. Output 250mV 100k.
OUR PRICE £8.97 P&P 20p



EA41 REVERBERATION AMPLIFIER

Self contained, transistorised, battery operated. Simply plug in microphone, extra etc. and output to your amplifier. Volume control and depth of reverb control. Beau-walnut cabinet, 184 x 77 x 108mm.
OUR PRICE £7.50 P&P 20p



Model A1018 FM TUNER

6 transistor high quality unit - 3IF stages and double tuned discriminator. For use with most amplifiers. Covers 88-108MHz. Powered by 9V battery.
OUR PRICE £9.65 P&P 30p
Stereo multiplex adapter £4.97 extra.



ALL PRICES EXCLUDE VAT

The Sinclair Cambridge... no other calculator is so powerful and so compact.

Complete kit-£24.95! (PLUS VAT)

The Cambridge – new from Sinclair

The Cambridge is a new electronic calculator from Sinclair, Europe's largest calculator manufacturer. It offers the power to handle the most complex calculations, in a compact, reliable package. No other calculator can approach the specification below at anything like the price – and by building it yourself you can save a further £5.50!

Truly pocket-sized

With all its calculating capability, the Cambridge still measures just $4\frac{1}{2}'' \times 2'' \times \frac{1}{16}''$. That means you can carry the Cambridge wherever you go without inconvenience – it fits in your pocket with barely a bulge. It runs on ordinary U16-type batteries which give weeks of life before replacement.

Easy to assemble

All parts are supplied – all you need provide is a soldering iron and a pair of cutters. Complete step-by-step instructions are provided, and our service department will back you throughout if you've any queries or problems.

Total cost? Just £27.45!

The Sinclair Cambridge kit is supplied to you direct from the manufacturer. Ready assembled, it costs £32.95 – so you're saving £5.50! Of course we'll be happy to supply you with one ready-assembled if you prefer – it's still far and away the best calculator value on the market.



Features of the Sinclair Cambridge

- * Uniquely handy package. $4\frac{1}{2}'' \times 2'' \times \frac{1}{16}''$, weight $3\frac{1}{2}$ oz.
- * Standard keyboard. All you need for complex calculations.
- * Clear-last-entry feature.
- * Fully-floating decimal point.
- * Algebraic logic.
- * Four operators (+, -, x, ÷), with constant on all four.
- * Constant acts as last entry in a calculation.
- * Constant and algebraic logic combine to act as a limited memory, allowing complex calculations on a calculator costing less than £30.
- * Calculates to 8 significant digits, with exponent range from 10^{-20} to 10^{79} .
- * Clear, bright 8-digit display.
- * Operates for weeks on four U16-type batteries. (MN 2400 recommended.)

A complete kit!

The kit comes to you packaged in a heavy-duty polystyrene container. It contains all you need to assemble your Sinclair Cambridge. Assembly time is about 3 hours.

Contents :

1. Coil.
2. Large-scale integrated circuit.
3. Interface chip.
4. Thick-film resistor pack.
5. Case mouldings, with buttons, window and light-up display in position.
6. Printed circuit board.
7. Keyboard panel.
8. Electronic components pack (diodes, resistors, capacitors, transistor).
9. Battery clips and on/off switch.
10. Soft wallet.



This valuable book – free!

If you just use your Sinclair Cambridge for routine arithmetic – for shopping, conversions, percentages, accounting, tallying, and so on – then you'll get more than your money's worth.

But if you want to get even more out of it, you can go one step further and learn how to unlock the full potential of this piece of electronic technology.



How? It's all explained in this unique booklet, written by a leading calculator design consultant. In its fact-packed 32 pages it explains, step by step, how you can use the Sinclair Cambridge to carry out complex calculations.

sinclair

Sinclair Radionics Ltd, London Road,
St Ives, Huntingdonshire
Reg. no : 699483 England
VAT Reg. no : 213 8170 88

Why only Sinclair can make you this offer

The reason's simple : only Sinclair – Europe's largest electronic calculator manufacturer – have the necessary combination of skills and scale.

Sinclair Radionics are the makers of the Executive – the smallest electronic calculator in the world. In spite of being one of the more expensive of the small calculators, it was a runaway best-seller. The experience gained on the Executive has enabled us to design and produce the Cambridge at this remarkably low price. But that in itself wouldn't be enough. Sinclair also have a very long experience of producing and marketing electronic kits. You may have used one, and you've almost certainly heard of them – the Sinclair Project 60 stereo modules.

It seemed only logical to combine the knowledge of do-it-yourself kits with the knowledge of small calculator technology.

And you benefit!

Take advantage of this money-back, no-risks offer today

The Sinclair Cambridge is fully guaranteed. Return your kit within 10 days, and we'll refund your money without question. All parts are tested and checked before despatch – and we guarantee a correctly-assembled calculator for one year.

Simply fill in the preferential order form below and slip it in the post today.

Price in kit form: £24.95 + £2.50 VAT. (Total: £27.45)

Price fully built: £29.95 + £3.00 VAT. (Total: £32.95)

PW 4/74

To : Sinclair Radionics Ltd, London Road,
St Ives, Huntingdonshire, PE17 4HJ

Please send me

a Sinclair Cambridge calculator kit at
£24.95 + £2.50 VAT (Total: £27.45)

a Sinclair Cambridge calculator ready
built at £29.95 + £3.00 VAT
(Total: £32.95)

*I enclose cheque for £ _____, made
out to Sinclair Radionics Ltd, and
crossed.

*Please debit my *Barclaycard/Access
account. Account number _____

*Delete as required.

Name _____

Address _____

PLEASE PRINT

SAFETY FIRST

TO encourage safety in the mere presence of electrical, electronic, radio or television apparatus, let alone during their operation, is not only laudable but vital. Hence the British Electrotechnical Approvals Board for Household Equipment (now affectionately BEAB) is extending the BEAB Approval Scheme to include audio and radio products including record players, radios, radiograms, mains/battery portable receivers with (curiously) "continuously rated audio outputs up to 6 + 6 watts stereo or 10 watts mono". Manufactured equipment that is licensed to bear the BEAB approval marking has to be first subjected to some detailed and stringent tests at the BSI laboratory.

The specification for the tests, detailed in BS 415: 1972 (with amendments), highlights for the more casual of the manufacturers, and probably some of the amateur constructor fraternity, areas of potential risk in mains driven equipment that all too often are taken for granted. There are, of course, extreme cases like the ladies' dangling necklace test and the test which inserts artificial fingers into apertures almost in determination to find live contact.

Generally the scheme is an excellent one. In most British equipment, that is designed and manufactured by responsible people, it is unlikely that no thought will be given to hazards such as shock, fire risk, ionised radiation, implosion and the like.

What has been needed is some form of yardstick by which a known hazard can be measured. Let us not be carried away by any thought that this standard is for manufacturers only. There are frequent cases where more strict attention to detail is needed by everyone who has mains driven appliances or electronic equipment.

We have only one serious complaint: that is the use of graphical symbols to indicate the nature of the supply (a.c. or d.c.) and to indicate live terminals. To the uninitiated layman, technical symbols mean nothing and he will not be inclined to buy BS3939 to find out before operating his new purchase.

Elsewhere in this issue we have highlighted only a few of the points in BS415 that we feel the general public need to know about. It is stressed that the detailed specification is designed to cover most contingencies of normal operation; we recommend manufacturers, suppliers and users to refer to this for more information.

M. A. COLWELL—*Editor*.

The May issue of *Practical Wireless* will include a special pull-out feature to make a handy booklet "Guide to Long Distance Reception of Radio and TV", (useful for locals, too!). Also appearing will be constructional projects: the medium wave "Mini-Pop" (goes in a jacket pocket); an audio booster and power supply to enable you to hear cassette recordings in the car; a trace doubler to enable you to convert a single-beam oscilloscope for four displays. We shall also be giving first details of a super new project that we know will appeal to sports fans all over the world. Don't miss out—order your copy regularly NOW.

(All advanced details are subject to the current national industrial situation).

Further details on page 1167

NEWS...

Export sales of British made Dolby

IN a recent statement Phoenix Videosonic Ltd., of Braintree, Essex, Europe's only manufacturer of Dolby Noise Reduction Units announced significant export sales to Europe, North America and Japan.

A Videosonic spokesman stated: "Videosonic leads the world in the technical specification of its equipment: in the PD4 we have introduced a new high level Dolby 'B' circuit providing a unique range of over 95dB between noise and 0.1% distortion. At this time the PD4 represents the ultimate way to take the PSSST! out of tape.

To further extend our lead in the World Hi-Fi market, the PD2b has been introduced as the world's first battery operated Dolby Unit, allowing 'field' use in the most rigorous conditions. The integral microphone pre-amplifier makes this an ideal unit for reporter or similar usage.

World recognition of Videosonic technical manufacturing competence has been most encouraging, and we can only take pride in our immediate penetration of the Japanese market in the face of very strong local competition. We are advised that our range of Dolby products will be displayed and demonstrated in the top 850 Hi-Fi Retail Shops in Japan, and that local response to date has been very positive. Our first shipment to Japan leaves this week.

Portable Fluorescent Lamp (March P.W.)

WILL readers please note, that the transformer specified is now no longer available. An improved transformer is available from Messrs G. F. Milward at 77p plus 20p p & p. This includes full modification details and uses fewer components. A 21 in. 13W tube is available at 50p + 20p p & p, and it is claimed that this tube gives a greater light output than the 15W tube. S.A.E. to G. F. Milward for further details.

Bargains galore

IF you are in the "Ally Pally" area on March 24th, pay a visit to the Collector's Bazaar which is being held in the Palm Court.

This is a five-bazaar event which includes militaria, vintage post cards, vintage toys, transport relics and, of most interest to our readers, vintage records, horn gramophones, phonographs and probably some items of vintage radio equipment.

Practical Wireless visited one of these bazaars held at St. Johns Wood a few months ago, and it was there that Colin Riches purchased an Edison "Gem" phonograph to be featured in a future "Going Back."

If any readers want to find out the details of hiring a stall at the bazaar (£3.50 for the day) contact the organiser John Carter, Smewins, Shottesbrooke, nr. Maidenhead, Berks, SL6 3SR (Tel. Shurlock Row 539).

Otherwise, put on your cycle clips and pedal along to Alexandra Palace, Wood Green, London N.22, on March 24th. They'll let you in at 1 p.m. but be sure to have your entrance fee of 30p at the ready.

Hi-Fidelity 74

HI-FIDELITY 74 is a rival exhibition to the Sonex show. It will be run at the same time and held at the Heathrow Hotel, Bath Road. It's the idea of Malcolm Blockley who is the Hi-Fi Division Sales Manager of Pyser-Britex Ltd.—the sole UK distributor of Marantz, Teledyne and Kenosonic equipment.

The organiser states that this show has been arranged because many manufacturers are fed-up with trying to demonstrate their products in small, cramped hotel bedrooms.

Hi-Fidelity 74 will run from March 27th to 31st inclusive but the first two days will be for the trade and press only.

Blast them out!

IN order to reduce the effects of interference from an East German station at night, the BBC has increased the transmitting power of the Radio 4 Moor-side Edge transmitter to 300kW.

R and TV Components Ltd.

IN their March advertisement, the price of postage and packing for the "Stereo 21" should have read £1.60. Apologies to R and TV Ltd.

Public Address Exhibition

Readers who have an interest in outdoor activities, such as rallies, will be planning events for the coming season. To get up to date on public address installations, it would be worthwhile to visit Sound '74, the international exhibition of the Association of Public Address Engineers. A lecture programme will be held concurrently on p.a. design, building acoustics, microphones, and the financial side of public address work from the practical point of view.

The A.P.A.E. has received more stand space bookings than previously, but there are still a few left for those who wish to come in at a late stage, including suppliers of disco equipment.

Admission is free to all in-

terested persons: tradesmen, manufacturers, buyers, and users of public address and allied equipment in the entertainments business. Tickets can be obtained from exhibitors or from the A.P.A.E. Secretariat, 6 Conduit Street, London W1R 9TG.

The scope of activities covered is extended to include audio-visual effects.

Overseas readers will be interested to learn that the A.P.A.E. are exhibiting in Hall 9A at the Hanover Fair from 25th April to 3rd May 1974 and at the I.C.E.T.I.A. exhibition at Melbourne, Australia from 7th to 11th October

Practical Wireless will be on show at the Hanover Fair.

UK wavebands and frequencies

THE BBC Engineering Department have issued a useful data sheet which shows the frequencies and wavebands allocated to broadcasting in the United Kingdom. Below we give the details from that sheet:

Band	Frequencies	Service
Low frequency (l.f.) (long waves)	160-255kHz (1875-1176m)	} a.m. radio
Medium frequency (m.f.) (medium waves)	525-1605kHz (571-187m)	
High frequency (h.f.) (short waves)	3950-4000kHz (75-m band)	
	5950-6200kHz (49-m band)	
	7100-7300kHz (41-m band)	
	9500-9775kHz (31-m band)	
	11700-11975kHz (25-m band)	
	15100-15450kHz (19-m band)	
	17700-17900kHz (16-m band)	
	21450-21750kHz (13-m band)	
	25600-26100kHz (11-m band)	
Band I	(v.h.f.) 41-68MHz (channels 1 to 5)	405-line television
Band II	(v.h.f.) 88-97.6MHz	f.m. radio
Band III	(v.h.f.) 174-216MHz (channels 6 to 13)	405-line television
Band IV	(u.h.f.) 470-582MHz (channels 21 to 34)	625-line television
Band V	(u.h.f.) 614-854MHz (channels 39 to 68)	625-line television
Band VI	(s.h.f.) 11700-12500MHz (11.7-12.5GHz)	Not yet in use for broadcasting



A VARIABLE TIME SWEEP WINDSCREEN WIPER

P. S. COLLINS

IMAGINE the situation: you are driving your car in drizzly rain, you put on the windscreen wiper. One sweep is sufficient, so you switch it off. Five, ten or fifteen seconds later the windscreen needs another wipe, so you switch on the wiper again for another single stroke. This could go on for some time and tends to be wearisome.

The circuit here described saves this tiresome routine and allows you to relax in the automation of a variable time-sweep wiper. Although the circuit is designed for wiper motors with automatic parking facility, there is some information at the end of the article which will be helpful to those who have wiper motors without this facility.

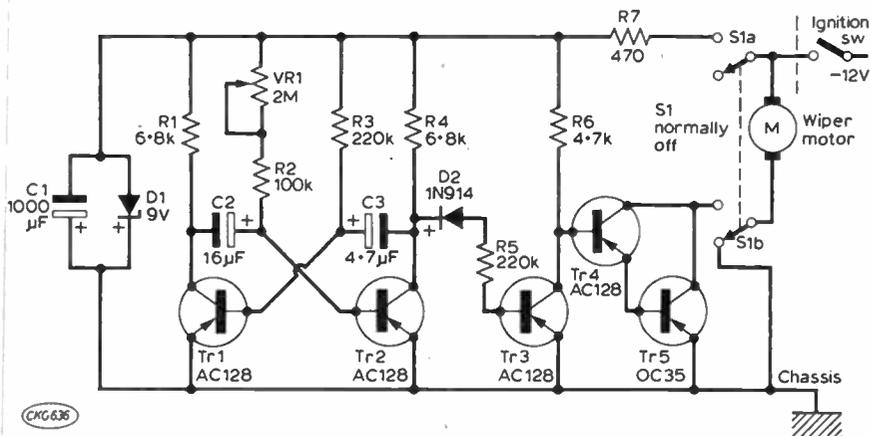
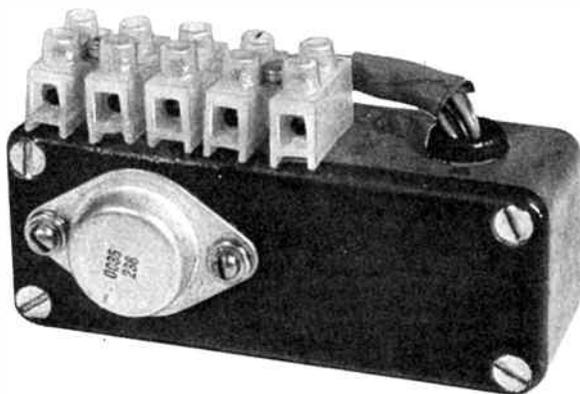
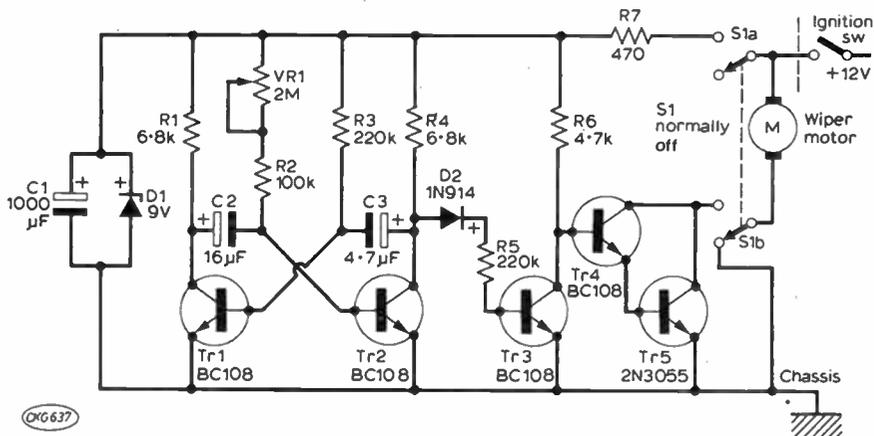


Fig. 1. Circuit of the Quickwipe for a vehicle with a **POSITIVE** earth system. It is essential to be quite sure which side of the battery is connected to chassis.

CMG636

Fig. 2. In this circuit for a **NEGATIVE** earth system, different transistors are used and capacitors and diodes are reversed compared to those in Fig. 1.



CMG637

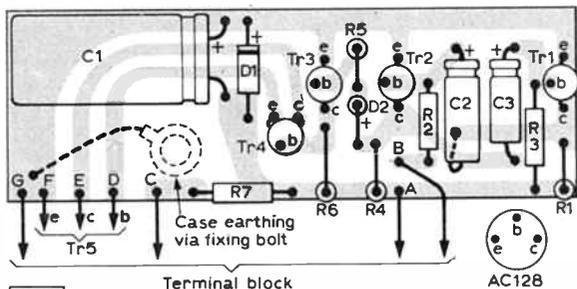
Figures 1 and 2 are the circuits for positive and negative earthed vehicles; the difference lies only with the active components and reverse connection of the polarised ones. The circuit action remains the same. Tr1 and Tr2 form a multivibrator generating a pulse of fixed length with a variable repetition rate. VR1 allows this rate to be varied between approximately 3 and 30 seconds. Tr3, 4 and 5 form a pulse amplifier to drive the wiper motor.

The fixed pulse length is $\frac{3}{4}$ second which is sufficient time to drive the motor long enough for its internal switches to take over the drive and thus return it to the park position. Switch S1 is centre off. One switch, S1b, switches for continuous operation, earth being directly applied to the motor.

In the other position, S1a, applies 12 volts to the circuit and S1b connects the motor as the load for the pulse amplifier. The vehicle wiper switch may now be regarded as redundant, or left in the circuit, as desired.

CONSTRUCTION

The whole unit can be comfortably housed in a die-cast box measuring $3\frac{1}{2} \times 1\frac{3}{8} \times 1\frac{1}{8}$ in. Figure 3



AM 0158

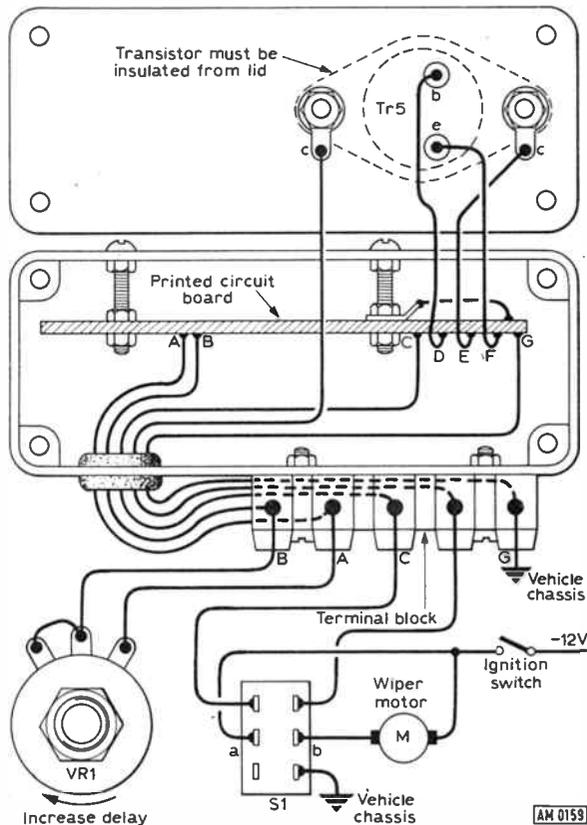
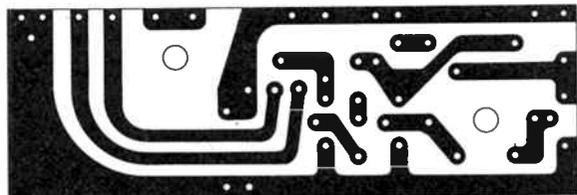
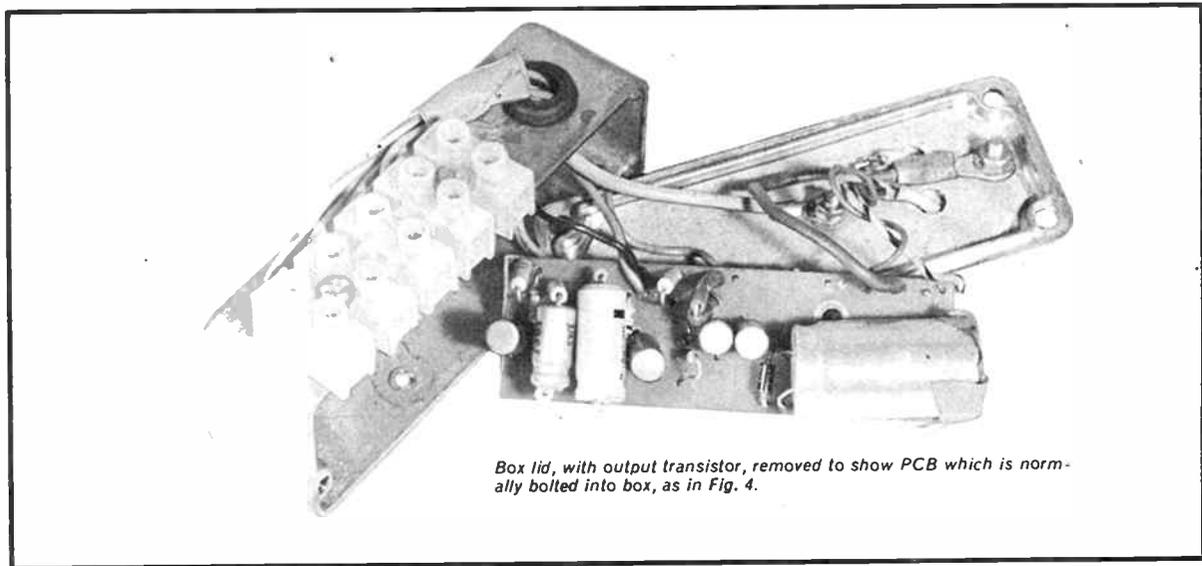


Fig. 3, left, shows PCB actual size and component layout for POSITIVE earth unit. Fig. 4, above, illustrates external wiring of Quickwipe.

shows the printed circuit board. Tr5 is mounted on the lid with insulating washer and bushes. All leads from the circuit board and Tr5 are connected to a five-way terminal strip fixed to the side of the box. This enables easy connection to the vehicle's wiring, as shown in Fig. 4.

Confirm the chassis polarity of the vehicle before constructing the unit, then use Fig. 1 OR Fig. 2 as appropriate.



Box lid, with output transistor, removed to show PCB which is normally bolted into box, as in Fig. 4.

★ components list

Resistors

R1	6.8k Ω	R5	220k Ω
R2	100k Ω	R6	4.7k Ω
R3	220k Ω	R7	470 Ω
R4	6.8k Ω	VR1	2M Ω linear

Resistors 10% $\frac{1}{2}$ W except R7 $\frac{1}{4}$ W

Capacitors

C1 1000 μ F 25V C2 16 μ F 16V C3 4.7 μ F 16V

Semiconductors

D1 9V zener 400mW D2 1N914

Positive Earth Tr1—4 AC128 Tr5 OC35

Negative Earth Tr1—4 BC108 Tr5 2N3055

Miscellaneous

S1, Double pole—double throw switch, centre off. Diecast box (RS Comps.—"Box 992"). Printed circuit board. Insulation kit for Tr5. Five way terminal block.

NOTE: It may be possible to arrange the fixed pulse length to correspond with the time taken for the wipers to travel one complete sweep, in the case of wipers without the self-park facility. This could be achieved by altering the values of R3 and C3.

These points are offered only as helpful guides. The author has conducted no tests in this regard and cannot therefore give any facts regarding accuracy or success. ■

Pw TECHNICAL CROSS PUZZLE No. 3 Solution



TELEVISION

IN THE APRIL ISSUE

CLOSED-CIRCUIT TV

Next month we start a new series aimed at giving an essentially practical account of closed-circuit TV equipment, its use and the servicing techniques required. To start with, the basic element in CCTV work, the vidicon camera tube, is explained along with its basic circuitry.

TRANSISTOR FIELD TIMEBASES

Fully transistorised field timebases have been around for some time now, particularly in colour receivers, and have proved to be generally very reliable. Nevertheless it is time we took a look at common faults and their causes, also at the operation of the class A output stage generally used.

THE DIODE DROPPER

The use of a diode dropper in the heater circuit reduces heat dissipation and is also cheaper than using a completely resistive dropper. The action of the diode dropper circuit is often misunderstood however, which can lead to the use of an incorrect accompanying resistor value and damage to the valves in the chain. The circuit action will be explained and the procedure for determining the value of the accompanying resistor given, either for designing a new circuit or for working out a diode dropper substitution for an existing set.

SERVICING TELEVISION RECEIVERS

The next chassis to be dealt with by Les Lawry-Johns is the Pye 169 single-standard monochrome chassis and its derivatives, the 569, 769 and 173.

PLUS ALL THE REGULAR FEATURES

Details of the April issue are subject to the current national situation at the time of going to press.

TO
(Name of Newsagent)

Please reserve/deliver the APRIL issue of TELEVISION (25p) and continue every month until further notice.

NAME

ADDRESS

GUIDE TO multi-range test meters

H. LEEMING G3LLL

IT does not seem many years since test meters were so expensive that, in the radio and TV trade, at least, one was shared between several engineers, the losers having to make do with wet fingers and neon screwdrivers! Test meters are now relatively cheap so that no enthusiast or handyman can really afford to be without one; whether it be for attending to the Hi-Fi system, fixing the car, or even sorting out a fault on the front door bell. Despite their simplicity in operation these meters can deceive the unwary and so it is hoped that a little basic theory will be of practical assistance.

The multi-range test meter commonly contains ranges such as AC and DC voltage, DC current and at least one resistance range. Other functions may be included on the more elaborate instruments but all use the basic meter movement plus the switching of various internal components in or out of circuit.

The DC Voltmeter

The meter movement fitted to most modern test instruments needs a current of something in the range of 1 to 1/100 of a milliamp to move a pointer across the full extent of the scale. The theoretical circuit of the basic meter movement is shown in Fig. 1. The "internal resistance" is not an actual resistor, but is the resistance of the coil of wire in the meter movement. From Ohm's Law, (voltage = current \times resistance) this 1mA meter movement shown will require a voltage of 0.1 volt for full scale deflection, ($1/1,000 \times 100/1 = 0.1$ volt). This basic meter could therefore be used to measure voltages of up to 0.1 volt or currents of up to 1 milliamp—not very useful!

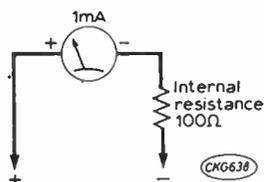


Fig. 1: Representation of meter movement must include resistance of moving coil.

The meter movement is basically a current operated device, but it can be made to read various quantities. A little thought will show that a 1mA meter movement will read full scale if 1 volt is

applied to it through a series resistance which, including internal resistance, totals 1,000 ohms. From Ohm's Law, 1 volt across 1,000 ohms causes a current of 1mA to pass. A voltmeter using a 1mA meter movement is said to have a sensitivity of 1000 ohms per volt.

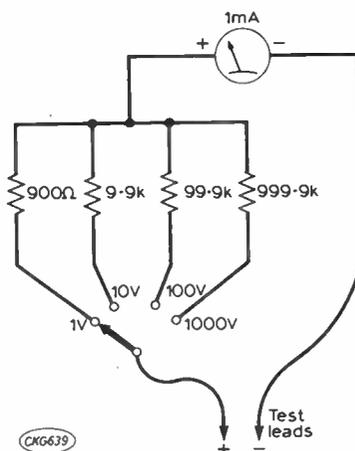


Fig. 2: Series resistors for voltmeter allow for coil resistance. Only of importance on lower ranges.

Fig. 2 shows the meter wired to read four ranges of voltage and it will be seen that the total resistance of the meter is 1,000 ohms for every volt of the range in question. For this reason it is referred to as 1,000 OPV and this would usually be marked on the meter scale.

Such a meter does have its disadvantages and its relatively low resistance can greatly affect circuit voltages as will be shown. In Fig. 3a two 1 ohm resistors are connected across the supply and the voltage between X and Y is measured. If the meter is switched to the 1 volt range it has a total resistance of 1,000 ohms (remember 1,000 OPV) this resistance being shunted across R2. As the meter resistance is very high, compared to R1 and R2, its effect is negligible and the reading is given accurately as 0.5 volts. If, however, the meter is transferred to the circuit in Fig. 3b and another reading is taken the resulting accuracy is quite different. Once again, the reading should be 0.5 volts, but note what happens when the meter is

connected across R2. R2 is shunted by the meter's resistance of 1,000 ohms and the resistance of the bottom half of the circuit drops to around 900 ohms. The voltage divides itself according to the ratio of the resistors and the meter reads just below 0.1 volts.

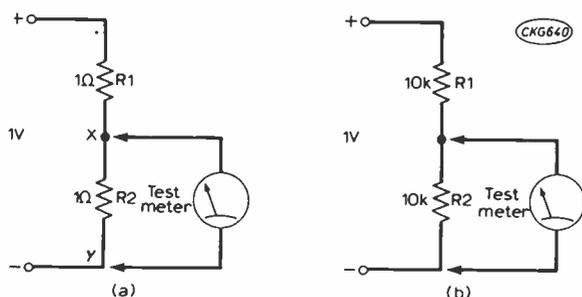


Fig. 3 (a) and (b) : to demonstrate effect of meter resistance on high and low resistance circuits.

The meter is not really wrong, it simply reads the voltage that is present when it is connected. Using the same meter a more accurate reading could be taken by switching to the 10 volt range when the test meter's resistance would rise to 10,000 ohms; the meter's resistance in parallel with R2 would then total 5,000 ohms and whilst the voltage reading would still be low at 0.33 instead of 0.5, it would be a little more realistic. Could we take the same argument further and switch to the 100 volt range with a meter resistance totalling 100,000 ohms, and obtain an accurate result? Unfortunately, no, since when the meter was switched to this range the pointer would move so little that we would not be able to take an accurate reading from it.

If we want a more accurate reading in a high resistance circuit the answer is a more sensitive meter movement that will allow us to insert larger values of voltage multiplier resistors. If for instance, we substitute a meter with a 50 micro-amp movement, (0.05mA), we will obtain a sensitivity of 20,000 OPV. Using circuit Fig. 3b we would then obtain, on the 1 volt range, a reading that was almost correct, (20,000 ohms being shunted across R2), or by switching to the 10 volt range using this higher sensitivity meter we would obtain a reading that was accurate to within all normal requirements.

As has been illustrated, the DC voltmeter can only read the voltage which is present when it is connected. It cannot guess at the voltage which appears when it is disconnected. When using a voltmeter one should get into the habit of comparing the resistance of the range being used with the resistance of the circuit being measured.

In many cases when operating in a high resistance circuit a more accurate reading will be obtained if a higher voltage range is used. If in doubt a reading should be taken on two adjacent ranges of the test meter. With any good quality instrument these readings should be about the same, but if they are not it implies that the meter is loading the circuit on the lower voltage range.

Valved or Transistorised Voltmeters

To obtain higher sensitivities using normal techniques requires very expensive and delicate meter movements. It is not common practice, therefore, to make multi-range test meters with a sensitivity

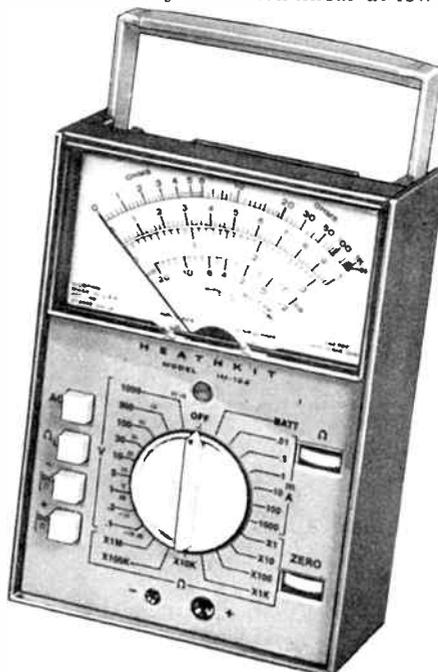
of much over 50,000 OPV. In some circumstances an even higher sensitivity is required, so that test meters of as high a sensitivity as this would be of little use at measuring, say, 0.1 volts in a circuit with resistance of several megohms. To enable higher sensitivities to be obtained, the valve and then the transistorised voltmeter were introduced. In these devices amplification is used so that an input resistance of 10 megohms or more is presented, even on the lowest voltage ranges. Such instruments are essential if tests are to be made in some high impedance transistorised circuits where very small voltages are present.

Frequency Response

Most test meters are basically intended for making tests at the mains frequency and their accuracy often falls off at frequencies in the audio range. One should check the frequency response of a test meter before relying upon it to check audio or bias frequency voltages. In the latter case it should be remembered that high frequency bias voltages can damage the rectifier in some test meters, and also that even if the meter's frequency response is adequate that its loading (possibly only a few hundred OPV) can, in many circuits, much reduce any voltage present. If it is desired to accurately measure voltages at high audio or radio frequencies the valve or transistorised voltmeter is again essential.

The AC Voltmeter

The AC ranges of multi-range test meter function in very much the same way as the DC ranges except that a rectifier is incorporated to enable the basic DC meter movement to function, see Fig. 4. As with the DC voltage section of the meter, the amount of loading on the circuit being tested is indicated by the sensitivity in ohms-per-volt. Rectifiers have a tendency to be non-linear at low current



The Heathkit IM-104 multimeter, a modern design providing 53 ranges on four scales. Frequency response up to 50kHz on AC voltage ranges. Input resistance of 10 MΩ on DC voltage ranges.

(Courtesy Heath (Glos.) Ltd.)

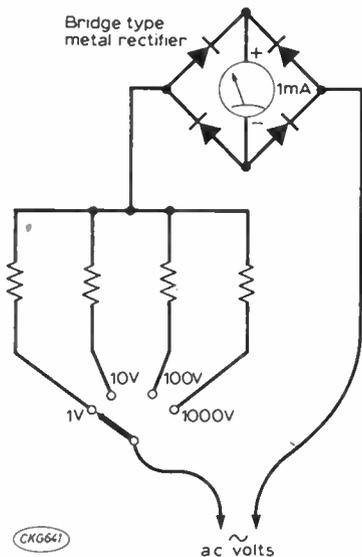


Fig. 4: Incorporation of meter bridge rectifier on AC voltage ranges.

levels and so, in the interest of accuracy, it is common to reduce the sensitivity of the test meter when switched to the AC ranges. The popular Avo Model 8, for instance, has a sensitivity of 20,000 OPV on the DC ranges but only 1,000 OPV on the AC ranges.

The Direct Current Ranges

The basic DC meter movement, as we have seen, will reach full scale when a small current is passed through it. The example shown in Fig. 1 needed 1mA for full scale deflection. If it is desired to measure a larger current, some of the current must be by-passed. The circuit with various resistors which are known as "shunts" is shown in Fig. 5. The value of shunt resistor R3, for instance, is calculated so that when the test meter is measuring 1A, 999 millicamps go via R3 and 1mA passes through the meter.

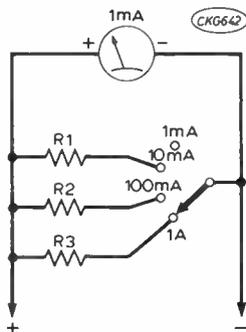


Fig. 5: Switchable shunts to increase current range of basic meter.

It is important to note that when measuring current, some voltage is required to operate the meter, as was shown earlier, when dealing with the DC voltmeter. In this case 0.1 volts will be dropped across the meter terminals. In most cases when making measurements, as in Fig. 6a, this small voltage drop will make negligible difference, being small in relation to the voltages in the circuit. If we try to make a test as shown in Fig. 6b however,

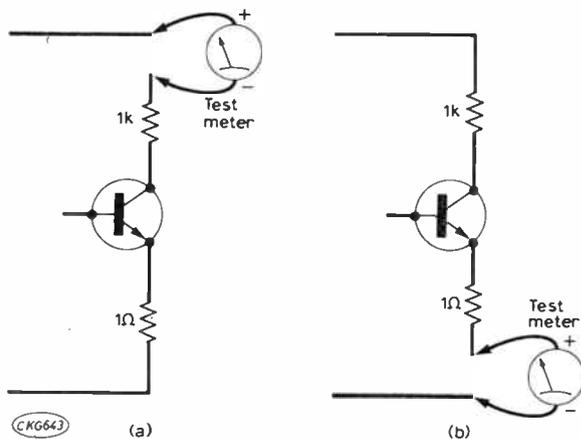


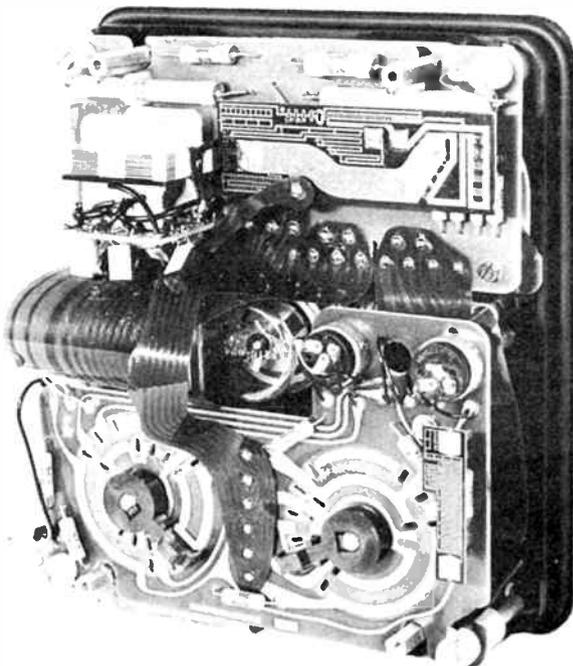
Fig. 6 (a) Correct and (b) incorrect method of inserting meter in transistor circuit.

this is not the case. Here the effect of adding the meter in series with the circuit is to considerably increase the value of the emitter resistor. Increasing this effective value would mean that the current which flowed with the test meter connected would be much less than the current which normally flowed in the circuit.

When checking current flow in low impedance circuits, it is better to measure the voltage across a known resistor and then to calculate the current.

The Resistance Ranges

Figure 7 shows a basic method of resistance measurement. If the test prods are touched together R2 can be adjusted until the meter reads full scale, the current being provided by the battery. As we have seen a 1mA meter when used as a voltmeter



An excellent view of the latest AVO Model 8. It uses printed circuit techniques for shunts and switchboards. (Courtesy AVO Ltd. Dover)

has a sensitivity of 1,000 OPV and here, if the battery is exactly 1.5V, R1 plus R2, plus internal resistance must equal 1,500 ohms, when R2 is set to provide full scale deflection with the test prods touching. If now, instead of touching the test prods together, we connect them to a resistor being tested, of 1,500 ohms, the meter will then read half-scale as an external resistor of the same value as the built-in resistance has been added to the circuit. The centre of the scale would be marked 1,500 ohms and with suitable calibration resistors of between, say, 50 and 50,000 ohms, resistors could be checked using this set-up, with reasonable accuracy.

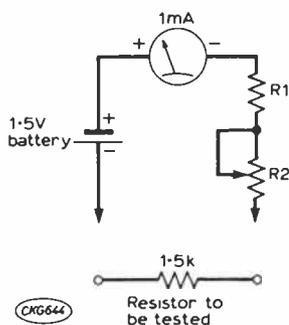


Fig. 7: Basic circuit for measuring resistance.

To divide the range by 10 we can shunt the meter as was done on the current ranges so that the sensitivity of the circuit becomes 100 OPV, enabling R1 and R2 to be reduced to 1/10 of their previous value. Alternatively, we can multiply the range by 10 by fitting a 15V battery and increasing R1 and R2 tenfold. In this way we obtain a meter with a centre scale range of 150, 1,500 and 15,000 ohms on three ranges enabling resistors from below 10 to above 500,000 ohms to be checked with good accuracy.



A large, clear scale with an anti-parallax mirror is the highlight of the latest AVO.

Use of Ohms Range

From the above discussion it will be seen that a current is passed through the component to be tested and that a voltage is also applied across it. In most cases this will do no harm, but it is wise to be aware that voltages of up to 25 or so are possible on the high resistance ranges and that currents in the order of 100mA or more may be found on the low ohms ranges of some test meters. When checking circuits where there is the slightest risk of damage being caused, it is wise to avoid using the highest or lowest ohms range on the test meter and to concentrate tests on the range which applies low voltage and low current. If magnetic devices, such as tape heads, are tested, note that they will be magnetised by the meter current. These tests should not be made, therefore, unless a de-fluxer is available to remove the residual magnetism.

It should be noted that no checks of resistance can be made unless the circuit which is being tested,

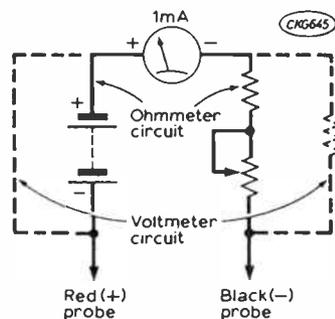


Fig. 8: Illustration of reverse polarity of probes in an ohmmeter circuit.

is completely dead. All voltage sources should therefore be disconnected before tests take place, as, quite apart from giving the wrong results, severe damage can be caused to the test meter and equipment if resistance tests are attempted on live circuits. Devices such as transistors, diodes and electrolytic capacitors are inherently polarity sensitive so the polarity of the voltage output of the test meter should be noted whilst making tests on these devices. As will be seen from Fig. 8 using normal circuit arrangements the polarity of the test prods is normally opposite to the ohms range to that marked on the meter for the voltage and current ranges.

Decibels

Many test meters have a scale marked in decibels marked in + and - values over a total of 15dB's or so. It must be clearly understood that the decibel is not an absolute value, such as the ohm or volt, but, as will be seen from the shape of the dB scale, is a logarithmically based system of comparison. Whilst many test meters are calibrated so that 0dB=0.775V this is just an arbitrary figure. In practical use, such as measuring the frequency response of an amplifier, the signal level is adjusted so that the output when measured with the test meter set to a suitable range, reads 0dB. If the input frequency is then varied the output variation, and hence the frequency response of the equipment being tested, can be read off directly in decibels.

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DY802	0.45	EF86	0.60	PC900	0.56	PL509	1.55	30C18/	
EABC80	1.00	EF89	0.91	PC984	0.52	PL802	0.98	PCF805	0.90
EB91	0.38	EF91	1.20	PC988	0.80	PY33	0.66	30F3/PF818	
EB81	0.75	EF92	1.40	PC989	0.65	PY81/800	0.50		1.10
EBF80	0.60	EF95	1.35	PC989	0.65	PY82	0.55	30FL1/	
EBF83	0.62	EF183	0.60	PC989	0.65	PY88	0.60	PCE800	0.75
EBF89	0.58	EF184	0.60	PC989	0.65	PY800A	1.05	30FL2	0.75
EC86	0.75	EF190	0.58	PC989	0.65	PY800	0.50	30FL12	1.05
EC88	0.77	EL34	0.95	PCF200	0.85	PY801	0.50	30FL14	0.85
EC81	0.48	EL36	1.05	PCF201	0.87	U25	1.00	30LI/PCC84	
EC82	0.48	EL81	0.90	PCF802	0.71	U191	1.00		0.52
EC83	0.45	EL84	0.47	PCF802	0.71	U193	0.50	30L15/PCC85	
EC84	0.65	EL85	0.55	PCF806	0.66	UABC80	0.98	U191	1.05
EC85	0.58	EL86	0.95	PCH200	0.88	UABC81	0.70	30L17	0.90
EC88	0.75	EL96	0.70	PCH200	0.88	UBF89	0.90	30P4MR	1.30
EC8189	0.71	EL91	1.81	PCL82	0.64	UCB81	1.00	30P12/PC801	
ECF80	0.55	ELK60	1.30	PCL83	0.66	UCB85	0.80		1.05
ECF82	0.78	EM84	1.18	PCL84	0.63	UCL84	0.70	30P19/PC802	
ECF86	0.71	EM87	1.18	PCL85/85		UFB8	0.90		1.00
ECF81	1.00	EY51	0.88	PD500	1.55	UL84	0.85	30P14/PC801	
ECF83	1.00	EY86/87	0.42	PFL200	0.80	U785	0.50		0.95
ECH84	0.78	EY86	0.64	PFL200	0.80	U786	0.50	30P12/	
ECL80	0.85	EZ80	0.51	PL81	0.75	6P23J/	1.00	PCF800	1.20
ECL82	0.61	EZ81	0.40	PL81A	0.88	6P23J/EF812		30P14/	
ECL83	0.68	GY501	0.90	PL82	0.50			PCL88	1.25
ECL86	0.63	GZ34	0.78	PL83	0.98	30C1/PCF80		30P16	1.05

BP41	3.00	6J6	0.30
8P61	0.75	6J7M	0.45
T41	1.00	6J7GT	0.40
U14	1.00	6K6GT	0.75
U25	0.58	6K7M	0.45
U26	0.85	6K7G	0.30
U191	0.75	6K8M	0.70
UABC80	0.40	6K8G	0.45
UAC42	0.78	6K25	0.78
U6A1	0.75	6L5G	0.55
UBC81	0.45	6Q7M	0.50
UBF80	0.40	6Q7G	0.50
UBF89	0.40	6SL7GT	0.48
UCC85	0.45	6SN7GT	0.48
UCH42	0.75	68Q7GT	0.48
UCH81	0.40	6U5G	0.75
CL82	0.35	6V6G	0.40
UC83	0.70	6V6GT	0.48
UF41	0.75	6X4	0.40
UF89	0.40	6X5G	0.40
UL41	0.85	6X5GT	0.45
UL84	0.48	7B6	0.75
U141	0.48	7B7	0.70
U785	0.40	7C9	1.30
VR105-30	0.40	7C6	0.75
VR150-30	0.40	7H7	0.70
OA2	0.40	7R7	0.75
OB2	0.40	787	2.25
1R5	0.45	7F4	0.75
1R5	0.40	12A7A	0.40
1T4	0.30	12A7T	0.40
384	0.40	12A06	0.45
3V4	0.70	12A07	0.38
5R4GY	0.80	12A X7	0.38
5U4G	0.40	12B A8	0.45
5V4G	0.50	12B B5	0.50
5Y3GT	0.45	30C1	0.80
5Z4G	0.45	30C15	1.05
6J30L2	0.90	30C17	1.10
6A K5	0.40	30C18	0.90
6A M5	0.90	30F6	1.10
6A Q5	0.45	30FL1	0.80
6A S7G	0.85	30FL2	0.75
6A T6	0.45	30FL14	0.90
6A U6	0.80	30LI6	1.05
6B A6	0.28	30LI7	0.95
6B E6	0.35	30P4MR	1.30
6B H6	0.75	30P12	1.05
6B J6	0.55	30P19	1.00
6B R7	1.00	30P1L	0.95
6B S7	1.35	30PL13	1.20
6B W6	0.90	30PL14	1.25
6B X7	0.90	30PL15	1.20
6C4	0.35	35W4	0.50
6C3DG	1.30	35Z4GT	0.70
6C H6	1.40	50C6DG	1.20
6C W4	1.00	807	0.50
6E23	1.05	813	ITT 213
6E25	1.00	813	ITT 213
6E28	0.70	813	ITT 213
6E35	0.65	865A	45.75
6E35	0.45	865A	1.00

NEW VALVES

Individually boxed and guaranteed but of European or other origin at greatly reduced prices. Quotations for any valve not listed. Send SAE for lists.

AZ1	0.60	EF90	0.25	PC86	0.60
AZ31	0.55	EF85	0.35	PC88	0.60
CHL31	1.20	EF86	0.30	PC97	0.50
CL33	1.50	EF89	0.28	PC900	0.48
CY31	0.50	EF91	0.37	PC984	0.40
DAF91	0.30	EF92	0.50	PC885	0.55
DAF96	0.50	EF95	0.40	PC989	0.50
DCC90	1.35	EF98	0.75	PC189	0.60
DF91	0.30	EF183	0.30	PCF80	0.30
DF96	0.50	EF184	0.35	PCF82	0.35
DK91	0.45	EL32	0.60	PCF86	0.60
DK92	0.70	EL33	1.75	PCF801	0.50
DK96	0.60	EL34	0.50	PCF802	0.50
DL92	0.40	EL36	0.60	PCF805	0.90
DL94	0.48	EL37	2.50	PCF806	0.75
DL96	0.55	EL41	0.90	PCF808	0.90
DY86/7	0.35	EL42	0.90	PCF82	0.35
DY802	0.37	EL84	0.28	PCL83	0.66
EABC80	0.88	EL95	0.40	PCL84	0.45
EAF42	0.75	EL80	1.00	PCL85	0.50
EB91	0.22	EM80	0.45	PCL86	0.45
EB33	1.00	EM81	0.60	PCL805/85	
EB41	0.75	EM84	0.35		
EB81	0.38	EM85	1.00	PD500	1.50
EBF80	0.40	EY51	0.40	PEN45	0.75
EBF83	0.40	EY86	0.40	PL36	0.55
EBF89	0.32	EZ40	0.75	PL81	0.50
EHL31	1.50	EZ41	0.75	PL82	0.45
EC81	0.40	EZ80	0.28	PL83	0.45
EC82	0.38	EZ81	0.26	PL84	0.40
EC83	0.35	GY501	0.80	PL500	0.75
EC84	0.30	GZ30	0.45	PL504	0.75
EC85	0.40	GZ32	0.50	PL508	0.90
EC88	0.40	GZ34	0.85	PL509	1.55
ECH36	1.25	GZ37	1.25	PL802	0.95
ECH42	0.30	HN209	1.50	PL84	0.40
ECH81	0.20	KT451	0.75	PLX4	3.50
ECH83	0.45	KT66	2.50	PX25	0.50
ECL80	0.55	KT81 (7C5)		PY81	0.30
ECL82	0.35			PY82	0.35
ECL83	0.70	KT81	1.75	PY83	0.38
ECL86	0.40	KT88	2.90	PY88	0.40
ECL880	3.00	KT451	1.00	PY900	1.00
EF7A	1.20	MU14	1.00	PY81/800	0.50
EF39	1.20	N74	2.75	PY901	0.50

TRANSISTORS-INTEGRATED CIRCUITS

EXPRESS POSTAGE

3p for first Transistor, for each additional add 1p.

AA119	0.7	BD132	0.50
AAZ13	0.10	BF115	0.22
AAZ15	0.10	BF167	0.25
AC107	0.35	BF173	0.28
AC126	0.25	BF179	0.33
AC127	0.25	BF180	0.35
AC128	0.20	BF181	0.35
AC176	0.25	BF194	0.13
AC187	0.20	BF195	0.13
AC188	0.20	BF197	0.15
ACY21	0.22	BF200	0.32
ACY39	0.65	BF861	0.25
AD140	0.50	BF898	0.25
AD149	0.50	BFX29	0.28
AD161	0.38	BFX28	0.22
AD182	0.39	BFY50	0.20
AF115	0.25	BFY51	0.20
AF116	0.25	BFY52	0.20
AF117	0.20	BFW10	0.81
AF186	0.40	BI100	0.15
AF239	0.44	BY128	0.14
ABY27	0.30	BY127	0.15
ABY28	0.25	BXZ61 series	
BA102	0.25		0.20
BA115	0.10	BZY88 series	
BC107	0.12		0.10
BC108	0.12	CR81-05	0.30
BC109	0.12	CR81-40	0.45
BC113	0.16	CR83-05	0.40
BC117	0.21	CR83-40	0.55
BC143	0.30	MJE340	0.50
BC147	0.12	MJE370	0.68
BC148	0.14	MJE320	0.65
BC190C	0.14	MJE2855	1.10
BC182	0.12	MJE3055	0.75
BC182L	0.12	MFP102	0.40
BC184L	0.13	MFP103	0.38
BCY32	1.20	MFP104	0.35
BCY33	0.38	MFP105	0.48
BCY34	0.45	MK7404	0.60
BCY70	0.15	OA5	0.60
BCY71	0.20	OA10	0.40
BCY72	0.15	OA79	0.10
BCZ11	0.65	OA81	0.10
BD121	1.00	OA91	0.10
BD124	0.30	OA90	0.08
HD131	0.45	OA202	0.10

All transistors, I.C.'s offered are new and branded. Manufactured by Mullard, Texas, RCA, Ferranti, Motorola, ITT, Fairchild, Lucas, etc. Quantity discounts on application. Send SAE for full lists.

OC16	1.00	ZTX500	0.15	2N2646	0.50
OC20	2.00	ZTX501	0.15	2N2904	0.20
OC23	1.25	ZTX503	0.16	2N2904A	0.25
OC25	0.40	ZTX531	0.25	2N2906	0.32
OC28	0.70	ZTX550	0.18	2N2905A	0.25
OC32	0.55	1N3014	0.06	2N2906	0.20
OC35	0.65	1N4001	0.8	2N2926	0.10
OC42	0.40	1N4002	0.7	2N3053	0.20
OC44	0.18	1N4003	0.8	2N3055	0.60
OC45	0.18	1N4004	0.8	2N3255	0.80
OC71	0.15	1N4005	0.10	2N3614	0.59
OC72	0.25	1N4006	0.12	2N3615	0.65
OC76	0.30	1N4007	0.12	2N3792	0.11
OC77	0.55	1N4009	0.08	2N3703	0.12
OC81	0.28	1N4148	0.06	2N3704	0.14
OC81D	0.28	18921	0.07	2N3705	0.12
OC81Z	0.45	18Z033	0.20	2N3706	0.10
OC83	0.25	18Z051A	0.10	2N3707	0.13
OC84	0.65	18Z00A	0.20	2N3708	0.07
OC170	0.25	18Z010	0.25	2N3709	0.10
OC171	0.20	2N696	0.16	2N3710	0.11
OC200	0.55	2N697	0.15	2N3711	0.11
OC201	0.80	2N706	0.10	2N3819	0.85
OC202	0.90	2N706A	0.12	2N3820	0.80
OC203	0.55	2N1305	0.25	2N3923	0.50
OC210	0.25	2N1301	0.25	2N3933	0.15
OC211	0.20	2N1302	0.25	2N3933	0.15
OC212	0.55	2N1302	0.18	2N3904	0.20
OC213	0.45	2N1303	0.18	2N3905	0.25
OC214	0.20	2N1304	0.22	2N3906	0.16
OC215	0.29	2N1305	0.22	2N4058	0.15
OC216	0.25	2N1306	0.25	2N4059	0.10



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THE Firm for speakers!

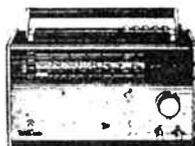
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Celestion MF1000, 8 or 15 ohm	£10.45
Celestion HF1300, Mk II	£6.16
Celestion G12M, 8 or 15 ohm	£12.00
Celestion G12H, 8 or 15 ohm	£15.00
Celestion G15C, 8 or 15 ohm	£24.00
Celestion G18C, 8 or 15 ohm	£33.00
EMI 13 x 8, 3, 8 or 15 ohm	£2.15
EMI 13 x 8 d/c, 3, 8 or 15 ohm	£2.35
EMI 13 x 8 t/w, 3, 8 or 15 ohm	£3.60
EMI 13 x 8 type 350, 8 ohm	£8.25
EMI 8 x 5, cer. mag., 8 ohm	£1.65
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Elac 9 x 5, 59RM109 15 ohm, 59RM114 8 ohm	£2.65
Elac 6 1/2" d/c roll surr., 8 ohm	£3.35
Elac 6 1/2" d/c cone, 8 ohm	£2.65
Elac Tweeter TW4 4"	£1.21
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Fane Pop 60 watt 15"	£13.00
Fane Pop 50 watt 12"	£11.00
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Fane Pop 15 watt 12"	£4.40
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Fane Crescendo 15	£36.00
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Goodmans 12P-G 8 or 15 ohm	£14.50
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Goodmans Axent 100	£6.60
Goodmans Axiom 401	£15.10
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Goodmans Twinaxiom 10, 8 or 15 ohm	£7.61
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Kef T15	£5.75
Kef B110	£6.75
Kef B200	£7.50
Kef B139	£11.75
Kef DN8	£1.92
Kef DN12	£4.12
Kef DN13	£2.75
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WMT1 speaker match. trans. 3-15 ohm	£1.10
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7" x 4" 3, 8 or 15 ohm	£1.38
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Attractive plastic instrument cases in 4 sizes. P1 80 x 50 x 30mm 60p (25p). P2 115 x 65 x 40mm 87p (30p). P3 155 x 90 x 50mm £1.20 (35p). P4 210 x 125 x 70mm £1.80 (45p).

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LEARNING BY PRACTICAL PROJECT STEPS

PART 6—GROUNDED EMITTER AMPLIFIERS

LAST month's emitter followers were all types of current amplifiers. In every case the output voltage was the same, or slightly less than the input voltage. Many applications require voltage amplification—e.g. raising the output level of a microphone to an extent that when current amplification is applied the resultant signal could drive a loudspeaker. The grounded emitter amplifier will provide a reasonable degree of voltage and current amplification and is, perhaps, the most used type of amplifier stage in the whole of electronics. Because both voltage and current is amplified we call the grounded emitter stage a *power amplifier* but not necessarily in the sense that you can expect several watts of useful output; specialised power stages are better equipped for the latter purpose and these will be covered later in the series.

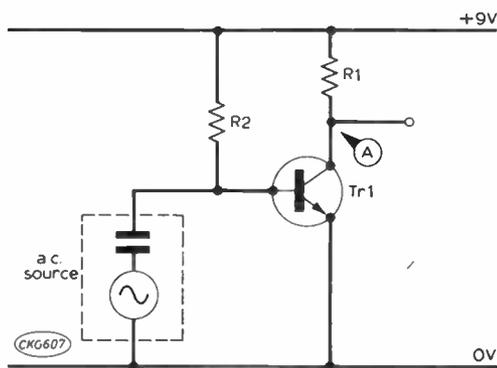


Fig. 42: It is difficult to predict a value for R2 to set the potential at A to mid-rail unless the h_{FE} for Tr1 is accurately known.

Referring to Fig. 42, we know that we can make the voltage at point A go to +9V by ensuring that the transistor is cut off (i.e. by passing zero base current) and conversely we can make it fall to zero volts by passing a certain amount of base current through R2. By knowing an accurate value of h_{FE} for the transistor we could calculate a value for R2 that will cause just sufficient collector current to flow that the voltage drop across R1 will be 4.5V. Theoretically we could hold the voltage at A exactly

mid-way between the two supply rails. At the same time we could connect a source of voltage through a capacitor to the base of the same transistor and (assuming the source voltage was zero at the time) this would not affect our bias condition. However, as soon as we begin to generate a voltage from the source this would cause current to be added or subtracted from the bias current (depending on the polarity of the a.c. signal) and would cause the voltage at A to rise and fall in exact relation—except for the 180° change of phase. Having point A biased “mid rail” allows maximum peak swings of voltage without the transistor clipping (going totally out of conduction) or bottoming (going into saturated conduction) unsymmetrically. In the ideal amplifier the voltage seen at A should faithfully represent that from the source.

In practice the method of obtaining this mid-rail bias shown in Fig. 42 is not very satisfactory because the h_{FE} for the transistor must be accurately known and this can vary widely from one device to another (even though they may be of the same type number).

Base current

A simple way of compensating for this device variation is to use the potential at A as the voltage source for providing the base current—shown in Fig. 43. If the potential at A is too high the base current will be increased, hence the collector potential falls; conversely if A tends to be too low the base current decreases and the potential at A is forced to rise. By careful selection of component values this feedback bias circuit caters well for quite wide variations in the gains of transistors. It is not perfect by any means but is an improved way of getting a mid rail voltage reliably. You can make up the circuit of Fig. 43 on T Dec and try different BC108 devices. The voltage you measure should not fall outside the range of +3.5 to +5.5V. For those interested it is quite easy to arrive at the component values. First of all assume that the collector load is to be 1k Ω . For the potential at A to be +4.5V (assuming a 9V supply) the drop of 4.5V across R1 will be caused by a collector current of

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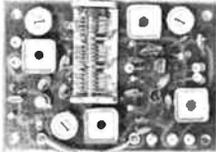
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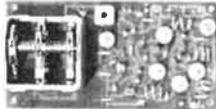
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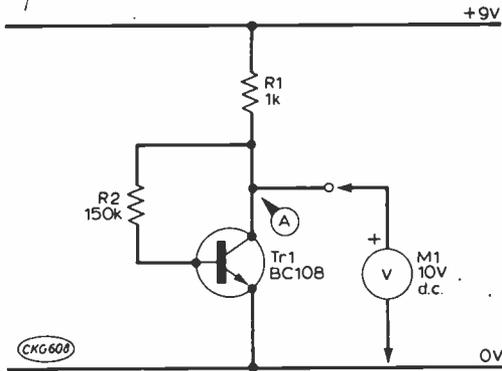


Fig. 43: Using the potential at A as the driving source for base current helps compensate for variations in h_{FE} .

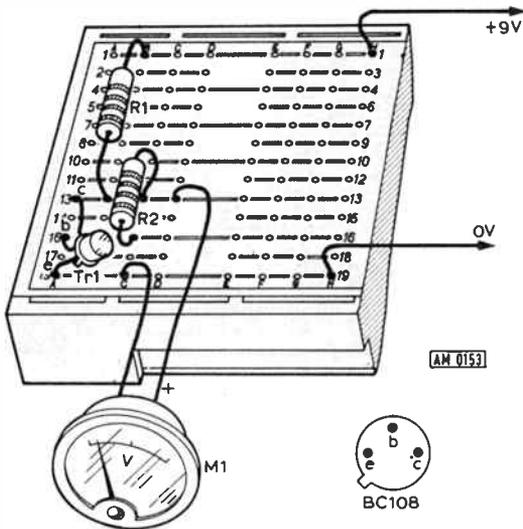


Fig. 44: Component layout for Fig. 43.

4.5mA. If we expect an h_{FE} of around 200 for the BC108 this means that the base current needed to cause 4.5mA collector current is $4.5/200 = 0.0225\text{mA}$. The value of R2, to give this current is calculated from the potential difference across it (potential at A minus the 0.6V base emitter drop) divided by the base current $3.9/0.0225\text{k}\Omega = 170\text{k}\Omega$. The small base current drawn will theoretically modify our original assumption of the potential at A but is so small that it can be ignored. Strictly speaking we should have shown R2 as having a value of 170k Ω but because of other experiments to follow we have made it 150k Ω . The effect of this is to cause the quiescent voltage to be slightly less than mid-rail—but near enough for the experiment.

A crystal microphone is a very easily obtainable source of a.c. voltage that is of a capacitive nature and this can be connected straight across the base of Tr1 and ground of our circuit without affecting the bias conditions (see Fig. 45). Note that we have split the value of our original R2 between two resistors (R2 and R3) in series. Initially leave out the capacitor C1 and connect a meter set to a low a.c. range through a capacitor to point A. Most modern

test meters have this capacitor built into them if you use the input socket marked "Output". The capacitor is there so that the meter only responds to a.c. components on top of the d.c. quiescent voltage at A. Whistle loudly into the microphone and you should see a slight movement of the meter (probably 1V maximum).

Remember, though, that the output from the microphone is unlikely to be greater than a few tens of millivolts. Clearly there is some form of voltage amplification. If you think about it, though, the a.c. fluctuations at A are being fed back, out of phase, to the base through resistors R2 and R3. This will negate the input signal and the overall gain of the amplifier is going to be considerably impaired. We can, however prevent the a.c. component of the feedback signal reaching the base by connecting a capacitor from the junction of R2 and R3 to ground. Do this while whistling into the microphone and you should see at least a two to one improvement in amplification. We call C1 a decoupling capacitor and it should be of a high enough capacitance to shunt even the lowest frequencies to ground.

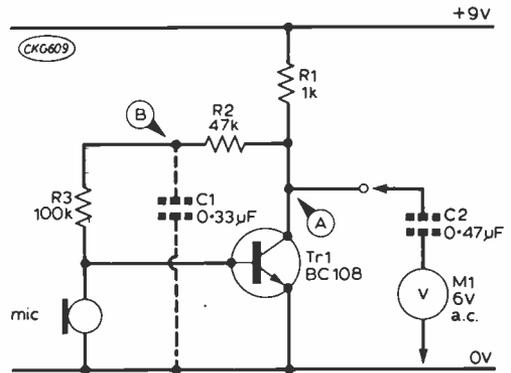


Fig. 45: A signal from a crystal microphone can be superimposed on the bias current but the components have to be slightly modified. Use a meter with an "Output" connection switched to a.c. or alternatively insert C2 when using an a.c. voltmeter.

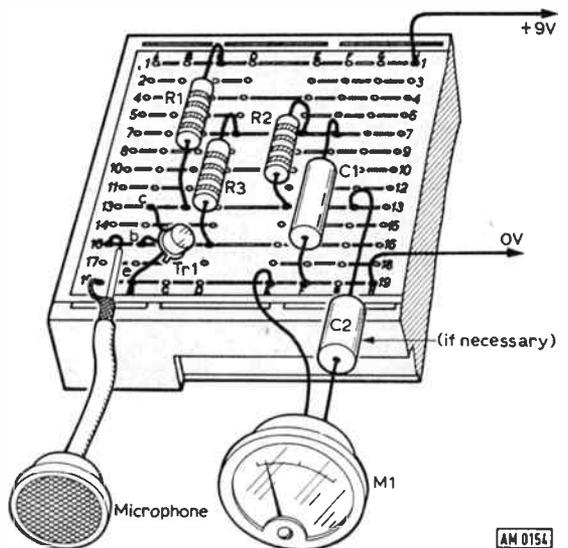
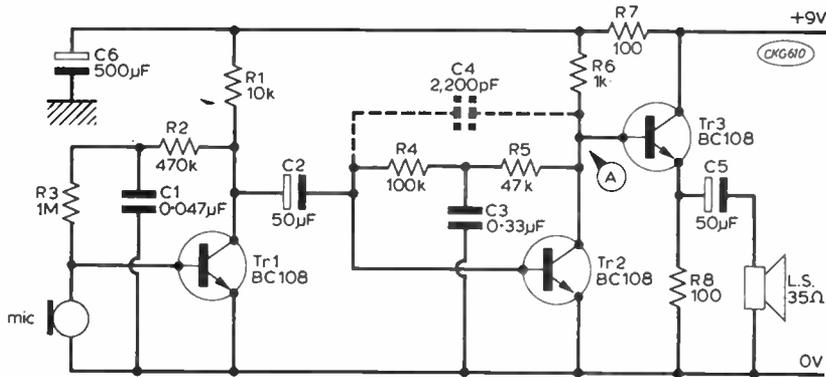
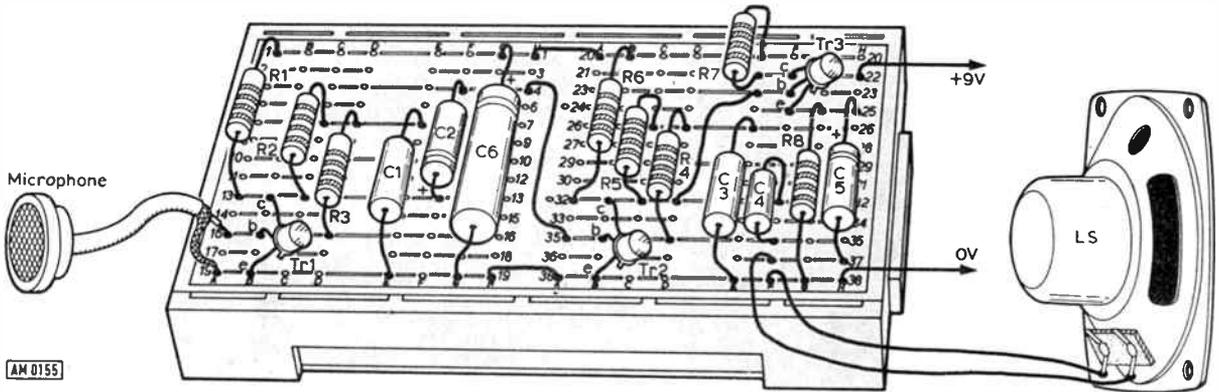


Fig. 46: Component layout for Fig. 45.



◀ Fig. 47: A basic amplifier capable of driving a small loudspeaker from a crystal microphone and suitable for an intercom or baby alarm.

Fig. 48: Component layout for Fig. 47.



AM 0155

The output current from a crystal microphone is very small—because of its high impedance—particularly at low frequencies but there must be quite a reasonable current generated between collector and emitter of the transistor to give rise to the voltage swings we can see at point A. Thus the transistor can be seen to give both current and voltage amplification. The component values in Fig. 45 are not really ideal for coupling from a crystal microphone because we require a fair amount of a.c. base current from the source, and as mentioned earlier, there is not much of this available at low frequencies. The low frequency response of this amplifier would therefore be pretty poor. We can, however, use exactly the same approach to make a stage that needs only one tenth of the input current by increasing all our resistance values by factors of ten (the first stage of Fig. 47. The output from the collector of Tr1 is now coupled as an a.c. signal source to the base of Tr2 which, excluding C4, is identical to the stage we have just described. Before connecting C4 or Tr3 measure the a.c. signal at point A exactly as before; you should see a really high voltage swing (getting on for three or four volts) and more than that, you can get a useful reading for ordinary speech a few inches away from the microphone.

The circuit is clearly providing more voltage gain and has a more useful response at the lower frequency of the human voice. Obviously by increasing the gain at low frequencies we must be overdoing it at high frequencies therefore we insert capacitor C4 which is used, deliberately, to feedback signal from the collector of Tr2 to its base. Because it has a low value it will provide more negative feedback

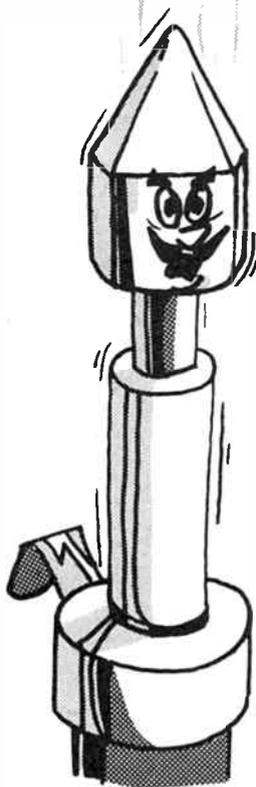
at high frequencies than at low frequencies and hence helps to linearise the frequency response of the two stage amplifier. Use the "whistle and speech" test to see that the amplitude for the whistle is reduced but the level for normal speech has not been appreciably affected. Because we now have a useful voltage swing at A for speech we can use a current amplifier (an emitter follower) to give sufficient current at that voltage to drive a loudspeaker. This is provided by Tr3.

Note that it is necessary to decouple the power rail between the output stage and the amplifiers by means of R7 and C6. Without these components the current drawn by the output transistor could cause voltage variations on the line which are then seen as a form of signal by the preceding stages and amplified. This leads to instability and the whole circuit would oscillate wildly.

The amplifier of Fig. 47 does not have a particularly good frequency response but is quite adequate for intercom or baby alarm applications. No volume control is provided and in some circumstances you might encounter acoustic feedback (howl-round). This can be prevented by keeping the microphone and the loudspeaker well apart.

A problem with the circuits we have covered, so far, is that the voltage gain is very much dependent on the h_{FE} of the transistor in question. There are other circuits which—at the expense of a little gain—enable us to get what there is under reasonably accurate control.

To be continued



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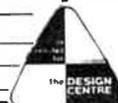
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IMPEDANCE MATCHING



THE WHYS AND WHEREFORES

C. BUDD

THE concepts of input impedance and output impedance are not really difficult to understand although there is no single rule to cover every situation. What is correct practice depends almost entirely on the individual design requirements.

The most important rule of impedance matching is derived from the maximum power transfer theorem.

The maximum power transfer theorem

If a signal source with a purely resistive output source is required to drive a purely resistive load, maximum power will be transferred from source to load when the load resistance is equal to the output impedance of the source. It should be noted that the theorem assumes that the input and output impedances to be purely resistive, which will rarely be the case in practice, and that to deliver maximum power to the load is the sole requirement.

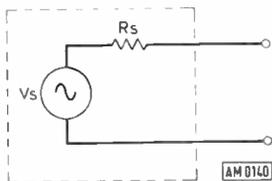


Fig. 1: Equivalent circuit of signal source with resistive output impedance.

Fig. 2: Equivalent circuit of resistive load.

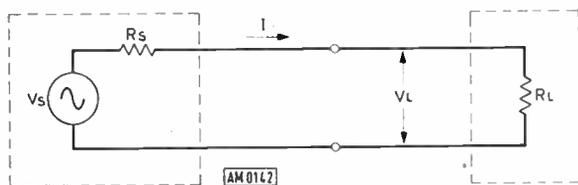
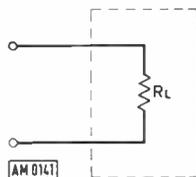


Fig. 3: Equivalent circuit of the source of Fig. 1 driving the load of Fig. 2.

Assuming that our signal source may be represented by an a.c. voltage source in series with a resistance (Fig. 1) and that our load may be represented by a pure resistance (Fig. 2), we can combine the two (Fig. 3) and write some pertinent equations as follows.

Calling the power delivered to the load P

$$V_L = \frac{V_S R_L}{R_L + R_S} \text{ by potential divider action}$$

and $I = \frac{V_S}{R_L + R_S}$ where I is the a.c. current flowing

$$P = IV_L$$

$$\therefore P = \frac{V_S^2 R_L}{(R_L + R_S)^2}$$

where V_L = load voltage, V_S = source voltage, R_L = load resistance, and R_S = source resistance.

Given the source voltage and the source and load resistances we can, with this formula, calculate the power delivered to the load. But we can do more than that. If we assume arbitrary values for V_S and R_S we can plot a graph of R_L against P. The curve obtained will be similar to that in Fig. 4. From the graph it may be seen that the power transferred is at maximum at approximately the point where R_L equals R_S . It may be shown that P reaches a maximum when R_L is exactly equal to R_S .

Maximum power transfer between source and load occurs when the source resistance is equal to the load resistance.

Other considerations

In practice, however, it is not as straightforward as this because maximum power transfer may not be our only concern. Consider the simple audio output stage shown in Fig. 5. The purpose if T1 is to match the speaker impedance to the output impedance presented by the transistor.

From the maximum power transfer theorem, one could reasonably assume the the "correct" load resistance would be the output resistance of the transistor, but this is not so. In this case maximum

efficiency (i.e. power transfer from amplifier to load) is not our main concern.

Of greater importance is the maximum power that the stage will deliver without distortion due to bottoming (the transistor being turned off by the input signal) or saturation. In fact the load resistance into which the stage will deliver the maximum power without distortion, known as the optimum load, is equal to the supply voltage divided by the quiescent collector current and has nothing to do with the actual output resistance of the stage.

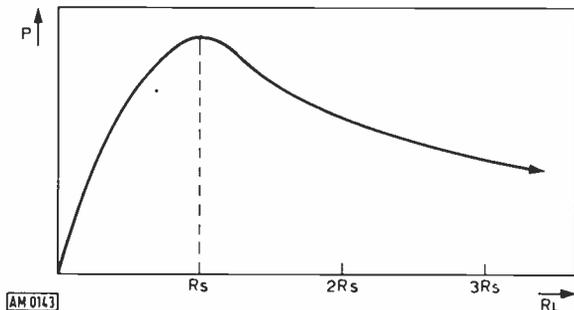


Fig. 4: Sketch graph showing that the power delivered to the load is at a maximum when $R_L = R_s$.

In a practical case the optimum load will generally be higher than the output resistance for an audio power amplifier, and this is the reason that commercial audio power amplifiers, intended to drive load impedances of 3, 8 or 16 ohms, often have output impedances of a fraction of an ohm.

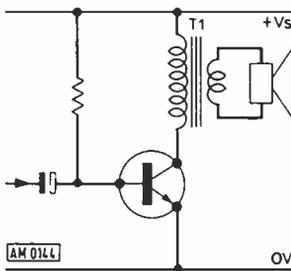


Fig. 5: Simple audio output stage.

Reactive components

An input or output impedance will have reactive components as well as a resistive one. If possible, the reactive element of the source impedance should be cancelled by those of the load impedance. In other words, a source with an equivalent series capacitance should "see" a load with an equivalent series inductance, the reactance being equal, but opposite, to that of the source capacitance.

In this way, the source capacitance and the load inductance form a series-tuned circuit which, ideally, has zero dynamic impedance (zero resistance). Any net reactance in the source-load circuit is undesirable since it reduces the maximum power that can be delivered to the load by the source. Such "reactance balancing" is only possible at a single frequency and in a system of large relative bandwidth (e.g. an audio preamplifier) it is of no use.

At r.f. however, the relative bandwidth will generally be much less and it is usually easy to make the reactive elements of source and load cancel out in the frequency band in use. As an example, one of the functions of the aerial tuning unit in a transmitting system is to cancel out the reactive elements of the aerial impedance.

Equal load and source resistance

Now let us consider another situation in which it would be better to deviate from the rule of making the load resistance equal to the source resistance because maximum power transfer is not our only concern. Fig. 6 shows the equivalent circuit diagram of a typical crystal microphone or ceramic pick-up. The output impedance of such a device consists of a fairly large resistance (typically a few megohms) in series with a small capacitance of perhaps two or three hundred picofarads. If the capacitive element was absent, the transducer drives a pre-amp with an input resistance equal to R_s and all would be well.

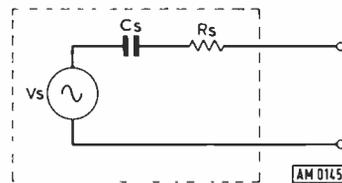


Fig. 6: Equivalent circuit of typical crystal microphone or ceramic pick-up.

However, at the lower audio frequencies, the reactance of C_s in a practical transducer becomes large enough to be significant in comparison to R_s and attenuation of the bass frequencies would result if the input impedance of the pre-amp were equal to R_s .

Since an inductance in series with the transducer would only cancel the capacitance at a single frequency and would, in any case be ridiculously large, the simplest solution to the problem is to make the input impedance of the pre-amp very large compared to R_s . The reactance of C_s at bass frequencies would then be insignificant compared to the total resistance in circuit and no significant attenuation of the bass frequencies would occur.

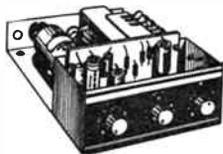
High impedance input

The circuit diagram of a crystal microphone driving a pre-amp with an ample input resistance of $10M\Omega$ is shown in Fig. 7. One could reasonably think, from the maximum power transfer theorem, that the large ratio between the resistive component of the source impedance and the load resistance would result in a large loss of available power.

This is the case, but it may be shown that the power gain of a common source f.e.t. stage (and that of a common cathode valve stage) is proportional to the value of the resistor (R_1 in Fig. 7) shunting the input, which is roughly equal to the

—continued on page 1166

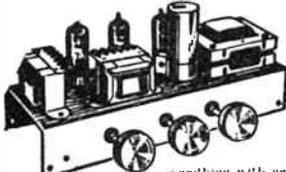
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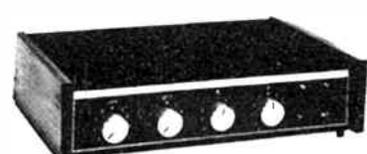
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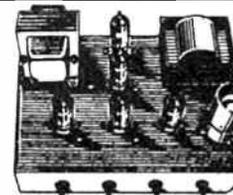
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AUTOMATIC 12V CAR BATTERY CHARGER

Richard Collin

THIS simple automatic battery charger was originally designed for use with the very popular battery operated fluorescent lamp described in the December issue of *Practical Wireless*. Its purpose was to keep the battery in a fully charged state, restoring energy used when mains power is available.

The circuit is of course suitable for charging any 12 volt car battery at a maximum rate of 2.25A. When the battery reaches full charge (13.5 volts) a "crowbar" circuit operates and shuts off the charge current. Interruption of the mains supply restores the crowbar to its off state.

Circuit description

The circuit diagram is shown in Fig. 1. A mains isolation transformer with a 30V centre-tapped secondary winding feeds a full-wave thyristor circuit to provide the charging current. The thyristors are triggered by the d.c. potential applied to the gate electrodes via diodes D1 and D2 and the associated smoothing capacitor C1.

Resistors R1, R2 and R3 limit the gate current together with the indicator lamp LP2. Resistor R1 and lamp LP2 also limit the current through the crowbar thyristor CSR3 when it is 'on'. Resistors

R4 and R5 are connected in parallel. They limit the charge current to 2.25A to protect the transformer, CSR1 and CSR2. Diode D3 is included to stop current flowing back from the fully charged battery into the crowbar circuit once it has triggered.

The crowbar trigger potential is set by the 6.8V zener diode D4 in the gate circuit of CSR3. By using the potentiometer across the circuit output it is possible to adjust the voltage of the output to a pre-determined level at which the crowbar circuit 'fires'. The crowbar thyristor 'shorts' the main gates to earth and stops them from receiving gate pulses, so stopping conduction.

★ components list

R1	68Ω 5W wirewound resistor
R2, R3	270Ω ½W
R4, R5	1Ω 10W wirewound
R6	1.2kΩ ½W
R7	330Ω ½W
VR1	2.2k potentiometer (miniature preset)
C1	640μF 25V
LP1	Mains neon indicator
LP2	6.3V 0.2A lamp
S1	Single pole, single throw toggle
FS1	3A fuse
T1	Mains transformer, secondary 30V centre tapped, 3A
CSR1	2N3228 TO-66 or any 50V 5A thyristor, and mounting hardware
CSR2	2N3228 TO-66 or any 50V 5A thyristor, and mounting hardware
CSR3	TIC44
D1	1N4001
D2	1N4001
D3	1N1612R or any 50V 5A stud type (stud is anode) and mounting hardware
D4	6.8V 1 watt zener diode

Lamp holder (m.e.s.), connecting wire, mains lead, fuseholder, nuts, bolts, etc. Heatsinks (see Fig. 3.)

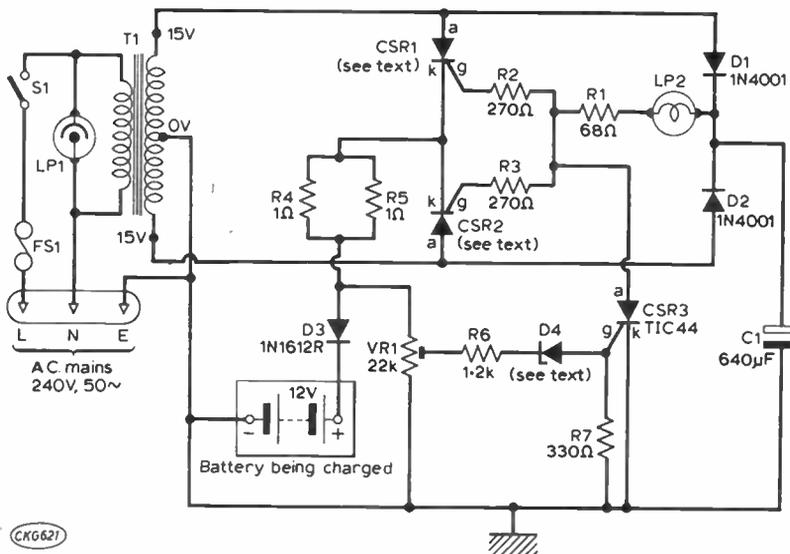


Fig. 1: Schematic circuit of the automatic battery charger.

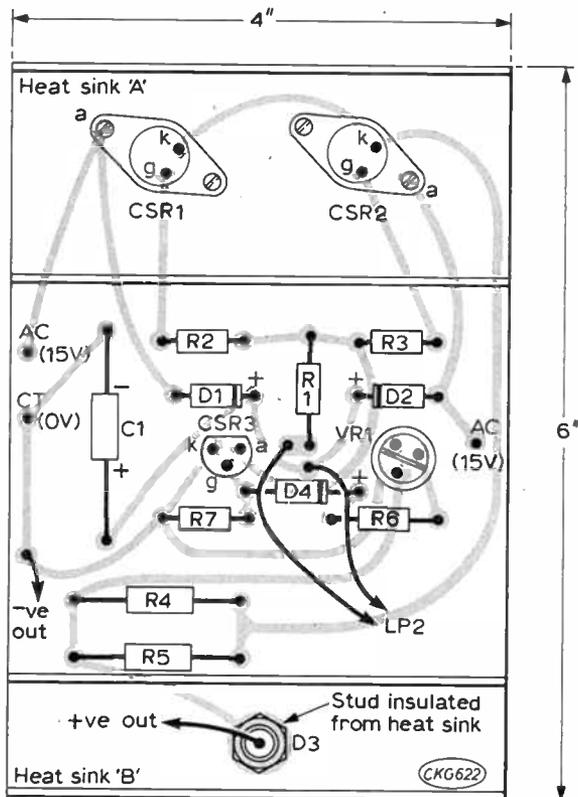


Fig. 2: Printed circuit board and component layout.

The circuit board layout is shown in Fig. 2. All components should be mounted onto the board and soldered up. Ensure that electrolytic C1 is connected correctly and check also the polarity of the thyristor and diode connections. The main thyristors, CSR1 and CSR2 and diode D3 must be mounted with insulators on their respective heatsinks. A smear of silicon grease should be applied to each side of the mica washers to ensure good thermal contact. Resistors R4 and R5 should be spaced clear of the board as they will run quite warm.

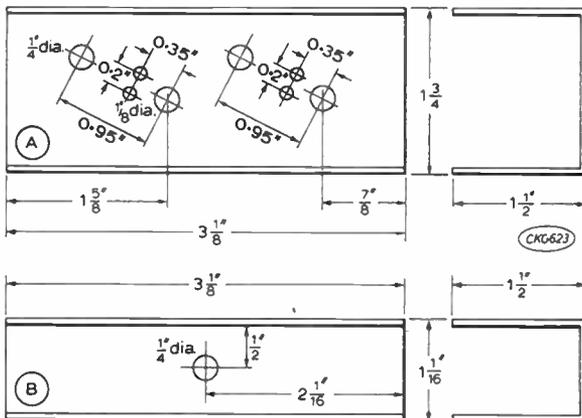


Fig. 3: Heat sink details, in 16 s.w.g. aluminium.

When the board is complete and all wires to the transformer are connected make a final wiring check. Then set VR1 fully anticlockwise, and switch on the mains. Measure the voltage across C1; it should be approximately 20V.

Then connect a fully charged 12V battery (about 13.4V off load) across the output terminals. Advance VR1 slowly until the crowbar circuit just operates (lamp LP2 comes 'on'). The voltage measured between earth and R4, R5 and D3 junction should then be about 14V. Do not move the setting of VR1 again—sealing with a dab of glue is a good safeguard. Switch off the unit and disconnect the battery.

Connect a discharged battery to the unit and switch on. If an ammeter is available check the charge rate—about 2.25A. Alternatively measure the voltage across R4, R5; this should be about 1.1V. The crowbar circuit should not operate until the battery is fully charged and reaches 13.4V. Once operated the crowbar cannot be reset unless the mains supply is interrupted.

During power cuts this will be "automatically" accomplished. ■

IMPEDANCE MATCHING—continued from page 1162

input impedance of the stage. Thus, a high input impedance makes for higher power gain and, hence, greater output power from the stage as well as improving the bass response, as it does in this particular application.

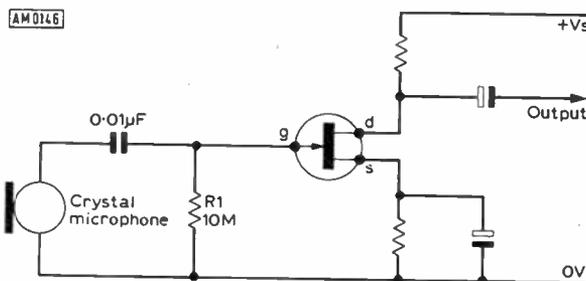


Fig. 7: A crystal microphone driving an audio preamp with a high input impedance.

Power fall-off

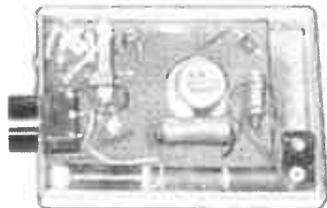
There are many such situations in which maximum transfer of power from source to load is not our only concern and load resistance should not be made equal to source output resistance. But the basic principles should be borne in mind. The maximum possible power will be delivered to the load when the input resistance of the load is equal to the output resistance of the source and any reactive components in the source impedance should be cancelled out by equal but opposite reactive elements in the load impedance.

In many practical cases exact equality of source and load resistances is not easy to achieve. It may be seen from Fig. 1 that the power transfer falls off more rapidly with decreasing load resistance than it does with increasing load resistance. Therefore, if it is necessary for a mismatch to occur, it is clearly much better to make the load resistance greater than the source resistance. ■

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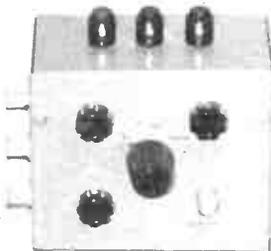
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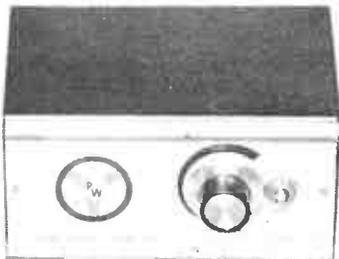
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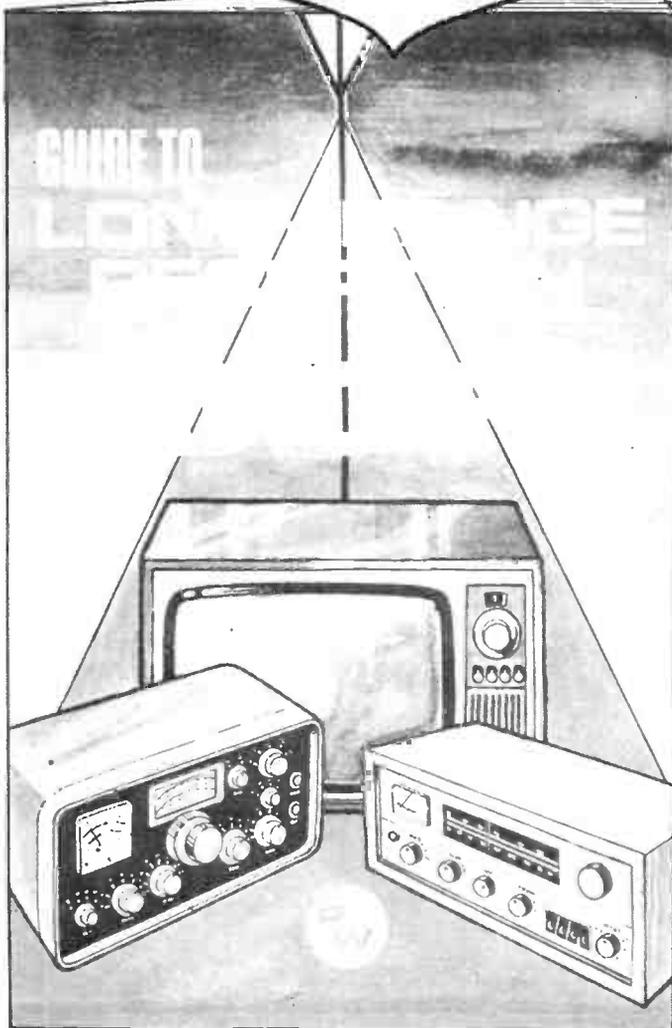
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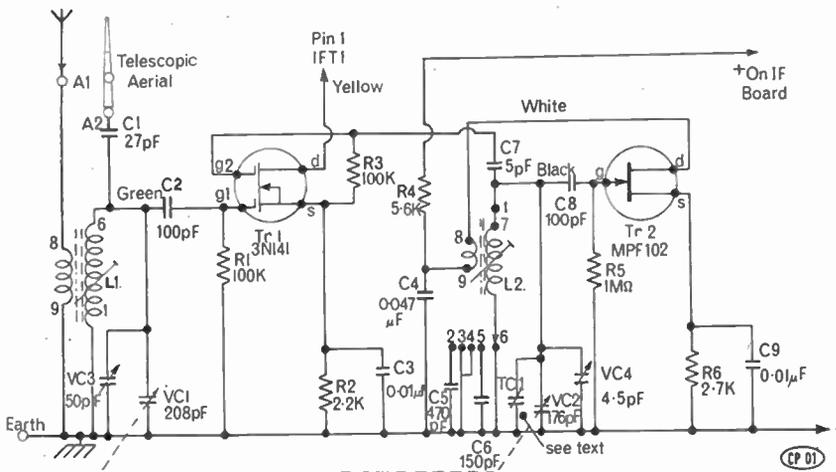


Fig. 1. First part of the circuit of the Slimline receiver. This contains the mixer stage Tr1 and the oscillator Tr2. Padders C5 and C6 are automatically connected into circuit when the appropriate coil L2 is inserted.

Fig. 2. The output from the mixer stage feeds into the first IF transformer IFT1 and amplified by Tr3 and Tr4. The capacitors across the windings are part of the IFT assemblies.

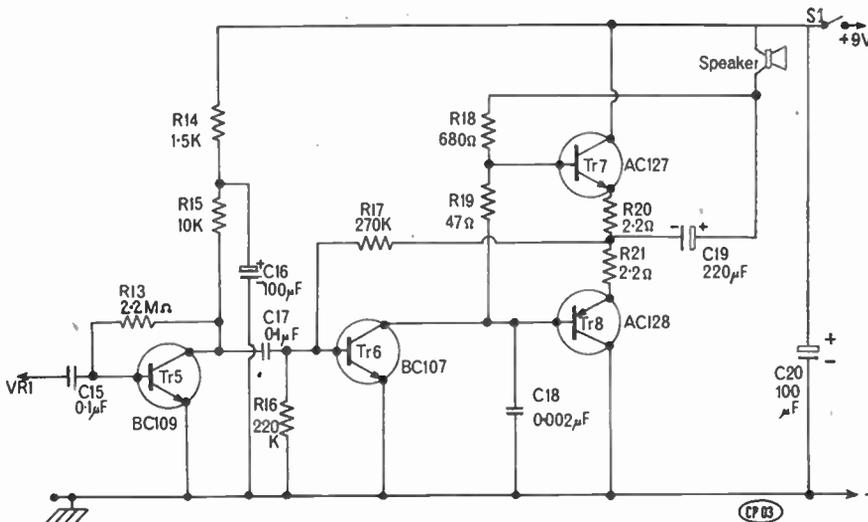
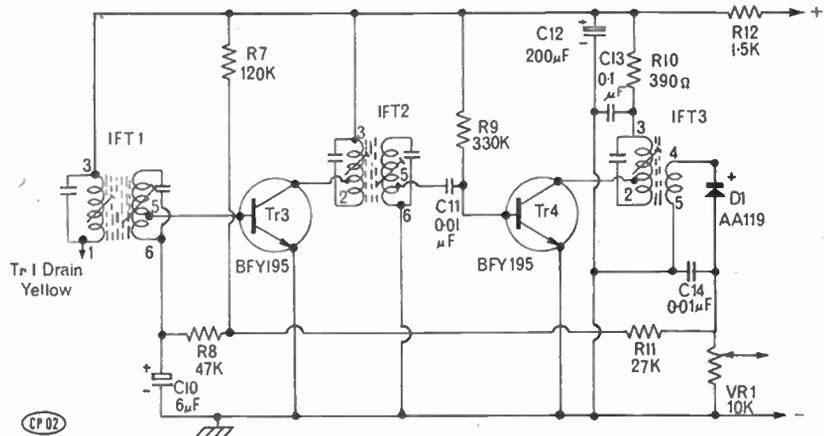


Fig. 3. The audio signal from the detector diode D1 in Fig. 2 is fed via the volume control to Tr5 and further amplified by Tr6, 7 and 8 and thence to the speaker.

Portable Receiver

THIS portable receiver is in a 7×5in. case only 1in. deep, though to these dimensions must be added those of the Trimmer, Fine Tuning and Volume/On-Off controls at one end, and the Band-setting dial on the front. These do not however increase the size very much. The receiver may be operated with its own telescopic rod aerial, with an improved aerial such as a few yards of thin insulated flexible wire or with a conventional aerial.

The coverage of the five bands is approximately as follows:—

Band 1	160—350kHz
„ 2	580—1500kHz
„ 3	1.75—4.0MHz
„ 4	5.9—11.5MHz
„ 5	13—27MHz

The receiver thus has a wide general utility, tuning medium and long waves, if required, in addition to the most popular short wave bands.

Eight transistors and one diode are employed and the receiver is wired and assembled in separate units. A dual-gate 3N141 mixer is used with an MPF102 FET oscillator, followed by two BFY195's and AA119 diode for IF amplification, demodulation and AGC. The audio section has a BC109 pre-amplifier and BC107 driving an AC127 and AC128 complementary output stage, which provides adequate power for the internal speaker.

CIRCUIT DETAILS

The telescopic aerial, or a short wire aerial, is connected to socket A2 Fig. 1, but longer indoor or outdoor aerials are plugged into socket A1, using



F. G. RAYER

the primary coupling winding of the aerial coil L1. This circuit is tuned by VC1 and the panel trimmer VC3 is provided so that this can be peaked for maximum efficiency with any aerial. Signals are taken to gate 1 of Tr1 and gate 2 is coupled by C7 to the oscillator Tr2. The oscillator coil L2 is tuned by the second section of the ganged capacitor VC1/VC2. VC4 is a bandspread tuning control to allow easy tuning on the short wave bands.

L1 and L2 are plug-in coils so there is no need to obtain coils for those bands which are not required. Band 1 is for long wave coverage and may not be wanted in some areas. The extreme high frequency end of this band is not used (above about 350kHz) as instability arises when this stage is tuned near the intermediate frequency, as would be expected.

Band 2 is for medium wave coverage while Band 3 includes shipping and other transmissions, as well as the 160m and 80m amateur bands. Most general short wave broadcasts come in Band 4 and also Band 5.

Capacitors C5 and C6 in Fig. 1 are padders and the correct value is brought into circuit for each coil when it is inserted, by wiring to the appropriate socket pins. TC1 is an integral trimmer on VC2. If VC1/2 is a type without trimmers a separate 30pF or similar small pre-set must be connected here.

Fig. 2 is the circuit of the IF amplifier. IFT1 and IFT2 are double tuned and IFT3 single tuned and these, with the two BFY195's, result in good selectivity and gain. The demodulator diode D1 provides audio signals for the volume control VR1, and automatic gain control bias for the first IF stage. Current for the IF stages is taken from the 9V supply, through R12, the mixer drain circuit being supplied through the primary of IFT1. The on-off switch S1 is incorporated with the volume control VR1.

The circuit of the audio stages is shown in Fig. 3. Tr5 is a low level high gain amplifier with output to the driver Tr6 which drives the NPN/PNP pair Tr7 and Tr8, R17 providing stabilisation of the DC operating conditions. The circuit is intended for an 18 ohm speaker but it will be found that good results are obtained with a 25 ohm or 35 ohm unit.

CONSTRUCTION

Both sides of the mixer/oscillator board are shown in Fig. 4. Plain perforated Veroboard is most suitable, with 0.15in matrix. The resistors and capacitors are inserted as shown and the board turned over and leads soldered underneath. In most places the wire ends of the components are long enough to reach other points. Soldered joints should be small and leads kept near the board, with sleeving on leads which may touch each other. The tag MC is later secured with a 6BA or 8BA bolt, to hold the board clear of the panel and to form a negative or earth return.

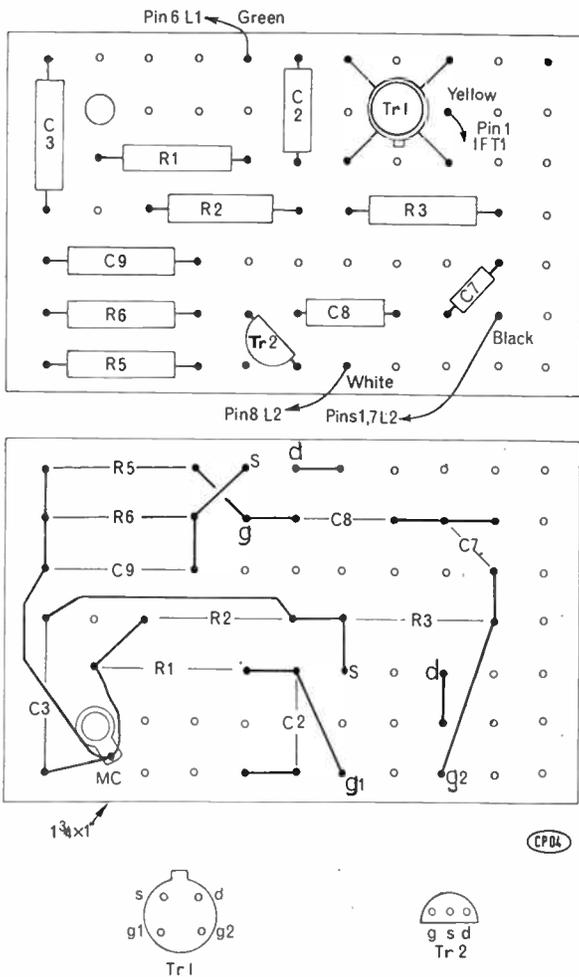


Fig. 4. Layout of the mixer/oscillator board. Veroboard pins can be used where necessary, if component leads are too short.

Important. An insulated gate transistor of the 3N141 type has an extremely high gate internal resistance and it can be destroyed by the static charge of metal or plastic tools, or by touching its leads with the fingers. Despite this, there is virtually no danger to the transistor if it is installed correctly and once R1, R2 and R3 are connected to it, these protect the gate circuits from static charges.

Leave Tr1 until other wiring on this board is finished. Tr1, as supplied, should have a thin spring or loop which short circuits its four leads, to protect it. This is not removed until the transistor is soldered in place. If it has to be unsoldered for any reason, a length of thin, clean wire should be wound round the four leads, under the transistor, before this is done. Spread the leads with a matchstick so that they come through the holes shown in Fig. 4, bend over the wires from R1, R2 and R3, and solder them to the transistor leads.

It is convenient to use colour coded leads for the external connections. These may be green from C2 for VC1 and pin 6 of L1, yellow for the drain circuit, white from Tr2 drain to pin 8 of L2 and black for VC2 and pins 1 and 7 of the holder for L2.

The IF board is shown in Fig. 5. Holes for the IFT pins and screening can tags should be drilled first. The pins are identified by their spacing, and should be arranged as in Fig. 5. A very small round file may

be useful in adjusting the positions of holes, if drilling is not quite correct, so that the IFTs fit without strain on their pins. Holes should also be drilled so that the cores can be reached. Two small tags are secured with the bolts MC, which also fix two angle brackets in place. These brackets allow the board to be fixed to the receiver panel.

Note the polarity of C10, C12 and D1. Proceed with the wiring as for the mixer-oscillator board, with insulated sleeving where required. The wire ends of R12 and C14 can be left projecting, so that other connections can be soldered on later.

The AF amplifier board is built in a similar manner, components being positioned as in Fig. 6. As it is rather difficult to see the transistor lead positions when these are in place, short pieces of coloured sleeving may be put on these wires first, to identify them—green for emitter, blue for base and orange for collector.

Capacitors C16 and C20 are arranged vertically. Bolts secure the tags MC and small brackets, as with the IF board. If necessary, these brackets can be cut from a small spare section of flanged universal

★ components list

Resistors

R1 100kΩ	R8 47kΩ	R15 10kΩ
R2 2.2kΩ	R9 330kΩ	R16 220kΩ
R3 100kΩ	R10 390Ω	R17 270kΩ
R4 5.6kΩ	R11 27kΩ	R18 680Ω
R5 1MΩ	R12 1.5kΩ	R19 47Ω
R6 2.7kΩ	R13 2.2MΩ	R20 2.2Ω
R7 120kΩ	R14 1.5kΩ	R21 2.2Ω

All resistors 5% $\frac{1}{4}$ watt

VR1 10kΩ log. pot. with switch S1

Capacitors

C1 27pF	C8 100pF	C15 0.1μF
C2 100pF	C9 0.01μF	C16 100μF 10V
C3 0.01μF	C10 6μF 4V	C17 0.1μF
C4 0.047μF	C11 0.01μF	C18 0.002μF
C5 470pF	C12 200μF 10V	C19 220μF 6.4V
C6 150pF	C13 0.1μF	C20 100μF 10V
C7 5pF	C14 0.01μF	

VC1/2 208—176pF gang (Jackson 00)

VC3 50pF (Jackson C804)

VC4 4.5pF (Jackson C804)

TC1 30pF trimmer, see text

Semiconductors

Tr1 3N141	Tr4 BFY195	Tr7 AC127
Tr2 MPF102	Tr5 BC109	Tr8 AC128
Tr3 BFY195	Tr6 BC107	D1 AA119

Inductors

IFT1/2 IF Transformer (Denco IFT18/465)

IFT3 IF Transformer (Denco IFT14)

L1/2 Plug-in coils, 9 pin miniature valve type for ranges required (Denco—'Blue' for aerial coils and 'Red' for oscillator coils)

Miscellaneous

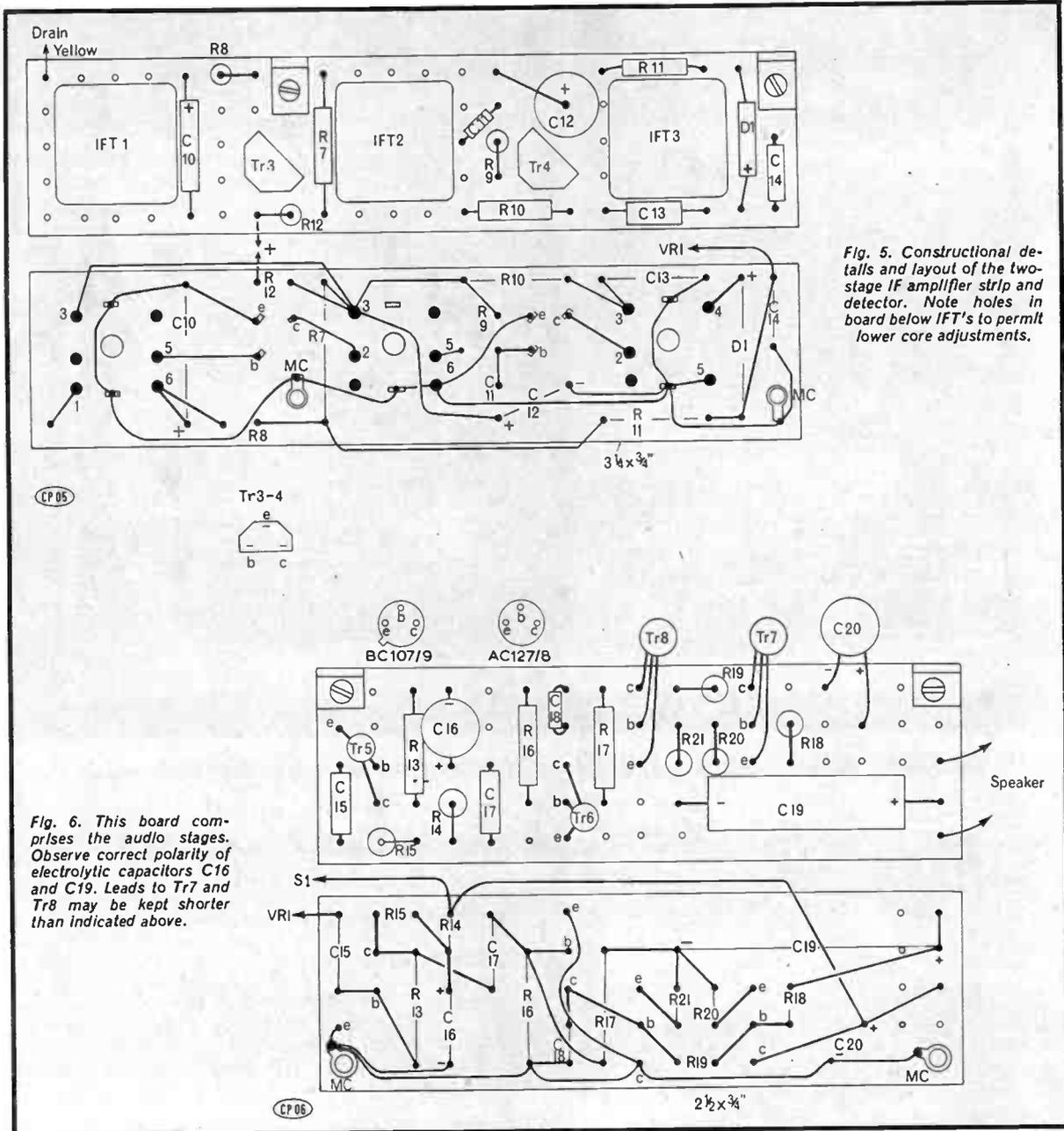
Speaker, about 2½in dia., 18 to 35 ohms. Telescopic aerial. Small sockets (2). B9A valveholders, plain (2). Perforated veroboard 0.15in matrix, 1½ x 1in, 3½ x ¾in and 2½ x ¾in. Knobs (4). Perspex for dial.

Casework Plates 7 x 5in (2) (CU168)

Flanged members 7 x 1in (2) (CU54A)

Flanged members 5 x 1in (2) (CU52A)

All from Home Radio.



chassis, as used later for the coil holders. Both brackets and insulated board are drilled for 8BA bolts.

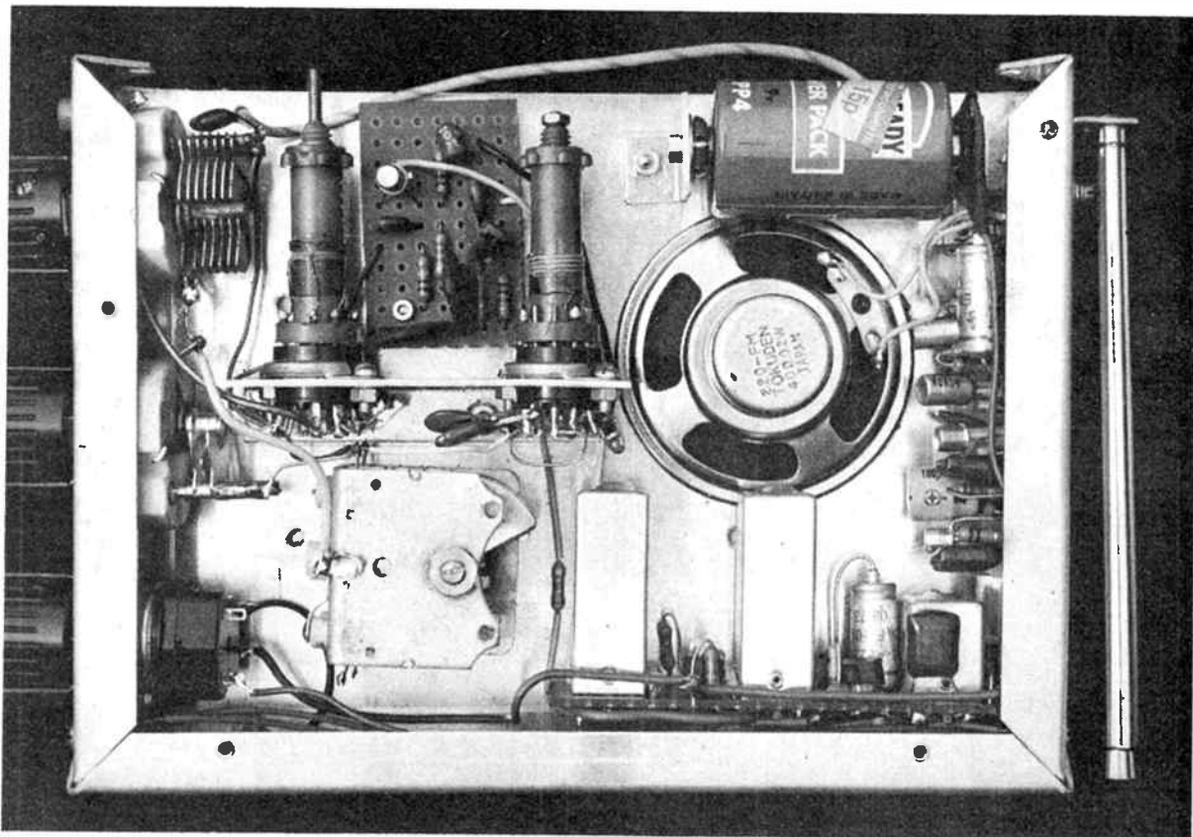
A piece of metal with a flange, for mounting the coil holders, is cut $2\frac{3}{4} \times 1$ in so that the holders can be fitted as in Fig. 7. A small section is cut away near L2 as shown, to allow the speaker to fit.

The flange is bolted 1 in. from the edge of the panel, as in Fig. 8. There is little free space so items should be positioned carefully. The flange is held with 6BA countersunk bolts and nuts. The ganged capacitor is held with three 4BA bolts, which must be cut or filed short so that they do not project beyond the thickness of the capacitor's front plate.

Wiring can then be completed as in the diagrams. The IF, AF and mixer-oscillator boards are held

with 8BA countersunk bolts. The one 5×1 in flanged runner is fixed with bolts or self-tapping screws so that VC3, VC4 and VR1 can be mounted, but the other flanged members are left off until later. Leads between units are run against the metal. The speaker is cemented over a $1\frac{3}{4}$ in diameter hole and the leads soldered to it. Other connections will be seen in Figs. 7 and 8.

The battery is mounted by a bracket, to which a negative snap connector is bolted. This both holds the battery and provides the negative connection. Two small sockets provide A1 and Earth connections. When all wiring is finished, except for the telescopic aerial, the receiver can be aligned. Do not forget to remove the shorting collar or wire from the mixer transistor.



Inside the Slimline receiver. Main components may be identified from Fig. 8.

IF ALIGNMENT

As the IFT's are supplied pre-aligned, the cores should not be touched until reasonable results are being obtained. A properly fitting tool must be used, such as that available from the IFT maker, as a wedge-shaped blade may easily break the cores so that they cannot be rotated. Where a signal

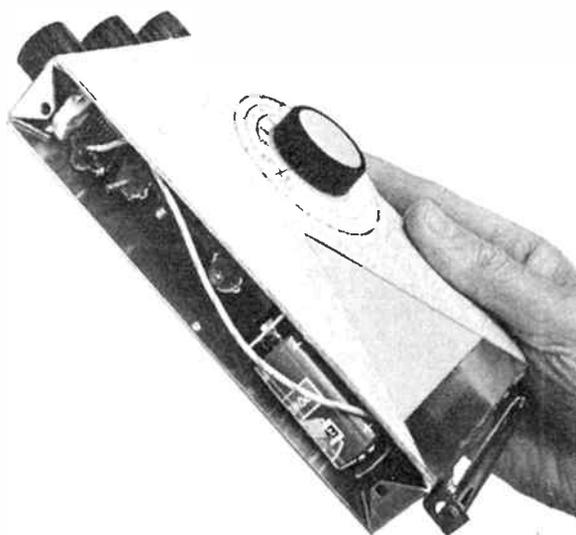
generator is available, place the output lead of this near the yellow lead (mixer drain) and adjust the cores for best output.

If no generator is available turn the audio gain control to near maximum and tune in a weak but stable signal, such as that obtained from a local BBC transmitter, with no aerial at all in use. With this tuned in correctly, adjust the five cores slightly, as may prove to be necessary, for best volume. An alternative is to connect a high resistance test meter across VR1 (positive to chassis) and use a somewhat stronger signal, so that cores can be peaked for the best reading. When these cores have been adjusted, they should be left alone since their settings are not changed when dealing with the mixer and oscillator circuits.

MIXER/OSCILLATOR ALIGNMENT

If VC1/2 has trimmers, open fully the trimmer on VC1 and screw down the trimmer on VC2 and set VC3 and VC4 about half open. Each range is dealt with separately. Suppose that Range 3 is aligned first. Adjust the core of L2 (Red coil) so that band coverage is approximately correct. Then tune in a signal around 3.5 to 4.0MHz and adjust VC3 for best volume. Leave VC3 at this setting and tune to a signal around 1.9MHz. The core of L1 is then adjusted for best results, after which there is little need for much adjustment of VC3, throughout the band. When VC3 is peaked for best results, it should be neither fully closed nor fully open.

The other ranges are dealt with in the same manner. The cores of L2 are adjusted in that



Removal of edge panel permits easy coil changing or replacement of battery.

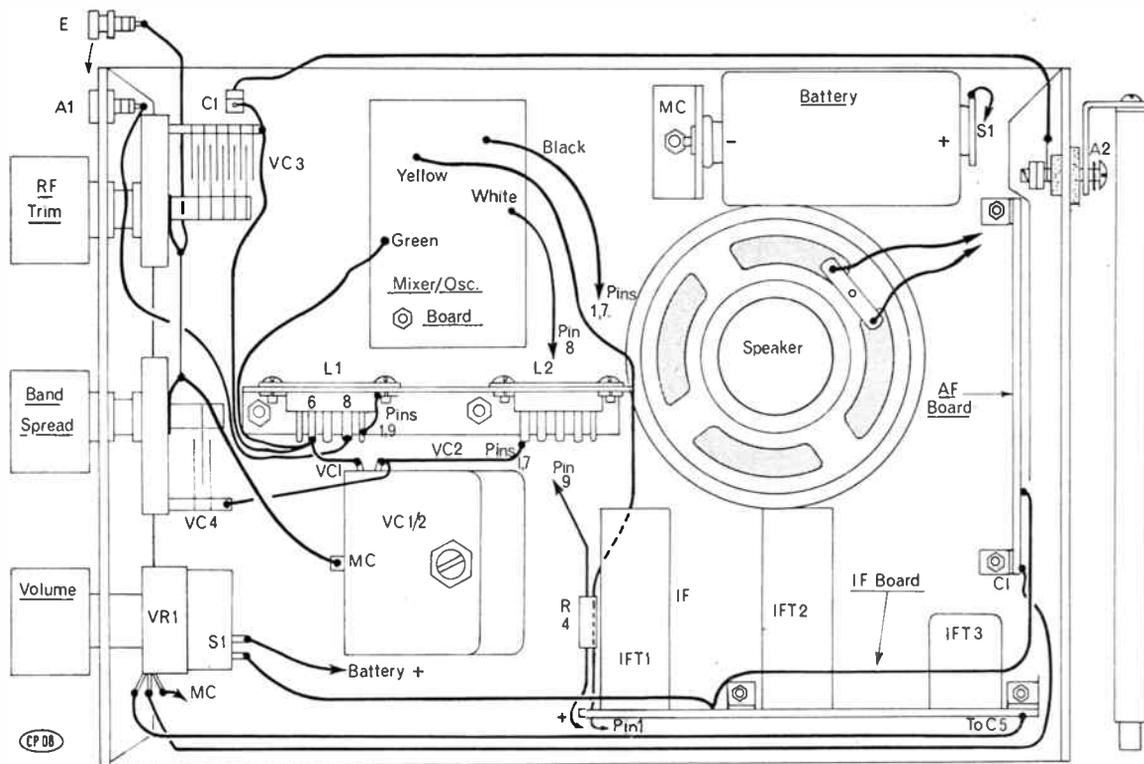


Fig. 8 Location of the three boards and major components. The battery is held in position by the bracket holding the negative clip.

direction which takes them away from the smaller winding for Ranges 1 and 3, otherwise continuous oscillation may prove troublesome at the high frequency end of these bands. This arises from the degree of coupling between L2 and its feedback winding. Should excess oscillation or "squegging" of the oscillator be troublesome, R4 could be increased in value. On the other hand, if Tr2 has somewhat reduced gain the value of R4 could be reduced. However, with the value shown, several MPF102 transistors proved satisfactory, so this should not be necessary.

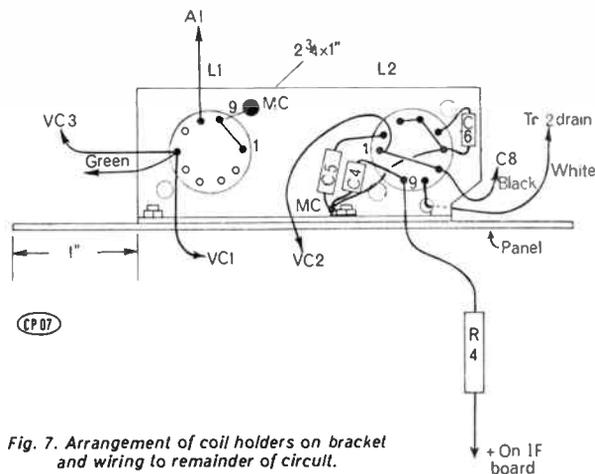


Fig. 7. Arrangement of coil holders on bracket and wiring to remainder of circuit.

FINISHING OFF

The aerial is fixed to a small right angle bracket which is pivoted on a 6BA bolt passing through the side of the case. The hole is drilled to take an insulated bush and an insulated washer rests between the bracket and case. A spring washer is placed under the screw head and the nuts locked together so that the aerial can be extended vertically with the case flat or standing upright. A flexible lead runs from the aerial to C1.

The dial is marked on card and is about 2 3/4 in. in diameter. The control knob is a shallow type to which is attached a 2 3/4 in. diameter disc of 1/16 in. thick Perspex. This can be fixed with adhesive or self-tapping screws. A line is marked across the Perspex. A disc can be easily cut with an adjustable tank or washer cutter, but if this is not available a pointer knob could be substituted for the disc.

The case is completed by screwing on one 7 x 1 in member and the remaining 5 x 1 in member. The 5 x 1 in members fit inside the 7 x 1 in members so that the top 7 x 1 in flanged member can be taken off to change the battery or coils. The back, a 7 x 5 in flat plate, is permanently attached with self-tapping screws, but only one screw is run into the top member flanges.

There is some opportunity for individual choice in the way in which the case is finished. If left bare or painted, gauze or perforated metal should be fitted over the speaker aperture inside. The case shown was covered at the front with fabric and self-adhesive material as used for shelves, boxes, etc.

CASSETTE RECORDER AND TUNER AMPLIFIER



Mount the strip of four output devices onto the circuit board and solder up the connections. Then mount the two driver transistors in a similar fashion. Once soldered ensure that the power transistors are not bent back and forth on their leads—plastic packaged devices can be easily damaged by stressing the lead outs. Once complete the power board should be put away safely until needed later on.

TUNER AND IF CIRCUIT (UNIT 3)

The AM section utilises the Ferranti ZN414 integrated circuit IC1 and a single transistor amplifier Tr1. A small ferrite rod aerial forms part of a double-tuned aerial circuit which is used to eliminate swamping effects of strong local transmissions by improving the selectivity. The circuit and printed board illustrated are for the single-station version. Further channels may be added by inserting a suitable two-pole rotary switch at the points marked "X" and "Y" in Fig. 10 to select additional pairs of trimmer capacitors for each station required.

The ferrite aerial may be insufficient in some areas of poor signal strength. The AM aerial socket, which is loosely coupled to the ferrite rod by two turns of insulated wire, allows adequate reception under such conditions by connection of an external aerial.

In the FM section, a Mullard varicap tuned module type LP1186 feeds an RCA IF amplifier integrated circuit IC2 through a ceramic filter tuned to 10.7 MHz. This integrated circuit requires only one IF coil to provide the audio output for the decoder and also an AFC control voltage.

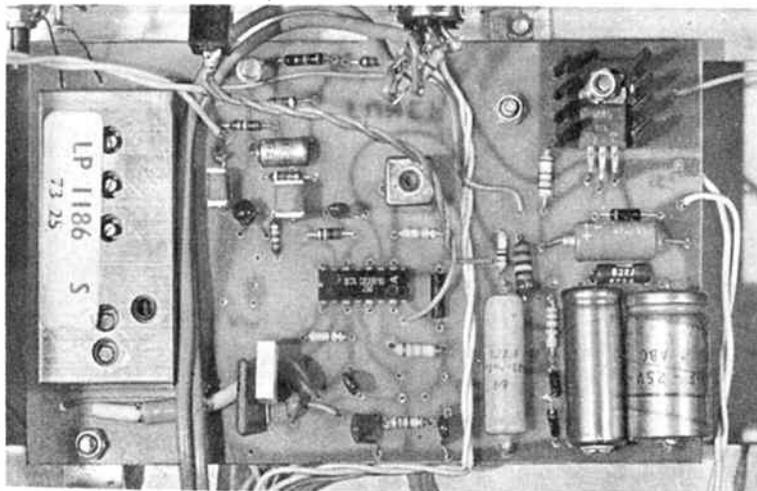
PART 2

RICHARD COLLIN

POWER AMPLIFIER ASSEMBLY

The first stage in assembly is to mount all components except the plastic power transistors onto the board, ensuring correct polarity of electrolytic capacitors. Solder each joint carefully—do not overheat the components, but make sure joints are properly made. Check that all parts are in the correct position and then cut off all excess lead wires. Note that R13 and C9 are mounted on the speaker sockets, not on the printed board.

Next fit the output and driver transistors onto their respective heat sinks ensuring that the mica washers and nylon bushes are correctly located. Check that each device is isolated from the heatsink after assembly. Then form the leads for insertion into the printed board. **Do not** bend the leads less than $\frac{1}{8}$ in from the transistor body. **Do** support the leads near the body with long-nose pliers whilst forming. **Do not** radius the bends tighter than $\frac{1}{16}$ in.



The prototype Tuner and IF board shown here has some variations in layout from the final version given in Fig. 12

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7404	21p	19p	7416	20p	18p
7405	21p	19p	7417	77p	74p
7406	54p	49p	7418	20p	18p
7407	54p	48p	7419	81p	78p
7408	20p	18p	7420	20p	18p
7409	28p	24p	7421	22p	19p
7410	20p	18p	7422	60p	58p
7411	23p	21p	7423	60p	58p
7412	40p	35p	7424	50p	48p
7413	31p	29p	7425	35p	31p
7414	49p	47p	7426	35p	31p
7415	57p	55p	7427	55p	51p
7416	20p	18p	7428	55p	51p
7417	77p	74p	7429	20p	18p
7418	20p	18p	7430	20p	18p
7419	81p	78p	7431	42p	39p
7420	20p	18p	7432	42p	39p
7421	22p	19p	7433	97p	91p
7422	60p	58p	7434	77p	74p
7423	60p	58p	7435	77p	74p
7424	50p	48p	7436	20p	18p
7425	35p	31p	7437	81p	78p
7426	35p	31p	7438	81p	78p
7427	55p	51p	7439	11p	10p
7428	55p	51p	7440	11p	10p
7429	20p	18p	7441	11p	10p
7430	20p	18p	7442	11p	10p
7431	42p	39p	7443	11p	10p
7432	42p	39p	7444	11p	10p
7433	97p	91p	7445	22p	19p
7434	77p	74p	7446	22p	19p
7435	77p	74p	7447	22p	19p
7436	20p	18p	7448	22p	19p
7437	81p	78p	7449	22p	19p
7438	81p	78p	7450	22p	19p
7439	11p	10p	7451	22p	19p
7440	11p	10p	7452	22p	19p
7441	11p	10p	7453	22p	19p
7442	11p	10p	7454	22p	19p
7443	11p	10p	7455	22p	19p
7444	11p	10p	7456	22p	19p
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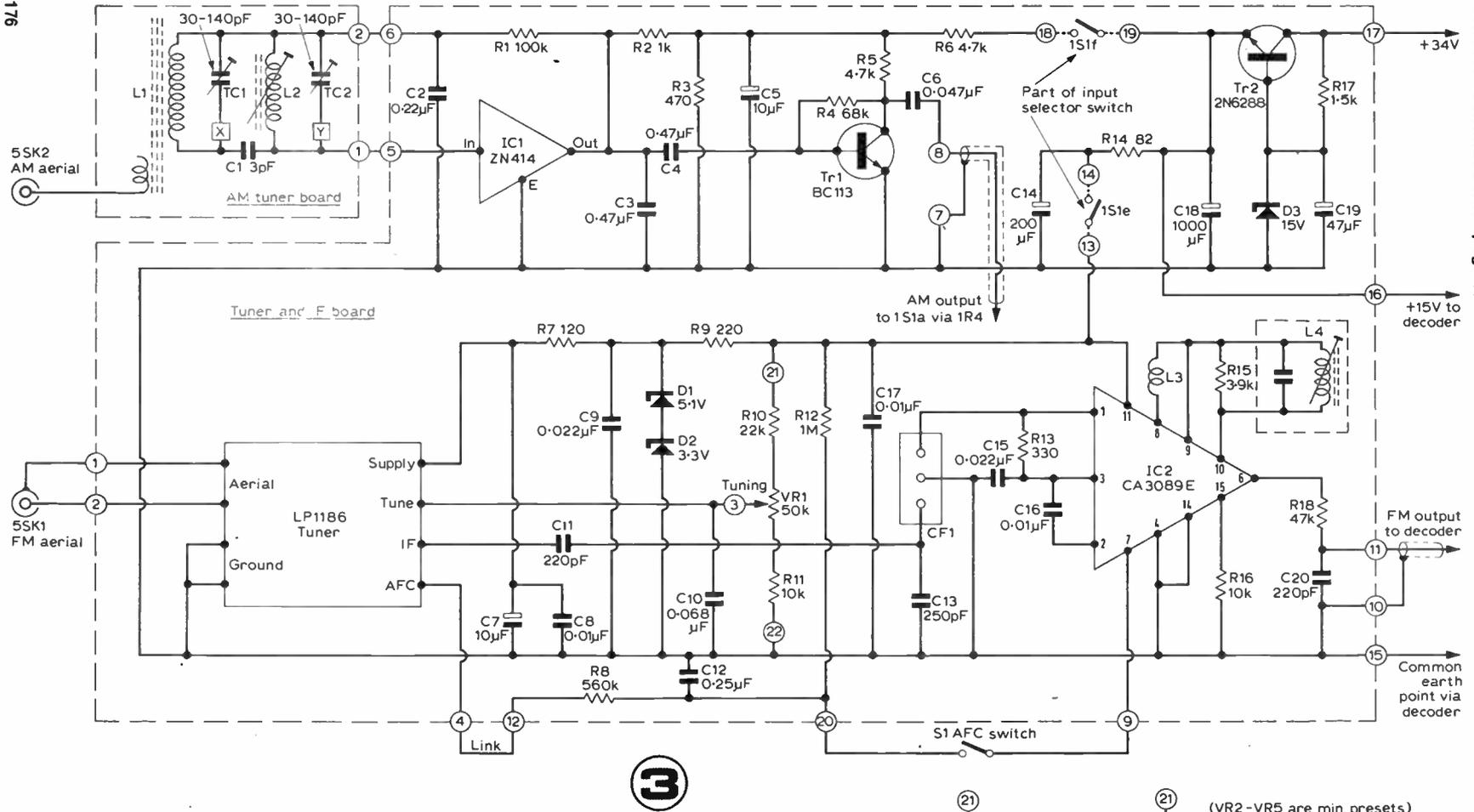
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	BC216 16p	BD219 42p	NKT300 28p		

Linear Integrated Circuits

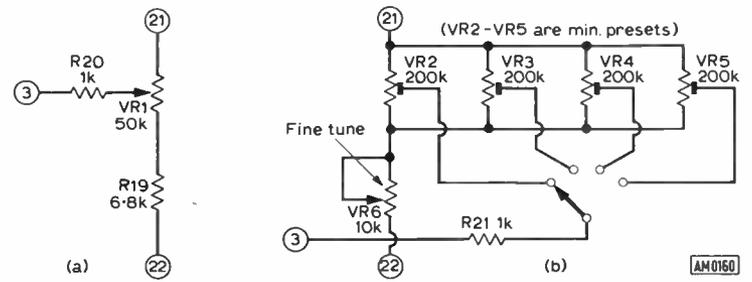
301 DIL	50p	723c DIL	89p
301 TO99	55p	723c TO99	95p
301 8 PIN DIL	46p	741c 8 PIN DIL	38p
301A DIL	69p	741c 14 PIN DIL	41p
301A TO99	69p	741c TO99	41p
301A 8 PIN DIL	69p	747c DIL	46p
307 DIL	69p	748c DIL	39p
307 TO99	69p	748c TO99	41p
307 8 PIN DIL			



CRATA—continued from page 1174

Fig. 10: Circuit of the Tuner and IF section, including the separate AM Tuner Board.

Fig. 11: Circuits of the alternative VHF tuning control arrangements described in the text:—
 (a) Full Band II coverage
 (b) Four-station preselected tuning.



AM0160

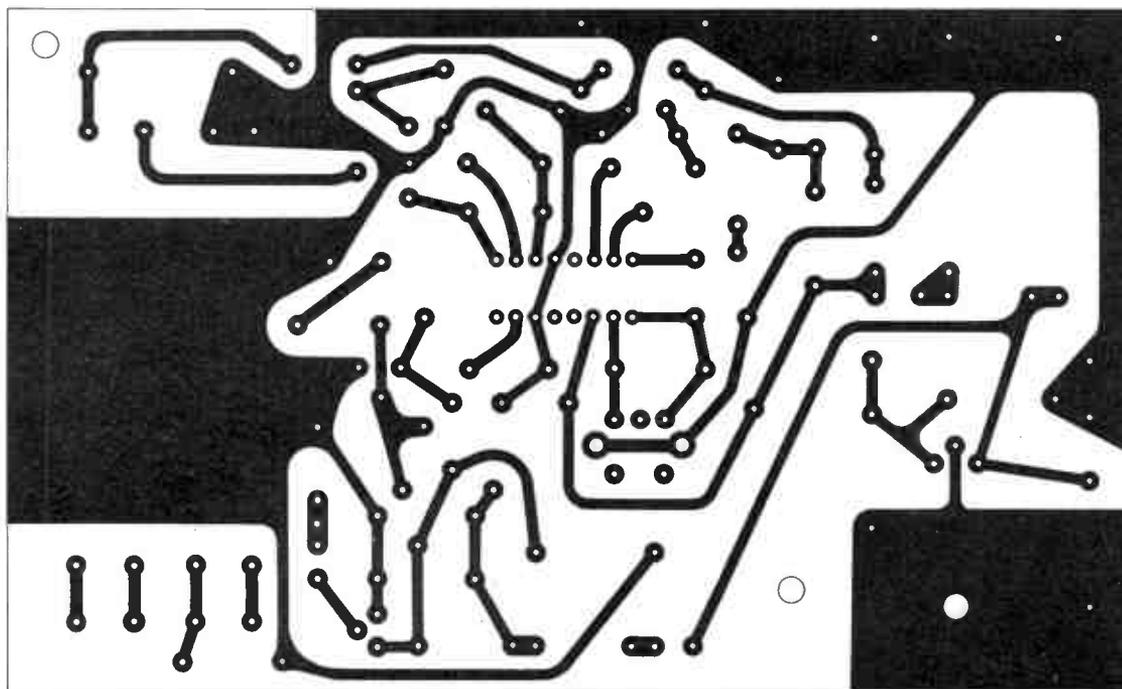
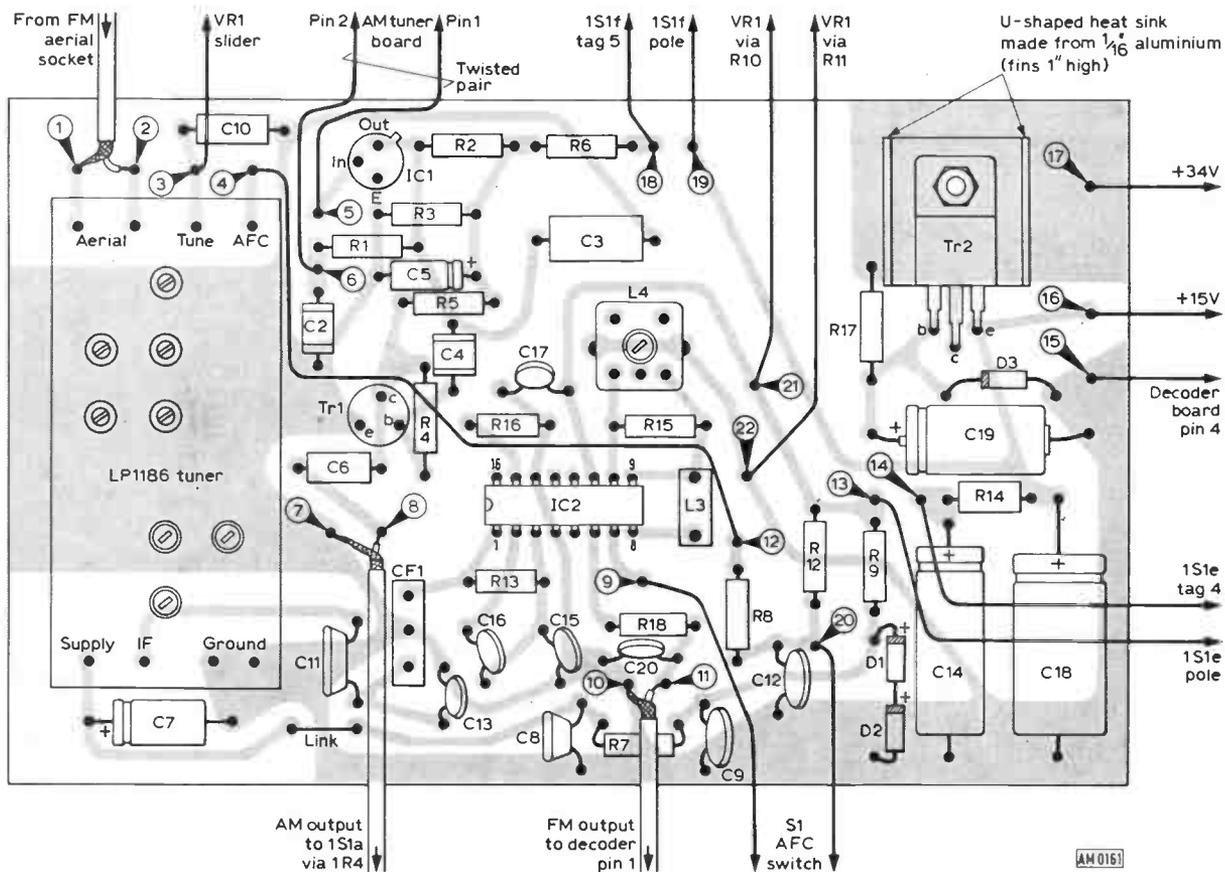


Fig. 12: Component location and printed circuit layout for the main Tuner and IF board. Both drawings are actual size.

★ components list

TUNER & IF BOARDS

Resistors

R1 100kΩ	R11 10kΩ
R2 1kΩ	R12 1MΩ
R3 470Ω	R13 330Ω
R4 68kΩ	R14 82Ω
R5 4.7kΩ	R15 3.9kΩ
R6 4.7kΩ	R16 10kΩ
R7 120Ω	R17 1.5kΩ
R8 560kΩ	R18 47kΩ
R9 220Ω	
R10 22kΩ	VR1 50kΩ lin

Note—The alternative VHF tuning arrangements require the following changes in components.

(1) Full range continuous tuning (Fig. 11a)

Delete R10 and R11 above and add
R19 6.8kΩ R20 1kΩ

(2) Preselected tuning (Fig. 11b)

Delete R10, R11 and VR1 above and add
R21 1kΩ VR2–VR5 each 200kΩ min. preset
VR6 10kΩ lin
All fixed resistors ¼W 5% carbon film

Capacitors

C1 3pF ceramic	C11 220pF ceramic
C2 0.22μF ceramic	C12 0.25μF ceramic
C3 0.47μF polyester	C13 250pF ceramic
C4 0.47μF polyester	C14 200μF 25V
C5 10μF 16V	C15 0.022μF polyester
C6 0.047μF polyester	C16 0.01μF polyester
C7 10μF 16V	C17 0.01μF polyester
C8 0.01μF polyester	C18 1000μF 16V
C9 0.022μF polyester	C19 47μF 16V
C10 0.068μF polyester	C20 220pF ceramic
TC1 30–140pF compression trimmer	
TC2 30–140pF compression trimmer	

Semiconductors

Tr1 BC113	IC1 ZN414 (Ferranti)
Tr2 2N6288 (RCA)	IC2 CA3089 E (RCA)
D1 BZY88 C5V1	D2 BZY88 C3V3
D3 BZY88 C15	

Miscellaneous

- L1 55 turns of 30swg enamelled copper wire on 2¼" x ⅜" dia. ferrite rod
- L2 Single-tuned Medium Wave coil
- L3 RF Choke 15μH Toko 7BA 150J
- L4 Toko KACS-K586-HM
- CF1 Crystal filter Vernitron FM4 or Toko CFS10-7
- S1 SPST min. toggle switch
- FM tuning head Mullard LP1186
- Tuning drive drum 1¼" dia.
- Slow-motion cord drive spindle
- Cord tension spring ¼"
- 3 small nylon pulleys
- Printed circuit boards

Notes

1. RCA semiconductors are available from E.C.S. (Windsor) Ltd. (see Part 1 of this project).
2. Toko components are available from Ambit International.

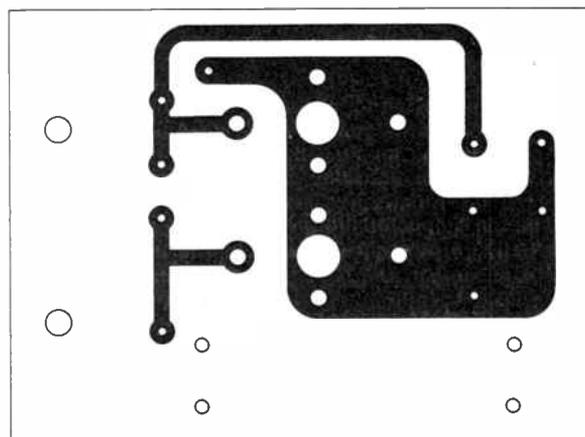
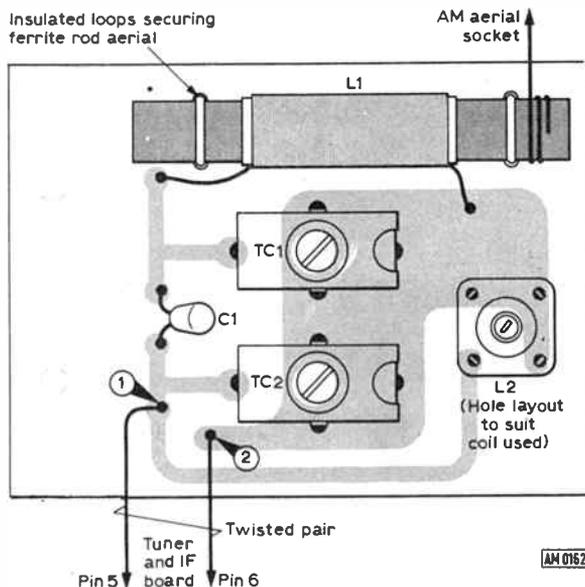


Fig. 13: Location of components and actual size layout for the AM Tuner Board.

Four power supplies are derived from the main 34V rail through a series stabiliser transistor Tr2 and various filter networks.

1. The decoder 15V supply is taken direct from the stabiliser and decoupled via C18.
2. The AM tuner 1.5V supply is provided by a resistive potential divider across the 15V supply R3/R6. Decoupling is provided by capacitor C5.
3. The FM IF and tuner varicap supply is taken from the 15V supply via R14 and decoupled by C14/C17. This supply is 12V.
4. The FM tuner 8V supply is provided from the 12V supply by R9, D1/D2 and R7. Decoupling is provided by C7, C8 and C9.

When assembling the printed board care must be taken not to overheat the integrated circuit pins and also not to short-circuit the adjacent connections as they are fairly close together. Ensure that all electrolytics and diodes are polarised correctly and that the ZN414 leads are correctly positioned. The ceramic filter CF1 may be mounted any way round—the centre pin is earthed and either of the other two pins may be input or output. The series stabiliser transistor Tr2 does not require isolation from either its heatsink or the copper print on the board.

The values given for the tuning control circuit allow coverage of 88–100 MHz. A restricted coverage has the advantage of making the tuning finer and spaces the stations farther apart. The alternative circuit of Fig. 11a provides coverage of the full band 88–104 MHz whilst a four-station preselected tuning arrangement is given in Fig. 11b.

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CRATA—continued

The AFC switch is mounted on the tuner back panel near the aerial sockets—it may be sited on the front panel if required, but do not locate it near to the mains neon and switch.

The AM aerial board, Fig. 13, on which the ferrite rod is mounted should ideally be mounted such that it can be rotated through 90° for maximum signal pickup. Alternatively it may be rigidly mounted in the correct position if the tuner will always be sited in one particular place. The leads between the printed board and the rotary switch in the multi-station version should be kept very short. A suitable position for the switch is immediately above the Input Selector.

Due to pressure on editorial space, details of the Stereo Decoder have been held over until our May issue which will also describe the Power Unit and Chassis.

oscilloscope

PART 2

techniques ALAN AINSLIE

OSCILLOSCOPE DISPLAYS

The very heart of any oscilloscope is the cathode ray display tube. After all the electronic functions have been executed the ultimate result is displayed, visibly, on the face of the tube. We shall take a look at a few types of CRT and their associated circuitry as applied to oscilloscopes.

The electron beam, produced by an electron gun, passes through a deflecting mechanism and arrives at the screen where it causes the screen material to fluoresce. The whole mechanism is housed in an evacuated glass container and, in an oscilloscope, only the front face is visible. Fig. 1 shows the general arrangement. For oscillographic use we require a bright spot of light, intense but very small.

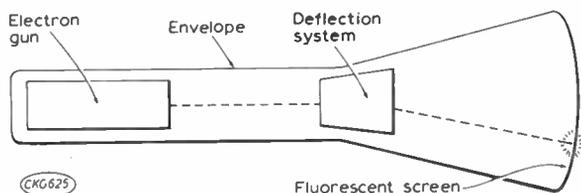


Fig. 1: Main elements in a CRT intended for use in an oscilloscope.

It is the purpose of the electron gun to produce the narrow stream of electrons of high energy to cause local luminescence of the screen. When the beam hits the phosphor screen it causes fluorescence. However, if the beam is cut off suddenly the screen continues to glow with phosphorescent light. It is this phosphorescent light that determines the after-glow of the tube.

ELECTRON GUN

A hot cathode on the axis of the tube produces electrons by thermionic emission, as in a conventional electronic valve. By a suitable arrangement of anodes an electric field distribution inside the tube is created focusing the electrons into a high velocity pencil, arranged to converge on to the screen. A simple gun arrangement is shown in Fig. 2. This type of arrangement is often used and is known as a pentode or five electrode gun.

The cathode is heated to emissive temperature and is surrounded by the grid, in this case shaped like a top hat with a hole in it, known as a Wehnelt cylinder. The grid is maintained slightly negative with respect to the cathode and focuses the space charge around the cathode along the axis of the gun.

The first anode (A1) is positive with respect to the cathode by perhaps a couple of hundred volts. Fig. 3 shows how the electrons are accelerated out of the grid area towards the first anode, and in so doing are focused at Z by the equipotential lines, shown dotted. The diameter at Z is used as an "image" and consequently should be as small as possible for a small spot on the screen. The electron beam enters the first anode diverging and a number of stops are added to keep the beam width small and keep out fringe electrons which impair definition. The diverging electron beam emerging from the first anode now needs to be focused on to the screen, or put another way, an image of Z is projected on to the screen.

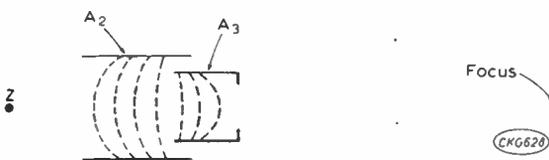
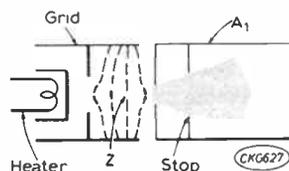
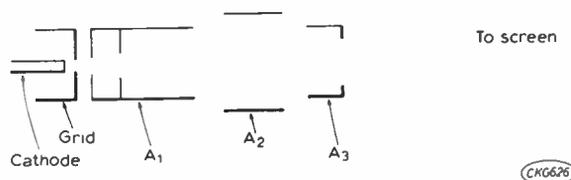


Fig. 2: top, arrangement of electrodes used in a pentode gun. Fig. 3, centre, shows the beam focusing action of the grid and A1. Fig. 4, bottom, the effect of the remaining anodes A2 and A3 in focusing the beam on to the screen.

Fig. 4 shows how the second (A2) and third (A3) anodes accomplish this focusing. The second anode is at a higher potential than A1, and A3, the final anode, is at a still higher potential. Thus the equipotential lines are as shown dotted. The beam of electrons now converges as it crosses the A2-A3 fields and by adjustment of the voltage between A2 and A3 the beam can be focused on the screen of the CRT.

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AC126	12p	AF139	32p	BF173	20p	OC44	12p	2N3708	10p
AC127	15p	AF178	32p	BF177	28p	OC45	12p	2N3709	11p
AC128	15p	AF180	40p	BF178	32p	OC70	12p	2N3710	11p
AC131	12p	AF181	40p	BF179	32p	OC71	12p	2N3711	11p
AC132	12p	BC107	12p	BF180	32p	OC72	12p	2N3819	32p
AC176	15p	BC108	12p	BF181	32p	OC81	12p	2N4062	12p
AC187	22p	BC109	12p	BF194	14p	OC82D	12p	2N4286	20p
AC188	22p	BC147	12p	BF195	14p	2N2646	60p	2N4289	20p
AD140	50p	BC148	12p	BF197	15p	2N2904	20p	40360	35p
AD149	45p	BC149	12p	BF200	32p	2N2926	10p	40361	35p
AD161	33p	BC157	14p	BFY50	20p	2N3054	50p	40362	40p
AD162	36p	BC158	14p	BFY51	20p	2N3055	60p	40408	40p
AF114	20p	BC159	14p	BFY52	20p	2N3702	12p	ZTX108	15p
AF115	20p	BC187	22p	BUY105	225p	2N3703	12p	ZTX300	15p
AF116	20p	BD131	75p	OC26	45p	2N3704	12p	ZTX302	20p
AF117	20p	BD132	75p	OC28	50p	2N3705	12p	ZTX500	15p
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IN4002	100V	1A	8p	OA91	5p	
IN4004	400V	1A	8p	OA202	7p	
IN4006	800V	1A	10p	IN4148	8p	
IN4007	1000V	1A	10p	BA114	8p	

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86mm x 9mm x 16mm, length of track 59mm.

SINGLE 10K, 25K, 100K log. or lin. 40p.

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106F	50V 4A	40p
106D	400V 4A	55p

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AB8	4" x 4" x 1 1/2"	50p	AB15	8" x 6" x 3"	108p
AB9	4" x 2 1/2" x 1 1/2"	50p	AB16	10" x 7" x 3"	122p
AB10	4" x 5 1/2" x 1 1/2"	50p	AB17	10" x 4 1/2" x 3"	108p
AB11	4" x 2 1/2" x 2 1/2"	60p	AB18	12" x 5" x 3"	120p
AB12	3" x 2" x 1"	44p	AB19	12" x 8" x 3"	160p

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60 Volts. All tapped at 0-12-15-20-30V.

Output Amps.	Ref. No.	Price	Output Amps.	Ref. No.	Price
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C-D Ignition System by R. M. Marston, Esq., Wireless World.

Reference 173AT

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In simpler types of CRT A2 is omitted giving a tetrode electron gun. The final focusing takes place between A1 and the final anode and geometrically is suitable for a fine spot. However, if focusing is achieved by varying A1 (the final anode potential is fixed as we shall see later) this affects the velocity of the beam because A1 is the primary accelerating anode. The change in velocity changes the position of the point Z and the range of focus is restricted for a good spot size. This situation in practice means that when the grid potential (brightness) or the A1 potential (focus) is altered the other potential must be changed as well, giving restricted focus and brightness range. It is for this reason that the pentode type of tube is almost universally used.

BEAM DEFLECTION

An electron has a negative charge of 1.6×10^{-19} coulombs. This is a very small charge, and conversely any electric field acting on the electron will produce only a very small force. However the mass of the electron is very small and so large accelerations can be produced with only moderate potentials.

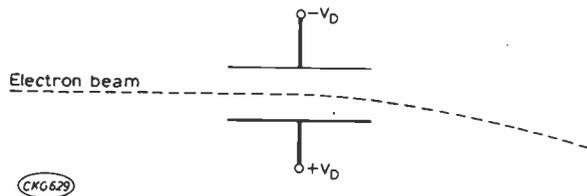


Fig. 5: Effect of the deflecting plates on the electron beam.

If a beam of electrons, focused into a fine pencil, is allowed to pass between two parallel plates as in Fig. 5, the electrons will experience a force towards the positive plate and it can be shown that the deflection is proportional to the deflecting voltage (V_d) and inversely proportional to the accelerating voltage (V_a). A purely mathematical outlook shows that electrostatic deflection produces a (theoretically) linear deflection mechanism.

DEFLECTION PLATES

In order to keep the sensitivity as high as possible the tube is physically large and the deflector plates are placed as close together as possible, usually of the form shown in Fig. 6 to permit high deflection sensitivity to be achieved without the beam catching the actual deflector plates. If this occurs (for example if the timebase is overdriven to give X expansion) secondary emission occurs at the surface of the plates, and the low energy secondary electrons can be accelerated towards the screen causing flare and high background illumination. This undesirable

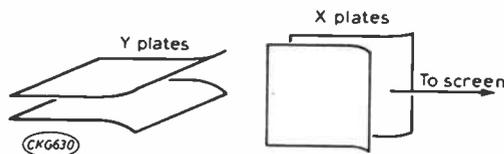
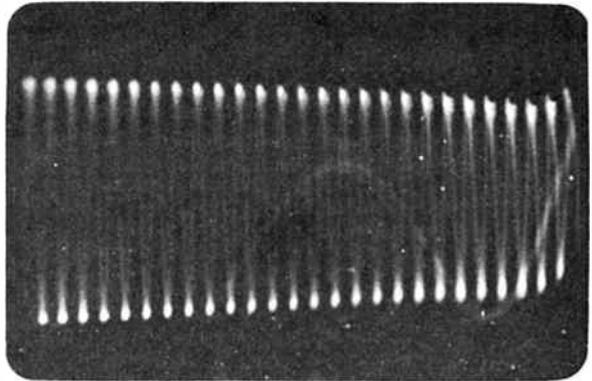


Fig. 6: Arrangement of the X and Y plates, the Y plates being nearer to the gun system.

effect can be avoided by coating the plates with a material of low secondary emission, or providing "beam catchers," small cups that accept the beam when driven off the screen. The X plates are usually mounted nearer to the tube face so that the Y plates have the maximum sensitivity.

To ensure that the electron beam does not become distorted in any way by extra acceleration due to the deflector plates they are arranged to be at the same potential as the final anode. Of course this is only true when the beam is travelling along the axis, but to prevent any gross errors on deflection it is common to provide symmetrical or push-pull deflection. This ensures that the mean electric field is not altered by deflection.



Trapezium distortion on a simple CRT operating with asymmetrical deflection on both axes. The focus and definition make this scope useful only for the simplest applications.

If the plates and final anode were at differing potentials then there would be a deformation of the circular cross-section of the beam (remember it is NOT in focus at this point, only at the screen where the cross-section area should be almost zero) by the plates attracting, or repelling, the outer electrons at opposite sides of the beam. This gives a sausage-shaped spot and the remedy is to make the final anode potential variable so that it may be matched to the Y plates. The X plates are then adjusted to be equal to the Y plate potential (as we shall see in a later section, it would be difficult to alter the Y plate potential). The control for setting the final anode volts is known as the "Astigmatism" potentiometer and is usually a front panel control.



The same CRT displaying a 1kHz square wave. Astigmatism is most noticeable as is the lack of HF response due to the simple deflection amplifier.

Another cause of incorrect spot size and shape is due to the pencil of electrons tending to spread, all being negatively charged. However, in high voltage tubes the velocity of the beam is high enough to keep the electrons in line by the magnetic field that they produce. The mechanism of electrostatic deflection relies on the electron beam being in the field of the deflector plates for a finite time. This means that when a very high frequency, say above 100MHz, signal is applied to the plates the signal may have changed before the electrons have emerged.

If, for example, a beam of electrons takes 10ns to travel through the plates a 100MHz signal will have completed one cycle and the deflection will be zero. In modern high velocity tubes the effect only occurs over 150 or 200MHz and the remedy is to arrange a series of deflectors, linked so that the velocity of the signal down the plates is the same as the velocity of the electron beam. However there are few uses for deflection amplifiers that can produce 200MHz output so this is of academic interest only.

THE FINAL ANODE

In order to produce the high velocity beams that are required to display fast transients, a high accelerating voltage is required. As we have seen, if this is applied to the final anode deflection sensitivity will be reduced so we apply the accelerating potential after deflection, called post deflection acceleration or PDA. Several methods of applying the PDA potential are used but they all aim at not reducing the deflection sensitivity, most important when the deflection amplifiers use transistors having only a limited output voltage swing.

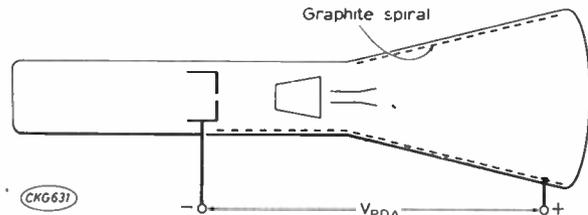


Fig. 7: Location of post deflection acceleration electrode in CRT.

The most popular form of PDA until a few years ago was the form shown in Fig. 7 and used in a lot of Cossor CRT's. The electron gun and tube are as they have been described so far and the beam is accelerated and deflected and focused normally. Around the inner wall of the tube is wound a resistive graphite spiral, connected to the final anode, and at the other end to a few kV positive. The beam is thus accelerated through this field to arrive at the screen with high velocity.

The screen tends to charge negatively at these high energies because more electrons are being gained than lost by secondary emission from the screen. The back of the phosphor is therefore given a very thin coating of aluminium and this conducts the charge to positive PDA, eliminating "screen sticking". This occurs where a local area of screen acquires a negative charge and tends to repel the beam, giving low light output. The aluminium also produces a more axial accelerating field giving better geometry and increased light output by reflecting the light forwards.

The field of the PDA is such as to produce a slightly convergent lens giving a smaller image and also, if it penetrates into the deflector plate region, causes acceleration before and during deflection, decreasing the scan even further. But in spite of this the PDA system offers a distinct advantage of increased trace brightness.

A fine wire mesh can be placed in the path of the beam just after deflection and if connected to the final anode acts as a screen to keep any PDA fields out of the deflection system. This arrangement gives rise to a PDA field that acts as a diverging lens, magnifying the deflection considerably, but also the spot size. Alternatively this mesh can be placed near the screen and PDA applied between the mesh and the screen. This gives very good results without affecting geometry but such tubes are prone to internal flashover.

SCREEN PHOSPHORS

The screen material or phosphor is arranged to give the highest possible light output of the correct colour and persistence. The table shows the range of phosphors used in cathode ray tubes, the most usual being P1 or P5, whilst P7 is sometimes used for medical applications.

Phosphor	Persistence	Fluorescence	Phosphorescence (Afterglow)	Uses
P1	Medium	Green	Green	Scopes (Visual)
P2	Long or Short	Blue/Green	Yellow/Green	Scopes (Visual)
P3	Medium	Yellow	Yellow	Television
P4	Medium	White	White	Scopes (Photography)
P5	Short	Blue	Blue	Television
P6	Medium	White	White	Radar
P7	Long	Blue/White	Yellow	Storage Tube
P8	Short	Blue/White	Yellow	Scopes (Photography)
P9	Long	White	White	Scopes (Photography)
P10	Permanent	Magenta	Magenta	Radar
P11	Short	Blue	Blue/Green	Storage Tube
P12	Long	Orange	Orange	Scopes (Photography)
P14	Long	White	Orange	Radar
P15	Short	Blue/Green	Orange/Green	Radar
P19	Long	Orange	Orange	Flying Spot Scanners Radar

Table of phosphor types and principal applications.

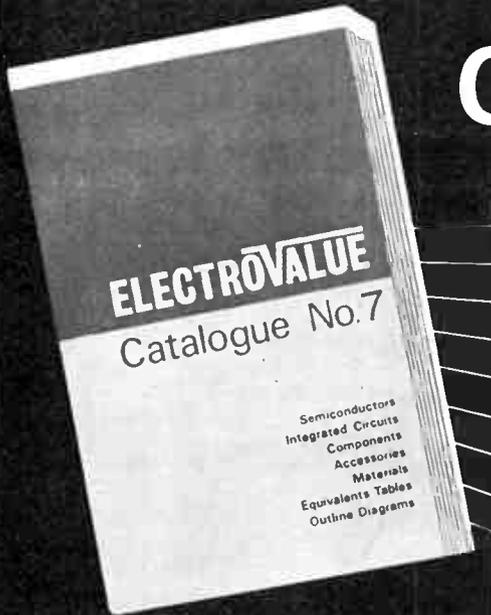
Although the trace produced on a tube can be intensely bright, even with only a couple of kV, the contrast between the trace and the background (grey/white) is usually quite small. A filter of about 65% transmission, of the colour of the trace, placed in front of the tube can increase the contrast by a large amount despite a decrease in light output.

GRATICULES

The graticule or measuring scale can be engraved on the filter or a better idea is to cut the graticule into a piece of 1/8in. perspex. If the markings are on the front, the observer can move so that the reflection of the line from the back surface of the graticule are in line with the actual lines. This ensures zero parallax when making measurements. The perspex can be lit from the side by a red bulb causing the cuts in the perspex to light up red, although white light is better for photography due to the uneven spectral response of films. Constructors making their own graticules out of perspex must bear in mind that the clearest line, especially with side illumination, is produced by cutting the perspex with a sharp knife and not by scratching.

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CC	1/2	4-7-10M	1-3	1-1	0-9 nett
C	3/4	4-7-10M	1-5	1-2	0-9 nett
C	1	4-7-10M	3-2	2-5	1-9 nett
MO	1/2	10-1M	4	3-3	2-3 nett
WW	1	0-22-3-9	9	9	8
WW	3	1-10K	7	7	6
WW	7	1-10K	9	9	8 nett

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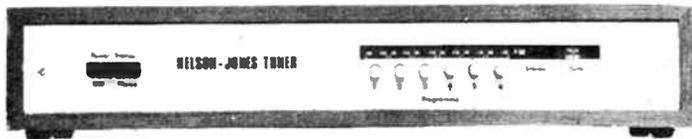
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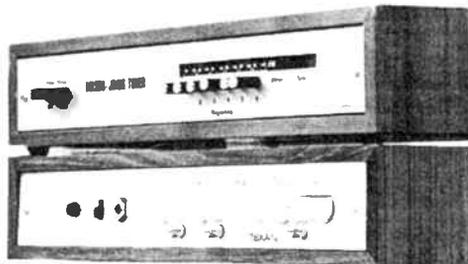
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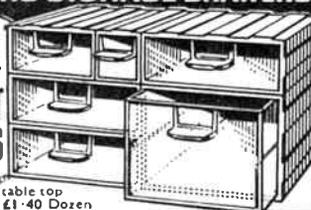
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PHOTOGRAPHY

Photographic film (even so called panchromatic) is most sensitive in the blue region and for this reason blue tubes are best suited to making photographic records. However, fast film (400ASA) together with a wide aperture, f2.8 or better, can give reasonably short exposures from a green tube.

When using single lens reflex cameras, best suited to this type of work, it is important to remember that the image on the film is scanned from right to left (lens inversion) and the direction of motion of the blind could well be from left to right, giving a small vertical exposure if the scope sweep speed is slow. The average shutter takes 1/30 or 1/60 of a second to scan the film and so one must be aware of these difficulties when dealing with fairly slow sweep speeds at fast shutter speeds. For single shot photography it is best to have the shutter completely open before the appearance of the trace.

ABERRATIONS

The ideal characteristics of a cathode ray tube are not always realised in practice due to assumptions in the theory, or plain constructional error (anodes off axis, etc.). One of the most important flaws or "aberrations" is that known as "Astigmatism" and this has already been dealt with, together with its cure.

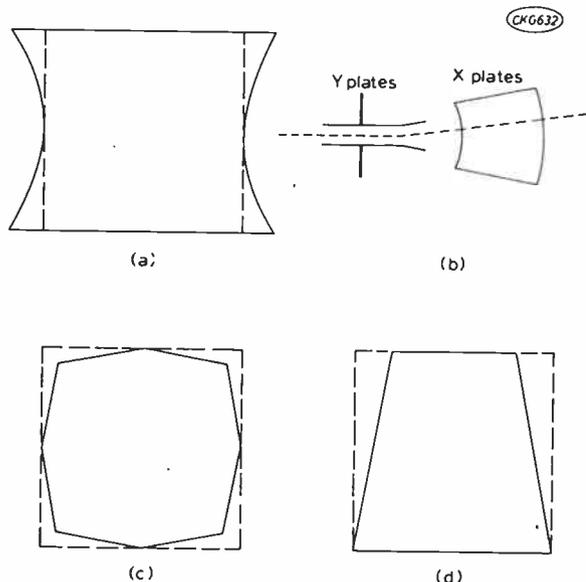


Fig. 8: Pin cushion distortion (a) can be corrected by shaping the plates as in (b). (c) illustrates barrel distortion and (d) trapezium distortion.

Most of the other aberrations are most apparent when the tube is displaying a raster. Ideally such a raster should be capable of being focused into a perfect square of scan lines, all in focus. Some defocusing occurs in deflections due to lens action between the final anode and plates, and between the plates. The effect between the plates is reduced by placing an "interplate shield" between the two sets of plates with a hole for the beam to pass through. This shield is at final anode potential and reduces the defocusing effects.

If the raster takes on the shape of Fig. 8a the distortion is known as pin-cushion distortion and is

caused by the deflected beam travelling through a greater distance between the second set of plates thus arriving at an oblique angle. This can be reduced by making the second pair of plates as in Fig. 8b. Fig. 8c shows barrel distortion caused by loss of extreme scanning sensitivity due to the PDA fields. This can only be reduced by careful design of the PDA spiral. Fig. 8d shows trapezium distortion. This is caused by asymmetrical Y deflection accelerating the beam as the driven Y plate goes positive and decreasing the X sensitivity accordingly. Specially designed plates are available for asymmetrical deflection only.

CRT DEFECTS

Other defects occur in specific tubes and it must be realised that any CRT is a compromise between conflicting factors. Consequently the best instrument tubes as fitted in laboratory scopes can cost several hundreds of pounds, but the home constructor can purchase surplus tubes for just a few pounds and many quite good home-made scopes have been built using these tubes.

With age or abuse cathode ray tubes tend to develop faults the most serious of which is likely to occur at virtually any time, is when the mechanical structure of the electron gun fails. The gun is constructed with tiny spot welds and severe shock or vibration can cause an element to be dislodged. If this happens the tube is almost surely destined for scrap.

Also linked to the mechanical structure of the tube is a fault producing what is known as a "soft" tube. This occurs when a small amount of air leaks into the bulb through an imperfect glass-to-metal seal. This may become evident only after many hours of operation and the symptoms are a diffuse display and a blue glow in the gun assembly. As the pressure inside the tube rises further, tracking occurs in the gun and external circuits can be damaged. In order to avoid this fault occurring it is necessary to take great care when handling the tube and making connections to it. Connections should never be soldered directly on to the tube pins as this is almost certain to break a seal or even crack the envelope, with glass flying everywhere at high velocity.

Perhaps the most common fault, linked directly to old age, is low cathode emission. The cathode surface loses emissivity either by the emissive layer evaporating or becoming poisoned by the remaining gas in the tube. The effect is that in order to see a trace at all the brightness control has to be advanced so far that the beam spot goes out of focus and silvery. The silvery effect is due to the cathode emitting in patches and on some scopes, if the focus control has sufficient range (making focus anode nearly the same potential as final anode), it is possible to produce an image of the cathode on the screen. The image looks a little like the full moon, the dark patches representing areas of low emission.

Sometimes a low emission tube can be improved by deflecting the spot off screen and turning brightness full up for a couple of hours. If this does not work a small transformer supplying 6.3V + 10% can be used to supply the heater (common practice in TV's). However the insulation of such transformers is doubtful over 1kV and a breakdown would make the tube heater/cathode short or damage it in an even worse manner. A small auto transformer is

perhaps the best idea, fed from the normal tube heater supply with a boost of about 10%.

Really bad tubes (that would be thrown out anyway) can sometimes be restored by the circuit in Fig. 9. The heater of the CRT is supplied with 6, 8 or 10V from T1. When the HT switch is closed a small current will flow due to cathode emission. This current strips the top coating off the cathode and if the emissive layer beneath is better then the current will rise. 10 or 15mA is typical of the current to be expected from a good tube if R1 is made 12kΩ.

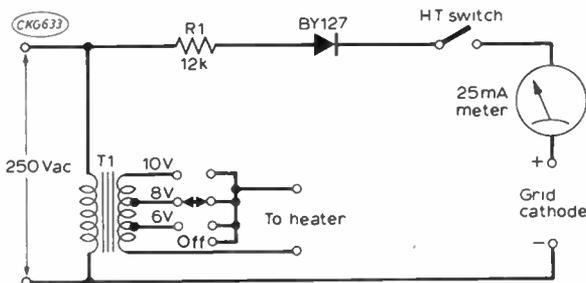


Fig. 9: Circuit of arrangement to restore the cathode emission of a CRT.

The pulse nature of the HT helps the stripping, but if nothing happens then 8 volts can be tried on the heater, 10V is for a real emergency! In many cases switching the heater off with HT still applied, at low cathode temperature, quite vigorous stripping can occur. This is shown by rapid kicks of the meter and small flashes in the gun. In this way really bad tubes can be recovered but it is also possible to weld the grid and cathode together or strip the cathode completely so it should be saved as a last resort.

A3 +150V, Y plates and X plates (depending on external deflection circuits) +150V, PDA anode +1kV. Springs on A3 contact the graphite coating leading to the PDA spiral.

R1, C2 and C3 smooth the -EHT line and R4, C5, and C6 smooth the PDA line. In simple scopes with PDA tubes the PDA is sometimes connected to the highest HT line. C1 couples pulses to the grid to bias the gun off during timebase flyback and R2 is merely to isolate the grid from the EHT line.

When the PDA potential required is only low the EHT is derived from a mains transformer, but when 10kV or so is required, together with high beam currents, use is made of an RF EHT supply. This generates AC at about 30kHz and is fairly safe. We shall consider this in greater detail in a later section on power supplies, but one important advantage must be mentioned here.

Because the RF EHT supply is self generating, involving usually an oscillator and a power output stage driving a transformer, the supply is easily stabilised against variations by sampling the output and applying feedback and, because of the high frequency, smoothing is relatively simple.

SPECIAL TUBES

Often it is necessary to present two traces simultaneously on one tube, scanned by a common X timebase. Although successful electronic methods are available to enable two traces to be presented apparently simultaneously a double beam tube is favoured for some applications.

The simplest approach is to construct two guns in one envelope, each with a set of Y plates and common X plates. This method is expensive, however, and the principle usually adopted is to split

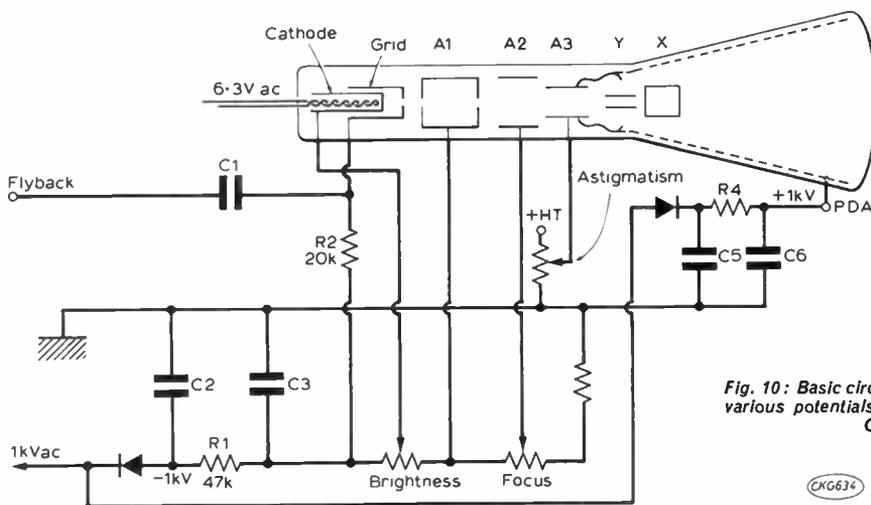


Fig. 10: Basic circuit for supplying the various potentials required by a PDA CRT.

CRT POTENTIALS

We are now in a position to consider the arrangement of the potentials on the tube to provide the necessary electric fields. Fig. 10 shows a typical arrangement. As we saw earlier A3 must be the same potential as Y plates and so the potentials are decided around this. Typical potentials might be grid -1000V, cathode -995V, A1 -850V, A2 -150V,

the beam. Usually the splitting is done by a splitter plate connected to the final anode. A snag with this method is that secondary electrons produced at the plate cause high background illumination of the screen. Sometimes this is prevented by performing the splitting between A1 and A2.

To be continued

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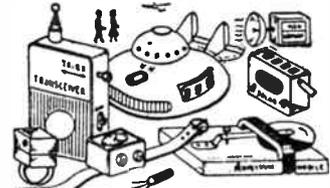
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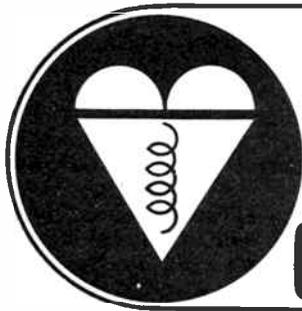
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SAFETY IN DOMESTIC ELECTRONICS

THE British Electrotechnical Approvals Board for Household Equipment was set up by the British Standards Institution to promote the widespread practice of standard safety rules in domestic electrical and electronic apparatus. The scheme is now being extended to include audio and radio products, within the first group, i.e. record players, record players with radio, radiograms and mains/battery portable radio receivers with rated audio outputs up to 6+6 watts stereo and 10 watts mono, both continuous sine wave ratings.

The scheme applies the specifications and testing procedures as detailed in BS415: 1972 (with amendments). This short article has been prepared to assist constructors and users of related equipment, since some of the specifications in BS415 are of particular interest to constructors.

The specification states the scope of the safety requirements, the definition of terms used in context, the general requirements, conditions of test, marking and instructions, ionizing radiation, heating, electric shock, insulation, fault conditions, mechanical strength, components, terminal devices, flexible cables, connections, television and other picture tubes and mechanical stability. The notes that follow are for guidance only, in the interest of practising safety considerations.

GENERAL REQUIREMENTS

Under the terms of BS415 adopted for the scheme, the apparatus is expected to be designed and constructed to present no danger and in particular provide for personal protection against electric shock, and the effects of excessive temperature, ionizing radiation, implosion, fire, mechanical instability and moving parts.

MARKING

The equipment should have indelible markings, that cannot be removed by rubbing with cloth soaked in petrol or water, on the exterior (but not on the bottom) or inside a removable lid. The information to be marked should include the following:

1. The nature of the supply, a.c. or d.c. using symbols according to BS3939.
2. The rated supply voltage or range of voltages. In the latter case the indicated voltage setting being used must be clearly shown.
3. The rated mains frequency in hertz if a.c.
4. The voltage and current or power which may be drawn from the main unit to supply other units.
5. Warning of live parts made accessible by removing or opening a cover.
6. Mains flexible leads should have a label attached if permanently connected to the equipment, or a marking should be close to the mains connector on the equipment, giving the following information (for U.K.): "Warning: this apparatus must be earthed".
7. Mains flexible leads should be connected in accordance with the British Standard colour code: Brown to "live", L, or red painted terminal; Blue to "neutral", N, or Black painted terminal; Green and Yellow to "earth", E, green painted or earth symbol terminal.
8. Fuses should be used to protect equipment and the ratings marked close to the fuse (if mounted on equipment) or by labelling the mains supply lead. (As a guide, for equipment of power consumption rated at less than 500W use a 3A fuse, or to withstand switch-on surges, a 5A fuse; for power consumption rated at less than

800W use a 5A fuse; for less than 3kW use a 13A fuse. It is seldom wise to use a 13A fuse to protect small equipment of less than 500W.) The power consumption should be indicated and not exceeded by more than 10%.

TERMINALS

1. Where a separate safety earth terminal is fitted the standard symbol (BS3939) should be visibly marked adjacent to it.
2. Where terminals are live under normal operating conditions a symbol should be marked adjacent to it to indicate this fact. This should include the output terminals of high power amplifiers and transmitters.
3. The outputs of "battery eliminator" units should clearly indicate by marking near the terminals the load power and voltage that can be handled.
4. Terminals used for inter-connecting one or more units to a "master" power supply source should indicate ratings as in number 3 above.

SHOCK PROTECTION

Inaccessible live terminals used for providing connections to other units should be protected by an insulated and captive cover. Live terminals should not be easily accessible during normal operation.

Accessibility is determined by BSI as being touchable by inserting through apertures, or otherwise easily applying, a "standard test finger". For test purposes, this finger is approximately equivalent in size to an average adult index finger 80mm long by 12mm across its narrowest thickness. Also used is a "standard test pin" 25mm long by 6mm diameter, being near the size of a pencil.

Live operating shafts and aper-

tures should be adequately protected so that a free hanging endless metal test chain of 2mm diameter (approximating to a lady's metal necklace chain of small links) cannot make electrical contact through any aperture.

Knobs, levers, push-buttons and similar manually operated devices should be fastened so that their operation will not impair the protection against shock. When removed by detaching the fixing screw, pin, or clip, there should be no exposed live parts.

A metal pin 100mm long and 4mm diameter should not be capable of being brought into contact with any live part, through any aperture, when held by the fingers.

Access holes for setting up of preset controls by means of a screwdriver or hexagonal key wrench should not introduce a risk of the tool touching live parts with a risk of shock. Any other hole within 25mm of this hole should not involve the risk of a shock.

OTHER POINTS

Accessible metal parts should be connected to the earth wire of a 3-core mains cable and effectively earthed through the mains wiring system.

Resistors should not present unstable overload conditions in the event of a short-circuit or disconnection through fault conditions, presenting a hazard under any of the safety require-

ments. Similarly, with the breakdown of capacitors, normally having adequate dielectric strength for the voltage rating quoted by the maker, such a hazard should not result.

High voltage components and assemblies (above 5kV) should not give rise to risks of fire to surrounding apparatus or give rise to any other hazard.

For equipment provided with a connector socket for the mains supply, the safety earth terminal should be an integral part of this socket.

Terminations (including screw soldered or crimped) should be so located or shielded that even one strand of the conductor, that may escape the termination, does not present a risk of accidental contact with another live part or metal accessible part.

Screw terminals should be fixed so that they will not work loose when the nut or screw is tightened or loosened during normal fixing or detachment of connections. Screw terminals should not cause damage to the wire when tightened, thus risking a subsequent fracture.

Flexible mains leads should comply with BS6500.

FINALLY

These are just some of the points worth noting. We would add here that small children are at particular risk unless special care is exercised regarding accessibility to equipment and, of course, hot soldering irons. If

you have small children please do not leave your workbench unattended without first making sure that they cannot gain access to your work. Best to lock the door and/or switch everything off. Large electrolytics hold their charge for some time; it is wise to tape the terminals to insulate against accident touching.

Always use a protective guard for your soldering iron and never leave an exposed hot iron hanging by a hook. Splashes of hot solder and flux can ruin your clothes; wear an overall or old working trousers.

It is always a wise move to have a first aid kit for cuts and shock. Minor burns can be best treated by running cold water on the affected area immediately for at least three minutes. More serious burns should be seen by a doctor. Never apply ointments or creams to a burn without first seeing your doctor.

British Standard specifications can be inspected free of charge at the BSI library in London, W.1. Purchases should be addressed to BSI Sales Dept., Newton House, 101 Pentonville Road, London N1 9ND.

Manufacturers and vendors wishing to be considered for application of BEAB approval to their products are invited to apply to BEAB, Mark House, 153 London Road, Kingston-upon-Thames, Surrey KT2 6NX with full details of their products. All applications within these categories should be received by 8th March, 1974. ■

off the record

AS this is the last issue of *Practical Wireless* in Volume 49, we thought that readers would be interested in a few details before we launch into the 50th volume next month.

Volume 49 carried the most number of pages (1,232 plus covers) in the 33½ years history of monthly *Practical Wireless*. The previous best was 1,184 in volume 37, 1961-62, for 12 monthly issues. Pre-September 1940 issues were weekly. Of these (taken over a six-month period) Volume 1 1932-33 carried 1,256 pages and Volume 3 1933-34 carried 1,184 pages.

There were 89 constructional articles and serial parts, 46 features and serial parts, 8 Datacards, 3 Crosswords, 2 Supplements, 1 competition, 1 special offer, plus the usual regular News and Comment items, all in Volume 49.

We have not counted the number of components that have been listed for our projects, but would make an estimate of several thousands. This may explain the reason why we have broken records with advertisements too, more than 760 pages in Volume 49. There were more than 500 pages of editorial material. What a bargain for £2.50!

The official ABC (Audit Bureau of Circulations) figure for the circulation of *Practical Wireless* for the six-month period July to December 1973 showed a 0.37% increase over the same period of 1972. This was greater than its nearest rivals in a similar field in the U.K., and it still represents the highest ABC figure of all U.K. do-it-yourself radio and electronics journals.

It does show that the magazine's strength is in the active participation of you, the readers, buying components and making them into working projects. Our records of response to advertisements endorse this statement. There must be many of you who are equally content to read about other constructors' activities. For these readers and those of you who are just starting to follow our projects, why not have-a-go now? What's that—you have no good tools? Then you simply must invest in our Special Offer Tool Kit!

COMING SOON

We have some unusual ideas coming in our summer issues, details of which will be given next month. If you can't afford a holiday this year, you can afford 25p for *Practical Wireless* each month. If you can afford a holiday, take P.W. with you. Thousands do!

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221	8	6	6	£2-90
320	12	8	12	£5-75

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15	16	6p	150	16 6p
15	40	6p	150	25 6p
15	63	6p	150	40 10p
22	10	6p	150	63 12p
22	25	6p	220	4 6p
22	63	6p	220	10 6p
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33	16 6p	220	25 10p	1500 6.3 12p
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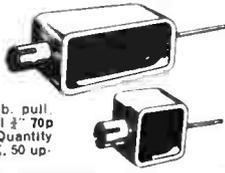
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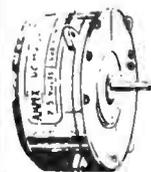
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BROADCAST BANDS

SHORT WAVE DX by MALCOLM CONNAH

ONE of the most frequent questions asked by those of you who have written to me recently has been about the modification of the CR100 receiver mentioned in an earlier article. These modifications were described in detail by C. Molloy in the April 1968 issue of *Practical Wireless*.

I appreciate that an issue of this age is rather difficult to come by, but I feel sure that anyone who is really interested should be able to obtain one. (Out of print—Ed.) Perhaps the best way of tackling the problem of finding a copy is to use the CQ column of this magazine.

Two months ago I mentioned that Radio New Zealand should soon be audible again. News has just reached me, via DX Corner Belgium, that the station has recently been heard in the U.S.A. Radio New Zealand was heard on 9540kHz at 0600 and again on 11780 at 0700. Reception was better on the latter frequency.

I know that it means getting up early in the morning, or alternatively staying awake all night; but how about one (or more) of our readers trying to receive this fairly rare station.

Radio Clube de Mozambique is reported to be using 120kW on 7210 from 0700 to 1400 and on 11820 from 0350 to 1500. Tests are also being carried out on 15293kHz.

Readers' Logs

By way of coincidence the first log this month comes from New Zealand. Ian Cook of Nelson has a Stewart-Warner R-146X, 7-valve receiver and a 120ft end-fed aerial which extracted the following signals from the Antipodean ether:

- 3995 *Solomon Islands BS*, in English at 0945.
- 5960 *R. Canada Int.*, in French at 0610.
- 9009 *Kol Israel* in English at 0510.
- 9520 *RNE, Spain* in Spanish at 0310.
- 9625 *R. Canada*, in English at 0830.
- 10135 *Voice of Vietnam, Hanoi* at 1030.
- 11745 *HCJB, Quito, Ecuador* in English at 0530.
- 11875 *Radio Japan*, in English at 0930.
- 11890 *FEBC, Manila* in English at 0935.

Simon Wormleighton and "J. P." Fletcher have returned to school in Cirencester and send the following log using an impressive line-up of equipment (Heathkit SW717 with 35ft wire; Astrad-Altair with 150ft wire and HRO with 8 metre folded dipole):

- 6090 *R. Luxembourg* in German at 1130.
- 7095 *R. Pakistan* in English at 1820.
- 9770 *ORF, Vienna* in German at 1200.
- 11705 *Kol Israel* in English at 2000.
- 15012 *Voice of Vietnam, Hanoi* at 1800.
- 15155 *RSA, South Africa*, in Dutch at 1700.
- 15185 *R. Finland* in English at 1820.
- 17920 *R. Cairo, U.A.R.* in English at 1405.

A gentleman from Northville Road, Bristol who remains anonymous as there is no name on his letter used his CR100 (Modified) and 150ft long-wire to hear:

- 5930 *R. Prague, Czechoslovakia* at 1930.
- 5995 *VOA, Tangier* noted at 2130.
- 6005 *R. Berlin Int.* in English at 1735.
- 6155 *ORF, Vienna* in English at 1830.
- 6190 *Vatican Radio* noted at 2000.
- 7065 *R. Tirana, Albania* at 2210.
- 7110 *VOA, Rhodes* noted at 2125.
- 7275 *RAI, Rome* in English at 1920.
- 9735 *TWR, Monte Carlo* noted at 0915.

Paul Broadhurst from Clevedon in Somerset obtained a Trio 9R59-DS three weeks before sending in this report which is the result of those three weeks of listening. The antenna was a 150ft long wire.

- 5930 *R. Prague, Czechoslovakia* at 1915.
- 6020 *R. Kiev* in English at 1932.
- 6025 *R. Portugal* noted at 2105.
- 6050 *RAI, Rome* in English at 1930.
- 6065 *R. Sweden* in English, at 1600.
- 6070 *R. Sofia, Bulgaria* noted at 1930.
- 6150 *R. Belgrade, Yugoslavia* at 2010.
- 6165 *Swiss Broadcasting Co.*, English at 1330.
- 6190 *Vatican Radio* in English at 2050.
- 7220 *R. Budapest, Hungary* noted at 1630.

Richard Starkey of Southampton is another reader with a new receiver, this time a Vega VEF 206. Using only the built-in telescopic aerial Richard heard the following stations:

- 5930 *R. Prague, Czechoslovakia* at 1900.
- 6025 *R. Budapest, Hungary* in English at 2300.
- 6065 *R. Sweden* in English at 2100.
- 6100 *R. Belgrade, Yugoslavia* at 2000.
- 9625 *R. Canada Int.* in English at 2100.
- 11740 *AFRTS, U.S.A.* in English at 1900.
- 11970 *RSA, South Africa* in English at 1900.

MEDIUM WAVE BROADCASTS by CHARLES MOLLOY

FROM Orkney, G. M. Christie reports hearing BBC Radio London on 1457kHz and IBA Radio Clyde 1151kHz at good strength but subject to fading. He remarks how surprising it is to hear local stations at such a distance. This of course highlights the attraction of medium wave DXing. The majority of medium wave stations serve areas limited by the ground wave (daylight range) but after dark signals can be propagated by skywave far beyond the service area to be picked-up, when conditions are favourable, by 'eavesdroppers' thousands of miles away.

F. F. Wildman (Bournemouth) has been listening to the "As it Happens" programme broadcast by CBA Moncton N.B. in Canada on 1070kHz between 2300hrs and midnight GMT. Using his Codar CR70A receiver with the *Practical Wireless* Medium Wave loop antenna he has logged WNEW 1130kHz in New York City; CHER in Sydney, Nova Scotia on 950kHz and WCBS also in NYC on 880kHz.

W. Pennington (Grimethorpe, Yorks) sent in an excellent log of North American DX using his Trio 9R59DS receiver and 25ft outdoor aerial. Canadians heard include CKCM Grand Falls, Newfoundland on 620kHz; CBN St John's Nfld on 640kHz; CJOX Grand Bank, Nfld 710kHz; CJON St John's on 930kHz; CHNS Halifax N.S. on 960kHz; CFRB Toronto on 1010kHz; CBA Moncton N.B. on 1070kHz. From the United States WHDH Boston on 850kHz; WCBS 880kHz; WINS 1010kHz; WHN 1050kHz and WNEW 1130kHz, the last four being in New York City. Reception was between 2300hrs and midnight in January but it is possible to hear these stations

in March and April from approx. 0100hrs GMT until sunrise.

Ed Baker brought along his Eddystone EB35 when he went on holiday to Majorca and he hooked onto the hotel heating pipes for an aerial. On the Long Waves Azilal, Morocco 209kHz and Tipaza, Algeria 251kHz were heard during daylight together with medium wave outlets in Algeria on 548kHz, 890kHz, 980kHz and 1421kHz. After dark, Caltanissetta, Sicily was heard on 566kHz; Cagliari, Sardinia on 1061kHz; Libya on 1124kHz and 1250kHz. Ed has been interested in MW DXing since 1962 and has received verifications from MW stations in 136 countries.

Simon Hockenhall (Helston, Cornwall) has an HMV 4-band receiver and a 60ft longwire antenna. He reports afternoon reception on the long waves of Motala, Sweden on 191kHz and Azilal, Morocco on 209kHz. On the medium waves Oviedo, Spain 548kHz; Cork, Eire 1250kHz and Nice, France 1554kHz were heard. John Thorburn (Glasgow) used a Vasco Radio with internal ferrite aerial to log BBC R. Merseyside 1484kHz; R. Bristol and R. Teesside on 1546kHz; Tunis on 629kHz; Cairo, Egypt 773kHz; Lisbon, Portugal 755kHz. Philip Allott (Knaresborough, Yorks) has an HRO receiver with vertical antenna and has picked-up BBC local stations at Blackburn 854kHz; Sheffield 1034kHz; Leeds 1106kHz; Stoke 1502kHz; Nottingham 1520kHz; Teesside 1546kHz.

Richard Buckby of BBC Radio Derby sends details of the transmitter operating on 1115kHz (269m). The temporary caravan transmitter is situated at the village of Burnaston, between Derby and Burton and runs 500W into a 110ft vertical mast. Reception reports are welcome and should be sent to Richard at BBC Radio Derby, St Helen's Street, Derby, DE1 3HY.

VHF/FM DXING

by SIMON DAVID

MUCH as I dislike saying this, some of you really are not trying hard enough. Often the cry comes up that you can get BBC programmes but no continentals and, in the south not a good IBA station. This is incredible for the Greater London area and home counties readers who write to me.

Success depends on a combination of factors including tuner sensitivity, aerial used, the nature of the terrain between aerial and transmitter, the rotational direction that achieves maximum pick-up by the aerial, atmospheric conditions. *Practical Wireless* has published considerable information recently to help which I recommend to all DXers of FM.

In the February issue, my article mentioned details of an aerial I have tried. One important aspect in its characteristics was uniformity of loading impedance over a broad band of the FM scale involving broadcast programmes. Without this inbuilt factor in the aerial design, the aerial is usually designed to tune at one frequency, the response tailing off slightly on either side.

This is usually the cause of noisy reception and lower levels at extreme ends, i.e. the 89MHz and 97MHz extremes. Since BBC Radio 2 and the L.B.C. programmes are near these frequencies their signal strength and/or noise will be inferior unless a broad-band near perfect match aerial is employed, such as the Antiference FM263T, 264T and 266T or the equivalents by other manufacturers.

Having fitted such an aerial, then you stand a

better chance of picking up the French stations I mentioned, although weak stations may still be subject to fading and drifting.

Many of you in Northern districts and in Scotland have some difficulty because of the hilly country but it should be possible to receive something, if your aerial is aimed in the right direction with reflector behind the dipole. You could try picking up Irish stations (in the north-west and Wales) and local BBC radio stations up to about 200 miles away. For those of you near the east coast from Aberdeen right down to Kent, you could try for stations in Scandinavia, Holland and Belgium.

Here are some stations to aim at: Oslo 88.65MHz, Bokn 93.5MHz (both Norway); Roermond 88.2MHz(s), 90.9MHz(s), 94.5MHz, all Netherlands; Aalter (Belgium) 90.4MHz, broadcasting the Dutch Network. Mild weather conditions and high humidity should help you.

Let me know how you get on and I will include your results in my article. In the meantime my thanks to the following readers, among others, who have written to me on subjects related to this article. H. Lincoln of Enfield also comments on the effects of mains voltage reductions; S. A. Logier of Belfast has just taken up DXing on retirement; N. S. Gonzales of Chiswick, London, wants less noise, particularly from disc jockeys.

Finally, some details on IBA developments; the following commercial stations are expected to go on the air in 1974, most frequencies to be announced: Birmingham (Feb.), Manchester (March/April), Swansea (summer), Tyneside Wearside (summer), Edinburgh and Liverpool in late '74.

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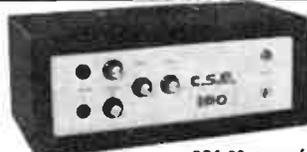
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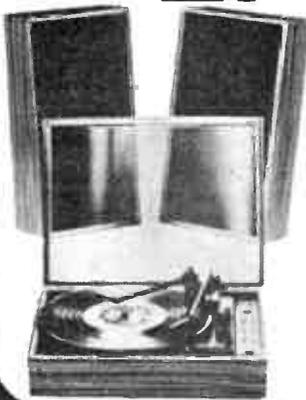
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Controls Volume, manual tuning and five push buttons for station selection, illuminated tuning scale covering full medium and long wave bands.

Size Chassis 7 ins. wide, 2 ins. high and 4 1/8 ins. deep approx.

Remember! one of the Top Ten Accessory Awards from Motor magazine PUSH BUTTON* CAR RADIO KIT

NOTE: The ability to solder on a printed circuitboard is necessary to complete this kit successfully. Circuit diagram and comprehensive instructions 55p. free with kit.

Car Radio Kit

£6.60 + 55p. postage & packing.

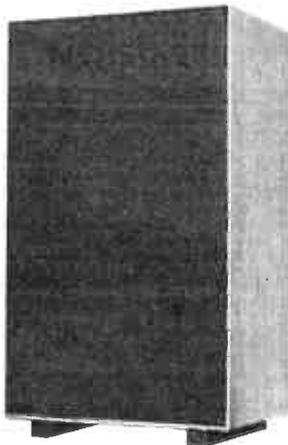
Speaker including baffle and fixing strips

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Recommended Car Aerial - fully retractable and locking.

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THE ULTIMATE COMPLETE SPEAKER SYSTEM EMI LE 315



Recommended retail selling price, £86.00.

Our price £45.00 +
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A professional standard five way speaker system with enclosure giving top quality performance.

Enclosure Dimensions approx. (3ft. x 2ft. x 1ft.).

Drive Units

Hand built - 15" diameter bass with 3" voice coil, - two 5" diameter Mid Range units,

- two 3 1/4" HF. units, plus matching crossover panel with two variable potentiometers for mid and high frequency adjustment.

Powder Handling

Continuous rating 35 W rms., Peak power rating 70 W.

Frequency Response 20 Hz 20,000 Hz.

EMI SPEAKERS FANTASTIC REDUCTION



15" 14A/780. Bass unit on a rigid diecast chassis. Superior cone material handles up to 50 watts RMS, and is treated to give a smooth frequency response. Resonance 30 Hz. Flux density 360,000 Maxwells. Impedance at 1 kHz is 8 ohms. 3" voice coil.

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950 Kit - Five matched speakers and crossover unit for handling up to 45 watts, frequency response from 20 to 20,000 Hz.

Huge 19" x 14" (approx.) high efficiency Bass-Speaker with 16,500-gauss magnet built on a heavy diecast frame.

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Gauss 14,000
Voice Coil Diam. 1 1/2 in
Fitted Tweeter Cone
Range 50-15,000 Hz
Rec. Retail Price



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12" 100 Watt 3" Pole Diam.

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Gauss 15,000
Voice Coil Diam. 2 in
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AN ALL PURPOSE UNIT OF HIGH sensitivity
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VA (watts)	Ref.	Cased	Open	£
60	149	—	£ 8.40	0.38
100	150	—	8.80	0.52
200	151	£ 9.20	8.80	0.52
250	152	11.18	8.70	0.65
350	153	13.00	10.40	0.82
500	154	14.83	12.00	1.00
1000	156	28.22	24.97	1.20
2000	158	55.90	50.40	—
3000	159	78.00	65.90	—

12 & 24 Volts Prim. 200-240V.

Amps	Type	No.	Price	P & P
0.3	0.15	242	1.22	0.22
0.5	0.25	111	1.22	0.22
1	0.5	213	1.45	0.22
2	1	71	1.90	0.22
4	2	18	2.50	0.38
6	3	70	3.24	0.42
8	4	108	3.60	0.52
10	5	72	4.25	0.52
12	6	116	5.18	0.52
16	8	17	6.04	0.52
20	10	115	9.30	0.69
30	15	187	15.50	0.97
40	20	252	18.60	1.00
60	30	226	20.50	1.10

30 Volts

Prim. 200-240V. Sec. 12, 15, 20, 24, 30V.		Price		P & P
Amps	Type	£	£	£
0.5	112	£1.44	£0.22	0.38
1	79	2.00	0.38	
2	3	2.90	0.38	
3	20	3.60	0.42	
4	21	4.25	0.52	
5	51	5.28	0.52	
6	117	6.30	0.52	
8	88	8.18	0.67	
10	89	10.00	0.67	

50 Volts

Prim. 200-240V. Sec. 19, 25, 33, 40, 50V.		Price		P & P
Amps	Type	£	£	£
0.5	102	£1.92	£0.30	0.38
1	103	2.80	0.38	
2	104	3.90	0.42	
3	105	5.25	0.52	
4	106	6.80	0.52	
8	107	10.00	0.67	
8	118	12.90	0.97	
10	119	16.00	0.97	

60 Volts

Prim. 200-240V. Sec. 24, 30, 40, 45, 60V.		Price		P & P
Amps	Type	£	£	£
0.5	124	£1.92	£0.38	0.38
1	126	2.70	0.38	
2	127	4.25	0.42	
3	125	6.50	0.52	
4	123	8.50	0.67	
5	40	10.50	0.67	
6	120	12.34	0.82	
8	121	14.58	1.00	
8	122	17.65	1.00	
12	189	19.68	1.10	

MINIATURE AND EQUIPMENT

Prim. 240V with screen.		Miliamps		Type	Price	P & P
Volts		Sec. 1	Sec. 2	No.	£	£
Sec. 1	Sec. 2	200	—	238	1.12	0.10
0-0.3	0-6	500	500	234	1.30	0.10
0-6	0-6	1000	1000	212	1.58	0.22
9-0 1/2	—	100	—	13	1.12	0.10
0-9	0-9	330	330	235	1.30	0.22
0-8-0	0-8-9	500	500	207	2.04	0.30
0-5-0	0-8-9	1000	1000	208	2.76	0.40
15-0-15	—	40	—	240	1.12	0.10
0-15	0-15	200	200	236	1.80	0.10
20-0-20	—	30	—	241	1.12	0.10
0-20	0-20	150	150	237	1.30	0.10
0-15-20	0-15-20	500	500	205	2.70	0.38
0-20	0-20	300	300	214	1.60	0.22
0-20	—	3500	—	1116	3.00	0.40
20-12-0-12-20	—	700 (D/C)	—	221	1.41	0.30
0-15-20	0-15-20	1000	1000	206	8.80	0.38
0-15-27	0-15-27	500	500	203	2.80	0.38
0-15-27	0-15-27	1000	1000	204	2.85	0.38

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6 1/2" 8 ohm, 10 watt	2-70		ADAstra 10" 8 or 15 ohm,	..	3-05
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Dualcone	..	1-60	P. & P.	..	10

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Cone Tweeter 8 or 15 ohm,	..	2-40	Crossovers CN23 (3 ohm),	..	1-05
10 watt	..	2-40	CN28 (8 ohm), CN216 (16	..	1-10
Cone Tweeter 8 ohm, 3 watt	1-40		ohm)	..	1-05
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metal	..		(2-5 & 3-5mm J/Ply)	..	
UD130 50K/600 ohm, uni-dir	..		P. & P.	..	
ball metal	

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BATTERY ELIMINATORS		£			£
240v Input 6, 7-5 or 9 300mA	..	2-20	lighter socket) 6, 7-5 or 9	..	2-20
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Spirit Lever	..	46	50p		
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2 1/2in x 5in	26p	23p	19p
3 1/2in x 3 1/2in	26p	23p	—
3 1/2in x 5in	30p	30p	22p
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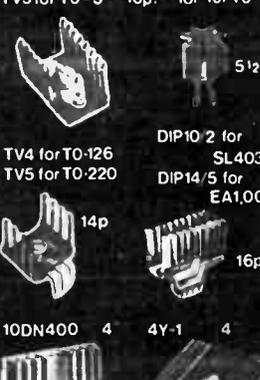
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DIP10/2 for SL403D
DIP14/5 for EA1,000

10DN400 4 46p, 4Y-1 4 35p

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P I V	1 amp	R M S	2 amp
100V	20p	50V	35p
200V	22p	100V	40p
600V	25p	200V	45p
1000V	38p	400V	50p

RECTIFIERS

P I V	1 amp	3 amp
50	1N4001 6p	1N5400 15p
100	1N4002 7p	1N5401 16p
200	1N4003 9p	1N5402 17p
400	1N4004 9p	1N5404 22p
600	1N4005 11p	1N5406 26p
800	1N4006 13p	1N5407 30p
1000	1N4007 16p	1N5408 33p
BY100	16p	BY133 23p
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Rating	Type	Tolerance	Range	Price Each	
1/2 watt	Carbon Film	± 5%	E12 Series	5Ω to 330KΩ	1p
1 watt	Metal Oxide Film	± 2%	E12 Series	10Ω to 1MΩ	4p
1/2 watt	Cormet Thick Film	± 2%	E12 Series	56Ω to 150KΩ	8p
1/2 watt	Carbon Film	± 5%	E24 Series	10Ω to 10MΩ	1p
1/2 watt	Carbon Composition	± 0.5Ω	(2 2Ω) 2 7Ω 3 3Ω 3 9Ω 4 7Ω	4p	
1 watt	Carbon Composition	± 10%	(5 6Ω) 6 8Ω 8 2Ω	5p	
1 watt	Carbon Film	± 5%	E12 Series	10Ω to 10MΩ	3p
2 watt	Carbon Film	± 5%	E12 Series	10Ω to 10MΩ	6p
2 1/2 watt	Wire Wound	± 10%	E12 Series	0.22Ω to 0.47Ω	10p
2 1/2 watt	Wire Wound	± 5%	E12 Series	1Ω to 270Ω	10p
5 watt	Wire Wound	± 5%	~E12 Series	0.5Ω to 8.2KΩ	10p
10 watt	Wire Wound	± 5%	10KΩ 15KΩ 20KΩ 25KΩ	11p	
10 watt	Wire Wound	± 5%	10KΩ 15KΩ 20KΩ 25KΩ	17p	
15 watt	Wire Wound	± 5%	10KΩ to 16.8KΩ	13p	

DISCOUNTS 10% on any 100 or more mixed value or wattage. 25% on any 100 or more same value and same wattage

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AC10*	18p	ASY25	33p	BC328	24p	BF180	33p	BSY95A	14p	T1P41A	8p
AC125	13p	BC17	11p	BCV70	17p	BF181	33p	BU105	£1-75	T1P42A	8p
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AC129	13p	BC109	11p	BC210	28p	BF185	28p	D13V	35p	T1S43	36p
AC175	15p	BC114	15p	BC211	28p	BF194	15p	MJ4000	£1-49	T1S91	31p
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AC187K	22p	BC147	20p	BD124	82p	BF196	37p	MJE340	52p	2N706	13p
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ACV19	25p	BC157	15p	BD131.2	£1-18	BF200	27p	MPF102	27p	2N1302	22p
ACV20	25p	BC158	12p	BD133	72p	BF214.9	27p	MPF103	41p	2N1303	25p
AD140	48p	BC159	14p	BD135	42p	BF262	25p	MPF104	45p	2N1305	24p
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AF126	27p	BC187	27p	BF160	25p	BFY51	22p	OC83	25p	2N4295	46p
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AF130	25p	BC213L	13p	BF173	24p	BR100	43p	OC170	28p	2N4295	18p
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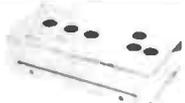
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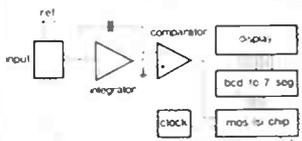
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ZTX213	14p	ZTX331	16p
ZTX214	15p	ZTX341	22p
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ZTX301	13p	ZTX551	17p
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1.5							61p	61p	61p	
2							61p	61p	61p	
2.2							61p	61p	61p	
3							61p	61p	61p	
3.3							61p	61p	61p	
4							61p	61p	61p	
6							61p	61p	61p	
6.8							61p	61p	61p	
8							61p	61p	61p	
10							61p	61p	61p	
15							61p	61p	61p	
22							61p	61p	11p	24p (16µF)
33		61p	61p	61p	61p	61p	61p	61p	33p (32µF)	
47		61p	61p	61p	61p	61p	61p	61p	25p (30µF)	
68		61p	61p	61p	61p	61p	61p	61p	25p	
100		61p	61p	61p	61p	61p	61p	61p	25p	
150		61p	61p	61p	61p	61p	61p	61p	25p	
220		61p	61p	61p	61p	61p	61p	61p	31p	
330		61p	61p	61p	61p	61p	61p	61p	47p	
470		61p	61p	61p	61p	61p	61p	61p	47p	
680		8p	10p	11p	14p	20p	25p	47p	59p	
1000		13p	14p	14p	19p	22p	25p	44p	79p	
1500			18p	19p	25p	39p	44p	79p	149p	
2200			18p	24p	24p	39p	44p	79p	149p	
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12" 8 ohm, 20 watt	5.75
12" 8 ohm, 20 watt	1.40
12" 8 ohm, 20 watt	1.40

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10 watt	
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G850	2.95

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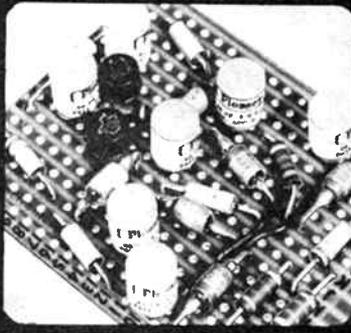
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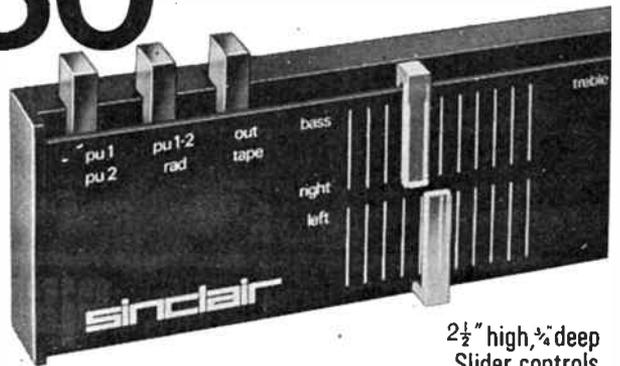


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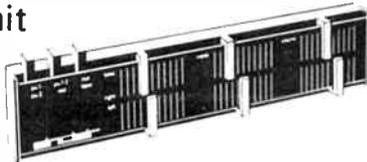
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2½" high, ¾" deep
Slider controls
New circuitry

Stereo 80 pre-amplifier and control unit

Each channel has independent tone and volume slider controls enabling exceptionally good environmental matching to be obtained. A virtual earth input stage forms part of the up-dated circuitry which includes generous overload margins. Clear instructions with template are supplied.

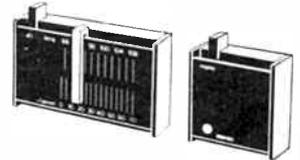


Size - 260 · 50 · 20mm (10½ · 2 × ¾ ins)
Inputs - Mag. P.U. 3mV RIAA corrected, Ceramic P.U., Radio, Tape
S/N ratio - 60dB
Frequency range - 10Hz to 25KHz - 3dB
Power requirements - 20 to 35 volts
Outputs - 100mV + AB monitoring for tape
Controls - Press button for tape, radio and P.U. Sliders for Volume, Bass and Treble

R.R.P. £11.95 +£1.19 V.A.T.

Project 80 FM-tuner and stereo decoder

FM Tuner
Size - 85 × 50 × 20mm
Tuning range - 87.5 to 108 MHz
Detector - I.C. balanced coincidence
AFC - Switchable
One 26 transistor I.C.
Twin dual varicap tuning
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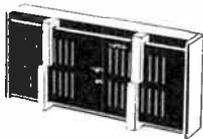


Decoder -
With gallium arsenide tuning beacon and 19-transistor I.C.
Size - 47 × 50 · 20mm

FM tuner R.R.P. £11.95 +£1.19 V.A.T.

Decoder R.R.P. £7.45 +0.45p V.A.T.

Project 80 active filter unit



Size - 108 · 50 · 20mm (4¼ · 2 · ¾ ins)
Voltage gain - minus 0.2dB
Frequency response - 36Hz to 27KHz, controls minimum
Distortion - at 1KHz 0.03% using 30V
HF cut off (scratch) 22KHz to 5.5KHz, 12dB/oct slope
L.F. cut off (rumble) - 78dB at 20Hz, 9dB/oct slope

R.R.P. £6.95 +0.69p V.A.T.

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Z.40
Size - 55 · 80 · 20mm
Input sensitivity - 100mV
Output - 15W RMS continuous 8 Ω (35V).
Frequency response - 10Hz 100KHz ± 1dB
Signal to noise ratio - 64dB
Distortion - less than 0.1% at 10W into 8 Ω
Power requirements - 12-35 volts

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Size - 55 × 98 × 20mm
Input sensitivity - 100-250mV
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Distortion - typically 0.03%
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H8/3	3µF	50V	4p	H7/8	125µF	16V	5p
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H8/9	20µF	6V	2p	H7/14A	220µF	16V	6p
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H8/10	22µF	50V	4p	H7/15A	220µF	35V	16p
H8/10A	22µF	100V	4p	H6/1A	250µF	4V	3p
H8/11	25µF	12V	4p	H6/2	250µF	25V	3p
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H8/12	32µF	1.5V	4p	H6/4	320µF	16V	4p
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H8/14A	40µF	16V	4p	H6/8	470µF	25V	10p
H8/15	47µF	50V	4p	H6/8A	470µF	35V	20p
H8/15A	40µF	35V	4p	H6/9A	400µF	40V	20p
H7/1	50µF	6V	3p	H6/13A	1000µF	25V	16p
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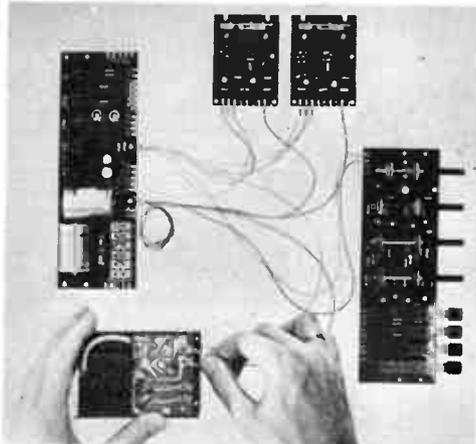
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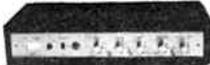
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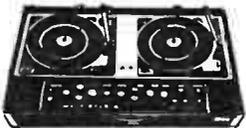


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