

EXPERIMENTAL MICROPHONES

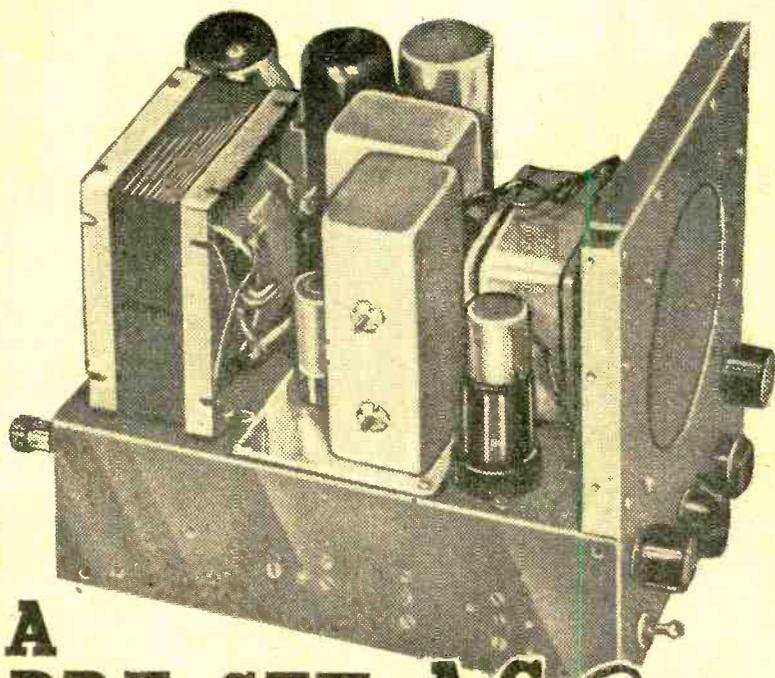


Vol. 30 No. 571

MAY, 1954

EDITOR:
F.J. GAMM

PRACTICAL WIRELESS



A
PRE-SET A.C. Receiver

RADIO COMPONENTS
EXHIBITION
CROSS-OVER NETWORKS
AUDIO AMPLIFIER DESIGN

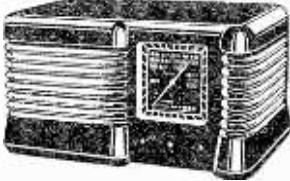
IN THIS ISSUE:

MODEL-CONTROL RECEIVERS
THE FIRST TWELVE YEARS
KLYSTRONS SIMPLIFIED
INTERFERENCE SUPPRESSION

CABINET as illustrated, 11 1/2 x 6 1/2 x 5 1/2 in. in walnut or cream, complete with T.R.F. chassis, 2 waveband scale, station names, new waveband, backplate, drum, pointer, spring, drive spindle, 3 knobs and back. 22/6. P. & P. 1/36.

As above with Superhet Chassis 23/6. P. & P. 1/36.

As above complete with new speaker to fit and O.P. trans., 35/- P. & P. 1/36 with Superhet Chassis 36/- P. & P. 1/36.



Used metal rectifier, 250 v. 50mA., 4/6; range with trimmers, 6/6; M. & L. T.R.F. coils, 5/-; 3 Govt. valves, 2/- hand circuit, 6/6; heater trans., 6/-; volume control with switch, 3/6; wave-change switch, 2/-; 32 x 2 mfd., 4/-; bias, condenser, 1/-; resistor kit, 2/-; condenser kit, 4/-.

M & L Superhet Coils with circuit, 6/6; iron cored 465 LF's, 7/6; min. gang, 5/6; volume control with switch, 4/-; wave-change switch, 2/6; heater trans., 7/6; 4 v. h., 1/6; 1 1/2 Govt. valves, metal rectifier and Ntd. diode with circuit, 14/6; 25 x 25 mfd., 1/-; 16 x 16 mfd., 3/3; condenser kit (17), 7/6; resistor kit (14), 3/6.

Used 5 valve A.C. mains 250 250 3-waveband superhet. Complete in outstanding walnut cabinet, size 22 x 14 x 10 1/2 in. Valve line up: 6X8, 6X7, 6B6G, 6F6 and U50 rec. 8in. P.M. speaker. In first class working order. £7 19/6. P. & P. 12/6. We have a few of these in A.C. D.C., price as above.

All day A.C. mains battery unit, 200 250 v. Metal case size 8 x 7 x 3 in., by famous manufacturer incorporating Westinghouse metal rectifiers, 3 500 mfd. 16 21 mfd. mains trans., 3 smoothing chokes, output 60 v., 10 mA., 1.4 v., .25 amp. P. & P. 24/- 39/6.

COMPLETELY BUILT SIGNAL GENERATOR

Coverage 120 Kc-820 Kc/s., 300 Kc-s., 900 Kc/s., 900 Kc-s., 2.75 Mc-s., 2.75 Mc-s., 8.5 Mc-s., 8.5 Mc-s., 25 Mc-s., 17 Mc-s., 50 Mc-s., 25.5 Mc-s., 7 Mc-s. Metal case 10 x 6 x 4 1/2 in., size of scale of 1 x 1 in., 2 valve sand rectifier, A.C. mains 250 250 v., internal modulation 400 c.p.s. to a depth of 40%. Modulated or unmodulated R.F. output continuously variable 100 millivolts. C.W. and mod. switch, variable A.F. output and moving coil output meter. Black crackle finished case and white panel. £4 19/6. P. & P. 4/-.

Used resistance and capacity bridge in leatherette covered case, with carrying handle, size 12 x 8 1/2 x 6 1/2 in., 10 pf. to 100 mfd. in 3 ranges, 1 to 10 meg., 3 ranges, power factor check 200, 300, 400 and 500 volts flash test. Magic eye, rectifier and triode. These require re-checking. £3 19/6. P. & P. 1/-.

High impedance plastic recording tape by famous manufacturer, 1,200 feet complete on spool, 17/6. P. & P. 1/6. 600 feet 8/- P. & P. 1/-.

Amplifier Case, black roxine covered, leather carrying handle, chrome plated corners, rubber feet, felt lined, detachable lid. External dimensions 13 1/2 x 13 1/2 x 9 1/2 in. £1. P. & P. 2/6.

Pr. 200 250 v., secondary 3, 4, 5, 6, 8, 9, 10, 12, 15, 18, 20, 24 and 30 volt at 2 amps., 13/-.

Terms of business: Cash with order. Dispatch of goods within three days from receipt of order. Where post and packing charges are not stated, please add 1/- up to 10/-, 1/6 up to £1. and 2/- up to £2. All enquiries and list, stamped addressed envelope.

Drop thro' 260-0-260, 200 mA. 6v 5 amps., 5 v. 3 amps. 27/6.

Heater Transformer. Pri. 230-250 v. 6 v. 11 amp., 6 v. 2 v. 21 amp., 5 - 2, 4 or 6 v. at 2 amps., 7/6; 2 v. 21 amp 5/- P. & P. 1/36.

R.F. MAINS TRANSFORMERS, filament mounting, float and voltage parcel. Basis-nials 250 250.

300-0-300 80 mA. 6.3 v. 1 a., tapped at 4 v. 6.3 v. 2 a. tap 4 v. 13/6.

350-0-350 75 mA. 6.3 v. 3 a. tap 4 v. 6.3 v. 1 a. 13/6.

350-0-350 70 mA. 4 v. 5 a. 4 v. 2.5 a., C.T., 18/6. P. & P. on the above transformers 2/-.

500-0-500 125 mA. 6.3 v. C.T. 4 a. 6.3 v. C.T. 2 a. 5 v. C.T. 2 a., 27/6.

500-0-500 120 mA. 4 v. C.T. 4 a. 4 v. C.T. 1 a. 4 v. C.T. 2.5 a., 27/6.

500-0-500 250 mA. 1 v. C.T. 5 a. 1 v. C.T. 3 a. 3 v. C.T. 1 a., 33/6.

P. & P. on the above transformers 3/-.

32 mfd., 350 wkg. 2/-

16 x 24 350 wkg. 4/-

1 mfd., 200 wkg. 1/3

10 mfd., 450 wkg. 3/6

16 x 8 mfd., 500 wkg. 4/6

14 x 16 mfd., 500 wkg. 5/9

8 x 16 mfd., 450 wkg. 3/9

12 x 32 mfd., 350 wkg. 4/-

42 x 32 mfd., 350 wkg. and 25 mfd., 25 wkg. 6/6

25 mfd., 25 wkg. 11d.

250 mfd., 12 v. wkg. 1/3

16 mfd., 500 wkg., wire ends 3/3

8 mfd., 500 v. wkg., wire ends 2/6

8 mfd., 350 v. wkg., tag ends 1/6

70 mfd., 25 v., wkg., wire ends 1/9

100 mfd., 350 wkg. 4/-

100 + 200 mfd., 450 wkg. 9/6

16 x 16 mfd., 350 wkg. 3/3

Ex Govt. 8 mfd., 500 v. wkg. size 3 1/2 x 1 1/2 for 2/6

60 + 100 mfd., 280 v. wkg. 7/-

16 x 16 mfd., 350 wkg. 6/-

50 mfd., 180 wkg. 1/9

65 mfd., 220 wkg. 1/6

8 mfd., 150 wkg. 1/6

60 100 mfd., 280 wkg. 8/6

50 mfd., 12 wkg. 11d.

32 x 32 mfd., min., 275 wkg. 4/-

50 mfd., 50 wkg., 8 mfd., wkg., wire ends 1/9

Miniature wire ends moulded 100 pt., 300 pt., and 400 pt. 7d.

Fully shrouded mains transformer, input 200 250 secondary 350-0-350 175 mA. 6.3 v. 7 amp., 5 v. 3 amp., p p 3 - 35/-

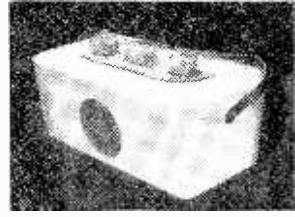
Fully shrouded pushpull transformer, Pri. 6,000 ohms, SEC 15 ohms, p p 2 - 20/-

Fully shrouded choke, 15 Hen. 180 mA., p p 2 - 15/-

Fully shrouded choke, 5 Hen. 120 mA., p p 1 - 8/6.

CONSTRUCTOR'S PARCEL, comprising chassis 12 1/2 x 8 x 2 1/2 in., cad. plated 18 gauge, v. h., 1F and trans, cut-outs, backplate, 2 supporting brackets, 3 waveband scale, new wavelength station names. Size of scale 1 1/2 x 4 1/2 in., drive spindle, 61m., 2 pulleys, pointer, 2 bulb holders, 5 paxolin international octal valve holders, 4 knobs and pair of 465 LF's, 16/6. P. & P. 1/9.

As ABOVE, but complete with 16 x 16 mfd. 350 wkg. and semi-shrouded drop thro' 250-0-250 80 mA. 8 v. 3 amp. Pri. 200-250, and twin-gang 31/6. P. & P. 3/-.



PERSONAL PORTABLE CABINET in cream coloured plastic, size 7 x 4 1/2 x 3 in. Complete 4-valve chassis. Scale and 3 knobs. Takes miniature 90 v. and 7 1/2 v. batteries, 10/- P. & P. 2/-.

3in. P.M. SPEAKER to fit above, 10-. Miniature output transformer, 5-. Miniature wave-change switch, 2-. Miniature 1-pole 4-way used as Volume and Off, 2-. 4 BTG valveholders, 2/4. Midret twin gang 3in. dia. 3in. long and pair medium and long-wave T.R.F. coils (in long x 1in. wide; complete with 4-valve all-dry mains and battery circuit, 9/6. Condenser Kit, comprising 11 miniature condensers, 2/6. Resistor Kit, comprising 15 miniature resistors, 4/6. 25 x 25 mfd. 16 P. & P. 2/6. Valves to suit above 10/- each. Point to Point Wiring Diagram 1-.



View of chassis as it would look when assembled with valves inserted.

Extension speaker cabinet, in contrasting walnut veneers size 15 x 10 1/2 in. Will take 6" or 8in. speaker, 17/6. P. & P. 2/-.

Volume Controls, Long spindle less switch, 50 K, 500 K, 1 meg., 2/6 each. P. & P. 3d. each.

Volume Controls, Long spindle and switch, 1, 1 and 2 meg., 4 each; 100 K, and 50 K, 3/6 each, 1 and 1 meg., long spindle, double pole switch, miniature, 5/- P. & P. 3d. each

Standard Wave-change Switches, 1-pole 3-way, 1/9; 5-pole 3-way, 1/9. Miniature 3-pole 4-way, 4-pole 3-way, 2/6.

Valveholders, Paxoline octal, 4d. Moulded octal, 7d. EF50, 7d. Moulded 67G, 7d. Loctal amphenol, 7d. Loctal pax., 4d. Mazda Amph., 7d. Mazda pax., 4d. 58A, 18A amphenol, 7d. BTG with screening can, 1/6. Duodecal paxolin, 9d.

Trimmers, 5-40 pf., 5d.; 10-100 10-250, 10-430 pf., 10d.

Twin-gang .0005 Tuning Condensers, 5/- With trimmers, 7/6.

Midret .00037 dust cover and trimmers, 8/6.

P.M. SPEAKERS with base trans. trans.
 3 1/2 in. 13/6
 5 in. 12/6
 6 in. 12/6
 6 in. 18/6
 10 in. 15/-
 10 in. 19/6
 Post and packing on each of the above, 1/6 extra.

Truxos BN11 12 in. P.M. 3 ohm speech coil, 45/- P. & P. 3/6.

Crystal pick-up with Sapphire Trailer Needle, with volume control, 23/- P. & P. 1/-.

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The 12AT7 is a very reliable frequency changer and is widely used in modern TV receivers, VHF and UHF communications equipment. It is also frequently employed in industrial equipment, computers, navigational aids and test equipment.

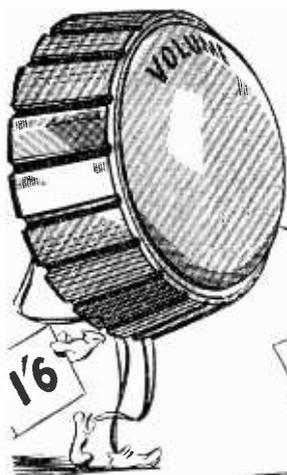
Use the BRIMAR 12AT7—with improved performance —at NO EXTRA COST
now is the time to



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12AT7	ECC31	B152 & B309	12AT7

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Sizes: Type "A" 1 3/8" dia. Type "B" 1 1/8" dia. Both types are 3/8" deep.

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AMPLIFIER: "Bass," "Treble" (plus any of above).
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SEPARATE COILS A full range is available for all popular wavebands and purposes. Fully descriptive leaflet and connection data available. Just note these 5 star features.

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- * Variable iron-dust cores. * Fitted tags for easy connection.
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RECEIVER 8A.
Channel checking Unit, working on 49-109 metres. Contains 5 VR91 (RF50), 1 VR8, 1 VR55 (FB33), 1 VR53 (RF80) Valves. Thermal switch breaking at 85 degrees F., etc., etc., in metal case 9 1/2in. x 7in. x 10in. Ask for P H477A. **29/6** Carriage 2/6 extra

POWER UNIT TYPE 266.
In Transit Case. Input 90 v. 1.5K c.p.s. A.C. Output 5 H.T. 120 v. D.C. bias 3 and 9 v. L.T. 2 v. Smoothed and stabilized. Complete with 5U4G valve VS110 stabilizer. 12 v. Ia metal rectifier, etc., etc., in attractive metal case with handles. Dim.: 11in. x 9 1/2in. x 7 1/2in. Ask for P H579. **22/6** Each Carriage Paid

GLASS DOME INSULATOR
With Threaded Terminal Top and Metal Lead-through Rod. Dome dim.: 2 1/2in. x 1 1/2in. high, lead-through projects 6 1/2in. Overall length 9 1/2in. Ask for P H54. **2/-** Each Post 3d. extra

CERAMIC AERIAL SPREADER
Individually boxed. Length overall 1 1/2in., between centres 9 1/2in. Ask for P H171R. **1/-** Per pair Post 3d. extra

EX-R.A.F. V.H.F. CONTROL PANEL TYPE 3A.
Input 24 volts. D.C. Intercom. Control contains 3 induction coils type 21A, 3 Retardation coils, Type 28A, 6 relays, type 26A tuning hand generator, Type 25 twin bell set, plus plugger key switches, key switches, panel indicator lamps, etc., etc. Panel finished grey with handles. Unit dim.: 19in. x 11in. x 9in. Ask for P H947. **21/-** Each Carriage Paid

BLACK PLASTIC CHAIN AERIAL INSULATORS.
comprising 3 links, 3 1/2in. long, 1 1/2in. wide, each link. Total length 7 1/2in. A.M. ref. 10A 125. Ask for P H323. **9d.** Per pair Post 2d. extra

AERIAL SYSTEM TYPE 62.
U.H.F. Antenna on streamlined moulding with VR92 (EA50) untuned detector stage. Overall dim.: 13in. x 4 1/2in. x 2 1/2in. Antenna 22.5 cm. Ask for P H496. **3/6** Each Post 9d. extra
Circuit 1/3 each.

WIRELESS REMOTE CONTROL UNIT D
No. 2, Mk. 2, ZA 20491. Wooden box 7 1/2in. x 8 1/2in. x 5 1/2in.; with hinged lid, containing 3 relays, 4 make, 500 ohms, 1 make, 30 ohms and H.D. double-coil type 1,750 ohms coil makes, 200 ohms coil breaks, plus QMB switch and 8 brass terminals. Ask for P H803. **7/11** Each Post Paid

SUPPRESSOR UNIT 5C 870.
Contains 4 P.F. chokes and 4 Tubular Condensers, 0.1 mfd., 250 v. D.C., carrying 5 amps. (2 sets on each lead), each choke and condenser separately screened in compartments of Aluminium Alloy Box 4 1/2in. x 4in. x 2 1/2in., 4 hole fixing. Ask for P H907. **2/6** Each Post 1/- extra

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T1154B TRANSMITTER UNIT in Transit Case. Ask for P E5A. **39/6** Each Carriage 7/6 extra
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RECEIVER UNIT TYPE 25
Ref. 10P IL. Part of TR1176. Range 4.3-6.7 mc/s. Ask for P H296. **35/-** Each Post Paid

WS-18 RECEIVER CHASSIS
with valves. Ask for P H22. **25/-** Each Post Paid
Circuit and Data 2/3.

WS-18 NMTR RECEIVER CHASSIS
partly stripped by the M.O.S. Ask for P H349. **33/6** Each Carriage Paid
Circuit 4/3.

RECEIVER CHASSIS
Range 150-200 mc s. Less valves. Ask for P H340. **21/-** Each Post Paid

28 WATT OUTPUT TRANSFORMER
Pameko type AF3091 IA. Mfg. surplus. Ask for P H565. **19/6** Each Post Paid

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- ★ Attractive New Cabinet.
- ★ Figured Walnut Veneered.
- ★ Size Approx. 10½" High, 10" Wide, 5" Deep.
- ★ Approx. Building Cost £7.10.0.

This is a Long-Medium Wave Receiver suitable for A.C. Mains 200/250 volts. Valve line up: 2. 6SG7, 6V6GT, 6X5GT. The Cabinet is of very attractive design and finished in light Walnut, with the sides and Dial surrounds in Peach. Only brand new components are used throughout the construction of this receiver, thus assuring a high degree of performance and reliability. All components required are available from stock.

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A new & manufactured range, fully guaranteed for 12 months.

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- 6 or 12 v. 3 amp. F.W. bridge type, at 12/6
- 6 or 12 v. 4 amp. F.W. bridge type, at 15/0
- 6 or 12 v. 6 amp. F.W. bridge type, at 23/6
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CHARGER TRANSFORMERS

High-grade. Wax-dipped. 220/240 v. input, 6/12 v. at 2 amp. output. Price 11/9 each. Also 6/12 v. at 4 amp. Price 17/6 each.

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Size: 6" High, 5" Wide and 4" Deep. Made from 20 Swg. Metal and spray finished in Black or Grey. Sides and Top louvred for ventilation. Front undrilled except for two outlet holes for L.T. Leads. Ideal for use with the above rectifiers and transformers. Price 9/- each.

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3-4 WATT AMPLIFIER

Suitable for A.C. Mains 210/230/250 v. Valve line up: 6F91, 6K6GT, 5Z4. Chassis size: 9" Long x 5" Deep. Overall height 6". Two controls, Volume On/Off, and Tone. High quality fully shrouded mains transformer fitted. Also screened P.U. Lead and O.F. Transformer. All components used are Brand-New, and are covered by the normal guarantee. This unit is ideal for use in constructing a low priced Record-Player. Price £7/10/-, plus 2/6 post and packing.

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OF EDUCATION
etc., etc.

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TEST PRODS with red and black leads. 2/- pair. P. & P. 6d.
TEST METER. 7 ranges as follows: 1.5 v. 3 v. 150 v. 6 ma., 60 ma., 5,000 ohms, 25,000 ohms, 2½ in. Dia. scale M.C. meter. Rotary selector switch, Black bakelite case, 6 x 4½ x 4½, fitted with removable lid, also provision for internal batts, ranges can be easily extended. Bargain Price, 30/- plus 1/6 post.
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SHADED POLE MOTORS for tape recorders or gram. units. With voltage tapping plate 200/250 volts, 3-hole fixing. Our price 12/6 ea. or 21/- pair. Post and pkg. on either, 1/6.
SPECIAL TRANSFORMER OFFER.—Pri. 115, 210, 240 v. Secs. 260/260 v. 100 ma., 6.3 v. 3 A. and 6.3 v. 1 A. for 6 x 5 rectifier. Universal mounting. Few only. 17/6 ea., post free.
CRYSTAL HAND MICROPHONES. High quality, very sensitive. Chrome finish, complete with screened lead and standard jack plug. Our price only 25/- ea. Few only.
Special Valve Offer. Kit of 4 midget valves 1.4 v. 1, each 155, 1R5, 1T4 and 154, 30/-, or 8/6 ea. separately. 607/3, 10/- ea. or 2 for 17/6. Most of the 1.4 v. B7G range available at 8/6 ea.
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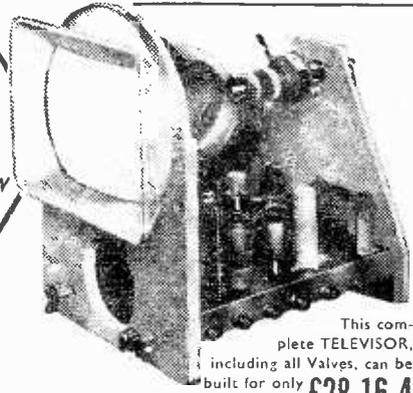
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 - Indicators, -ID17 APN3, ID18 CPN3, IC151, BC1152, I-8A, I-2A.
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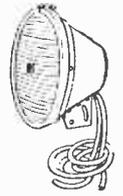
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POWER SUPPLY UNIT. 12/6 Ex No. 19 set. Z.A. No. 5108. New. 12v. in. two H.T. output at 275v. and 500v. Carriage 2/6.
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Practical Wireless

EVERY MONTH
VOL. XXX, No. 571, MAY, 1954

Editor: F. J. CAMM

22nd YEAR
OF ISSUE

COMMENTS OF THE MONTH

By THE EDITOR

Purchase Tax

THE Treasury has benefited by £28,000,000 extracted in purchase tax on radio receivers, radio gramophones and television receivers during the year which ended on March 31st. Purchase tax paid in the two previous years was £24,000,000 (1952/3) and £21,000,000 (1951/2). These figures reflect the rise in the sale of radio and TV sets. The former rose by 20 per cent. during the year to reach the grand total of 951,000 and TV by 44 per cent. to reach the record figure of 1,129,000. Export sales, however, fell by 26 per cent. and 16 per cent. respectively, although radio exports as a whole rose about 5 per cent. Thus radio and television sales show no real diminution, apart from seasonal variations. They are still the cheapest form of entertainment and, although it may be felt by some that purchase tax is another form of entertainment tax, it must be remembered that it is a non-recurring charge and, spread over say 5 years, it is still much less per pound than the tax which would be paid on cinema and theatre tickets.

Although the TV licence is being raised to £3 it will still be the cheapest form of visual entertainment in this country, and, with the exception of countries where there are only sponsored services, British television is probably the cheapest entertainment in the world.

The chief object of raising the licence is to improve the service and, therefore, it will tend to increase rather than decrease the sale of receivers. The commercial TV Bill makes it clear that the independent TV authority must radiate programmes predominantly British in tone and style, of high quality and well-balanced in subject matter.

THE RADIO SHOW

THE main feature at this year's Radio Show, which takes place from Aug. 25th to Sept. 4th, will again be electronics, with the purpose of demonstrating some of its many applications outside the field of domestic radio and television. They will be grouped under such descriptions as "Electronics in industry," "Electronics in medicine," etc. The exhibits will be of special displays made up for the occasion to demonstrate a principle and not any particular piece of production equipment: equipment of unusual interest taken from the production line, from

service or from development, and ready-made displays which have already been exhibited elsewhere. This journal will, of course, be represented there as in former years.

THE CABINET MAKER

ONE of the smallest trade associations is the British Radio Cabinet Manufacturers' Association. The cabinet which houses the set proper is seldom given a thought, but a great deal of design work is involved in its production. The external appearance of the cabinet has a great deal to do with sales. No matter how efficient the receiver itself may be it is often the external appearance of the magic box which influences its sale. The manufacturer must produce a variety of styles to match in with furnishing schemes, and he must co-operate with the set designer on matters of the position of the speaker grille, height of auto-record changer, location of knobs and dissipation of heat. The association has been in existence for 33 years, and in that time it has brought about radical changes in cabinet design. One has only to compare present cabinet styles and finishes with those of, say, 20 years ago to mark the change.

"THE PRACTICAL MOTORIST AND MOTOR CYCLIST"

AS announced last month, our new monthly *The Practical Motorist and Motor Cyclist* is now on sale. Published at 1s. on the 8th of each month, its contents are entirely devoted to the upkeep, overhaul, maintenance and repair of all types of motor vehicles—motor cars, motor cycles, and motorised bicycles, irrespective of the year of manufacture. Its policy in a word is Service! Service to its readers and the vehicles they run. As with all our companion practical journals there is a free reader service. Readers of the first two issues have the opportunity of entering competitions, each of which carries £250 as first prize. There is no entrance fee. The newcomer to our practical group covers entirely new ground in automobile journalism, and fills a need in these days when the high cost of repairs makes it more than ever necessary for the owner-driver to carry out his own repairs. Indeed, it is a fascinating hobby.—F. J. C.

ROUND the WORLD of WIRELESS

Broadcast Receiving Licences

THE following statement shows the approximate number of sound receiving licences issued during the year ended January, 1954. The grand total of sound and television licences was 13,315,969.

Region	Number
London Postal ...	1,637,592
Home Counties ...	1,440,448
Midland ...	1,256,676
North Eastern ...	1,636,248
North Western ...	1,276,775
South Western ...	1,008,953
Wales and Border ...	634,840

Total England and Wales	8,891,532
Scotland ...	1,101,926
Northern Ireland ...	216,867

Grand Total ... 10,210,325

New V.H.F. Transmitters

IN connection with their plans for the introduction of V.H.F. sound broadcasting in this country the BBC have placed an important order with Standard Telephones and Cables Limited for their latest type of frequency modulated V.H.F. broadcasting transmitters. The order calls for 12 10 kW

transmitters, type C.F.4, and 12 1 kW transmitters, type C.F.2.

The transmitters embody all the latest principles and practices of modern design. An important feature is an entirely new approach to the system of transmitter control ensuring the high standard of reliability essential to unattended remote-controlled operation. At each station twin transmitters will be used for each programme so that either transmitter can be switched off without interrupting the service.

Booking by Radio

PYE LIMITED of Cambridge are to supply radio for the first radio-equipped mobile ticket office in the world. This new idea will enable people going to football matches, race meetings or garden parties to book their theatre seats on the spot without going to the trouble of visiting agencies or theatres. Not only will the mobile van provide working people on their way to factories within the Greater London area with a prompt service, but it will also make it possible for early morning workers in Covent Garden, Smithfield and Billingsgate to obtain

tickets while they are actually at work in the markets.

The van, belonging to Keith Prowse, is to be in constant communication with a Poland Street control room which acts as a central clearing office for the whole of their network of ticket agencies.

Third Exhibition for Radio Amateurs

HUNGARY'S amateur radio fans will hold their third annual exhibition in May. Special interest is attached to this year's exhibition as the first experimental television broadcasts have already been started in Hungary.

Exhibitors, either individuals or amateur radio clubs, can send in their own products under five categories — receivers, aerials, measuring instruments, microphones and transmitters—and raw materials should preferably be of Hungarian origin to facilitate construction.

Commercial Telephone Service

THE only municipal telephone service in this country is to be found in Hull, where callers may ask to be connected with the city's amusement telephone service.

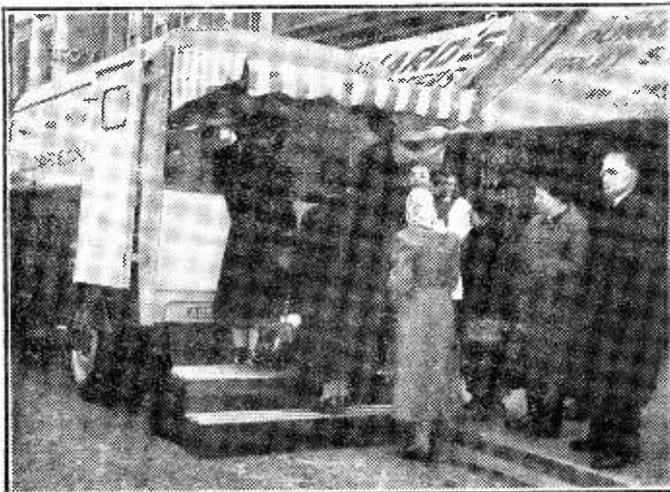
For only twopence they can hear Eddie Calvert's recording of "Oh Mein Papa," advertising a local music store, or listen to part of the sound track of the film showing at their favourite cinema. Normal calls also cost no more than twopence.

B.I.R.E.

THE following meetings will be held during April, 1954:—

London Section.—Wednesday, April 21st, 6.30 p.m., at the London School of Hygiene and Tropical Medicine, Keppel Street, Gower Street, W.C.1.—"Crystal Valves in Radio and Electronics." B. R. A. Bettridge (G.E.C. Ltd.).

South Wales Section.—Wednesday, April 7th, 6.30 p.m., at Glamorgan Technical College, Treforest.—"The Manufacture of Radio Receiving Valves." G. P. Thwaites, B.Sc. (S. T. & C. Brimar).



Shoppers queue to take advantage of the new Keith Prowse mobile booking office.

North-Eastern Section.—Wednesday, April 14th, 6 p.m., at Neville Hall, Westgate Road, Newcastle-upon-Tyne.—“Electroencephalography.” Prof. Alexander Kennedy, F.R.C.P., and J. W. Osselton, B.Sc. (Durham University—King’s College, Newcastle-upon-Tyne).

West Midlands Section.—Tuesday, April 27th, 7.15 p.m., at Wolverhampton and Staffordshire Technical College, Wulfruna Street, Wolverhampton.—“Radio Telephone Equipment.” T. C. Howell.

SOS and Police Messages

LAST year the BBC broadcast 426 SOS messages. Of those broadcast from London, 188 were successful, 82 unsuccessful and the result of 48 was not known. Of those from the Regions, 46 succeeded, 33 failed and the result of 29 was not known.

Of 334 police messages for witnesses of accidents, etc., 96 broadcast from London were successful and 111 unsuccessful; 44 from the Regions succeeded and 83 failed.

General Sales Manager

MR. C. L. G. FAIRFIELD, M.A., M.I.E.E., A.M.I.Mech.E., Barrister-at-Law, who joined the Telegraph Construction and Maintenance Co. Ltd., in April last as manager of their Overseas Division, has now been appointed general sales manager covering cables, plastics and engineering products.

Mr. E. H. Gosling, A.S.M.A., previously home sales manager of Telcon’s Cables Division, has been appointed home sales manager for these products.

Mr. A. W. Montgomery

MR. A. W. MONTGOMERY, joint general manager of Standard Telephones and Cables Ltd., has been elected a Fellow of the (U.S.) Institute of Radio Engineers for his leadership in radio and telecommunication research in England and his services in the international liaison in these fields.

International Training Centre

UNDER the American Mutual Defence Assistance Programme of foreign military aid, students from the Armed forces of America’s allies in Europe, Asia and South America are able to attend service schools primarily

intended for American servicemen only. One such training base is Keesler Air Force Station, Mississippi, where officers and enlisted men of fifteen friendly nations throughout the world study as electronics technicians.

At all times the foreign students are given every consideration and encouragement. If they encounter difficulties, not compensated for

A group of five students, from three different countries, are engrossed in the operation of a cathode-ray oscillograph during a class in electronics training at Keesler Air Force Base, Mississippi.



by the regular language classes, they are given additional assistance by qualified interpreters who can help with both language and technical problems.

Use of Electronic Valves

PARTS 1 and 2 of the British Standard Code of Practice on the use of electronic valves has now been published.

Part 1 gives general information and recommendations for all types of electronic valves, whilst Part 2 sets out additional recommendations on the use of domestic receiving valves, cathode-ray tubes and rectifiers.

The Code was prepared by a committee set up jointly by the Institution of Electrical Engineers, and the British Standards Institution. Copies of the Code CP. 1005 (Price 6/-) may be obtained from the British Standards Institution, 2, Park Street, London, W.1.

Improvement in Home Service Coverage

AS a further step in the plan to make local improvements in the coverage of the Home Service,

the BBC has installed a new low-power transmitter at its station at Whitehaven, Cumberland.

The new transmitter took over the service from the present temporary transmitter on Sunday, March 14. It has a power of 2 kW., four times that of the existing temporary transmitter, and it is expected that this will extend the area of improved reception as far

as Maryport and Cockermouth in the north and beyond Egremont in the south. Like the present temporary transmitter the new transmitter will radiate the North of England Home Service on 434 metres (692 kc.s).

200th “Ray’s a Laugh”

ON March 25th, just under five years after it first went on the air, “Ray’s A Laugh” reached its 200th programme. The original broadcast was on April 4th, 1949. There have been changes in form during that time but four of the cast who were in that first edition have been heard in every programme since. They are Ted Ray himself, Kitty Bluett, Patricia Hayes and Peter Sellers. George Inns, who devised the show, has been in charge throughout.

Morphy-Richards Ltd.

MORPHY-RICHARDS, LTD., announce that as from March 25th, their new London office address is 6, Conduit Street, London, W.1, to which all home and export sales and advertising enquiries should be addressed.

AMPLIFIER DESIGN

2.—BASIC CONSIDERATIONS—CONTINUED

By R. Hindle

(Continued from page 234, April issue)

IN order to make the input signal operate over the selected parts of the characteristic it is necessary to apply a grid bias and this is now determined by reading the voltage on the characteristic corresponding with the mid-point of the chosen section of the characteristic.

All operating details can now be filled in. The valve will operate with the H.T. supply voltage for which the curve has been prepared and with the anode resistor specified by the maker on the curve being used. The grid bias has been determined as above and the amplitude of signal was specified in the original design stipulation. The makers' characteristic graph will also give a curve of amplification factor for the same constants and from this μ is read for the set of working voltages chosen. This figure is now used in the formula for actual gain previously obtained, giving the voltage output signal that will be available. Before giving a practical example, however, there are some other considerations to refer to.

In actual practice, of course, these valve characteristics are never absolutely straight and, therefore, perfectly distortionless distortion can never be achieved. The deviation from true amplification is specified by quoting the percentage distortion, or more correctly the percentage that the amplitudes of the harmonics introduced as a result of the distortion bear to the amplitude of the total output signal. Valve makers commonly quote working constants for a distortion of 5 per cent. Often, of course, a much lower degree of distortion is required and in such a case the valve is worked well short of the specified signal amplitudes permissible for the 5 per cent. distortion condition. If a reduction in signal amplitude is not permissible the decrease in distortion can be obtained by increasing the H.T. voltage. Thus, the Brimar 6BS7 (triode connected) with an H.T. supply of 100 volts and an anode load of 200 K Ω gives a maximum peak output voltage of 26 with a stage gain of 13; this is for 5 per cent. distortion and if 26 volts output is essential the distortion will have to be tolerated. However, if the H.T. supply is increased to 300 the valve will

A short series of articles dealing with the theoretical considerations of amplifier design, and containing at a later stage constructional features of various types of amplifier.

give a maximum peak output of 96 with the same anode load and about the same gain (actually quoted as 14). Now, the valve will accept about 3½ times as much input with only the same distortion factor,

but if the input is restricted to that required for only 26 volts output the percentage distortion will be much less than with the lower H.T. There are other methods of reducing distortion that will be introduced later on in this series of articles.

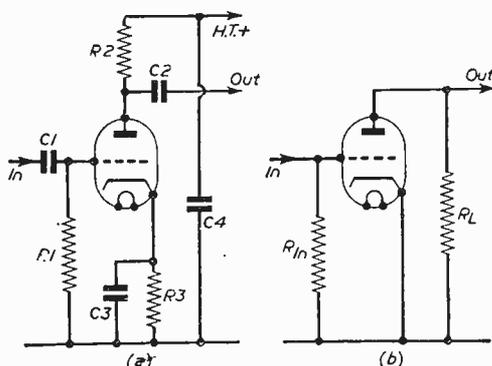


Fig. 8.—Basic Triode Amplifier.

The basic amplifying circuit is given in Fig. 8(a). A fluctuating voltage applied to the grid of the valve causes current through the valve to vary in sympathy. Note that the valve is not an amplifier in the basic sense of the word; it is actually a converter, accepting D.C. from the H.T. supply and converting it into an A.C. varying in sympathy with the varying voltage applied to the grid. The anode current has to flow through R2 and, by Ohm's Law, it will produce across R2 a voltage which will be in proportion to the current flowing through it, and as this current is varying in sympathy with the grid signal so must the voltage across R2 vary in a manner similar to the input voltage. The extent to

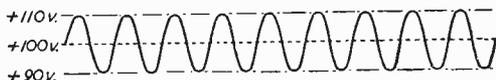


Fig. 6.—This illustration should have been given last month in place of Fig. 9 on the right.

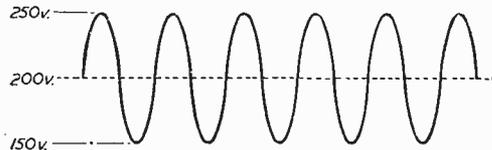


Fig. 9.—A.C. 100 v. Peak-to-Peak, with D.C. 200 v.

which the voltage across R2 varies depends upon the amplitude of the current fluctuations and upon the value of R2; in practice, the anode voltage fluctuations can be made considerably larger than the input fluctuations and so amplification results.

Consider the moment when the grid input moves more negative. Then the flow of electrons through the

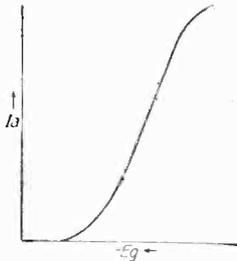


Fig. 10.—Triode anode current/grid voltage curve.

valve is reduced and this lower voltage causes fewer volts to be dropped across R2, causing the anode voltage to move towards the H.T. voltage: in other words the anode goes positive when the grid goes negative, giving effectively a phase reversal across the valve. Besides the fluctuating voltage, however, there is still the steady voltage from the H.T. supply also present at the anode. In case any reader is wondering how two different voltages can be at one point at the same time it will be as well to explain that an alternating voltage is considered to move equally on each side of zero volts, i.e., positive and negative. If the mean voltage is not zero, however, but has some value positive or negative, the waveform is looked upon as an alternating voltage and a steady voltage combined. Thus, in Fig. 9, the anode voltage is shown to vary between the limits of 250 volts and 150 volts in sine waveform and, of course, the anode has only one voltage at any given instance. The steady H.T. applied to the valve is 200 volts and the waveform is clearly the combination of this steady voltage shown dotted in Fig. 9, and an alternating voltage of peak-to-peak amplitude 100 volts fluctuating about zero. As only the fluctuating voltage and not the steady component is normally required by the following valve or circuit (there are some complications in pulse and television technique that can conveniently be avoided for the present) C2 in Fig. 8, is introduced, which in the first instance can be considered as being so large in capacitance as to be negligible in impedance so far as audio signals are concerned. C1 serves a similar purpose in isolating the grid of the valve from any steady voltage in the preceding circuit and is similarly assumed to be so large that it can be neglected to a first approximation. R3 is introduced to bias the valve, the steady current through the valve in the absence of signal potentials having to pass via this resistance, consequently developing a voltage across it. The fluctuating signal currents would also need to pass through this resistance except that C3 across it is assumed to be so large that it has negligible reactance to audio frequencies and so shorts out R3 so far as signals are concerned, and these two components R3, C3 can be ignored from an audio point of view for the time being. C4 is the smoothing capacitor in the power equipment and this also is so large as to be a short-circuit to audio signals and so the upper end of R2 can be considered to be connected to earth so far as the audio signals are concerned. The circuit thus simplifies to Fig. 8(b), and so long as the

input resistance R_{in} and the load R_L are, in fact, pure resistances the only component that can now cause distortion is the valve itself; the valve can cause distortion only if the relationship between grid voltage and anode current is non-linear, or in other words if a small change in grid voltage does not always cause the same amount of change in anode current. Here attention has to be turned to the valve characteristic curves, and in particular to the grid voltage (E_g)/anode current (I_a) curve, which has the shape shown in Fig. 10. Linear (and therefore, distortionless) operation requires a characteristic that is itself a straight line; then at all parts of the characteristic it will be seen that a given small change in E_g will cause the same change in I_a . But according to Fig. 10, there is a curve in the characteristic, so it is essential to work the valve in such a manner as to avoid bringing the curved part into play. Hence the need for negative bias on the grid to bring it on to the straight part of the characteristic. The signal applied in the case of sound amplification swings equally on each side of the bias point and care must be taken to see that this does not swing on to the curve. Bias is not very critical if only a small signal is to be fed into the valve, but if the maximum possible signal has to be handled without overloading, it is necessary to read off carefully the range of E_g over which the "curve" is substantially straight. In practice it is

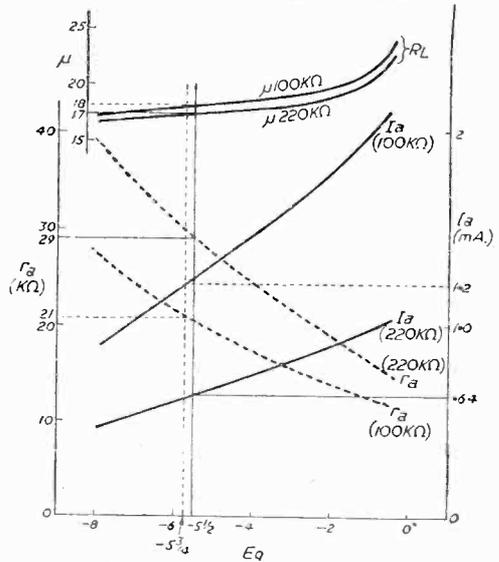


Fig. 11.—Dynamic characteristic of the 6BR7, triode connected. H.T. is 250 v.

never absolutely linear and so there must always be some slight distortion. The applied grid bias must then be exactly mid-way between the two extremes to allow the grid to swing linearly on either side of the bias point.

These curves are usually printed in "families," each curve in the family being for a different anode voltage. The higher the anode voltage the longer the straight part of the characteristic becomes though as the anode voltage increases the maximum permissible current through the valve decreases, being limited by the maximum anode dissipation determined by the valve makers, so beyond a certain critical anode

voltage the *usable* part of the straight section of the characteristic becomes shorter.

Dynamic Characteristic

This is all very well so far as it goes but the curve that has been used above is a static one and assumes that all except the two factors plotted, E_g and I_a , remain constant. This would be so if there was no anode load, but then there would be no output voltage produced by the fluctuating current and so the circuit would not be much use as an amplifier. In practice, however, the load resistance causes the anode voltage to fluctuate with the signal and this has its effect on the current flowing quite apart from and in addition to the grid voltage fluctuations already referred to. What is wanted for design work is a dynamic characteristic that takes into account the load resistor. Fortunately, the valve manufacturers provide this. As an example the Brimar 6BR7 would be a good choice as an audio amplifier and the following data are derived from the maker's leaflet to illustrate the method. This valve is a pentode designed for audio work, being made very rigid to avoid microphony (i.e., mechanical ringing when subjected to shock or vibration as, for instance, from a speaker), and the construction is such as to reduce hum to a minimum and to reduce valve hiss to a minimum. It can be worked as a triode by connecting the screen grid to the anode and the suppressor grid to the cathode.

Fig. 11 reproduces the dynamic characteristic of the 6BR7 triode connected and assuming the anode load to be either 220K Ω or 100K Ω , and in each case 250 volts H.T. It will be noted that the inclusion of a load resistance lessens the slope of the characteristic. If a straight-edge is put along the I_a characteristic for 220K Ω load, it will be seen to be substantially straight from -3 to -8 volts grid bias. Thus the valve will accept an input grid swing up to five volts peak to peak without distortion, though the valve must have a fixed bias midway between these extremes (i.e., -5½ volts) so that the signal will swing between the quoted limits. If the maximum input signal is less than five volts the fixed grid bias can deviate from the optimum value quoted. For instance, if the maximum signal to be handled is one volt peak to peak, it will be safe to bias to half volt below the maximum quoted above, i.e., to -7½ volts. At the same time it is good practice to design for optimum and so a bias of -5½ volts is decided upon. The anode current at this working point is read from the graph and is found to be .64 mA. The bias resistor is then indicated by Ohm's Law, i.e.,

$$R = \frac{1000 \cdot E}{I} \text{ (I being in mA; hence the factor 1000)}$$

$$= \frac{1000 \times 5.5}{.64}$$

$$= 8500 \text{ ohms.}$$

The striking thing about this valve worked in this way is the size of the cathode resistor required; one has been accustomed to think of bias resistors in hundreds rather than in thousands of ohms. This is due to the low anode current resulting from the use of a high value of anode load.

The curves show that with the working characteristic chosen the amplification factor (μ) of the valve is 17 and the anode impedance (r_a) is about 29,000 ohms. This compares with the static figures for the same valve (as quoted in less comprehensive data lists) of 20 for μ and 11,600 for r_a ,

The gain of an amplifying stage is :

$$\text{Gain} = \frac{\mu \cdot R_L}{R_L + r_a}$$

where R_L is the load resistance (220 K Ω as above) and μ and r_a are as given above.

$$\text{i.e., Gain} = \frac{17 \times 220000}{220000 + 29000} = 15.$$

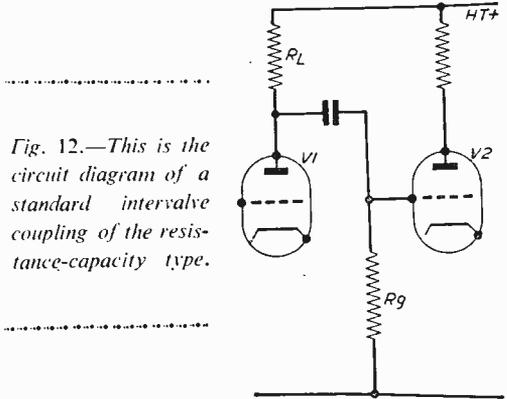


Fig. 12.—This is the circuit diagram of a standard intervalve coupling of the resistance-capacity type.

Following Circuit

This ignores the circuit to which the amplifier is connected and being a voltage amplifier it will probably be connected to a second such amplifier or to the output stage. In either case there will be a resistance in the input circuit of the following valve as in Fig. 12. It has been shown that R_L can be considered as being connected between the anode of V1 and earth so, as the coupling capacitor is large enough to be ignored from an audio point of view, R_g can be considered as being effectively in parallel with R_L . The resultant of these two in parallel is thus actually the load across which V1 produces its audio output, but the coupling capacitance is an effective stopper to D.C. and consequently D.C. conditions are determined by R_L alone. The procedure is to determine the value of the grid resistor of the following stage, which will normally be as large as the valve at V2 will permit. Now the figure of gain produced as above has to be reduced to allow for the effective reduction of load by virtue of the following grid leak. The usual formula for resistances in parallel applies. Designate the effective load (i.e., R_L and R_g in parallel) Req. Then

$$\frac{1}{R_{eq}} = \frac{1}{R_L} + \frac{1}{R_g}$$

$$R_{eq} = \frac{R_L \cdot R_g}{R_L + R_g}$$

The actual gain is now $\frac{R_{eq}}{R_L}$ times the gain calculated

for R_L alone (i.e., 15), so

$$\text{Gain} = \frac{15 \cdot R_L \cdot R_g}{R_L (R_L + R_g)}$$

$$= \frac{15 \cdot R_g}{R_L + R_g}$$

But R_L is taken as 220 K Ω . Assume an R_g of 1 M Ω . Then the amplification will be :

$$\frac{15 \times 1}{1 \times .22} \text{ (all resistance in M}\Omega\text{)}$$

$$= 12 \text{ times.}$$

(To be continued)

EXPERIMENTAL MICROPHONES



DETAILS OF SOME EASILY-CONSTRUCTED COMPONENTS WHICH WILL FORM A BASIS FOR EXPERIMENT BY THE BEGINNER

By W. S. Fowler, M.A.

THE radio amateur from time to time requires microphones for various purposes without having to go to the expense of purchasing a really good quality instrument. The microphones here described can be constructed from the odds and ends in the experimenter's box and have been found to give satisfactory results, especially when the main requirement is for intercommunication and speech work.

Electro-magnetic Types

A simple but highly efficient microphone can be constructed from a headphone earpiece. Simply connect the two leads from the headphone to the amplifier input socket and you have a microphone capable of delivering fair quality and volume.

The headphone must be of the high-resistance type—about 2,000 ohms is the usual value. Low-resistance headphones can be used as microphones but the leads from the headphones must be taken through a step-up transformer (a pentode output transformer used in reverse will do) before being connected to the amplifier input (Fig. 1).

An improvement in quality with this type of microphone can be effected by "damping" the earphone diaphragm. To do this, remove the earpiece, take off the diaphragm and place a piece of paper between it and the poles of the earphone

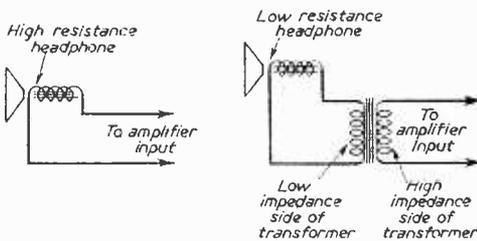
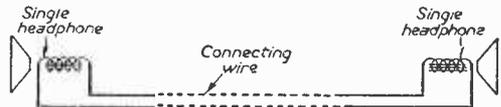


Fig. 1.—Using headphones as microphones.

magnet. Then replace the diaphragm and earpiece in the usual way.

An intercommunication outfit can easily be made with two pairs of headphones. Simply connect the two pairs together by means of a piece of flex and one earphone in each set can be used as a headphone and one as a microphone. The output, without amplification, is only small, but with high-resistance phones the signal can be heard quite clearly over a



Each headphone is used alternately for speaking and listening

Fig. 3.—Simple experiment to show use of headphone units.

good length of connecting wire (Fig. 2). To economise, using only one pair of headphones, split the two phones and use each alternately as a headphone and a microphone (Fig. 3).

Moving-coil Types

A very efficient, good quality microphone can be constructed from any small moving-coil loud-speaker. Simply connect the speaker leads via a step-up transformer (preferably a microphone transformer, but an output transformer can be used) to the amplifier input and speak into the loudspeaker. The 2 1/2 in. and 3 in. core speakers make the best microphones, and with these really good results can

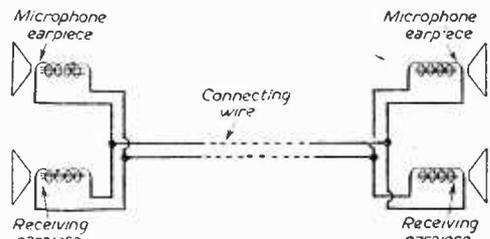


Fig. 2.—A relay system without amplification.

be obtained (Fig. 4). It is important to screen the transformer and also the leads from the transformer to the amplifier. The transformer ratio should be approximately 100 : 1 step-up. If an output transformer is being employed use the highest ratio possible, usually about 60 : 1.

Ribbon Types

An interesting experimental ribbon mike can be constructed from an old magnet and a piece of aluminium foil. The best type of magnet to use is one taken from an old meter movement or a magnetic pick-up. Take a 1 in. strip of aluminium, or other non-magnetic metal foil, about a 1/4 in. wide and press it between two pieces of corrugated cardboard to give it resilience. Take the "corrugated" foil

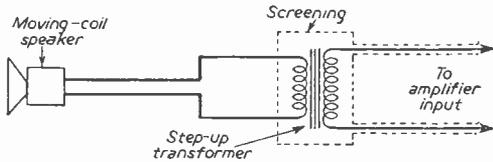


Fig. 4.—Using a small loudspeaker as a microphone.

and arrange it across the air-space of the magnet by means of copper wire clamps or bolts (Fig. 5). Take a lead from each end of the foil and connect to the low-impedance side of a step-up transformer (100 : 1). The high-impedance side of the transformer is then connected to the amplifier input. The whole microphone can be placed inside a wire mesh frame for protection and will be found to give quite good results.

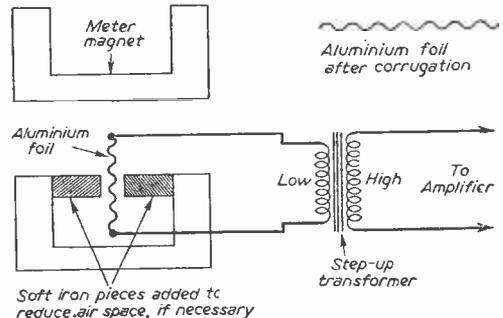
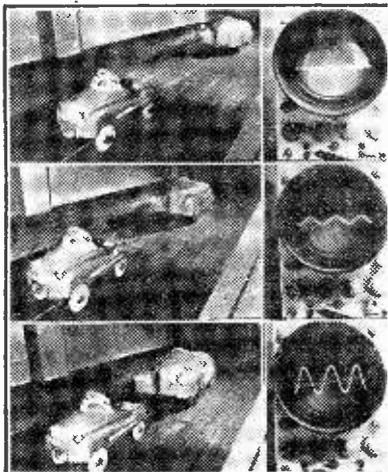


Fig. 5.—Details of construction of a ribbon mike.

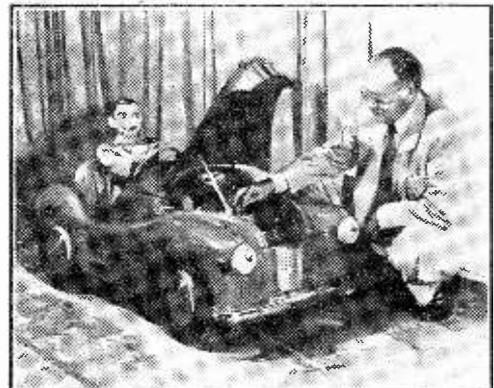
Radio Safety Aid

AN exploration of how electronics can be put to work to reduce highway accidents and to relieve drivers of tiresome tasks on modern superhighways, has been initiated by Dr. V. K. Zworykin, pioneer television and electronic scientist of the Radio Corporation of America. To study the basic problems of automatic driving Dr. Zworykin and assistants at the David Sarnoff Research Centre of R.C.A., in Princeton, N.J., U.S.A., have equipped a model five-foot car with electronic equipment. This laboratory car, which is powered by a storage battery, can: (1) Steer itself along a prescribed route. (2) Stop itself when approaching a metal

obstruction. (3) Turn out of its original lane into a second lane as if to pass another car moving at a slower speed. In the laboratory set-up, the model car is guided by a wire which represents a cable that would be laid in the roadbed of a superhighway. The wire sets up a magnetic field at a certain frequency, and this is picked up by two coils, one on each side of the car. If one coil receives more of the signal than the other it means the car is no longer centred over the wire, and electronic equipment controlling the steering wheel immediately brings the car back "on course." To prevent a collision with an obstruction simple transistor circuits associated with the guidance wire send out warning signals (at another frequency) whenever an obstruction passes or is stalled over them. These warning circuits, in effect, produce a "radio tail" at the rear of any metal obstruction on the route. When equipment in the model car receives the warning signal the brakes are automatically applied and the car comes to a halt.



The car and oscilloscope patterns of the "radio tail."



Dr. V. K. Zworykin and the radio-equipped car.

1912 *The* FIRST TWELVE YEARS 1925

AN EARLY AMATEUR CONTINUES HIS REMINISCENCES OF THE PERIOD
BETWEEN 1912 AND 1925

By C. H. Gardner

(Continued from page 242, April issue)

THE events described in my last article brought us nearly to the outbreak of the first World War, an event which was to stop completely the amateur movement for a period of some four years. For some little time before the outbreak of war quite an amount of wireless gear had been made available to the amateur by some of the big stores and also by certain dealers who had specialised in providing electrical equipment suitable for the enthusiastic schoolboy.

Some of the catalogues describing such equipment, both wireless and electrical, were masterpieces, and it is a matter of great regret that one has not kept one of these historical documents. These various suppliers also appeared to employ correspondence clerks who were geniuses in schoolboy psychology, as considerable technical correspondence had to be entered into by them in regard to the merits of a 10s. dynamo or a half-crown accumulator. Credit is due to these concerns for having encouraged youthful interest in this way, and thus provided a considerable nucleus for manning what was to develop into a major industry.

In fact, so varied was the equipment made available that it was possible to buy, ready made, the pieces of apparatus necessary to install quite an effective spark transmitter and an efficient receiving set. Little technical knowledge was needed to connect these various pieces of apparatus together but, so far as the receiving equipment was concerned, we early home constructors never felt that it rose to the same efficiency as the equipment that we had designed and made ourselves.

It was early in 1914 that an amateur friend asked if he might bring along a gentleman who had become very enthusiastic in transmission and reception. He had, my friend explained, purchased a lot of extremely expensive apparatus which he would like to bring to my den in order that he could be shown how to connect and operate it. In due course the gentleman arrived with the apparatus in the back of his car and it must be confessed that this equipment, obviously purchased regardless of expense, was a matter for considerable envy.

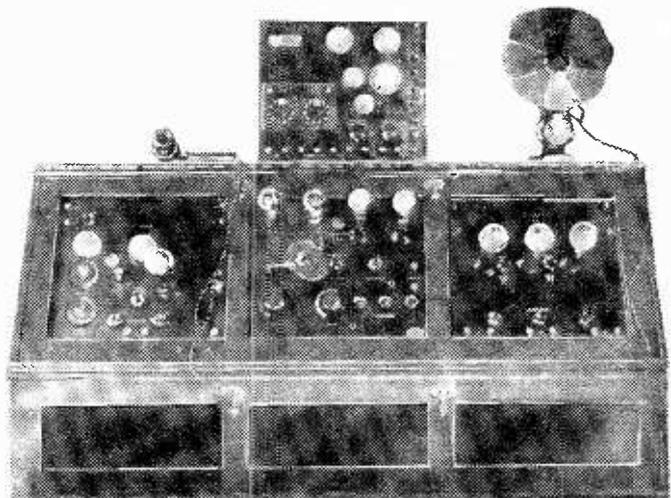
Shortly afterwards an invitation was received to view this equipment, which had been installed in elaborate glass-faced cupboards, in his private house although, as he explained, it had not as yet been put into operation.

The few weeks immediately preceding the outbreak of war were times of great excitement to the amateur wireless enthusiast, and a few days before war was declared it was possible to log the recall by Germany of a considerable number of their merchant ships sailing on the high seas. Shortly afterwards we received notification from the Post Office that our licences would be withdrawn and that a representative would be calling to collect our equipment, seal it, and take it to the Post Office, where it would be held for us until the termination of hostilities.

When the representative duly called, he asked for information concerning any amateurs in addition to those he had on his list, and two things became apparent at the same moment: one was that my friend with all the elaborate equipment had apparently never taken out a licence, and also that he had an extremely Germanic name. It was felt to be a duty to give his name and address to the Post Office representative and explain the extent of his installation. The result was interesting. Our acquaintance did indeed prove to be Germanic. He had more than a little working knowledge of wireless, and on investigation it was found that he had erected a concealed aerial running up inside one of his chimneys. Needless to say, he spent the remainder of the war in internment.

The First World War

Personal war experiences need not be dwelt upon



An early 2H.F.-Det.-L.F. receiver.

as only in the very earliest few weeks had they any remote connection with radio. Having enlisted as an "instrument mender" and spent three weeks without seeing an instrument other than a pitchfork, which was provided to clean out some stables, it was decided that some more rapid method of using one's hobby in wartime was desirable, and as luckily the Signals Section had taken on over strength, a transfer was not difficult to obtain.

One dark and dire deed whilst home on leave must be confessed to. The desire to hear some wireless signals (even if they could not be understood) was too great, and a friend and myself one dark evening wound an inductance, took a crystal and headphones, and journeyed to a certain factory to which he had access and which had conveniently a factory chimney up which ran a lightning conductor. Details need not be entered into here, but for ten minutes we forgot the woes of war and once again heard some of our old commercial station friends bleating out their Morse signals. I have often wondered since how my friend managed to explain away and get repaired the curious break which occurred in the bottom two feet of the lightning conductor.

It may be difficult for the present-day amateur to appreciate the intense enthusiasm which resulted in one committing such a heinous offence, but the amateur of those days just lived for his hobby, a fact which no doubt was accentuated by its rapid development which gave so much scope for experimental work, even by those with next to no technical knowledge.

Demobilisation led me into a line of business not immediately connected with radio, but allowed of the opportunity of gathering up the lost threads and getting together some equipment. In the intervening period the valve had, of course, made its appearance, and the first item on the agenda was somehow or other to obtain one of these desirable articles. So early in 1919 I became the proud possessor of one triode valve, and the first purpose to which it was put was as an amplifier to boost up the rectified signals from the crystal detector. This coincided with the time of the General Strike, and seeing somewhere that radio amateurs were required to establish lines of communication, contact was made with Headquarters, Western Command, who suggested a discussion on the matter. A 200-mile trip on a motor-cycle resulted in a gift of no less than three triode valves and a roughly drawn circuit showing how to make one of these oscillate and produce signals.

Instructions were received to get this "transmitter" into operation as quickly as possible and call Headquarters on a given frequency.

This probably all sounds extremely simple to the present-day amateur, but in view of the fact that the only available H.T. supply was from a number of dry cells in series, that one could only roughly guess at the frequency at which one was transmitting, and the distance to be covered was the best part of 100 miles with intervening hills, it is not to be wondered at that communication had not been established during the few days before the strike terminated.

Following this period there was a short period during which personal conditions prevented any time being spent on radio matters, and when the time came to start rigging things up again there had become available the extreme excitement of the possibility of receiving telephony transmissions as well as the Morse signals which had hitherto provided the basis of experimental work. It is very difficult to describe

one's feelings at the time of first hearing speech come over radio. One's immediate inclination was to rush out to the street and call in every casual passer-by to hear the new miracle which was occurring. What amateur of those days will ever forget the transmissions from Two Emma Toc, Wrrrrittle calling, with Captain Peter Eckersley counting up to ten and repeating the days of the week, and certainly none will forget the occasion upon which Dame Melba gave us what was almost our first song to be heard transmitted over wireless.

Curiously enough, most of us were still using crystal or crystal plus a valve amplifier, and circuitry for us had changed very little.

Telephony

The advent of telephony, however, very naturally made us more than a little anxious to start experimenting on transmissions of this type, and it was not long before we had developed simple circuitry for such transmissions which were carried out on 440 metres.

It would take up too much space to detail the step-by-step technical advances that were made, or to recall incidents concerning early official broadcasts, but in these early stages many of us were still using dry cells or inert cells for the H.T. supply for the transmitter and a grid modulation circuit which put the microphone at high potential to earth. This latter detail of circuitry occasionally had some amusing results. On one occasion my station quite suddenly went off the air following a request from the friend to whom transmission was being made to speak a little more closely into the microphone. As the microphone had been fitted with a small tin trumpet, the result of this request can easily be imagined, and it took some little time to disintegrate the operator from numerous pieces of transmitter and several hundred dry cells which he had pulled on top of himself as a result of falling flat on the floor following an applied potential of some 400 volts to the tip of his nose!

Racing Car Aid

In the spring of 1922 a friend called at my office and told me that the well-known racing motorist, the late Mr. S. F. Edge, was proposing to try to beat the world's double twelve hour record and was due to start on this endeavour at the Brooklands Track the following morning.

As a result of a conversation over lunch, it had been agreed that I would provide some radio equipment whereby Mr. Edge would be able to communicate between his car and the pits during the course of this run.

Even to-day, with only a few hours' notice, it would not be easy to carry out such a project. Thirty years ago it appeared completely impossible, but in those days the enthusiastic amateur was inclined to supreme optimism in the possibility of attaining the apparently impossible.

Transmission of speech was, in the light of available knowledge and in view of the time available, out of the question. Morse communication seemed a faint possibility if some way could be found of installing a spark transmitter in a racing car in a matter of a few minutes. *(To be continued.)*

THE BATTERY CORONET FOUR

IN the theoretical diagram and wiring diagram of this receiver, published in the last issue, the polarity of the 25 μ F condenser across the bias resistor in the output stage was reversed. The positive side of the condenser should, of course, be connected to earth.

Model-control Receivers

DETAILS OF A DIRECT-COUPLED AMPLIFIER

By F. G. Rayer

MODEL-control receivers using a single valve have one or two disadvantages which can become very grave in certain circumstances. If carrier-wave control is used with a single-valve receiver and the latter employs a "hard" or vacuum valve, the range at which control can be obtained is rather limited. To overcome this, a gas-filled valve is usually employed. This is very satisfactory in small models, and equipment used for comparatively short periods, and the range is very much increased. However, this type of valve has a rather limited operating life (usually in the neighbourhood of about twenty hours). This fact makes it unsuitable for equipment which is to have long periods of use.

These disadvantages may be overcome by using a directly-coupled amplifier or control valve. The size of the equipment is increased, and additional batteries are required. In some instances, however, these considerations are not very important, and the life of the valves is very long—similar, indeed, to that obtained from such valves when used in ordinary broadcast band or other receivers. This consideration alone can make such circuits well worth using.

The Quenching Detector

Single valve model control receivers usually employ one valve in a conventional U.S.W. self-quenching detector circuit. Such a detector operates in a state of continuously-interrupted oscillation (usually termed "super-regeneration") which greatly increases sensitivity. Oscillation at radio-frequency (usually about 27 Mc/s) is obtained by a suitable anode/grid coil, while quenching (normally at about 10 Kc/s) may be obtained by a suitable choice of grid condenser and leak values.

When the receiver is operating, the bias produced by oscillation settles to a steady value, and the valve anode current depends upon this value. When the transmitter carrier is radiated, the strength of oscillation is modified, resulting in a change of bias and anode current. With a gas-filled valve, the anode current may change from 1½mA, with transmitter off, to ½mA or less, with transmitter on, even at fair range. This is ample to operate a sensitive relay. With a vacuum valve, however, the change in anode current is very much smaller—possibly only 0.1mA or so—even at reduced range. Direct operation of a relay then becomes impossible, or unreliable, unless "amplification" of this change in anode current is obtained.

The D.C. Amplifier

Conventional forms of amplifier circuits cannot be used because they operate with A.C. signals only, and not with a change in D.C. potential. The desired result can, however, be obtained, and the circuit in Fig. 1 shows how this arises.

Here, R1 is the anode load of the quenching detector, and may be from 25,000 to 100,000 ohms, according to type of valve and H.T. voltage available. Assuming that the transmitter is switched

off, and that the anode current and load are of such values that a voltage drop of 20V arises in R1, then it will be seen that the control grid of the second valve is 40V positive relative to the filament of V1. A suitable tapping on the H.T. battery enables the filament of V2 to be 45V positive. The grid of V2 is then 5V negative, relative to filament, and V2 passes an anode current according to this value of bias.

When the anode current of V1 falls, the voltage drop in R1 also falls, thereby tending to bring the grid of V2 more positive. This results in an increase in anode current in V2, and this increase is very much greater than was the decrease in anode current in V1. A relay may therefore be operated.

With this circuit, separate filament batteries are essential. It must also be noted that the operation of the relay is reversed—relay coil current *increases* when the transmitter is switched on, instead of falling, as with the usual I-valver. The relay contacts must accordingly be wired in such a way that the exterior circuit is closed by the armature being energised, instead of when it is released. This is a simple matter when alternative, or change-over armature contacts are provided. If they are not, then a small secondary relay may be introduced to produce the required effect.

2-Valve D.C. Receiver

A complete circuit employing this method of operation is shown in Fig. 2. The detector may be a 2V small-power triode type, if 2V accumulators are to be used for the filament supply, or an output type valve, either octal based or of B7G type, may be used for dry-battery operation. For the control valve, a pentode of the output type is used, since this gives increased changes in anode current for given changes in grid voltage, compared with the triode in Fig. 1.

The tuning coil will require approximately 11 to 13 turns of wire, if self-supporting and about 1in. in diameter, wound with 18 to 20 s.w.g. wire. (The exact number of turns will depend upon the stray

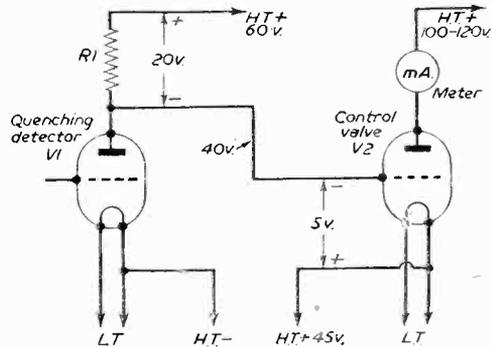


Fig. 1.—Action of a D.C. amplifier.

capacitances of wiring, holder and valve.) The detector stage should be adjusted, with a meter included in series with H.T.1, to obtain the maximum possible change in anode current when the transmitter is switched on. To accomplish this, the

When oscillation and correct tuning have been obtained, the 25 K Ω regeneration control should be adjusted to bring the valve into its most sensitive condition. Local oscillation should not be too fierce, or control by the transmitter will be lost, especially as range is increased. A little experiment will, however, enable the most sensitive point to be found, and a change in anode current of about 0.5 mA should be obtainable at short range from a transmitter with an output of 1 watt or so.

When the detector is operating correctly, the grid bias value should be adjusted so that adjustment of the 25 K Ω potentiometer enables the grid of the controlled valve to pass through a suitable voltage range for operation of the relay. Final adjustments may be made with a meter in the anode circuit of the second valve, the aim being maximum increase in anode current when the transmitter is switched on. A current change of several milliamps should be obtained at short range, but

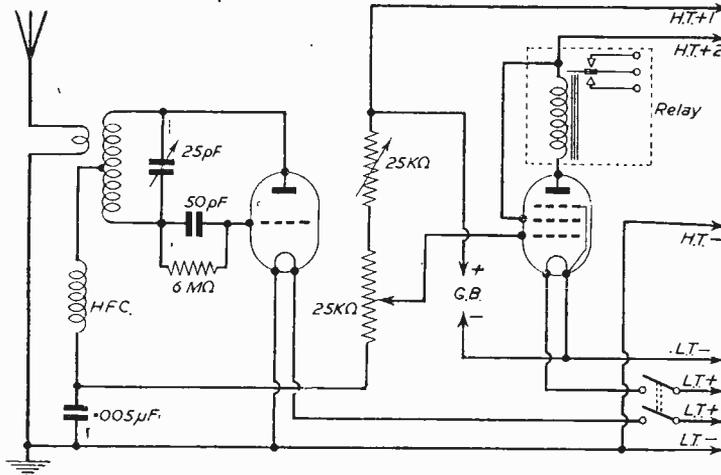


Fig. 2.—Practical circuit for a two-valve receiver.

tuning condenser should first be rotated until a dip arises in anode current, when tuning to the transmitter carrier. If no dip is obtained, the valve is either failing to oscillate, or the receiver is not tuning to the correct frequency. If shorting the tuning condenser does not cause an increase in anode current, the valve is not oscillating. This may be caused by tight aerial coupling, low filament voltage, a poor valve, or insufficient H.T. voltage.

this will, of course, gradually fall as the range is increased.

The relay should be adjusted so that the armature is just released when the transmitter is not radiating. Maximum range will be then secured. Incorrect relay adjustment may very considerably reduce range, so that the relay only operates when transmitter and receiver are close together and the change in anode current is relatively great.

F.M. Transmitters for BBC

THE BBC has placed an order with Marconi's Wireless Telegraph Co., Ltd., for the construction of twenty-six V.H.F. Frequency-Modulated (F.M.) transmitters for sound broadcasting. Delivery will commence within fourteen months.

These transmitters, of Marconi design, comprising twenty-four of 4½ kilowatts power and two of 10 kilowatts, will form part of the BBC's plan to provide a powerful reinforcement to the coverage of its present medium- and long-wave stations, by the use of V.H.F. F.M. stations.

As envisaged, the 4½ kilowatt transmitters will operate in parallel pairs, each pair handling one programme. Thus, six of these transmitters will be used on each three-programme station. The two 10 kilowatt transmitters will be used in parallel at the BBC's existing V.H.F. station at Wrotham, where there are already two 25 kilowatt Marconi transmitters.

Nine Marconi station monitors have also been ordered by the BBC for use on this project.

Technical Details

The range of transmitters has been designed to cover output power-requirements of 1 kW, 4½ kW, 10 kW, and 25 kW. Many new features are incor-

porated, and the performance of each is outstanding in its own particular output-category.

These transmitters, comprising units of basically similar design, but suitably arranged to provide the various output ratings, operate on the frequency-band 87.5-108 Mc/s. Air-cooled valves are used throughout, leading to a simplification of equipment, with reduced installation and maintenance costs.

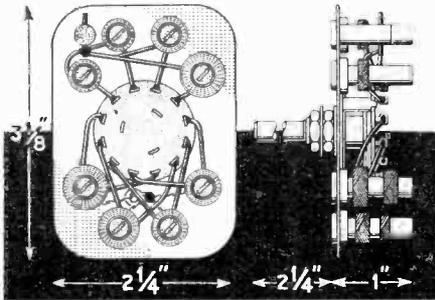
The F.M.Q. drive unit used on these transmitters, employs a frequency-modulated quartz crystal, and supplies an output at the carrier-frequency. This signal is then amplified to raise it to the required output level, the number of amplification stages used depending on the rated power-output.

The initial R.F. amplification stages consist of a double-tetrode stage, capacity coupled to a pair of tetrode valves, the anode circuits of which take the form of quarter-wave balanced lines magnetically coupled to a 50 ohms line, from which the output is taken at 250 W.

A third amplifier stage is added (in this case a triode), for the 1 kW equipment. The input is fed via the 50 ohms line to the cathode, the two cathode leads being at the same R.F. potential and forming the inner member of a tuned unbalanced line. The grid is grounded, and the anode circuit takes the form of a concentric line whose electrical length is variable by moving an R.F. short-circuit along the line.

We **GUARANTEE** these four Coil Packs to be the finest of their class in the Country. Mechanical precision, design and technical performance unsurpassed

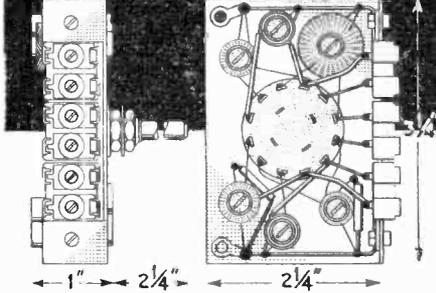
CP.4/L & CP.4/M



These compact 4-station Coil Packs are available for either—1 Long wave and 3 Medium wave stations (CP.4/L), or 4 Medium wave stations (CP.4/M). They are fully wired and require only four connections for use with any standard frequency changer valve.

Retail Price of each unit :
25/-, plus 8/4 P.T.—Total 33.4

CP3/370 pF. & CP3/500 pF

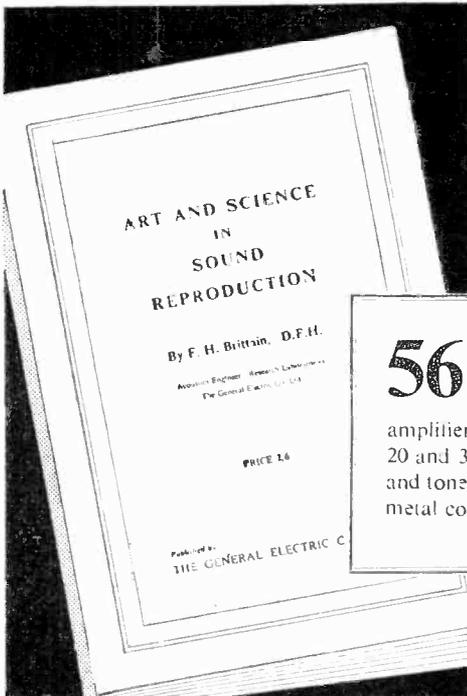


These 3 waveband Coil Packs are available for use with either 370 pF or 500 pF tuning condensers. The coverages are : Long wave 800-2,000 metres. Med. wave 200-550 metres, Short wave 16-50 metres. Designed for use with Jackson Bros. Full Vision Drive or SL.8 Spin Wheel Drive.

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32/-, plus 10/8 P.T.—Total 42/8.

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P. & P. 1/6

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On Your Wavelength

BY THERMION

Not Sacked!

As a result of many pleas from readers the Editor has decided not to sack me—yet! Readers have pleaded with him to give me another chance! Naturally I am touched by this reader concern that I should not join the dole queue and live like so many others on the welfare state. One reader, Mr. F. J. Jane, of Lostwithiel, one of my fans, says, however, that I have disappointed him recently in that I have “let up” in my attack on those who are paid money for crooning instead of being shut up in a sound-proof chamber with every other crooner and jazz band at full moan, groan and blast. I thought I had written the last word on this topic. Every reader knows my views about *ridm*, and I can assure him I have not changed my views. This reader says that if I am sacked “Mr. F. J. C. can expect a row.” He wishes more power to my pen.

Jet-propelled Steam Radio

MR. P. H. SPAGNOLETTI, B.A., Chairman of the B.R.E.M.A., recently referred to V.H.F. as jet-propelled steam radio and stated that it would prevent any further deterioration in the sound programme. V.H.F., of course, has been tried in America, but because it did not live up to expectations in that country it is thought by some that it would be an equal failure over here. This is false reasoning for the conditions which apply in America with its hundreds of broadcasting stations which have comparatively small coverage are by no means the same as over here. In this country we rely upon a few high-powered stations whereas in America large numbers of stations are of comparatively low power. Interference over here has been largely due to the increase in the power of stations and it is my view that V.H.F. will eliminate many of the problems of interference.

Parlour Games

NO change in system, however, can eliminate problems not concerned with technique but with programme selection. The tendency to-day is to convert radio programmes into a series of parlour games, or to drag someone to the microphone or the TV screen to deal with such childish and elementary subjects as putting a washer on a tap. Some items give me the impression of having been dragged in by the skin of their teeth. These “panels” with giggling pulchritudes answering stupid questions irritate me. They always remind me of that obnoxious person to be found in most house parties who wants to organise party games. Some of the bearded youths in corduroy trousers, baggy at the knees, suede shoes, green ties and yellow shirts, should be purged from the Augean stable, and the whole subject of programme selection placed in the hands of skilled impresarios or entrepreneurs.

In any case when technical programmes are put out, an expert should be commissioned for the job and not some amateur who knows little of the subject. It would do the BBC good to listen to some of the comment of skilled craftsmen when listeners or viewers are told how to paper a room or repair a crack in the wall. One such aspirant to radio fame recently advised a friend to repair a leaking cistern by putting a film of concrete over the bottom of it!

Reception by Land Line

THIS country has pioneered a system of relayed broadcast reception free from distortion and atmospheric or electrical interference. This is enjoyed in many towns and cities in this country through the operation of British Relay Wireless and Television, Ltd., an organisation that brings direct land line reception from the BBC studios to the terminal unit in the subscriber's premises.

A typical installation is in Leeds, in the industrial north, where B.R.W., as they are generally known, operate their service to a variety of places, including private homes, factories, canteens, hotels, blocks of flats, offices, institutions, hospitals and schools. Subscribers have the choice of four programmes by the simple operation of a selector switch and volume control. No other controls are necessary.

The three BBC programmes are relayed from the studios by direct land line, leased from the General Post Office, to a B.R.W. Central Control Room in each of their main operating areas, where the programmes are monitored and amplified.

In addition to the three BBC programmes B.R.W. also relay their own fourth programme—a composite one composed of selected items from foreign broadcasts. To receive the many stations that help to make up a day's programme a main radio receiving station at Saxmundham, Suffolk, one of the most modern in Europe, is equipped with a large number of specialised aerial arrays. Every known and many unique techniques are employed in the aerial systems to ensure as perfect reception as possible, irrespective of the many variable factors in reception conditions.

Two 100-mile (161-km.) Post Office music circuits connect the receiving station with B.R.W.'s Main Control Centre in London. Other Post Office circuits carry the programme to the company's other operating areas in the Midlands and the West and North of England. In each of these areas Post Office circuits carry the four programmes to amplifying stations which distribute them direct to subscribers by unobtrusive overhead lines.

Many types of receiving units are offered to subscribers and specialised equipment is available to hospitals and schools.

To cover the considerable area in which B.R.W. operate—they have over 160,000 subscribers—many hundreds of miles of cable are required, and for this purpose they make extensive use of our polythene insulated and sheathed cables.

R.E.C.M.F. EXHIBITION, 1954

THE ELEVENTH RADIO COMPONENT SHOW TO BE HELD AT GROSVENOR HOUSE,
APRIL 6th-8th, 1954

LIST OF EXHIBITORS

<i>Firm</i>	<i>Stand No.</i>	<i>Firm</i>	<i>Stand No.</i>
A.B. Metal Products, Limited.....	33	Hallam, Sleigh and Cheston, Limited.....	90
Advance Components, Limited.....	11	Hassett and Harper, Limited.....	117
Aerialite, Limited.....	118	Hellermann, Limited.....	81
Antiference, Limited.....	52	Henley's, W. T., Telegraph Works Co., Limited	2
Associated Electronic Engineers, Limited.....	1	Hunt, A. H. (Capacitors), Limited.....	44
Associated Iliffe Press, Limited.....	104		
Associated Technical Manufacturers, Limited...	29	Igranic Electric Co., Limited.....	7
Automatic Coil Winder and Electrical Equip- ment Co., Limited.....	111	Imhof, Alfred, Limited	57
Allan Richard Radio, Limited	114	Jackson Bros. (London), Limited.....	51
		Langley, London, Limited.....	126
Bakelite, Limited.....	122	London Electrical Manufacturing Co., Limited	42
Belling and Lee, Limited.....	55	London Electric Wire Co. and Smiths, Limited	14
Bird, Sydney S., and Sons, Limited.....	53	Long and Hambly, Limited.....	31
Bray, Geo., and Co., Limited.....	93		
British Electric Resistance Co., Limited.....	28	Magnetic and Electrical Alloys, Limited.....	39
British Insulated Callenders Cables, Limi ed...	68	Marconi Instruments, Limited.....	103
British Mechanical Productions, Limited.....	62	Marrison and Catherall, Limited.....	110
British Moulded Plastics, Limited.....	113	McMurdo Instrument Co., Limited.....	64
Bulgin, A. F., and Co., Limited.....	46	Micanite and Insulators Co., Limited.....	59
Bullers, Limited.....	4	Morgan Brothers (Publishers), Limited.....	128
		Morganite Resistors, Limited.....	23
Carr Fastener Co., Limited.....	21	Mullard, Limited.....	65
Clarke, H., and Co. (Manchester), Limited.....	92	Mullard Overseas, Limited.....	109
Collaro, Limited.....	82	Mullard (Valves), Limited.....	108
Colvern, Limited.....	38	Multicure Solders, Limited.....	66
Connollys (Blackley), Limited.....	60	Murex, Limited.....	5
Cosmocord, Limited.....	76	Mycalex Co., Limited.....	86
Creators, Limited.....	100		
		Neill, James, and Co. (Sheffield), Limited.....	123
Daly (Condensers), Limited.....	105	N.S.F., Limited.....	61
Dawe Instruments, Limited.....	73		
De La Rue, Thomas, and Co., Limited (Plastics Division)	80	Painton and Co., Limited.....	27
Diamond H. Switches, Limited.....	3	Parmeko, Limited.....	48
Dubilier Condenser Co. (1925), Limited.....	69	Partridge Transformers, Limited.....	22
Duratube and Wire, Limited.....	24	Plessey Company, Limited.....	67
		Plessey International, Limited.....	49
Edison Swan Electric Co., Limited.....	63	Pye, Limited.....	130
Egen Electric, Limited.....	20		
Electro Acoustic Industries, Limited.....	40	Radio Instruments, Limited.....	106
Electronic Components.....	98	Reliance Electrical Wire Co., Limited.....	47
Electrothermal Engineering, Limited.....	88	Reproducers and Amplifiers, Limited.....	75
English Electric Co., Limited.....	101	Reslosound, Limited.....	45
Enthoven Solders, Limited.....	43	Rola Celestion, Limited.....	35
Erg Industrial Corporation, Limited.....	119	Ross Courtney and Co., Limited.....	102
Erie Resistor, Limited.....	15		
Ever Ready Co. (Great Britain), Limited.....	124	Salford Electrical Instruments, Limited.....	36
		Scott, Geo. L., and Co., Limited.....	89
Ferranti, Limited.....	16	Simmonds Aerocessories, Limited.....	116
Fine Wires, Limited.....	91	Simon Equipment, Limited.....	83
		Spear Engineering, Limited.....	127
Garrard Engineering and Manufacturing Co., Limited	37	Stability Radio Components, Limited.....	72
General Electric Co., Limited.....	129	Standard Telephones and Cables, Limited.....	32
Goldring Manufacturing Co. (Great Britain), Limited	74	Standard Telephones and Cables, Limited (Valves Division).....	79
Goodmans Industries, Limited.....	12	Static Condenser Co., Limited.....	94
Gresham Transformers, Limited.....	30	Steatite and Porcelain Products, Limited.....	54
Guest, Keen and Nettlefolds, Limited.....	107	Stocko (Metal Works), Limited.....	99

<i>Firm</i>	<i>Stand No.</i>	<i>Firm</i>	<i>Stand No.</i>
Stratton and Co., Limited.....	10	United Insulator Co., Limited.....	8
Suffex, Limited.....	77	Vactité Wire Co., Limited.....	13
Supply, Ministry of.....	112	Vitavox, Limited.....	41
Swift, Leveck and Sons, Limited.....	125	Walter Instruments, Limited.....	85
Symons, H. D., and Co., Limited.....	97	Wego Condenser Co., Limited.....	25
Taylor Electrical Instruments Limited.....	18	Welwyn Electrical Laboratories, Limited.....	58
Telcon-Magnetic Cores, Limited.....	95	Westinghouse Brake and Signal Co., Limited.....	34
Telegraph Condenser Co., Limited.....	17	Weymouth Radio Manufacturing Co., Limited.....	115
Telegraph Construction and Maintenance Co., Limited.....	78	Whiteley Electrical Radio Co., Limited.....	19
Telephone Manufacturing Co., Limited.....	26	Wimbledon Engineering Co., Limited.....	84
Thermo-Plastics, Limited.....	9	Wingrove and Rogers, Limited.....	56
Transradio, Limited.....	120	Wireless Telephone Co., Limited.....	70
Truvox, Limited.....	71	Woden Transformer Co., Limited.....	50
Tucker, Geo., Eyelet Co., Limited.....	6	Wolsey Television, Limited.....	96
Tufnol, Limited.....	87	Wright and Weaire, Limited.....	121

A Brief Review of Some of the Exhibits

THERE will be 130 exhibitors in the Eleventh British Radio Component Show, to be held at Grosvenor House, London, from April 6th to 8th, 1954. This is more than at any previous show, and includes six firms who have not previously taken part in this exhibition. This annual private exhibition is organised as usual by the Radio and Electronic Component Manufacturers' Federation (22, Surrey Street, Strand, London, W.C.2), from whom invitations may be obtained. It crowds into the space of a few thousand feet, in a comfortable hotel, a representative display of an industry which employs 40,000 people and turns out nearly 1,000,000,000 components, valves and accessories a year.

The exhibits comprise British-made components for the radio, electronic and telecommunication industries, as well as gramophone components, valves and test gear.

While several manufacturers will not announce their new products until the opening day, it is possible to give some idea of the scope of the exhibits and trend of development and to give some examples. As might be expected, there will be a good many exhibits catering for the development of television all over the world and for its expansion in England to the higher frequencies. Several manufacturers will show multi-channel tuners for TV receivers, there will be valves for the new British TV frequencies and picture tubes with improved focusing units. Some new instruments for television servicing will be shown and there will also be camera cables and television aerials for continental as well as home use.

Resistors, capacitors and other components will be shown in new ranges, meeting still more stringent tests of efficiency under the most severe conditions of temperature and humidity and there will be new applications of some of the latest plastics and other materials. Several firms will show tape recorders this year. Gramophone components, including a new ceramic pick-up, will be well featured and there will also be new microphones and loudspeakers. Printed circuits will also be seen.

The following are extracts from early information received about exhibits in the Radio Component Show.

Aerials

Aerials for sound radio, including FM, and for TV suitable for export to particular markets. One firm has a range of 300 different aerials, specially designed for the American and Canadian standards, including 10-element arrays and stacked all-band aerials. Elimination of metal-to-metal contacts which are prone to corrosion has been accomplished, and universal mounting of telescopic car-radio aerials is also mentioned.

Cables and Couplers

A coupler specially designed for use with centimetre link equipment, but expected to receive other applications.

Demonstration of reduction of residual cable noise by a factor greater than 50 : 1, following special treatment of inner and outer surface of the core insulant.

Wire-end terminals in 150 different sizes.

New 50-ohm helical membrane coaxials and a new 75-ohm cable of 1¼ in. diameter.

Air-spaced articulated cable, claimed to be closely approaching the ideal 100 per cent. air-insulated concentric line.

Capacitors and Resistors

A new stable high permittivity ceramic for by-pass capacitor manufacture.

Improved characteristics in reduced size in electrolytics for radio and TV, specialised electronics and A.C. motor starting. Average reduction in size over past year for given capacitance and voltage is estimated.

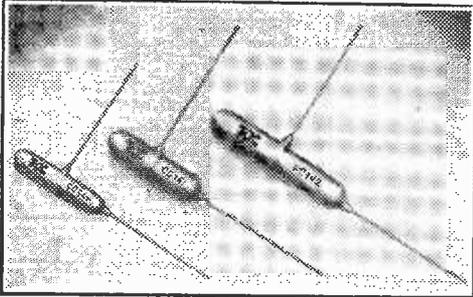


The New Collaro Model 2010 3-speed Transcription Gramophone Unit.

mated at 10 per cent. Standard commercial range operates from minus 20 deg. C. to plus 80 deg. C., and works inspection standards for leakage current has improved by 33 $\frac{1}{3}$ per cent.

Miniature metallised paper capacitors for use up to 85 deg. C.; thermic metal-cased midgets for operation from minus 100 deg. C. to plus 120 deg. C.

Variable condensers in range of 16 standard patterns covering the whole electronic field from



In the T.C.C. range these ceramic pulse-feed condensers have many advantages.

miniature receivers to transmitting types up to 5,000 v. test.

Extension of capacities and voltages to the range of subminiature electrolytics for transistor circuits and hearing aids.

Controls and Switches

A hermetically-sealed 5-watt rheostat potentiometer, stated to be the only potentiometer of its type fully approved to "H.1," the highest Service specification for resistance to temperature (minus 60 deg. C. to plus 100 deg. C.) and humidity.

Sine/cosine potentiometer 20 K to 30 K to an accuracy of plus/minus one per cent.

A new rotary main switch combining a number of micro-sensitive switches which can be ganged together in any number up to 12 units. It is compact and small and switches up to 750 watts per section.

Four-channel composite control unit for 3-D sound.

Germanium Exhibits

Apparatus illustrating applications of transistors.

Germanium junction power rectifier a quarter of the size of the present metal rectifier with electrical efficiency of 99 per cent.

Plastics

Silicone mouldings for heat stability, polyester resins for potting miniaturised circuits.

Nylon mouldings, large injection mouldings such as radio cabinets made from medium impact polystyrene as opposed to articles formed from glass fibre impregnated mat.

Extruded insulation in two and three colours, spirally applied—giving colour in depth, not by surface printing.

Terylene as insulation for copper conductors and resistance wires for operation up to 130 deg. C.

Sound Reproduction and Recording

A new transcription motor and ceramic pick-up, to be in production soon, suitable for tropical use.

Tape recordings at a variety of tape speeds—11/16in., 1 $\frac{1}{2}$ in., 3 $\frac{1}{2}$ in. and 15in. per second.

Tape monitor for long duration air/ground communications.

New microphones in both general purpose and deaf aid ranges.

High-fidelity power speakers for large gatherings.

Miscellaneous

New rubber-to-metal bonding technique.

Complete soldering and fluxing process for printed circuits and an automatic soldering head for repetition soldering processes. This automatically feeds the solder forward and brings the iron down to the component to be jointed, making up to 3,000 joints an hour.

Photo-electric cell measuring $\frac{1}{4}$ in. by $\frac{1}{8}$ in., so sensitive to light that it will operate a relay direct without any form of amplification.

"C" cores with improved bonding technique giving complete stability in operation in temperatures up to 200 deg. C.

A range of small diameter ceramic tubes, the smallest being 0.018in. (0.45 mm.) diameter with a bore of 0.004in. (0.1 mm.), suitable for temperatures up to 1,600 deg. C.

Electronic gauge used in guided missile and supersonic flight research, capable of rapid measuring and calibrating machine parts to a few millionths of an inch.

New nickelising technique for bushes and seals.

Fifteen volt battery for hearing aids of the following dimensions: 19/32in. x 35/64in. x 1 $\frac{1}{8}$ in. (15 mm. x 14 mm. x 35 mm.).

TV Valves and Components

New valves for the new British television frequencies (Band III) and V.H.F. F.N. reception.

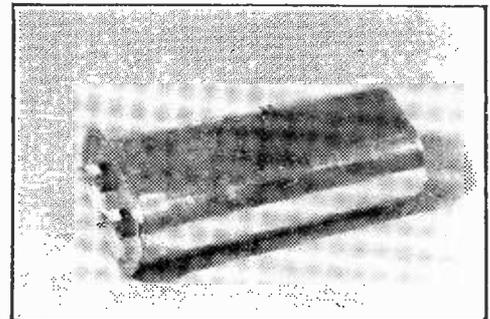
Claimed to be the first wide-angle electrostatically focused tube to be manufactured in Britain, featuring semi-automatic focus, eliminating the need for an external focus coil or magnet.

A new 21in. TV tube giving nearly twice the area of the 17in. tube.

Dual magnet focus unit made more compact than hitherto and incorporating a less expensive method of picture positioning for use in low cost TV receivers.

New focusing unit departing from the use of ring magnets.

Multi-channel turret TV tuners.



A Dubilier "Duconol" capacitor in special aluminium container.



TRANSMITTING TOPICS

DX AND THE GROUND-PLANE AERIAL

By O. J. Russell, B.Sc., A.Inst.P. (G3BHJ)

ONE simple and highly effective aerial system is the ground-plane aerial. However, there are certain aspects of this aerial which are not sufficiently stressed in the few articles describing it. It is too often assumed, for example, that it is a "one-band" system, and thus of little interest to those wishing to work upon all of the DX bands. Moreover, the particular properties of the ground-plane aerial, making it of special value for extreme DX working, may in fact make a casual experimenter think that it is a poor arrangement. This is due to its suppression of "semi-local" signal of the short-skip type of up to, say, 1,000 miles radius. Actually, this feature enables weak DX of long range to be received at up to some 20 Db better discrimination as against a conventional horizontal aerial.

It is clear, therefore, that the ground-plane aerial must be treated with respect. Furthermore, some appreciation of the actual operating principles of a ground-plane aerial are in order, as this will enable effective use to be made of a ground-plane for DX working. In fact, of course, a ground-plane aerial is no more than a scaled-down version of a quarter-wave Marconi aerial, plus a full quarter-wave radial counterpoise system. In practice, of course, few amateurs could possibly erect such a system on top band or

even 80 metres for operation on the L.F. bands. However, upon the H.F. DX bands, such a scaled-down system becomes the ground-plane. In operating principle there is very little difference between them. However, there are a few points to watch. First of all with an H.F. ground-plane aerial, the whole aerial—ground-plane radials as well—can be comfortably erected at a reasonable height above the ground. On V.H.F. systems it may, in fact, be erected at a very considerable height above ground. The London Taxi service aerial near the Crystal Palace is, no doubt, familiar to many readers. However, for the DX bands it is still possible to erect the ground-plane radials well above earth. This is well worth while if it can be arranged, as the ground-plane radiates a very low-angle pattern. The effects of nearby obstructions may, in fact, interfere badly if the aerial system is erected at ground level. Accordingly, the absorption of nearby buildings can conveniently be overcome by raising the ground-plane aerial system well above earth. The diagram of Fig. 1 shows the theoretical radiation pattern obtained over a perfectly conducting earth, plus the effects of the lower conductivity of a normal location.

Radials

While the basis of the ground-plane aerial is a quarter-wave vertical with quarter-wave radials, optimum performance is obtained by having the radials slightly longer than the vertical "whip" section. As a basis for

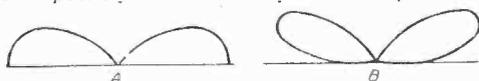


Fig. 1 (above). A. Vertical radiation pattern of a ground-plane over a perfectly conducting earth. Maximum radiation at zero angle. B. Vertical pattern of ground-plane over average location. Radiation pattern is still good at low angles, but zero angle radiation is attenuated.

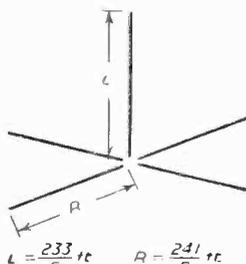
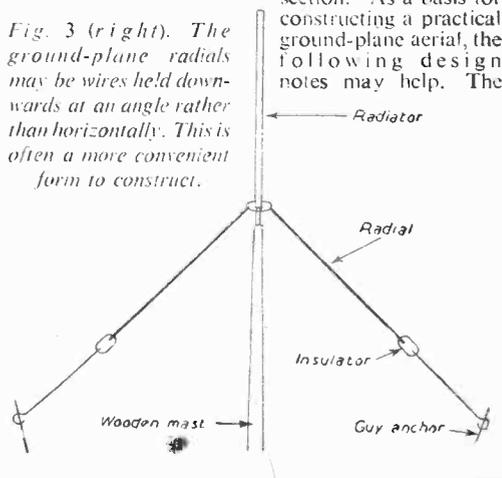


Fig. 2.—Dimensions of whip and radials for a frequency "F." Four radials are conventionally used.

Fig. 3 (right). The ground-plane radials may be wires held downwards at an angle rather than horizontally. This is often a more convenient form to construct.



vertical "whip" should be cut for a frequency of F megacycles to $\frac{233 \text{ ft.}}{F}$, and the radial wires should each be $\frac{241 \text{ ft.}}{F}$ long. However, if ground effects or nearby buildings interfere, these lengths may need very slight readjustment.

One aspect of the ground-plane is that the vertical "whip" is quite short on the DX bands. This has an important bearing upon construction. Thus for 20 metres, the vertical will be, say, 16ft. 8in. for C.W. edge operation. This can, therefore, be made of the well-known interlocking steel tube units available as "surplus" items. Some supporting guy wires may be necessary for 20 metres, but certainly not for a 10-metre band ground-plane. On 40 metres more rigid tube is needed, but a "gas-pipe" whip is a possibility. Furthermore, where it is not feasible to have the ground radials at right-angles to the "whip," they may be sloped downwards. This actually raises the centre impedance of the ground-plane from its 36-ohm figure for right-angled radials, and the limit is reached then the whips hang down so that the aerial becomes a centre-fed vertical of 72 ohms centre-feed impedance. However, with the radials at an intermediate angle, they still function as a ground-plane, but need no longer be self-supporting, as they can be wires maintained in tension by guys taken to anchors (Fig. 3).

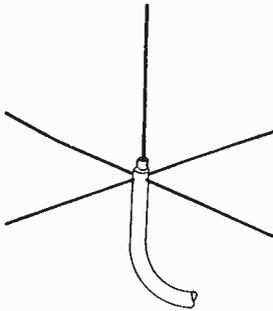


Fig. 4.—Method of attaching aerial components to a coaxial feed line. Radials are soldered to the outer sheath. The centre "whip" goes to the centre wire of the coaxial cable.

Feeding

Methods of feeding such ground-plane aeriels are, of course, of importance. The conventional method is to use coaxial feed, with the centre conductor of the coax taken to the whip, and the radials grounded to the outer sheath of the coaxial cable (Fig. 4). This is an elegant method, much in vogue for V.H.F. radiators. However, despite the agonies of self-appointed "experts," there is no real need to use coaxial cable. In fact, a tuned resonant parallel wire feed may be used. This is of real utility, as it makes multiband operation of a ground-plane feasible. Spaced wire feeders,

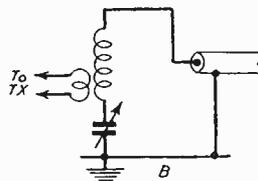
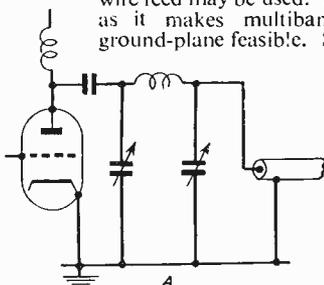


Fig. 5.—Arrangements A and B are most useful for feeding coaxially fed ground-plane aeriels. However, arrangement C may be of value in case of difficulty with A or B methods.

or 300 ohm line, preferably the round-section type for all weather use, are satisfactory in this application. Despite the presence of standing waves, efficiency will be high. It might well be higher than if cheap coaxial cable were used. Moreover, if multiband operation is desired, the parallel tuned line is more convenient. Thus a 20 metre ground-plane will also operate on 10 metres with reasonable efficiency. A 20 metre ground-plane will operate on 40 metres, although not with the highest efficiency. Thus three-band operation is feasible. A 20 metre ground-plane would thus be useful for 40 metres and 10 metres as well. However, while a 40 metre ground-plane would be effective upon 20 metres, it would not give correct low-angle radiation on 10 metres. It would still be useful for shorts skip 10 metre Q.S.Os however, while retaining the full DX capabilities for 20 and 40 operation.

The transmitting end coupling circuits also need

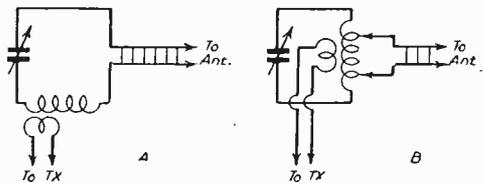
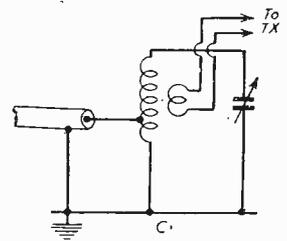
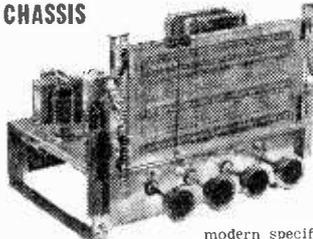


Fig. 6.—Parallel resonant wire feed lines are easily handled by the appropriate series circuit A, or the parallel circuit B, according to line length and band of operation.

some discussion. Coaxial feed for one-band operation requires a low-impedance feed. Three suitable circuits are shown in Fig. 5. A Pi output TX for example, designed to operate into a low-impedance line (the usual arrangement), Fig. 5A, is thus a popular choice. Also for low-impedance feeds, the series-tuned circuit link coupled to the TX (Fig. 5B) is also very useful. Under some conditions the use of taps across a link-coupled parallel-tuned circuit (Fig. 5C) may be more effective. For parallel-feed systems, using tuned lines, the conventional series-tuned or parallel-tuned link-coupled tuning systems (Fig. 6) will be used. For lines approximately an odd number of quarter waves long (for fundamental ground-plane frequency working) the parallel-tuned system will be used. For lines multiples of half-waves (i.e., an even number of quarter waves), the tuning system will be the series circuit. However, for operation on other than the fundamental frequency, it may be necessary to change from series tuning to parallel tuning or vice versa, depending on circumstances.



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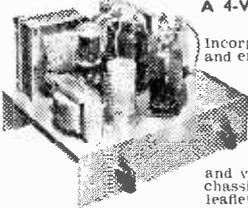
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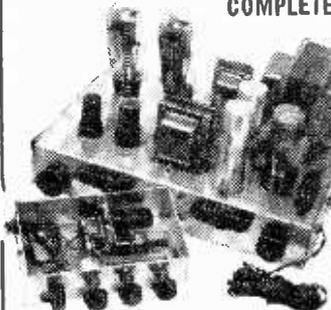
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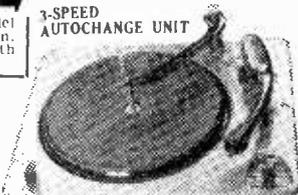
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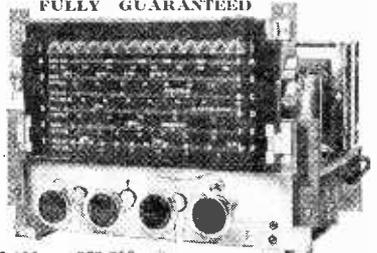
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The Beginner's Guide to RADIO



The Thirteenth Article of a Series Explaining the Fundamentals of Radio Transmission and Reception. This Month the Transmission of the Signal is Being Discussed

By F. J. CAMM

WE carry the pendulum analogy a little farther. Suspend a weight from a piece of string and swing the weight. If, whilst it is swinging, you hold the centre of the string you will notice that the rate of swing increases. If you suddenly increase the length of the string while the pendulum is in motion its speed will be reduced. In this example the pendulum may be considered as the aerial circuit of a receiver. If the pendulum is of the right length, so to speak, it will swing in harmony with the waves, but if it is not it will get out of step. In other words, if the aerial circuit of the receiver is accurately tuned it will resonate in sympathy with the incoming wireless waves, but not otherwise.

Station Selection

It is because a set must be tuned to a particular frequency in order to receive a particular programme that it is possible for a number of transmitting stations to broadcast at the same time and to receive only one of them. Each broadcasting station radiates on a different wavelength (length of pendulum analogy). Refer back to Figs. 55, 56 and 57 on page 210 of the April issue. The pendulum is shown swinging in unison with the waves on the water. The crest of each approaching wave strikes it at the right point in its course to keep it swinging continuously. Now suppose that the waves become more crowded (of shorter wavelength) so that before the pendulum has time to swing back from the first stroke it receives an impact from another wave.

Obviously, the swing of the pendulum will be upset and it would not respond to the action of the waves. In the same way, if the waves are more widely spaced (longer wavelength) there will still be no response from the pendulum. These three conditions correspond to the conditions prevailing when a set is tuned to a particular station while two other stations are also transmitting, one on a shorter and the other on a longer wavelength. Only one station would be received, not three. To pick up either of the other two stations the aerial circuit must be retuned in the same way as the length of the pendulum would have to be altered if it were to keep in synchronism with shorter or longer waves.

The Aerial Tuning Coil

Aerial tuning coils take many forms. We have seen earlier that it may consist of a simple hank of wire, a number of turns wound round a cardboard former or it can take the more com-

plicated form seen in receivers to-day. The wire for the coils is copper and it is covered with either cotton or silk so that the turns are insulated from one another. This is necessary in order to compel the small electric current picked up by the aerial to travel from one end of the wire to the other and not to jump across from one turn to the next.

The simplest way of connecting the aerial coil is to join one end of the wire to the aerial and the other to the earth. This latter may be a metal rod or plate bedded in the earth, a water pipe or some piece of metal in connection with the earth. The tuning of the aerial circuit is dependent on the size of the aerial coil (number of turns) and the capacity of the tuning condenser.

The Tuning Condenser

The use of the tuning condenser is to vary the capacity of the aerial circuit. It is a sort of vernier device. The aerial coil is wound with sufficient turns to receive all stations on the particular wavebands to be covered—medium and long, and sometimes short, medium and long (as in the case of all-wave receivers). The condenser is used to vary the range of the coil. The tuning knob varies the interleaving of the fixed and moving plates and by rotating the knob you can

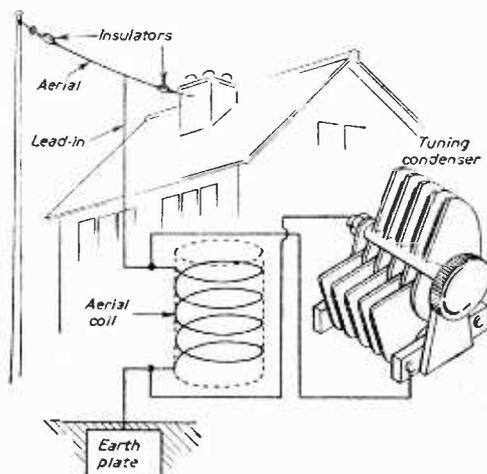


Fig. 58.—The elements of the aerial tuning circuit shown diagrammatically.

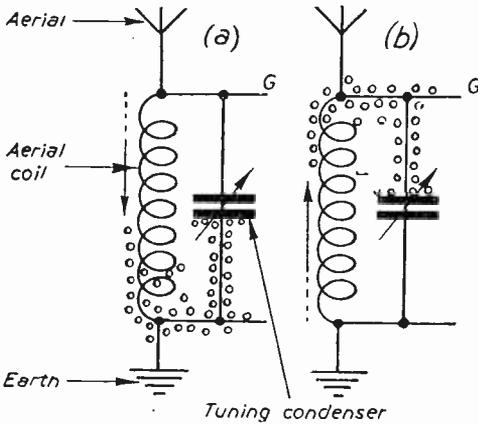


Fig. 59 (a) and (b).—Diagram illustrating the flow of electric currents in the aerial circuit of a receiver. The electrons first flow to one end of the tuning circuit as at (a), and then to the other end, as at (b).

tune the receiver to various wavelengths. This is similar to being able to adjust the rate of the pendulum in the examples previously given. If you wish to receive a station on the lower wavelengths the plates are moved outside the fixed plates and the reverse for the higher wavelengths.

The Carrier Wave (see Fig. 58)

As soon as the broadcasting station is switched on, and before anyone speaks into the microphone, wireless waves are being radiated. These I liken to waves on the surface of water, and, as previously explained, they are all of the same height and follow one another at the same interval of time. What happens when anyone speaks into the microphone is that the waves no longer remain the same height, but fluctuate in accordance with every variation in the tone of the speaker's voice. Of course, they do not vary in length (distance between each crest), but only in height. Naturally, the length of the waves must not vary, otherwise we should not be able to tune them in. This means that the waves will still cause electric currents to surge up and down your aerial, but they will vary in strength according as the waves vary in height, these variations in turn having been caused by the fluctuating sounds of the speaker's voice. Thus, the height of the waves varies while the length is constant.

The Speed of Waves

It is perhaps as well at this stage to make some mention of the velocity of wireless waves. Actually they travel incredibly fast, something like 300,000,000 metres per second. This means, for instance, that waves 200 metres in length sent out by a broadcasting station would strike your aerial at the rate of 1,500,000 per second. These in turn set up electric currents in your aerial circuit which surge up and down it at the same speed. Owing to their very rapid oscillations these currents are known as high-frequency currents. It is with these that the first valve in our receiver has to deal. In order to explain the action of this valve we shall have to make one or two elementary studies of electricity.

What is Electric Current ?

The accepted theory of electricity is that all matter of whatever nature, whether it be solid, liquid or gaseous, whether it be metal, wood, stone, water, air or anything else, is composed of minute particles called atoms. But these atoms are not simply tiny pieces of one sort of stuff. They in themselves are composed of a centre core or nucleus of positive electricity. This nucleus is surrounded by a number of negative particles of electricity. These latter are the electrons—and in size we know them to be infinitesimally small—which are responsible for electric currents. These, unlike the positive nuclei, need not remain stationary on a substance, but can move about. If a number of them are made to travel to one end of a wire it is said that an electric current flows along the wire.

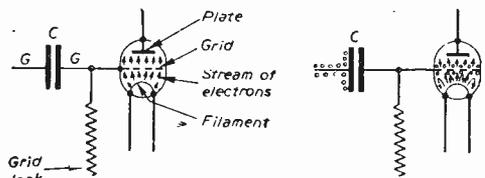
In the ordinary way there are just sufficient electrons in each atom electrically to balance the positive nucleus ; but if some of the electrons leave the atoms at one end of the wire and go to the other end, then the end to which they have gone will have a larger proportion of negative particles than normally, and is, therefore, said to be negative ; in the same way, the other end of the wire having a deficiency of negative particles will be positive.

Electric Currents in a Radio Receiver

First the electrons mentioned above travel to one end of the circuit and then to the other. This is going on all the time your set is tuned to a station, the only difference being that sometimes a larger and sometimes a smaller flow takes place, according as the wireless waves vary in magnitude with the speech or music being transmitted. By connecting a wire to the first valve, the electrons are made to do some useful work.

The reason that we cannot connect up the loud-speaker right away and hear the music is that the currents in the aerial circuit move too fast. We have already seen how quickly they oscillate backwards and forwards, the result being that the loud-speaker would be unable to follow them, for as soon as it commences to respond to the flow in one direction, the current would have already changed and be flowing in the opposite direction, the average effect being nil.

(To be continued.)



Figs. 60 and 61.—(Left) The normal flow inside the valve. (Right) the signal electrons on the grid and grid condenser.

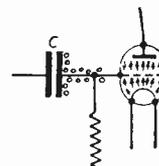


Fig. 62.—The accumulation on the grid side of the condenser.

A PRE-SET A.C. Receiver

A SIMPLE AND COMPACT 5-VALVE SUPERHET

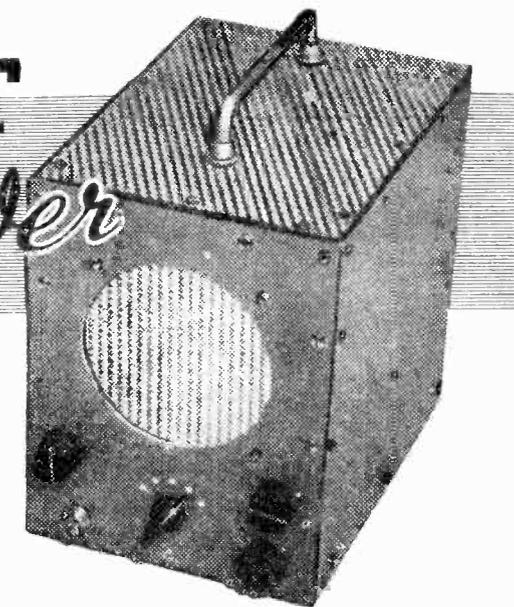
By D. A. Smith

THIS receiver was constructed for portability and was required to provide for the reception of either the long-wave Light Programme on 200 kc/s or the medium-wave Home Service on 908 kc/s by the operation of a single switch. It is robust, and small enough to be carried from room to room, making a useful secondary receiver. A switch is incorporated to enable it to take its power supplies from an external source via an octal socket in the rear, so that with the installation of a vibrator pack in the car it can be used on picnics, etc.

The circuit diagram shows that it is quite straightforward. Some non-essential components have been left out in order to make it easier to wire up, and to keep the size down without resorting to the use of miniature components.

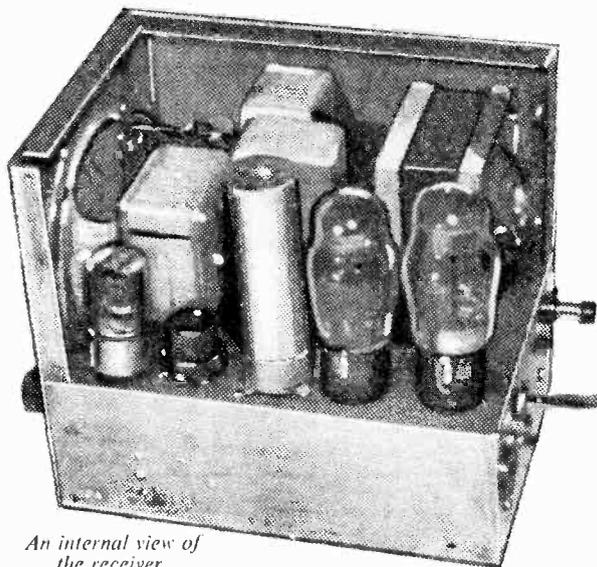
To use up some I.F. transformers already to hand, an intermediate frequency of 175 kc/s was selected, but there is, of course, no reason why the conventional 465 kc/s should not be used if the local oscillator is adjusted accordingly.

A triode hexode, such as the 6K8, is the obvious

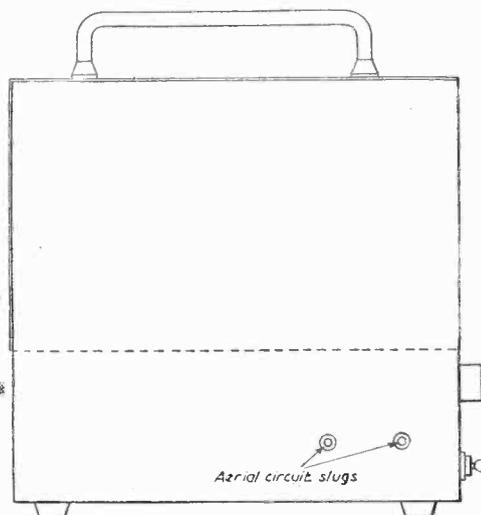


valve to use as the frequency changer, but a 6L7 pentagrid was available in the spares box so this was used. This particular pentagrid is designed for use as a mixer only, with a separate oscillator. It was found to function satisfactorily in this application, however, as a combined oscillator and mixer, the cathode and first two grids forming the oscillator section and the signal being applied to grid No. 3.

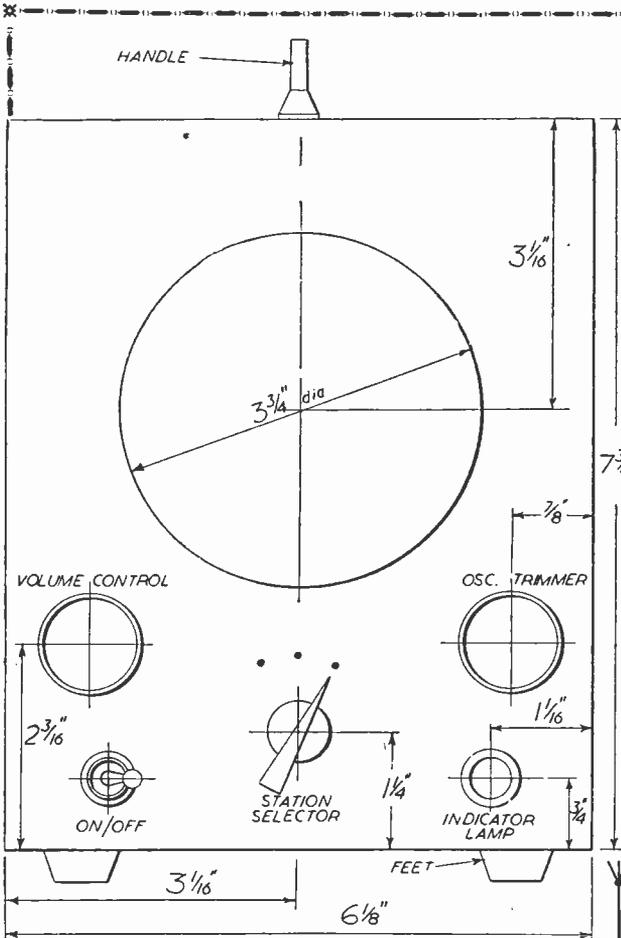
A four-pole three-position switch is used as station selector, the third position being a silent one—a useful facility. This switch selects tuned circuits for the frequency changer input and oscillator circuits. The coils used in this case were surplus from a BC433 radio compass receiver, but proprietary ones



An internal view of the receiver.



Side view, showing position of trimmers.



Details of the front or panel.

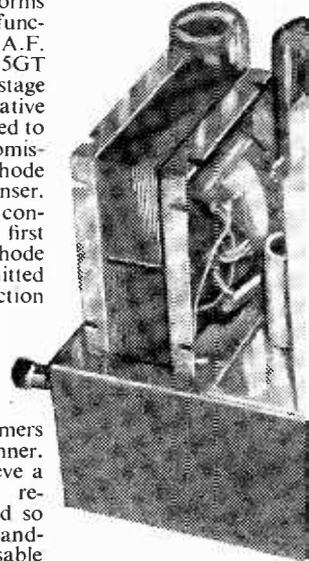
would be more suitable, providing they have adjustable slugs for tuning.

The I.F. amplifier is a 6BA6 vari- μ pentode—here, of course, there is a wide choice of suitable R.F.

LIST OF COMPONENTS

C1, C3, C6, C8, C9, C10	0.1 μ F	R1, R2, R9, R11	1,000 ohms 2.2 Megohms
C2, C7, C4m, C5,	0.05 μ F 100 μ F 25 μ F, variable	R3, R6, R7, R4, R5,	100,000 ohms 15,000 ohms 33,000 ohms
C11, C12, C13, C14, C15,	200 μ F 0.01 μ F 25 μ F, 12 v. wkg. 0.0065 μ F	R8, R10, R12, R13, R14,	100 ohms 1 Megohm 2,700 ohms 500,000 ohms, Pot. 220 ohms
C16, C17, Ca, Cb, Cc, Cd	32-32 μ F, 350 v.w.	Ch1, T1,	10 Henry, 100 mA Output transformer, 40 : 1 ratio
V1, V2, V3, V4, V5, V6,	6I7 6BA6 6H6 6J5GT 6V6G DW2	T2,	Power transformer. Secondaries : 4 v. at 2 a. : 6.3 v., at 2 a. : 250-0-250 v. at 80 mA.

pentodes. There are no frills to the second detector and A.V.C. circuits, and the number of components used has been restricted to the bare minimum. A single diode performs both the above functions. The first A.F. stage uses a 6J5GT and the output stage is a 6V6G. Negative feedback is applied to this stage by the omission of a cathode decoupling condenser. The decoupling condenser on the first A.F. stage cathode can also be omitted with a small reduction in gain.

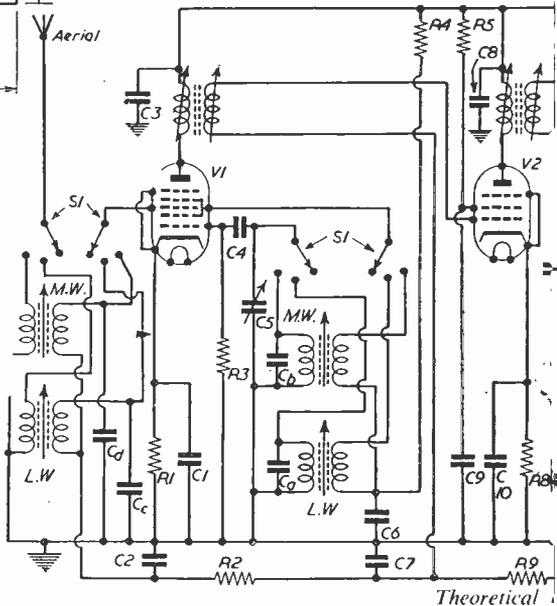


Another view of the receiver.

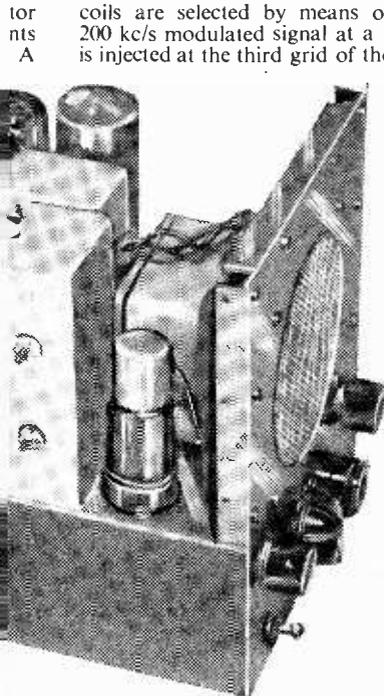
Adjustment

Lining up commences with the I.F. transformers in the usual manner. In order to achieve a double-humped response curve, and so improve the bandwidth, it is advisable to connect a temporary shunt consisting of a 30 K Ω resistor in series with a 0.1 μ F condenser across each winding of the transformers in turn while tuning the other winding.

Having lined up the I.F. transformers the L.



Theoretical



coils are selected by means of the switch, and a 200 kc/s modulated signal at a level of about 1 volt is injected at the third grid of the frequency changer. The value of the fixed condenser, C_a , required across the oscillator grid can then be determined by connecting across this coil temporarily a 500 pF variable condenser. This is adjusted until the signal is heard in the output, the coil slugs having previously been set to approximately the mid-position of their travel. The

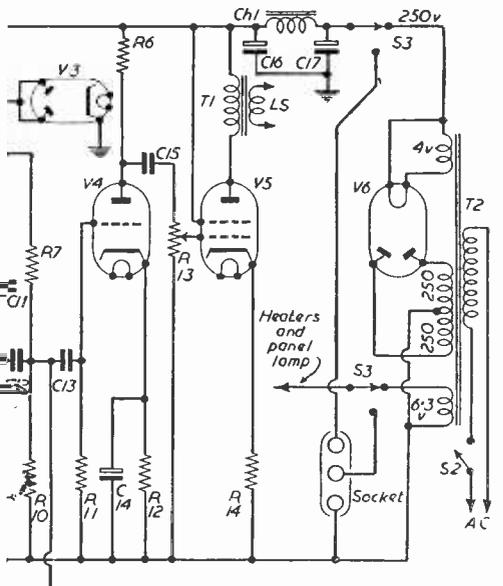
The signal generator is then transferred to the aerial terminal and its output reduced to a reasonably low level. The same technique can now be used to find the value of C_c across the input circuit coil.

This procedure is then repeated to line up the medium-wave channel on 908 kc/s for the Home Service, unless some other station is required. The final adjustment is made on the coil slugs when receiving the programme, and using about 3ft. of wire as an aerial. This should produce ample output.

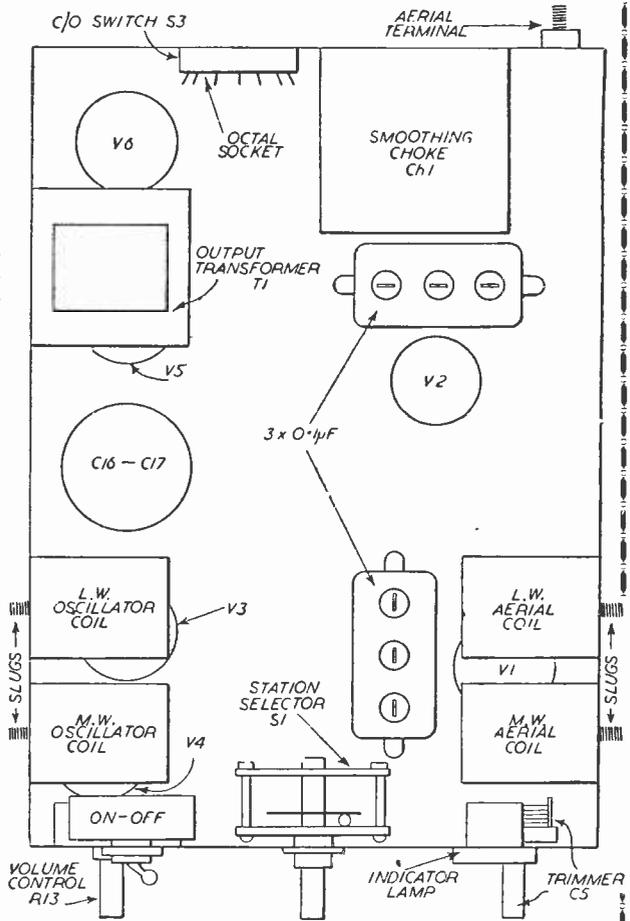
Panel Control

A small variable condenser of about 25 pF maximum is connected across the oscillator grid circuit on both ranges, and is available as a control on the front panel to allow for oscillator drift. This has not proved to be essential in practice, however, and any long term drift can be corrected by means of the coil slugs which are accessible from the outside of the cabinet.

value of the variable condenser at this setting is then measured on a bridge and the appropriate value of fixed condenser, or combination of condensers, fitted.



circuit.

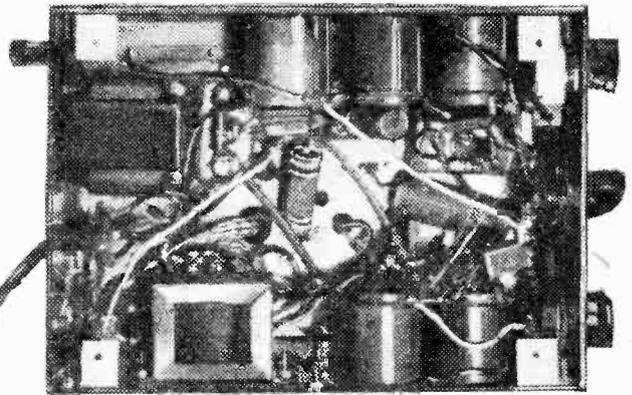


Details of underchassis component layout.

Lining-up

If a capacity bridge is not available, it is necessary to resort to trial and error methods for the lining up procedure of the frequency changer stage. Start by connecting, say, a 100 pF condenser in circuit for C_a and find out to what frequency the signal generator must be tuned to produce an output in the receiver. There will, of course, be two such frequencies, separated by an interval equal to twice the intermediate frequency. The lower of the two is the one required. The oscillator frequency can then be calculated by adding the intermediate frequency to the signal generator frequency found above. You are then in a position to alter the value of C_a to bring the oscillator frequency towards the required figure (665 kc/s for L/W Light Programme when using 465 kc/s I.F.).

Another method of finding the oscillator frequency would be to listen for it on an accurately calibrated receiver. A similar trial and error process must then be applied to the frequency changer input circuit to find the values of C_c and C_d .



View of underside of chassis. The principal components are identified in the illustration on page 289.

Layout

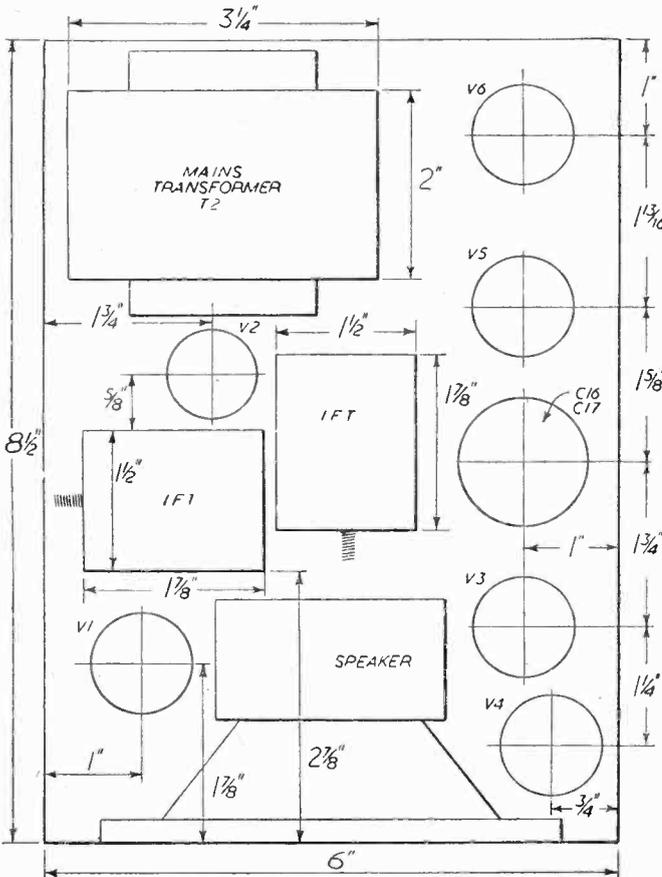
The receiver layout is shown in the accompanying illustration. It is built on a chassis 6in. x 9in. x 3in. deep, the bottom of which is covered in with a piece of expanded metal fixed by four 4 B.A. screws to four pieces of angle brass. These are secured to the chassis sides and drilled and tapped to take the fixing screws, which also hold four feet in position. There is a cut-out in the front of the chassis to accommodate the bottom of the 5in. speaker, which is bolted to the front panel.

The front and side panels are of 16 gauge duralumin sheet. They are bolted to the chassis sides, and above chassis level are held together at the corners with 3/16in. angle brass drilled and tapped 4 B.A. Angle brass also runs round the inside edges of these panels at the top and down the back inside edges of the side panels. To this is secured the top and back cover of expanded metal, which is easily bent to make the required L shape. 4 B.A. screws are used for fixing. A carrying handle bolted to this cover completes the job.

Speaker Fret

Expanded metal can also be used for the speaker fret. An alternative to the labour involved in making the large circular hole for the speaker aperture is to make a pattern of four or five holes with an octal chassis punch.

The positions of the station selector switch can easily be marked on the front panel by making shallow holes in its surface with a small drill (No. 25 say) and filling them with white paint with the aid of a sharpened matchstick, keeping the panel horizontal until dry. This should be done after the panels have been painted.

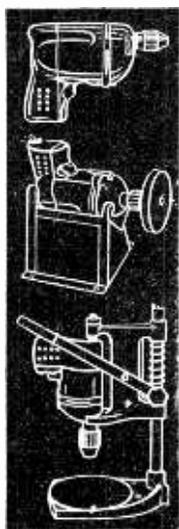


Another dimensioned layout.

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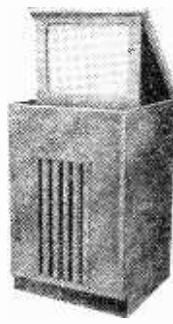
THE PORTA-PLAYER



This a robust, handsome carrying case finished in two-tone leather cloth with fold-away carrying handle and clasps. Approximate dimensions 19in. x 14in. x 10in., ample for 8in. speaker, mains or battery driven amplifier, and tape deck or other record-playing mechanism. Price £3 19.6. carr. and ins. 10/-.

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THE NON-REPEATABLE



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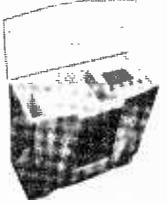
THE MIDGETRONIC



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THE EMPRESS



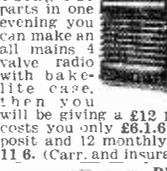
A cabinet to delight the eye of any discerning connoisseur, beautifully styled and elegantly veneered medium full-grained walnut. High polish finish. The amply sized control board is raised to a convenient level, but is not cut or drilled. Motor board, again uncut, measures 16in. x 14in. deep and has a clearance of 5in. To the extreme left is a space for recordings storage. Size 1ft. wide, 2ft. 8in. high, 1ft. 4in. deep. Price £15 15/- or £5 5 - deposit.

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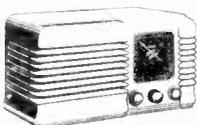
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KLYSTRONS SIMPLIFIED

AN ELEMENTARY EXPLANATION OF THE V.H.F. VALVES AND THEIR USE

By D. Currie and D. R. Sharp (Technical Officers, Admiralty)

Introduction

A GREAT number of modern electronic devices depend for their operation upon the use of very high frequencies, which are known as centimetric wavelengths. These are of the order of 10^4 and 3×10^9 megacycles, which is 3 cm. and 10 cm. wavelengths respectively. The object of this article is to explain one method by which these V.H.F.s are generated, amplified and propagated.

Basic Electronic Phenomena at V.H.F.

At these frequencies the use of a normal thermionic valve as used in commercial radio receivers would be unsuitable. This is because the inter-electrode capacity (mostly that existing between anode and grid) together with stray capacities in the necessary external circuitry form feedback loops which introduce heavy losses, thereby preventing oscillation at the desired frequency.

Another undesirable feature of this type of valve is that the density modulation of the electron beam produces a certain amount of velocity modulation. This is partly responsible for the non-linear characteristics.

In all Klystrons both forms of modulation are used. In fact, the electron beam is first velocity modulated in order to produce density modulation.

The Two-cavity Klystron

Of the various types of Klystrons we will discuss first the two-cavity Klystron (Fig. 1). This consists of the usual heater-cathode assembly electron gun, an accelerator grid, the Rhumbatron or "Buncher," the "Catcher" and an electron "trap."

Electrons leaving the cathode reach a velocity which is determined by the potential of the accelerator grid. We will assume that a V.H.F. is present at the "Buncher" which, in itself, is an oscillatory circuit consisting of the capacity between its two grids (G_1 and G_2) and the inductive loop joining them. The two grids are in very close proximity and the transit time of an electron passing through the gap will be a very small fraction of a cycle. As each electron passes through the gap it will be either further accelerated or retarded or remain at its original velocity, according to the phase and magnitude of the V.H.F. present in the gap at that instant.

The electrons will next traverse the "Drift-space," which is a "null" region between "Buncher" and "Catcher," where density modulation is formed due to the variations in kinetic energy of the electrons in the beam. In other words, bunches will be formed as faster-moving electrons draw nearer to those moving at a slower rate, and in this way velocity modulation produces density modulation.

These electron bunches now pass through the gap of the "Catcher" which again is a resonant cavity (oscillatory circuit), and the V.H.F. component of the beam current produces excitation.

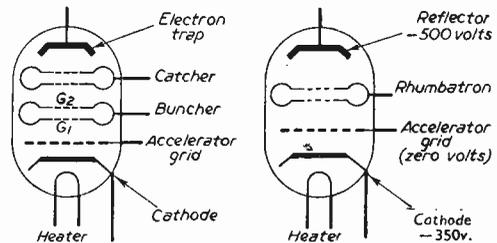
It will be seen that this device constitutes an amplifier, the power being derived in the normal way from the D.C. component of the electron beam. It will amplify at one particular frequency only (i.e.,

that at which both "Buncher" and "Catcher" are resonant).

The phase relationship between input and output is dependent upon the transit time of the electrons in the drift space, which is a function of the physical dimensions of the drift space and the velocity of the electron beam.

Effect of Transit Time on Coupling

If transit time in the drift space is too short then the electrons will not have time to form "bunches" correctly, and if the time is too long then "debunching" will take place as faster electrons overtake the slower-moving ones, and the distance between them increases. Therefore to obtain a maximum



Figs. 1 and 2.—Diagrams of two common forms of Klystron.

efficiency of the system it is essential that the transit time be of a critical period.

Transit Angle

It is customary to express transit time effects in terms of the transit angle:

$$\theta = 2\pi fT \text{ radians.}$$

where f = frequency of oscillation in cycles/sec., and T = transit time in seconds.

Thus, at a frequency of 1,000 Mc/s (10^9 c/s) and a transit time of 1,000th of a microsecond (10^{-9} seconds), the transit angle would be 2π radians or 360 deg.

The Two-cavity Klystron as an Oscillator

Any oscillator is fundamentally dependent upon its regenerative properties. Considering the two-cavity Klystron: if the transit angle is such that the "Catcher" is oscillating in-phase with the "Buncher," then a portion of the output may be fed back to the input (as with normal oscillating circuits) by means of an external feedback loop, and the system becomes regenerative. Thus, the Klystron can become a self-oscillatory device, any small change in beam current being sufficient to drive it into oscillation. This feedback loop usually takes the form of a concentric line. Care must be taken to ensure that this inductive loop produces the requisite coupling co-efficient. The main disadvantage of the two-cavity Klystron oscillator lies in its rather limited frequency coverage of the band for which it is designed. Variation of frequency is effected by producing a physical change in the dimensions of the resonant cavities, which are each provided with a flexible diaphragm for this

purpose. No variation, however, can be made in the physical dimensions of the drift space, therefore the initial beam velocity must be kept constant. This, of course, can be achieved by providing a stabilised voltage to the accelerator grid.

The Reflex Klystron Oscillator

A schematic diagram of the Reflex Klystron is shown in Fig. 2. It will be seen that there is one resonator only and this performs the dual function of "Buncher" and "Catcher."

The electron beam, after being accelerated, is velocity modulated by the "Rhumbatron." In the drift space the beam encounters a strong repelling field provided by a negative voltage on the reflector. It is thus caused to reverse its direction and return to the "Rhumbatron" where, providing the phasing is correct, the V.H.F. component of the beam current will produce excitation and thereby maintain oscillation. Typical electrode voltages are shown. The "Rhumbatron" is normally D.C. connected internally to the accelerator grid. Bunching takes place in the drift space, but the action of the reflector produces a phase change of 180 deg. during this procedure.

Electrons travelling faster than their initial velocity will penetrate further into the retarding field of the reflector before having their direction of travel reversed and will thus take a longer period of time to make the "round trip" than those electrons which, starting later but having less velocity, are more readily turned back by the reflector.

Phase Relationship for Optimum Power Output

For the resonator to absorb maximum power from the reflected beam then the centre of the bunches must pass through the gap at the time when it is

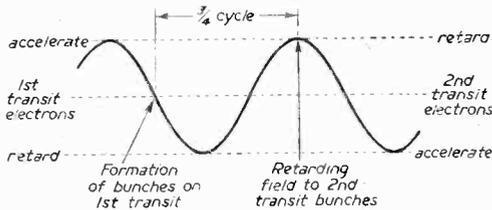


Fig. 3.—Phase relationship illustration.

exerting its most retarding effect upon them. Electrons at the centre of a bunch have travelled at a constant velocity and are those that pass through the gap on their first transit when the field was changing from an accelerating one to a retarding one. (This will actually cause low density areas which will become bunches after the 180 deg. phase change at the reflector.)

Since the reflected beam is travelling in the opposite direction, then the retarding effect upon them is not until three-quarters of a cycle later. Fig. 3 may help in explaining this rather complex function. The transit angle of the drift space will therefore be of the order:

$$\frac{3\pi}{2}; \frac{7\pi}{2}; \frac{11\pi}{2} \dots \text{radians.}$$

It is not necessary for the physical distance between "Rhumbatron" and reflector to be critical as the effective drift space is determined by the mean distance from the "Rhumbatron" at which the reversal of the

electron beam takes place, this being a function of reflector voltage.

Tuning Range of the Reflex Klystron

The Reflex Klystron, although less efficient than the two-cavity type, has a greater frequency coverage or tuning range over the band for which it is designed.

The variation of frequency can be effected by means of varying the reflector potential and also by

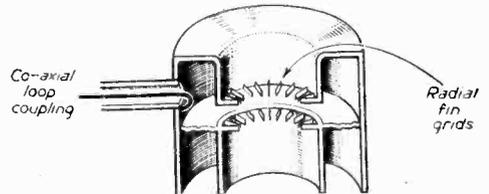


Fig. 4.—Detail of taking out the output.

mechanical means consisting of an adjustable probe which protrudes into the "Rhumbatron" chamber. The function of the probe is to vary the capacity of the resonator and thus the frequency. A relatively small variation of reflector voltage alters the impedance of the "Rhumbatron" gap and will produce a change of frequency over a limited range as a result. Too great a variation of reflector voltage will, of course, produce inadequate coupling between reflected beam and "Rhumbatron" so that oscillation will cease.

To maintain maximum power output when varying the frequency it is essential to adjust both probe and reflector voltage as the two are not inter-dependent. However, the frequency can be varied over a small portion of the band by varying the reflector voltage only and without serious diminution of power output.

Propagation of V.H.F. from Klystrons

The output power from the Klystron can be removed by means of a probe or loop which is inserted into the output resonator. This feeds directly into a concentric line. At these frequencies, of course, correct matching of feeder to resonator is essential.

The power can also be propagated through a glass window in the wall of the tube and thence into a wave-guide via a suitable matching cavity.

Uses

The Klystron as a voltage amplifier is of little use due to its high noise factor, but is finding increasing popularity as a power amplifier and pulse generator. Its main uses are, in Reflex Klystron form, as a Local Oscillator in micro-wave receivers and as a signal source in test equipment.

The efficiency of this class of valve is expressed as a figure of merit, this being the Gain-Bandwidth product.

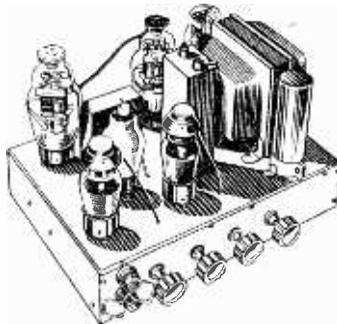
This article is of an elementary nature dealing with the fundamental principles of Klystron operation. We have, therefore, purposely avoided any complex mathematical analysis having given a purely physical treatise in order that it be more clearly understood by those whose knowledge of this subject is limited.

As a result of this, we beg to be excused by the more academically minded readers who, no doubt, delight in the practice of that "black art" known as mathematics.

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16μF 450 v	2/9	40μF 450 v	4/11
24μF 350 v	3/6	84μF 350 v	3/9
32μF 350 v	3/6	84μF 450 v	3/9
25μF 25 v	1/3	8-15μF 450 v	3/9
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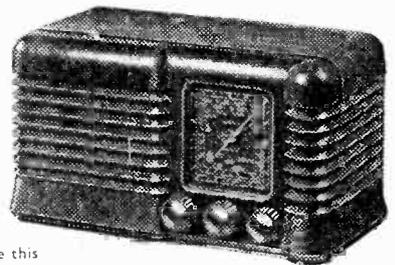
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SUPPRESSION OF ELECTRICAL INTERFERENCE

THE CAUSES AND CURES OF INTERFERENCE BY ELECTRICAL APPARATUS By A. E. Lofing

RADIO interference from one source and another is becoming an increasing nuisance and, if one is to enjoy radio listening, a serious attempt must be made to prevent or by-pass all objectionable "noises off," which can mar a good programme and ruffle the best of good humours.

The old adage of "prevention is better than cure" has its applications with interference, so we give a few hints first on how to prevent interference at its source, by far the most satisfactory remedy.

Among the most objectionable offenders are appliances using small fractional h.p. motors, such as in sewing machines, electric hand-drills, hair dryers, vacuum cleaners, etc. For these motors a pair of 0.01 μ F capacitors, one from each brush terminal to earth, will work wonders, being careful

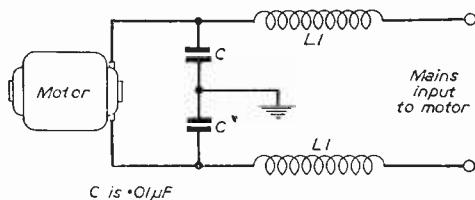


Fig. 1.—How to suppress a brush-type motor.

to wire them as near to the terminals as possible, and inside the end shield if there is one. This remedy is good for most fractional motors, but one may encounter a motor that requires extra attention in the way of an inductance in each lead to the motor, and possibly the screening of the complete motor. Screening may be required if only a bakelite casing exists. A suitable inductance for currents up to 1 amp. is a 1 or 2 millihenry coil of 24 s.w.g., dimensions of which are given in the table. These coils will prove most effective if wired in conjunction with capacitors, as shown in Fig. 1. For screening purposes a gauze or punched metal sheet is ideal, giving both ventilation and electrical screening. Points to note are that the joints of the screen should be well bonded together, by solder, rivets or small bolts, and most important of all that the screen is connected to a reliable earth.

This question of a good earth is of vital importance with suppression. No matter how many capacitors and inductors are added they will not give satisfactory reduction of interference unless the electrical oscillations are led away to earth. Inductors, etc., will keep the oscillations from travelling down the mains lead, but unless earthed they will "bottle up" as it were and re-radiate causing as much trouble as before.

Radiations

Many appliances do not have an earth wire, so before fitting any suppressor to these appliances be sure to fit one, and have a three-pin plug and socket with the earth socket to earth!

So much for commutator suppression. Now we are left with a good deal of apparatus most of which give out a fair amount of interference, such as electric refrigerators, thermostats for water heaters, sewing

machine foot switches and other switches having a regular usage. Most of these can be suppressed by an arrangement as in Fig. 2. Component values are given in the table on the following page. Incidentally, all capacitors for this connection should have a working voltage of 350 A.C. or more, and should withstand a 2,000 volt D.C. test. Therefore, only the most reliable components must be used. But an easy safeguard against this is to have a fuse of about 100 mA. inserted as shown by X in Fig. 2, these being readily obtainable.

With some switches this suppressor would be too cumbersome. An alternative is to use only the capacitor and fuse, the residual interference being reduced by a suppressor next to the radio itself.

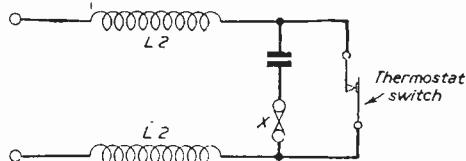


Fig. 2.—Suppressing a contact device such as a thermostat.

Cures

Now we come to the "cure" category, which will apply to most of us. In some cases, when a house is isolated from its neighbours and other sources of interference, an effective cure is achieved by placing a capacitive suppressor at or near the main house fuse box, shown in Fig. 3.

A reliable suppressor to be fitted on or near the radio receiver is shown as Fig. 3. If fitted within the receiver it should be wired immediately after the fuses, when wired outside the receiver a pair of fuses should still be incorporated, shown by dotted line in Fig. 3. Fig. 4 shows coil former details. The central supports are of 1/4 in. dia. ebonite or wood, the discs of 1/4 in. thick paxolin, alternatively these could be square, making construction somewhat simpler. Two of the discs are drilled to allow the wire ends to be led out and secured. The whole coil assembly is drilled with a 4 B.A. clearance hole through its centre for fixing purposes. The wire is 20 s.w.g. enamelled copper and wound to fill the bobbin each side.

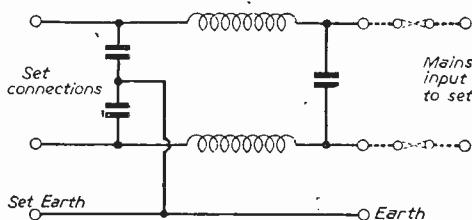


Fig. 3.—A filter circuit for use with a receiver. The condensers should be 0.1 μ F components.

This suppressor is very effective for mains borne interference. If a considerable amount of interference exists throughout the house and neighbourhood then the whole receiver will require attention to prevent direct pick-up on to the chassis and possibly the H.F. circuits. First and foremost, earth the chassis (if an A.C./D.C. type then earth through a 0.1 μ F

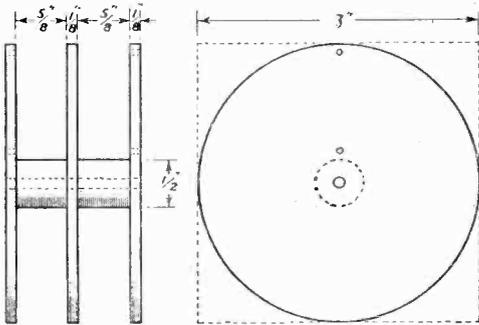


Fig. 4.—Details of a former for the chokes in Fig. 3.

capacitor). Next, ensure that all the screening cans are well bonded to the chassis. If the tuning capacitors and coils are not screened it is advisable to screen the whole receiver. This is done by lining the inside of the receiver cabinet with a metal foil such as aluminium. The foil can be glued into place, taking care to make good metallic contact at every joint and leaving sufficient holes for ventilation. The foil should be connected to earth.

Now the receiver is screened, but the most important and most sensitive part is still exposed to interference, the aerial downlead. The best solution is to use a screened cable as the downlead, but some matching arrangement is necessary to balance the low impedance of the screened cable to the high impedance of the receiver input, otherwise little signal input will reach the receiver circuit. For this purpose a pair of H.F. matching transformers will be required, shown in Fig. 5. Suitable iron-dust cores for the coils can be found in many ex-W.D. kits. Dimensions are 3/4 in. dia. by 3/4 in., but a near approximation to this size will be satisfactory. To construct the coils, first place a strip of thin paper around the core, sticking it in place with good

Coil	Current	Wire	D	L	N
L1	Up to 1 amp.	24	0.75"	4"	160
L2	Up to 1 amp.	24	0.75"	4"	160
L2	Up to 3 amp.	18	1.0"	5"	100

Where D = Diameter.
L = Length.
N = Number of turns.
All wire is enamelled copper.

insulating shellac. Wind L1, secure in place with another strip of paper glued firmly down. Repeat for L2. A serviceable screening can is the zinc casing of a U2 battery cell, removed by sawing near the top joint, and cleaned by boiling in water. The same sized can must be used over each coil. A brass bolt keeps the coil in place within the can, and serves to secure the whole to a bracket for outdoor mounting, shown in Fig. 5. Some loss in signal will be

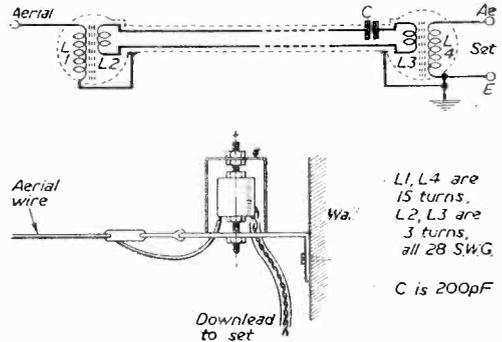


Fig. 5.—Details of an interference-free aerial system.

noticed with this transformer, but the freedom from interference will make up for that. The best aerial to use with these transformers is a vertical one, from 10ft. to 15ft. long. This is because interference has a larger horizontal component than vertical. Thus, if a vertical rod aerial be mounted as high as possible on the roof, the very minimum of interference is picked up.

New Mullard U.H.F. Valve

THE new Mullard double triode, PCC84, has several novel features. It has been specifically designed for operation as a series connected cascode amplifier on the V.H.F. with an H.T. supply of 180 v. In the cascode circuit, the first triode operates as a neutralised grounded-cathode amplifier and the second as a grounded-grid amplifier. This arrangement results in a considerable improvement in noise factor over pentodes at frequencies of hundreds of Mc/s. The series-connected cascode amplifier, in which the anode of the neutralised stage is coupled directly to the cathode of the grounded-grid stage, leads to a simpler circuit than when the two triodes are connected in parallel across the H.T. line. This is particularly attractive at ultra-high frequencies since it is not necessary to change the anode circuit of the input triode when switching from one frequency to another. A simple "series

peaking" coil of the type familiar in video stages, inserted between the anode of the neutralised stage and the cathode of the grounded-grid stage, acts to maintain the response over the whole band.

Series connection results, however, in two disadvantages: a high voltage is placed across the heater-cathode insulation of the grounded-grid stage, and the amount of H.T. available for either triode is only half the total H.T., which can result in a low amplification factor and mutual conductance. The PCC 84 has been carefully designed to avoid these disadvantages. The heater-cathode voltage rating is -250 v. and +90 v. peak, the maximum D.C. component being 180 v. Each triode can therefore be operated with a maximum H.T. of 180 v. (total HT = 360 v.). With an H.T. line of 180 v. the valve is therefore operating well within its maximum ratings. The amplification factor (μ) is 24 and the mutual conductance (g_m) is 6 mA./V. with an H.T. of 90 v. per valve.

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CROSS-OVER NETWORKS

PRINCIPLES AND DETAILS OF CONSTRUCTION OF FILTERS FOR FEEDING DUAL LOUDSPEAKERS

By W. J. Delaney (G2FMY)

There is a greatly increased interest in high-fidelity reproduction, and we continually receive requests for details of filter or cross-over networks suitable for use with a bass and "tweeter" speaker. We have, of course, dealt with this subject on many occasions in the past, but unfortunately all the appropriate issues are now out of print, so we are giving the essential data again for those who wish either to purchase or make-up suitable units.

There are two main circuits which are in general use, although there are various combinations of these which may be employed. The simplest scheme is that shown in Fig. 1, whilst the most popular variation is that shown in Fig. 2. The network or filter is connected between the output stage and a pair of speakers chosen for their efficiency in reproducing

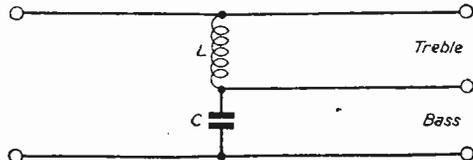


Fig. 1.—The simplest cross-over arrangement.

either the bass or treble (high notes). The most common procedure is to use a 12in. bass speaker—either one of those specially manufactured for the purpose or a standard 12in. unit which gives really good low-note reproduction or has been modified for the purpose, together with a small cone speaker, say about 5in. to 8in. in diameter, or one of the small horn-units, again specially designed for the purpose.

Cross-over Frequency

The principle is that the output from the amplifier or receiver is split up in the network and all frequencies above a predetermined value are fed to the high-note unit, whilst all below are fed to the bass unit. The reason for using a filter is that without it it is very difficult to find a speaker which will handle satisfactorily the entire range of musical frequencies delivered by a good quality amplifier. Hence, the arrangement is of little value unless a really good amplifier is being used. If the two speakers are connected without a suitable network there is a risk of the small speaker being damaged by the large amplitudes fed to it in the bass range, and the large speaker may produce spurious tones due to intermodulation resulting from the high frequencies beating with the low ones, or the speaker will not deliver the very high notes. By separating them through the network the bass unit is called upon to handle only those frequencies which it can handle satisfactorily, and the high note unit—sometimes referred to as a "tweeter"—will not be damaged by trying to handle low notes of large amplitude. Opinions differ as to the most satisfactory frequency at which to make the cross-over, some designers preferring a reasonably low frequency, say 800 to 1,000 c.p.s. whilst others prefer about double this value.

It is important to remember that the network must be

chosen according to the output impedance of the output transformer and the impedance of the speakers, and as a general rule these should be identical. The most common impedance now met with is 15 ohms and, therefore, the following data apply to this type of output only.

The filters should cut-off fairly sharply and as will be seen all that is required is a suitable choke and condenser. In the simplest arrangement of Fig. 1 only one of each of these components is required, whilst for the more elaborate system of Fig. 2 two of each are used. It will be seen from the diagrams that the choke is connected across the high-note unit and the capacity across the low note, the two components also being connected in series in the second arrangement.

Suitable Values

Where it is desired to make the cross-over frequency at 1,000 c.p.s. the capacity should be about 10 μ F and the choke from 2 to 3 millihenries. For a cross-over at 2,000 c.p.s. the capacity and inductance values would be halved. No difficulty should be experienced in arranging for the capacity values, as standard paper condensers may be connected up in parallel to any desired value, using 2 or 4 μ F units, with 1 μ F components to make a required odd value. The inductances do present a problem as they must be at low resistance and air cored and consequently become bulky items. For those who wish to wind their own, a 1.5 mH choke would consist of about 200 turns of wire on a 3in. diameter former, whilst space could be saved for the larger component by using slightly thinner wire so that the larger number of turns would not occupy very much greater space. The gauge of wire must, however, be sufficiently large to provide the lowest possible resistance and therefore ordinary commercial tuning coils or similar components will not, as a rule, be found satisfactory. It is possible to purchase these coils ready-made now from such firms as Webb's Radio, and obviously in view of the large amount of wire used they are expensive, costing round about 15/- each.

Connections

The complete network is connected between the output transformer and the two loudspeakers, and it is essential to mount the two speakers as close to each other as possible. It is also desirable that the two speakers should be "phased" correctly, that is, that

(Concluded on page 314)

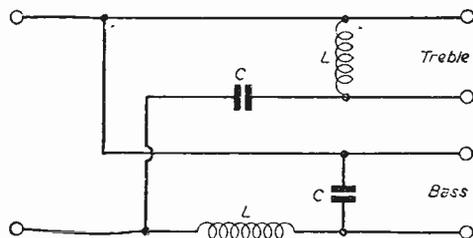


Fig. 2.—A more efficient circuit, and one which is in general use.

Programme Pointers



National Radio Awards

THE *Daily Mail* national radio awards for 1953 have been announced and made and once again Gilbert Harding finds himself the "Personality of the Year." Few will dispute that this is on merit. Wilfred Pickles was bound to suffer through the substitution of "Have a Go" for "May I Come In?" Now that the former is back again, Wilfred's hour may yet return.

Tom Jenkins, as a musical entertainer, is preferred to all his more highbrow colleagues, whose programmes are regularly broadcast, and Marjorie Westbury and James McKechnie are signalled out from drama. "The Name's the Same" was obviously the best new programme of the year and I hope it will soon be back on straight radio.

It is when we come to "the most entertaining programme of the year" that I am at a loss to understand public taste. "Take It From Here" and "The Archers" tie for first place! (Mrs. Dale, apparently, cannot compete with Dan and Doris Archer.) As regular entertainment features, in addition to being both instructive and enlightening, I would consider "The Critics," "Any Questions?" and "Music Magazine" to be far and away superior. One is always sure of both a good laugh as well as some new information, although this type of programme never gets a look in any more than "Twenty Questions" does. "We Beg to Differ," too, is excellent entertainment. I suppose "Take It From Here" is about the best of the regular half-hour medleys. But as the others are mostly too dreadful to permit of quiet discussion in polite circles, it really has no competition except perhaps from "Life with the Lyons," which has worked hard for a long time now. A vast amount of the success of all radio must depend on the script, and this is obviously where the two winning programmes score over their rivals, as did "Itma" before them.

Bermondsey Enquiry

"Riverside Borough," an autobiographical sketch of a community—Bermondsey—collected and edited by Tom Hopkinson, was in four half-hour programmes. Excellently produced and compiled, one was made to feel one with the burgesses and not, as is so often the case, a keyhole or fanlight trespasser. Opinions violently differ as to the propriety of asking people to disclose the most intimate secrets of both their income and its disposal. Also of their social habits and customs (one lady said she had had nine children, three of them married!). But as people are much less shy of admitting they have seven pounds a week than they are of having seven thousand a year, this side of the enquiry may not be so conclusive as would seem.

"Those Were the Days"

The five hundredth performance of "Those Were the Days" confirms the justified success and popularity of a very pleasant show.

By MAURICE REEVE

"Talk About Jones," a new series in which Peter Jones is with Lind Joyce, Mary Mackenzie, etc., but without Peter Ustinov, was very funny on the two occasions on which I heard it. Similar in style and format to the Ustinov-Jones shows. Let us hope it maintains its early promise.

Drama

I was very disappointed in "The Pirate," by S. N. Behrman, which Sam Wanamaker chose for his starring vehicle and for which the *Radio Times* gave such a lush blurb. It is obviously a comedy of situation and spectacle, and without these adjuncts the wit was not sufficient to sustain one's interest or keep one amused for an hour and a half. The mesmerising scene could be very amusing in the theatre. Mr. Wanamaker, Marjorie Westbury and the others laboured very successfully against invisibility.

"Robert's Wife," by St. John Ervine, on the other hand, has a plot, a dialogue and poses issues of sufficient interest to overcome this handicap. A very good and interesting play of ideas in the Shavian manner, beautifully played by Dame Edith Evans with Patrick Barr, Kynaston Reeves and Cyril Chaps. The Church, pacifism and careers for married women were the chief subjects discussed by the protagonists. The way Robert's wife, a doctor practising birth control—Robert is a clergyman—is, in the dying moments of the play, removed from her profession back to the domestic fold, as it were, bodily, is both a splendid coup de theatre and a lesson in how such things should be done.

In Strindberg's "Queen Christina" I found an absorbing play, history and the author's famous anti-feminism. Yvonne Mitchell was quite brilliant as the youthful Queen who was both a menace to her country and to each of the many men who fell under the spell of her charms.

"The Tenth Man" is early and good Maugham. What would any of us do who unhappily found ourselves confronted with the one chance in ten? Eric Portman was most powerful as George Winter and gave quite a tour de force. He was splendidly supported by the whole company.

Final Thought

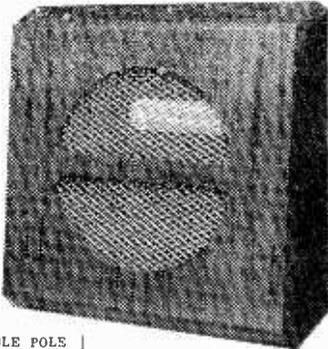
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T.C.C.	CE28L	24 x 8 mfd. 350 v.	2'6 ea.
T.C.C.	CE10P	24 mfd. 450 v.	3' ea.
T.C.C.	CE27L	16 x 8 mfd. 350 v.	3' ea.
B.E.C.	CE827	22 x 22 x 8 mfd. 350 v.	6'9 ea.
B.E.C.	CE15164	8 x 16 mfd. 350 v.	3'9 ea.
B.E.C.	CE2916	22 x 22 mfd. 350 v., 25 mfd. 25 v.	6'9 ea.
B.E.C.	CE562	64 mfd. 350 v.	2' ea.
B.E.C.	CE10610	16 mfd. 450 v.	3'6 ea.
B.E.C.	CE3007	32 x 72 pF 450 v.	7'9 ea.
B.E.C.	CE15749	8 x 32 mfd. 450 v.	3'9 ea.
B.E.C.	CE15592	16 x 16 mfd. 450 v.	2'9 ea.
T.M.C.	—	16 mfd. 450 v. (voltage limiting)	2'9 ea.
Ediswan	—	8 x 8 mfd. 450 v.	4' ea.
Dubilier	—	20 x 20 mfd. 500 v.	3'6 ea.
Dubilier	—	32 x 16 mfd. 350 v.	3'6 ea.
Dubilier	—	24 x 16 mfd. 350 v.	4'3 ea.
Dubilier	—	8 x 8 mfd. 350 v.	3' ea.
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T.C.C.	CE28L	16 mfd. 350 v.	2'9 ea.
T.C.C.	CE35L	24 mfd. 350 v.	3'6 ea.
T.C.C.	CE24L	8 mfd. 350 v.	1'1 ea.
Dubilier	—	8 x 8 mfd. 350 v.	3'6 ea.
Dubilier	—	8 mfd. 500 v.	3'3 ea.
Dubilier	—	100 mfd. 25 v.	1'9 ea.
B.E.C.	CE317	32 mfd. 450 v.	2'1 ea.
B.E.C.	CE15653	32 mfd. 350 v.	1'9 ea.
B.E.C.	CE312	16 x 16 mfd. 450 v.	4'8 ea.
Ediswan	—	8 x 16 mfd. 450 v.	4' ea.

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Dubilier	BR1950	16 mfd. 500 v.	3'6 ea.
Dubilier	BR2050	20 mfd. 500 v.	3'6 ea.
B.E.C.	CE508	8 mfd. 450 v.	2'1 ea.
B.E.C.	CE404	25 mfd. 25 v.	1'9 ea.
Ediswan	—	50 mfd. 50 v.	2'3 ea.

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2' ea. 5K Ω , 200 Ω , 2K Ω , 5K Ω , 10K Ω , 10K Ω Double, 25K Ω , 20K Ω , 50K Ω , 50K Ω , 500 Ω , all 2'4 each.
COLVERN CLR901, 1,000 Ω , 1'9 each.
COLVERN TYPE CLR901 -3K Ω and 5K Ω Double Unit, 1'9 each, 20K Ω , 10K Ω , 20 Ω , 1'3 each.

CONTROLS WITH DOUBLE POLE SWITCH

25K Ω , 2 Meg Ω , 1 Meg Ω , 1 Meg Ω , Log. 4 Meg Ω , 1 Meg Ω , 50K Ω , 20K Ω , all 3'9 each.

VOLUME CONTROLS SINGLE POLE SWITCH

500 Wire Wound 2.10 each. 5K Ω , 10K Ω , 100K Ω , 1 Meg Ω , 1 Meg Ω , Log. 2 Meg Ω , all 3'9 each.

STANDARD CONTROLS LESS SWITCH

50K Ω , 1 Meg Ω , 1 Meg Ω , all 2'6 each.
 Vexley Switch 1 pole 7-way ... 1'6 ea.
 Multi Ratio 5 Pole Vexley ... 6' ea.
 Vexley Switch 4 pole 3-way ... 2'6 ea.

EX. GOVT. CONTROLS ALL CARBON TRACK

500 Ω , 600 Ω , 1,500 Ω , Double type, 2K Ω , 5K Ω , 10K Ω , 20K Ω , 25K Ω , 50K Ω , 200K Ω , 100K Ω , 100K Ω , 1 Meg Ω , 1 Meg Ω , 1 Meg Ω , 2 Meg Ω , 25K Ω , Double type, 50K Ω Double type, 1'2 each.
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 Battery Charger Bulldog clips 3d. ea.
 465 kv's I.F. transformers ... 8'3 ea.
 Varnished Cotton Sleeveing, doz. yds., ... 1'6
 Wearite 12 v. Vibrators 4-pin 6'6 ea.
 Crystal Diodes Wire Ends ... 1'8 ea.
 Can type 20 x 20 mfd. 500 v. ... 3'6 ea.

FOR TERMS SEE OUR ADVERTISEMENT ON PAGE 316

VALVES GUARANTEED NEW AND BOXED

OZ1	6' - 6H6	4'6 80	8'8 DHT3M	9' - PY81	11'6
1A5GT	6'6 - 6J5G	5'5 - 807	8'8 E1148	2' - Q122B	7'6
1C5GT	8' - 6J5GT	5'6 8D2	2'8 ER041	11' - Q121	7'6
1L4	7'6 - 6J5GT	6'6 954	2' - EL42	11'6 - T122	8' -
1R5	7'9 - 6J74	6'6 955	4'8 E1H42	10'8 - U21	8' -
1R4	8' - 6J74	6' - 956	3'8 E2H35	13' - U16	6' -
1M5	7'9 - 6K7M	6'6 9001	6' - EB80	11'6 - U81	10' -
1T4	8' - 6K74T	6'6 9002	6' - EB41	11' - UB41	9'6
1U5	10' - 6K8G	6'6 9004	6' - ECL80	11'6 - UB41	11'6
220V8G	6'6 - 6K6GT	6'6 9006	6' - EP36	6'8 - UCH42	12'6
XC2	5' - 6K8GT	9' - 10C1	11' - EP41	10' - UF41	12' -
3A4	9' - 6A6	8'6 10F9	11' - EP80	11'6 - UY41	10' -
5Q4 (N18)	9' - 6L64	9' - 10L111	11' - EZ40	11' - EP39	6'6
3D6	5' - 6L74	7'6 12A7	6' - ERM3	9' - EB34	2'6
384	8'6 857	7'6 12A7T	9' - EY91	9' - EB32	7'6
4D4	8' - 6D74	9' - 12A7T	9'6 EY91	15' - EP30	6'6
4F1	3' - 6D74T	9' - 12S8	8' - EZ41	11' - SP61	3'9
42	8' - 6S4GT	8'6 12H6	5' - FC13	9' - EK32	8' -
5U0	8'6 6867	7'6 12J5	6' - HD14	10' - SP41	3'6
5Y3GT	8'6 6817	6' - 12K7	9' - H63	7'9 P61	3'9
2Z6	8'6 6J76T	8'6 12K84T	9' - H90	8' - EP50	6' -
6Z4G	6'6 68K7	6'6 12S87	5'8 HD13DD	8' - EP30 851	8' -
6A7	9'6 68L7	9' - 12S87	5'8 HD13DD	8' - EA50	2' -
6A8G	9'6 68N7GT	9' - 12S87	7'6 K72	5' - VR116	4' -
6A8GT	10'6 68Q7	9' - 12S87	7'6 K73C	10'6 DD14	4' -
6A7	6'6 68S7	8' - 12K87	6' - KT74	8' - EB8	6'6
6A3	7'6 68J4	8'6 12K87	7'6 K76	10'6 EP34	7' -
6AK5	9' - 6V64	8'6 12S87	8'6 K778	10' - EA52	5'9
6AL5	5' - 6V6GT	7'6 12Q7	9' - KTW61	7'6 VR105 30	9' -
6AM6	8' - 6X4	8' - 12D2	4' - KTZ41	6'9 VR150 30	9' -
6AT6	10' - 6X3GT	7'6 20I1	10'6 KTZ63	6'6 EL32	8' -
6AM3	9' - 6X44	7'6 25A6G	9' - M14	5'8 TT11	3'6
6BR4	4' - 7H7	8'6 25L6GT	8'6 MS.PEN	5' - VP23	8' -
6BE6	11' - 7H6	8'6 25Z4G	9' - OM9	9' - VC39	8'6
6C4	8' - 7C5	8'6 25Z6GT	8'6 PEN25	8' - VU11	3'6
6C6GT	7'6 7Q7	8'6 35L9GT	8'6 PEN36	8'6 VU20A	3'6
6C8G	7'6 7X4	8'6 35S6G	9'6 PEN220A	4'9 VU33	3'6
6C9	3' - 7H7	8'6 30P4GT	8'6 PL33	9' - W77	8'6
6D3	2'6 7T7	8' - AT164	6'6 PL83	13' - W81	10' -
6D6	7'3 757	8'6	8'6 X65	10' -	10' -
6P6G	7'6 7Q7	8'6 AC6PEN	5'6 PL89	11'6 X66	11'6
6S8G	7'6 7X4	8'6 35V6	6' -	11'6 V64	9' -
6G6G	6'6 75	10' - CV71	1' - PY80	11'6 V61	9' -

A SPECIAL PURCHASE OF TUNGSRAM VALVES ENABLES US TO OFFER THE FOLLOWING:

25Z5	9' - 10V6G	9' - AS4125	11'8 25V5	9' - LQ10	6' -
HP4101	11'8 4V6GT	9' - EB311	6'3 9H76	8'6 8P220	8' -
6J7G	9'6 9	9' - PV30	9' - 1P220	9' - HP210	5'9
				1HR210	5'9



SPECIAL OFFERS

GRAM AMPLIFIER.—Brand new three-valve amplifier. Suitable for standard and LP records. Fitted with volume and tone controls. A.C. mains 200/250 volts only. Supplied complete with three valves. Suitable Pick-Ups and Speaker are listed below. PRICE £4.15.0 post free.

PICK UPS. Goldring 130. Magnetic for 78 records, 33/-; ACOS GP30. Turn-over crystal for 78 and LP, 66/-.

SPEAKER. 8in. well-known make, 22/6.

TR 1196B TRANSMITTER RECEIVERS. Brand new. Complete with nine valves (EF50, EL32, TT11, EBC33, EK32, two EF39, two EF36). This unit contains the well-known Receiver Unit type 25 and which can be converted to a broadcast receiver. Complete in transit case.

PRICE £3.0.0. Carriage paid.

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Dual Range Miniature 2/6 with Crystal Set Coil with Circuit

Dual Range Coil 4/- with 2 Mains and with Reaction 2 Battery Circuits

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Best Buy at Britain's

FILAMENT TRANSFORMERS

Standard tapped primary, two types: Type "A," 12 volts 11 amps, 6.3 volts 11 amps; Type "B," 12 volts 11 amps, 4 volts 11 amps. Either type 7/6.

TELEVISION RECTIFIERS. 3in. long. 2in. dia., 235 volts A.C. input. Type "A" Output 300 mA, price 13/6. Type "B" Output 380 mA, price 14/6. Brand-new. Either type 1/- post.

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R1155. Brand-new £119.6. Soiled £7.19.8. Carr. 10/6 ex. Send 1/3 for circuit and data.

R1155 POWER PACKS. Three types—at £4.10.0. £5.5.0 and £6.10.0. Send S.A.E. for details.

A2074 contains standard mains transformer 315-315 v. 70 mA, 6.3 v. 2A and 5 v. 2A (Admiralty rating), paper smoothing, 10 Hy choke, etc., etc. In steel case 11in. x 18in. x 6in. and in mint condition.

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RINGING CHOKES to supply 2.5 kV. E.H.T. using EF50 v. 12/6. or with EY51 Re-tifier, 35/6. Full instructions with each choke.

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BRIDGE RECTIFIERS suitable for use with the above transformers, 2 amp., 11/3; 3 amp., 12/6; 4 amp., 15/-; 6 amp., 23/6; 10 amp., 30/-; Post 1/4.

HALF WAVE. 125 volts A.C. input. RMI 60 mA., 3/9; RM2, 120 mA., 4/3; RM3, 125 mA., 5/3; RM4, 250 v. 275 mA. for T.V., 15/6; DRM2B, 120mA., 250 v., 10/9. Post 6d.

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VALVES.—6AM6, 6CH6, 6RA6, 6BH6, 6RF6, 12BE6, 6C6, 6BW6, 3A4, 1U5, 6AL5, W77, N18, 6BJ6 50C5, 1S5, 7/6 each; 6K8gt, 12K8gt, 1R5, VR150 30, 6BH7, 9/6 each.

35 Tenison Way, London, S.E.1.

TELEGRAM AMPLIFIERS

£3.19.6 P. & P. 2/6d.

Fits inside your record player leaving room for speaker. Dimensions 10in. x 31in. x 2 1/2in. 4 watts quality output. Suitable for all speakers and with standard or L.P. pick-ups. Built-in power pack for 200-250 v. A.C. only. Valves 6J7 and 6V6 available at 20/- per pair extra, if required. Other models with neg. feedback, etc. 6d. stamp for illustrated details.

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PRE-TUNER 5-CHANNEL TV. SUPER-HEAT VALVES. 6BW7 and 12AT7. Fit one of these to your set for better pictures. 52/6.

SPECIAL OFFER. New and boxed ARP12/VP29 valves, 5/6 each, 4 for £1.

FISHING ROD AERIALS. 12in. Set 3, 7/6. Mounting Base 3/6. Screw-in Type, 9/6.

0-5 AMPMETERS. 2in. square M.C. 11/-.

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SELENIUM RECTIFIERS. F.W. 6 or 12v. 4A., 22/6; 5A., 30/-; 3A., 14/6; 100 mA., 3/6; 1A., 8/6; 24v. 2A., 30/-; 250v. 100 mA., H.W., 9/-; 250v. 275 mA., 17/6.

TRANSFORMERS. 200-210 volts, tapped 3-4-5-6-8-9-10-12-15-18-20-24 and 30 volts at 2 A., 21/6. Tapped 17-11-5 volt 5A., 22/6; Tapped 17-11-5 volt 1 A., 16/6; 6.3v., 2 A., 8/-; One year guarantee.

MC MICROPHONES AND TRANSFORMERS. 15/6.

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MINIATURE VALVES. New, 9091, 9002, 9003, 7/6; 6AG5, 1S4, 1S5, 1T4, 1R5, 10/6; 6AL5, 8/6; 12AT7, 6AM6, DH77, 6A7B, EP91, EP92, EY51, 6BE6, 11/6.

NAV VALVES. 35Z4, 25L6, 25Z4, 25L6, U281, U50, 5Y3GT, 6K7GT, 6V6GT, 50L6, 42, 80, 11/-; 6K8GT, 11/26, 12/6.

NAV 0-100 MICRO-AMP METERS. 41in. Made by Ernest Turner. £4 12/6.

TR.1196. Transmitter Section. New and complete, 4/6.8 Mo's. Easily converted. Less valves 15/-; with valves £2.

BREAST PLATE TELEPHONE CARBON MICROPHONES. 4/-; Throat Microphones with cord and plug, 4/-.

ALL POST PAID IN U.K.

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A REALLY SMALL RADIO RECEIVER

This radio receiver, although as small in size as a matchbox, gives loud, clear reception of the BBC Home, Light and Third Programmes on the medium waveband, about 180-550 metres. The set also tunes the Light Programme on the long waves, 1500 metres. No catwhiskers, valves, or batteries are required, and the receiver works off a short indoor aerial in many districts.

PRICE **9/-** POSTAGE 3d. EXTRA

This offer applies only to Gt. Britain, and Northern Ireland.

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SPARKS' DATA SHEETS

Constructional Sheets of Guaranteed and Tested Radio Designs

IF YOU WANT A REALLY EFFICIENT PORTABLE

It will pay you to send for the Full Constructional Details of

THE "ECLIPSE"

All-Dry Battery Superhet Portable. A Tried, Tested & Guaranteed Design of the Personal Portable Type. Neat, Compact and Efficient.

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FULL SIZE EASY TO FOLLOW BLACK AND WHITE DATA SHEET showing all details and simple point-to-point wiring.

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COMPLETE WITH FULLY DETAILED DESCRIPTIVE MATTER. The Circuit covers Medium- and Long-waves, and as it incorporates the Latest type of Valves is most economical on batteries.

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Mathematics and the Service Engineer

SOME OF THE SIMPLER FORMULÆ EXPLAINED

By F. E. Apps

FOR the radio and/or television service engineer to be really efficient, it is necessary for him to keep up to date with all the advances of science in his particular job. To do this, he must read and thoroughly understand the various technical articles given in the many technical journals and books that are published from day to day. For a real understanding of these articles, it is imperative for him to know quite a reasonable amount of mathematics. This is because practically all these textbooks and articles give formulæ. Now formulæ in a technical article are as necessary as maps in a book on geography. They illustrate to a discerning mind the main points of the text, and for a reader to peruse one of these articles without the faintest idea what

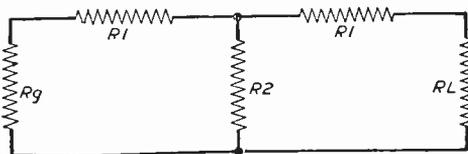


Fig. 1.—A "T" Attenuator.

these formulæ mean is a waste of time, as he cannot really follow the gist of the article if he does not understand them.

Now, if the foregoing is accepted, then it is necessary to find out what mathematics, etc., are needed by the service engineer, and also how far it is necessary for him to go in his studies.

Most service engineers, I believe, have an education up to the ordinary national certificate, which enables them to solve ordinary arithmetical problems; but more is required, especially now that complicated circuitry is being employed, for instance, in television and pulse circuitry notably. The subjects required are, in my opinion, geometry, algebra, trigonometry, indices, graphs and logarithms. Also a knowledge of the standard symbols used, including the Greek and English letters used as such. A list of books suggested may be obtained from this office.

Geometry and Trigonometry

These two subjects are, of necessity, bound up with each other and are required for the purpose of understanding angles of lead and lag, and vector diagrams. Some of the simpler trigonometrical formulæ should be memorised, such as

$$\cos^2 \theta + \sin^2 \theta = 1$$

$$\sin \theta = \sqrt{1 - \cos^2 \theta}$$

$$\cos \theta = \sqrt{1 - \sin^2 \theta}$$

$$\tan \theta = \frac{\sin \theta}{\cos \theta}$$

$$\text{Power factor} = \frac{EI \cos \theta}{EI} = \cos \theta =$$

cosine of the angle of phase difference between the line voltage and the current.

Indices

To be conversant with these is very necessary. One often meets such things as this in formulæ

$$2.3 \times 10^{-6}$$

$$3 \times 10^8, \text{ etc., etc.}$$

Only a short period is required to know this quite thoroughly, but unless you understand them the whole thing might just as well be written in Chinese.

Graphs

Most articles on electronics have at least one graph. They are mostly connected with valve characteristics, acoustical response of loudspeakers, and also vision response curves of television receivers. To be able to read these as easily as the written word is of enormous value to the engineer. It is helpful in studying graphs to make up some of your own, using any two associated factors and reading the resultant off on a curve and then proving same mathematically.

Algebra

This is definitely a "must," and should go at least as far as simultaneous equations and on to quadratics, if possible. I do not think the "j" factor or the calculus need be included.

Here are a few formulæ showing the need for algebraical knowledge.

For a T attenuator as Fig. 1

$$R_1 = RL \left(\frac{\alpha - 1}{\alpha + 1} \right)$$

$$R_2 = RL \left(\frac{2\alpha}{\alpha^2 - 1} \right)$$

For a Wien Bridge measuring audio frequencies as Fig. 2

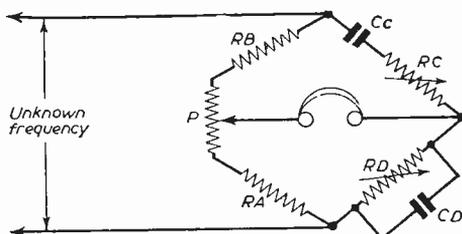


Fig. 2.—A Wien Bridge measuring audio frequencies.

$$f = \frac{1}{2\pi \sqrt{RC RD CC CD}} \text{ also } \frac{CD}{CC} = \frac{RB}{RA} - \frac{RC}{RD}$$

When $CC = CD$, $RC = RD$ and $RA, RA' = 2$

$$\text{Then } f = \frac{1}{2\pi RC CC}$$

Now beyond all this, there are many formulæ that apply particularly to electronics with which it is necessary to be very conversant. Amongst them the following will be found necessary.

$$\text{Ohms Law for D.C. } I = \frac{E}{R}$$

$$\text{Ohms Law for A.C. } I = \frac{E}{Z}$$

$$\text{Impedance } Z = \sqrt{R^2 + \left(\omega L - \frac{1}{\omega C}\right)^2}$$

$$\text{RMS value} = \frac{1}{\sqrt{2}} \times \text{max. value}$$

Resistances in series, parallel or series parallel.
Condensers in series, parallel or series parallel.
Inductances the same.

The relationship of frequency to wavelength

$$WL = \frac{\text{Velocity}}{\text{Frequency}}$$

Capacity of parallel plate condenser

$$C = \frac{NKA}{4\pi d}$$

The charging of a condenser where $Q=CV$ and the energy stored is $\frac{1}{2}CV^2$. The time constant of circuit containing C and $R = CR$ seconds. The wavelength of an oscillatory circuit

$$WL = 1885 \sqrt{LC}$$

Inductance of a single wound coil

$$L = .7^2 d^2 n^2 K \times 10^{-9}$$

Now this list may seem formidable, but it is only a very few of those required. Many a service engineer will, no doubt, say that all this knowledge will not assist him in locating an intermittent fault in a radio

or television receiver any quicker. That may be so directly, but indirectly it will help because with this knowledge he is able to read more about his own particular branch of science and be able to set about the job in a more knowledgeable manner.

Test Equipment

With the more complicated circuitry now employed, more elaborate testing equipment is necessary. Now the price of instruments, such as the oscilloscope, the Q meter, and inductance and capacity bridge, puts them beyond the reach of many service engineers, so they have to make do with instruments they have built themselves. Now although many circuits are given of test equipment in PRACTICAL WIRELESS and *Practical Television*, many engineers may wish to alter these designs to suit their own particular requirements. To do so may mean circuit alteration that may have a deleterious effect upon the efficiency of the instrument concerned. This is where "maths" can help by enabling the engineer to work out the correct value of the required new components and estimate very accurately their effect upon the circuit as a whole.

Then, again, many service engineers have "brain-waves" about how to achieve a certain result with an entirely new circuit idea. In most of these cases many, many hours of work and much heartbreak would be avoided, when it is finally found that it does not work, if the engineer in question had only worked it out mathematically beforehand and seen he was attempting the impossible.

A Charter for Mobile Radio

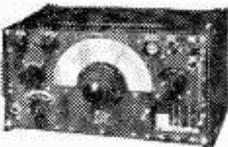
THE following points are put forward by the Mobile Radio Users' Association as being of paramount and urgent importance from the point of view of users of mobile radio:

1. The Government should recognise mobile radio as a service of great importance which has a real contribution to make to the national economy.
2. The Government should state that it will do all in its power to encourage the full use and extension of mobile radio.
3. The Government should undertake that the views of users of mobile radio will be considered when decisions affecting them are taken, and that the Mobile Radio Users' Association will be officially recognised and called into consultation together with other interested bodies.
4. The Government should maintain available an adequate supply of frequencies upon which the mobile radio services can operate effectively.
5. The Government should undertake that frequency allocation shall be conducted in accordance with the following principles:
 - (a) The total bands available for mobile radio should be clearly and publicly defined, in order to give security to users and manufacturers. This is essential, particularly for long-term development.
 - (b) The block allocation of frequencies should be made for a stated period, to be not less than 10 years, and then in the event of a change of

frequency, due to Government action, the principle of compensation should apply.

- (c) The use to which all individual frequencies within a particular block are put should be made public.
 - (d) The blocks of frequencies available to mobile radio should, as far as possible, be protected from interference by users in adjacent blocks.
 - (e) There should be recognition of the fact that although a large number of channels can be made available for mobile radio, the number is not unlimited, and due regard must be paid to this fact in allocating frequencies, in order to prevent overloading of channels.
 - (f) In making more frequencies available to mobile radio, the Government should recognise that many classes of user would be satisfied with a frequency made available on a strictly peace-time basis. It is believed that there are many frequencies, at present allocated to military purposes and unused in time of peace, which could readily be made available to civil users.
6. At a time when Ministers are calling upon transport and industry to reduce costs in the face of foreign competition, and in view of the acceptance by Government publications and Government-sponsored Productivity Committees of the importance of mobile radio in providing an economic means of communication, and in view of its importance to health and safety, all the above points should be treated by the Government as matters for urgent decision.

EX-A.M. RECEIVER TYPE R1155



Brand new and unused
5 Frequency ranges: 1.5-7.5 Mc/s; 7.5-3.0 Mc/s; 1,500-600 Kc/s; 500-200 Kc/s; 200-75 Kc/s
Supplied in maker's original wood transit case. LASKY'S PRICE £11/19/6 Complete.
R.1155 Receivers. Secondhand aerial tested. £7/19/6.
Carriage and packing 12.6 per unit extra, including 10/-, which will be refunded on return of packing case.

ASSEMBLED POWER PACK OUTPUT STAGE FOR R.1155 RECEIVER



For use on 220-250 v. A.C. mains. Complete with 2 valves. In metal case size: 12 x 7 x 5 1/2 ins. LASKY'S PRICE, 79/6. Carr. 5/- extra

Power Pack as above. Fitted with 6 1/2 in. p.m. speaker. LASKY'S PRICE. £5/5/-. Carriage 5/- extra.

PORTABLE RECORD PLAYERS

Containing a new Plessey single speed automatic record changer. (78 r.p.m.). Magnetic pick-up, and 2 valve amplifier, with metal rectifier. For use on 200-250 v. A.C. mains. Amplifier uses EF 36 and EL 32 giving 3-watts output, tone and volume controls, 5 in. speaker. In rexine covered cabinet, size: 17 x 17 x 8 ins. With carrying handle. LIMITED QUANTITY. LASKY'S PRICE. £10/19/6. Carriage 10/6 extra. Though store soiled, these players are new and every one is fully tested before despatch.

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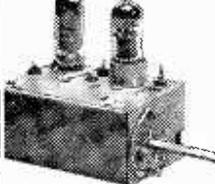
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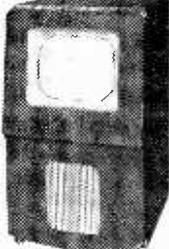


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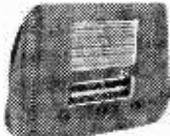
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2AS5	—	8/0	6Q7CT	10/0	8/9	EB91	—	2/3
6AK5	—	8/8	6S10	5/8	—	EC31	—	2/6
6AM6	—	6/3	6SK7	6/9	—	EC2H	—	7/0
6B4	7/8	—	6V6CT	8/6	—	EC180	—	11/6
6H6	3/8	—	6V6S	—	6/9	EF50	—	10/6
6M4T	5/0	—	9D6	—	7/9	KTW41	—	6/3
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6K7	6/9	—	751	2/8	—	VU111	3/0	—

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Surplus Frequency-changer Valves

DETAILS OF EX-SERVICE VALVES, WITH BASE CONNECTIONS

By E. G. Bulley

VALVES of this design are so named because when installed in a suitable circuit they convert an alternating current at a certain frequency into a current of lower or higher frequency without any undue distortion. They are, of course, found in superheterodyne circuits, wherein the frequency of the incoming signal is converted to that of an intermediate frequency. The latter is then amplified before being rectified in the second detector stage.

The essential requirement of a frequency-changer valve is that it has an oscillator section as well as a mixing part.

The input to the actual valve consists of two frequencies, namely, that from the local oscillator and the other from the incoming signal. These frequencies are combined and converted as previously mentioned. However, the output consists of many

Various Types

There are numerous types of valves for frequency changing, but as we are only concerned with those available upon the surplus market, they will, therefore, only be dealt with in this article.

With reference to the tabulated list of valves, the reader will note that there are several triode-hexodes. Such valves, however, consist of a triode and mixing section in one envelope. The latter section has a separate anode and four grids, the cathode being common to both the triode and hexode parts of the valve.

It is usual practice, however, for G1 to be the control

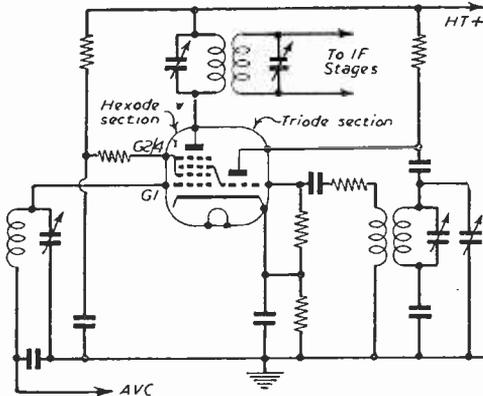


Fig. 1.—Basic triode-hexode circuit.

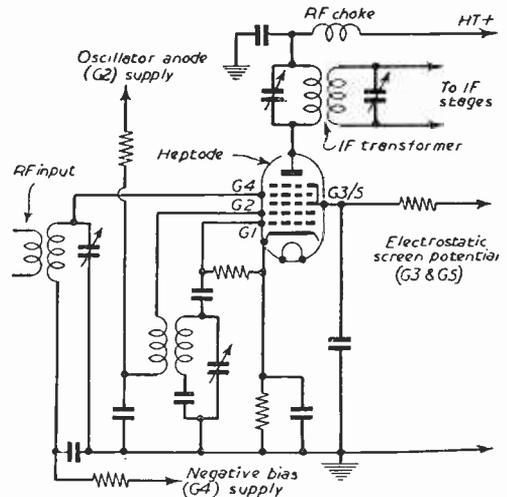


Fig. 2.—Basic circuit of heptode frequency changer.

more frequencies, the main ones being the sum of the two input frequencies, the difference of the two input frequencies and, furthermore, the oscillator frequency. Nevertheless, one must not overlook the fact that these frequencies generate harmonics which will generate still more frequencies of different values.

SURPLUS FREQUENCY-CHANGER VALVES

British Type	Cathode	Vf	If (amps)	Va (Max.)	Ia	V _{G2} Max.	Base
ARH1	1.H	6.3	0.3	250	—	150	0 (Hept)
ARTH2	1.H	6.3	0.3	{ 150 (Triode) 300 (Hex) }	2.2	100	0 (Triode Hex)
VR57A	1.H	6.3	0.2	300	1.0	225	0 (Octode)
VR99A	1.H	6.3	0.3	{ 100 (Triode) 300 (Hex) }	3.0	200	0 (Triode Hex)
VT147	1.H	4.0	1.2	{ 150 (Triode) 250 (Hex) }	—	80	B7 (Triode Hex)
<i>U.S.A.</i>							
VT151	1.H	6.3	0.3	330	3.6	220	0 (Hept)
VT151B	1.H	6.3	0.3	330	3.6	220	0 (Hept)
VT87	1.H	6.3	0.3	330	3.5	110	0 (Hept)
VT208	1.H	7.0	0.3	300	3.5	100	LOK (Hept)
VT194	1.H	6.3	0.3	{ 275 (Triode) 300 (Hex) }	6.0	110	0 (Triode Hex)

grid and G3 as the injector grid. This grid is internally connected to the grid of the triode unit. The injector grid is shielded by G2 and G4: these grids are internally strapped and so prevent electrostatic interaction between the oscillator and signal grids.

Type	BASING									
	1	2	3	4	5	6	7	8	TC	
ARTH2	M	H	A	G2-G4	G1-G3	A1	H	C	GI	
VR57A	M	H	A	G3-G5	G1	G2	H	C & G6	G4	
VR99A	—	H	A	G2-G4	G1-G3	A1	H	C	G1	
VT147	A	G1-G3	G2-G4	H	H	C	A1	—	G1	
VT151	S	H	A	G3-G5	G1	G2	H	C	G4	
VT151B	S	H	A	G3-G5	G1	G2	H	C	G4	
VT87	S	H	A	G2-G4	G3	—	H	C & G5	G1	
VT208	H	A	G2	G1	G3-G5	G4	C	H	—	
VT194	H	A	A1	G1-G3	G2-G4	G1	C & G5	H	—	

A basic circuit using a triode-hexode is shown in Fig. 1, and may prove of interest to the newcomer to radio.

Another type of frequency changer that seems to be in plentiful supply is the heptode, or pentagrid as it is sometimes called. Such a valve has seven electrodes, namely, the anode, cathode and five grids. These valves are so constructed that they have a tetrode and triode unit, both sections being coupled by a common electron stream.

This electron stream is accelerated through G1 (oscillator grid) by the positive potential on G2, otherwise called the oscillator anode. However, some of the electrons shoot past G2 and G3 and approach G4, which is, in effect, the modulation electrode or grid of the tetrode unit.

Furthermore, G4 is operated at a negative potential

and does, therefore, retard the electrons that have passed through G2 and G3. This phenomenon creates a cloud of electrons between G3 and G4 and forms what is known as a virtual cathode. Electrons are, therefore, drawn from this source similar to the process in which they were accelerated from the cathode proper.

The R.F. signal voltage is fed to G4 and the I.F. output circuit is connected in the anode proper. It may be as well to mention, however, that G3 and G5 are internally strapped and form the electrostatic screen.

Such a valve can be connected in a circuit as shown in Fig. 2, wherein the tetrode unit is modulated by the oscillator section, solely by the variation of the electron stream from the cathode. Valves of this type are to-day very popular and will prove interesting to those who wish to experiment with frequency changer circuits.

News from the Clubs

CLIFTON AMATEUR RADIO SOCIETY

Hon. Sec. : C. H. Bullivant (G3DIC), 25, St. Fillans Road, S.E.6.

ATTEENDANCE remains at a high level and several new members were welcomed during the past few weeks. Meetings continue to be held every Friday at 7.30 p.m. at the clubrooms, 225, New Cross Road, S.E.14.

It is hoped to run a series of DF events again this summer, when members will compete for the DF shield, and an evening will shortly be devoted to a talk, with hints and tips, by last year's winner. Transmitting and listening contests continue to be popular and the next is scheduled to be held in April.

EDINBURGH AMATEUR RADIO CLUB

Hon. Sec. : D. Black, 16, Edina Place, Edinburgh, 7.

THE Club meets every Wednesday at 7.30 p.m. in the clubrooms, 16, Bothwell Street (off Easter Road), Edinburgh. Morse and Radio Theory classes for the Radio Amateur Examination are held every week and all interested are invited to attend. Fuller particulars may be obtained from the Hon. Secretary.

BRIGHTON AND DISTRICT RADIO CLUB

Hon. Sec. : T. J. Huggitt, 15, Waverley Crescent, Brighton, Sussex.

THE club Tx. under the call-sign G3EVE is on the air on both phone and C.W., 180 metres and top band.

Morse instruction is now a regular feature and Mr. E. Bannister has commenced a series of talks on "Radio Mathematics." The Club meets every Tuesday at 7.30 p.m. at the "Eagle Inn," Gloucester Road, Brighton.

LEEDS AND DISTRICT AMATEUR RADIO SOCIETY

Hon. Sec. : B. A. Payne, 454, Kirkstall Road, Leeds, 4.

MEEETINGS are held on Wednesday evenings at the Swarthmore Educational Centre, where visitors are always welcome. Recent events were a visit to the Radiotherapy Dept. of the Leeds General Infirmary on March 17th and a talk, "Realistic Sound Reproduction," by Dr. K. A. Exley, on March 31st.

SOUTHEND AND DISTRICT RADIO SOCIETY

Hon. Sec. : J. H. Barrance, M.B.E., 49, Swanage Road, Southend-on-Sea, Essex.

MR. W. A. SMITH, B.Sc., of Hockley, continued his talks on "Aerials and Wave Guides," on March 5th in Room L, Queens Road Laboratories of the Municipal College. He pointed out and illustrated how an unmatched aerial causes "standing waves" to appear on the aerial system, resulting in loss of radiation on the true frequency of a transmitter and inferior reception on a receiver. He also showed how, by a simple device, reflections from the aerial the cause of these obnoxious "standing waves" could be eliminated.

Mr. J. L. Goss presided.

ACTON, BRENTFORD AND CHISWICK RADIO CLUB (G3IU)

Hon. Sec. : R. Hindes (G3IGM), 85, Inverness Terrace, W.2.

CLUB meetings at high level are held each Tuesday evening at the A.E.U. Rooms, 66, High Road, Chiswick, W.4, from 7 to 10.

February activities included a lecture, "Radio in Aviation," given by G3BPM, also a visit to the L.P.T.B. power station at Lots Road was ably organised by G3GEH.

Future events include lectures on "DX peditions" and "History of Amateur Radio" to be given by G6LX and G3VA respectively.

WEST LANCs RADIO SOCIETY

Hon. Sec. : S. Turner, 5, Balfe Street, Seaforth, Liverpool, 21.

THE annual general meeting of the club took place on Tuesday, March 9th. Officers elected were Mr. T. Searle (president), Mr. S. Turner (secretary) and Mr. F. Clusby (treasurer). After the formal business of the meeting was over, a lively discussion took place regarding future programmes: everything of interest was suggested, e.g., Practical, Technical and Morse classes and Talks, Films and Visits. The building of the club's transmitter was also discussed. A temporary rig for top-band C.W. is in use, call sign G3JQA. The club meets every Tuesday evening at 8 p.m. over Gordon's sweetshop, St. Johns Road, Waterloo, Liverpool 22. New members and visitors warmly welcomed.

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OPEN TO DISCUSSION

The Editor does not necessarily agree with the opinions expressed by his correspondents. All letters must be accompanied by the name and address of the sender (not necessarily for publication).

The "Gothic"

SIR,—Your article in the January issue describing the wireless installation in the *Gothic* said that the 7 kW. transmitter was believed to be the most powerful ever fitted to a merchant vessel. The old Cunarder *Caronia* was fitted for some years with a 10 kW. Poulson Arc transmitter. It was scrapped in 1925.—A. R. COOMBER (Maidstone).

Extended Use of Tape Recordings

SIR,—With reference to your issue dated February, 1954, we would venture to observe that this Company has supplied the British Broadcasting Corporation with portable high-grade magnetic-tape recording equipment, certain of which is at present being used on the Royal Australasian Tour. This Company has also supplied the Corporation with certain tape recording accessories including a quantity of our bulk erasers, the LeeRaser.—J. F. J. COOPER (Sales Manager, Leever-Rich Equipment Limited).

Whilst we are always pleased to assist readers with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying surplus equipment. We cannot supply alternative details for receivers described in these pages. WE CANNOT UNDERTAKE TO ANSWER QUERIES OVER THE TELEPHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupon from page iii of cover.

A.C. or D.C.?

SIR,—I am writing to you having received some encouragement from February's issue of PRACTICAL WIRELESS to ask you to add my name to the list of D.C./A.C. enthusiasts. Although I am only a "potterer" as far as radio goes I would most certainly welcome circuits that would allow me to make use of my D.C. mains. At the same time I realise that to cater for us D.C. people must present some problem. For we are a small number and continue to grow smaller.

In the past the PRACTICAL WIRELESS gave considerable circuits of battery and A.C. receivers, but few for D.C. stuff. I rather feel there must have been a reason for this and that you have tried to cater for the majority. Nevertheless I'll add my plea for a D.C. circuit and point out that the commercial people can produce some very fine radios and television sets that are worked by the old "Steam" D.C. Surely us D.C. users are a worthwhile market? —C. JEWELL (London, N.I.).

Improving Superhet Performance

SIR,—With reference to my article in the March issue, "Improving Superhet Performance," I must apologise for an omission from the text. The tuning indicator I have shown in Fig. 6 is really an output watt-meter and the needle will oscillate in sympathy with the signal being received. It is neces-

sary to steady the needle by careful use of the meter set and audio gain before commencing any adjustments. If this is done I have found the meter quite useful for the purpose indicated.—K. C. IRELAND (Ealing).

Radio Sales Losses

SIR,—Reading in the March issue of PRACTICAL WIRELESS about Philips Electrical Ltd. wishing to re-establish the popularity of sound radio, here is one reason why the public will not buy sound radio communication receivers.

I wish to buy a three or four valve set for my nephew, who is in the Boy Scouts, so that he can practise receiving messages in the Morse code. He wishes later on to become a radio officer at sea.

I am unable to buy a communication receiver complete; all I am offered is a blueprint to build one for him and a list of several items to make a set.

Personally, I do not know anything of the mysteries of a wireless set, and even if I did I have not the time to build this receiver.

If I wished to make a present of a bicycle or electric train set, I am not offered a blueprint and told to build it myself, buying wheels at one shop, frame, lamps, bell, dynamo, etc., at others. I can buy these articles complete and ready for use.

So why cannot one buy a simple communication receiver for a learner all complete and ready for use by plugging in on the electric mains?

According to advertisements there is a big shortage of radio officers for the Merchant Navy and the Forces, so there should be a good market for learners' receivers; every Scout and Girl Guide needs them to practise the receiving of radio code messages.

Probably the wireless companies who are in need of learners will see that some of these sets are placed on the market for amateur use.—H. M. GARDNER (Portslade).

Radar Reporting Unit

SIR,—The Commanding Officer, Wing Commander Fennessey, asked me before he went abroad to convey his personal thanks to you for printing the paragraph on this unit. This has resulted so far in 61 men applying to join this unit, and, moreover, of exactly the type that we find we can train quickly and efficiently. As the training of radar operators is of paramount importance you have done the country good service by helping in this matter.—R. L. ROBERTS, Fg. Off. (Recruiting Officer, for Officer

Commanding 3700 Radar Reporting Unit, Royal Auxiliary Air Force).

Modification of the 38 Set

SIR—Some readers might be interested in alterations I made to the receiver section of the type 38 ex-Army "walkie-talkie."

I found that the sensitivity was rather poor; only two or three stations were obtainable in the set's frequency range (7.4-9 Mc/s). This was due largely to a rather insensitive copper-oxide rectifier located near the I.F. coils. When this was replaced by two germanium diodes in parallel, the sensitivity was excellent.

By manipulation of a trimmer near the tuning condenser I was also able to extend the range to 7 Mc/s; consequently the set is very useful for listening on the "40" band.—M. H. I. BAIRD (Helensburgh).

Battery Receivers

SIR—I was very interested in "Thermion's" article in the March issue on "How Many Battery Set Users?"

I think many people prefer a battery set because it is much quieter in operation, but go for a mains set because the majority of battery sets give such poor reproduction. Surely with the vast strides which have been made in valve construction it should now be possible to manufacture a battery set capable of giving first-class reproduction for a very low battery consumption. What has happened to push-pull output in battery receivers? Why cannot a manufacturer produce a set with push-pull output and a phase inverter preceding it? In my view there is a vast field still unexplored for battery sets, always provided the quality of reproduction is comparable with a mains receiver. A receiver badly needed by the over 60s in both battery and mains is a three-button job, marked Off, Home, Light, with first-class quality using at least a 10in. speaker.—H. WHETTER (St. Austell).

A.C./D.C. Retrograde?

SIR—In the February issue of PRACTICAL WIRELESS I read with concern your comments about making all your designs A.C./D.C. I sincerely hope you are not going to adopt this questionable practice just to please a small minority who must be outnumbered by ten to one.

It is generally admitted that A.C./D.C. circuitry is a compromise, and in addition it presents a number of difficulties in practice. Live chassis, hum and limitation of H.T. volts are only too well known. To resort to this in a country where the grid system supplies 230 volts, 50 cycles A.C. over a vast area is, in my opinion, a retrograde step to say the least.

It may just as well be argued that all circuitry published should be A.C./D.C./Battery in order to pacify those readers who have no mains at all. Then, in theory, you please everyone. No, your best

policy is to continue as before and follow up an important A.C. design, e.g., the "Coronet," with an A.C./D.C. version. Surely no reader on A.C. mains would complain of the space devoted to this.

If you give way and cease to publish A.C. designs in order to gain the support of a few hundred D.C. readers, you may well lose the support of thousands of A.C. readers in the process.—L. D. C. PARKER (Bath)

Long-range F.M.

SIR—For the last year I have been in possession of a simple super-regenerative V.H.F. receiver which, in spite of many modifications, covers 85 to 130 Mc/s fairly comprehensively. This band, of course, includes both the Wrotham F.M. and A.M. stations as well as many police, fire, ambulance and aircraft services. However, being a Leeds operator, I did not expect to hear anything from a station as far away as Wrotham (at least 200 miles), especially since there is no R.F. amplifier, and the aerial is a dipole with no directive properties whatsoever. Consequently on hearing music issuing from the speaker one morning I thought nothing of it, thinking that it was a break-through on the wiring from my R1155. Imagine my surprise when I heard a voice announcing that "This is Wrotham; we are now closing down." Fortunately I had the tape recorder running at the time and have this announcement as a treasured possession, although since that date I have heard Wrotham often, the set picking up each sideband of the F.M. transmission separately to give reasonable results, and the A.M. transmission also. The signal is quite weak, and I can receive it only at certain times, but to receive it at all at that distance with only one R.F. stage seems quite a feat. What do your readers think?—C. B. HANSON (Leeds University).

CROSS-OVER NETWORKS

(Concluded from page 301)

when the cone of one speaker moves forward that on the other should also move in the same direction. A reduction in volume will be noted if they are incorrectly phased, whilst it is also possible to introduce a form of distortion from the same cause. The leads to the speakers should, therefore, be of red and black flex and they should be fitted after testing the movement by means of a low-voltage cell.

Separate Amplifiers

For those who wish to go farther in the direction of high-quality reproduction there is the possibility of using two separate channels for the two frequencies, again using the same principles as in the cross-over network, but including the components after, say, the first audio stage. The separate channels would then be fed into further audio stages with the output stages chosen according to the channel used, i.e., push-pull triodes for the bass and perhaps a single pentode for the treble unit.

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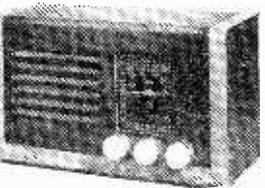
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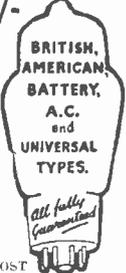
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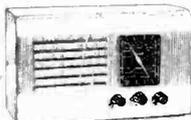
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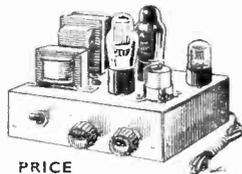
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