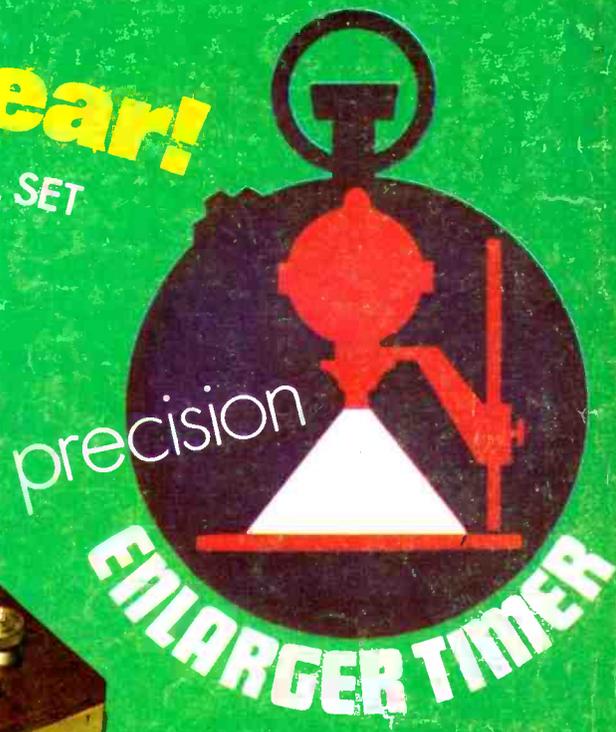
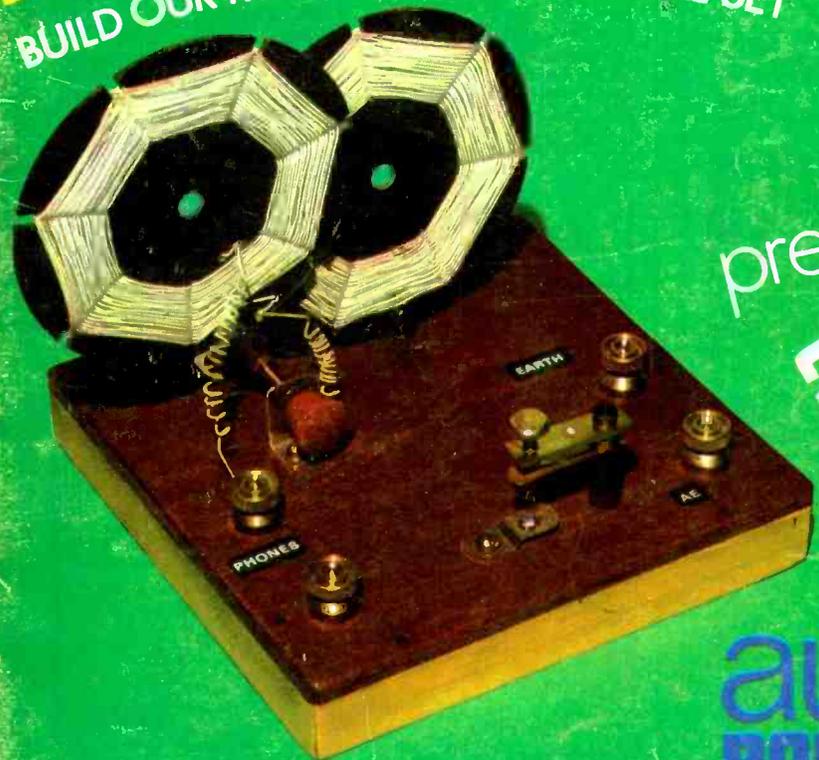


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SEPTEMBER 1972

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BUILD OUR REPRODUCTION CRYSTAL SET



SELECTIVE



4-BAND RECEIVER

auto PARKING LIGHT



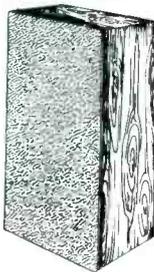
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THE SHELLEY

Size 21 x 11 x 6 1/2 in.

An extremely elegant speaker system made of 12mm. chipboard covered with black leathercloth with mottled Vynair front. This unique system uses three ex-TV speakers. Carefully matched and tested. Will handle 10 watts and will match 8 ohms impedance, if preferred the speakers can be wired in series parallel to match 3 ohms impedance. A real bargain at £5 15 plus 70p. P. & P. MATCHING TRANSFORMER for 15 ohms 87p post free. British Isles. Send for Hi-Fi & Electronic Catalogue 7p. each.



CARTRIDGES—Stereo

Sonotone 9TA H/C Diamond £2 40. Ronette S105 Medium Output, £1 40. S106 High Output £1 40. Acos GP93/1 Sapphire, £1 90. GP94 1 Sapphire, £2. TA700 equivalent to B.S.R. SKIM, £1 75. Japanese equivalent to B.S.R. TC8s, £1 75. P. & P. 7np on each.

CARTRIDGES—Mono

GP.91 Stereo Compatible £1 25. Acos GP67/2 will replace Collaro and Garrard Mono cartridges, 95np. T.T.C. Crystal High Gain, 75np. B.S.R. TC8H Jap. equivalent £1 25. P. & P. 7np.

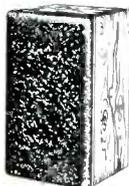
FARRADAY

5 1/2" x 11" x 4 1/2" covered in White, Green or Black rexine or Teak cloth with Silver coloured metal front 3ohm ex. tv speaker. £2 90 P & P 25p



ELF

An extension speaker of quality; 9 x 5 1/2 x 3 1/2 in. veneered in natural teak with smart gold and mottled Vynair front 3 ohm ex-TV speaker. The baffle is half inch thick. A real bargain at £1 92 1/2. Post and packing. 37 1/2p.



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3, 7, 15 ohms, 8 watt, 70np. P. & P. 17np.

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Padded ear cushions seal out room noise. Perfect coupling between reproducer and ears assure full response impedance 8 ohms. frequency range 30-15,000 Hz 6ft. cord and standard stereo plug. Only £2 57 1/2. P. & P. 27 1/2p.



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Simple unit connects direct to amplifier and speakers to give attenuated headphone output has 3 position switch to give headphones only, speakers only, speakers and headphones. Only £1 50. P. & P. 13p.



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P. & P. 57p
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SOUND BARGAINS



GIANT POWER COMMUNICATIONS RECEIVER

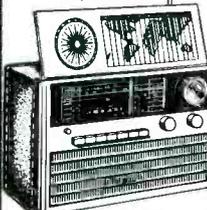
WITH 3 in 1 AC/DC POWER SUPPLY SYSTEM MAINS/BATTERY plus BUILT-IN BATTERY BOOSTER

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8 WAVE BANDS AND WORLD MAP & TIME ZONE DIAL

Tune into the world with this amazing communications receiver. A truly exceptional unit in performance and looks—leatherette with stainless steel trim. Looks good anywhere. Use either as a portable with standard batteries or plug it directly into 220-240 volt domestic mains supply. 14 Transistors; 9 diodes; 1 thermister. Internal ferrite rod antenna plus telescopic aerial. Separate tone, volume and tuning controls with push-button selectors for the 8 WAVE BANDS. Complete with Hi-Fi earphone for personal listening. Frequency ranges: Long wave 150-350Kcs. Medium 350-1500Kcs. Marine 1.6-4.5Mcs. Short Wave 19-24Mcs. FM/VHF 88-108Mcs. Aircraft 108-135Mcs. PUBLIC SERVICE BANDS 135-174Mcs. Fully guaranteed.

N.B. The Ministry of Post & Telecommunications has pointed out that a licence (not generally available to the public) is required for reception of transmissions by Fire Brigade, Aircraft, Shipping, etc.

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 £7.75 complete.
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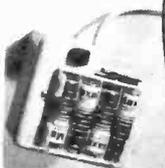
A complete set of parts to enable the do-it-yourself man to build the Electronic Ignition as described in Practical Wireless June-July 1972. Fully approved by the Author Mr. D. G. Fripp. Reprints of the two part feature are available at 10 pence each or 20 pence for the two. Everything supplied except nuts-n-bolts, solder and connecting wire. State + or - earth and send cheque or PO for £7.75 including p & p to Jermyn Industries, Vestry Estate, Sevenoaks, Kent.



£7.75 complete

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Mallory Cells in U2, U11 and Penlite U7 sizes, Kestrel Battery Charging Unit



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All items post paid in **GREAT BRITAIN**

P-C BOARDS (not computer panels).

1 off 6 transistors single wave band
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 1 off 3 transistor **£1.50** the three

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Transistor F.M. Stereo Multiplex Decoder. Size: 5½ x 2½ x 1½. As used in well known British stereo units with circuit **£3.75**

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All units guaranteed new and perfect. Prompt despatch p. & p. 25p per speaker.

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Garrard Record Players



SP25 Mk. III Deck Only

4 speed Automatic Single Player
Lasky's price **£11-50**

Garrard SL95B Deck	£35 00
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complete with stereo cartridge	£11 50
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WB4 Mk. II Plinth	£5 45
SPCA Mk. II cover	£4 25
Price together	£8 70
WB1 Plinth	£3 70
SPC1 cover	£3 60
Price together	£6 50

SP 25 Package

SP25 Mk. III Single player	List	£15 85
AD76K stereo magnetic cartridge	List	£4 35
Lasky's teack plinth & cover	List	£4 75

Total List Price £24 95

Package Price £20-50

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Package Price £35-00

CARRIAGE—all units

DECK ONLY 50p. PLINTH & COVER ONLY 25p. DECK WITH PLINTH AND COVER 75p.

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Two waveband all transistor car radio that covers full Medium and Long wavebands with slide switch wave change. Large easy to grip controls. Illuminated dial with "easy to read" scale. Externally adjustable aerial trimmer. Powerful output through either one or two speakers. Operates on 12 volt D.C. Negative or positive earth. Standard size 6 1/2 in (W) x 4 1/2 in (D) x 2 in (H). Black with chrome trim. Complete with speaker, baffle, leads, mounting brackets.

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NOW WITH ILLUMINATED DIAL EXCLUSIVELY FROM LASKY'S



The clock measures 5 1/2 W x 2 1/2 H x 3 1/2 D (overall from front of drum to back of switch). SPEC.: 210/240V a.c. 50Hz operation; switch rating 250V, 3A. Complete with instructions. ● COMPLETE WITH KNOBS. FEATURES: ● MAINS OPERATION ● 12-HOUR ALARM ● AUTO "SLEEP" SWITCH ● HOURS, MINUTES AND SECONDS READ-OFF ● FORWARD AND BACKWARD TIME ADJUSTMENT ● SILENT OPERATION ● SHOCK AND VIBRATION PROOF ● BUILT IN ALARM BUZZER

SPECIAL QUOTES FOR QUANTITIES LASKY'S PRICE **£6-75** C & P 25p

SINCLAIR PHASE LOCK LOOP STEREO FM TUNER

Incorporates varicap diodes, printed circuit, coils, squeeze circuit I.C. Decoder, etc., supplied completely built and tested and ready to be mounted into any cabinet you choose. It may be used with any High Fidelity Amplifier. Power requirements 25/30V DC. Size 8 1/2" x 1 1/2" x 3 1/2". LIST PRICE **LASKY'S £16-95** C & P 25p
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EAGLE AM/FM POCKET TRANSISTOR RADIO

This super compact two-band radio **ORIGINALLY COST £9 81!** The ideal pocket set for all ages. Receives all Med. wave and FM stations (local news, etc.) —separate tuning scales. Grey/chrome trim cabinet with carry strap. Excellent tone. Uses single PF3 type battery. Telescopic FM aerial. Size: 4 1/2 x 2 1/2 x 1 1/2 in. comp. with battery and ear-piece.



LIST PRICE **LASKY'S £4-75** C & P 15p
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LASKY'S NEW LOW NOISE CASSETTES FROM THE USA

Type	Single	5	10	15
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C120	48p	£2 35	£4 63	£6 84

Each cassette individually boxed in Philips, type plastic library.
C & P: each 7p, 5—25p, 10—40p, 20—68p.

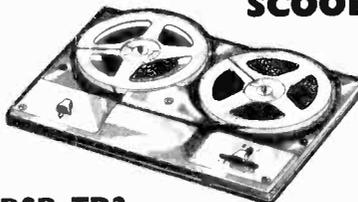
Leak Speaker "Scoop"

Leak 150 Speakers
List price £49.00 per pair
Lasky's Price **£38-95** C & P £2 00

Leak 250 Speakers
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Leak 600 Speakers
List price £99.00 per pair
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BSR TAPE DECK SCOOP

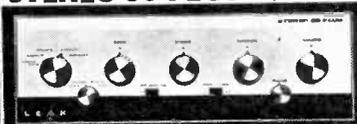


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FANTASTIC VALUE, ONLY Lasky's can offer you a tape deck at such an amazing price. The BSR TD2 tape deck operates by a simple reliable mechanism using the minimum of controls. Available with 1/4 track or 1/2 track mono or stereo heads. Incorporates fast wind and fast rewind, records at 3 1/2 ips. giving up to 3 hrs playing time, takes up to 5 1/2 in. spools. Size 13 in. x 8 1/2 in. front to rear, 2 1/2 in. below plate, 1 1/2 in. above plate.

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LEAK BARGAINS STEREO 30 PLUS amplifier (cased)



List Price £62-50 **PRICE £45-00** C & P £1 00

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List Price £75-00 **LASKY'S PRICE £55-00** C & P £1 00

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Teak case for Stereofetic tuner only.
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Teak double case for 30 or 70 and stereofetic tuner.
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LEAK TRUSPEED



2 speed belt drive turntable comp. with plinth, cover and SHURE cartridge.
LIST PRICE £69 50
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RADIO BARGAINS

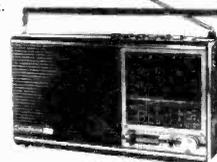
Nordmende Galaxy 4000

AM/FM/LW/SW Battery/Mains Portable Radio
Both these sets offer fantastic quality and almost unbelievable value! Each superbly finished in teak black and chrome. Covers medium, long and FM waves plus 3 band spread short wave ranges. Fitted with slider volume and tone controls. Size: 13 1/2 x 7 1/4 x 3 in. Power: Batteries/Mains 220/240, 50/60Hz.

ORIGINAL LIST PRICE £49 50

LASKY'S PRICE £39-50

C & P 25p



Nordmende Galaxy 6000



AM/FM/LW/SW Battery/Mains Portable Radio
Covers medium and long waves, FM (local) and world-wide short waves cover in 6 band ranges. Size: 16 1/2 x 8 x 3 in. Filter switch, ext. speaker socket, tape record and record player socket. Batteries or 220/240v. Mains, 50/60Hz.

LASKY'S PRICE £49-50 C & P 5p

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A QUARTER TURN RIGHT!

...opens a world of real stereo sound



VISCOUNT III AUDIO—£52 complete

PRICES SYSTEM 1	Viscount III R101 amplifier	£22.00 + 90p p&p	PRICES SYSTEM 2	Viscount R101 amplifier	£22.00 + 90p p&p
	2 × Duo Type II speakers	£14.00 + £2 p&p		2 × Duo Type III speakers	£32.00 + £3 p&p
	Garrard SP25 Mk. III with MAG. cartridge plinth and cover	£23.00 + £1.50 p&p		Garrard SP25 Mk. III with MAG. cartridge, plinth and cover	£23.00 + £1.50 p&p
	Total	£59.00		Total	£77.00
Available complete for only £52 + £3.50 p&p			Available complete for £69 + £4 p&p		

14 + 14 watts r.m.s. 40 Hz to 40kHz ± 3dB. Total distortion at 10 watts at 1kHz — 0.1%

This is real value for money! We have designed 2 systems and the heart of them is the Viscount III amplifier. A unit of great eye appeal with teak finished cabinet. FET's (Field effect transistors) are incorporated on the input stages, just like top priced units. FET's give you more of the signal you want and almost none of the hiss you don't. Both units have output sockets for headphones and tape recorder. Filters and tone controls give a wide range of bass and treble adjustment.

For both systems we have chosen the famous Garrard SP25 Mk. III deck which comes complete with simulated teak plinth and dust cover.

The exclusive Duo loudspeaker systems are incomparable for quality within their price range. Large speakers in extremely substantial cabinets. There's a choice of the Duo II's for the smaller room or the big Duo III's for real bass response.

SPECIFICATION

14 watts per channel into 3 to 4 ohms (suitable 3-15 ohms). Total distortion @ 10W @ 1kHz 0.1%. P.U.1 (for ceramic cartridges) 150mV into 3 Meg. P.U.2 (for magnetic cartridges) 4mV @ 1kHz into 47K equalised within ±1dB R.I.A.A. Radio 150mV into 220K. (Sensitivities given at full power). Tape out facilities: headphone socket, power out 250mW per channel. Tone controls and filter characteristics: Bass +12dB to -17dB @ 60Hz. Bass filter: 6dB per octave cut. Treble control: treble +12dB to -12dB @ 15kHz. Treble filter: 12dB per octave. Signal to noise ratio: (all controls at max.)—P.U.1 and radio —65dB. P.U.2 —58dB. Cross talk better than -35dB on all inputs. Overload characteristics better than 26dB on all inputs. Size approx. 13½in × 9in × 3½in.

SPEAKERS

Duo Type II

Size approx. 17in × 10½in × 6½in. Drive unit 13in × 8in with parasitic tweeter. Max. power 10 watts, 8 ohms. Simulated Teak cabinet. £14 pair + £2 p&p.

Duo Type III

Size approx. 23½in × 11½in × 9½in. Drive unit 13½in × 8½in with H.F. speaker. Max. power 20 watts at 3 ohms. Freq. range 20Hz to 20kHz. Teak veneer cabinet. £32 pair + £2 p&p.



Goods not despatched outside U.K.

S.A.E. for fully illustrated leaflet

Radio and TV Components (Acton) Ltd. 21c High Street, Acton, London W3 6NG. 323 Edgware Road, London W2.
Mail orders to Acton. Terms C.W.O. All enquiries S.A.E.



£25

takes the wraps off UNISOUND a new concept in stereo



See opposite page for address

The whole system is complete including superb cabinets in simulated teak—just simply screw together the components and you save pounds! Amplifier is based on the famous Mullard Unilex system. Garrard 2025TC turntable complete with stereo ceramic cartridge, teak simulated plinth and tinted acrylic cover. Plus the big 13" x 8" EMI Twin-cone speakers ready for mounting in their elegant cabinets, which simply need screwing and gluing together. All glue and screws supplied. Easy to follow step-by-step instructions guide you quickly and effortlessly to taking the wraps off truly realistic stereo sound.

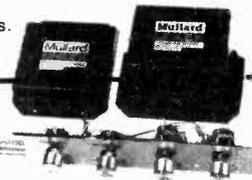


£25 complete plus £2.80 p. & p.
Diamond Stylus £1.25 extra.

Power output: 4 watts per channel into 8 ohms.
Inputs: 120 mV (for ceramic cartridges).
Stereo headphones with adaptor £4.00

UNISOUND MODULES ONLY £6.95

If you prefer, you can buy the three modules—pre-amplifier, power supply/dual power amplifier, and control panel—by themselves for only £6.95. P. & P. 50p extra.



No soldering, just simply screw together with screwdriver supplied. Their overall specification is the same as shown for the complete Unisound console, using the high efficient I.C. monolithic power chips to ensure very low distortion at all power levels, correct operation in all ambient temperatures, full power over the audio spectrum.

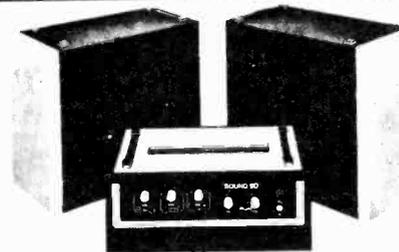


RELIANT MK IV

★ 3 Individual Mixing Controls. ★ 5 Electronically Mixed Inputs, common to all 5 inputs. ★ Mixer employing F.E.T. (Field Effect Transistor). ★ Solid State Circuitry. ★ Attractive Styling.

£10.50

plus p. & p. 60p
INPUTS:—1. Crystal Mic or Guitar 9mV. 2. Moving coil Mic or Guitar 8mV. Inputs 3, 4 & 5 are suitable for a wide range of medium output equipment (Gram., Tuner, Monitor, Organ, etc.). All 250mV sensitivity.
CONTROLS:—3 Volume controls. Bass control range: 13dB @ 60Hz. Treble control range ±12dB @ 15KHz. Separate ON/OFF Switch. Neon Indicator. POWER OUTPUT:—12 Watts R.M.S. into 3 to 4 ohms speaker.
SIGNAL/NOISE:—Better than -60dB on Inputs 3, 4 and 5 & -50dB on 1 & 2.
SUPPLY:—220-250 AC Mains. SIZE:—12½" x 6" x 3½"



SOUND 50 50 WATT AMPLIFIER AND SPEAKER SYSTEM

Output Power: 45 watts R.M.S. (Sine wave drive). Frequency Response: -3dB points 30Hz at 18KHz. Total Distortion: less than 2% at rated output. Signal to noise ratio: better than 60dB.

Speaker Impedance: 3, 8 or 15 ohms. Bass Control Range: ±13dB at 60Hz. Treble Control Range: ±12dB at 10KHz. Inputs: 4 inputs at 5mV into 470K. Each pair of inputs controlled by separate volume control. 2 inputs at 200mV into 470K.

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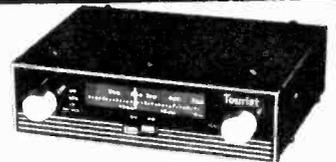
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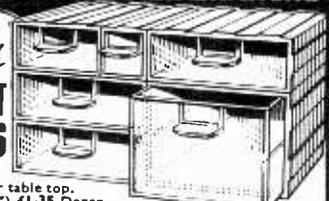
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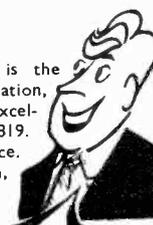
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BF274	0-20	OC23	0-10
BFY50	0-15	OC25	0-25
BSY25	0-13	OC26	0-25
BSY26	0-13	OC28	0-30
BSY27	0-13	OC35	0-25
BSY28	0-13	OC36	0-37
BSY29	0-13	AD149	0-30
BSY95A	0-10	AUY10	1-25
OC41	0-15	25034	0-25
OC44	0-10	2N3055	0-50
OC45	0-10	Diodes	
OC71	0-10	AA442	0-10
OC72	0-10	OA95	0-07
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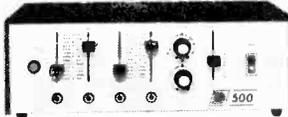
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- ★ Fault Condition warning lamp.
- ★ Built in base boost below 30 Hz.
- ★ 4 channel mixer with slider controls.



All three amplifiers have a built in emitter follower output socket for connecting a slave amplifier to enable the power output to be increased up to 1000 watts or more if required. A matching range of slave power amplifiers and a separate matching 100v line transformer is available

SPECIFICATION

Frequency Response 50-20,000 Hz \pm 3db (10dB Bass Boost at 10 Hz)
 Signal/Noise Ratio better than -50db.
 Harmonic Distortion less than 1%
 Speaker Impedance 8-16 ohms.
 Inputs: Mic 1 & 2 5mV at 50K ohms (50 or 600 ohm to order)
 Aux 3 & 4 100mV at 1 meg ohm.
 Size (all models) 15 1/2" x 5" x 6".
 Power Output: Model D.J.500 — 50 watts R.M.S. £56-95
 (at 8 ohms) Model D.J.700 — 70 watts R.M.S. £67-50
 Model D.J.1000 — 100 watts R.M.S. £79-00

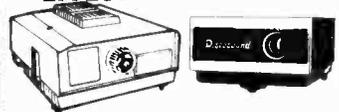
DISCO MINI

Hardly larger than a suitcase yet contains all the necessary features or a high quality mobile unit. The pre-amp has separate tone controls for both mic. and decks, and each input has its own individual volume controls and inputs, plus the addition of a cross fade for deck to deck sound transfer. A built in P.F.L. system for cueing, together with mic-over-ride facility are standard on all units. Response 20-20,000 Hz. Mic. input 5mV, 50K. Output 1 volt.

McDonald M.P.60 Turntables are used with high quality ceramic cartridges, and each deck has its own individual cut out switch fitted. This unit is suitable for Discos or Clubs having a power amplifier, or for use with the "Discmaster" 100 watt power amplifier as above. Size 32" x 20" x 8". £98-50.



EFFECTS PROJECTORS



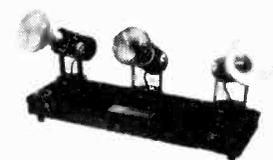
DISCO COLT. 150 watt.
LIGUMATIC MINI. 50 watt Q1 with 6" wheel.
DISCOWHEEL. 50 watt Q1 with quick change Cassette
GNOME 150. 150 watt Q1 with Cassette.
LIGUMATIC. 150 watt Q1 with 6" wheel.
PLUTO TUTOR-2. 250 watt Q1 with Cassette and 6" wheel.
TUTOR-2. with Liquisplode Tank.
KALEIDOSCOPE LENS (for Tutor-2) 6" Liquid Wheel and Crystal Wheel Liquid Cassette and Moire (24 different types to choose from).
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High efficiency 12" speakers. Ferrite magnets. Heavy duty voice coils and cones for Disco and Group use.
 12" 50 watt rms. 8 ohm Full range.
 12" 25 watt rms. 15 ohm Mid-Treble.
 15" 50 watt rms. 15 ohm. Full range.
 15" 100 watt rms. 15 ohm. Bass.

DISCO SPOT BANK



Designed to take three E/8 Type spot or colour bulbs up to 150 watts each. The unit is of all metal construction and has one 3-pin mains input socket plus one 3-pin mains output socket for connecting more than one bank together if required. The unit can be left free-standing or wall mounted if needed. Black crackle finish gives the unit a very professional appearance.

Size 18" x 6" x 7" (excluding bulbs)

Also in stock: Ultra Violet Spot Lamps and Fluorescent Lamps, Standard and Colour Spot Lamps and Fittings. Rotating Colour Displays. Flexlights, Fibre Optics, Dimmers, Flashers Effects Foils, etc. Your enquiries invited.

MIXER UNITS

DJ.101. Battery powered, 6-channel, variable levels, 3 x 50k mic., 1 x 100mV. aux., 2 x 100mV p.u. Output 250mV.

DJ.102. Mains operated, 4-channel, variable levels. 2 x 50k mic., 2 x 100mV p.u. PFL control, master volume, mic. over-ride, output variable 0-500mV.

DISCO 40. Pre amp part of Disco amp (see above). All facilities. Output will drive up to ten 100 watt amplifiers.

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The Pullman PB is suitable for 12 volt working on both negative and positive earth vehicles. It covers the full medium and long wave bands. Four push-buttons for medium wave, one for long wave. It is permeability tuned and sturdily constructed. Output is a full 2.5 watts into an 8 ohm speaker. But the Pullman PB will operate into any loudspeaker from 8 to 15 ohms. Power consumption approx. 1 amp.

* Circuit diagram and comprehensive instructions 50p, free with parts.
* Car aerial £1.25 post paid.

If you can solder on printed circuit board, you can build this push-button car radio kit.

It's simple - just follow the step-by-step instructions

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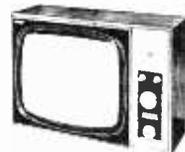
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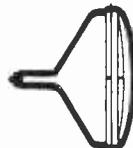
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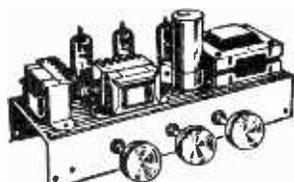
SUPERSOUND 13 HI-FI MONO AMPLIFIER



A superb solid state hi-fi amplifier. Brand new components throughout. 6 silicon transistors plus 2 power output transistors in push-pull. Full wave rectification. Output approx. 13 watts

r.m.s. into 8 ohm. Frequency response 12Hz-30KHz \pm 3db. Fully integrated pre-amplifier stage with separate Volume, Bass boost and Treble cut controls. Suitable for 8-15 ohm speakers. Input for ceramic or crystal cartridge. Sensitivity approx. 40mV for full output. Supplied ready built and tested, with knobs, escutcheon panel, input and output plugs. Overall size 3" high x 6" wide x 7 1/2" deep. AC 200/250V. PRICE £10.60. P. & P. 25p.

De Luxe Stereo Amplifier



A.C. mains 200-240 v. U a i n g heavy duty fully isolated mains transformer with full wave rectification giving adequate smoothing with negligible hum.

Valve line up:- 2 x ECL86 Triode Pentodes, 1 x EZ90 as rectifier. Two dual potentiometers are provided for bass and treble control, giving bass and treble boost and out. A dual volume control is used. Balance of the left and right hand channels can be adjusted by means of a separate 'Balance' control fitted at the rear of the chassis. Input sensitivity is approximately 300mV for full power output of 4 watts per channel (8 watts mono), into 3 ohm speakers. Full negative feedback in a carefully calculated circuit, allows high volume levels to be used with negligible distortion. Supplied complete with knobs, chassis size 11" w x 4" d. Overall height including valves 5". Ready built & tested to a high standard. PRICE £2.92 P. & P. 45p.

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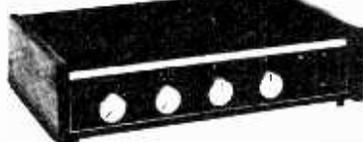
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Fully detailed 7 page construction manual and parts list free with kit or send 18p plus large S.A.E.

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A super quality gram amplifier using a double wound fully isolated mains transformer, rectifier and ECC82 triode stage. Impedance 3 ohms. Output approx. 3.5 watts. Volume and tone controls. Chassis size only 7in. wide x 3in. deep x 6in. high overall. AC mains 200/240v. Supplied absolutely Brand New completely wired and tested with good quality output transformer.

BARGAIN PRICE £2.75 35p

10/14 WATT HI-FI AMPLIFIER KIT

A stylishly finished monaural amplifier with an output of 14 watts from 2 EL84s in push-pull. Super reproduction of both music and speech, with negligible hum. Separate inputs for mike and gram allow records and announcements to follow each other. Fully shrouded section wound output transformer to match 3-15Ω speaker and 2 independent volume controls, and separate bass and treble controls are provided giving good lift and cut. Valve line-up 2 EL84s, ECC83, EF86 and E280 rectifier. Simple instruction booklet 13p (Free with parts). All parts sold separately. Only £7.97 P. & P. 55p.

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Four fully wired units ready to 'plug in'.

- ★ SUPER 30 AMPLIFIER (15 + 15 watt) in veneered housing
- ★ GARRARD SP25 MK III Turntable on Plinth with cover
- ★ GOLDRING G850 Magnetic cartridge with diamond stylus
- ★ PAIR OF STANWAY II Speaker Units

Special Total Price **£86-95**
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- ★ Super 30 Amplifier (15 + 15 watt) in veneered housing
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- ★ Pair of Stanway II speaker units.

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PACKAGE AS ABOVE but with Garrard 3000 Autochanger and Sonotone 9TA Ceramic Cartridge in lieu of SP25 and CS90 Carr. £1-25
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★ Moderate size only 25 x 14 x 10in. approx. COMPLETE KIT **£23**
★ Response 30-20,000 c.p.s. Impedance 15 ohms Carr. 65p

★ Performance comparable with units costing considerably more. Consists of (1) 12in. 15 watt Base unit with cast chassis, roll rubber cone surround for ultra low resonance, and ceramic magnet. (2) 3-way quarter section series cross-over system (3) 8 x 5in. high flux middle range speaker. (4) High efficiency tweeter. (5) Appropriate quantity acoustic damping material. (6) Handsome Teak veneered cabinet. (7) Circuit and full instructions. Terms: Dep. £4-60 and 9 monthly payments £2-47 (Total £28-83).

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Dual Cone speaker. Imp. 3 or 15 ohms.

STANWAY II Size 20 x 10 1/2 x 9 1/2in. appr. Rating 10 watts. Inc. 13 x 8in. speaker with highly flexible cone surround, long throw voice coil and 10,000 line magnet. High flux tweeter. Handsome Scandinavian design cabinet. Range 35-20,000 c.p.s. Imp. 8 ohms. Gives smooth realistic sound output. See 'package offers' for £17-85 illustration Carr. 50p

RSC G66 MkII 6.6 WATT high quality STEREO AMPLIFIER

Individual Ganged Controls: Bass, Treble, Volume and Balance. Printed circuit construction employing 10 Transistors plus Diodes. Output rating I.H.F.M. Frequency range 20-20,000 c.p.s. Bass Control ± 12db. Treble Control ± 13db. Selector switch for P.U. or Tape/Radio. For loudspeaker output impedances of 3 to 15 ohms. For standard 200-250v. A.C. mains operation. Attractive Black and Silver finished metal fascia plate and matching control knobs.

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R.S.C. TA12 MKIII 6.5 + 6.5 WATT STEREO AMPLIFIER

FULLY TRANSISTORISED, SOLID STATE CONSTRUCTION HIGH FIDELITY OUTPUT OF 6.5 WATTS PER CHANNEL
Designed for optimum performance with any crystal or ceramic Grain. P.U. cartridge. Radio tuner, Tape recorder etc. ★ 3 separate switched input sockets on each channel ★ Separate Bass and Treble controls ★ Slide Switch for mono use ★ Speaker Output 3-15 ohms ★ For 200-250v. A.C. mains ★ Frequency Response 20-20,000 c.p.s. -2dB ★ Harmonic Distortion 0-3% at 1,000 c.p.s. Hum and Noise -70dB ★ Sensitivities (1) 50mV (2) 400mV (3) 100mV. Output rating I.H.F.M. ★ Handsome finish. Facia plate and Knobs.

COMPLETE KIT OF PARTS WITH FULL WIRING DIAGRAMS & INSTRUCTIONS. **£15-50** Carr. 40p. 12 mths. guarantee £19-50
Deposit £3 and 9 mthly pymts £2-15 (Total £22-35). Or in Teak veneer housing £23
Dep. £3 & 9 mthly payments £2-55 (Total £25-95). Send S.A.E. for leaflet.



AUDIOTRINE HI-FI SPEAKER SYSTEMS

Consisting of matched 12in. 11,000 line 15 Watt 15 ohm high quality speaker, cross-over unit and tweeter. Smooth response and extended frequency range ensure surprisingly realistic reproduction.

OR SENIOR 15 WATT INCLUDING HF126 15,000 LINE SPEAKER **£6-95** Carr. 35p



HI-FI SPEAKER ENCLOSURES MODERN DESIGN

Teak veneer finish. Acoustically lined. Sizes approx. Carr. 35p. per enc.

JEB Size 16 x 11 x 9in. SE8 For optimum performance with any 8in. Hi-Fi speaker. Size 22 x 15 x 9in. **£6-47**

8in. Hi-Fi speaker. SE12 For excellent performance with 12in. Hi-Fi speaker and tweeter Size 25 x 16 x 10 1/2in. **£7-87**



AUDIOTRINE HIGH FIDELITY SPEAKERS

Heavy construction. Latest high efficiency ceramic magnets. Plasticized Cone surround. "D" indicates Tweeter Cone providing extended frequency range up to 15,000 c.p.s. Impedance 3 or 8-15 ohms. PLEASE STATE IMPEDANCE WHEN ORDERING.

Exceptional performance at low cost.

HF808T	8"	15W	£2-83	HF120D	12"	15W	£4-99
HF102D	10"	10W	£3-40	HF128	12"	15W	£5-75
HF120	12"	15W	£4-50	HF126D	12"	16W	£6-25



FANE 807T HIGH FIDELITY SPEAKER

A full range 8in. 10 watt unit for excellent sound quality, in suitable enclosure. Cast chassis Roll P.V.C. cone surround and long throw voice coil to achieve very low fundamental resonance of 30 c.p.s. Tweeter cone is fitted to extend high note response. Frequency range 25 Hz to 15 KHz. Gauss 10,000. Impedance 3 or 8-15 Ω. PLEASE STATE IMPEDANCE WHEN ORDERING **£3-85**



R.S.C. BATTERY/MAINS CONVERSION UNITS

TYPE BM1. An all-rly battery eliminator. Size 4 1/2 x 4 1/2 x 2in. approx. Completely replaces batteries supplying 1.5v and 90v. to battery radio where A.C. mains 200/250v. 50c/s is available. COMPLETE KIT **£3-25** ASSEMBLED READY FOR USE **£3-75**

R.S.C. TA6 6 Watt HI-FI AMPLIFIER

200-250v. AC mains operated. Frequency Response 30-20,000 c.p.s. -2dB. Harmonic Distortion 0.3% at 1,000 c.p.s. Separate Bass and Treble 'lift and cut' controls. 3 input sockets for Mike, Gram, Radio or Tape. Input selector switch. Output for 3-15 ohm spkrs. Max. sensitivity 5mV Output rating I.H.F.M. Fully enclosed enamelled case. 9 1/2 x 2 1/2 x 6 1/2in. Attractive brushed silver finish facia plate 10 1/2 x 3 1/2in. and matching knobs. Complete kit of parts with full wiring diagrams and instructions. **£7-75** Carr. 40p

OR FACTORY BUILT WITH 12 MONTHS' GUARANTEE **£10-95**



R.S.C. MkIII SUPER 30 HIGH FIDELITY STEREO AMPLIFIER

A COMPLETELY NEW DESIGN FURTHER IMPROVED IN BOTH APPEARANCE and PERFORMANCE. REPRESENTING VALUE FAR HIGHER THAN THE PRICES SUGGEST.

Only high grade components by leading manufacturers. COMPLETE KIT OF PARTS OR FACTORY BUILT WITH 12 months guarantee. Dep. £5-75 and 9 monthly payments £3-50 (Total £37-25.) OR FACTORY BUILT IN cabinet as illustrated. Dep. £7 and 9 monthly payments £3-99 (Total £42-91)

TECHNICAL DETAILS (Applying to each channel where appropriate)
CONTROLS: PUSH-BUTTON SELECTOR (1) Disc (2) Radio (3) Tape (4) Mono L (5) Mono R (6) SPEAKER DIS. (7) Mains on/off. Bass, Treble and Balance. Plus Ceramic Mag P.U. Switch.



PRINTED CIRCUITRY TWENTY SILICON TRANSISTORS. FOUR DIODES. FOUR RECTIFIERS

- ★ SATIN SILVER METAL FACIA with black lettering. Black edged knobs with bright silver centres.
- ★ PUSH-BUTTON SELECTOR SWITCHING
- ★ NEON INDICATOR
- ★ JACK SOCKET FOR HEADPHONES
- ★ CABINETED MODEL VENEERED IN SATIN TEAK. SUITABLE FOR ANY MODERN PICK-UP CARTRIDGE. CERAMIC or MAGNETIC REGARDLESS OF PRICE. WE RECOMMEND USE WITH THE BEST ANCILLARY EQUIPMENT THAT CAN BE AFFORDED.

OUTPUT: 15 watts R.M.S. (Continuous) into 8 ohms. 10 watts R.M.S. (Continuous) into 15 ohms. HARMONIC DISTORTION 0.1% at 1000 Hz 10 Watts

HUM & NOISE -75dB Min. Vol. -65dB Full Vol. FREQUENCY RESPONSE: -3dB 7Hz to 70KHz TREBLE CONTROL: +15dB to -12dB at 14KHz BASS CONTROL: +17dB to -16dB at 40Hz CROSS TALK -58dB

SENSITIVITIES: Disc Mag. 2-5mV. Ceramic 35mV. Radio 120mV. Tape 120mV. REAR PANEL SOCKETS ARE FOR 3 PAIRS OF INPUTS (1) P.U. (2) Radio. (3) Tape Amp. Plus pair for tape recorder signal take off and 2 pairs for speaker connections.

RSC GROUP/DISCO UNITS PACKAGE OFFER
Units listed below

FAL
F.G.1/2A DISCO CONSOLE
Incorporating twin Garrard SP95 Mk.III turntables and Ceramic Cartridges with diamond stylus. Separate Vol. controls for each turntable. Also MONITORING FACILITIES, plus Treble and Bass Controls. Separate input for 'mike' with vol. control switch. Black Rexine covered Cabinet with lid. see illus. on left.
Carr. £1.25
Or Dep. £18.25 and 9 mthly pymts £6.75 (Total £27.40) or Dep. £15 and 18 mthly payments £2.50 (Total £29.00).

100w POWER AMPLIFIER
PAIR OF HEADPHONES
High quality. Matching Dynamic Moving Coil Microphone fitted to Headphones.
PAIR 50w SPEAKERS
Black Rexine covered. Size approx. £72-85
18" x 18" x 8 ins.

Terms on Amps. Speakers and Headphone/Mike. Deposit £15 and 18 monthly payments of £3.95 (Total £86.10).

50 WATT SPEAKER
100 WATT AMPLIFIER
HEADPHONES MICROPHONE
SEND S.A.E. FOR LEAFLET

TWIN TURNTABLE WITH PREAMP FG1/2A

R.S.C. COLUMN SPEAKERS IDEAL FOR VOCALISTS AND PUBLIC ADDRESS
All types 15 Ohms covered in Rexine and Vynair
TYPE C4100 IS ALSO SUITABLE FOR BASS GUITAR OR ELECTRONIC ORGAN

TYPE C48S 25-30 WATTS
Fitted four 8" high flux 8 watt speakers
Overall size approx. 48 x 10 x 5in.
Terms: Dep £3 and 9 monthly payments £2 (Total £21) Carr. 75p

TYPE C412S 50 WATTS
Fitted four 12" 11,000 gauss 15 watt speakers
Overall size approx. 56 x 14 x 9in
Terms: Dep. £4 and 9 monthly payments £3.10 (Total £24.33) Carr. 75p

TYPE C4100 100 WATTS Inc. four 12" 50 watt speakers for conservative rating. Extra heavy construction. Size approx. 28" x 16" x 10" Acoustically filled and pressurised. Term: Dep. £11 and 9 mthly. pmts. £6.75 (Total £21.75). Carr. £1

FAL ULTRA HIGH POWER LOUDSPEAKERS
All power ratings are R.M.S. continuous 2 YEARS' GUARANTEE
High flux ceramic magnets. ALL CARR. FREE.

'POP' 100	'POP' 60	'POP' 50
18" 100 Watt 14,000 gauss 8/15Ω	15" 60 Watt 14,000 gauss 8/15Ω	12" 50 Watt 13,000 gauss 15Ω
£22-95	£12-90	£10-90
Dep. £6 and 9 mthly payments £2-20 (Total £25-80)	Dep. £3-30 and 9 monthly payments £1-30 (Total £21-60)	Dep. £2 and 9 monthly payments £1-20 (Total £12-80)

FOR BASS GUITAR, ELECT. ORGAN, ETC.

R.S.C. AIO 30 WATT ULTRA LINEAR HI-FI AMPLIFIER Highly sensitive. Push-Pull high output. Hum level -70dB. Response 20-20,000 c/s. All high grade components. Valves 6F86, 6F86, ECC83, 6X4, 6X4, 6X4. Separate Bass and Treble Controls. Sensitivity 36 millivolts. For High Impedance microphones. For Clubs, Schools, Theatres, Dance Halls, Outdoor Functions, etc. For Electronic Organ, Guitar, String Bass, etc. Gram, Radio, etc. For Electronic Organ, Guitar, String Bass, etc. to be used or Tape. Two separate inputs with vol. controls permit such as "mike" and 15 ohm speakers. Complete kit of parts with wiring diagram and instructions. Twin-handled perforated cover

TERMS: Deposit £4 and 9 monthly payments of £2-10 (Total £22-90). Send S.A.E. for leaflet.

FAL SPEAKERS 'POP' 25/12 in. 25 WATT
Dual Cone 15 Ω (for uses free) or Dep. £1 and 9 mthly payments 75p (Total £7.75)

R.S.C. TRANSFORMERS, L.F. CHOKES & RECTIFIERS
FULLY GUARANTEED. Impregnated and Interleaved where necessary.

Primarys 200-250v. 50c/a. Screened MIDGET CLAMPED TYPE 21 x 21 x 2 1/2 in.

250v., 60mA, 6-3v. 2a.	99p
250-250v. 60mA 6-3v. 2a.	£1-05

FULLY SHROUDED UPRIGHT MOUNTING

250-0-250v. 60mA, 6-3v. 2a., 0-5-6-3v. 2a.	£1-40
250-0-250v. 100mA, 6-3v. 4a., 0-5-6-3v. 3a.	£2-20
300-0-300v. 100mA, 6-3v. 4a., 0-5-6-3v. 3a.	£2-20
300-0-300v. 150mA, 6-3v. 4a., c.t., 6-3v. 1a.	£2-25
For Mullard 510 Amplifier	
350-0-350v. 100mA, 6-3v. 4a., 0-5-6-3v. 3a.	£2-20
350-0-350v. 150mA, 6-3v. 4a., 0-5-6-3v. 3a.	£4-95
425-0-425v. 200mA, 6-3v. 4a., c.t., 5v. 3a.	£2-20
425-0-425v. 200mA, 6-3v. 4a., 6-3v. 3a., 5v. 3a.	£5-10
450-0-450v. 250mA, 6-3v. 4a., c.t., 5v. 3a.	£5-30

TOP SHROUDED DROP-THERO TYPE

250-0-250v. 70mA, 6-3v. 2a., 0-5-6-3v. 2a.	£1-55
250-0-250v. 100mA, 6-3v. 2a., 0-5-6-3v. 2a.	£1-55
250-0-250v. 100mA, 6-3v. 2a., 6-3v. 1a.	£1-60
350-0-350v. 80mA, 6-3v. 2a., 0-5-6-3v. 2a.	£1-65
250-0-250v. 100mA, 6-3v. 4a., 0-5-6-3v. 3a.	£2-20
300-0-300v. 100mA, 6-3v. 4a., 0-5-6-3v. 3a.	£2-20
300-0-300v. 130mA, 6-3v. 4a., c.t., 6-3v. 1a.	£2-60
Suitable for Mullard 510 Amplifier	
350-0-350v. 100mA, 6-3v. 4a., 0-5-6-3v. 3a.	£2-20
350-0-350v. 150mA, 6-3v. 4a., 0-5-6-3v. 3a.	£2-60

FLAMENT OR TRANSISTOR POWER PACK
Types 6-3v. 1.5a. 49p; 6-3v. 2a. 54p; 6-3v. 3a. 76p; 6-3v. 6a. £1 80; 12v. 1a. 50p; 12v. 3a. or 24v. 1.5a. £1 35; 0-5-10v. 1.5a. £1 10; 0-10-10-25v. 2A117. 76p; CHARGE TRANSFORMERS 0-5-15v. 1.5a. 99p; 2A. £1 10; 3a. £1 25; 6a. £1 45; 6a. £1 65; 8a. £2 00
AUTO (Step Up/step DOWN) TRANSFORMERS 0-110/120v. 200-230-250v. 50-80 watts £1-10. 150 watts, £1-80 250 watts £2-75: 500 watts £5-75
OUTPUT TRANSFORMERS Standard Fetode 5,000 Ω or 7,000 Ω to 3 Ω 50p
Push-Pull 8 watts EL84 to 3 Ω or 15 Ω 83p
Push-Pull 15-18 watts, sectionally wound £1-20
Push-Pull 10 watts 6V6, ECL86 to 3, 5, 8 or 15 Ω £1-87
Push-Pull EL84 to 3 or 15 Ω 10-12 watts. £1 85
Push-Pull 15-18 watts, sectionally wound £1 85
6L6, KT66, etc. for 3 or 15 Ω £1 99
Push-Pull 20 watt high quality sectionally wound EL34, 6L6, KT66 etc. for 3 or 15 Ω £3-80
SMOOTHING CHOKES 150mA, 7-10H. 250 Ω 70p; 100mA, 10H, 100 Ω 60p; 80mA, 10H, 350 Ω 50p; 60mA, 10H, 400 Ω 25p.
SELENIUM RECTIFIERS F. W. (Bridged) All 6/12v. D.C. output. Max. A.C. input 15v. 1a. 25p. 2a. 35p. 3a. 50p. 4a. 65p. 6a. 80p.

GROUP/DISCO EQUIPMENT PACKAGE OFFERS

F.A.L. PHASE 50 MK.III AMPLIFIER PR. FAL POP 25/12 L/SPEAKERS	£34-95 £13-50	PACKAGE PRICE £45
Terms: Deposit £6.50 and 9 monthly payments of £4.72 (Total £48.98)	£48-45	£1
F.A.L. PHASE 50 MK.III AMPLIFIER PR. FAL POP 50 L/SPEAKERS	£34-95 £21-80	PACKAGE PRICE £52
Terms: Deposit £10 and 9 monthly payments of £5-25 (Total £57.25)	£56-75	£1
F.A.L. PHASE 50 MK.III AMPLIFIER PAIR L12/25 25W L/S in cabinets	£34-95 £23-90	PACKAGE PRICE £56
Terms: Deposit £10 and 9 monthly payments of £5-75 (Total £61-75)	£59-85	£1-25
F.A.L. PHASE 100 AMPLIFIER 4 FAL POP 50 L/SPEAKERS	£81-85 £48-80	PACKAGE PRICE £99-95
Terms: Deposit £15-95 and 9 monthly payments of £10-50 (Total £110-45)	£105-85	£2

HIGH QUALITY LOUDSPEAKER UNITS
ALL TWO TONE REXINE AND VYNAIR FINISH
L125 50 WATT Fitted pair of 12" 50 watt high flux speakers for conservative rating. Impedance 8-15 ohms. Carr. £1-50
Or deposit £4-50 and 9 monthly pmts. of £3-62. Total £27-08

L12/25 12" 25 WATT 10,000 lines 15 ohms. Carr. 50p	L13/13" x 8" 10 Watt 10,000 lines 3 or 15 ohms. State impedance required. Carr. 40p
£11-95	£5-25

FAL PHASE 50 Mk.III AMPLIFIER 50W
Solid state. 4 Separately controlled inputs Plus master vol. control. Ind. Bass and Treble Controls. Protective circuit to guard against damage from accidental shorts. Output for Speakers 3 to 30 ohms. Size 17" x 7" x 7"
200-250v. A.C. mains. Output 50 watts music rating. Or deposit £7-25 & 9 monthly payments £3-50. Total £38-75. £34-95 Carr. 75p.

CREDIT TERMS AVAILABLE ON PURCHASES OVER £8 (Kits Excepted)
INTEREST CHARGES REFUNDED ON CREDIT SALES Settled in 3 months

R.S.C. Branches listed below open all day Sats.
BRADFORD 10 North Parade (Half-day Wed.). Tel. 25349
BLACKPOOL (Agent) O & C Electronics 227 Church Street
BIRMINGHAM 30/31 Great Western Arcade, Tel. 021-236 1279 (Half-day Wed.).
DERBY 26 Osmonston Rd., The Spot (Half-day Wed.). Tel. 41361
DARLINGTON 18 Priestgate (Half-day Wed.). Tel. 68043
EDINBURGH 101 Lothian Rd. (Half-day Wed.).
GLASGOW 326 Argyle St. (Half-day Tues.). Tel. 248 4159
HULL 81 Paragon Street (Half-day Thurs.). Tel. 20505.
LEICESTER 32 High Street (Half-day Thurs.). Tel. 56420
LEEDS 5-7 County (Mecca) Arcade, Briggate (Half-day Wed.). Tel. 28252
LIVERPOOL 73 Dale Street (Half-day Wed.). Tel. 236 3573
LONDON 238 Edgware Road, W.2. (Half-day Thurs.). Tel. 723 1629
MANCHESTER 60A Oldham Street, (Half-day Wed.). Tel. 235 2778
MIDDLESBROUGH 106 Newport Rd. (Half-day Wed.). Tel. 47096
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NOTTINGHAM 19/19A Market Street (Half-day Thurs.). Tel. 48068
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Opening late July
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TERMS C.W.O. or C.O.D. No C.O.D. under £1.
POSTAGE 25p EXTRA UNDER £2. 30p EXTRA
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S.A.E. PLEASE WITH ENQUIRIES.
SUPPLIER TO GOVERNMENT DEPARTMENTS,
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MAIL ORDERS MUST NOT BE SENT TO SHOPS

RSC BASS-REGENT 50 WATT AMPLIFIER
A powerful high quality all-purpose unit for lead, rhythm, bass guitar, vocalists, gram, radio, tape. Peak Output rating. Loudspeaker unit optional horizontal or vertical mounting.
★ Two extra heavy duty 12in. 50w L'spkrs.
★ Four Jack inputs and two Volume Controls for instant use up to four pick-ups or "mikes". Bass and Treble controls.
Credit Terms: Deposit £15 and 9 monthly pmts of £3-25 Carr. £65 for leaflet.
(Total £71-25)

RSC GP30 HI-FI AMPLIFIER
For Guitar, Vocal or Instrumental Group.
A 4 input, 2 vol. control Hi-Fi 30 watt unit with Separate Bass and Treble controls. Current vres. Peak output rating. Strong Rexine covered cabinet with handles. Attractive black/gold P.V.C. fascia. Neon indicator. For 200-250v. A.C. mains. For 3 or 15 ohm speakers. Send S.A.E. for leaflet.
Terms: Deposit £4-80 and 9 monthly payments of £2-80 (Total £25-00). £22-50 Carr. 50p

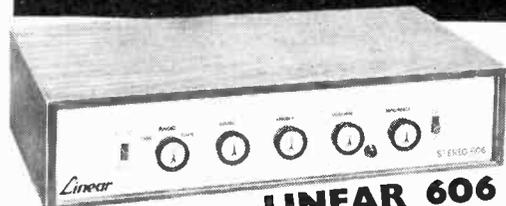
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LINEAR

Representing really exceptional value

TWO STEREO AMPLIFIERS

IN ELEGANT TEAK FINISH CASES!



LINEAR 606
6+6 WATTS
Recommended Retail Price
£22.50

0-200-230-250v. 50 Hz
A.C. mains operation.
Inputs for magnetic or
Ceramic Pickup, Tape
or Radio Tuner.

TECHNICAL DETAILS

Bass Control ± 12 dB at 40 Hz.
Treble Control ± 12 dB at 14 KHz.
Sensitivities Mag. P.U. 3.5 m.v.
into 47K ohm R.I.A.A. Ceramic
P.U. 35 m.v. into 100K ohm. Tape
Amp. 100 m.v. into 100K. Radio
Tuner 400 m.v. into 400K ohm.
Crosstalk 53 dB.
Hum and Noise -75 dB min.
vol. -65 dB max. vol.
Total Harmonic
Distortion 0.1% at 1 watt
into 15 ohms.
Output (per channel)
6.5 watts I.H.F.M.

- ★ Individual Bass and Treble Controls.
- ★ Frequency Response $\pm 1\frac{1}{2}$ dB
20 Hz to 65 KHz.
- ★ Outputs for Speaker impedances
between 3 and 15 ohms.
- ★ Stereo/Mono Switch.
- ★ Input Selector Switch.
- ★ Solid State Circuitry.
- ★ Attractive silver finished metal facia
and matching control knobs.

- ★ A modestly priced solid state unit.
- ★ The Silver Facia with black lettering enhanced by
matching control knobs, provides a high standard of
appearance.
- ★ Suitable for crystal Gram. Pick-up cartridges and
Radio input.
- ★ A wide range of tone variation is provided by the
separate Bass and Treble 'lift' and 'cut' controls.
- ★ A selector switch permits instantaneous selection of
Gram, or Radio.
- ★ Speaker impedances between 3 and 15 ohms are
suitable.

TECHNICAL DETAILS

Frequency Range 20 Hz to
20 KHz
Output (per channel) 5 watts
I.H.F.M.
Bass Control ± 12 dB at 60 Hz.
Treble Control ± 14 dB. at
14 KHz.

PRINTED CIRCUIT CONSTRUCTION
EMPLOYING 10 TRANSISTORS



LINEAR 505
5+5 WATTS
Recommended Retail Price
£17.50

0-200-250v. 50 Hz A.C.
mains operation

Wholesale and Retail enquiries to the Manufacturers

LINEAR PRODUCTS LTD., Electron Works, Armley, Leeds. LS12 3SA Tel.630126

ALL LINEAR AMPLIFIERS GUARANTEED FOR 12 MONTHS

ELECTRONIC VALVES

DY86	0.23	PC97	0.36	PY83	0.26
DY87	0.23	PCC84	0.28	PY500	0.95
EABC80	0.30	PCC89	0.43	PY800	0.32
EB91	0.09	PCC189	0.47	PY801	0.32
ECC81	0.15	PCF80	0.27	UABC80	0.30
ECC82	0.18	PCF86	0.44	UCC85	0.34
ECC83	0.24	PCF802	0.38	UCC81	0.30
ECL80	0.25	PCF806	0.56	UCL82	0.31
EF80	0.22	PCF808	0.68	UL41	0.54
EF85	0.26	PCL82	0.30	UY85	0.24
EF86	0.28	PCL83	0.53	6/30L2	0.58
EF89	0.23	PCL84	0.33	6AT6	0.18
EF91	0.12	PCL85	0.37	6AU6	0.20
EF183	0.26	PCL86	0.37	6BA6	0.20
EF184	0.28	PFL200	0.51	6BE6	0.21
EH90	0.35	PL36	0.47	6F23	0.67
EL41	0.53	PL81	0.43	12AT6	0.23
EL84	0.22	PL82	0.29	12AT7	0.15
EY51	0.30	PL83	0.31	12AU7	0.18
EY86	0.28	PL84	0.29	12AX7	0.22
EZ80	0.20	PL500	0.61	12BA6	0.30
EZ81	0.21	PL504	0.61	12BE6	0.30
PC86	0.45	PY81	0.23	35W4	0.23
PC88	0.45	PY82	0.24	50C5	0.32

POSTAGE: 1 VALVE 5p, EACH ADDITIONAL VALVE 1p.
ORDERS OVER £5 POST FREE. CASH WITH ORDER ONLY.

Quotations for any type not listed send SAE.

NO CALLERS. ALL VALVES GUARANTEED AND INDIVIDUALLY BOXED.

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Input 240 volts. Output 3V, 4.5V, 6V, 7.5V, 9V,
12V d.c. Current 500mA.
Price £4.47 postage paid

EEC Car Adaptor

Input 12 volts. Output 6V, 7.5V, 9V.
Price £5.10 postage paid

MD 800 Sound Headphones with volume control £3.90

Garrard 2025 with plinth cover and cartridge £12.30

Shira Car Radio MW/LW—

Manual £8.50

Twin Speaker £8.95

Push Button £10.45

Plinth and Cover suitable for Garrard SP25, £3.25

Headphones DHQ25, £2.25

Siran Battery Chargers 6V and 12V, £2.85

Please send 25p for postage and packing

Quality Cassettes at cheapest prices

C60 35p plus 5p P. & P.

C90 47p plus 5p P. & P.

CI20 60p plus 5p P. & P.

Pocket Transistors

Radio AM with Battery, Magnetic Earphone and
Carrying Case, £1.95 Postage Paid.

Mixed packet of resistors 25p postage paid

Build yourself a TRANSISTOR RADIO

NEW! ROAMER 10 WITH VHF INCLUDING AIRCRAFT

10 TRANSISTORS. 9 TUNABLE WAVEBANDS, MW1, MW2, LW, SW1, SW2, SW3, TRAWLER BAND. VHF AND LOCAL STATIONS AND AIRCRAFT BAND

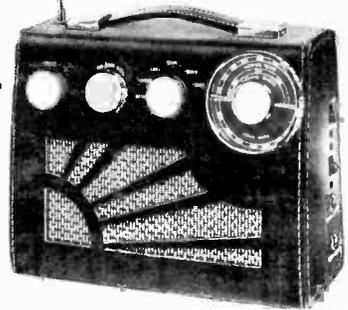
Built in Ferrite Rod Aerial for MW/LW. Retractable, chrome plated Telescopic Aerial for peak short wave and VHF listening. Push Pull output using 600mW Transistors. Car Aerial and Tape Record Sockets. Switched Earpiece Socket complete with Earpiece. 10 Transistors plus 3 Diodes. 8" x 2 1/2" Speaker. Air Spaced ganged Tuning Condenser with VHF section. Volume on/off, Wave Change and Tone Control. Attractive Case in black with silver blocking. Size 9" x 7" x 4". Easy to follow instructions and diagrams. Parts price list and easy build plans 30p (FREE with parts).

Total building cost

£8-50

P. P. & Ins. 50p

(Overseas P. & P. £1)



ROAMER EIGHT Mk I

NOW WITH VARIABLE TONE CONTROL



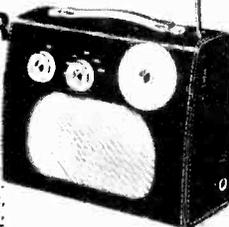
7 Tunable Wavebands: MW1, MW2, LW, SW1, SW2, SW3 and Trawler Band. Built in ferrite rod aerial for MW and LW. Retractable chrome plated Telescopic aerial for Short Waves. Push pull output using 600mW transistors. Car aerial and Tape record sockets. Selectivity switch. Switched earpiece socket complete with earpiece. 8 transistors plus 3 diodes. 8" x 2 1/2" Speaker. Air spaced ganged tuning condenser. Volume/on/off, tuning, wave change and tone controls. Attractive case in rich chestnut shade with gold blocking. Size 9" x 7" x 4in. approx. Easy to follow instructions and diagrams. Parts Price List and Easy Build Plans 25p (FREE with parts).

Total building cost **£6-98** P. P. & Ins. 41p. (Overseas P. & P. £1)

ROAMER SEVEN MK IV

7 Tunable Wavebands: MW1, MW2, LW, SW1, SW2, SW3 and Trawler Band. Extra Medium waveband provides easier tuning of Radio Luxembourg, etc. Built in ferrite rod aerial for MW and LW. Retractable 4 section 24in. chrome plated telescopic aerial for SW. Socket for Car Aerial. Powerful push-pull output. 7 transistors and 2 diodes. 8" x 2 1/2" speaker. Air spaced ganged tuning condenser. Volume/on/off, tuning and wave change controls. Attractive case with carrying handle. Size 9" x 7" x 4in. approx. Easy to follow instructions and diagrams. Parts price list and easy build plans 15p (FREE with parts). Earpiece with plug and switched socket for private listening, 30p extra.

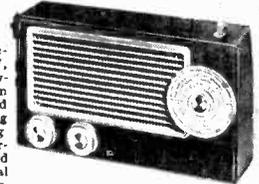
Total building costs **£5-98** P. P. & Ins. 41p. (Overseas P. & P. £1)



ROAMER SIX

6 Tunable Wavebands: MW, LW, SW1, SW2, Trawler band plus an extra M.W. band for easier tuning of Luxembourg, etc. Sensitive ferrite rod aerial and telescopic aerial for Short Waves. 3in. Speaker. 8 stages—5 transistors and 2 diodes. Attractive black case with red grille, dial and black knobs with polished metal inserts. Size 9" x 6 1/2" x 2 1/2in. approx. Easy build plans and parts price list 15p (FREE with parts). Earpiece with plug and switched socket for private listening 30p extra.

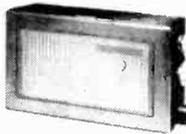
Total building costs **£3-98** P. P. & Ins. 26p. (Overseas P. & P. £1)



POCKET FIVE

3 Tunable Wavebands: MW, LW, Trawler Band with extended M.W. band for easier tuning of Luxembourg, etc. 7 stages—5 transistors and 2 diodes, super-sensitive ferrite rod aerial, fine tone moving coil speaker. Attractive black and gold case. Size 6 1/2" x 4 1/2" x 3 1/2in. Easy build plans and parts price list 10p (FREE with parts). Earpiece with plug and switched socket for private listening 30p extra.

Total building costs **£2-29** P. P. & Ins. 23p. (Overseas P. & P. 63p)

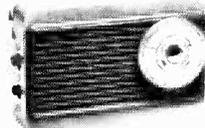


TRANSONA FIVE

5 TRANSISTORS AND 2 DIODES

3 Tunable Wavebands: MW, LW and Trawler Band. 7 stage—5 transistors and 2 diodes, ferrite rod aerial, tuning condenser, volume control, fine tone moving coil speaker. Attractive case with red speaker grille. Size 6 1/2" x 4 1/2" x 1 1/2in. Easy build plans and parts price list 10p (FREE with parts). Earpiece with plug and switched socket for private listening 30p extra.

Total building costs **£2-50** P. P. & Ins. 22p. (Overseas P. & P. 65p)

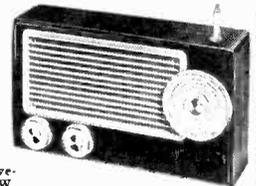


TRANS EIGHT

8 TRANSISTORS AND 3 DIODES

6 Tunable Wavebands: MW, LW, SW1, SW2, SW3 and Trawler Band. Sensitive ferrite rod aerial for M.W. and L.W. Telescopic aerial for Short Waves. 3in. Speaker. 8 improved type transistors plus 3 diodes. Attractive case in black with red grille, dial and black knobs with polished metal inserts. Size 9" x 6 1/2" x 2 1/2in. approx. Push pull output. Battery economiser switch for extended battery life. Ample power to drive a larger speaker. Parts price list and easy build plans 25p (FREE with parts). Earpiece with plug and switched socket for private listening 30p extra.

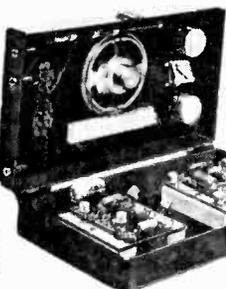
Total building costs **£4-48** P. P. & Ins. 31p. (Overseas P. & P. £1)



NEW! "EDU-KIT"

BUILD RADIOS, AMPLIFIERS, ETC. FROM EASY TO FOLLOW STAGE DIAGRAMS. FIVE UNITS INCLUDING MASTER UNIT TO CONSTRUCT. COMPONENTS INCLUDE:
Tuning Condenser: 2 Volume Controls: 2 Slider Switches: 3 inch Speaker: Terminal Strip: Ferrite Rod Aerial: 3 Plugs and Sockets: Battery Clips: 4 Tag Boards: Balanced Armature Unit: 10 Transistors: 4 Diodes: Resistors: Capacitors: Three 1" Knobs.
Units once constructed are detachable from Master Unit, enabling them to be stored for future use. Ideal for Schools, Educational Authorities and all those interested in radio construction

All parts including **£5-50** P. P. & Ins. 31p. (Overseas P. & P. £1)



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ROAMER TEN ROAMER SEVEN
ROAMER EIGHT TRANS EIGHT
TRANSONA FIVE ROAMER SIX
POCKET FIVE EDU-KIT

Parts price list and plans for

Name

Address

PW45

CONTROL DRILL SPEEDS

DRILL CONTROLLER NEW IKW MODEL
Electronically changes speed from approximately 10 revs. to maximum. Full power at all speeds by finger-tip control. Kit includes all parts, case, everything and full instructions. \$1.50 plus 43p post and insurance. Made up model also available. \$2.25 plus 13p post & p.

MAINS OPERATED CONTACTOR

220/240v. 50 cycle solenoid with laminated core so very silent in operation. Closes 4 circuits each rated at 10 amps. Extremely well made by a German Electrical Company. Overall size 2 1/2 x 2 x 2in. \$1.50 each.

NEED A SPECIAL SWITCH?

Double Leaf Contact. Very slight pressure closes both contacts. 6p each, 60p doz. Plastic push-rod suitable for operating, 5p each, 45p doz.

AUTO-ELECTRIC CAR AERIAL

with dashboard control switch—fully extendable to 40in. or fully retractable. Suitable for 12v. positive or negative earth. Supplied complete with fitting instructions and ready wired dashboard switch. \$5.75 plus 25p post and ins.

MAINS TRANSISTOR POWER PACK

Designed to operate transistor sets and amplifiers. Adjustable output 6v., 9v., 12 volts for up to 500mA (class B working). Takes the place of any of the following batteries: PP1, PP3, PP4, PP5, PP7, PP9, and others. Kit comprises: mains transformer rectifier, smoothing and load resistor condensers and instructions. Real snip at only \$1 plus 18p postage.

MICRO SWITCH

5 amp changeover contacts, 5p each, \$1 doz. 15 amp Model 10p each or \$1.05 doz.

MINIATURE WAFER SWITCHES

2 pole, 2 way—4 pole, 2 way—3 pole, 3 way—4 pole, 3 way—2 pole, 4 way—3 pole, 4 way—2 pole, 6 way—1 pole, 12 way. All at 20p each, \$1.80 for ten, your assortment.

QUADRAC

The latest thing in variable power control. This is a power thyristor with built in triggering circuit. Requires only variable capacitor and condenser. We can offer the 400V 5 amp model with circuit at only \$1.65.

FLEX CABLE SNIP

3-core heavy circular T.R.S. waterproof flex, ideal for running down the garden to pool or shed. 1.5mm. cores (0 amp). 100 yard coils \$4.25 plus carriage: 75p up to 200 miles; \$1 300 miles, \$1.50 500 miles.

NUMICATOR TUBES

For digital instruments, counters, timers, clocks, etc. Hi-vac XN. 3, Price \$1.45 each. 10 for \$13.

12 WAY SUB-MINIATURE MULTICORE CABLE

7-0076 copper cores each core P.V.C. insulated and of different colour. P.V.C. covered overall and approx. 3/16in. thick. Price 20p per yard.

0-8 AMPMETER

2 1/2" square full vision for flush mounting. Moving iron instrument. Ideal for battery charger. Price 60p each. 10 for \$5.40.

LIGHT CELL

Almost 2% resistant in sunlight increases to 10 K Ohms in dark or dull light, epoxy resin sealed. Size approx. 1in. dia. by 1/2in. thick. Rated at 500 MW, wire ended. 43p with circuit. Also ORP 12 light cell 45p.

TREASURE TRACER MARK II

Complete Kit (except wooden battens) to make the metal detector similar to the circuit in Practical Wireless August issue. \$3.95 plus 20p post and insurance.

BAKELITE INSTRUMENT CASE

Size approx. 6 1/4" x 3 1/2" x 2" deep with brass inserts in four corners and bakelite panel. This is a very strong case suitable to house instruments and special rigs, etc. Price 45p each.

MULLARD I.F. MODULE

This is a fully screened intermediate frequency module for amplification and detection of f.m. signals at 10.7MHz and a.m. signals at 470kHz. The first stage is used as an i.f. amplifier for f.m. and a self-oscillating mixer for a.m. operation, in conjunction with an external oscillator coil. 75p each. 10 for \$6.75. 100 for \$62.50p. With connection dig.

STANDARD WAFER SWITCHES

Standard size 1 1/4" wafer—silver-plated 5-amp contact, standard 1" spindle 2" long—with locking washer and nut.

No. of Poles	2 way	3 way	4 way	5 way	6 way	8 way	9 way	10 way	12 way
1 pole	40p	40p							
2 poles	40p	40p							
3 poles	40p	40p							
4 poles	40p	40p							
5 poles	40p	40p							
6 poles	40p	40p							
7 poles	70p	70p							
8 poles	70p	70p							
9 poles	70p	70p							
10 poles	70p	70p							
11 poles	70p	70p							
12 poles	70p	70p							

13 AMP TWIN GANG SOCKETS

Offered at less than wholesale price your opportunity to replace those dangerous old-fashioned bakelite flush mounting—considerable air flow but virtually no noise. Approx. dimensions 10 1/2 in. wide x 12 in. dia. outlet trunking 10 1/2 x 4 1/2 in. \$4.95 plus 1p post and insurance.

THIS MONTH'S SNIP

YOUR TIME is the most precious thing you have. Do you waste it waiting for the soldering iron to heat up? You can be soldering in a few seconds with the E.T.P. Solder Gun which we offer at a specially kept price. It is in fact this month's snip. A well made lightweight unit with flash lamp to illuminate the work. Has 100 watt double insulated main Transformer and is built into a shockproof Thermo-plastic case. Suitable for 240volt, 50 c.p.s. This comes complete with 5 spare tips and is offered at a special snip price \$2.25. plus 20p post and insurance.

CENTRIFUGAL FAN

Mains operated, turbo blower type. Pressed steel housing contains motor and impeller. Motor is 1/10th h.p. giving considerable air flow but virtually no noise. Approx. dimensions 10 1/2 in. wide x 12 in. dia. outlet trunking 10 1/2 x 4 1/2 in. \$4.95 plus 1p post and insurance.

THERMOSTAT WITH THERMOMETER

Made by Honeywell for normal air temperatures 40°-80°F. (5-25°C). This is a precision instrument with a differential which can be adjusted to better than 1-5°F. A mercury switch breaks on temp. rise—the switch is operated by coiled bi-metal element and an adjustable heater is incorporated for heat anticipation. Elegantly styled and encased in an ivory plastic case with clear plastic windows, thermometer scale and switch settings scale below. Size approx. 3-8" x 3-2" x 1-4" deep. Can be mounted on conduit box or directly on wall. Price \$1.25 each or 10 for \$11.25.

MULLARD AUDIO AMPLIFIER MODULE

Uses 4 transistors, and has an output of 500mW into 8 ohm speakers. Input suitable for crystal mic. or pickup. 5 volt battery operated. Size 2" long x 1 1/2" wide x 1" high. SPECIAL SNIP PRICE 60p each. 10 for \$5.40

DISTRIBUTION PANELS

Just what you need for work bench or on 4 or 13 amp sockets in metal box to take 13 amp plugs and on/off switch with neon warning light. Supplied complete with 7 feet of heavy cable. Wired up ready to work, \$2.25 less plug; \$2.50 with fitted 13 amp plug; \$2.65 with fitted 15 amp plug, plus 23p P. & P.

1 HOUR MINUTE TIMER

Made by Smiths. Complete with control knob and calibrated dial. This month's special bargain at 60p. Useful in the kitchen, office and dark-room, etc.

ELECTRIC TIME SWITCH

Made by Smiths these are A.C. mains operated. NOT CLOCKWORK. Ideal for mounting on rack or shelf or incorporated for heat anticipation. Contacts rated at 15 amps. Operable time periods per 24 hours, 5 amp change-over contacts will switch circuit on or off during these periods \$2.50 post and ins., 23p. Additional time contacts 50p pair.

3000 WATT IMMERSION HEATER

220-250 volts. Suitable all water tanks. 1 1/2" long, normal hole fixing complete with bakelite cover over connections. This is a standard immersion heater made by the famous Remploy Company. Price \$1.50. Thermostat 30p extra.

50 MICRO AMPMETER

Square, panel mounting type: \$2.

MAINS OPERATED SOLENOIDS

Model 772—small but powerful 1 1/2" tall—approx. size 1 1/2" x 1 1/2" x 1 1/2" 60p
Model 400/1 1/2" tall Size 2 1/2" x 2 x 1 1/2" 75p

Model TT10 1 1/4" tall size 3 x 2 1/2 x 2 1/8 plus 20p. post and insurance.

MAINS RELAY BARGAIN

Special this month are some single, double and treble pole change-over relays. Contacts rated at 15 amps. Operating coil wound for 240V A.C. Good British Make. Unused. Size approx. 1 1/2" x 1". Open construction. Single pole 25p each 10 for \$2.25
Treble pole 35p each 10 for \$3.15

CD CAR IGNITION

This system which has proved to be amazingly efficient. We offer kit of parts as P.W. Circuit \$5.95 plus 20p p. & p. De luxe model with prepared circuit board \$6.95. When ordering please state whether for positive or negative systems.

ELECTRONIC IGNITION

22 POSITION SOLENOID OPERATED STUD SWITCH
Mains operated, each current pulse to switch solenoid moves switch arm through one position on to the next contact stud—current to release solenoid brings back switch arm to position. These are ex-equipment but in good working order. Any not so would be replaced. Price 50p each.

TIMED 'ON' SWITCHES

Made by Smiths for washing machines etc. Centre spindle closes double pole 15 amp switch directly it is turned. A full 360° turn or only a part turn winds the clockwork mechanism and keeps the switch closed until the spindle returns to the 'off' position. A dial therefore could be fitted to indicate hours and minutes and the switch on period could be set quite accurately. 3 models available—90 minutes, 120 minutes and 360 minutes. Price 95p each. Metal clad pointer knob 15p. Suitable relay to make the switch 'on' instead of 'off' 35p.

MOTOR GENERATOR

Ex Admiralty—24 volt D.C. input—240v 50 cps output. Admiralty rating 80 watt but we have tested this to 50% overload—120 minutes and 360 minutes. Price 95p each. Metal clad pointer knob 15p. Suitable relay to make the switch 'on' instead of 'off' 35p.

PAPST MOTORS

Est. 1/40th h.p. Made for 110-120 volt working, but two of these work ideally together off our standard 240 volt mains. A really beautiful motor, extremely quiet running, and reversible. \$1.50 each. Postage one 23p, two 33p. 230v model \$3.

PRESSURE SWITCH

Containing a 15 amp. change over switch operated by a diaphragm which in turn is operated by air pressure regulated so suitable to control TV or instrument. In case with metal cover—controls on front include voltmeter. Probably cost £200 each to make. Our price only \$25 each plus carriage. \$2 up to 200 miles \$4 up to 400 miles.

TAPE HEADS

Miniature size, approximately 1" square by 1 1/2" long. These are double wound for stereo. Offered at a very low price of 45p each. New and unused.

LEVER SWITCH REF. H52/4

Ideal for intercom or similar. Pressing the lever down operates 6 pairs of change-over contacts, pressing the lever up operates 4 pairs of change-over contacts. The switch is spring loaded and normally returns to the off or centre position. Size approximately 1 1/2" long x 2 1/2" deep x 1" thick. 40p each.

PUSH BUTTON SWITCHES

Mains, suitable for audio or R.F. Each switch rated at 250v 15 amps. Lat (black push button) closes 2 circuits. 2nd (white push button) operates one change over. 3rd (white push button) operates one change over. 4th (white push button) opens one circuit. Note: depressed buttons remain down until cleared by the 5th (red button). Further note:—It is a relatively easy job to alter the position of the tags thus making the switches suit your circuit. Fitted with 3 white 1 red and 1 black button. 80p each or 10 for \$7.70.

7 POS ROTARY MAINS SWITCH

Rated 15 amp at 230v. 4 circuits. Position A—all circuits open. Position B—circuit 1 closed. Position C—circuit closed. Position D, circuits 2, 3 & 4 closed. Position E—2 & 3 circuits closed. Position F—1, 2, 3, & 4 circuits closed. Position G—2 & 4 circuits closed. 15p each or 10 for \$1.35.

EDGE CONNECTORS

32 way for 2" strip boards. Gold plated contacts. 50p each or 10 for \$4.50

VEROBOARD

Offcuts—10 pieces—1—15 & 2 matrix. All good useful sizes. Total not less than 160 sq. ins. Very useful for circuit prototyping. Regular price value at least £2. Price \$1 the lot.

8 AMP VARIACS

These are variable voltage transformers. British made by the famous Zenith Co. Fully enclosed for bench use and fitted with calibrated scale and control knob. Zenith Model No. 100 L.M. 220-240 A.C. output 0-240volt up to 8 amps. This model is listed at nearly £20. We have a limited quantity only, absolutely brand new still in makers cartons, offered to you at \$13.50 each plus 41 carriage and insurance up to 400 miles.

Where postage is not stated then orders over £5 are post free. Below £5 add 20p. Semiconductor add 5p. Over £1 post free. S.A.E. with enquiries please.

J. BULL (ELECTRICAL LTD.)
(Dept. P.W.), 7 Park Street, Croydon CRO 1YD
Callers to: 102/3 Tamworth Road, Croydon.

POWERTRAN ELECTRONICS

Specialists in high quality kits for high quality audio equipment. Previously concentrating on advanced Wireless World designs (pre-amps, power amplifiers from 10 to 100 watts, power supplies, tape recorder) we now proudly add the Practical Wireless TEXAN to our range

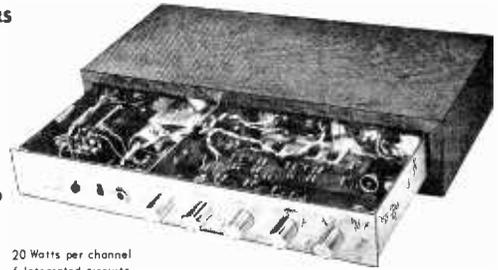
APPOINTED DISTRIBUTORS

FOR THE

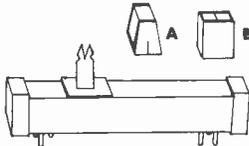
'TEXAN'

TEXAS INSTRUMENTS DESIGNED

& APPROVED FULL KIT



SLIDER POTENTIOMETERS



LENGTH 87mm WIDTH 10mm TRAVEL 55mm

Single: log or lin 10K, 22K, 47K, 100K 35p
 Dual: log or lin 10K, 22K, 47K, 100K 55p
 Balance: special dual track 10K 60p
 Black/Chrome knob-type A or B 12p

23mm CARBON POTENTIOMETERS

Single: lin 1K to 2M2 12p
 log 4K7 to 2M2 12p
 Dual: lin or log 4K7 to 2M2 35p
 Balance: 10K log/A log 40p
 Switched: log single 10K, 100K 30p
 log dual 10K, 100K, 1M 55p

£28.50

post (UK) 45p

INCLUDES TEAK CASE

SEMICONDUCTORS

2N699	0.30	40361	-0.40	MPSA66	0.40
2N1613	0.20	40362	0.45	MPSH05	0.20
2N1711	C	BC107	0.08	MPSU05	0.60
2N2926G	0.10	BC108	0.08	MPSU55	0.70
2N3053	0.20	BC109	0.08	SN72741P	0.95
2N3055	0.45	BC125	0.15	SN72748P	0.95
2N3442	0.10	BC126	0.15	THB11	1.10
2N3702	0.11	BC182K	0.10	TIP29A	0.50
2N3703	0.10	BC212K	0.12	TIP30A	0.60
2N3704	0.10	BC182L	0.10	TIP31A	0.60
2N3705	0.10	BC184L	0.10	TIP32A	0.70
2N3706	0.09	BC212L	0.11	TIP33A	1.00
2N3707	0.10	BC214L	0.14	TIP34A	1.50
2N3708	0.07	BF257	0.55	TIP41A	0.74
2N3709	0.09	BF259	0.60	TIP42A	0.90
2N3710	0.09	BFX29	0.30	TIP3055	0.60
2N3711	0.09	BF150	0.20	1B08T20	0.50
2N3819	0.25	MJ481	1.20	1B40K20	1.40
2N3904	0.20	MJ491	1.30	1N914	0.07
2N3906	0.20	MJES21	0.70	1N916	0.07
2N4058	0.12	MPSA05	0.30	1544	0.05
2N4062	0.11	MPSA12	0.55	15920	0.10
2N4302	0.60	MPSA14	0.35	153062	0.25
2N5457	0.30	MPSA55	0.35	5B05	1.20
2N5830	0.30	MPSA65	0.35		

20 Watts per channel

6 integrated circuits

10 transistors

HARMONIC DISTORTION

0.05% at 15W 1KHz into 15 ohm

0.09% at 20W 1KHz into 8 ohm

FREQUENCY RESPONSE

5Hz to 35KHz (-3dB)

SIGNAL TO NOISE RATIO

60dB magnetic pick-up

72dB radio

Components available in separate packs

Eg.

Resistors and capacitors £ 3.70

Switches and controls £ 2.35

Fibre Glass PCB £ 2.50

Semiconductors £ 8.35

For other parts and full specification please see our free list.

THYRISTORS

PIV	1A	3A	7A	16A	1A	1.5A	3A
50	25p	27p	45p	60p	2p	8p	19p
100	27p	30p	50p	65p	7p	9p	20p
200	35p	37p	55p	75p	8p	10p	22p
300	40p	45p	60p	85p	9p	11p	25p
400	45p	50p	65p	90p	10p	12p	26p

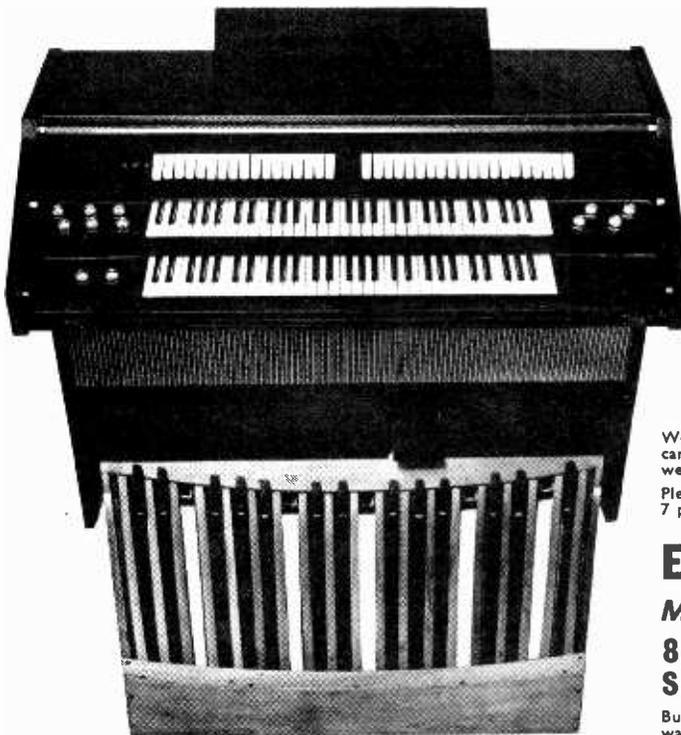
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MAIL ORDER ONLY



ORGAN KITS

Build your own Electronic Organ, if you want the best value for your money. Yes you really save over 50% and get the best and up-to-date designs. There are four models to choose from.

★ Portable—4 octave keyboard with 10 voices, 3 pitches—vibrato, at £103.00, P/P £1.50.

★ Console—5 octave keyboard with 10 voices, 3 pitches. Keyboard can be split into solo and accompaniment. Vibrato built in amplifier and 50 watt 12" Goodmans speaker at £167.00, P/P £5.00.

★ Console—2 x 4 octave keyboards and 13 note pedal board, 29 voices, Vibrato, Delay Vibrato, Sustain Reverberation, Precussion, Wah Wah, etc. at £406.00. Carr. paid on complete kit U.K. only.

★ Console—2 x 5 octave keyboards and 32 note pedal boards, 32 voices, Vibrato, Delay Vibrato, Sustain Reverberation, Precussion, 3 Couplers, etc., at £572.55 carr. paid on complete kit U.K. only.

We regret H.P. facilities are not available, but components can be bought separately. Trade and overseas enquiries welcomed. Send 25p for latest catalogue.

Please call in for demonstration. Business hours: 10 a.m. to 7 p.m. Monday to Saturday. Thursday closed.

ELVINS ELECTRONIC MUSICAL INSTRUMENTS

8, PUTNEY BRIDGE RD., LONDON
S.W.18 TEL: 01-870 4949

Bus numbers 37, 220, 225, 168 pass the door. 10 minutes walk from East Putney or 15 minutes walk from Putney Bridge Underground Stations.

The largest selection

NEW LOW PRICE TESTED S.C.R.'s

PIV	3A		7A		10A		16A		30A	
	TO-5	TO-66	TO-66	TO-66	TO-48	TO-48	TO-48	TO-48	TO-48	TO-48
30	0.23	0.25	0.47	0.50	0.53	0.63	1.15			
100	0.33	0.35	0.53	0.58	0.63	1.40				
200	0.35	0.47	0.57	0.61	0.75	1.60				
400	0.43	0.47	0.67	0.75	0.93	1.75				
600	0.53		0.77	0.87	1.25					
800	0.63	0.70	0.90	1.20	1.50	4.00				

SIL. RECTS. TESTED

PIV	300mA 750mA		1A		1.5A		3A		10A		30A	
	5p	5p	5p	5p	5p	5p	5p	5p	5p	5p	5p	5p
50	0.04	0.05	0.05	0.07	0.14	0.21	0.21	0.47				
100	0.04	0.06	0.05	0.13	0.16	0.23	0.23	0.75				
200	0.05	0.09	0.06	0.14	0.20	0.24	1.00					
400	0.08	0.13	0.07	0.20	0.27	0.37	1.25					
600	0.07	0.16	0.10	0.23	0.34	0.45	1.85					
800	0.10	0.17	0.13	0.25	0.37	0.55	2.00					
1000	0.11	0.25	0.15	0.30	0.46	0.63	2.50					
1200		0.33		0.33	0.57	0.75						

TRIACS

V _{BM}	2A		6A		10A	
	TO-1	TO-66	TO-66	TO-66	TO-66	TO-66
100	30	50	50	76		
200	50	70	70	90		
400	70	75	75	1.10		

DIACS

FOR USE WITH TRIACS	
BR100 (D3)	37 each

UNIJUNCTION

UT46	Evnt. 2N2646
UT47	1T1843, BEN3646
27p	each 25-30 25p

PN SILICON PLANAR
BC107/108, 10p each.
50-99 8p; 100 off.
8p each; 1,000 off.
7p each. Fully tested
and cooled TO-18 case.

FREE

One 50p Pak of your
choice free with
orders valued \$4 or over.

SPECIAL OFFER

2N2926 (Y) (O)
10 for 50p, 25 for £1
20,000 TO CLEAR

CADMIUM CELLS

ORP12 43p
ORP60, ORP61 40p each

GENERAL PURPOSE NPN SILICON SWITCHING TRANS. TO-18

SIM. TO 2N706/8, BSY-27/28/95A.	
20	Por 1.50
50	Por 1.75
100	Por 1.75
500	Por 7.50
1000	Por 13.00

PHOTO TRANS.

OCP71 Type 43p

SIL. G.P. DIODES

300mW 30 0.50
40PIV(Min.) 30 0.50
Sub-Min. 500 5.00
Full Tested 1,000 9.50
Ideal for Organ Builders

DIS12 Silicon Unilateral switch 50p each.

A Silicon Planar, monolithic integrated circuit having thyristor electrical characteristics, but with an anode gate and a built-in "zero" diode between gate and cathode. Full data and application circuits available on request.

FULL RANGE OF ZENER DIODES

2-33V 400mW TO-7 (base) 13p ea. 1W (Top Hat) 35p ea. (SO-10 Stud) 25p ea. All fully tested, 5% tol. and marked. State voltage required.

10 amp POTTED BRIDGE RECTIFIER on heat sink.
100PIV, 90p each

JUMBO COMPONENT PAKS MIXED ELECTRONIC COMPONENTS
Exceptionally good value

Resistors, capacitors, pots, electrolytics and coils plus many other useful items. Approximately 3lbs in weight. Price incl. P. & P. 21.50 only

Plus your satisfaction or money back guarantee.

BRAND NEW TEXAS GERM. TRANSISTORS

Coded and Guaranteed

PaK No. EQVT

T1	8 2G3713	OC71
T2	8 D1374	OC75
T3	8 D1216	OC81D
T4	8 2G381T	OC81
T5	8 2G382T	OC82
T6	8 2G344B	OC44
T7	8 2G345B	OC45
T8	8 2G347R	OC78
T9	8 2G399A	2N1302
T10	8 2G417	AF117

2N3060 NPN SIL. DUAL TRANS. CODED NPN TEXAS. Our price 23p each

120 VCB MIXIE DRIVER TRANSISTOR. 8im. B8X21 & C407, 2N1893 FULLY TESTED AND CODED ND 120, 124 17p each. TO-5 P.N.P. 25 up 15p each.

Sil. trans. suitable for Pk. Organ Metal TO-18 Evnt. ZTX300 5p each. Any Qty.

NEW LINE

Plastic Encapsulated 2 Amp. BRIDGE RECTS. 60 v RMS 32p each
100 v RMS 37p ..
400 v RMS 45p ..
Size 15 mm x 6 mm.

KING OF THE PAKS Unequalled Value and Quality

SUPER PAKS NEW BI-PAK UNTESTED SEMICONDUCTORS

Satisfaction GUARANTEED in Every Pak. or money back.

Pak No.	Description	Price
U1	120 Class sub-min. general purpose germanium diodes	0.50
U2	60 Mixed germanium transistors AF/RF	0.50
U3	75 Germanium gold bonded diodes sim. OA5, OA47	0.50
U4	40 Germanium transistors like OC81, AC128	0.50
U5	60 200mA sub-min. Sil. diodes	0.50
U6	30 Silicon planar transistors NPN sim. BSY95A, 2N706	0.50
U7	16 Silicon rectifiers Top-Hat 750mA up to 1,000V	0.50
U8	50 Sil. planar diodes 250mA, OA/200/202	0.50
U9	20 Mixed volts 1 watt Zener diodes	0.50
U11	30 PNP silicon planar transistors TO-5 sim. 2N1132	0.50
U13	25 PNP-NPN sil. transistors OC200 & 2N104	0.50
U14	150 Mixed silicon and germanium diodes	0.50
U15	25 NPN Silicon planar transistors TO-5 sim. 2N697	0.50
U16	10.3-Amp silicon rectifiers stud type up to 1,000 PIV	0.50
U17	30 Germanium PNP AF transistors TO-5 like ACY 17-22	0.50
U18	8 6-Amp silicon rectifiers BY213 type up to 600 PIV	0.50
U19	25 Silicon NPN transistors like BC108	0.50
U20	12 1.5 Amp silicon rectifiers Top-Hat up to 1,000 PIV	0.50
U21	30 A.F. germanium alloy transistors 2G300 series & OC71	0.50
U23	30 Malt's like MAT series PNP transistors	0.50
U24	20 Germanium 1-Amp rectifiers GJM up to 300 PIV	0.50
U25	25 300 Mc/s NPN silicon transistors 2N708, BSY27	0.50
U26	30 Fast switching silicon diodes like IN914 micro-min	0.50
U29	10 1-Amp SCR's TO-5 can up to 600 PIV CRS1/25-600	1.00
U31	20 Sil. Planar NPN trans. low noise amp 8N3707	0.50
U32	25 Zener diodes 400mW D07 case mixed volts, 3-18	0.50
U33	15 Plastic case 1 amp silicon rectifiers IN4000 series	0.50
U34	30 Sil. PNP alloy trans. TO-5 BCY26, 28302/4	0.50
U35	25 Sil. planar trans. PNP TO-18 2N2906	0.50
U36	25 Sil. planar PNP trans. TO-5 BFY50/51/52	0.50
U37	30 Sil. alloy trans. 80-2 PNP, OC200 28322	0.50
U38	20 Fast switching sil. trans. NPN, 400Mc/s 2N3011	0.50
U39	30 RF germ. PNP trans. 2N1303 5 TO-5	0.50
U40	10 Dual trans. 6 lead TO-5 2N2060	0.50
U41	25 RF germ. trans. TO-1 OC45 NKT72	0.50
U42	10 VHF germ. PNP trans. TO-4 BC17687, AF117	0.50
U43	25 Sil. trans. plastic TO-18 A.F. BK135/114	0.50
U44	20 Sil. trans. plastic TO-5 BC115/116	0.50
U45	7 3A SCR's TO-66 up to 600 PIV	1.00

Code Nos. mentioned above are given as a guide to the type of device in the Pak. The devices themselves are normally unmarked.

NEW QUALITY TESTED PAKS

Pak Description	Price	
Q1	20 Red spot trans. PNP AF	0.50
Q2	16 White spot R.F. trans. PNP	0.50
Q3	4 OC77 type trans.	0.50
Q4	6 Matched trans. OC44/46/81/81D	0.50
Q5	4 OC75 transistors	0.50
Q6	4 OC72 transistors	0.50
Q7	4 AC128 trans. PNP high gain	0.50
Q8	4 AC126 trans. PNP	0.50
Q9	7 OC81 type trans.	0.50
Q10	7 OC71 type trans.	0.50
Q11	2 AC127/128 comp. pairs PNP/NPN	0.50
Q12	3 AF116 type trans.	0.50
Q13	3 AF117 type trans.	0.50
Q14	3 OC171 H.F. type trans.	0.50
Q15	2 2N2926 Sil. epoxy trans.	0.50
Q16	2 6FT890 low noise germ. trans.	0.50
Q17	3 NPN 1 BT141 & 2 BT140	0.50
Q18	4 Malt's 2 MAT 100 & 2 MAT 120	0.50
Q19	3 Malt's 2 MAT 101 & 1 MAT 121	0.50
Q20	4 OC44 germ. trans. A.F.	0.50
Q21	3 AC127 NPN germ. trans.	0.50
Q22	20 NKT trans. A.F. R.F. coded	0.50
Q23	10 OA202 sil. diodes sub-min.	0.50
Q24	8 OA81 diodes	0.50
Q25	6 IN914 sil. diodes 75PIV 75mA	0.50
Q26	8 OA95 germ. diodes sub-min. IN69.	0.50
Q27	2 10A 600PIV sil. rect. 1845R	0.50
Q28	2 Sil. power rect. BY213	0.50
Q29	4 Sil. trans. 2 x 2N696. 1 x 2N697.	0.50
Q30	7 Sil. switch trans. 2N706 PNP	0.50
Q31	6 Sil. switch trans. 2N708 NPN	0.50
Q32	3 PNP sil. trans. 2 x 2N1131.	0.50
Q33	3 Sil. NPN trans. 2N1111	0.50
Q34	7 Sil. NPN trans. 2N3369, 500MHZ.	0.50
Q35	3 Sil. PNP TO-5 2 x 2N2904 & 1 x 2N2905	0.50
Q36	7 2N3646 TO-18 plastic 300MHZ NPN	0.50
Q37	5 2N3053 NPN sil. trans.	0.50
Q38	7 NPN trans. 4 x 2N3703, 3 x 2N3702	0.50
Q39	7 NPN trans. 4 x 2N3704, 3 x 2N3705	0.50
Q40	7 NPN amp. 4 x 2N3707, 3 x 2N3708	0.50
Q41	3 Plastic NPN TO-18 2N3004	0.50
Q42	6 NPN trans. 2N5172	0.50
Q43	7 BC107 NPN trans.	0.50
Q44	7 NPN trans. 4 x BC108, 3 x BC109	0.50
Q45	3 BC118 NPN TO-18 trans.	0.50
Q46	3 BC115 NPN TO-5 trans.	0.50
Q47	6 NPN high gain 3 x BC167, 3 x BC168	0.50
Q48	4 BCY70 NPN trans. TO-18	0.50
Q49	4 NPN trans. 2 x BFY51, 2 x BFY52	0.50
Q50	7 BSY28 NPN switch TO-18	0.50
Q51	BSY95A NPN trans. 500MHZ	0.50
Q52	8 BY100 type sil. rect.	1.00
Q53	25 Sil. & germ. trans. mixed all marked new	1.50

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Packed with semiconductor and component. 10 boards give a guaranteed 30 trans and 30 diodes. Our price 10 boards. 50p Plus 10p P. & P. 100 Boards 23. P. & P. 30p.

POWER TRANSISTOR BONANZA!

GENERAL PURPOSE GERM. PNP
Coiled GP100. BRAND NEW TO-3 CASE. POSS. REPLACE. —OC25-28-29-30-35-36. NKT 401-403-404-405-406-430-451-452-453. T13027-3028, 2N260A, 2N456A-457A-458A, 2N611 A & B, 2G220-222, ETC. VCB0 80V VCEO 50V IC 10A PT. 30 WATTS Hfe 30-170.
PRICE: 1-24 25-99 100 up 43p each 40p each 66p each

AD161 NPN
AD162 PNP
M/P COMP GERM TRANS.
OUR LOWEST PRICE OF 55p PER PAIR

2N3055
115 WATT SIL POWER NPN
50p EACH

SILICON High Voltage 250V PNP
TO-3 case. G.P. Switching & Amplifier Applications. Brand new Coded R 2400 VCB0 250V VCEO 100IC 6A/30 Watts. HFE type 20/IT 5MHZ.
OUR PRICE EACH: 1-24 25-99 100 up 50p 45p 40p

EX-STOCK TYPE EACH AS PRICED
OC220 50p OC228 40p AD149 43p BD131 70p BD139 75p
OC223 30p OC229 40p AL102 85p BD132 80p BD140 85p
OC235 30p OC35 33p AL103 85p BD135 70p BD155 75p
OC245 30p OC36 40p BD121 60p BD136 80p BU105 23
OC245 25p AD149 40p BD123 75p BD137 70p 2N3054 45p
OC245 30p AD142 40p BD124 70p BD138 80p

SILICON PHOTO TRANSISTOR. TO-18 Lens end NPN 5mm to HF x 25 and P21. BRAND NEW. Full data available. Fully guaranteed. Qty. 1-24 25-99 100 up Price each 45p 40p 35p

E.E.T.'S

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2N3820	30p	2N5459	40p
2N3821	30p	BFW10	40p
2N3823	30p	MPP105	40p

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TRANSISTOR EQUIVALENTS BOOK. A complete cross reference, and equivalents book for European American and Japanese Transistors. Exclusive to BI-PAK 90p each.

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14 & 16 Lead Sockets for use with

DUAL-IN-LINE I.C.'s. TWO Ranges PROFESSIONAL & NEW LOW COST.
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T80 16 " " 35p 32p 30p

LOW COST No.
BPS 14 15p 13p 11p
BPS 16 16p 14p 12p

-the lowest prices!

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Check our 74 Series List before you buy any I.C.'s. Our prices are the lowest possible. All devices ex-stock. Full spec. guaranteed

BI-PAK Order No.	Price and qty. prices			BI-PAK Order No.	Price and qty. prices		
	1-24	25-99	100 up		1-24	25-99	100 up
BP00 = 8N7400	0.15	0.14	0.12	BP96 = 8N7486	0.87	0.80	0.28
BP01 = 8N7401	0.15	0.14	0.12	BP97 = 8N7490	0.87	0.84	0.58
BP02 = 8N7402	0.15	0.14	0.12	BP98 = 8N7491AN	0.87	0.84	0.78
BP03 = 8N7403	0.15	0.14	0.12	BP99 = 8N7492	0.87	0.84	0.58
BP04 = 8N7404	0.15	0.14	0.12	BP99 = 8N7493	0.87	0.84	0.58
BP05 = 8N7405	0.15	0.14	0.12	BP99 = 8N7494	0.77	0.74	0.88
BP07 = 8N7407	0.18	0.17	0.16	BP99 = 8N7495	0.77	0.74	0.88
BP08 = 8N7408	0.18	0.17	0.16	BP99 = 8N7496	0.77	0.74	0.68
BP09 = 8N7409	0.18	0.17	0.16	BP100 = 8N74100	1.75	1.65	1.55
BP10 = 8N7410	0.15	0.14	0.12	BP104 = 8N74104	0.97	0.94	0.88
BP13 = 8N7413	0.28	0.26	0.24	BP105 = 8N74105	0.97	0.94	0.88
BP16 = 8N7416	0.43	0.40	0.38	BP107 = 8N74107	0.40	0.38	0.36
BP17 = 8N7417	0.43	0.40	0.38	BP110 = 8N74110	0.55	0.53	0.50
BP19 = 8N7419	0.15	0.14	0.12	BP111 = 8N74111	1.25	1.15	1.00
BP20 = 8N7420	0.15	0.14	0.12	BP118 = 8N74118	1.00	0.95	0.90
BP40 = 8N7440	0.15	0.14	0.12	BP119 = 8N74119	1.35	1.25	1.10
BP41 = 8N7441	0.87	0.84	0.58	BP121 = 8N74121	0.87	0.84	0.58
BP42 = 8N7442	0.87	0.84	0.58	BP141 = 8N74141	0.87	0.84	0.58
BP43 = 8N7443	1.85	1.85	1.75	BP145 = 8N74145	1.50	1.40	1.30
BP44 = 8N7444	1.85	1.85	1.75	BP150 = 8N74150	1.80	1.70	1.60
BP45 = 8N7445	0.87	0.84	0.58	BP151 = 8N74151	1.00	0.95	0.90
BP46 = 8N7446	0.87	0.84	0.58	BP153 = 8N74153	1.20	1.10	0.95
BP47 = 8N7447	0.87	0.84	0.58	BP154 = 8N74154	1.80	1.70	1.60
BP48 = 8N7448	0.87	0.84	0.58	BP155 = 8N74155	1.40	1.30	1.20
BP50 = 8N7450	0.15	0.14	0.12	BP156 = 8N74156	1.40	1.30	1.20
BP51 = 8N7451	0.15	0.14	0.12	BP160 = 8N74160	1.80	1.70	1.60
BP53 = 8N7453	0.15	0.14	0.12	BP161 = 8N74161	1.80	1.70	1.60
BP54 = 8N7454	0.15	0.14	0.12	BP164 = 8N74164	2.00	1.90	1.80
				BP165 = 8N74165	2.00	1.90	1.80
				BP181 = 8N74181	2.75	2.60	2.40
BP60 = 8N7460	0.15	0.14	0.12	BP182 = 8N74182	0.97	0.94	0.88
BP70 = 8N7470	0.28	0.26	0.24	BP190 = 8N74190	3.50	3.25	3.00
BP72 = 8N7472	0.28	0.26	0.24	BP191 = 8N74191	3.50	3.25	3.00
BP73 = 8N7473	0.37	0.35	0.32	BP192 = 8N74192	2.10	1.95	1.75
BP74 = 8N7474	0.37	0.35	0.32	BP193 = 8N74193	2.10	1.95	1.75
BP75 = 8N7475	0.43	0.40	0.38	BP195 = 8N74195	1.10	1.05	0.95
BP76 = 8N7476	0.43	0.40	0.38	BP196 = 8N74196	1.80	1.70	1.60
BP80 = 8N7480	0.87	0.84	0.58	BP197 = 8N74197	1.80	1.70	1.60
BP81 = 8N7481	0.87	0.84	0.58	BP198 = 8N74198	5.50	5.00	4.00
BP82 = 8N7482	0.87	0.84	0.58	BP199 = 8N74199	5.50	5.00	4.00
BP83 = 8N7483	1.10	1.05	0.95				

PRICE-MIX. Devices may be mixed to qualify for quantity prices.
PRICES for quantities in excess of 500 pieces mixed, on application.
Owing to the ever increasing range of TTL 74 Series, please check with us for supplies of any devices not listed above, as it is probably now in stock. WARE 3442.

ROCK BOTTOM PRICES LOGIC DTL 930 Series I.C.'s

Type No.	Price
	1-24 25-99 100 up
BP930	12p 11p 10p
BP932	13p 12p 11p
BP933	13p 12p 11p
BP935	13p 12p 11p
BP936	13p 12p 11p
BP944	13p 12p 11p
BP945	25p 24p 22p
BP946	12p 11p 10p
BP948	25p 24p 22p
BP951	65p 60p 55p
BP992	12p 11p 10p
BP9903	40p 38p 35p
BP9904	40p 38p 35p
BP9907	40p 38p 35p
BP9909	40p 38p 35p

Devices may be mixed to qualify for quantity price. Larger quantity prices on application. (DTL 930 Series only).

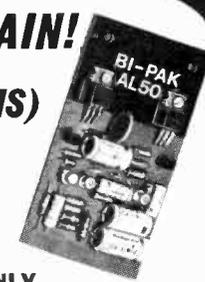
LINEAR I.C.'s—FULL SPEC.

Type No.	Price
	1-24 25-99 100 up
BP 201C—8L201C	85p 53p 45p
BP 701C—8L701C	85p 50p 45p
BP 702C—8L702C	85p 50p 45p
BP 702—72702	53p 45p 40p
BP709—72709	53p 45p 40p
BP 709P—8L709C	53p 45p 40p
BP 710—72710	53p 40p 35p
BP 711—8L711	58p 45p 40p
BP 741—72741	75p 60p 50p
8L7403C—8L7403C	43p 34p 27p
TAA 263—	70p 60p 55p
TAA 293—	90p 75p 70p
TAA 350—	170p 158p 150p

R.G.S. EA1000 2-83

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50W pk 25w (RMS)



0.1% DISTORTION!

HI-FI AUDIO AMPLIFIER

THE AL50

- ★ Frequency Response 15Hz to **ONLY 100,000—1dB.**
- ★ Load—3, 4, 8 or 16 ohms.
- ★ Distortion—better than 1% at 1KHz.
- ★ Signal to noise ratio 80dB.

£3.25p each

★ Supply voltage 10-35 Volts.

★ Overall size 63mm x 105mm x 13mm.

Tailor made to the most stringent specifications using top quality components and incorporating the latest solid state circuitry and AL50 was conceived to fill the need for all your A.F. amplification needs.
FULLY BUILT—TESTED—GUARANTEED.

STABILISED POWER MODULE

AP80 is especially designed to power 2 of the AL50 Amplifiers, up to 15 watt (rms) per channel, simultaneously. This module embodies the latest components and circuit techniques incorporating complete short circuit protection. With the addition of the Mains Transformer MT80, the unit will provide outputs of up to 15amps at 35volts. Size: 63mm x 105mm x 30mm.

These units enable you to build Audio Systems of the highest quality at a hitherto unobtainable price. Also ideal for many other applications including: Disco Systems, Public Address, Intercom Units etc. Handbook available 10p.

STABILISED POWER MODULE-SPM80 £2.95

TRANSFORMER BMT80 £1.95 p. & p. 25p.

SPECIAL COMPLETE KIT COMPRISING 2, AL50's, 1, SPM80 & 1, BMT80 ONLY £11 FREE p. & p.

DTL & TTL INTEGRATED CIRCUITS

Manufacturers' "Fall outs"—out of spec. devices including functional units and part function but classed as out of spec. from the manufacturers' very rigid specifications. Ideal for learning about I.C.'s and experimental work.

Pak No.	Price	Pak No.	Price
UIC930 = 12 x μ A 930	50p	UIC948 = 8 x μ A 948	50p
UIC932 = 12 x μ A 932	50p	UIC951 = 5 x μ A 951	50p
UIC933 = 12 x μ A 933	50p	UIC961 = 12 x μ A 961	50p
UIC935 = 12 x μ A 935	50p	UIC9093 = 5 x μ A 9093	50p
UIC936 = 12 x μ A 936	50p	UIC9094 = 5 x μ A 9094	50p
UIC944 = 12 x μ A 944	50p	UIC9097 = 5 x μ A 9097	50p
UIC945 = 8 x μ A 945	50p	UIC9099 = 5 x μ A 9099	50p
UIC946 = 12 x μ A 946	50p	UIC9 25 Assorted 930 Series	£1.50

Packs cannot be split but 25 Assorted Pieces (our mix) is available as Pack UIC9 9 Data Booklet available for the BP930 Series, PRICE 13p

UIC00 = 12 x 7400N	50p	UIC46 = 5 x 7446N	50p	UIC81 = 5 x 7481N	50p
UIC01 = 12 x 7401N	50p	UIC47 = 5 x 7447N	50p	UIC82 = 5 x 7482N	50p
UIC02 = 12 x 7402N	50p	UIC48 = 5 x 7448N	50p	UIC83 = 5 x 7483N	50p
UIC03 = 12 x 7403N	50p	UIC50 = 12 x 7450N	50p	UIC86 = 5 x 7486N	50p
UIC04 = 12 x 7404N	50p	UIC51 = 12 x 7451N	50p	UIC90 = 5 x 7490N	50p
UIC05 = 12 x 7405N	50p	UIC53 = 12 x 7453N	50p	UIC91 = 5 x 7491N	50p
UIC10 = 12 x 7410N	50p	UIC54 = 12 x 7454N	50p	UIC92 = 5 x 7492N	50p
UIC13 = 8 x 7413N	50p	UIC60 = 12 x 7460N	50p	UIC93 = 5 x 7493N	50p
UIC20 = 12 x 7420N	50p	UIC70 = 8 x 7470N	50p	UIC94 = 5 x 7494N	50p
UIC40 = 12 x 7440N	50p	UIC72 = 8 x 7472N	50p	UIC95 = 5 x 7495N	50p
UIC41 = 5 x 7441AN	50p	UIC73 = 8 x 7473N	50p	UIC96 = 5 x 7496N	50p
UIC42 = 5 x 7442N	50p	UIC74 = 8 x 7474N	50p	UIC121 = 5 x 74121N	50p
UIC43 = 5 x 7443N	50p	UIC75 = 8 x 7475N	50p	UICX1 = 25 x Ass'd	£1.50
UIC44 = 5 x 7444N	50p	UIC76 = 8 x 7476N	50p		
UIC45 = 5 x 7445N	50p	UIC80 = 5 x 7480N	50p		

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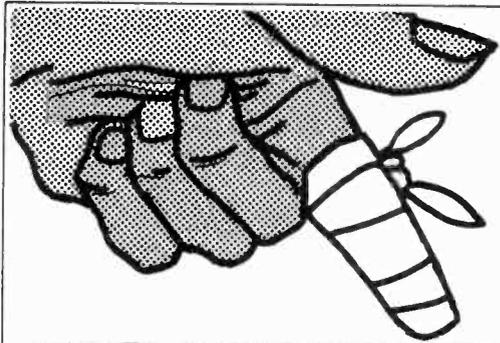


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ARMSTRONG 525	90-14	67-75
ARMSTRONG 526	102-72	77-50
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TELETON CR55	125-26	68-50
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GARRARD 401	39-04	25-95
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CELESTION Ditton 15	37-40	26-45
CELESTION Ditton 25	65-00	44-95
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AKAI CR80T Tuner/amp with 8-track recorder. McDONALD MP60 turntable including plinth, cover and G800 cartridge fully wired. 2 Wharfedale Linton MKII speakers	230-85	144-50
GARRARD AP76 with base cover and Shure M55E cartridge. Arena 2600 AM/FM and SW Tuner/Amp and 2 Goodmans Havant speakers	214-95	138-15
GOODMANS Module 80 Tuner/Amplifier, Garrard AP76 Turntable with Goldring G800 Cartridge and 2 Goodmans Havant Speakers	192-97	135-85
LEAK Delta 30 amp in teak case, 15 watts RMS per channel. Garrard AP76 transcription deck with plinth, cover and G800 magnetic cartridge, fully wired. 2 Ditton 15 speakers	189-36	129-60
PHILIPS RH 802 Stereo Tuner/Amp./player. 2 x 15 watts LW/MW1/MW2/SW/FM. GP400 magnetic cartridge, speakers extra	155-00	118-95
PHILIPS RH 811 Stereo, Stereo Tuner/Amp./Cassette recorder. Complete with 2 RH411L/S.	117-00	88-95
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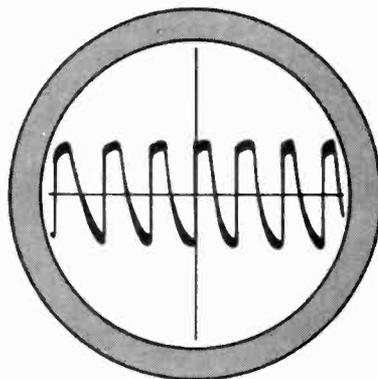
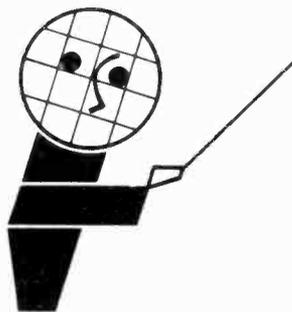
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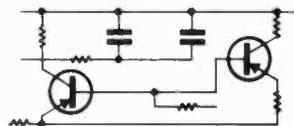
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PRACTICAL WIRELESS

VOL 48 NO 5

Issue 787

SEPTEMBER 1972

Anyone for Going Back?

ON looking at our front cover this month, readers may be forgiven for thinking that due to shortage of material we are having to ransack the archives! We hope the following words of explanation will dispel any such unworthy and infamous notions.

First of all, the response to our *Going Back* feature is large enough to indicate a real interest in the adolescence of electronics. Perhaps some people are becoming blasé about modern technological progress; perhaps the erstwhile mystery and romance has fled the scene; perhaps the pioneer days are now sufficiently remote in time to give an aura of the unknown; perhaps—but why go on?

Secondly, wireless, radio, electronics (call it what you will) is in danger of becoming taken far too seriously by the amateur, when it should be a relaxation. It *should* be fun.

We recently visited the Southampton plant of Mullard and saw how the integrated circuit designer, having determined the basic performance requirements and circuit elements, then enlists the aid of a computer with disc stores and a graphics unit. He can simulate circuits on the computer and obtain a readout of predicted performance.

Having found the optimum circuit elements, he then calls on the computer to provide cost and performance comparisons using different technologies of manufacture. The computer then takes the designer's rough IC layout and feeds in his information, using a special 'language' calls out transistor types from the computer memory store. The drawing for the mask is then generated by the computer.

To check that the circuit is correct, the engineer feeds his circuit programme into the computer, which examines the circuit and its geometry. The engineer then asks the computer to generate a control tape to reproduce the circuit on a photographically-treated glass plate reticle ten times up on final circuit size.

As a parallel operation, the computer examines the logic design of the circuit and is programmed to determine which test procedures and stimuli are wanted for the computer-testing of the complete circuit. Chips incorporating up to 6,000 transistors and all their interconnections can be designed without making a single error.

For those who boggle at such marvels, we thought it would be therapeutic to dip into the past and publish something from the days when wireless was young and unabashed. Hence the 'reproduction' crystal set. It should even please the transistor men who have been lambasting the valve lovers—after all, it *is* solidstate!

W. N. STEVENS—*Editor*

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**THE OCTOBER ISSUE WILL BE
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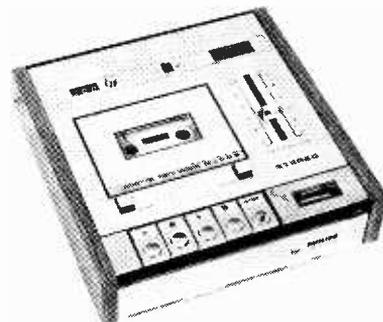
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NEWS...

NEWS...

NEWS...

Philips Audio



Philips announce the RH811, a tuner/amplifier/cassette recorder with built-in DNL—the first to include this feature.

The amplifier is rated at 2×10 watts (music) into 4 ohms, with a signal to noise ratio of better than 50dB. Inputs are provided for gram, microphone and external recorder. The tuner in-

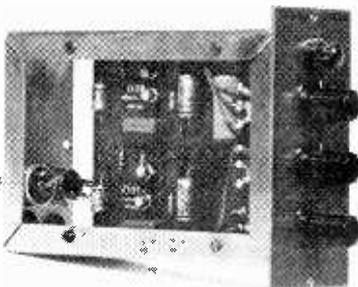
cludes long, two medium, short and f.m. wavebands. Decoder and stereo signal lamp are built-in as is a.f.c. Wavebands are selected by recessed push buttons located beneath the fascia. Stations are selected through a large diameter control to the right of the fascia.

Push buttons on the top of the cabinet control the stereo cassette recorder which is linked internally for trouble-free direct recording in stereo or mono. The cassette unit incorporates automatic recording level, pause con-

trol, cassette eject control and 3 digit counter. The RH811 is finished in walnut and matt chrome and will be supplied with matching RH411 speakers. Retail price is £125.

Also announced is the N2506: a sophisticated high specification mains stereo cassette deck with built in Dynamic Noise Limiter. The DNL is Philips special electronic circuit for reducing the hiss content of a signal—especially noticeable in soft passages of music. The DNL facility is switchable. Recommended retail price £60.

Audio Modules



A new middle of the road range of audio preamplifier and mixer modules have been produced by Partridge Electronics, who until recently specialised in the manufacture of audio mixers to customers own individual requirements. They have now produced a range of units to provide a flexible and economical method of constructing small or large mixers. The majority of these are available in kit form, or fully assembled and tested. Most items use a standard panel of 16

gauge anodised aluminium, with black lettering, size 50×150m/m. A free fourteen page catalogue is available on receipt of 5p for posting and packing, on application to *Partridge Electronics, 21/25 Hart Road, Benfleet, Essex.*

Figure it out

West Hyde Developments Limited introduce a new, small 7×9½×3¼in. 3½lb. calculator which multiplies and divides. The arithmetic can be mixed, i.e. 2+6-3×5-6÷2+4·5=14. The decimal place can be set with 0 to 7 digits



to the right and the machine automatically clears after the equals sign is pressed. Price is £99 for 1 off dropping to 2 at £89 and £75 for 10 off.

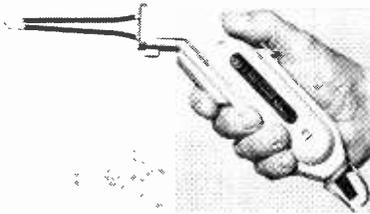
Features include 16 digits and a constant factor, 6 months guarantee, Pandicon display tubes (Mullard), 6 LSI chips, 1 I.C., Plug in printed circuit board, Plug in keyboard (gold plated connectors), Tobicons available on sale or return, *West Hyde Developments Ltd., Ryefield Crescent, Northwood Hills, Middlesex, HA6 1NN.*

Tape Q and A

The second edition of Heinz Ritter's 120-page book, "Tape Questions & Tape Answers" is now available from the Audio/Video Tapes Division of BASF UK Ltd.

The book contains useful hints and tips on all aspects of tape recording and costs only 40p.

P.O. Box 473, Knightsbridge House, 197 Knightbridge, London, S.W.7.



Amtron kits

Amtron, the Italian electronics company recently sent us some samples of their range of construction kits. As yet, the company have not appointed a sole agent and all enquiries should be made to *Box 102, Advertisement Dept., Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD.*

The kits are packed in "bubble packs" and contain all the components right down to the last nut and bolt and in many cases a printed circuit board.

The Twilight Switch (shown) circuit contains a photo-electric cell, two transistors, two diodes and can switch up to 1kW using a relay. The unit is activated by a wide range of light intensities and the action is reversible. It can be set to operate at pre-determined light intensities as light falls or increases, making it ideal for switching on a household light at dusk when the owners are out or away on holiday.

Power source is 220-240V a.c.

The other unit illustrated is a 27MHz Radio Control Receiver, designated UK 345. This is a superhet employing four high-gain, low-noise transistors and one detector diode. The oscillator is crystal controlled. Supply voltage is 6V and current consumption 5mA.

Primaxa gun

S. Kempner Ltd. announce their Primax and Primaxa soldering guns. Full heating is obtained six seconds after the "on" switch is depressed and twin spotlights mounted in the gun enable the user to get "a bit of light on the subject". The special alloy tip never needs retinning and the unit is guaranteed for 12 months (except tips and bulbs). Replacement tips are available for different soldering jobs and two models of gun are available: the 60W model which retails at £5.40 and the 100W model priced at £7. Postage and packing on each solder gun is 25p. Further details and soldering guns are available from *S. Kempner Limited, 421 High Road, London, N.12. Tel. 01-346 6222.*

Zeta windings

Zeta Windings Ltd. inform us that they can undertake to manufacture and design iron/ferrite cored transformers for any application that constructors may require for the development of their circuitry. They will also make them for P.W. projects and they are available by type number via: *Tidman Mail Order, 236 Sandycombe Road, Richmond; H. L. Smith, 287 Edgware Road, London, W.2 or (callers only) Zeta Windings Ltd., 26 All Saints Road, London, W.11.*

Other services provided by Zeta Windings are their rewinding of one-off prototype facilities on all kinds of transformers, and their rewind and prototype service which takes about 3 to 5 days.

The "voice"

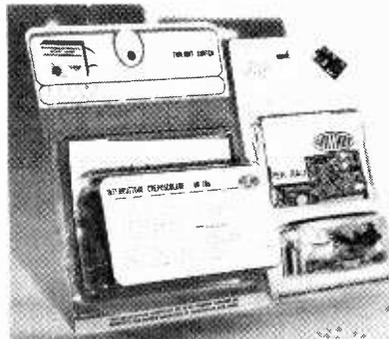
In a recent experiment, Bell Laboratories and the Western Electric Company gave a computer a "voice" so it could speak instructions helpful to production-line workers assembling complex communications equipment.

Previously, computers had been used to calculate efficient wiring instructions, and to print them in typewritten form. To get the instructions into a spoken form—so the assembler need not divert eyes or hands from the job—they were read aloud by a human announcer, and recorded, checked and corrected by technicians. Frequent changes in the complex wire lists meant frequent re-recording and re-checking.

In the recent experiment, the human steps were bypassed, and the computer made to "speak" the wiring instructions directly to an automatic recorder, which were then tested on the production line by an assembler of telephone crossbar switching equipment.

"Black ... three ... thirty-one A ... terminal strip ... four A ... valve socket," the recording said, to "tell" the assembler information about wire colour, length, and connection points. Using a cassette tape player with a foot pedal for control, she could start or stop the recorded voice during any of 58 steps involved. Assembly of each crossbar unit takes about 15 minutes.

Bell Labs engineers have been doing research on computer-generated "speech" because this is one way to make the computer respond in human terms.



Amtron Kits





Next November the British Broadcasting Corporation will be commemorating the first broadcasts, made in 1922, by the original British Broadcasting Company. We thought that readers might be interested in listening to these 50th anniversary programmes on a reproduction crystal set, typical of receivers in use in those early days.

Reproduction

crystal set

R.F. GRAHAM

IN the early days of radio crystal sets were used in many homes, and this project is a reproduction of such a receiver. Variable capacitors were available for tuning, but their cost often resulted in some other means of tuning such as tapped coils, coils with sliding contacts bearing on the turns and swinging coils where mutual coupling (and hence the inductance and resonant frequency) could be adjusted.

In addition to the headphones, such receivers required only a few components such as terminals, a detector crystal and "cat's whisker", wire to wind the coils, an insulated board or panel and a few small parts such as bolts and brackets to make a detector assembly.

The receiver shown here is something of a novelty, and sure to arouse interest when it is seen.

COILS

These are a flat type quite popular in the early days, and wound with 26 s.w.g. cotton-covered wire. Actually, any silk covered or enamelled wire, from 30 s.w.g. to 24 s.w.g., is suitable. If heavier wire is used then larger discs will be required.

Each disc is about 4in. in diameter, and can be stout cardboard or thin paxolin sheet. Seven slots, each about 1/8in. wide, are cut about 1in. deep.

Pass the wire through two small holes, and wind in and out of each slot in turn, as winding progresses. This results in half the turns lying on one face of the disc, and half on the other face, crossing over in the slots. Each coil has about 40 turns, the wire being finally anchored through two small holes, leaving the ends long enough to reach to the terminals.

With such a circuit, the parallel capacitance is mainly due to that of the aerial and earth. As a matter of interest, "tuning" coverage was tested with a signal generator, and was 1300-1700kHz with a 25pF aerial/earth system, 850-1100kHz with 100pF,

and 550-750kHz with the aerial/earth placing about 250pF across the receiver.

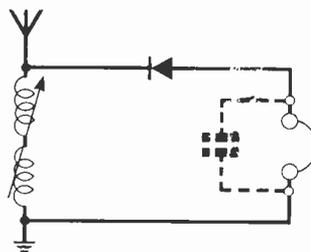
With such a receiver it was quite usual to adjust the number of turns to suit the aerial, or wavelength of local stations.

One coil is fixed on a small bracket. The other is bolted to a strip of material about 1in. long, secured to a threaded rod by lock-nuts. The rod runs in two brackets, and is rotated by a large terminal head or small knob. "Tuning" is accomplished by swinging one coil over the other thus varying the effective inductance.

The base is varnished plywood or ebonite or paxolin about 6×6in. Strips raise it about 3/4in. to clear the terminals projecting underneath.

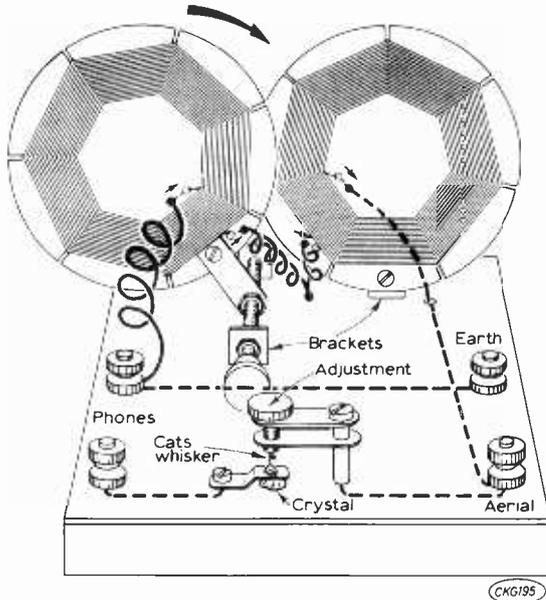
DETECTOR

A strip of brass about 1×3/8in. (from an old lamp battery) is bolted to hold the crystal firmly, a corner or point on the latter projecting up through a hole in the strip.



It could hardly be more simple! The suggested additional 'condenser' shown dotted can be about 1000pF. It will be cheaper to buy it rather than to follow the method described in the text for making a 'condenser'!

A 1½in. bolt with spacers holds a similar strip about 1¼in. long to which the catswhisker is soldered. Above this strip is a stouter strip of metal, and a screw or terminal head runs through a threaded hole in this, or through a nut soldered to it. Turning this screw or terminal adjusts pressure of the catswhisker on the crystal.



This drawing, showing the constructional details of the crystal set, should not be difficult to follow.

The catswhisker is made by winding about 1½in. of copper, tinned-copper or brass wire, about 34 s.w.g., on a small drill about ¼in. diameter, and then stretching the winding slightly. These bygone detectors used wonderful combinations of crystals and even gold-tipped whiskers, all of which appeared to give about the same result. There is great room for experiment here, using various kinds of wire, or soldering the crystal (use Woods metal) or packing it with metal foil. All these trials will probably give a detector of about equal efficiency to that shown, which is about the same as a modern crystal-diode, when a sensitive spot on the crystal has been found.

AERIAL AND EARTH

The aerial ought to be at least 25ft long, and preferably over 50ft. Maximum range is usually considered to be about 25 to 150 miles from a major transmitter, anything over about 50 miles generally needing some 50-100ft or so of outside aerial, 20ft or more high.

The earth lead runs to a metal spike or other earth rod in damp soil. With a 180ft aerial ample volume was obtained by the author some 25 miles from a transmitter. No earth was used but the earth is usually desirable.

The headphones ought to be good-quality, sensitive headsets of about 500Ω to 2,000Ω resistance, so as to give best volume with the rather limited output of the crystal set. Strictly speaking, a capacitor of about 1,000pF should be connected across the headphones but it was not always fitted in the early days. A description of how to make such a "telephone condenser" appeared in "Amateur Wireless" in 1922.

"The telephone condenser is made up of twenty-five small sheets of tinfoil measuring 1½in. by ¾in. with a small strip left at one corner to make a lug. It is built up by placing the strips of tinfoil, with strips of waxed paper in between, with the lugs alternately at one end and then at the other. When the condenser has been built up the ends of the tinfoil should be carefully soldered together by means of a blob of solder, two pieces of cardboard being placed either side of the condenser and a length of linen tape wound round to keep the whole together. The condenser should then be immersed in molten paraffin and allowed to set in a solid block."

The "components list" is short and sweet! One galena crystal (ref. X6), four 4BA brass terminals, 2oz. reel of 26 s.w.g. enamelled wire and a length of 4BA brass studding, all of which are obtainable from Home Radio (Mitcham) as a "kit" for 96p which includes post and packing. ■

TELEVISION

SEPTEMBER ISSUE

SIMPLE CROSSHATCH AND DOT GENERATOR

Constructional details for this essential item of colour TV servicing equipment. The instrument is cheap enough to be of interest to enthusiasts for do-it-yourself convergence adjustments. Notable features of the new design are: a choice of four patterns; miniature size made possible by the use of TTL MSI integrated circuits; sync amplifier for stability; suitability for use with any 625-line set with only two easy connections.

TV NOISE FIGURES

Noise factor, signal-to-noise ratio, front-end noise, aerial noise, valve and transistor noise—are you sure of yourself in this important area? If not read Gordon J. King's clear presentation of the subject this month. The usable sensitivity of a television receiver is dictated by its noise performance so this is a subject of practical importance—especially for fringe area reception. The article shows how a decision can be made on the type of aerial required and the improvement that can be expected by using an aerial preamplifier.

COLOUR RECEIVER

This month the timebase board—complete sync, field timebase and line oscillator circuits plus the line output stage with the exception of the line output transformer assembly. With board layout.

SERVICE NOTEBOOK

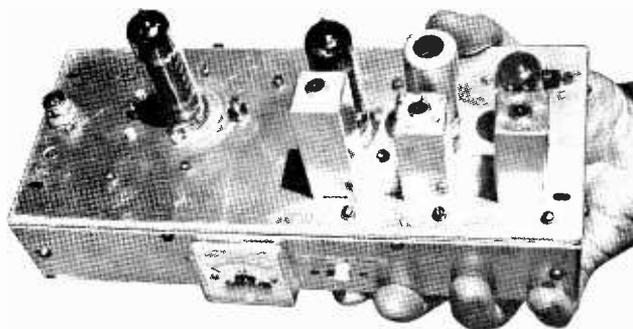
More items from G. R. Wilding's day-to-day experiences of TV fault conditions.

PLUS ALL THE REGULAR FEATURES

ON SALE AUGUST 21

TRANSMITTER for 2 metres

PART 1 F. G. RAYER G3OGR



There is quite a lot of interest in 144MHz equipment, especially among the Amateur Class B licencees who are permitted to transmit on 144MHz and above. Apart from this, some of the advantages of the use of this band may be noted. There is considerable frequency space, the 2-metre band being 2MHz wide, from 144 to 146MHz. A large space for an aerial is not necessary, aerials for 144MHz usually being single-mast affairs resembling those used for TV purposes. Many stations use low power, in the 10 to 15 watt region, and crystal control of the transmitter is quite usual, which makes the equipment relatively simple to build and operate. There is also a very good chance of clear, solid QSO's, free of all the interference that makes 160m or 80m so uncomfortable.

The transmitter described here runs about 10 watts input, so it can be run from a power supply and modulator such as may already be in use on a 160m transmitter. If the inductors are made and adjusted as described, it will be found virtually impossible to make the transmitter operate outside the permitted band.

CIRCUIT

Fig. 1 shows the complete transmitter circuit which uses four valves. Operation of the various stages will probably be more clearly understood if they are dealt with separately.

V1 Oscillator. This is a simple crystal oscillator using a 6C4 in which L1 is tuned to the same frequency as the crystal, approximately 8MHz, and V1 cannot be made to work on any other frequency. The test point TP1 allows the grid current of V2, produced by grid rectification of r.f. from V1, to be measured, to facilitate the initial tuning of L1.

V2 Tripler. The 6BH6 receives input at 8MHz, and triples this to 24MHz, to which L2 is tuned. Point TP2 allows a meter to indicate grid current of the following stage, as an aid to the initial tuning of L2. The wrong multiple, if selected by L2, would be 16MHz or 32MHz, and these frequencies, which would result in incorrect operation cannot be tuned by L2.

V3 Tripler-Driver. This is a double beam tetrode QQV03-10. The first section receives drive at 24MHz and triples to 72MHz, to which frequency L3 and L4 are tuned. Grid current of the following section of this valve can be monitored at TP3. L3/L4 cannot be tuned to a wrong harmonic.

The second half of V3 receives drive at 72MHz from L4, and doubles to 144MHz, to which L5 is tuned. Trimmer TC1 aids in balancing the centre-tapped circuit L5.

V4 Power Amplifier. L6 is tuned to 144MHz and grid current of the QQV03-10 develops about 30-60V bias across R14. The switch S1a/b allows grid current

to be monitored, which is essential. For grid current indications, the 5mA meter reads directly.

Cathode current for V4 flows through R19. With the meter switch in the second position, R20 is in series, and the meter reads 0.0-5V, which corresponds to a full-scale deflection of 50mA, so that the cathode current of V4 can be measured.

A separate h.t. connection is provided for V4, so that modulation can be applied for speech transmission. This type of valve does not need neutralising although acting as a straight-through 144MHz amplifier. L7 is tuned to 144MHz, and output is from the link coupling L8, TC2 allowing adjustment of loading. The transmitter will work directly into a co-axial feeder to a dipole or similar aerial.

With a 280V supply for the early stages, it was found quite easy to obtain more grid drive than was required. Running the p.a. with about 10 watts d.c. input will light a 6 watt lamp used as a dummy load very well, so a good level of efficiency is obtained.

INDUCTORS

L1 and L2 are wound on $1\frac{7}{8} \times \frac{1}{4}$ in. dia. formers and L3 and L4 on a single $2\frac{3}{8} \times \frac{1}{4}$ in. dia. former. The formers fit in $\frac{3}{4}$ in. square screening cans and are mounted by 6BA bolts which pass through lugs on the cans and into tapped holes provided on the square bases of the formers. Fig. 2 shows winding details. To make L1, bare and solder 32 s.w.g. enamelled wire in the tag used for h.t. Leave $\frac{1}{2}$ in. clear space, then wind on 50 turns close wound. Secure the ends with polystyrene cement or similar adhesive, clean the wire end and solder it in the A (anode) tag. The wire ends should slope down clear of the windings, and clear of the screening can.

If surplus or other formers or cans are used, these need to be long enough to avoid having the windings near the chassis or top of the can. It might also be necessary to make sure that the cores of surplus coils are suitable for the frequencies involved.

L2 is wound in the same way, and has 15 turns of 24 s.w.g. enamelled wire, close wound.

L3 and L4 each have $5\frac{3}{4}$ turns of 24 s.w.g. enamelled wire, close wound. A gap of $\frac{1}{8}$ in. is left between the two coils. Begin winding at G, Fig. 2, and finish this coil at the bias circuit lead, R11. Then begin L3 at the h.t. positive end, continuing to wind in the same direction as for L4, and terminate this at end A (anode). The long former listed has soldering eyelets, and the wire ends pass down through these and soldered but not cut off. The leads emerge as in Fig. 5. They are cleaned and left long enough to reach the required points. To avoid possible short circuits pieces of sleeving are put on the pins of L1 and L2, and the wire ends of L3 and L4. For easy identification, the wire ends of the latter can

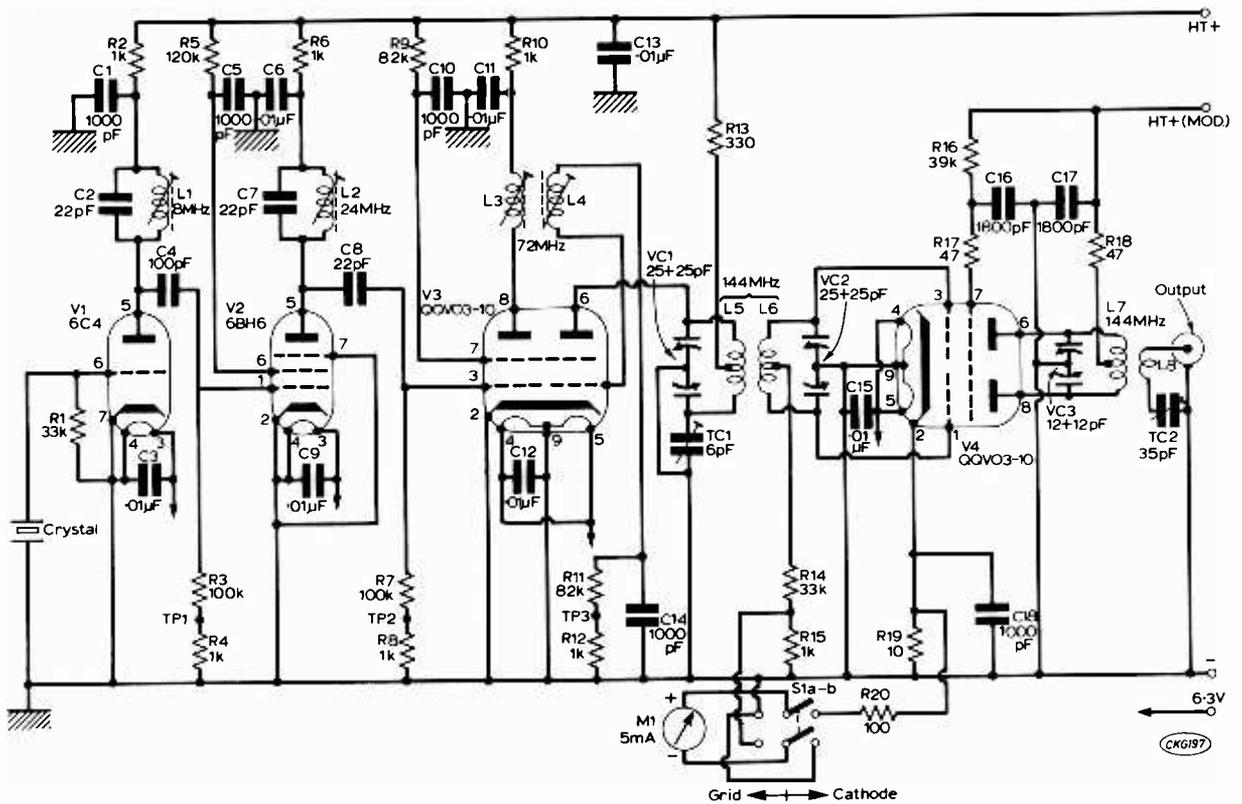


Fig. 1: Circuit of the 2-metre transmitter which uses 8MHz range crystals in the oscillator stage.

have coloured sleeving, as follows: Black—grid; Green—bias resistor; Red—h.t.; Yellow—anode.

Place each former in its can with the threaded holes matching the lugs, which are bent over. To prevent the cores moving, a piece of a thin elastic band can be put into each former, before screwing in the core.

The windings for L3 and L4 may be tuned to resonance with the cores only using stray circuit capacitances. If cores are employed, the core material must be good for 72MHz.

The 144MHz inductors are shown in Fig. 3. L5 and L6 are wound with 18 s.w.g. wire, and L7 with 16 s.w.g. wire. Sleeving should be put on the wire for L5 before winding to prevent possible contact with L6.

L5 has five turns wound on a suitable object, such as a pencil, so that its outside diameter is 0.4in. and turns are spaced to occupy 0.6in.

L6 has six turns, 0.3in. outside diameter, and is 0.7in. long. L7 is four turns, spaced to occupy 0.5in., and its outside diameter is 0.6in. L5 has a centre tap soldered on the top of the central turn, while L6 and L7 have taps on the bottom of the centre turn. The loop L8 is a single turn of 16 s.w.g. or similar wire, placed in sleeving, and with ends shaped to reach the coaxial socket and loading capacitor.

CHASSIS ASSEMBLY

The chassis and screen across V4 valveholder consists of six "universal chassis" flanged members. The top, 10x4in., is prepared for the valveholders etc. as in Fig. 4. The screened coils need four holes to clear the pins, two holes for 6BA bolts, and a central hole under L3/L4 to reach the bottom core.

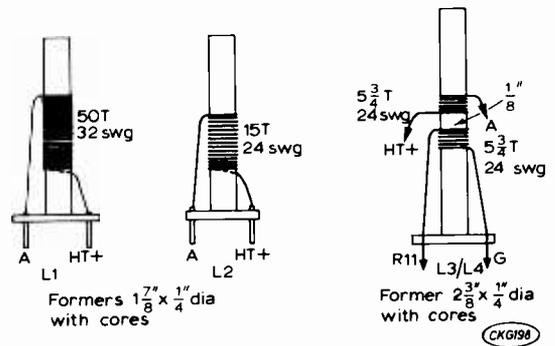


Fig. 2: Winding details of the coils for the oscillator and multiplier stages.

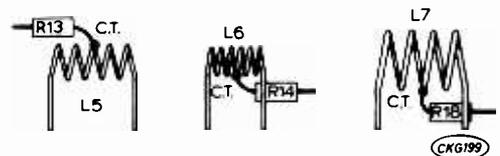


Fig. 3: Construction of the coils for the power amplifier. Put sleeving on L5 before winding.

A 4x2in. member is bolted inside each end flange of the top. The third 4x2in. member is cut so that it can be placed across the holder for V4 as in Fig. 5, clearing tags 4 and 5 (heater). It is bolted to the top at the valveholder.

The 10x2in. front member has the top flange cut off, and takes the meter and 2-way switch in the positions shown in Fig. 5. It is bolted to the chassis

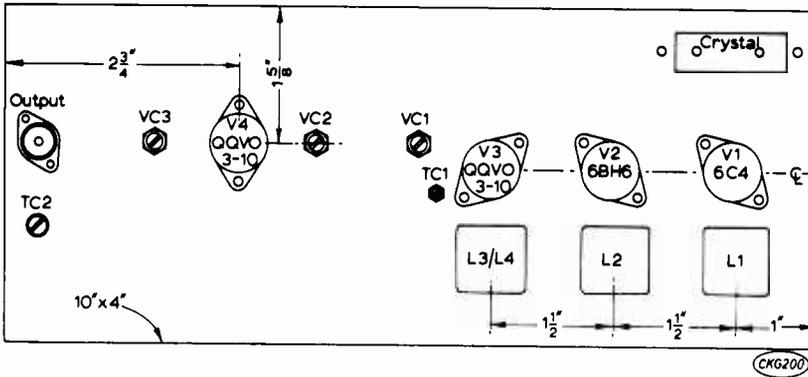


Fig. 4: Marking-out details on top of the chassis. Holes for the single tag stand-offs can be drilled as construction proceeds.

top, both ends, and the screen. The back is fitted in the same way.

It is best to prepare the front and back but leave them off until most of the wiring is completed.

WIRING

Fig. 5 shows wiring and other details. All by-pass capacitors, and particularly C10 to C19, should be connected from the various tags to adjacent chassis tags with the shortest possible leads. Resistors R13, R14 and R18 are soldered with very short leads from resistors to centre-taps, and R17 is wired directly to pin 7 of V4.

Capacitors VC1, VC2, VC3 and TC2 may be fixed by the spindle bushes, or by bolts. In either case the rotors are grounded by stout leads to near-by chassis tags. All r.f. leads in the 144MHz circuits must be stout and no longer than necessary.

Single tag stand-offs were used to provide anchor points for R2, R6, R10, etc., and also for the grid current test points TP1, TP2 and TP3.

A 4-way tag strip is bolted as shown, for flexible supply leads or a 4-way cord. This provides 6.3V, chassis or common return, h.t. positive, and modulated h.t. connections to the power supply and modulator.

CIRCUIT ADJUSTMENTS

When an indication of grid current has been obtained on the meter this can be used for all tuning adjustments. However, it is not very likely that this indication will be obtained immediately, so it is generally necessary to adjust the stages one at a time, as described below.

A 6.3V 2A supply is necessary for the heaters. A 250-300V supply at about 60mA is required for the h.t. for V1, V2 and V3, actual current depending on the voltage and adjustments. Temporarily leave h.t. to V4 (Mod.) disconnected.

Crystal. Multiplication is $3 \times 3 \times 2$, or 18 times. Crystals in the region of 8MHz are thus necessary. To

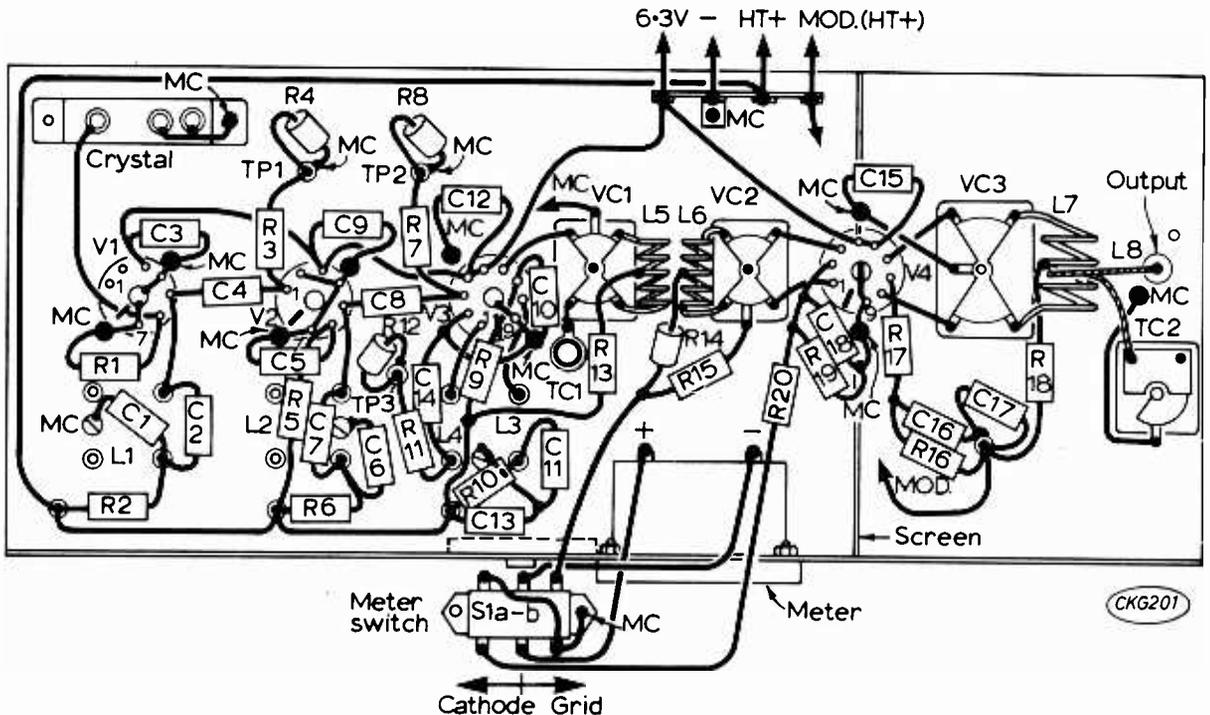


Fig. 5: Wiring underneath the chassis. Stand-off insulators are used for the test points TP1, 2, 3 and to support resistors R2, 6 and 10.

★ components list

Resistors

R1 33kΩ ½W	R8 1kΩ ½W	R15 1kΩ ½W
R2 1kΩ ½W	R9 82kΩ ½W	R16 39kΩ 1W
R3 100kΩ ½W	R10 1kΩ ½W	R17 47Ω ½W
R4 1kΩ ½W	R11 82kΩ ½W	R18 47Ω ½W
R5 120kΩ ½W	R12 1kΩ ½W	R19 10Ω ½W
R6 1kΩ ½W	R13 330Ω ½W	R20 100Ω ½W
R7 100kΩ ½W	R14 33kΩ ½W	

Capacitors

C1 1000pF 350V disc	C10 1000pF 350V disc
C2 22pF SM	C11 0.01μF 350V disc
C3 0.01μF 12V disc	C12 0.01μF 12V disc
C4 100pF SM	C13 0.01μF 350V disc
C5 1000pF 350V disc	C14 1000pF 350V disc
C6 0.01μF 350V disc	C15 0.01μF 12V disc
C7 22pF SM	C16 1800pF 1kV disc
C8 22pF SM	C17 1800pF 1kV disc
C9 0.01μF 12V disc	C18 2000pF 350V disc

VC1-VC2 25+25pF butterfly capacitor (Jackson type C713 (0.015" gap))

VC3 12+12pF butterfly capacitor (Jackson type C713 (0.045" gap))

TC1 6pF tubular trimmer (Home Radio VC88B)

TC2 35pF pre-set air spaced

Valves

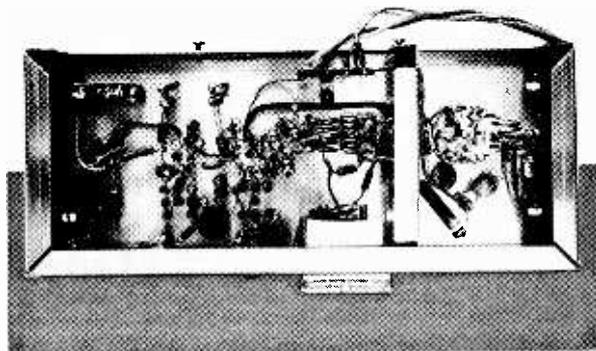
V1 6C4	V3 QQVO3-10
V2 6BH6	V4 QQVO3-10

Chassis

"Universal chassis" flanged members.
10 x 4in. type CU58A (1), 10 x 2in. type CU139 (2),
4 x 2in. type CU133 (3) (Home Radio)

Miscellaneous

M1, 5mA miniature panel meter. Valveholders B7G, skirted with screening cans (2) B9A (2). S1a-b, 2 pole 2 way slide switch. Crystal 8MHz (see text) and holder. Coil formers type CR14 (2), CR16 (1), screening cans CR15 (2), CR17 (1). Cores type CR19 (4) (Home Radio). Tag strip, stand-off insulators etc.



View underneath the chassis. The vertical screen isolates the input and output circuits of the p.a.

meter can be unclipped, and cores L1 to L4 can be touched up, as necessary.

Should a peak in grid current arise with VC2 fully open, slightly stretch L6, and re-adjust VC2. On the other hand, if VC2 is fully closed, press the turns of L6 a little closer together. This also applies to L5 and L7.

Unscrew TC1, and peak grid current with VC1. Slowly screw down TC1 meanwhile re-adjusting VC1 for best grid current. This will give a peak somewhere the middle setting of TC1, but is not critical.

Final grid current can be adjusted by varying the spacing between L5 and L6, and anything around about 1.5mA is suitable.

It is best to make the first output test into a lamp load. This can be a 12V 6W bulb, connected to a co-axial plug to connect to the output socket.

Open TC2 to minimum capacity and switch the meter to read cathode current. Provide about 300V or so at the "Mod" connection. Rotate VC3 for a dip in cathode current, which should cause the bulb to light. The meter can then be returned to "Grid" and VC2 readjusted (also possibly VC1).

LOADING

The loading of V4, and thus the final current drawn when VC3 is tuned to resonance, is adjusted by rotating TC2, and if necessary moving L8 in or out of the coil L7.

Maximum listed ratings for the QQVO3-10 are 300V for anode and 175V for the screen grid, with an anode current of 76mA (d.c. input 22W), 3mA grid current, resulting in an output of about 14W. The power supply and modulator used was more suitable for about 40mA at 280-290V or an input of about 12W. Screen-grid current is about 3mA, and the meter fitted shows the total cathode current, anode current alone being a little less. If the meter is to read 0-100mA, for larger inputs, R20 should be 200Ω.

The modulator should be able to furnish at least one half of the input to V4 in watts—say 5W for 10W input to V4. A 12AX7 followed by a single 6BW6, as a Class-A modulator (as used for a 160m transmitter) was found to work well with an input of up to about 10 watts to V4.

Next month we shall describe a power supply and modulator for use with this transmitter. It can also be used as a conventional audio amplifier or as a power supply for a higher powered transmitter.

find the output frequency with a given crystal, multiply the crystal frequency by 18. Alternatively, to obtain a crystal to operate on a particular frequency, divide the wanted frequency by 18.

Oscillator. A suitable tool to adjust the coil cores can be made by filing flats on the end of a plastic knitting needle. Clip a multi-range meter or other suitable instrument from tag TP1 to chassis. A 5mA or similar range is suitable. Or if a voltage range is used, 1V will indicate about 1mA, and so on.

Rotate the core of L1 for nearly maximum grid current at TP1. Do not tune L1 exactly for peak current, or it will be found that the crystal oscillator will not start, when switched on. This is usual with this type of oscillator.

Tripler V2. Transfer the meter to TP2 and adjust the core of L2 for best grid current.

Tripler-Driver V3. Transfer the negative meter lead to TP3 and rotate the cores of L3 and L4 for best grid current. These are quite critical, and interact to some extent.

Power Amplifier. S1a/S1b should be set to read grid current. Slowly rotate VC1 and VC2 for best grid current. When a reading is obtained, the test-

IC auto PARKING LIGHT

J. N. JONES

ALTHOUGH the regulations regarding the lighting of cars after dark have recently been relaxed, there are many areas and situations where parking lights are still required. If your car has to display lights regularly, it is a chore having to go out to turn them on—and there is always the risk of forgetting to do this.

For quite a small cost (only about £1.25), it is a simple matter to arrange for a parking light to come on automatically when the light level falls below a certain level and to switch itself off at daybreak. This obviously conserves the battery, especially during the winter (with the long nights), the time when the battery needs to be in peak condition. Such a device is especially useful when the car is used only occasionally.

THE CIRCUIT

The circuit shown in Fig. 1 is suitable for cars with either a negative or positive chassis with appropriate modifications. The circuit makes use of an LDR (light dependent resistor) and the type 741 operational amplifier IC. The latter is an extremely useful and well protected differential amplifier which is available for as little as 34p—low enough to promote serious consideration in simple circuits such as this. The main features of the circuit are the low cost, already mentioned, and the low current drain in the standby position; in daylight the current drain is only about 2.5mA.

The positive earth circuit functions as follows: R3 and R4 fix the non-inverting input of the IC to a potential of about -6V. This is slightly modified by the positive feedback action of R5, but only by a fraction of a volt. VR1 is set so that at lighting-up time the potential of the inverting input, going negative with falling light levels, is just passing through -6V. This causes the inverting input to become negative with respect to the non-inverting input, which in turn causes the output potential to change from about -10V to about -2V. The values of R6 and R7 are selected so that when the output

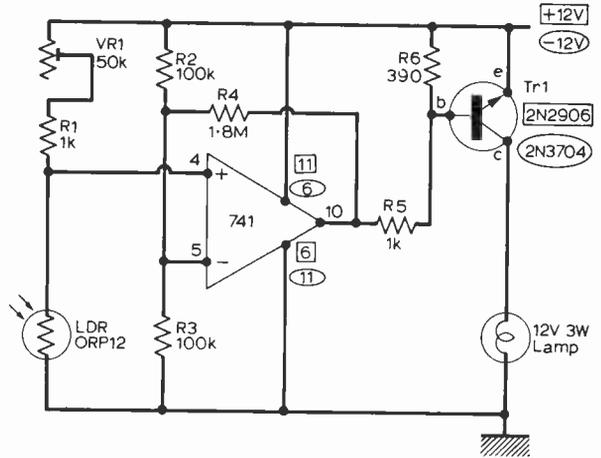


Fig. 1: The circuit for both positive and negative chassis cars. Where there is a variation, +ve details are in a squared box, -ve details in an oblong box.

changes over this range, the transistor is switched from completely off to fully on, causing the bulb in the collector to light.

The purpose of the positive feedback action of R5 is to prevent possible oscillation and to ensure that the switching action is fast enough to prevent destruction of the transistor which can only handle the current in fully on or fully off states.

The negative earth circuit functions in exactly the same way but the transistor type needs to be changed and the voltages reversed.

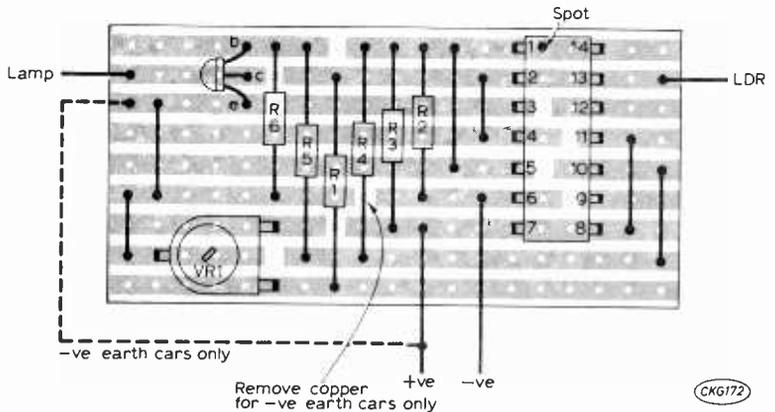


Fig. 2: Component layout on Veroboard. Note that for negative chassis cars R2 and R3 reverse notation but, as they are of the same value, no circuit changes are necessary.

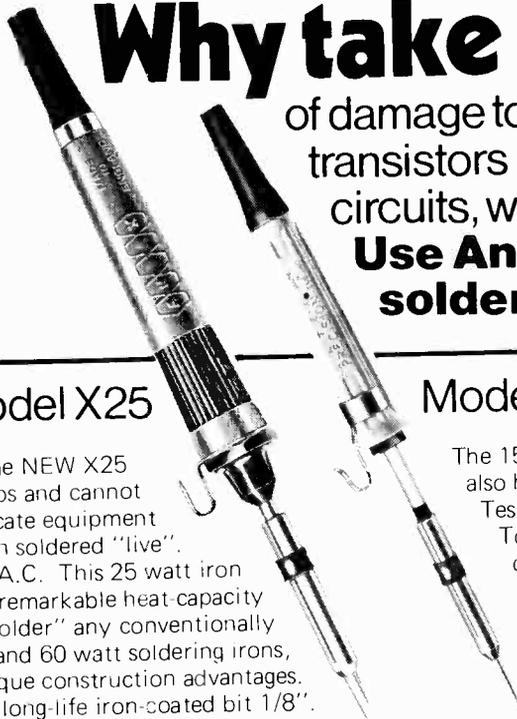
CONSTRUCTION

A suggested layout on Veroboard is given in Fig. 2, with the changes from one chassis potential to another given. This circuit can be mounted anywhere in the car but the LDR has obviously got to face through the window. It should not face the parking light; if it does the unit will "oscillate" as the circuit cannot differentiate between the light it is meant to switch on and daylight!

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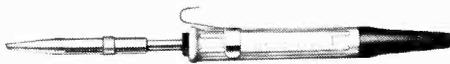
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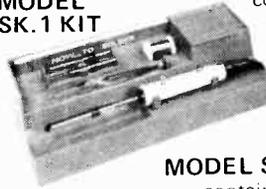


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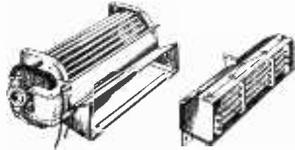
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3B4	26	30F5	64	EB41	54	EM87	50	PCL84	34	UBC4	45
3V4	47	30FL1	65	EB81	30	EY61	38	PCL85	38	UBF80	34
5U4G	31	30FL2	69	EB90	22	EY86	29	PCL86	38	UBF89	32
8V4G	35	30FL14	68	EBF80	32	EY87	29	PCL88	65	UCC84	32
9Y3GT	34	30L1	29	EBF83	39	EZ40	43	PCL800	75	UCC85	35
5Z4G	35	30L15	57	EBF89	29	EZ41	43	PCL805	38	UCF80	38
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A good turn

With reference to the insertion in your CQ? Column June '72 you will be very pleased to know I have received a copy of the book I was looking for, "Simple Radio Circuits."

The reader who sent me this is in search of some detail concerning "Modification details of any ex-military receiver" if you could help him in this matter through your column I shall be very grateful.

The name of the writer whose request I mention is Alan Salisbury, 28 Dyke Street, Brymbo, Wrexham, N. Wales LL11-5 AH.—**J. Wheelton (Staffs)**.

Greek notes

With reference to W. D. Logan's letter in the May editorial; I wouldn't try to disappoint him, since I am too a vintage radio enthusiast and collector but I think that the early days of Radio-telegraphy were not so romantic and sentimental as he often dreams.

Until high frequency communications were developed, signals were pushed long distances by brute force. To generate the necessary power, great sparks buzzed, molten arcs sizzled, and mechanical alternators revved up madly to as high as 20,000 r.p.m. their rotators yearning to fly apart.

To make these rock-crushers work, an early operator had to be electrician, steeple jack, rigger, mechanic and oiler.

To turn on some arc transmitters he also had to be something of an acrobat. Trouble was when the arc chamber was filled with hydrocarbon gas—if there also was the right amount of air in the chamber, the gas blew up and the carbon was fired back to the operator.

Because receivers had little or no amplification, the operator had to develop sensitive hearing. According to the expression, a man had to crawl into the headphones in order to copy weak signals!

Stations ordinarily were hundreds of miles apart and sending had to be slow. A distant spark

signal, for example, sounded like a gnat sighing through a screen and the burbly signal of a far away transmitter might be weaker than the noise, the methodically taped dihs and dahs audible only through holes in the static.

So all important was an individual's adeptness that every operator struggled to avoid ending up with the trade's own brand of punch-drunkenness, a tin ear and a glass arm.—**Chris Petsikopoulos (44 Atlantos str. P. Faliron, Athens, Greece)**.

CQ! G. Saunders

While reading through the C.Q. section of June *Practical Wireless* I came across a book wanted by a Mr. George W. Saunders with no address given. Could you please ask him to write to me if he is still looking for this book. The book I have is "Mullard", Circuits for Audio Amplifiers; reprinted June, 1966. Please ask him to write to the address below for details.—**E8097840 SAC Lim Hangar 91, RAF Brize Norton, Oxford, OX8 3LX**.

Cassette decks

With reference to the letters of V. S. Watts and A. R. Knight, I have a source of Philips type cassette mechanisms in about three different models. They are expensive (nominally £25 each) and if Mr. Watts and Mr. Knight or any others contact me I will endeavour to help them.—**S. R. Beeching (Consortium Engineer) (Bishop Grosseteste College Lincoln)**.

Egg-shaped

I have just recently invested in a Henry's Radio catalogue, and I note that on page 274 it says at the bottom, "Note, deliveries of speakers, particularly elliptical tapes, can sometimes be difficult." Is this a new type of tape? and are these tapes supplied on elliptical reels?

I should be interested in your comments.—**F. G. Jennings (Sussex)**.

[This appears to be a type error! —Editor]

Bang!!

Although it is too late to enter for the competition for the most interesting find made by the PW Treasure Tracer Mk I, I thought you might be interested to know that I found a bomb in my garden recently. The police think it is some kind of mortar bomb which has been fired but has not exploded. When I think how roughly I handled it compared with the way that the three policemen handled it I nearly died of fright.

The bomb is made by ICI and is about 9 inches long and has corroded terribly. It was buried about 2 inches in the ground and just to think that I walked over it many times a day. Apart from the mortar bomb and tail fin I also found a spent cartridge about three feet away from it.

If I had dropped this long cylindrical bomb I dread to think what would have happened to me and my neighbour who was watching.—**N. Moyes, (Croydon, Surrey)**.

Equipment

Mrs. V. E. Whetstone has informed us that she has a large amount of radio and television equipment that belonged to her late husband. Items include Radio and Television Servicing volumes 1-8, numerous issues of *Practical Wireless* and *Television* dating back to the 1940s, loudspeakers, oscilloscopes, valves, tubes, transformers etc. and many items of test equipment including meters. There are many line output and e.h.t. transformers, resistors, capacitors, coils, valveholders and television i.f. panels. There is a sound measuring device together with time switches, turntable and many other items of useful equipment, including CME 2301 and CRM 172 television tubes to name but two.

If any readers are interested in making offers for any of these items (and Mrs. Whetstone has expressed a wish that she would like radio clubs to have some of the equipment) would they please phone 01-500-1513.

'Project Autumn'

presentation



Practical Wireless Designer's Trophy

1972

At a presentation luncheon in London recently John Thornton Lawrence was presented with the PW Designers Trophy for 1971 by Editor Norman Stevens. The winning article "A Digital Frequency Counter/Timer" was published in PW from September to December 1971 and was considered by a panel of judges to be the best entry in the PW "Project Autumn" competition.

John's interest in radio began at school. An apprenticeship in radio engineering at an electronics factory on the inspection side gave him a good insight into multiband short wave receivers. In 1947 he switched to the radio trade as the service manager for a company specialising in radio, sound systems, disc recording and TV. At home, he designed and built a 12in. TV set together with an oscilloscope and pulse generator to align the set before regular BBC transmissions started.

In 1953 he became GW3JGA operating mainly on Top Band and 2 metres, but in 1958 as GW3JGA/T made the first GW two way television contact, with GW3FDZ/T, at a distance of 18 miles. He was a founder member of the Flintshire Radio Society and was the RSGB's Region 11 representative for a period. In 1960 he joined the Electronic Engineering Department of the University College of North Wales where he now holds the post of Senior Scientific Officer, and incidentally, founded the UCNW Amateur Radio Society whose station GW3UCB is frequently heard in contests on all bands.

John's interest in amateur TV expanded and in 1962 he completed a sequential colour system and transmitted what are believed to be the first amateur colour TV pictures in this country. With later transistorised equipment he achieved a two way TV contact with the Isle of Man at a range of 79 miles. Among other qualifications John is a Fellow of the Society of Electronic and Radio Technicians and a member of the Royal Television Society.

The pay-off! JTL (left) gets his award from WNS.



To encourage new authors, entries for the 1972 Trophy will be restricted to readers who have not previously had an article published in PW. This leaves the field wide open for those wanting to try their hand at writing technical constructional articles. Contestants will not be in competition with well-known authors, only with other newcomers, so the cup can only be won by a new writer. **It Could Be You.**

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1. The winning entry will be chosen by a panel of judges from among articles published in issues of PW dated September 1972 to August 1973 inclusive. The Editor's decision on all matters arising will be final.
2. The winner of the competition will receive and retain outright the PW Designer's Trophy 1972. Other prizes will be awarded to the best runners-up. Articles will be paid for shortly after publication.
3. The competition is open only to authors who have not previously had any work published in PW.
4. Articles submitted for the competition should conform to the general style of material published in PW and must describe the operation and construction of a piece of radio, audio or test equipment that has been designed and built by the author.
5. Articles should, preferably, be typed using double spacing, leaving wide margins, on one side only of each sheet. Circuit diagrams and any other drawings must be separate and numbered to agree with the text. Author's roughs must be clear enough to permit re-drawing. Components list must also be separate and laid out to the standard PW format.
6. Photographs of the equipment are desirable and should be in black and white, sharp and clear. Photographs may be identified by sticking a label on the reverse instead of writing on the back of the photograph itself.
7. Components used in the design must be readily available from retail sources.
8. Articles should be sent to the Editor, Practical Wireless, Old Fleetway House, Farringdon Street, London, E.C.4. Authors will be advised as soon as possible of the acceptance or rejection of their articles. Equipment, the subject of an article, must not be sent to the Editor until advised to do so.
9. Employees and staff of PW are not eligible for entry to this competition.

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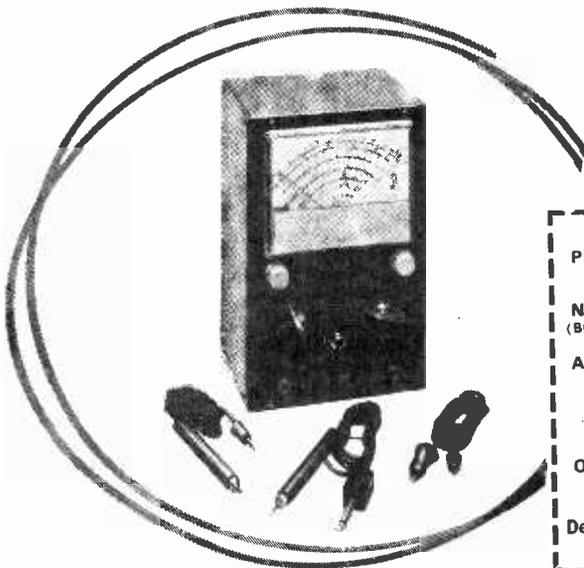
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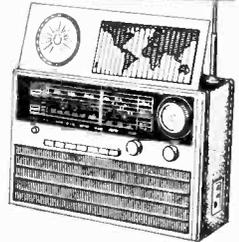
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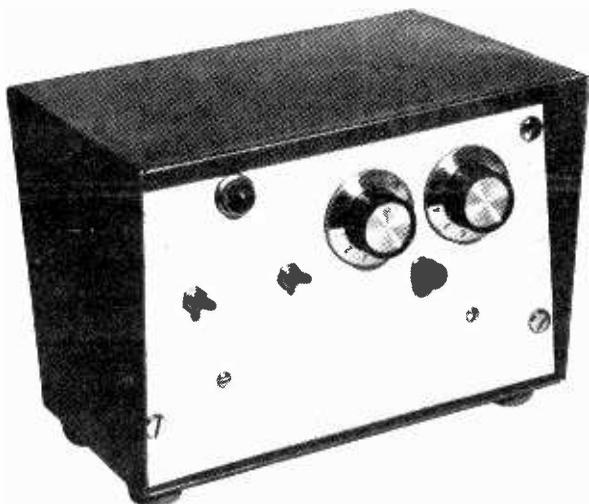
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EBF89	12p	PL36	20p	20P1	10p
ECC81	10p	PL81	17p	20D1	10p
ECC82	12p	PY81	8p	30P4	20p
ECC83	12p	PY33	17p	30F5	10p
ECL80	8p	PY82	8p	30P12	20p
EF91	4p	PL82	8p	30FL1	20p
EY86	20p	PL83	8p	6/30L2	20p
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Precision ENLARGER TIMER

R.A. BOTTOMLEY

Most electronic enlarger times utilize the principle that a capacitor, when connected to a supply voltage by way of a series resistor, takes a certain time to reach a predetermined voltage. Some form of voltage level detector is then used to indicate when this level has been reached and then the capacitor is discharged in readiness for a further timing cycle. The voltage level detector can take various forms but nowadays most enlarger timers are designed around the unijunction transistor. These timers are reliable but they suffer from one or two disadvantages.

Due to the fact that the UJT requires a minimum amount of emitter current to trigger it, a limitation is imposed on the amount of resistance that can be used in the timing circuit. In order, then, to get a reasonably long time interval a large value capacitor has to be used and this is invariably of the electrolytic type which is not the most stable of components. The variable element is usually a potentiometer and this requires a hand-calibrated scale which is a drawback to those of us who lack that particular drawing skill! Even should we possess this skill there remains the difficulty of reading the scale in the subdued light of the darkroom. It was this last factor, more than any, which was mainly responsible for the present design.

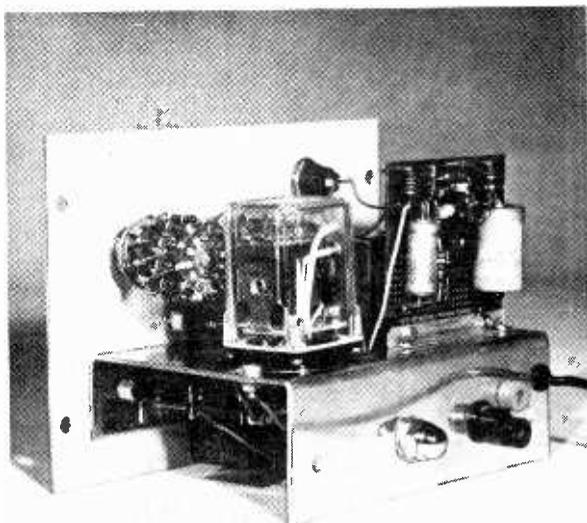
Any time interval, within the range of the instrument, can be set on two decade switches by *feel*; a simple matter, akin to stopping down a lens by the feel of the click stops. Indeed the operation of the instrument has proved to be so simple that no panel marking has been considered necessary.

DESIGN CONSIDERATIONS

The use of decade switches imposes certain restrictions upon the design of the instrument. If a high degree of accuracy is to be achieved, there must be no leakage in the timing capacitor. This rules out the use of a capacitor of the electrolytic type, although a tantalum type should be better in this respect. Since a fairly large value capacitor will still be required, a low voltage polycarbonate type seems to be indicated and in the prototype a $6.8\mu\text{F}$ component is used. This particular value was largely dictated by size and cost.

In order to obtain fairly long time intervals even

with a capacitance value of this order, the resistive component of the time constant amounts to several megohms. This, as previously stated, rules out the use of a UJT and in the present design a Schmitt trigger is employed as the voltage level detector. Since this, too, would present a low resistance load to the timing circuit an f.e.t., connected as a source follower, is interposed between the timing circuit and the Schmitt trigger.



A rear view of the completed prototype.

CIRCUIT DESCRIPTION

The circuit diagram, Fig. 1, shows the state of the push-button switch and the relay contacts immediately before the timing cycle. The timing capacitor, C1, is fully discharged by relay contacts RLA/1 and the gate of Tr1 is at zero potential. Only a small voltage appears at the source due to the self-biasing effect of the small amount of drain current which flows through the resistor chain R22, VR1, R23. As a

Fig. 1: Above is the complete circuit of the timer with the power supply circuit shown below.

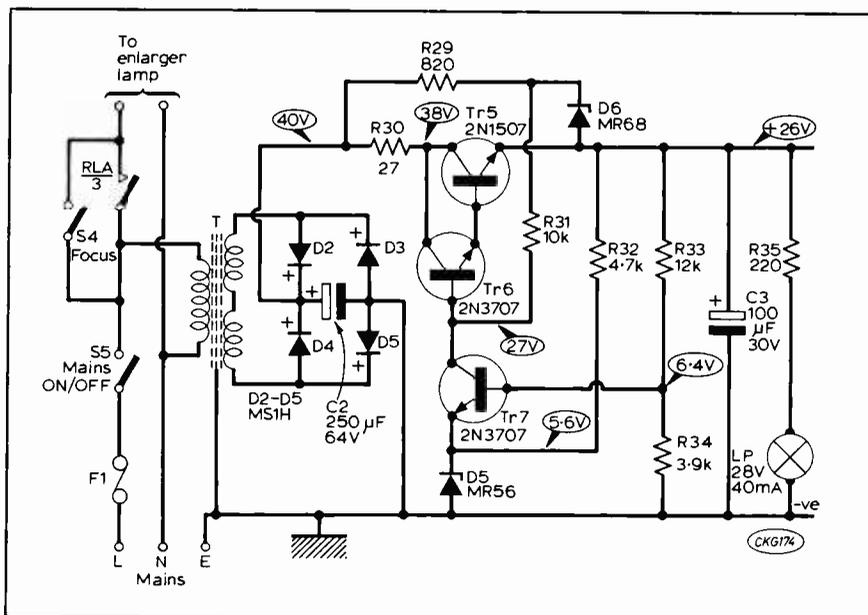
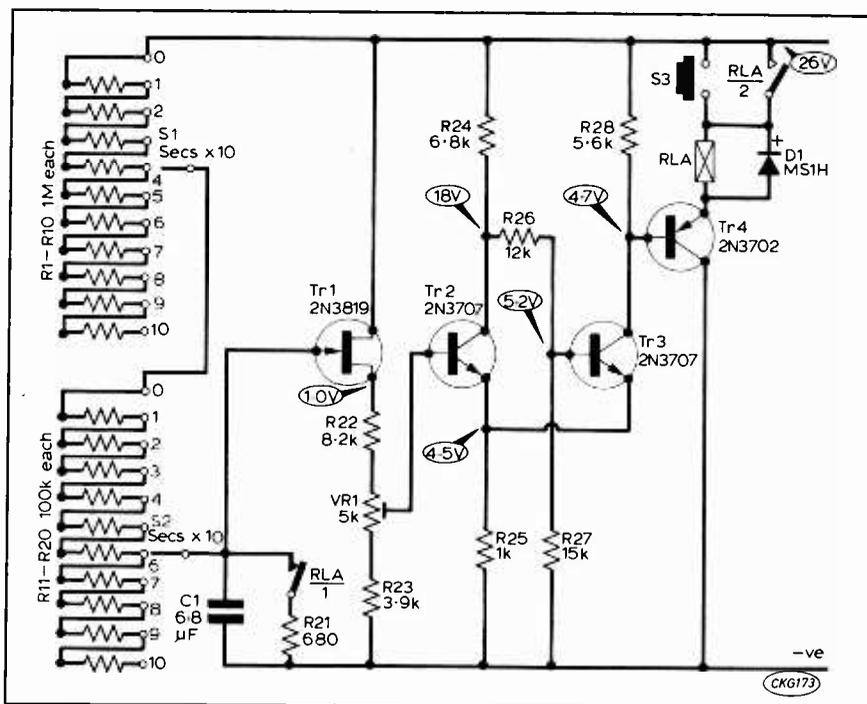
consequence, Tr2 is off, Tr3 is on and Tr4, which is a PNP transistor, would also be on were it not for the fact that the relay contacts RLA/2 and the push-button switch S3 are both open. When the push-button switch is actuated, Tr4 conducts, the relay coil is energized, relay contacts RLA/2 close and the relay is held on by these contacts.

Simultaneously, relay contacts RLA/1 open and allow the timing capacitor to start charging up through the series of resistors selected by the decade switches. The voltage on the gate of Tr1 then rises in an exponential manner and the voltage on the source follows in sympathy. When this voltage reaches a certain value, Tr2 goes into conduction and Tr3 switches off smartly due to the regenerative action which is a characteristic of the Schmitt trigger. Tr4 is also switched off and the relay falls out thus completing the timing cycle. During this timing cycle, relay contacts RLA/3 close, thus applying the mains supply voltage to the enlarger lamp.

In order that the timer should give consistent accuracy it is necessary that the supply voltage be held constant. Transistors Tr5, Tr6, Tr7 and their associated components form a fairly conventional stabilised power supply and the instrument is proof against mains voltage fluctuations over the range of 220 to 260V. Although Tr5 (2N1507) is operating within its rating, a small TO5 heat-sink is mounted on it for added security.

CONSTRUCTION

There is nothing critical about the layout and the constructor is left to use his own ideas on this subject. Several prototypes have been constructed utilising various layouts and no spurious results have been encountered. The photographs show one neat layout which has become the writer's final choice. The



★ Specification

RANGE	0-110 seconds, in 1 second steps, selected by two decade switches.
ACCURACY	5 per cent of set time or better (see text).
"SET-ABILITY"	By feel.
STABILITY	Unaffected by mains voltage variations between 220 and 260V.
REPEAT-ABILITY	Of a very high order as there is no possibility of disturbing a moving scale.

circuit has been conveniently split into two portions and each part has been constructed on a small piece of Veroboard. The one above the chassis, along with the miniature mains transformer, comprises the regulated power supply. The one below the chassis accommodates all the components, with the exception of the relay, which go to make up the timer unit itself. These boards are fixed to the chassis by means of small angle brackets fabricated from short strips of light-gauge aluminium.

The decade switches, push-button switch, focus switch (which by-passes the relay contacts RLA/3 during the composing and focussing procedure), mains on/off switch and pilot lamp are mounted on the front panel. The whole is housed in a Contil 755 instrument case which comes complete with non-slip plastic feet. As its type number suggests, this case has dimensions of 7in x 5in x 5in and completes a very neat instrument which occupies little space. The decade switches, as shown on the circuit diagram, are single-pole 11-position types but in the final prototype 2-pole 2-wafer switches are used and the decade resistors are conveniently mounted between the two wafers resulting in a neat assembly.

The relay is mounted by means of its 11-pin valveholder type base. Some comment on this relay is called for. An incandescent lamp is a very non-

★ components list

Resistors

R1 -R10	1MΩ	R28	5.6kΩ
R11-R20	100kΩ	R29	820Ω
R21	680Ω	R30	27Ω
R22	8.2kΩ	R31	10kΩ
R23	3.9kΩ	R32	4.7kΩ
R24	6.8kΩ	R33	12kΩ
R25	1kΩ	R34	3.9kΩ
R26	12kΩ	R35	220Ω
R27	15kΩ		

All resistors $\frac{1}{2}$ watt high stability carbon film, $\pm 5\%$
VR1 5kΩ preset

Capacitors

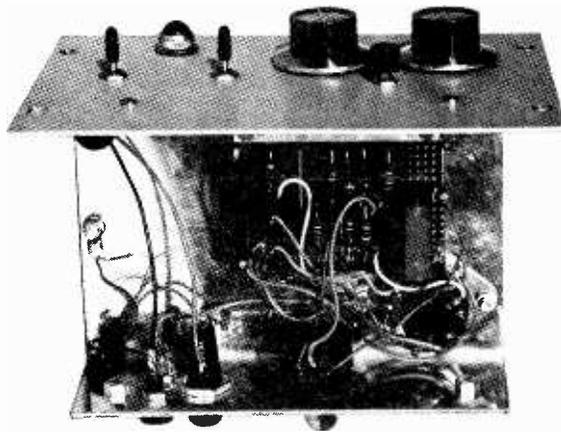
C1	6.8μF $\pm 10\%$ 63V polycarbonate
C2	250μF 64V electrolytic
C3	100μF 30V electrolytic

Semiconductors

Tr1	2N3819	D1	MS1H
Tr2	2N3707	D2	MS1H
Tr3	2N3707	D3	MS1H
Tr4	2N3702	D4	MS1H
Tr5	2N1507	D5	MS1H
Tr6	2N3707	D6	6.8V 5mA Zener
Tr7	2N3707	D7	5.6V 5mA Zener

Miscellaneous

RLA	Relay, Radiospares Type 34A or Omron Type MK3P
T	Radiospares miniature mains transformer, 12V type (The two 12V secondaries are connected in series)
S1, S2	1-pole, 11-way switch (but see text)
S3	1-pole push-button switch
S4, S5	1-pole mains on/off switch
F1	1A fuse-link in fuse-holder
LP	28V 40mA lamp (under-run) in pilot lamp-holder with RED bezel Knobs (Eagle type NK2. Graduations 0-10 at 30° intervals which match switch detent) TO5 Heat sink Instrument case



A top view of the prototype enlarger timer.

linear resistor and it exhibits a relatively low resistance when it is cold. Thus, when it is switched on, there is a comparatively high "in-rush" current and the contacts of the relay should be such as to cope with this heavy load. This is the reason for specifying the particular Radiospares (now R.S. Components Ltd.) heavy duty relay. The mains transformer is also Radiospares type. Before leaving the subject of the relay, however, it might be as well to remark that its rating is quoted for some hundred million operations. This would amount to an awful lot of enlargements! A lighter duty relay could be, and has been, used successfully but it is not considered to be good engineering practice.

SETTING UP

The accuracy of the instrument will depend upon two factors; the tolerance of the decade resistors and the care with which VR1 is adjusted. The 5 per cent tolerance resistors should be good enough for photographic purposes but if one's pocket is deep enough or if the timer is to be used for a more exacting purpose, 2 per cent or even 1 per cent resistors could be used to improve the accuracy. The writer selected the resistors from a batch of 5 per cent carbon film resistors, using a highly accurate bridge for matching purposes.

Once the construction has been completed and the wiring checked, the instrument should be switched on. VR1 should be set with its slider at the end connected to R22 (8.2kΩ). If it is set to its other extremity the voltage at this point may never rise high enough to switch the Schmitt trigger. With the decade switches set for 1 second (x10 at 0 and x1 at 1) the push-button should be actuated and, if all is well, the relay will close and fall out again after approximately one second.

The decade switches should then be set for a period of 30 seconds (x10 at 3 and x1 at 0), the push-button should be actuated and the timing period should be measured and found to be something less than 30 seconds. If this is so, indicating correct operation, the slider of VR1 should then be moved away gradually from its end stop until a position is found where the contact closure is as near to 30 seconds as possible. Once this position has been found, the potentiometer should be left undisturbed and all the other timing periods as set on the decade switches should fall into place.



MOST readers will have seen and tried one of those games where you have to pass a small metal loop over a bent wire, trying to avoid touching it. When the two touch, a bell rings.

Our Buzz-Bar is similar in many ways but it has extra facilities which make it much more fun to use. The level of skill, unlike the simple version, can be varied so that children stand an equal chance with their elders. A lot of fun can be had from a project of this type and it makes an attractive sideshow at a fete or bazaar—especially as it is a bit out of the ordinary.

The main difference between ours and the more conventional set-up is that the “wand” (the small metal loop) can touch the bar for a limited period or number of times. This allows the shape of the wire to be bent into really weird and wonderful shapes and it can be made so that a mistake-free run is virtually impossible.

We have said a limited number of times. Each time contact is made, the electronics part of the circuit adds up the total time that the two have been touching and only causes the bell to ring when a certain level has been reached. In the prototype, using the component values shown, the total time that the two are allowed to touch can be varied from about 0.1 to 1.5 secs. This time range matches pretty closely average skills encountered by the author.

Most people, including children, can manage on the 1.5 sec setting (assuming that they try hard) but, as yet, no one has managed the shape used in the prototype on the shortest time.

The skill control is infinitely variable over the whole range, from 0.1 to 1.5 secs and this control is calibrated so you can even compete against your-

self, trying for a “best” result. On a sideshow, the control can be set to “easy” for children and to a shorter delay for adults, giving everyone a fair go. If you give a prize to anyone managing it and you find out you are giving too much away, the setting can be altered.

The circuit

Obviously no one would want to build in this extra sophistication if the cost was high but as you can

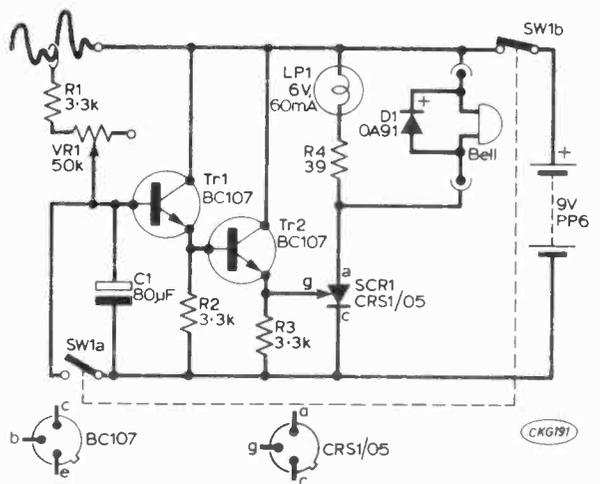


Fig. 1: The circuit of the Buzz-Bar.

see from the circuit in Fig. 1, it is very simple. Even assuming that you have to buy all the components brand new, this should set you back no more than £1. This is of course in addition to the cost of the simple unit; the costs of this with a bell, battery and a framework may come to another £1 or so.

The bar itself is connected to the positive supply line with the "wand" connected via R1 and a variable part of VR1 to C1.

When the wand is touching the bar, C1 charges up through R1 and VR1. When the two are apart, C1 still holds the voltage. This is the main part of the circuit and controls the operation. When the voltage across C1 reaches a certain level, it is arranged that the bell should ring.

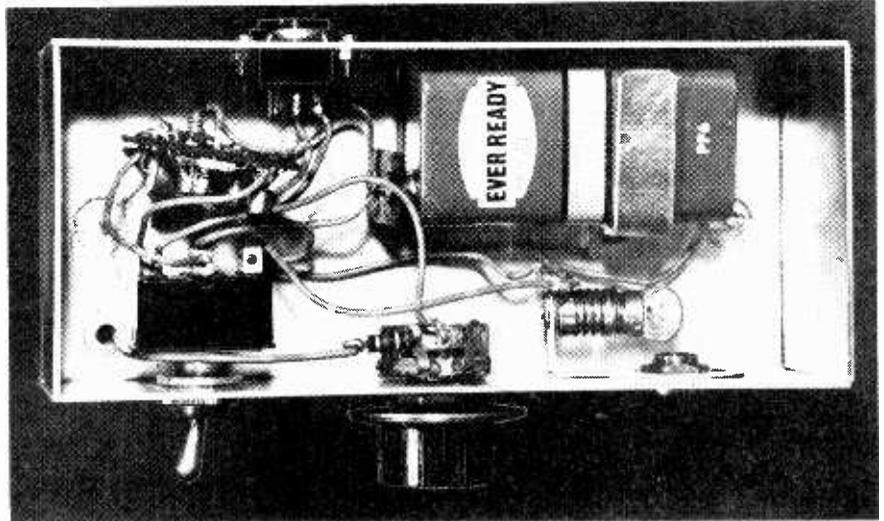
It is vital that we take only a tiny current from

such a small current that it can be considered unimportant.

C1 must be a first class quality component, able to hold its charge properly. Electrolytics vary enormously in their leakage and a decent one must be used. All British electrolytics tried have been found to be good, something which cannot be said for many imported types.

The emitter of Tr2 is connected to the gate of an SCR. As the voltage builds up on C1, this also raises the voltage at the gate until the point is reached when the SCR switches on, causing the battery voltage to be applied across the bell. Two circuits are incorporated in conjunction with the SCR. It was found that the continual ringing of the bell was very annoying—especially indoors and for those

A underside view of the prototype. The various controls can be seen on the front panel. The circuit board is viewed from directly overhead. Compare this with Fig. 3.



C1 otherwise it would be discharging in between "touches." In other words we want to make sure that C1 holds its charge for a reasonably long time. For this reason we connect C1 to a high impedance stage, two emitter followers connected in series. This presents a very high impedance and draws

★ components list

Resistors

R1 3·3kΩ
 R2 3·3kΩ
 R3 3·3kΩ All resistors ½W, 5% types.
 R4 39Ω
 VR1 50kΩ lin. pot.

Semiconductors

Tr1 BC107—see text
 Tr2 BC107—see text
 SCR CRS1/05 (1amp, 50V)
 D1 OA91

Miscellaneous

C1 80μF, 10V or similar, value is not critical;
 6V, 60mA bulb; bulb holder; double pole toggle switch; battery clip; PP6 battery; planed timber; wire coat hanger; Veroboard; Aluminium chassis available from H. L. Smith Ltd, 287 Edgware Road, London W.2. Size: 6½ x 2½ x 1½in, price 60p including postage.

not actually doing the test. For this reason two indicators are used—a bulb as well as the bell; the latter can be disconnected. The bulb lights up when the "error" limit has been exceeded. If this facility is not required a resistor should still be wired in its place—100Ω is about right. Since the bell is a make-and-break device the SCR will switch itself off as soon as the gate voltage falls, unless current is drawn all the time. Including this parallel resistor prevents premature switch off.

The diode across the bell prevents the build up of large back e.m.f. voltages which might otherwise damage the SCR.

SW1 is a double pole switch. In the off position C1 is short circuited, ensuring that when the cycle starts that it is completely discharged; this short is broken when the unit is switched on.

The transistors shown are type BC107 but pretty well any silicon NPN types are suitable. In the unit shown these were later replaced by surplus devices, so salvaging good types for other uses.

Construction

There is nothing at all critical about the construction. In the prototype the electronic components were mounted on a small piece of Veroboard—the layout is shown in Fig. 2. No breaks are necessary in the conductor strip other than those around the mounting screw. This provides a neat and compact layout for the major components.

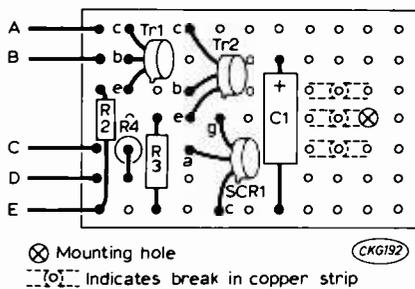


Fig. 2: The component layout on a small piece of Veroboard.

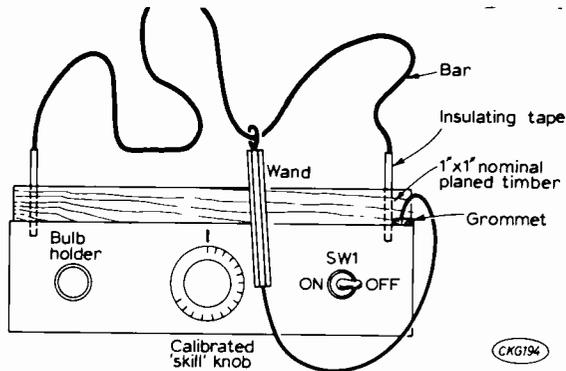


Fig. 4: Front view of the Buzz-Bar.

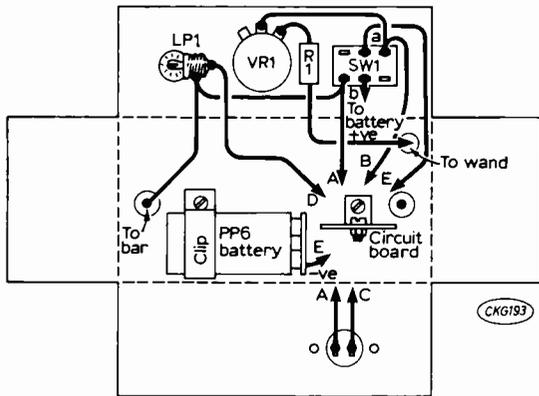


Fig. 3: The wiring diagram. The sides of the chassis have been bent out for clarity.

making a good wand. The wire should then be bent to form a tight loop.

Bands of insulating tape can be wound around the bases of both ends of the bar to prevent it ringing at the beginning and end.

Part of the fun will be bending the wire into shape. As we have said, the shape can be made virtually impossible and bends can be in three dimensions.

When someone does cause the bell to ring, the unit should be switched off. This will discharge the capacitor and allow another run to be tried. Many hours have been spent with the unit described here and although originally designed with children in mind, adults seem to monopolise it. It is only for fun but competitions and all sorts of games can be built up around it. ■

The prototype was built into an aluminium chassis available from the suppliers mentioned in the components list, but once again all sorts of arrangements may be used. Fig. 3 shows the wiring of the components not on the Veroboard; the wires to the board are marked A to E, matching up with the same letters in Fig. 2.

Two large holes are drilled in the top of the chassis to provide access to the bar itself. A piece of planed timber, 1in x 1in, is mounted on top of the chassis by means of two wood screws which also serve to hold the Veroboard mounting bracket and a battery retainer bracket.

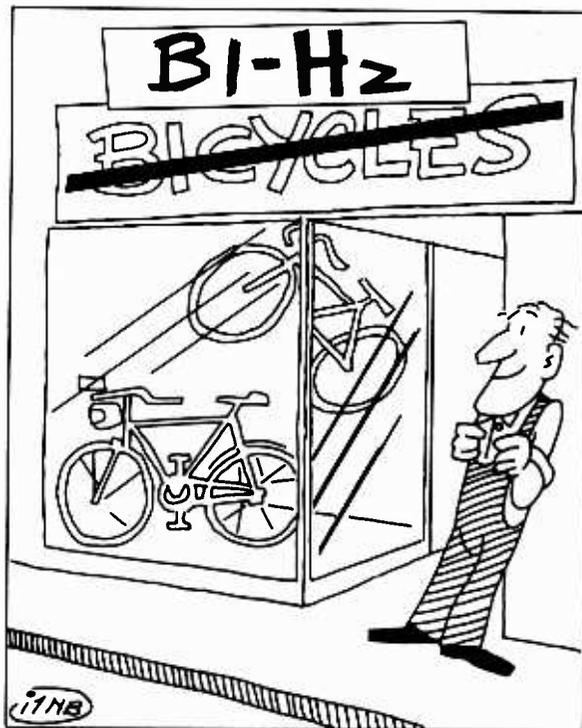
The bell is mounted separately and the leads to this are connected via a plug. A DIN speaker plug and socket were used in the prototype but other types will do just as well.

One other hole is needed in the chassis; to bring the wand wire outside. This hole should be protected by a rubber grommet.

The bar

The bar itself is mounted by pushing each end through small holes drilled through the piece of timber. The holes should be quite small to make the fit tight.

Any firm wire can be used for the bar but a good source is a wire coat hanger; these are cheap and are often given away by dry cleaners. The part just below the hook, where the wires are twisted can be cut, these twisted wires will then fit nicely as a push fit into the body of a "Bic" ball-point pen



IN NEXT MONTH'S

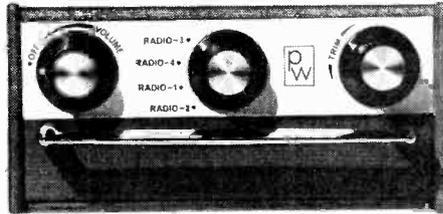
PRACTICAL WIRELESS

FREE INSIDE

PRACTICAL AERIAL DATA WALL CHART

Whether your interests are short wave listening, medium wave DX'ing or listening to FM radio, you will find an aerial design on this wall chart that will improve your reception. Get rid of that odd bit of wire and use our design data to make an aerial for your favourite band. Give that stereo tuner a chance to work properly by feeding it with a solid signal from a decent aerial. Finally, medium wave DX'ers will really appreciate the data for a loop aerial that will effectively reduce that European QRM.

THE

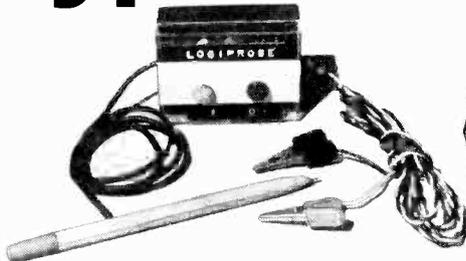


PRE-TUNED CAR/PORTABLE RADIO

Using just six cheap transistors, this radio provides four pre-tuned switched channels, three of which can be adjusted to stations in the medium wave band, the fourth being intended for reception of Radio 2 on long waves. In the home or garden, the internal ferrite aerial is sufficient to provide a good signal in most areas. Placed on the parcel shelf of a car it will perform well utilising the car aerial, the pre-tuned facility being especially useful in moving vehicles.

BE CERTAIN NOT TO MISS THE NEXT ISSUE PRICE 20p

THE 'logiprobe'



Have you ever built a project using digital IC's, only to find that it didn't work first time? The "Logiprobe" will enable you to see what is going on in TTL systems, giving a visual indication of the logic level at any point.

AUDIO REFERENCE SOURCE

What do you use an audio signal generator for? Certainly the full frequency range is useful but 95 per cent of the time spot frequencies are sufficient. This project describes a simple unit with square wave outputs at 100Hz, 1kHz and 10kHz with a calibrated output anywhere in the range 0.1mV to 1V. The cost is only a fraction that of a conventional design and it makes an ideal unit for those who have only occasional use for an a.f. signal source.



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ALL IN THE OCTOBER ISSUE ON SALE 1st SEPTEMBER

PW Microtune



WITH congested amateur and short wave bands generally, there is more and more need for really sharp selectivity, and this circuit is excellent in this respect as well as being a relatively easy and inexpensive project. Coverage is approximately 515kHz to 30MHz in four bands, and the use of a 1.6MHz intermediate frequency gives much better freedom from second channel interference on the high frequency bands, than is obtainable with a similar circuit using 465kHz i.f. The receiver is suitable for the reception of a.m., c.w. and s.s.b. signals.

V5 is a small double triode, used as a.f. amplifier and output stage. This is economical on h.t. and heater current while giving reasonably powerful loudspeaker reception. The secondary of T1 runs to a panel socket where phones or speaker may be plugged in. T2 is a small mains transformer providing up to about 40mA h.t. and 1.5A for the heaters. HT drain is around 30mA and heater current 1.2A, thus leaving the possibility of fitting an extra i.f. stage later, or using a triode-pentode in the V5 position for greater audio output.

Circuit

Fig. 1 is the circuit, and five valves provide the following functions: V1, r.f. amplifier (6BH6); V2, mixer and local oscillator (ECH81); V3, beat frequency oscillator (6C4); V4, i.f. amplifier and diode demodulator (EBF89); V5, a.f. amplifier and output stage (12AT7).

Aerial, mixer and oscillator coils L1, L2 and L3 are tuned by the 3-gang capacitor VC1/VC2/VC3. For maximum possible efficiency throughout all ranges, and with any aerial, the panel aerial trimmer VC4 is provided. VC5 is a similar mixer trimmer. To avoid band switching and the attendant losses L1, L2 and L3 are miniature plug-in coils.

For exact tuning of signals in a congested band, the "microtune" capacitor VC6 is used, having a panel control. This is also very useful when keeping a difficult signal in tune, where even a small movement of the main ganged tuning capacitor may lose it. VC6 also becomes essential when receiver selectivity is at maximum, despite the reduction drive on VC1-3.

Two degrees of selectivity are provided. For normal reception S1 is closed. This gives easy tuning, and ample bandwidth for proper reception of broadcast or similar signals. With S1 open, and the crystal circuit correctly adjusted with TC1, selectivity is very much greater. Closing S2 brings in the b.f.o. necessary for c.w. and s.s.b. reception. No product type detector is included because strong s.s.b. signals can be reduced by the r.f. gain control VR1, while V3 is coupled to the grid circuit of V4 providing a suitable balance of s.s.b. signal and local carrier, so that the diode can function satisfactorily.

Chassis and cabinet

This is of novel construction, the result being inexpensive, easy to make and of quite satisfying appearance.

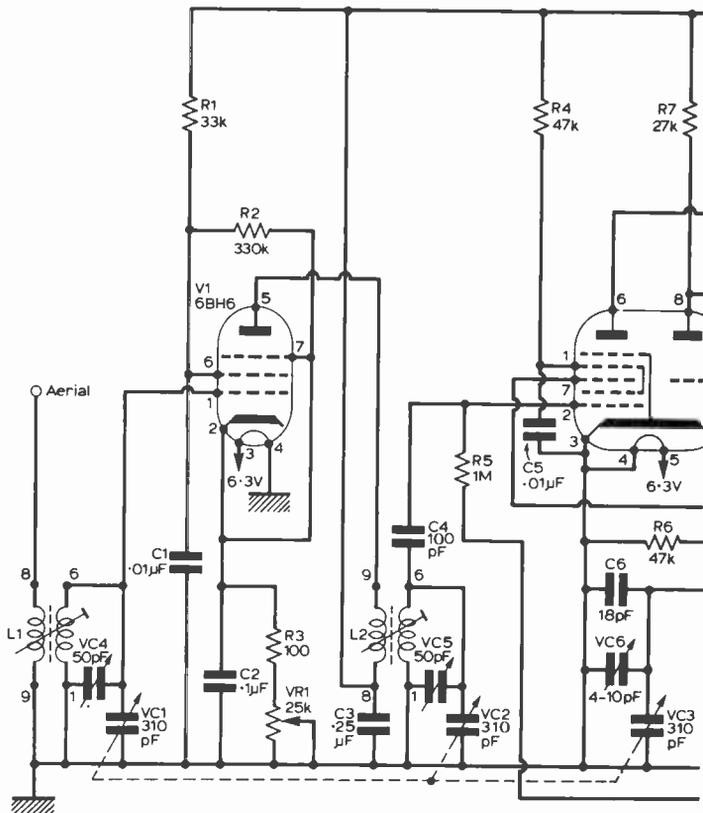


Fig. 1: Complete circuit of the Microtune receiver ▶

4-band receiver

WITH VARIABLE SELECTIVITY

F. G. RAYER

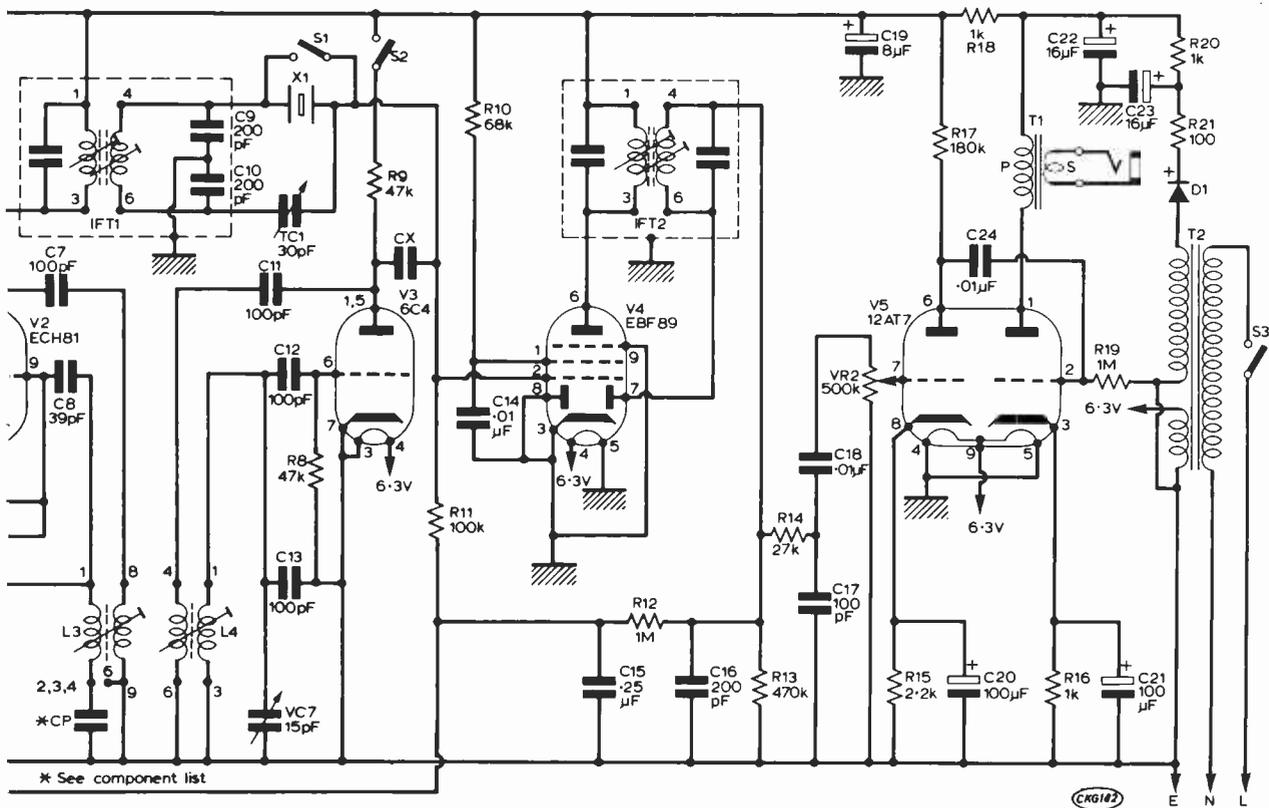
The chassis itself consists of two 12×2in. and two 8×2in. flanged "universal chassis" members with a 12×8in. flat plate. The same screws which hold the 2in. wide members to the plate also secure two 12×4in. and two 8×4in. flanged members on top, thus forming a complete chassis/cabinet 12×8×6in. high. The final appearance of this cabinet, with the top closed by a hinged 12×8in. plate, is quite reasonable, and is obtained with the minimum amount of work.

In the receiver shown, it was decided to cover the front with a sheet of $\frac{1}{8}$ in. paxolin, held in place with component fixing nuts. Sides are cut from 3-ply wood and varnished. These are 8 $\frac{1}{4}$ ×6 $\frac{1}{2}$ in. to give a little overlap at top, bottom and front. The sides are held with chrome headed 4BA screws run through the holes which will be found in the flanged

members. A lid to match is also cut from plywood.

The best way to facilitate construction is first to bolt together the 12×2in. and 8×2in. members, placing the end flanges of the 12×2in. members *outside* the 8×2in. members. Check for squareness, put the 12×8in. plate on, and drill three holes along each 12in. edge, and two on each 8in. edge, about 1 $\frac{1}{2}$ in. from the corners.

Drill through the chassis flanges to match, so that these can be bolted to the 12×8in. flat plate. Assemble the 12×4in. and 8×4in. members to match, put the plate on these, and drill the flanges. The whole can then be bolted together, though construction is easier if the 12×4in. back member is left off until later. In any case, drill and punch holes for the components as in Fig. 2 before assembly, and punch holes for the panel controls, as in Fig. 3.



* See component list

CRG182

before screwing on the 12×2in. front runner.

Mark out and drill the 12×4in. front member before finally screwing it in place.

If an overall panel of thin paxolin or other material is to be fitted, mark it now by holding it in position and scribing through the existing holes with a sharply pointed tool. Holes will then match up correctly.

Above the chassis

Holes are drilled near T1 and T2 so that adequately insulated leads can pass down through the chassis. Fit valve and coil holders with tags as in Fig. 3, including soldering tags under the nuts. Drilling positions for L4 and the i.f.t.s can be found by pressing paper on the pins, holding this on the chassis, and marking through with a sharp point. A central hole is necessary to allow adjustment of the cores. It is as well to put pieces of insulated sleeving on the pins.

The front is carefully marked with the height of the ganged capacitor spindle, so that the drive can be fitted, and the spindle should line up exactly with this. Solder insulated leads to the tags of VC1, VC2 and VC3 and pass them down through holes, before bolting the capacitor in place.

There is some latitude in the choice of VC6, and a component with a maximum value between 4pF and 10pF is most suitable. If VC6 is too small, it may give adequate tuning near the h.f. end of a band, but not near the l.f. band end. The capacitor should be smooth and electrically silent in action. Cheap surplus capacitors in good condition may be used by removing some plates.

In a similar way, though 15pF is shown for VC7, values of from about 10pF to 25pF are possible.

Below the chassis

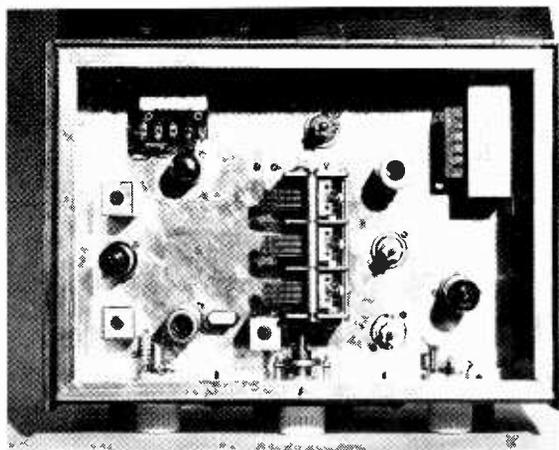
All connections etc. are shown in Fig. 3. Capacitors VC4 and VC5 need not be 50pF, but values of about 25pF to 50pF are most suitable. VC4 is on a bracket cut from scrap metal, and operated by a ¼in. insulated or metal shaft and coupling.

The aerial socket is an insulated type and the adjacent terminal on the back runner is for earth.

The contact-cooled rectifier is bolted flat on the chassis side, and all burrs should be removed from the associated holes after drilling. Capacitors C22 and C23 are a double unit in Fig. 3, but separate capacitors give the same result. Tag strips are used to support various items and connections.

In general, run heater and h.t. leads against the chassis. Leads to r.f. and other circuits should be clear of the metal chassis. It is useful to employ differently coloured wires or sleeving, such as red for h.t. positive, blue for heaters, etc.

The leads to VR2 run along the side of the chassis as shown. All leads should be reasonably short and direct, especially those of grid and anode circuits, which should be well separated from each other. Leads run from the primary of the output transformer T1 to C22 positive, and pin 1 of V5. Leads from the secondary run against the chassis to the miniature output jack. The transformer is intended for a 3 ohm or similar speaker, which should be in a cabinet or fixed to a baffle board. Put extra sleeving over the primary leads of the mains transformer and bring them down to the "neutral" tag N, and to S3. Connect S3 back to the tag L of the tag strip. Run a 3-core flexible cord from the tag strip, brown to L,



View into top of cabinet. Compare with Fig. 2, right.

blue to N, and green-yellow to E (metal chassis). Connect the cores correctly to a 3-pin plug fitted with a 3A fuse.

The 6.3V secondary leads pass through a hole, and are taken to MC and pin 4 of V1, Fig. 3. The h.t. leads go to MC and rectifier negative.

Modifying IFT 1

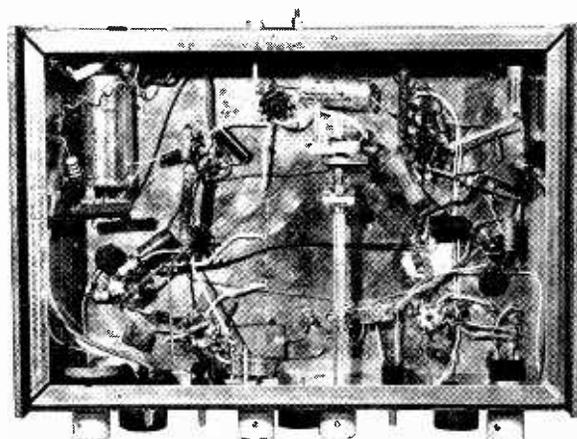
If wished, the receiver can be tested by fitting i.f.t.1 as supplied, omitting TC1 and the crystal, and wiring pin 4 to pin 2 on V4. However, i.f.t. has to be modified, to secure a balanced output circuit, when fitting the crystal.

Straighten the screening can tags and remove the can. 100pF capacitors are internally fitted between pins 1 and 3, and between pins 4 and 6. Cut the leads of the capacitor between pins 4 and 6, and remove it. Replace the can and bend over the tags.

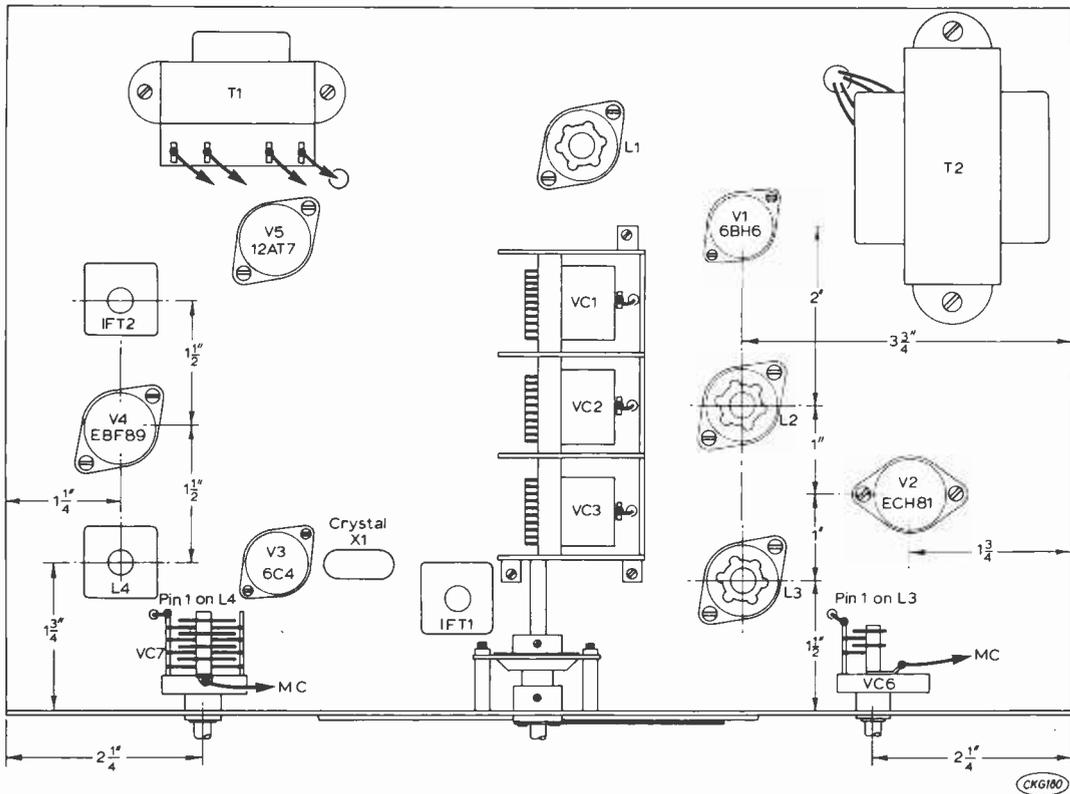
The i.f.t. is fitted as in Fig. 3, and C9 and C10 (each 200pF) are soldered from MC to pins 4 and 6, as shown. The receiver can be tested in this form without TC1 and the crystal.

Crystal filter

The i.f.t.s are intended for 1.6MHz, but have some range of adjustment, so that it is not essential that

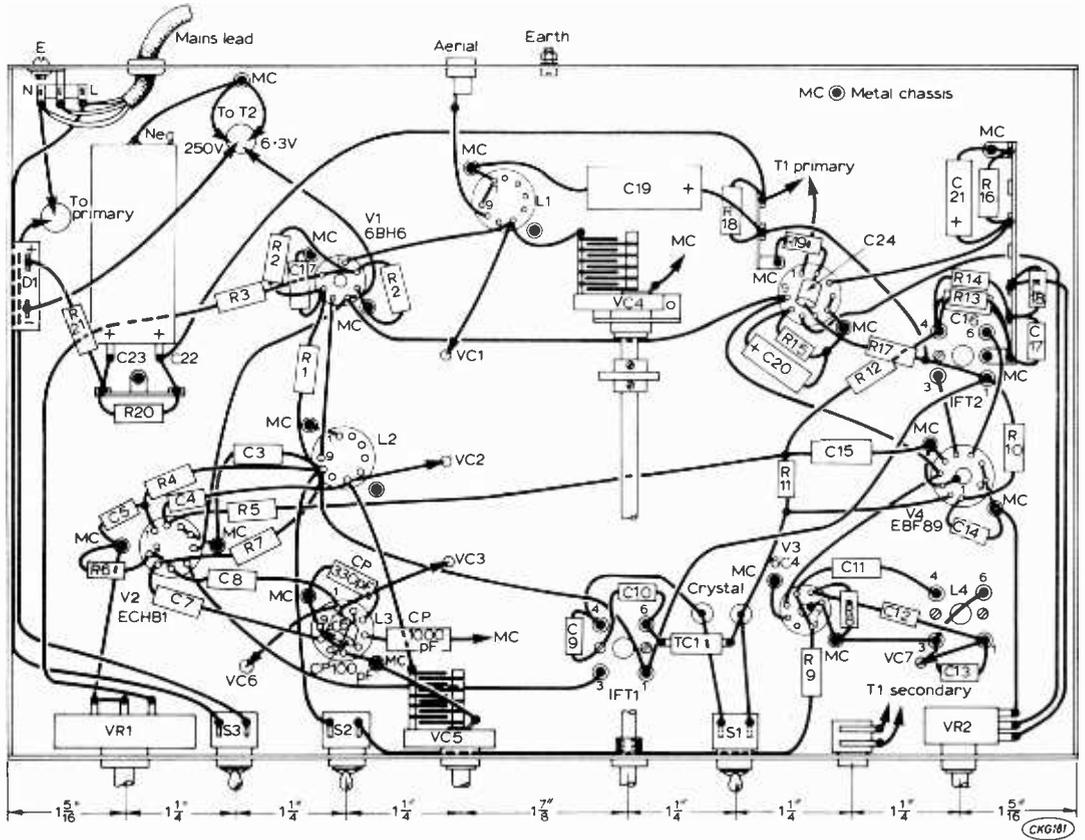


This view may help when wiring underneath the chassis from Fig. 3, right.



▲ Fig. 2: Layout of components mounted on top of the chassis.

▼ Fig. 3: All wiring is shown in this under chassis diagram.



the crystal be exactly this frequency. But to avoid the possibility that the i.f.t.'s cannot be adjusted to the crystal frequency, the latter ought if possible to be in the 1575-1625kHz range. In some commercial equipment, where an interfering transmission may fall around 1.6MHz, it is usual to fit a 1.6MHz wave-trap in the aerial circuit. In the receiver described, no trouble of this kind was encountered.

Adjustments to the crystal filter are best carried out with a signal generator, or, if this is not available, by tuning in a strong, stable signal, such as a BBC transmission on medium waves.

With S1 open and TC1 about half closed tune slowly through a strong signal, to locate the crystal resonance. It will probably be found that the response of the i.f.t.'s gives strong reception over a few degrees of the tuning scale. Near this, one side or the other, the crystal resonance point should be heard. This may be quite weak if far from the i.f.t.'s in frequency, but should be very sharp, having a peak covering only a small part of a degree on the scale.

If this peak is not found, close S1, move all the i.f. cores a little one way, and search for it again. If it is still not found, repeat, moving the cores the other way.

When a signal can be tuned in on the crystal resonant point, adjust all the i.f.t. cores to this, using a proper core adjusting tool. This should give an enormous increase in sensitivity and signal input should be reduced, or VR1 turned back. A high resistance voltmeter may be clipped across C14 (negative to chassis) and adjustments made to secure maximum voltage, as this is more accurate than adjusting by ear.

TC1 should then be adjusted to balance stray capacitance. This is easy with a signal generator, but can be done without it.

Tune slowly through a stable transmission, carefully noting volume (or preferably the voltmeter reading). It will probably be found that there is a dip in volume one side the signal, and a less selective response the other side. Adjust TC1 a little at a time, noting how this changes. When TC1 is adjusted too far, the dip or notch will move to the other side of the signal, and the less selective response will appear on the opposite side of the signal to that originally. The best setting for TC1 is midway between these two situations. Tuning should then be extremely sharp, while music will sound very muffled, due to sideband clipping.

This type of crystal filter can be used with a variable capacitor instead of TC1, with panel control, but this has to be completely insulated from the chassis and panel. A variable control allows the filter rejection notch mentioned to be moved across the pass-band of the i.f. amplifier, reducing or eliminating an interfering carrier.

With VC7 half open tune in accurately an a.m. transmission, close S2, and rotate the core of L4 until a strong heterodyne is heard. Set the core in the zero beat position and seal. Moving the core either way from this position causes a tone which rises in frequency. Rotating VC7 from the central position has the same result.

Cx is an extremely small coupling capacitance, and it may be found that the lead from R11 to pin 2, V4, is near enough to C11 to provide this. If not, run an insulated wire from pin 5, V3, near this lead.

If the coupling of V3 is too great, weak signals will be lost. If, on the other hand, coupling is very small,

★ components list

Resistors

R1 33kΩ 1W	R8 47kΩ ½W	R15 2.2kΩ ½W
R2 330kΩ 1W	R9 47kΩ 1W	R16 1kΩ ½W
R3 100kΩ ½W	R10 68kΩ ½W	R17 180kΩ ½W
R4 47kΩ 1W	R11 100kΩ ½W	R18 1kΩ 1W
R5 1MΩ ½W	R12 1MΩ ½W	R19 1MΩ ½W
R6 47kΩ ½W	R13 470kΩ ½W	R20 1kΩ 2W
R7 27kΩ 1W	R14 27kΩ ½W	R21 100kΩ 1W

VR1 25kΩ pot. linear. VR2 500kΩ pot. log.

Capacitors

C1 0.01μF 350V	C13 100pF SM
C2 0.1μF 150V	C14 0.01μF 350V
C3 0.25μF 350V	C15 0.25μF 150V
C4 100pF SM	C16 200pF
C5 0.01pF 350V	C17 100pF
C6 18pF SM	C18 0.01μF 150V
C7 100pF SM	C19 8μF 450V
C8 39pF SM	C20 100μF 6V
C9 200pF 5% SM	C21 100μF 6V
C10 200pF 5% SM	C22 16μF 450V
C11 100pF SM	C23 16μF 450V
C12 100pF SM	C24 0.01μF 350V

Padding capacitors: Range 2, 100pF SM: Range 3, 330pF SM: Range 4, 1000pF SM.

VC1-2-3 3 x 310pF gang (Jackson—E type)
 VC4 50pF variable (type C804)
 VC5 50pF variable (type C804)
 VC6 5pF variable (type C804)
 VC7 15pF variable (type C804)

TC1 30pF compression trimmer

Valves

V1 6BH6	V4 EBF89
V2 ECH81	V5 12AT7
V3 6C4	

Inductors

L1 Miniature plug-in, valve type (Denco "Blue").
 L2 Miniature plug-in, valve type (Denco "Yellow").
 L3 Miniature plug-in, valve type (Denco "White").
 (Frequency ranges as in text)
 L4 BFO coil (Denco BFO2/1-6)
 IFT1/2 IF Transformers (Denco IFT16)

Metalwork

"Universal chassis" flanged sides: 12 x 4in. (2), 12 x 2in. (2), 8 x 4in. (2), 8 x 2in. (2), panels 12 x 8in. (2) (Home Radio).

Miscellaneous

T1, Valve output transformer (Home Radio TO43).
 T2, Mains transformer, 250V 40mA, 6.3V 1.5A. (Home Radio TM24A). X1, crystal 1.6MHz, type HC6U, and holder (Sensor Crystals). D1, contact cooled rectifier, 250V 50mA. Valveholders, B7G (2, with screening cans), B9A (3). Dial and drive (Jackson 4103/A), coupling (Jackson 5610). On/off toggle switches (3). Headphone socket. Polystyrene rod and panel bush. Knobs.

s.s.b. signals, even when resolved, will sound like very much over-modulated a.m. However, VR1 allows signals to be reduced, so Cx is not critical.

When receiving s.s.b., turn VC7 one way or the other, as needed to resolve the signal. The a.f. gain (VR2) should usually be well advanced, while strong

signals have to be reduced at the demodulator diode by turning back VR1. With correct adjustment, the circuit gives very good results in s.s.b.

CW is dealt with in a similar manner, VC7 adjusting the beat-frequency note. Switch S2 is off for a.m. reception, and VC7 is inoperative.

It will be seen that strong injection from V3 will create an a.g.c. voltage, reducing gain, but this was not found too important, using minimum coupling, as explained. This effect can if wished be overcome by switching the a.g.c. out for c.w. and s.s.b. reception.

Band coverage

Coils are inserted in a set of three for each band, and the ranges are approximately as follows:

Range 2. 515-1545kHz.

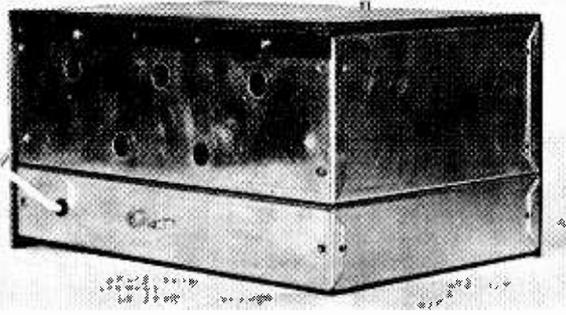
Range 3. 1.67-5.3MHz.

Range 4. 5.0-15.0MHz.

Range 5. 11.0-30.0MHz.

Range 2 gives m.w. coverage, and may not be required. Range 3 includes the two l.f. amateur bands 80 and 160m, and many other transmissions. Range 4 covers most general s.w. broadcasts, with Range 5 taking over for the h.f. bands.

Coverage is adjusted by closing VC1-3, and adjusting the core of L3 for the l.f. band end. To simplify adjustment, C6 is fixed, and no adjustment is made at the h.f. end of the bands. If this is required, replace C6 by a 30pF trimmer.



This not very inspiring view of the back of the receiver shows how the flanged "universal chassis" members are bolted together with a flat plate in between, forming the top of the chassis.

Tune in a signal near the h.f. end of the band (VC1-3 open) and peak VC4 and VC5 for best volume. Tune towards the l.f. end of the band, adjusting the cores of L1 and L2 to give best volume. When the cores of L1 and L2 are correctly adjusted, little movement of VC4 and VC5 will be required. However, some adjustment of these controls will improve weak signals. No efficiency is lost if both VC4 and VC5 can be peaked with any set of coils, and are not then fully open or fully closed. The core adjustments are thus not too critical.

L1 and L2 are separated and partially screened by the can on V1, and by the ganged capacitor. With some aerials it may be found that VC1 becomes regenerative at maximum setting of VR1 at some frequencies, and this effect can be used to boost sensitivity.

CHARLES MOLLOY

THE Medium Wave Column

PROPAGATION over the long sea path between the UK and the northern part of South America is often good during the late summer. From midnight until sunrise is the time to search for medium wave stations from this area and many Latin Americans can be heard, Venezuelans being particularly prominent. Listen for Radio Giradot, Maracay on 650kHz; Radio Rumbos, Caracas on 670kHz; Radio Caracas 750kHz; Radio Puerto la Cruz 760kHz; Radio Margarita, La Asuncion 1020kHz; Radio Zulia, Maracaibo 1080kHz; Radio Carupano 1110kHz; Ordas del Lago, Maracaibo 1120kHz; Radio Tiempo, Caracas 1200kHz; Radio Valera 1230kHz.

Medium wave broadcasters in the Caribbean area are capable of being logged in the UK at this time of year. The most conspicuous is PJB on 800kHz which is a 525kW outlet of Trans World Radio, located on the island of Bonaire in the Netherlands West Indies. This station broadcasts religious programmes in English and other languages and it also relays Radio Nederland. Other English speaking transmissions to look for are from Georgetown, Guyana on 760kHz; Radio Belize on 834kHz; Radio Caribbean in St Lucia in the Windward Islands 840kHz; Radio Victoria, Arubia, NWI on 925kHz; ZDK St Johns, Antigua on 1100kHz.

DX'ers generally find it useful to have a list of known broadcasting stations arranged in order of frequency. J. S. Smith of Enfield, Middlesex; S. F. Hannaford, Plymouth and David Cotterall, Helensburgh, Scotland have enquired about published lists of medium wave stations. "Guide to Broadcasting Stations" Butterworth Press is on sale in many bookshops at 50p. It covers all medium wave stations in the European area and North Africa plus a number of the more powerful ones from North and South America and it should be of value to the newcomer to the band. For the serious DX'er there is the World Radio-TV Handbook published in Denmark and distributed in this country by Fountain Press. It costs £2.80 but in addition to comprehensive lists of the medium wave stations in the different continents it contains detailed information, by country, of radio stations and broadcasting organisations in every country in the world. For the specialist there is "Broadcasting Stations of the World, Part 2" produced by the Foreign Broadcasting Information Service of the United States Government. All known stations outside the United States in the range 150kHz to 26MHz are listed. The current edition, can be obtained for \$2, post paid, by writing to the Superintendent of Documents, Government Printing Office, Washington, DC 20402, USA quoting catalogue number PX EX 7.9.971 Part 2.

Please send logs and information about the medium waves to the author at 132 Segars Lane, Southport PR8 3JG.

GAS FILLED VALVES and TUBES

I. R. SINCLAIR

IN AN AGE of semiconductors, the continued and increasing use of valves may seem curious, the use of gas-filled valves even more so. The facts are that semiconductors have by no means completely conquered the electronics market; there are still useful jobs for which valves are either more suitable or considerably cheaper, and there are some jobs for which only gas-filled valves are suitable at all.

The conventional hard (meaning evacuated) valve uses a cathode, heated by a wire filament, as its source of electrons which will then travel from the cathode to any positive electrode in the valve. The current which can be drawn depends on the rate at which the cathode can emit electrons and the field which the anode can create to attract them. There is little difficulty in creating high fields, an anode at a higher voltage or placed nearer the cathode will ensure higher fields, but there is a limit to the current which can be taken from a cathode of any given area, and there is also a limit to the field strength which can be applied to the usual oxide cathode without pulling the coating off the nickel tube which supports it.

The effect of gas

Before we can understand the effect of gas in a valve, we have to understand the way in which a gas behaves at low pressure. Gases, like other materials, are made up of atoms which are usually grouped together as molecules. Air, for example, is mainly a mixture of two gases, oxygen and nitrogen, and each of these gases consists of molecules of two atoms each. Carbon dioxide, another gas present

in air, consists of molecules containing three atoms, one of carbon and two of oxygen. The important difference which distinguishes gases from liquids and solids is that gas molecules are spaced well apart; the average spacing at normal pressure is about 300 times the diameter of the molecules, so that the molecules are fairly free to move about and exert force (noticeable as pressure) on the walls of the container. If a small amount of gas is allowed to enter a large evacuated container, the distance between the molecules increases and the gas fills the container; we say that the gas has expanded. If we compress a gas to fill a small container, the spacing between the molecules decreases; we can decrease it so much for some gases that they turn into liquids. The laws connecting the pressure and volume of a gas were discovered by *Boyle* some 300 years ago, but it was only in the middle of the last century that it was discovered that gases at low pressures conducted electricity.

Electricity is conducted when charged particles move in a substance. In metals, the free electrons are the charged particles, in liquids, mainly solutions of certain materials in water, conduction takes place by positive and negative particles together. These particles are termed *Ions*; they are charged fragments of atoms which have been split by the action of dissolving the solid in water. In gases, we have molecules moving at high speeds around 500m per second at normal room pressure and temperature) and colliding with each other violently, but all this movement does not cause conduction because the particles are not charged. We can make charged particles of the molecules only by the violent means of splitting the molecules into atoms and the atoms into charged ions, as in the case of liquid conductors. We can do this by hitting the molecules so hard that they separate into atoms and the atoms lose one or more of the electrons which surround the central portion. We are then left with large positive ions and negative electrons. Note that these positive ions have a real independent existence, and can be collected, they must not be confused with semiconductor holes, which, though just as "real" in the sense of having measurable mass, velocity and charge, cannot be separated from the crystal lattice of the semiconductor.

Ionisation

The splitting up, or ionisation, of the atoms of a gas can be carried out by any form of energy sufficient in size. Early workers with static electricity had noticed their capacitors rapidly discharging when they were held near a flame; the heat was producing some ions which were then attracted to the negative end of the capacitor while electrons, usually attached to atoms, arrived at the positive end. Ultra-violet light is another source of the energy needed to ionise a gas; Heinrich Hertz had noticed in his pioneer work on radio transmission and reception that a spark passed more easily between two electrodes at a given voltage if they were illuminated. The application of heat also causes ionisation; a hot ionised gas is called a "plasma" and conducts well enough to be used as a conductor at temperatures where metals would melt. Since heating a gas is simply a method of making the molecules move faster, we might expect that any method of making the molecules move faster might also cause the gas to become ionised if we apply enough energy.

If gases are so easily ionised, why do they not conduct electricity well? The answer is that ions in a gas cannot move easily to the anode or cathode, whichever is attracting them. Imagine a gas confined between two electrodes (Fig. 1) and one atom ionised. Clearly the positive ion will be attracted directly to the negative electrode and the negative ion to the

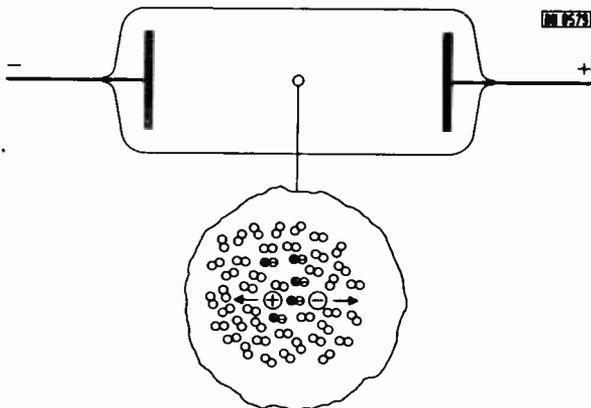


Fig. 1: The electrodes attract the ions but other atoms hinder this movement. The shape, size and spacing of atoms can be measured to a considerable degree of accuracy.

positive electrode; the forces act in straight lines from electrode to ion. It is, however, impossible for the ions to move in straight lines without colliding with other atoms, and it is the process of making collisions which accounts for the odd behaviour of gases. If the forces acting on the ions in our example are not very great, then the ions may rebound into each other and recombine, or they may slowly make their way, with many collisions, to the electrodes. The current in the second case will be so small that only electrostatic instruments will detect it. If we increase the voltage between the electrodes, still keeping the gas at normal pressure, then the forces on the ions will be greater and so the collisions will be more violent. Eventually, as we raise the voltage, the collisions may become so violent that new ions are created on each collision. When this happens, the number of ions available to carry the current increases enormously, and the current is large. We see a spark pass when this happens. If the voltage supply is well regulated, a continuous spark will pass; if, as is usually the case, the voltage drops when the spark passes, the ions are collected by the electrodes leaving no more available until the voltage rises high enough again to start more ionisation by collision, so that sparking is intermittent.

Reducing pressure

When we reduce the pressure of a gas, we are separating the atoms so that there are fewer collisions. Note that "fewer" still means many millions of collisions per second, even for currents of a few nanoamps. If we create a pair of ions in a gas at low pressure (about one ten thousandths of the normal atmospheric pressure) they will move very much further before colliding with atoms. Since a steady force of attraction between ion and electrode causes the ion to accelerate steadily, the ion can be travelling at a very high speed when it eventually hits another atom and it is very much more likely that it will cause the atom to ionise. If the pressure is low enough, each ion is capable of creating another ion pair at each collision, so that the number of ions

formed rises extremely rapidly. This sort of thing is called a "chain reaction" (Fig. 2) and it causes the gas to become a good conductor very rapidly. There are several important points about this chain reaction. It takes place only in a range of pressures; at high pressures the molecules are too close to allow the ions to reach a speed fast enough for ionisation by collision. Only if the voltage is made very high, about 30kV per inch gap between the electrodes, will ionisation take place to allow sparking. If the pressure is very low it may be possible for an ion to travel, on average, all the way from one electrode to the other without hitting another particle, in which case the current is only that carried by the original ions and is very low. Only in the range of pressures between these extremes can ionisation be reliably produced with low voltages (of the order of 150-300V) but high currents.

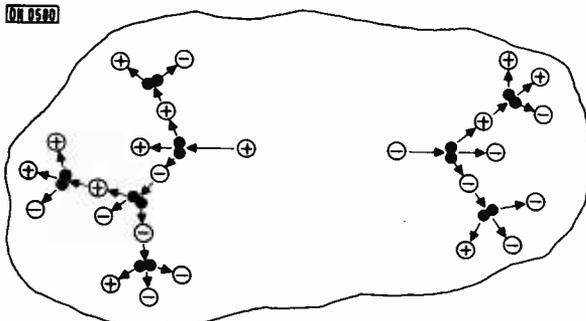


Fig. 2: A chain reaction occurs when ions can move far enough to accelerate to high speeds; when collision occurs more ions are produced.

The voltage used is also critical. Below a voltage called the "striking voltage," no ionisation takes place to a sufficient extent to cause noticeable currents because the voltage cannot give any ions which are formed enough speed to ionise other atoms by collision. The value of this striking voltage depends on the gas used, its pressure, and the materials used for the anode and cathode.

When current is flowing and the gas is already ionised, the voltage drop between anode and cathode is smaller than the striking voltage, and is called the "running voltage." Most of the voltage drop takes place near the cathode, as this is where most of the collisions take place due to electrons leaving the cathode. This region is visible because the excess ions recombine, causing light to be emitted. The value of the running voltage is also dependent on the gas used, its pressure and on the anode and cathode materials. In the running condition, the gas discharge behaves as a negative resistor, meaning

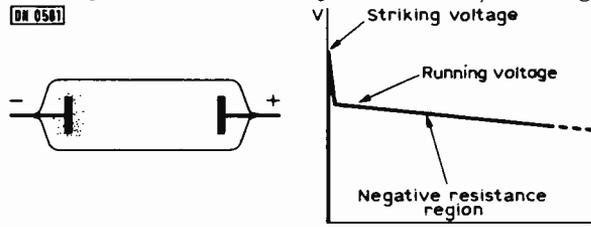


Fig. 3: A gas discharge appears around the cathode at fairly low pressures (about one millionth of atmospheric pressure). On the right is shown the characteristic for a gas tube.

that the voltage between the electrodes decreases as the current increases see Fig. 3. Contrast the behaviour of a normal resistor, where the voltage

drop increases as the current through it is increased.

Armed now with some knowledge of the complex processes which take place in a gas at low pressure, let us now see how these processes can be used.

Gas filled rectifiers

An ideal rectifier should have a very small forward voltage drop when conducting, a very high reverse resistance, the ability to withstand high reverse voltages and the ability to pass high forward currents. For low voltages, semiconductors which answer this specification fairly well have been available for some time and have superceded the diode valves formerly used. Problems arise, however, when voltages of several kV and currents of several amps are required, as they often are in a transmitter. Connecting semiconductor rectifiers in series is not always suitable (it is difficult to ensure that the same voltage appears across each rectifier) and can be expensive when really high voltages are used. Valve rectifiers using oxide cathodes can be used up to a few kV, but the high electric field causes the oxide to peel off at higher voltages. Valves using thoriated tungsten filaments can be used, but the currents available are restricted, since these filaments are not such efficient producers of electrons as oxide cathodes. The solution, which has been used for many years, is the gas-filled rectifier.

If a rectifier contains some gas, then the electrons which are emitted cause ionisation of this gas, and a low anode-to-cathode voltage will be able to cause conduction. The resistance of the valve is very low, a combination of the resistance of the leads and the resistance of the gas, and the *slope resistance* is negative, as previously explained.

Since electrons are provided in large numbers by the cathode the running voltage is very low, but when the voltage reverses, electrons are no longer emitted from the cathode and the gas will ionise only if the voltage between the anode and the cathode exceeds the striking voltage. By making the pressure of the gas low enough, this striking voltage can be made almost as high as we like so that a gas rectifier can be used up to very large values of peak reverse voltage, several hundred kV. The valve-makers' problem is to make the pressure of gas constant despite the absorption of gas by the anode and the emission of other gases by the cathode. If the design of the rectifier is such that these problems are overcome, then the gas rectifier is reliable and long-lived. Note the difference between this case and that of the hard valve rectifier which has become gassy through leakage or overheating. Here there is no control of gas type or pressure, and the valve fails when the striking voltage is less than the back reverse voltage. In commercially made gas rectifiers, the gases commonly used are *Mercury-Vapour* for the smaller types, and *Xenon* for the larger varieties.

Some precautions are needed when using gas rectifiers. When mercury vapour rectifiers are in use, the temperature of the valve must be allowed to come up to full operating temperature before high voltages are applied. This is because the mercury is in the liquid state at room temperatures and has a very low pressure at such temperature. If high voltages are applied in these conditions, there is a risk of sparking between anode and cathode, or at least of a very high resistance discharge. Either way, the resulting dissipation can be very destructive to the cathode, and dangerous to the operator if the valve should

fracture, as mercury-vapour is poisonous. Most mercury-vapour rectifier circuits incorporate some sort of automatic delayed switching to ensure that the heaters have been on for at least one minute before the anode volts are switched on. Such a circuit is shown in Fig. 4.

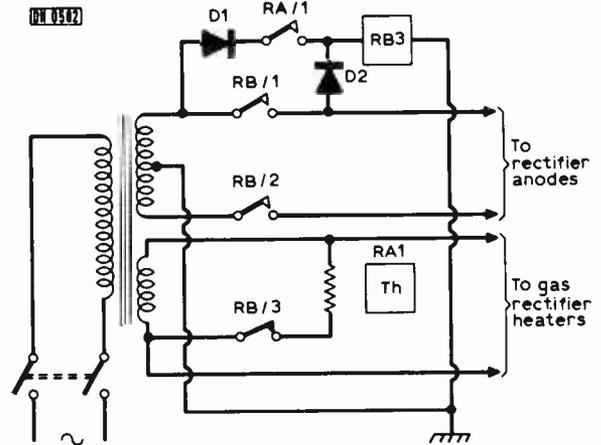


Fig. 4: A delayed switching circuit for gas filled rectifiers. The thermal relay in the heater circuit ensures that there is a delay before the h.t. is applied.

Voltage stabilisers

Another use of gas-filled valves is bound up with the stability of the running voltage. We have said earlier that, as current through a gas-filled rectifier increases, the voltage across the valve decreases. This change of voltage with current is small, and, with suitable choice of materials for anode, cathode, and gas, can be made very small. This is the essence of a voltage stabiliser, that a voltage should be unchanged while current varies.

The circuit of Fig. 5 is a simple stabiliser. When

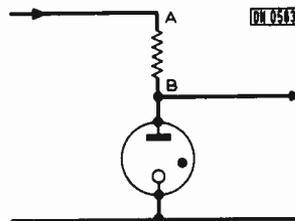


Fig. 5: A simple voltage stabiliser circuit.

voltage is applied at point A and raised until it equals the striking voltage of the gas, current will flow in the valve, and the voltage at B will be the running voltage. As the voltage at A is raised, the current through the resistor and the valve increases, but the voltage at B remains almost constant. If current is taken from B, it is taken at the expense of the current in the valve. If the current taken at B is greater than the current which was flowing in the valve, then the gas discharge will cease and the voltage at B will no longer be stabilised. The actual value of the running voltage, as said before, depends on the gas, and the materials used for anode and cathode; standard values obtainable with well-tried combinations of materials are 45V, 70V, 85V, 105V, and 150V. By more careful choice of materials, the change of voltage for a given change of current can be made smaller than normal, and the change of running voltage with temperature change can also be made very small. Such carefully designed

valves are known as *voltage reference valves*, and can be used, not in the simple circuit of Fig. 5, but in more complex stabiliser circuits such as that of Fig. 6, where the current through the reference valve is fairly constant.

Normally, the voltage difference between striking and running is fairly large, so that a 105V stabiliser needs about 150V to strike, and the voltage required for striking becomes higher when the valve is in darkness. The reason for this is that light provides enough energy to cause some ionisation in the gas, and so provide the conditions for easier striking. When light is excluded, the voltage must be raised to help start ionisation off from the very few ion

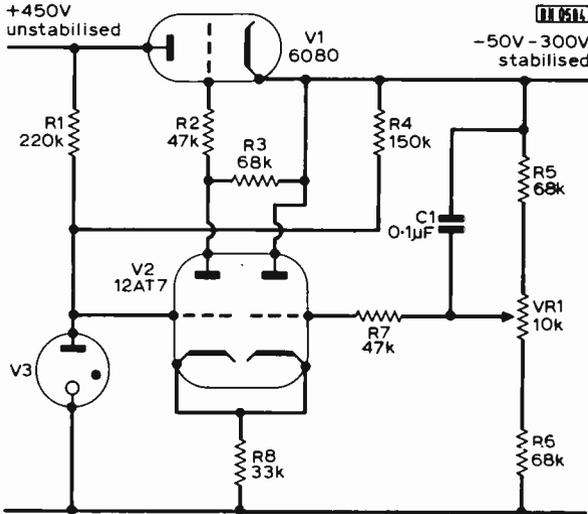


Fig. 6: A complex stabilised power supply.

pairs produced solely as a result of the temperature of the gas. To avoid the difference in striking voltages with light, which can be troublesome in reference tubes, the gas in the valve is often made slightly radioactive. The ions produced by radioactive disintegration then start off the ionisation in the valve, so that the striking voltage is much less dependent on the effect of light.

Neon lamps

Small neon lamps are commonly used as indicators of voltages greater than their striking voltage. Such lamps are used with a large resistance, in the order of 500kΩ, in series so that the running current is extremely low. There are, however, other uses. Since a neon is a gas-filled tube, the running voltage is fairly constant, and neons can be used as stabilisers for circuits which take low currents and for which a large degree of stabilisation is not necessary. For this purpose, neons have to be separated from the

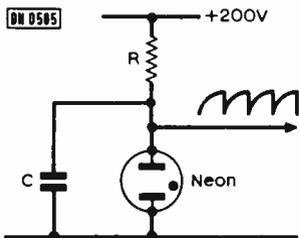


Fig. 7: A simple sawtooth generator. The capacitor must have low leakage and should not be an electrolytic.

series resistor which is built into the base of many types, or neons without a resistor purchased.

There is usually a large voltage gap between striking voltage and running voltage, and this can be

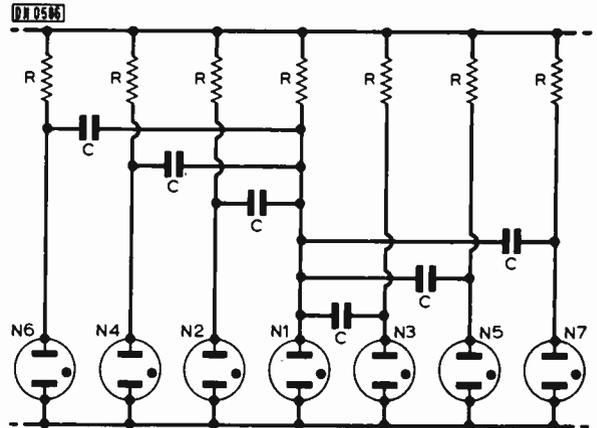


Fig. 8: A random flasher circuit. R can be between 220kΩ and 2.2MΩ and C between 0.1µF and 1µF (low leakage types must be used).

used in sawtooth circuits of the type in Fig. 7. Such signals are used as wide-range frequency sources, or as time delays where high accuracy is not needed. One amusing circuit based on neons is the random flasher of Fig. 8. When the supply is connected, one neon will inevitably strike before any other. The drop in voltage caused by the change from striking voltage to running voltage is communicated to all the others by the capacitors, and delays the rise of volts across all the other neons. The next neon to strike will have the effect of extinguishing the first and also of delaying the firing of the others yet again. The neons will then wink in random order as long as voltage is applied. This can be used as a decoration, but has serious uses when a large number of neons are used, as it can generate random numbers—the **ERNIE** principle is based on such a scheme for selecting Premium Bond winning numbers.

TO BE CONTINUED

CQ! CQ! CQ! CQ! CQ!

ISSUES WANTED

- ...The issue containing details of the 6V car radio.—P. J. Day, 43 Highgate Lane, Farnborough, Hants.
- ...The issue containing details of the Treasure Tracer.—C. Weaver, 30 Cherry Garden Road, Canterbury, Kent.
- ...The June issue containing the Electronic Ignition System.—S. Bennon, 312 Warrington Road, Galzenbury, Nr. Warrington, Lancs.
- ...Jan., June, Aug. and Sept. 1970.—P. D. Williams, 52 Acacia Road, Sutherland, N.S.W. 2232, Australia.
- ...The issues containing Parts 1 and 2 of Transistor Circuitry for Beginners.—P. M. Bontomme, 28 Greencroft Gardens, Reading, Berkshire.
- ...The issue containing the Treasure Tracer.—M. A. Branford, Flat "C", The Clint, 4 Parade, Chudleigh, South Devon.
- ...October and November 1971 P.W.—R. Burke, 62 Garner Road, Walthamstow, London, E.17.
- ...The issues of P.W. containing the three transistor amplifier Take 20 project.—P. Mieszkowski, 25 Kingsway, Wembley, Middlesex.
- ...June 1964 P.W.—H. Hallybone, 7 Saucy Avenue, Harpenden, Herts.
- ...September-December 1961 issues of P.W.—R. B. Howard, 3 St. George's Place, Macclesfield, Cheshire.
- ...July 1971.—D. C. Dick, 97 Curtis Avenue, Kings Park, Glasgow, S.4.
- ...July 1968 P.W.—P. J. Chapman, 90 Melody Road, Wandsworth, London, S.W.18.
- ...Fault-finding chart No. 1 issued April 1968.—H. Symonds, 16 Newhaven Street, Paillea 4655, Queensland, Australia.
- ...April 1969 and subsequent copies of the P.W. Double-12 amplifier.—K. Stean, 101 Atherley Road, Shirley, Southampton, Hants.
- ...The issue of P.W. containing the 7MHz Transceiver.—P. Matlock, 60 Down Avenue, Whitstable, Kent.
- ...February 1971 issue of P.W.—Mrs. M. M. Buckner, 13 Tankerton Road, Tankerton, Whitstable, Kent.
- ...The issue containing the Treasure Tracer.—R. Birby, 1 Gloucester Place, Haughton Road, Darlington, Co. Durham.

JUNK? what junk?



MORAG GREER

THIS XYL *never* complains about the junk in her husband's shack, for the simple reason that he might one day take the notion to have a prowling round *her* shack and decide that it is full of junk which rightfully should be gracing the local rubbish tip.

I must admit that my husband's obsession has added somewhat to my vast store of bits of half-digested knowledge, useful or otherwise. Prior to my marriage six years ago I knew nothing about wireless beyond how to switch the set on and off, find a suitable station, and adjust the volume. An aesthetically satisfying array of lit valves might very well have been left-overs from last year's Christmas tree, and I wouldn't have recognised a silicon epitaxial planar transistor if one had jumped up and yelled, 'Boo!' I still wouldn't, but I read it in an advertisement and it sounds fascinating. Anything to do with transistorised planarians, I wonder?

"No, it isn't!" shouts a voice through the intercom connecting the two shacks. "And how about making some coffee?" This, despite the fact that his junk resides in the kitchen while mine is in a bedroom.

I comply with his request and brew the coffee while watching his usual antics as he tangles himself in various cables and wishes desperately that he could get a third hand for Christmas or increase the length of his arm because the part he wants is just out of reach and where the hell is the soldering bo . . . Aah! "Found it, darling?"

Having consoled him with coffee and a kiss, I leave him muttering about microhenrys and picro-

farads. I sometimes have nightmares about poor Messrs. Henry, Faraday, Volta and all the others, wandering around in that maze of liquorice-allsort components.

In my own shack I am faced with nothing more frightening than a typewriter, a small sheaf of completed manuscript on the right, and a whacking great pile of unsullied, virginal white paper on the left. I have only one problem: that of intelligently and successfully transferring the reams of paper from left to right via the typewriter. My husband maintains that the simple and logical solution would be to shift it straight into the wastepaper basket.

I really can't imagine why Wireless Widows let themselves get into such a situation in the first place. They don't know what they're missing. Listening to shortwave radio can be, among other things, very entertaining, but even more so is watching *one's husband* listening to shortwave radio.

Having finished my "scribbling" for the evening, I make the cocoa, which comes very shortly after the coffee. I hand his mug to him, then retreat to a safe distance, that is, a distance at which I can watch yet not be *seen* to be watching.

There he sits with the earphones on his head, and the oddest expressions darting across his face. His lips purse, his beard wiggles, his eyebrows flit up and down like a couple of frenzied pussmoths. A calm swig of cocoa erupts into an unexplained gale of choking laughter, he scribbles something on a pad and mumbles a few indistinguishable words. I say, "Yes, dear," just in case they were intended for me. When he stands up suddenly to reach for his list of call signs he unknowingly pulls the jack-plug out and has a silent fit, trying to discover what has gone wrong with his beloved B40. Finally he finds the plug dangling around his knees, thrusts it back in, and performs a magnificent impromptu Indian war-dance because, during his frantic fiddling with the controls, he turned the volume full on and now doesn't know which to do first—turn down the volume, tear the headset off, pull the jack-plug out again, or simply collapse in a twitching heap on the floor!

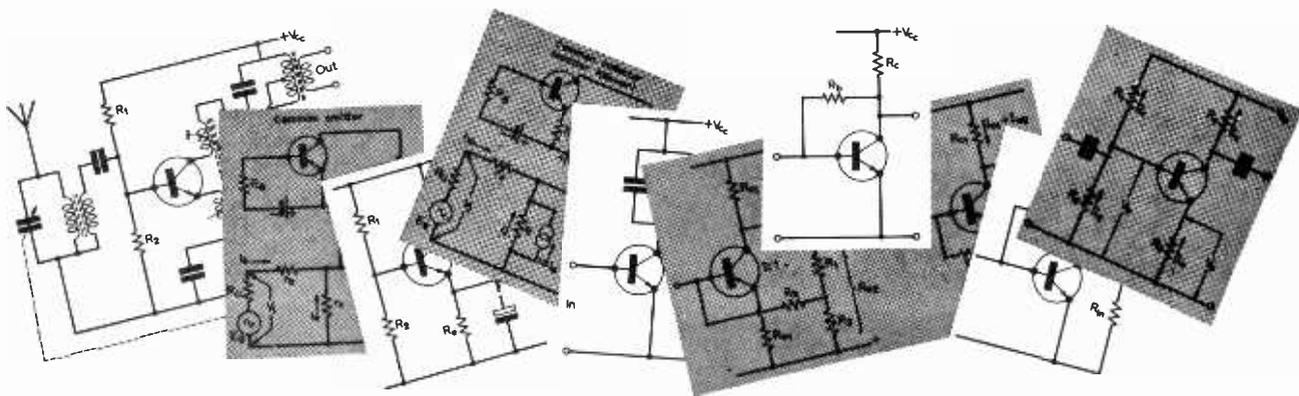
Oh, yes, ladies. Shortwave radio can be fun.

Then there's the "*helping husband in the shack*" act. Any XYL can do this, no previous experience required.

When he has spent half an hour searching for a certain component which he "had in his hand not two minutes ago", and it's the only one of that kind that he has, and the shops are closed so he can't get another till Monday; that is the moment at which the loving, devoted and helpful XYL enters the hallowed precincts and retrieves said component from floor/tobacco tin/inside of radio chassis/shirt pocket/hip pocket/coffee mug. The XYL then places the component quietly, unobtrusively and without comment, on the bench and beats a strategic retreat.

She is also handy for testing electrolytic capacitors, to see if they are safe or not. "*Just touch this, darling, and tell me what you feel.*" Or for holding a tiny part in a restricted space while the expert solders blindly. And heaven help her if she is weak-willed enough to allow the "slight warmth" at her finger-tips to force her to relinquish her grip, thereby breaking the delicate joint.

Painful? I wouldn't ever want to do away with the radio shack. It keeps him quiet for hours, so what are a few burnt fingers? ■



TRANSISTOR CIRCUITRY for beginners

PART 10

H.W. HELLYER & MICHAEL HOLLIER

Matching

It is no great hardship to answer letters that begin: "Thank you for your series of articles . . ." and go on to pose a query. More difficult, if only because one is obliged to clench one's teeth and answer as objectively as possible, when someone with an opinion to air uses a criticism of the previous text as an excuse to ride his own hobbyhorse. But, answered they must be, so let's begin with the pleasant task of selecting a letter from Mr. Edward Tarrant of Rochester, as representative of one body of readers, who ask questions on matching.

It has been said that audio engineers would be out of a job if their customers understood the simple rules of matching. They have been expounded before in these pages. In Part 4, for example, dealing with Buffer Amplifiers, I took some trouble to explain some of the difficulties and expound the basic "rule of ten".

To come back to our correspondent: he says that his trouble is one of adding together 'bits of circuits.' He has made up the Fig. 4 complementary pair of the 'Experimenter's Circuit Supplement' of PW January, 1972 and obtained highly satisfactory results and now wants to add the active tone control circuit, Fig. 102, Page 131 of the Mullard 'Transistor Audio and Radio Circuits', but is worried because the output impedance of the latter is only 180Ω. 'Can one follow it with a common-base stage?' he asks.

Well, yes, one can—but why should we go to that trouble? Input impedances of the PW circuits are in the region of 30,000Ω and over. Just as the amplifiers we have described, and have built for this article, sport a low output and high input impedance. That, Mr.T. is the whole point. Basically, one can match a low impedance output into a high impedance input of the succeeding section of equipment without too much bother.

There are exceptions, true; no use sticking the very low Z of the mains supply into the very high Z of your crystal microphone socket unless you want your tape recorder to go up in smoke. But, if it is

millivolts to millivolts, i.e., small signal handling devices, then the 'rule of ten' can be invoked more often than not. This is to say that an output will safely match into an input which has an impedance of ten times or more than itself. So our 10kΩ output wants to 'see' at least 100kΩ. And, in Mr. Tarrant's case, 180Ω is very well catered for by upwards of 30kΩ.

It is not, repeat NOT, a matching rule that like equals like—that a 5kΩ output has to be matched into a 5kΩ input. If you stop and think about it, those conditions will cut the available voltage exactly in half. And, as one of the ideas behind this series was to produce those handy buffer-links that allow us to squeeze the utmost from a source that may be delivering barely enough output, then you can see what a mistake such 'exact' matching would be.

To take a practical example: loudspeaker matching. An amplifier is rated at X watts into 8Ω. So it wants to 'see' an 8Ω nominal load to produce that power. But take a close look at an output circuit and you will see that its actual impedance is more like a fraction of an ohm. In fact, one of the designer's aims is to get it as low as possible to derive the greatest power and efficiency.

So to repeat: match up! And if, like Mr. Tarrant, you are 72 years old, then I salute you, and hope that I shall still be enjoying the thrills of construction when my three-score years and ten have been rung up!

Adding stages

So, for that matter, does Mike, who has been sweating away over a tepid soldering iron, producing a direct-coupled circuit to illustrate this month's argument. He has a little farther to go to reach the Biblical milestone, but, wise beyond his years, suggests we explain at this stage what we are getting at. 'You know, I know, and perhaps the Editor may know,' he says, but the series of articles has entered its decade and we are still scratching around at fundamentals, so let's explain why!

It is possible to take someone else's evolved circuit and build around it, taking for granted the basic design work, and come up with a beautiful piece of electronic wizardry that all your friends will admire.

This is, fundamentally, what our other typical correspondent, Mr. E. F. Good, from Malvern, has complained about. In Part 7 of this series we described the Darlington Pair transistor, and gave some of the calculations from which it was derived. This, we thought, was a legitimate demonstration of the evolution of transistor circuitry, from which the beginner could see where the application of the rules we had laid down might be leading him. The insertion was a legitimate 'leader'—but Mr. Good took exception to it.

'You do let your enthusiasm carry you away,' he complained. The only place where he would be likely to use it would be as part of the triples of a power amplifier. In other positions, a pair of opposite conductivity would be more suitable and would cost only a little more. 'A manufacturer's economics are different.'

Well, of course, Mr. G., but give us credit for some insight: we are coming to the complementary pair. All in good time. This series is for the beginner, which your letter shows you not to be. Palpably, for you complain that our circuit that was intended to get the best from a crystal microphone could have been better served by a j.f.e.t.

That is true, but, I beg leave to argue, irrelevant. Until we have got the hang of simple circuitry, there is no point in progressing to more sophisticated devices. Much of the rest of this long letter, picking out points from preceding articles—in no sequential manner, either—has been dealt with in Part 9. Some wrongly captioned drawings have been explained. Some omitted references (for simplicity) have been taken up, and there is one formula in which no account was taken of r_o , because we did not at that point want to confuse beginners: we have since dealt with that subject.

Mr. Good ends his letter with the statement: '... instructing beginners is the most responsible job one can undertake, and should be performed with the greatest possible care.'

Agreed, Sir, so without more ado we shall go on to discuss the biasing of BC109 transistors, with particular reference to the modifications necessary in our thinking when we add two stages together.

Coupling up

It is possible, in theory, to cascade similar circuits like erected chains of dominoes. But if we do, taking no account of voltage swings, etc., our amplifying edifice is likely to fall down. When this series was being discussed, the Editor wanted us to call it 'Building Bricks', and this example is a case in point. We must consider the composite circuit, the two transistor unit, when we add one stage to another.

Take Fig. 52. Here, we have Tr1 operating as a collector follower, capacitively coupled via C_c to the second transistor, Tr2, working as an emitter follower. Bias for Tr1 is provided by a conventional potential divider, R1 and R2.

The input signal is coupled to base of Tr1 by C_{in} . A measure of gain may be expected from this stage in its collector follower mode. The emitter resistance R_{e1} is bypassed by C_e and the amplified signal at the

collector of Tr1 is capacitively coupled to the base of the following stage. All very good, except that, as some of our correspondents have been quick to point out, the output impedance is higher than would be desirable. So, adopting Mr. Tarrant's suggestion, almost, we use another stage between our Tr1 and whatever we are feeding.

This time, we are not interested so much in the gain—we've got that—but must preserve what we have got and present a low output impedance. So the second stage is operating at slightly less than unity gain in its emitter follower mode, but it does give us a low output impedance. The output voltage is developed across R_{e2} and is coupled to the following stages via C_{out} . The snag? The circuit, as given, is wasteful of components. It is a general rule that extra components in any circuit are extra possible sources of trouble: noise, instability, excessive current drain. So we shall proceed to whittle down the circuit.

To begin with, there is an alternative way of biasing Tr2. Readers of the previous articles will have no trouble in following the train of thought. We have already dealt with the collector follower and the emitter follower circuits. From the information given in past articles, the 'circuit' of Fig. 52 could be derived without much trouble.

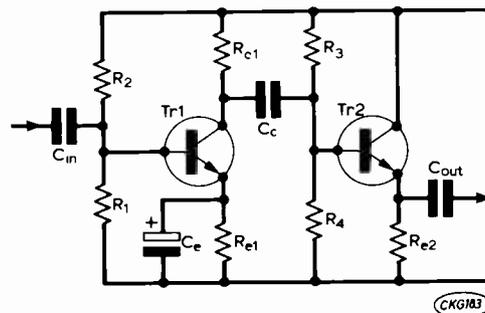


Fig. 52: Two stages already considered, a common emitter (collector follower) stage with an emitter follower stage added to it. The object being to produce a low impedance output while preserving the gain. This method of adding stages is wasteful of components.

Our alternative method is to remove bias resistors R3 and R4 and the coupling capacitor, C_c . We now couple direct: that is to say, the collector of the first stage is taken directly to the base of the second. The result is that the base bias for Tr2 can now be derived from the collector of Tr1. Hence the term 'directly coupled.'

Operating conditions

Calculating the operating conditions is a matter of logical progression, as before. We start with Tr2. We know the transistor characteristics—we have dealt with the BC109 before. We know the supply voltage and the 'rail' voltage, V_{cc} , which we shall adjust to 8 volts by manipulation of the series resistor, R_{dec} , through which all the current in the circuit flows, Fig. 53.

The things we do not yet know, and which we shall have to define, are the load at the output and the drive voltage at the input.

Remembering what we have said about matching already, we shall define the 'worst case' load. If we decide that the maximum r.m.s. output voltage we

require is, say, 200mV (0.2V), and that the *minimum* impedance into which our circuit can feed is 5kΩ, we have some more guidelines to follow. Next thing we want to know is the peak voltage—remember, it is the voltage swing that gives us the operating voltages, i.e., defines our limits.

Here, we have $0.2V \times 1.414$ (Peak = r.m.s. $\times \sqrt{2}$) = 0.2828V peak.

For a 300mV r.m.s. output, we shall need $0.3 \times 1.414 = 0.4242V$ peak, and this is the value we shall choose.

To calculate the current which will be driven into our minimum load of 5kΩ, we divide our peak voltage by the load impedance,

$$\frac{0.4242}{5000} = \frac{4242}{50} \approx 82\mu A$$

To allow for a safe margin, we should operate Tr2 at an emitter current of five times or more than this. A convenient emitter current to use in calculations would be 1mA.

We know that, for a BC109, the h_{FE} (d.c. current gain) at a collector current of 1mA is 380. We know the collector current, and can now say:

$$I_b = \frac{1mA}{380} = \frac{100\mu A}{38} = 2.6\mu A$$

The collector current of Tr1 should be four or five times greater than this. To get a more satisfactory h_{fe} (a.c. current gain), we shall choose a collector current for the first transistor of 200μA. Again, plenty in hand. In comparison with the base current of Tr2, this collector current of Tr1 is very large, and the effect of I_{b2} on the load of Tr1 can be ignored in our calculations.

$$\text{This load, } R_c = \frac{V_{cc} - V_{c1}}{I_{c1}} \text{ or}$$

$$R_c = \frac{8-4.6V}{200(\mu A)} = \frac{3.4}{200(\mu A)} = \frac{34,000}{2} = 17,000\Omega$$

The nearest preferred value is 18kΩ.

Emitter voltage

Referring back to Part 9, a table was given to show the effects of a spread of emitter current, resulting from changes in H_{FE} and V_{BE} , for alternative supply voltages. From this, we can say that to get good stability with our given circuit we need an emitter voltage somewhere around 3V for Tr1, if we use potential divider biasing, as here.

If Tr1 is to operate with an I_e of 200μA, we know that the emitter current will only be a little less than this. We shall ignore the effect of the relatively small base current for this calculation. (This is no trick of convenience, as one accusing reader expressed it! Simply that if we wasted our time calculating to the minutest figure, the resultant resistor values would not be available. The variations due to these current differences come within the preferred value 'spread' of resistors we propose to use.)

So, if you will grant us this much dispensation, ignoring I_{b1} , we will calculate R_{e1} as

$$\frac{V_{c1}}{I_c} = \frac{3V}{200\mu A} = \frac{3 \times 10^6}{200} = 15k\Omega$$

a preferred value of resistor.

Voltage gain

The d.c. voltage gain, A_v , of Tr1, ignoring the effect of r_e , the internal emitter resistance (if Mr. Good will allow us to do so!), can be calculated from the collector load resistance divided by the unbypassed emitter resistance. That is,

$$A_v = \frac{18,000}{15,000} = 1.2$$

From a knowledge of the d.c. current gain of Tr1, which is operating at a collector current of 200μA, we can calculate the true base current of the transistor. h_{FE} of a BC109 at a collector current of 200μA is typically 280.

$$I_{b1} = \frac{I_{c1}}{h_{FE1}} = \frac{200\mu A}{280}$$

which works out to approximately 0.7μA.

The emitter voltage of Tr1 has already been

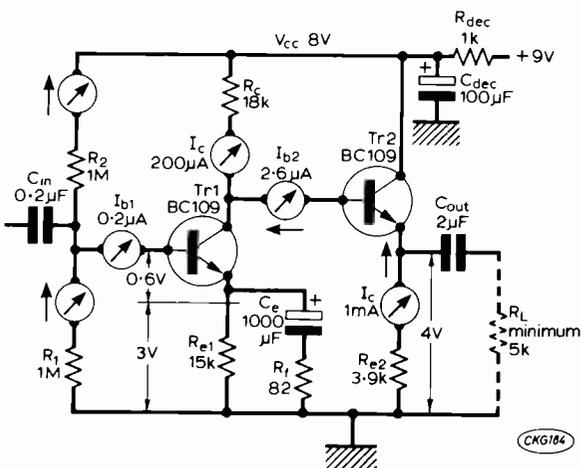


Fig. 53: A practical direct-coupled circuit. Linearity is good and distortion very low.

Operating Tr2 at an emitter current of 1mA and with an emitter voltage of 4V (half V_{cc} , which is 8V), giving us a swing of 8V, peak-to-peak, again a good margin of safety is obtained.

Using Ohms Law, we calculate the value of R_{e2} .

$$R = \frac{V}{I} \text{ or } \frac{4V}{1mA} = \frac{4000}{1} = 4,000\Omega$$

The nearest preferred value of resistor will be 3.9kΩ.

From the graphs

Turning now to the base conditions of Tr2. We have already said that bias is derived from the collector of Tr1 (see Fig. 53). We know that a silicon transistor such as the BC109, when forward biased, will have a voltage of 0.6V developed across the base-emitter junction. If we add this to the emitter voltage of Tr2, we get an expected base voltage of 4.6V, and so can say that the collector voltage of Tr1 will be the same, since the two transistors are directly coupled.

To calculate the base current of Tr2, we need to refer to the graphs which have previously been

published, remembering that $I_b = \frac{I_c}{h_{FE}}$

worked out: the base-emitter voltage will be 0.6V, as explained before; we shall aim at a current through the potential divider network, R1, R2, of five times the base current of Tr1.

Calculating R1, the lower resistor, this equals:

$$\frac{V_{b1}}{5 \times I_{b1}} = \frac{3.6v}{3.5\mu A} = \frac{36 \times 10^6}{35} = 1.03M\Omega$$

And again, the nearest preferred value will be chosen, 1MΩ.

The current flowing through R2 is the base current of Tr1 as well as this base current multiplied by five, which we decided as our desirable current through the potential divider. In other words, $6 \times I_b$.

$$\text{So, } R2 = \frac{V_{cc} - V_{b1}}{6 \times I_{b1}} = \frac{8 - 3.6V}{4.2\mu A}$$

again working out approximately to 1MΩ.

Input resistance

In this context, we refer to transistor input resistance, which, in the case of the input resistance to the base of Tr1 is the effective emitter resistance of the transistor plus the effect of the unbypassed resistor.

Calculating first the internal emitter resistance of Tr1, we have the formula:

$$r_e = \frac{25}{I_c \text{ (mA)}} = \frac{25}{0.2} = 125\Omega$$

R_{in} , ignoring R1 and R2, is equal to the effective emitter resistance plus the internal emitter resistance, multiplied by the a.c. current gain, $(R_{eff} + r_e) \times h_{fe}$.

Let's backtrack. Referring to Fig. 53, we bypass R_{e1} with a whacking great capacitor. Now, the stage gain

is going to be determined by $\frac{R_c}{r_e}$. We can't do much

about R_c without mucking up the d.c. conditions (to quote verbatim from Mike's notes). If we want to modify the stage gain, therefore, we have to find an alternative way of doing it, and the solution is as shown in the drawing, a resistor, R_f , in series with a large value of capacitor, C_e , both across the emitter resistor, R_{e1} .

Now we find that R_f cannot affect the d.c. conditions. The amount of feedback in the circuit will depend on the sum of the feedback resistor, R_f , and the internal emitter resistance of the transistor, r_e . We have already agreed that r_e is 125Ω. If we make R_f 82Ω, the total emitter resistance (as far as a.c. is concerned) will be $82 + 125 = 207\Omega$.

Our stage gain will be controlled by the formula:

$$A_v = \frac{R_c}{R_f + r_e} = \frac{18,000}{207} = 87$$

Reverting to the point where we backtracked and putting in our value of feedback resistor for the effective emitter resistance, we get an input resistance of $R_{in} = 207 \times 360$ (the h_{fe} from the curves for the BC109) = 74520.

Having got the input resistance of the transistor settled, we can calculate the input resistance of the stage, which, you may remember, is obtained from the following formula:

$$\frac{1}{R_{IN}} = \frac{1}{R_{in}} + \frac{1}{R1} + \frac{1}{R2} = \frac{1}{74.5k\Omega} + \frac{1}{1M\Omega} + \frac{1}{1M\Omega} = 65.2k\Omega$$

Gain control

We can see that the gain of the circuit is obtained by altering the feedback resistor but this also affects the input resistance. Work out a few alternatives for yourself. When you do so, one fact will strike you: that is the major controlling factor of R1 and R2. We have already seen that there are decided limits to the amount of juggling that can be done, so in the next article we shall dispense with this pair of resistors altogether and show how the bias for the base of the first transistor can be derived from a single resistor fed from another part of the circuit.

Results

The final circuit, built up on 0.15in. matrix Vero-board gave us a measured gain of 90 (calculated 87), the input resistance was higher than calculated, and the output resistance when the circuit was fed from a low impedance source was approximately 522Ω. The output, measured and viewed on the oscilloscope, was 300mV.

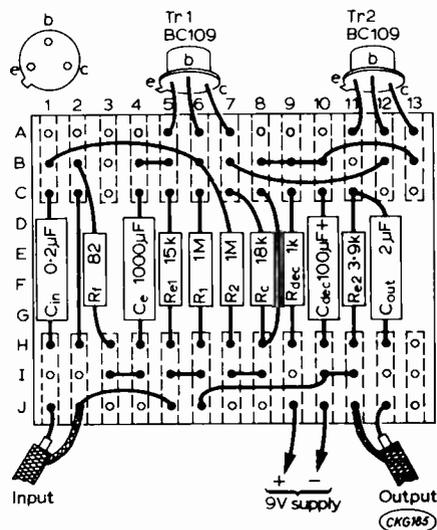


Fig. 54: Suggested layout of Fig. 53, on a 0.15in. matrix Vero-board.

Power supply details are as before, calculating R_{dec} to drop 1V from the sum of the various currents we have already considered, and decoupling with a large electrolytic to prevent the audio signals from modulating the supply. Coupling components are chosen from experience rather than calculated in exact detail. An input coupling capacitor could be 0.2µF and for an output coupling capacitor, 2µF might be chosen.

TO BE CONTINUED

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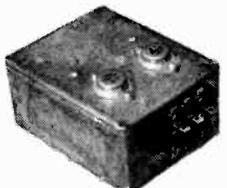
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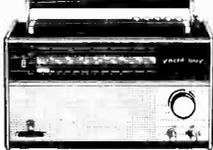


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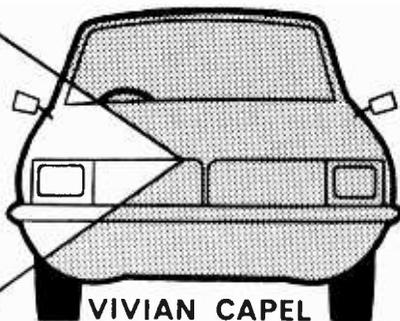


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CAR RADIO INSTALLATION



PART 2

THE main source of engine interference is, as we have said before, the distributor. Suppression is achieved by inserting resistance in the central high-tension lead from the coil. Modern British cars already have this fitted, often it takes the form of a resistive carbon brush for the rotor contact. No additional suppression should be fitted. In the case of older cars, and some of foreign manufacture, a suppressor should be fitted as a routine job when installing the car radio. A value of $10k\Omega$ is suitable which can be of the screw-in or cut-lead type, whichever is the most convenient.

The coil

The next point to consider is the ignition coil. This can generate interference which can be suppressed by fitting a $2\mu F$ capacitor. This should be of the metal-cased type, the case being secured to the car bodywork as near to the coil as possible. The capacitor lead, which must be kept as short as possible, must be connected to the low-tension lead coming from the ignition switch.

One type of capacitor-suppressor which is specially suited for this application, is the co-axial type. This is similar to the lead-through capacitors often found in television tuner-units. The metal case is clamped to the car bodywork, or better still the metal case of the coil, one connection is taken to the ignition switch-lead and the other to the coil. Thus the low-tension supply to the coil passes through the capacitor casing which thereby forms an effective barrier to interference pulses. The two capacitor leads must be kept as far apart as possible to prevent any inductive coupling to bypass the capacitor.

Dynamo suppression

Next, comes the dynamo. Again, interference can arise from this component, and a metal-cased ordinary or co-axial capacitor suppressor of $0.5\mu F$ should be used. What has been said about earthing the case and keeping leads short applies here too. Two leads come from the dynamo, one is the field-coil connection and the other is the output lead. On no account should the suppressor be connected to the field terminal as actual damage could result. One method of identification as to which is which, is that the field coils carry much less current than the output lead from the armature and so is wired with much thinner wire. The suppressor then, must be wired to the thick-wire connection.

We have described the three suppression points which should be attended to as a matter of routine on every car-radio installation. In most cases it will be found that interference is down to a very low level and the installation can be considered successfully completed. There are though the stubborn cases, and we will now see what can be done to silence these.

Stubborn cases

It may be that you are fitting a radio in a second-hand car that previously had a radio which was removed by the previous owner. Do not assume that the three points we have described were properly suppressed, check each one. Some garage mechanics have a habit of disconnecting or removing suppressors when looking for faults. In most cases the aerial will have been left on the car and of course this will be used in the new installation. As the majority of faults are attributable to the aerial, always check it in case of persistent interference. Check that the circuit from the aerial-rod to the radio-plug is continuous with a meter or other type of circuit tester. Check that the screening goes all the way and that there is no break or badly made join. Check that there is no leakage between the aerial and screen, and that the screen is a dead short to the bodywork.

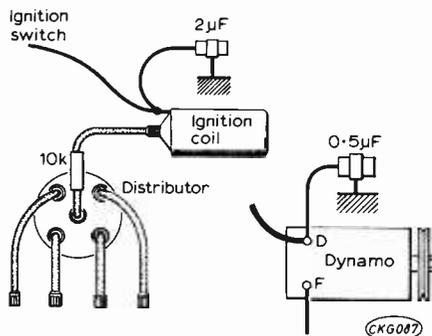


Fig. 2: Three routine suppression points for all radio installations.

Check that the part of the body that the aerial is mounted on and therefore the part that the screen is earthed to, is in fact in good electrical contact with the main bodywork. Sometimes new wings are fitted that are primed with undercoat before being bolted into place, and therefore make poor electrical contact. Lastly, check that all sections of a telescopic

aerial are in good contact with each other. Oxidization sometimes prevents this and the bottom section is 'on its own' with poor, if any, contact with those above it, thus resulting in a short aerial length, poor signal pickup and degraded signal/noise ratio.

If interference persists we must look elsewhere for the trouble. Cases have been known where after the most careful and extensive suppression the trouble has remained, and the cause has been traced to a burnt and pitted rotor-arm. It is worth replacing it if in doubt. Similarly the high-tension terminals in the rotor head may be worth checking and cleaning up.

If all is in order here, the plug leads may be radiating. A set of $5k\Omega$ resistive suppressors can be fitted, one in each plug lead, as near to the distributor as possible. It may even need a second set wired close to the plugs. Some makers use resistance wire for the plug leads and if this is the case (as can be checked with the meter) no further resistance will be of much help. Actually these resistive leads are better than wired-in suppressors, because the resistance is distributed along the complete length. Special h.f. filters may prove the answer.

It is assumed that the plugs themselves are in good condition, and of course these should be replaced at the stipulated intervals in the interests of petrol economy and engine performance. Old and worn plugs can cause interference, so if yours are due for a change, try a new set before getting too involved in suppression methods.

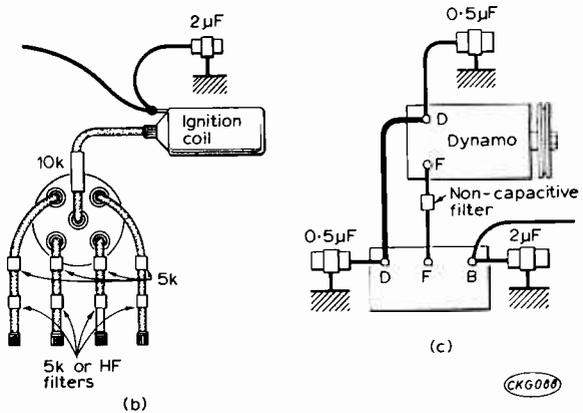
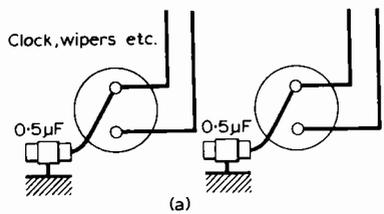


Fig. 3: All possible suppression points. Rarely necessary except in stubborn cases or FM radios.

Other interference

Any interference that yet remains will very likely be due to causes other than the high-tension ignition circuit, if all the measures here described have been taken.

This can be ascertained by revving up the engine and then switching off the ignition. Any interference arising from the ignition circuits whether low or high-tension will immediately cease. Any noise that continues as the engine slows down and stops must therefore be due to the dynamo or voltage-regulator. If it is still the ignition circuit that is giving the trouble, about the only thing left is inductive coupling between the l.t. ignition circuit and radio leads. One possibility that has been known, is coupling between the car wiring to the ignition-switch and the radio loudspeaker leads. Moving the latter may improve things, but in stubborn cases it sometimes pays to rewire the speaker with screened-cable. Some radios already have screened loudspeaker wire fitted by the makers, but often the screening is earthed to some point inside the metal case of the radio. Thus if any r.f. interference pulses are picked up by the screen they will be conducted inside the radio, and possibly affect the r.f. circuits. A worthwhile move is to disconnect the internal earth and to earth the screening to some external point on the case.

If in fact, the engine rev test eliminates the ignition circuits, we can absolve the dynamo if it is properly suppressed as we have described. This leaves the voltage regulator. It is usually easy to tell if interference is coming from this source because the sound has quite a distinctive character. It has what can best be described as a chattering sound, and it seems to affect the long-waves more than the medium waves.

Suppression will usually be effected by the connec-

tion of a $2\mu F$ capacitor to the regulator terminal that goes to the battery. Do not connect it to the one that goes to the dynamo field coil.

If the main engine interference has been suppressed, as indeed it should be after the measures we have described, there may be a residual noise, especially with installations that have the aerial mounted at the front of the car. We have seen that this is more probable than those with rear mounted aerials, but in some cases the level may be higher than it should be. One possible reason for this is that the bonnet is not earthed electrically to the rest of the car. Thus its shielding effect is poor and the aerial is exposed to direct radiation from the engine. A couple of jumpers of copper braiding should be connected across the hinges to provide a low-resistance earth-path.

There are other causes of radio interference besides the engine and its necessary subsidiaries. A common one is the ticking of the electric-clock and the whine of windscreen-wipers. Fortunately, the cause is self-evident, and all that needs to be done is to fit a suppressor to the offending item. A metal-cased $0.5\mu F$ should suffice as long as it is fitted as close to the accessory as possible with the shortest leads to it and to earth.

There is one final source of interference which has nothing to do with the car's electrical system, and this is static. It is easily identified because it is not present when the car is stationary, even though the engine is running, and it is present when the car is coasting with the engine switched off.

Although thus easy to recognise, it is not so easy to find the precise cause and effect a cure. It is generated by some part that is in poor electrical contact with the rest of the bodywork, and the problem is to find out which one. A common cause is the tyres; friction builds up an appreciable charge which then leaks through various paths producing the interference.

One possible cure, is the dangling-chain which a

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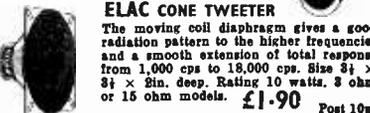
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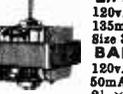
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1B5	6BH6	75	6J7G	40	7D6	60	19AQ5	50	50B5	50	DC90	\$1-35	EC81	35	EL43	25	OC3	38	FL603	95	UBC41	50	
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1B5	6BK7	40	6K7M	35	787	\$2-25	20L1	\$1-10	50CDA6	\$1-20	DF70	45	ECC83	30	ELL90	\$1-00	PC88	60	PX25	\$2-50	UBF80	40	
1N5GT	6BR8	70	6K7G	35	7Y4	65	20P4	\$1-10	50	20P5	50	DF92	50	ECC84	30	EM80	45	PC88	60	PY33	45	UBF99	35
1N5GT	6BR8	\$1-30	6K7GT	35	9BW6	60	20P5	\$1-10	75	50	DF96	45	ECC85	40	EM81	60	PC97	50	PY81	30	UCB84	48	
1R5	6BW6	35	6K8M	60	10C2	85	25A6	35	80	55	DH3-91	\$7-00	ECH21	65	EM84	35	PC94	40	PY82	30	UCB85	60	
1R4	6BW7	30	6K8Q	40	10P1	75	25L6GT	50	85A2	40	DH7	35	ECH21	65	EM84	35	PC94	40	PY83	38	UCB86	60	
1R5	6C4	33	6K8GT	50	10P8	90	25V5	65	150B2	60	DK32	45	ECH42	75	EZ35	40	PCF80	55	PY600	\$1-00	UCH42	70	
1T4	6CB8	35	6K8Q	50	10P9	80	25Z4	60	160C4	60	DK91	40	ECH81	30	EZ40	50	PCF82	35	PY801	50	UCL82	35	
2A4	6CB8	25	6L8G	40	10P18	50	25Z5GT	55	801	60	DK92	55	ECH82	45	EZ41	50	PCF84	40	R2	75	UCL83	60	
2Q4	6CD6G	\$1-25	6L18	45	10LD11	65	25Z6	65	807	50	DK96	50	ECL80	45	EZ80	27	PCF86	60	R19	50	UCL84	60	
3Q5	6CQ6	60	6Q7G	40	10P13	60	30C1	30	813UBA	\$3-75	DL66	\$1-25	ECL82	35	EZ81	25	PCF87	50	SP4	\$1-75	UF89	40	
3B4	6CQ4	65	6Q7GT	42	11E3	\$4-00	30C15	80	866A	75	DL92	35	ECL83	70	EZ82	40	PCF89	50	SP4	60	UL41	65	
3V4	6D6	45	68A7M	40	12A7E	30	30C17	90	854	60	DL93	40	ECL84	40	EZ83	40	PCF90	50	SP41	60	UL84	40	
5R4G	75	6E5	60	68C7M	75	12AT7	35	30C18	80	1825	55	DL94	48	ECL85	40	EZ84	50	PCF91	55	SP42	75	UM80	30
5Y4G	45	6F3G	70	68G7M	40	12AT8	35	30P5	85	4022AR	\$5-50	DL95	50	ECL86	40	EZ85	50	PCF92	55	SP43	75	UV80	30
5Y3GT	40	6F8G	35	68J7GT	30	12AX7	30	30FL12	\$1-20	7193	30	DM70	45	EF9	75	HN309	\$1-60	PCF82	35	STV280/80	UU6	\$1-75	
5Z4G	40	6F8G	50	68K7GT	40	12AR6	40	30FL14	85	7475	30	DY86	35	EF37A	\$1-20	K736	\$1-00	PCF83	65	STV280	UU8	\$1-75	
6/30L2	80	6F11	40	68L7GT	35	12B6GT	40	30L16	85	A81	48	DY87	35	K761	\$1-55	PCF84	65	STV280	UU9	UU8	\$1-75		
6A7	75	6F13	45	68N7GT	35	12C6GT	35	30L17	85	ATP4	45	EM80	25	K761	\$2-05	PCF85	40	T41	\$1-00	UY21	50		
6A8G	40	6F14	70	68Q7M	40	12E1	\$2-30	30P4	\$1-15	ATP6	60	EAD0	20	K761	\$1-75	PL86	45	TD14	60	UY41	48		
6AK5	35	6F23	55	6H40T	55	12E6GT	30	30P12	80	AT17	60	FA8C90	35	K788	\$2-00	PEN44	\$1-00	U14	75	VMP4G	85		
6AM5	35	6F25	55	6U5G	40	12F7GT	30	30P19	85	AU2	\$4-00	EA42	55	K788	\$2-00	PEN45	75	U25	80	VP43	\$1-25		
6AM6	35	6F25	\$1-00	6V6M	60	12K7GT	40	30PL12	75	AU5	75	EB91	20	K788	\$2-00	PEN46	40	U26	80	VR105/30	35		
6AM6	35	6F28	65	6V6G	30	12K8GT	40	30PL13	75	AZ1	55	EB33	50	K788	\$2-00	PEN47	40	U27	80	VR150/30	35		
6AQ5	35	6F32	25	6V6GT	40	12Q7GT	40	30PL14	90	AZ31	55	EB34	55	K788	\$2-00	PEN48	40	U28	80	VR150/30	35		
6A87G	35	6G6	25	6X4	35	12Q8GT	40	30PL15	90	35A5	75	EB35	55	K788	\$2-00	PEN49	40	U29	80	VR150/30	35		
6AT6	35	6H6	28	6X5G	40	12S07	35	35L6	55	35L6	55	EB36	55	K788	\$2-00	PEN50	40	U30	80	VR150/30	35		
6AU6	25	6J5M	50	6X5GT	40	12SH7	35	35Z3	70	CY30	65	EBF89	30	K788	\$2-00	PEN51	40	U31	80	VR150/30	35		
6B4G	\$1-00	6J5G	20	7B6	70	12S7	40	35Z4GT	60	CY31	48	EBL1	\$1-00	K788	\$2-00	PEN52	40	U32	80	VR150/30	35		
6B8G	25	6J5GT	30	7B7	70	12SK7	50	35Z5	60	DCA32	50	EBL2	\$1-00	K788	\$2-00	PEN53	40	U33	80	VR150/30	35		

All prices in pounds and new pence

Transistors

1N914	07	2N3702	10	BFY50	22	0A91	07	OC170	25
18113	25	2N3819	10	BFY51	20	0A211	30	OC171	30
18202	25	2N4289	15	BY100	15	0A2301	50	OC200	40
2G309	25	AAZ12	30	BZY88	15	0A2507	45	OC271	37
2G371	25	AC126	20	CR81-40	45	0A2510	35	ORP12	60
2N404	20	AC127	25	DD003	15	0A2922	45	Z8170	10
2N697	15	AC128	20	GET102	30	0A2924	45	Z8178 P on A	7401
2N706	10	AC129	30	GET882	25	0A2941	25	ZTX107	15
2N1132	25	ACY39	50	GJ7M	37	0A2942	25	ZTX108	18
2N1305	25	AD140	50	KR100A	20	0A2946	25	ZTX300	12
2N2147	75	AD149	50	MJE290	87	0A2955	60	ZTX304	15
2N2160	60	AD161	37	MJE2955	87	OC44	17	ZTX500	16
2N2218	20	AF115	25	NKT212	27	OC45	12	ZTX503	17
2N2219	20	AF117	25	NKT214	15	OC57	60	ZTX531	25
2N2369A	15	ASV26	25	NKT223	33	OC71	12		7400
2N2444	\$1-01	BC107	10	NKT251	24	OC72	20		7412
2N2646	45	BC108	10	NKT713	25	OC81	20		7413
2N2904	20	BC109	10	OA70	10	OC82	25		7416
2N2926	10	BC169C	15	OA71	10	OC82	25		7417
2N3055	75	BF898	25	OA85	12	OC84	25		7420

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7438	65	7474	40	7494	75	74123	\$2-70	74176	\$1-50
7440	20	7476	55	7495	80	74141	\$1-00	74190	\$1-95
7441AN	75	7478	45	7496	\$1-00	74145	\$1-50	74191	\$1-95
7442	75	7479	80	7497	\$2-25	74150	\$3-35	74192	\$2-00
7443	48	7480	20	7498	87	74151	\$1-10	74193	\$2-00
7444	48	7481	20	7499	\$1-00	74152	\$2-00	74194	\$2-50
7445	42	7483	20	7500	75	74110	30	74195	\$1-35
7446	20	7484	20	7496	45	74111	\$1-45	74196	\$1-50
7447	20	7485	20	7497	75	74118	\$1-00	74197	\$1-50
7448	20	7486	20	7498	75	74119	\$1-90	74198	\$4-80
7449	42	7470	30	7499	75	74120	\$2-10	74199	\$4-80
7450	30	7472	70	7499	75	74121	\$2-00	74199	\$4-80

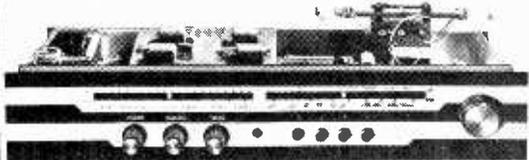
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While the Yaesu Musen FRdx400 receiver is just about the best you can get, in the Amateur Band line, the price of £160 is beyond a lot of pockets, so to cater for the lower-priced field, we very proudly introduce the Yaesu Musen FR-50B at a very incredible £52. In spite of this rock bottom price, the FR-50B is a very good Amateur Band receiver indeed and provides a high degree of sensitivity, selectivity and stability. Basically, it is a double conversion receiver covering 80 to 10m with a VFO, the first oscillator and a crystal controlled second oscillator. Being double conversion (5173.9 kHz and 455 kHz) explains the incredibly good image rejection figure of better than 50 db. When it comes to sensitivity, the 6BZ6 r.f. amplifier ensures 0.5 microvolt for 10 db S/N ratio. Selectivity is achieved by two ceramic transducer filter elements which give a noise band width of 3.6 kHz at 60db and a skirt band width of 10 kHz at 50 db. These figures are extremely good for equipment in this price class (even for equipment costing much more!). A high order of stability is achieved by a stabilized transistor VFO and VFO buffer amplifier. Other niceties of design built in are:— 100 kHz calibrator, speaker, geared VFO drive, "5" meter, product detector.

- Frequency range: Amateur Bands 80-10 plus WWWW.
- Sensitivity: Better than ½ microvolt for 10 db S/N ratio in the 5SB mode.
- Selectivity: 3-6 kHz—6db 10 kHz—50db
- Image rejection: 50 db or more.
- Audio: 1-5W/4600 ohm output. Built-in speaker.
- Power: 240 v.a.c.
- Size: 13" wide, 6" high, 10½" deep.
- Weight: 17½ lb
- Controls: BFO, monitor

few years ago was widely used to prevent travel sickness. It discharges to ground any static that may be built up by the tyres or by the movement of the car body. This can be quite effective in the latter case but not so much in the former because of the rather long path from tyres to the chain. The most effective cure for tyre static is to provide a conductive path from the tyre tread to the car body. Painting the inside wall of the tyres with a conductive paint such as lead paint, or a rubber conductive paint, should do the trick. It is not necessary to paint the whole of the wall, several wide strips will do, providing they are taken from the wheel rims to the tread.

It may be that the wheels themselves are not in good contact with the body due to the wheel bearings. Packing them with graphite grease should make them conductive. Alternatively, special springs that are made for the purpose can be fitted inside the hub-caps. These form a bridge between hub-cap and axle.

In the case of the rear wheels it could be found that the back axle is not in electrical contact with the body, and if this is so it will be necessary to fit a copper-braid jumper from axle to body; the top bolts of the differential housing should prove a convenient anchoring point.

Other parts of the body or engine components can cause static through poor earthing, although it is usually the larger parts. Exhaust systems are a possibility and also the steering column.

From all this it may well be assumed that installing a car radio and suppressing all interference is a major job and one that is not to be lightly undertaken. This is not actually so, rarely will all the measures here described be found necessary, in the majority of cases the three routine suppressors we have before described will be sufficient. However, the stubborn ones do sometimes crop up, and it is hoped that in such an eventuality these tips will prove helpful.

It should be noted though, that f.m. car radios are more troublesome in the matter of car interference than a.m. All the suppression measures here described, except for static, should be carried out as routine when installing one. In addition to these an extra 0.5 μ F suppressor should be connected to the voltage-regulator, this time to the D terminal, and also a special non-capacitive suppressor to the F or DF terminals. As stated before, an ordinary capacitive suppressor must not be connected to the field-coil circuit.

The resistive suppressors used for plug suppression will probably not be sufficient, and special h.f. filters may have to be used instead. ■

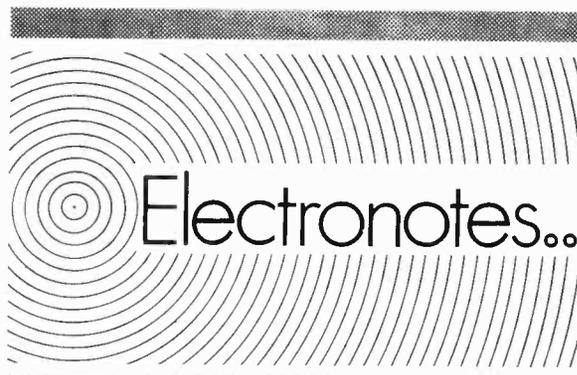


TOP BAND CONVERTER. August 1972

Figure 1. Pin 8 on L2 should be connected to chassis and not to the junction of C2/C3. The wiring in Fig. 2 should be amended accordingly.

TAKE 20. August 1972

VR1 is given as 5k Ω in the circuit and 10k Ω in the components list. Either will work but the circuit is correct and in preference VR1 should be 5k Ω .



S. GINSBERG

ONE of the problems (in certain applications) of using a standard typewriter keyboard to put characters or letters into a computer, is that you are stuck with exactly those characters. Thus a capital letter A is always exactly the same shape, thickness, height etc. It will be the same no matter who presses the key. It would be very useful if one could write, just as with an "ordinary" pen, and have the resultant "shapes" stored. These could be called up onto a visual display unit (v.d.u.) at will and could be transmitted to remote v.d.u.'s at another location. No longer would we be restricted to characters and numbers, and we could, if we wished, send a circuit diagram. It would be possible to send a signature which could be checked and verified by, say, a bank or security personnel.

Well, it can be done. As far as the "sender" is concerned he/she merely writes on a special tablet with an electronic pen. The method has been developed by the Siemens laboratories in Munich. Any handwritten marks may be displayed immediately on a large cathode ray tube or stored in the computer, or transmitted to another computer or v.d.u.

The special writing tablet is a sheet of piezoceramic material. Ultrasonic pulses at about 500Hz are applied to two edges of the plate which are at right angles to each other. The result is that a wave front is generated from each of the two edges. These fronts travel across the plate but remain parallel to their edge of origin.

The pen doesn't write by pressure. It acts as a capacitive probe which reacts with these voltage fronts travelling across the piezoceramic at constant speed. Electronic circuitry interprets the pen's position in relation to the x-y axis formed by the wave fronts. The position of the pen is converted into signals used for the v.d.u. and computer.

Lasers are back in the news again. RCA has built a laser beam image reproducer. It is reckoned to produce film copies of TV pictures with a sharpness improvement of some forty times. The system has a line resolution of something like 20,000 lines. This is a considerable improvement over earlier RCA systems which had resolutions of 6,000 lines.

The other laser story comes from the Mecca of electronic innovation—Bell Laboratories in the U.S. Here, miniature gas lasers have been made which are only two inches long and 0.02in. in diameter. Operating at 6328 Angstroms, the first successful model employed helium-neon discharge. Using glass capillary tubing with a 430 μ m bore, gains of 2.7dBm were obtained.

TAKE 20

JULIAN ANDERSON

A series of simple transistor projects, each using less than twenty components and costing less than one pound to build.

THERE is nothing much wrong with crystal microphones that a decent preamp will not cure. They are not as good as decent moving coil or ribbon types but it needs a discerning listener to notice the difference with one proviso: that the mike is properly matched to a high impedance source. Crystal microphones have got a bad name mostly because they are more often than not fed directly into a simple transistor amplifier with an input impedance of perhaps 10kΩ providing a very bad mismatch. To get the best out of these inexpensive mikes, they must be connected to a really high impedance—at least half a megohm.

Figure 1 shows the circuit which comprises two sections. Tr1 and the associated components give the high input impedance as they are connected as a common-collector (or emitter-follower) stage. The input impedance to such a stage is roughly equal to the emitter resistor multiplied by the gain of the transistor and so we shall find that the input impedance is about 1MΩ which will provide a very decent match to the crystal. Since we are dealing in high impedances we only require a low value coupling capacitor to d.c. block the input, in the circuit this is C1, a 0.1μF capacitor. The base bias for this stage is provided by R1.

The output of this stage will show no voltage amplification, in fact as far as voltage is concerned the output will be marginally less than the input. The transistor has used up its gain in converting the impedance, not in amplifying the signal in the conventional sense. The output from a crystal mike will vary with the type but for our purposes we shall take it as being 1mV. So we shall still be getting only a small output across the emitter resistor R2. To bring this up to a usable level to feed an amplifier we have to amplify the signal further. C2 d.c. blocks the output from Tr1 and this feeds to a series resistor. The function of this resistor is fairly complex but if it is omitted the signal will become distorted, the value is not critical but it will be found to lie around the level of that shown, 3.3kΩ.

This resistor connects directly to the base of the conventional common-emitter amplifier Tr2 which, like Tr1, is a BC109. If this has a gain of 300 the output will be about 300mV, enough to drive pretty well any transistor amplifier. R4 provides the base bias and R5 acts as the collector load and the output is taken from the collector via the capacitor C3. C4 decouples the supply line. The version shown is for a negative earth type circuit but, if it is needed for a positive earth amplifier, all that is necessary is to change the transistors to 2N3702 types and reverse the polarity of the electrolytics. The gain may be slightly less but it should still be more than adequate.

As the input is a high impedance it is important that the input is screened. Crystal microphones are usually provided with a screened wire lead, the

No. 40 CRYSTAL MIKE PREAMP

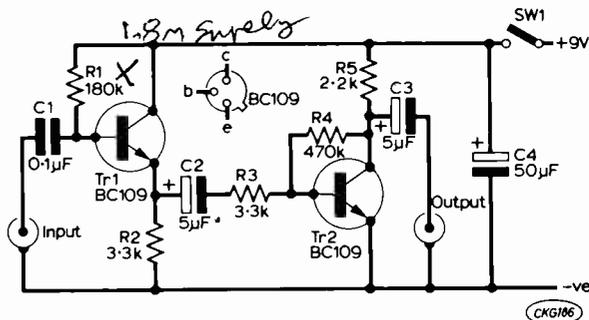


Fig. 1: The circuit of the crystal mike preamp.

★ components list

R1	180kΩ 5%, 1/4W	X 1p
R2	3.3kΩ 5%, 1/4W	1p
R3	3.3kΩ 5%, 1/4W	1p
R4	470kΩ 5%, 1/4W	1p
R5	2.2kΩ 5%, 1/4W	1p
C1	0.1μF mylar or ceramic	4p
C2	5μF 10V minimum	4p
C3	5μF 10V minimum	4p
C4	50μF 10V minimum	4p
Tr1	BC109	10p
Tr2	BC109	10p
SW1	On-off switch	7p
		48p

Prices are those recently advertised and may have changed. No allowance is made for minimum order costs or for postage and packing and these points should be checked carefully before ordering.

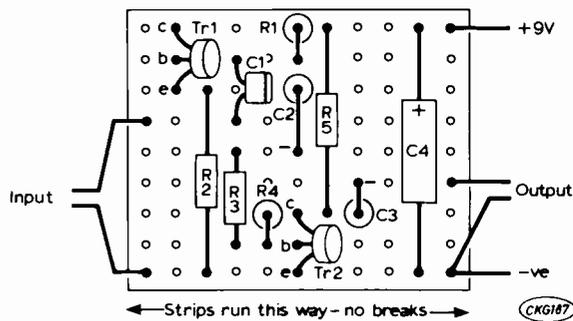


Fig. 2: A suggested component layout.

screening itself should go to the negative line (or positive line if that version is built). The output impedance is about 10kΩ and although this is much lower than the input, a screened wire should still be used between it and the amplifier if it is more than a few inches long.

A suggested layout on a small piece of Veroboard is shown in Fig. 2 but building the circuit up on tagboard is just as good.

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SN7402	0.20	0.18	0.16	SN7452	0.20	0.18	0.16	SN74151	1.30	0.95	0.90
SN7403	0.20	0.18	0.16	SN7453	0.20	0.18	0.16	SN74153	1.35	1.27	1.10
SN7404	0.20	0.18	0.16	SN7454	0.20	0.18	0.16	SN74154	2.00	1.75	1.55
SN7405	0.20	0.18	0.16	SN7455	0.20	0.18	0.16	SN74155	1.55	1.47	1.35
SN7406	0.30	0.27	0.25	SN7472	0.30	0.27	0.25	SN74156	1.55	1.47	1.35
SN7407	0.30	0.27	0.25	SN7473	0.40	0.37	0.35	SN74157	1.80	1.70	1.50
SN7408	0.20	0.19	0.18	SN7474	0.40	0.37	0.35	SN74160	2.60	2.40	2.25
SN7409	0.45	0.42	0.35	SN7475	0.55	0.52	0.50	SN74161	2.60	2.40	2.25
SN7410	0.20	0.18	0.16	SN7476	0.45	0.42	0.35	SN74162	3.40	3.25	2.70
SN7411	0.22	0.20	0.20	SN7480	0.80	0.75	0.67	SN74163	4.40	3.25	2.70
SN7412	0.42	0.40	0.35	SN7481	1.25	1.15	1.10	SN74164	2.75	2.30	2.10
SN7413	0.30	0.27	0.25	SN7482	0.87	0.80	0.70	SN74165	4.00	3.50	3.00
SN7416	0.30	0.27	0.25	SN7483	1.00	0.90	0.85	SN74166	4.00	3.50	3.00
SN7417	0.30	0.27	0.25	SN7484	0.90	0.85	0.80	SN74167	6.25	5.50	5.10
SN7420	0.20	0.18	0.16	SN7486	0.45	0.41	0.38	SN74170	4.10	3.65	3.30
SN7422	0.48	0.44	0.40	SN7490	0.75	0.70	0.65	SN74174	2.00	1.75	1.80
SN7423	0.48	0.44	0.40	SN7492	1.00	0.95	0.90	SN74175	1.35	1.27	1.15
SN7425	0.48	0.44	0.35	SN7492	0.75	0.70	0.65	SN74176	1.50	1.35	1.20
SN7427	0.42	0.39	0.35	SN7493	0.75	0.70	0.65	SN74177	1.60	1.35	1.20
SN7428	0.50	0.45	0.42	SN7494	0.50	0.45	0.40	SN74180	1.55	1.30	1.20
SN7430	0.20	0.18	0.16	SN7495	0.50	0.45	0.40	SN74181	7.00	6.00	5.50
SN7432	0.42	0.39	0.35	SN7496	1.00	0.97	0.95	SN74182	2.00	1.80	1.60
SN7433	0.70	0.61	0.44	SN7497	8.25	5.50	5.00	SN74184	2.40	2.00	1.80
SN7437	0.65	0.60	0.50	SN74100	2.50	2.30	2.00	SN74185	2.40	2.00	1.80
SN7438	0.85	0.80	0.40	SN7492	1.00	0.95	0.90	SN74190	1.85	1.45	1.30
SN7440	0.20	0.18	0.16	SN74105	1.45	1.35	1.20	SN74191	95	85	1.75
SN7441A	0.75	0.72	0.70	SN74107	0.45	0.45	0.40	SN74192	2.00	1.80	1.80
SN7442	0.75	0.72	0.70	SN74110	0.80	0.70	0.60	SN74193	2.00	1.90	1.80
SN7443	1.00	0.95	0.90	SN74118	1.00	0.95	0.90	SN74194	2.50	2.25	1.90
SN7445	2.00	1.75	1.60	SN74119	1.80	1.78	1.65	SN74195	1.85	1.70	1.60
SN7446	2.00	1.75	1.60	SN74121	0.80	0.65	0.50	SN74196	1.50	1.40	1.30
SN7447	1.75	1.60	1.45	SN74122	1.35	1.25	1.10	SN74197	1.50	1.40	1.30
SN7448	1.75	1.60	1.45	SN74123	2.20	2.05	2.47	SN74198	8.00	7.00	3.35
				SN74141	1.00	0.95	0.90	SN74199	4.60	3.70	3.35

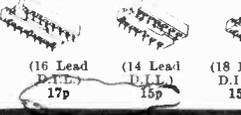
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AC126 25p	BCY32 75p	BY213 35p	OC72 25p	ZTX301 15p	2N3614 50p
AC127 25p	BCY34 35p	C106D 85p	OC77 45p	ZTX302 18p	2N3615 75p
AC128 25p	BCY39 1.00	GET111 55p	OC81 25p	ZTX341 20p	2N3702 10p
AC176 25p	BCY42 30p	GET115 55p	OC83 25p	ZTX500 10p	2N3704 10p
AC187 25p	BCY43 35p	GET880 45p	OC84 50p	ZTX503 17p	2N3705 10p
AC188 25p	BCY52 2.50	GEY093 2.50	OC170 30p	2N400 30p	2N3714 1.00
ACY17 30p	BCY70 1.50	(T03) 1.87	OC171 30p	2N404 20p	2N3771 1.75
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ACY39 55p	BCY87 2.89	MJE370 70p	OC202 80p	2N697 15p	2N3819 35p
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AD162 35p	BD132 80p	MJE3055 1.10	ORP60 40p	2N1131 25p	2N3906 12p
AF117 20p	BF115 25p	P346A 20p	RAS810AF 45p	2N1132 25p	2N4061 12p
AF118 50p	BF167 35p	MPP105 40p	RAS808AF 45p	2N1302 18p	2N4062 12p
AF124 25p	BF173 30p	NKT214 20p	TAA263 75p	2N1304 22p	2N4126 15p
AF139 30p	BF179 25p	NKT216 40p	TIP209 35p	2N1305 22p	2N4871 35p
AF186 40p	BF180 30p	NKT217 45p	TIP209 35p	2N1307 25p	2N5457 30p
AF239 40p	BF194 15p	NKT403 70p	TIP29A 50p	2N1308 25p	2N5777 55p
AS27 30p	BF195 15p	NKT404 50p	TIP30A 60p	2N1613 20p	28001 1.00
AS27 25p	BF861 25p	OA5 50p	TIP31A 60p	2N1671 1.00	28012 10.00
BA102 30p	BF898 25p	OA10 35p	TIP32A 70p	2N2147 75p	28018 8.25
BA115 7p	BFX13 25p	OA81 10p	TIP33A 70p	2N2160 50p	28026 8.80
BA145 15p	BFY90 85p	OA91 7p	TIP34A 1.00	2N2217 25p	28027 50p
BAX13 5p	BFY97 30p	OA200 7p	TIP34A 1.50	2N2220 25p	28033 65p
BAX16 7p	BFX88 20p	OC202 10p	TIP35A 1.50	2N2222A 25p	28234 95p
BC107 10p	BFY60 20p	OC16 75p	TIP35A 1.50	2N2224 25p	40250 50p
BC108 10p	BFY51 20p	OC20 95p	TIP36A 2.50	2N2369A 40p	40360 40p
BC109 10p	BFY82 20p	OC23 85p	TIP36A 2.50	15p 40381 40p	40382 40p
BC109 12p	BFY64 50p	OC25 85p	TIP36A 3.00	2N2906 20p	40392 60p
BC113 15p	BFY90 85p	OC28 85p	TIP41A 75p	2N2926 (all)	40408 50p
BC117 20p	BSX20 15p	OC35 65p	TIP41A 75p	2N2926 (all)	40486 75p
BC143 35p	BSY27 18p	OC42 40p	TIP42A 85p	2N3053 (20p)	40636 1.10
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SC45A	100	85p
SC45B	200	1.00
SC45D	400	1.25
SC45E	600	1.45
15 AMP RANGE (T048)		
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SC50E	600	1.85
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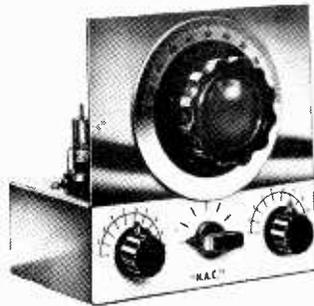
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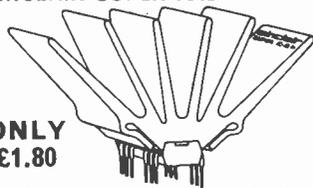
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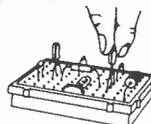
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ON THE SHORT WAVES

MONTHLY NEWS FOR DX LISTENERS

ONE of the many problems faced by the newcomer to the hobby of Shortwave Listening is the bewildering number of abbreviations which are used by more experienced listeners. Contrary to rumour these abbreviations are not used solely to confuse the uninitiated. Every branch of science and technology has its own set of abbreviations and jargon and Shortwave Listening is no exception to this.

To assist the uninitiated I will explain the meanings of some of the more common abbreviations which may be used on this page from time to time.

anncr	Announcer.
Ant	Antenna, aerial.
BC	Broadcast or Broadcasting.
condx	Conditions (propagation).
DX	Long distance reception.
GMT	Greenwich Mean Time.
hrd	heard
Hz	Hertz, measurement of frequency equivalent to one cycle per second.
ID, Ident	Identification.
IRC	International Reply Coupon, sent to help a station with return postage.
kHz	1,000Hz.
LA	Latin American.
MHz	1,000,000Hz.
Mx	Music.
NA	North America.
Nx	News.
QSL	Card sent by a station verifying reception.
rcvd	Received.
Rx	Receiver.
SA	South America.
Sce	Service (Home Sce., Overseas Sce., etc.).
Sched	Schedule.
s/off	Sign off.
s/on	Sign on.
SW	Shortwave.
SWL	Shortwave Listener.
TNX	Thanks.
Tx	Transmitter.
Wrp	Weather report.
Wx	Weather.
Xmsn	Transmission.
Xtal	Crystal.
//	Parallel transmission.

Adrian R. Pell has compiled the schedule of Radio Bangladesh which reads as follows: —

Address: Broadcasting House, 20 Green Road, Dacca.

THE BROADCAST BANDS

Malcolm Connah

Frequencies in kHz ● Times in GMT

Stations:

kHz.	m.	kHz.	m.
9690	30·96	15335	19·56
11620	25·82	15520	19·32
11650	25·75	17925	16·74

Programmes in English (Overseas Service):

0230 - 0300 GMT on 9690 and 15520 kHz.
1230 - 1300 GMT on 11620 and 17925 kHz.
1715 - 1800 GMT on 11650 kHz.

Listeners' Letterbox: Saturday at 1230, Sunday at 1715, Wednesday at 1230 and 1715.

Adrian also sent in the following log using his VEF 204 receiver:

7210 ICRC, Geneva via SBC at 1705.
9745 R. Baghdad, Iraq, s/on at 1930.
11650 R. Bangladesh at 1740.
11930 VOA, Okinawa, s/on at 2200.
11955 FEBA, Seychelles at 1730.
15335 R. Bangladesh in Bengali at 1430.
15520 R. Pakistan at 2050.
17705 VOA Monrovia, s/off at 0830.

Ian Howes of Lowestoft has used his R209 Mk. II receiver and TV antenna to log the following stations:

3265 R. TV Congolaise, local Mx. at 2015.
3380 Malawi BC, local language at 2020.
4800 R. Lara, Venezuela, Spanish at 2345.
4880 Kinshasa, Congo local Mx. at 2315.
4940 Abidjan, Ivory Coast, local Mx. at 2320.
15245 R. Australia, ID in English at 2100.
15300 HCJB, Quito, Ecuador at 2030.
15345 TWR, Bonaire in Spanish at 2328.

R. Cooper of Foulden, near Thetford used his Philips 6 valve domestic receiver and a Bush 4 valve domestic to log the following stations:

11750 HCJB, Quito, Ecuador, English at 0830.
11915 BBC, Cyprus relay in English at 1645.
15020 R. Hanoi with Nx. in French at 1830.
15620 WINB, Red Lion at 2120.
15795 R. Nacional, Brazil, Mx. at 2010.
21500 RSA, South Africa, Nx. in English at 1000.

Richard Witney of Braintree is only 14 years old and is to be congratulated for sending in the following log:

6185 Radio Norway, Oslo at 1825.
7135 TWR, Monte Carlo at 1930.
9625 Radio Sweden in English at 1100.
9915 AIR, Delhi in English at 2100.
11725 Radio Bucharest, Rumania at 1515.
11910 Bangkok, Thailand at 1150.

Reports should arrive by the 15th of the month and be addressed to me at 5 Ranelagh Gardens, Cranbrook, Ilford, Essex.

SHORT WAVES

THE AMATEUR BANDS

David Gibson, G3JDG

Frequencies in kHz • Times in GMT

NOT a very good month for listening between 1.8 and 30MHz, especially up the h.f. end. It seems that the summer evenings haven't lost their knack of making 20 metres the main dx band and logs indicate that most s.w.l's. appreciated this fact.

David Knott (Middlesborough) enquires about DD3FK. Anyone know if DD works wonders in any other country?

Hands up if you live anywhere near Newtown in Montgomeryshire. Now hands down and get a pen! Seems that there's a newly-formed Amateur Radio Club which welcomes prospective members. All queries to: R. Litten, 512 Maesyrrhandir, Newtown, Montgomeryshire.

Hot tip from **Ian Hotchkiss** (Hatfield) that there is an interesting net on Sundays on about 14300kHz (his dial not very accurate) at 1600 hrs. How's about a quick QRX next Sunday?

Sam Elsdon (Halesowen) has been doing strange things with a 500µA meter, diode and l.s. output terminals. (Never mind, the wounds will soon heal). Sam describes his antenna as "310ft. wire arranged in a sort of tapered square spiral in the loft". He asks, "Is there a name for that?" Well is there? Anyone care to suggest something? Gear, besides the above mentioned "thing" in the loft is, a CR70A and PR40. The 21MHz log for s.s.b. reads: CR3MD, CT1EAL, CT2AZ, F6VAA, FL8MM, JA1LCG, JW7FD, LU5AJ, OD5BA, PY2BC, PY7BF, TN8AU, VP8MM, W7GRH, YV4AGP, 4X4NX, 6W8AL, 9Q5DF.

Big round of applause for **Stephen Worrall** (Stafford). He dared to listen on four metres. Two receivers are in use (anyone tried ham stereo transmissions yet?)—a B44 and FR-DX-400, the latter covering all amateur bands from 160 to 2 metres inclusive. (Cor! Think of winding the front-end coils by hand). Antenna for 70MHz is a four-over-four in the loft. Signals on 4 metres heard from G2FOS, G3LR, G30J, G3ANH, G3A00, G3CDM/P, G3FBW/P, G3JFO, G3JHM/A, G3JUB, G3JXN, G3KSU/P, G3KTH/P, G3LUP/P, G3MWQ, G3NAS, G3NEO, G3OCC, G3OHC, G3OHH, G3OQT, G3OWW, G3PXP, G3RCQ/P, G3TQF, G3TVW, G3UGN, G3VPF/P, G3VPS/P, G3WCS, G3WXI, G3YBY, G4AGO, G4ALE, G4AYU, G5DF, G13GLT, GW3ABR/P, GW3ITZ/P, GW3NWR/P, GW3OXD/P, GW3UCB/P, GW3XFY/M So who says there's nothing on 4 metres?

Up (or should that be down?) on 14MHz, Steve's log reads: CPIKRT, HP9AHD, JA1AEA, JA1AGH, JA3BQF, JA6LAE, KP9AID, KR6DO, 44 VK stations (Wow!), VQ9R, XT2AF, ZL1AFO, ZL1BER, ZL1BHB, all s.s.b. with the same gear except antenna; 75ft. end fed at 20ft.

Alan Smith (Nelson) says he will continue to burn the midnight oil. Also committed to this awful pledge is a 680X and a 100ft. length of wire in the loft. Late night oil burnings to date raised 20 metre smoke signals from: CN8HD, CR4BS, CT1QN, EA3JE, EA6BH, EL2CB, EP2TW, HK4BNC, HK5AZA, HP9JW, IT9SPI, JA6GBB, JX2HK, JY9VO, KZ5SD,

PY8ZAA, PZ1DR, VE1YW, VK2AVA, VK3BCM, VK4SD, VP1BH, YS1MAX, YV5AK, ZD3M, 4X4VB, 5B4CDN, 5W1AU, 6Y5SR, 9K2AL, 9X5VA, 9Y4T. A quick single on 15 metres brought in: AP2DU, EA7GF, JA6WAS, JH1DBU, JH1LZW, KV4FY, K9QFR, OD5CS, SV0WZ, SV0WP, VQ9R, VQ9MC, W9MEL, ZD8FM, ZB2A, ZD3M, 4X4BL, 9K2AL, 9X5VA all s.s.b.

Roger Hunt lives in a road I can't pronounce in Carmarthen. Listening utensil is a CR70A plus PR30. Antenna is a 190ft. long wire, end fed. Happenings on 28MHz include: CR6OZ, PY2DVM, ZS6UR, 9J2DT, 9Q5SF. Down on the dreaded forty, where brave receivers cringe, signals were logged from: PY7BBD, PY8YT, TR8VE, ZD8TS, 4U1ITU, 5Z4LW, 9G1DY. I wouldn't mind living in a road I couldn't pronounce just to hear things like that on 7MHz.

A self-confessed agent of **Charles Molloy** has written in! (Gad, these Medium wave devils are everywhere!) Gorgeous gear includes a FR-DX-400 with an 80 metre inverted V (wot, no dx loop wound on broom handles?). Said agent has purged his soul by listening on 3.5MHz to: CP1DN, CP6FG, CR4BS, CX2AX, KP4AST, KP4AN, KV4FZ, OY7JO, OY9LV, PY1HA, PY2ERS, PY3ABH, PY5CDZ, PY6SL, PY7BFN, VE1WV, VE2AL, VE3PT, VO1CQ, ZD8CS, ZD8RR, ZL4KF, 4X4UF, 3A2EE, 5R8AZ. Even 7MHz produced: ZL4KF, VK2AVA, YN9MQ and 9Q5BG. On two metres using a 6-ele homebrew and the same receiver: G4ART, G8AVH/P, G4BBH, G4BEL, G8BXX, G8CGG, G8CKC, G8DYX, G8FAB, G3ZVC. Name of the convert is **W. Waldron** (Cwmbran). Welcome home, brother Bill.

Alan Harper (Manchester) has a VEF204 receiver (I thought it was a new prefix for Rockall). Being b.f.o.-less, he uses a second receiver to get a beat note. Careful adjustment gave readable s.s.b. signals from CR6EM, EA5KR, HC1JB, HP1GS, KV4AD, PY2FCD, W8GL, ZF1WE, 4X4HT, 5N2ABG, 8P6DV, 9H1CV.

Ian Leslie (Mold) says that there are probably better logs about than his. Well, how does the one you didn't send in compare? Gear is an R107 and an end fed of unspecified length which bagged: CO2FA, CT1ZE, EA5IW, EP2MJ, JA2PJC, JX2AK, KV4AV, KZ5NG, M1B, OD5FA, PY4BSX, PY8BX, PZ1AX, TI2GI, VE0NEC/MM, VE1KG, VE2ACP, VE6BB, VK2SG, VK5SV, VK6FP, VK7TR, VK9KA, WA1NGK/P/TF, YN1FI, YN1RSJ, YV1OJ, ZD3D, ZD7CE, ZP5KA, ZD3HT, 4S7AB, 4U1ITU, 4X4HT, 5Z4GG.

August is one of the busiest months in amateur radio. Six mobile rallies and three contests with another two early in September. Contests are: August 5-6, WAE c.w.; 12, 4 metre contest (worth a listen); 20, two metre s.s.b. contest; September 2-3, v.h.f. NFD; 2-3, IARU v.h.f. event; 3, qualifying round of the DF contest at Rugby.

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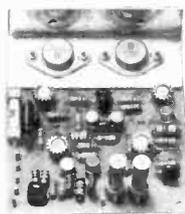
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2E16GT	18	DL92	24	ECL85	32	PC86	44	PL81	41	UC182	31
30C15	56	DL94	46	EP39	36	PC88	45	PL82	29	UF89	26
30C17	75	DL96	36	EP80	22	PC97	35	PL83	31	UL84	28
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30F5	63	DY87	21	EF86	28	PCC84	27	PL500	59	UY85	29
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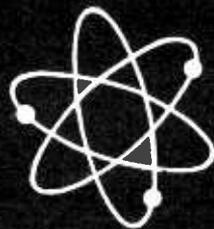
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FULL WAVE POWER CONTROL CIRCUIT L. MacNAMARA

A NUMBER of designs have been featured in past issues of Practical Wireless illustrating how s.c.r.'s (silicon controlled rectifiers) may be used to control such things as the speed of an electric motor and, although these devices worked perfectly well for their intended use, their versatility was limited when applied to light dimming control. In this particular application the s.c.r. has an obvious drawback in that it conducts only on one half cycle of the mains a.c. and the resulting 25Hz frequency appears as a flickering on the bulb, especially when run at low intensities. The obvious method to overcome this difficulty is to use a related device, the TRIAC, which conducts in both directions and the present article illustrates how a very simple and inexpensive power control unit may be assembled from a mere handful of components.

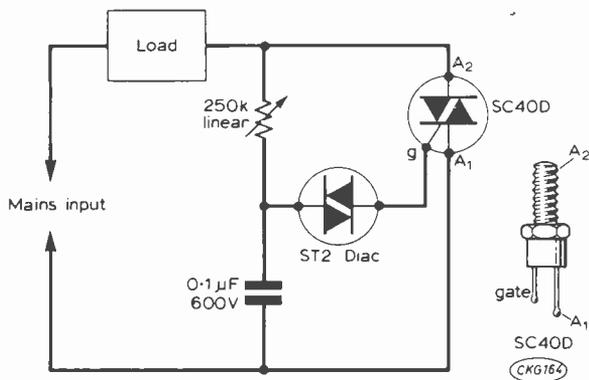


Fig. 1: Full wave power control circuit using a minimum of components.

At the heart of the unit is a G.E. D45D TRIAC (SC40D) which can effectively handle up to 6A at 240V. Basically it can be considered as consisting of two SCR's connected in inverse parallel either of

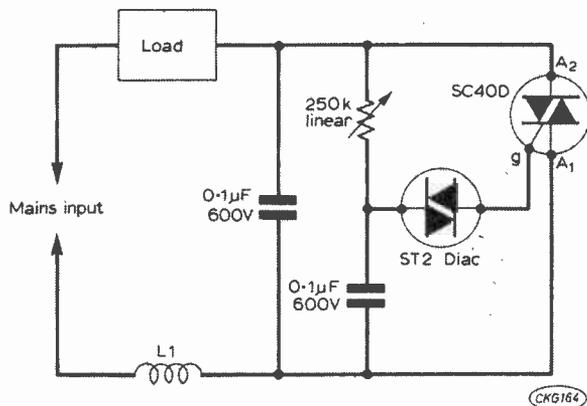


Fig. 2: The same circuit with r.f. suppression. L1 must be capable of handling 5A.

which can be triggered by a pulse applied at the gate. If the time at which this pulse is applied can be varied complete control of the power entering the TRIAC can be effected and this can be realised by a simple resistance/capacity variable phase shift network. An ST2 DIAC, which conducts when the voltage across it reaches about 20V of either polarity, acts as the trigger link between the TRIAC and the phase shift circuit. Fig. 1 shows how such a circuit can be designed using a minimum of components. However due to the sudden switching of the TRIAC from the "off" to the "on" state r.f. interference is produced and this can be a nuisance if the device is operated in the vicinity of radio or TV set. A simple inductance/capacity circuit was therefore incorporated to reduce the interference to a minimum and the prototype was constructed along the lines of Fig. 2. The complete unit was mounted in a plastic box with an ordinary 13A 3-pin socket attached. In addition a 5A fuse was incorporated in the plug to prevent the TRIAC being damaged should excessive current be drawn.

'SCOPE TRIGGER UNIT

P. ROUSE

MANY government surplus oscilloscopes are of extremely high quality and well worth preserving, but sometimes they require an external trigger signal to produce a visible time base. The unit described below produces such a signal and also synchronises the oscilloscope input waveforms to the timebase frequency thus providing a very stable display for accurate measurements. It consists

of an astable multivibrator or square wave generator which is coupled to the trigger input on the oscilloscope by a small step-up pulse transformer. The circuit diagram is shown in Fig. 1 and its operation is briefly described.

The multivibrator produces square waves of either polarity at either collector but Tr2 is used because the frequency can be varied over a small range by

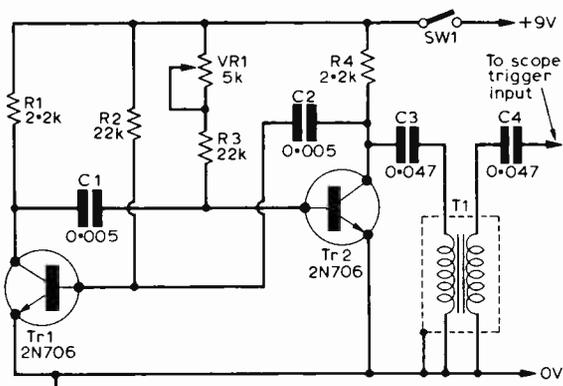


Fig. 1: The circuit of the trigger unit.

adjusting VR1. With the components specified, this range is from 5300Hz to 6500Hz which is quite adequate for synchronisation purposes. The waveform at this collector is shown in Fig. 2. The amplitude is only 8 volts and this must be increased to about 16 volts to trigger most of these old oscilloscopes. Furthermore, a fast pulse rise time is also required. In order to satisfy these two requirements a step-up differentiating pulse transformer must be used. This has the added advantage of producing both positive and negative voltage spikes thus allowing positive and negative triggering. The waveform between C4 and earth is shown in Fig. 3.

Differentiating pulse transformers should have very low leakage inductance and high permeability at their operating frequency. Consequently, a miniature ferrite i.f. transformer is ideally suitable but a Mullard ferrite pot core can be used. The i.f. transformer must be rewound in order to give the correct turns ratio and a diagram of the type used is shown in Fig. 4.

The i.f. transformer must be carefully dismantled and its windings removed. It is then rewound as follows. Firstly 100 turns of fine enamelled wire are wound onto the ferrite bobbin and the ends are soldered on to the lead-through pins in the plastic base. With thin enamel wire such as this, the heat of the soldering iron is sufficient to remove the enamel for easy tinning. Secondly 200 turns of the same gauge wire are wound on to the bobbin and the ends are soldered to the pins as before. The i.f. transformer is then reassembled.

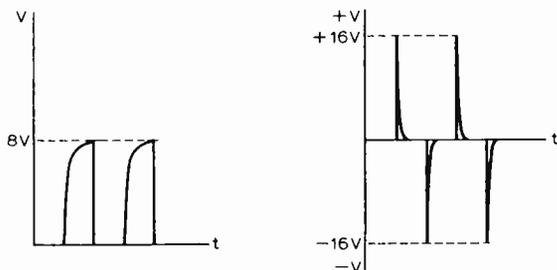


Fig. 2: (left) Waveform at the collector of Tr2.
Fig. 3: (right) Waveform at C4.

★ components list

Resistors:

R1 2.2kΩ
R2 22kΩ
all 10% 1/4 watt
R3 22kΩ
R4 2.2kΩ

Capacitors:

C1 0.005μF
C2 0.005μF
C3 0.047μF
C4 0.047μF

Transistors:

Tr1 2N706
Tr2 2N706

Miscellaneous:

VR1/SW1, 5kΩ potentiometer with switch; T1, miniature i.f. coil 0.7cm. x 1cm; tag strip 2 1/2in x 1 1/2in; screened box 3in. x 2in x 1 1/2in; battery PP9; wire; 3 x 6BA nuts and bolts 1/2in long.

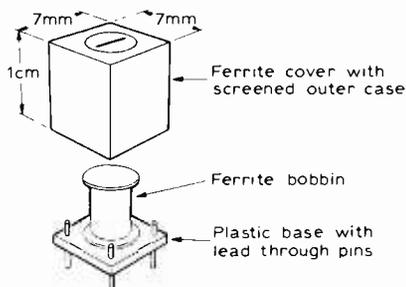


Fig. 4: Construction of the pulse transformer.

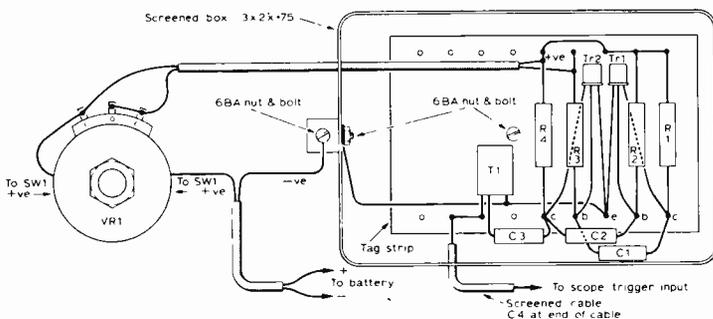
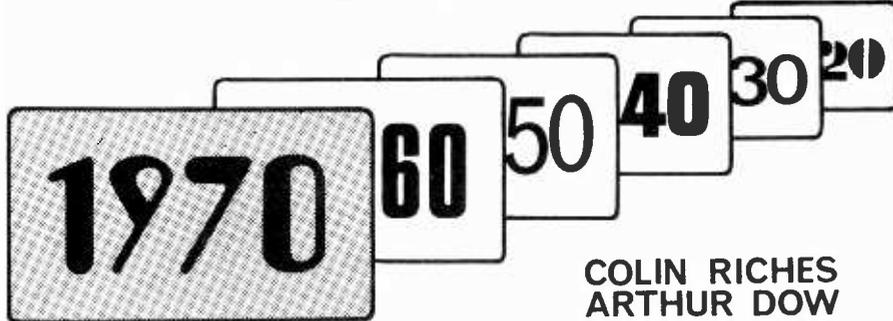


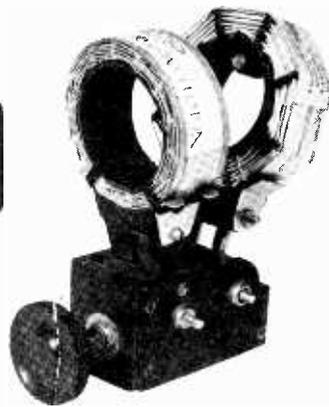
Fig. 5: A suggested component layout.

The circuit is wired up on a small piece of tag strip and mounted in an old tobacco tin for screening purposes. The switch on the back of the variable resistor VR1 is used as SW1 and the whole unit is small enough to be mounted inside the oscilloscope if required, in which case a hole of diameter 3/8in should be drilled in the front panel to hold VR1 and SW1. A 9 volt battery is used to provide power supplies and this voltage ensures that the transistors operate well within their limits thus providing good operational reliability. A diagram of the assembly is shown in Fig. 5.

GOING BACK...



COLIN RICHES
ARTHUR DOW



MR W. W. Pickard from Lowestoft, Suffolk, tells us he still has an "Osram Music Magnet" with 2 volt valves and the old springy "Benjamin" bakelite valve holders, the set is in near perfect condition. He also has quite a lot of 2-volt valves, all sorts, given to him recently by a local dealer, and two old sets, one of which is a Gecophone, and the other he thinks a "Marconi". He says if any readers happen to be in Lowestoft at any time, they are welcome to see this ancient equipment and valves, if they will call at his business address, 192 London Road South, Lowestoft—an outfitters shop. Phone 5675 (closed Thursday).

He can go back to 1923, and had a 3-valve wireless set with plug-in coils then, and remembers well the first broadcast from 5XX Daventry. He remembers he had at that time an Amplion "Dragon" oak-horn loudspeaker—the price was 5 guineas in those days!

★ ★ ★

Mr. S. D. Smith, 292 Whitton Avenue East, Greenford writes "The article "Going Back" prompts me to write down a few memories of my first home built wireless receiving sets. I used a similar device to the buzzer "thing" shown recently in "Going Back" to find a sensitive spot on the galena crystal. My buzzer was coupled inductively however and had no A or E terminals. Bypassing the galena, bornite Zincite etc., etc., we come to my first valve set. This was built on the bottom of a cut down wooden box from the grocers. A, E and phone terminals were P.O. type with steel wood screws for fixing. The valve holders were bought as separate sockets which were screwed separately into the box. The coils were 45 and 30 turns hank wound round the first three fingers and tied with thread. The aerial coil was clamped between two strips of wood by a centre screw which fixed it to the box. The reaction coil was tied to the end of a lath about 15in. long. The pivot screw (with washers) passing through a cotton reel fixed the assembly to the box above the aerial coil. A similar piece of wood was attached to the condenser, thus providing both slow motion and antipacity control. One needed to be quite a good oarsman to avoid catching a crab! The condenser was straight line capacity and bunched the stations at the bottom end.

The phones were Sterling from the first World War for which I paid 2/6d. The valve I remember best had a horizontal assembly. It started to go blue above about 20V h.t. and was at that time treasured and only brought out for special occasions! My only

measuring instrument was an old Post Office galvo and a few resistances (resistors had not been invented). This was "calibrated" against new h.t. and g.b. batteries. All readings were strictly comparative. This instrument was almost indestructible and could be reversed on overload without ill effect. Once it was connected momentarily to the a.c. mains when on the 120V d.c. range. The only result was a slight demagnetisation, easily corrected by moving the paper "calibrations". The original variable grid leak consisted of a short length of glass tube, two corks, a bit of brass wire and burnt sugar. The degree of burning determined the resistance range—more or less. As I had no megohm meter I had to "suck it and see"!

I heard KDKA New York on two successive mornings at about 1.30 a.m. (My mother gave me a tongue lashing for my bleary eyes and threatened to smash up the gear.) It was many years before I heard America again and never since on medium wave. This experience made me very cynical about the "low loss" components which proliferated later and the degradation of the once honourable term High Fidelity. This was commented upon in the Marconi Book of Wireless (1936).

Memory ranges over unit sets, the Popular Wireless Combination Set which, after various mods. finished up with more SP and DP knife switches than a power house. It was more effective as an exercise in ingenuity and oneupmanship than a wireless set, but fun for all that. The Transatlantic Five with plug in McMichael r.f. transformers which never crossed the Atlantic for me, but which did give me a little ephemeral notoriety when I broadcast to all who cared to listen the results of the first election won by Labour. An early three gang neutrodyne I never did succeed in aligning and reverted to a separate aerial condenser, the old Transatlantic Five arrangement.

Later things became much more commercial and stereotyped so I will conclude with a two valve circuit which gave me a lot of fun for several years. In its final form it had a Ferranti choke and transformer and a BTH moving coil speaker, the latter replacing the Amplion horn, simple moving iron and the Blue Spot balanced armature speakers which served in turn. No screening was used and with all those fields and triode valves you may be able to imagine the stabilising devices that were tried out! Just before it was scrapped I found that reaction was very smooth and the set quite sensitive

if r.f. instability was induced over the whole wave band and the reaction coil used back to front. I did not recognise the possibilities of N.F.B. and thought no more about it for years. Hilversum and Paris came in well on L.S., i.e. speech clearly readable in any part of a normally quiet room. Brussels was somewhat weaker but it was only about 100 watts at that time, if my memory is not at fault. It wasn't one of the giants anyway.

I wonder how it would work now? Pentodes, ferrite aerials screened coils and valves, reaction to the first anode and three tuned circuits. Perhaps I'll try it one day if I can find a parafeed 3-1 valve transformer. The AF 5 was a bit bulky.

As an after thought—how many remember the very formal announcement --- "Hallo, Hallo, Hallo, this is 2LO calling; this is the London Station of the British Broadcasting Company calling. You will now hear the news, copyright by Reuter, Press Association, Exchange Telegraph and Central News"?

Marconi Kemp Stamp

On September 13th the Post Office will issue a set of four commemorative stamps. One of these, valued 7½p, commemorates the 75th Anniversary of the first wireless transmissions across water. These tests were carried out by Marconi and Kemp from Lavernock Point, near Barry, to Flatholm Island in the Bristol Channel and Brea Down in Somerset.

The Barry College of Further Education Radio Society commemorates these tests annually by operating amateur radio stations from these historic locations. The Society was responsible for suggesting to the Post Office the issue of this stamp, and are justifiably proud of their association with its issue.

In connection with this issue, they are making available a special commemorative first day cover service from Flatholm Island. For the first time the

Post Office has granted a postmark from Flatholm Island. The special postmark will include their call-sign GB3BCT (Bristol Channel Tests)—the call-sign to be used by their station operating from the island on the 13th September. The first day cover is an embossed design showing the location of the three historic sites.

This unique combination should be of great interest to radio enthusiasts and philatelists alike and the Society will provide the special commemorative envelope, the 7½p Marconi stamp, address and post from Flatholm Island on the first day of issue for . . . 20p.

Remittance should be made by crossed postal order or cheque. All monies should be made payable to BARRY COLLEGE F.E.R.S.

Names and addresses should be printed clearly, and orders should be forwarded to:

The Secretary,
Barry College of Further Education Radio Society,
Colcot Road,
Barry, Glamorgan.
to arrive not later than 11th September, 1972

Vintage Records

Once again we ask readers to let us know the titles and labels of any pre-1930 78's they may have as we have received a number of queries asking the whereabouts of such records.

In addition, if anyone has any gen or pictures of "talking machines" cylinder or disc, we would be glad to hear from them as we are considering writing a feature on this subject in a future "Going Back."

Vintage CQ CQ CQ

EQUIPMENT FOR DISPOSAL

...photographs and constructional details of the "All Concert de luxe" receiver by Percy W. Harris, about 1924 also two Scott-Taggart books. Offers to—A. E. Robinson, 34 Haddon Way, Carlyon Bay, St. Austell, Cornwall.

...3 volumes of Hamsworth Wireless Encyclopedia in good clean condition. Together with other items. See for details please—F. L. Harris, 80 Queens Walk, Ashford, Middlesex, TW15 3JB.

...Buzzer Wavemeter similar to the one in your column a short time ago, various wirewound, pancake and plug-in coils by Igranic and others, Ferranti and Formo intervalve transformers and chokes, filament rheostats, ebonite panels etc. and several examples of single and multiple variable condensers by Ormond and Newey. These later being mechanical cursorless in their own right—and mostly brand new. I think there are a couple of complete (?) receivers somewhere in the attic but have not yet come across them. Any offers—J. C. Priest, 21 Levens Grove, Blackpool, Lancs. FY1 5LA.

...Wireless Telegraphy and Telephony; Charles R. Gibson; Seeley Service, 1914. "The Armstrong Super Regenerator Circuit; George J. EL72; Radio Directory and Publishing Co. New York, 1922. "The Art and Science of the Gramophone" Gaydon 1928.—V. C. Calver, 11 Robin Dene, Manor Road, Brighton, BN2 5EX.

INFORMATION WANTED

...any gen on Marconiphone V2 receiver type R.B.I.A.M3 Inst. No. S/A 1725. Inside the lid is a Post Office stamp reading "Type approved by the Post Master General P.O. Regd. No. 2001".—A. P. Linsell, 7 Canewdon Hall Close, Canewdon, Rochford, Essex.

...Info on Gecophone 3 valve (Det & 2 I.). This is a finely made set with ebonite covered coils loading coil and reaction. Loading coil marked 1250, BC1347 other coil 300, BC1360. But think that these coils are interchangeable. One was used as reaction to the other. In between the two coils is a disc of aluminium which can be slid in and out presumably for adjustment of reaction. Lovely rheostats controlling valve filaments, also neat little cylindrical aerial coupling condenser, made in brass. Marconi 2 valve set. Good slow motion condenser gear. This receiver is marked

"Marconiphone Receiver Type 22 Inst. No. S.C.2661". Unfortunately I have only one coil, longwave, 1000-2200 metres. This is a black ebonite cylinder enclosing coil and beautiful little reaction coil (adjustable from dial on front) marked "Aerial reaction unit, Marconiphone Pat. No. 217042". I would be very pleased to hear of a medium wave coil, 200-500 metres. It clips on to a base with four clips. The two valves fit into one holder mounted on sponge rubber.—W. W. Pickard, 333 Long Road, Lowestoft, Suffolk.

EQUIPMENT WANTED

...receiver, separate speaker or valves from the 1920's or earlier.—Gunnar Carlstrom, S-540 50 Moholm, Sweden. (Radio Amateur SM6KT).

...bright emitter valves or dull emitter with exhaust pipe on top. Also horn fit diaphragm-type speaker, and pre-1920 components.—P. Beckley, 14 Beechdale Road, Newport, Monmouthshire, NPT 8AE.

"J. S. T."

In the article last month on John Scott-Taggart the call-sign of his amateur radio station shown on page 321 should have been 4U (later LUX). The receiver illustrated on page 322 was the ST400, not the ST300.



The design on the envelope in blue and red.

BRAND NEW GUARANTEED

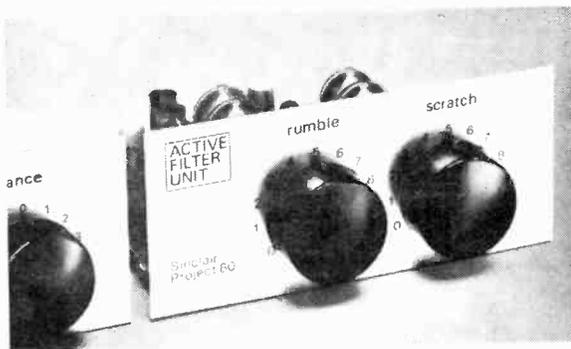
SEMICONDUCTORS & COMPONENTS
SOLE AGENTS FOR SOLID STATES DEVICES INC., (U.S.A.), IN U.K.

RETURN OF POST SERVICE

TRANSISTORS

2G301	0-15	2N2924	0-12	2N4931	2-70	AF116	0-25	BC307	0-09	BF271	0-21
2G302	0-15	2N2925	0-12	2N5172	0-09	AF117	0-20	BC307A	0-09	BF272	0-21
2G303	0-25	2N2926	0-18	2N5173	0-09	AF118	0-20	BC307VI	0-09	BF273	0-21
2G304	0-25	2N2927	0-18	2N5174	0-09	AF119	0-20	BC308	0-08	BF274	0-21
2G305	0-25	Yellow	0-10	2N5175	0-09	AF120	0-22	BC308A	0-08	BF275	0-21
2G344A	0-20	Orange	0-10	2N5190	0-22	AF121	0-22	BC309	0-09	BF276	0-21
2G345B	0-25	Orange	0-15	2N5191	0-22	AF122	0-20	BC309A	0-09	BF277	0-21
2G371	0-15	2N3064	0-15	2N5192	1-24	AF123	0-23	BC309B	0-09	BF278	0-21
2G374	0-15	2N3065	0-15	2N5193	1-01	AF124	0-25	BC310	0-20	BF279	0-21
2G381	0-25	2N3066	0-15	2N5194	1-10	AF125	0-25	BC327	0-21	BF280	0-21
2G417	0-25	2N3390	0-20	2N5195	1-45	AF126	0-25	BC328	0-21	BF281	0-21
2N109	0-49	2N3391	0-20	2N5245	1-45	AF127	0-25	BC329	0-21	BF282	0-21
2N174	1-40	2N3391A	0-22	2N5199	0-22	AF128	0-20	BC330	0-17	BF283	0-21
2N176	0-75	2N3392	0-13	2N5199	0-22	AF129	0-20	BC331	0-17	BF284	0-21
2N274	0-75	2N3393	0-13	2N5457	0-33	AF130	0-20	BC332	0-17	BF285	0-21
2N335	0-75	2N3394	0-13	2N5458	0-33	AF131	0-20	BC333	0-17	BF286	0-21
2N351	0-25	2N3402	0-17	2N5459	0-33	AF132	0-20	BC334	0-17	BF287	0-21
2N376	1-00	2N3403	0-19	2N5460	0-33	AF133	0-20	BC335	0-17	BF288	0-21
2N384	0-93	2N3404	0-24	2N5461	0-33	AF134	0-20	BC336	0-17	BF289	0-21
2N388A	0-40	2N3405	0-27	2N5462	0-33	AF135	0-20	BC337	0-17	BF290	0-21
2N404	0-23	2N3414	0-10	2N5463	0-33	AF136	0-20	BC338	0-17	BF291	0-21
2N404	0-23	2N3415	0-10	2N5464	0-33	AF137	0-20	BC339	0-17	BF292	0-21
2N456	0-75	2N3416	0-15	2N5465	0-33	AF138	0-20	BC340	0-17	BF293	0-21
2N456A	0-75	2N3417	0-15	2N5466	0-33	AF139	0-20	BC341	0-17	BF294	0-21
2N457A	0-80	2N3570	1-25	2N5467	0-33	AF140	0-20	BC342	0-17	BF295	0-21
2N491	3-25	2N3571	1-12	2N5468	0-33	AF141	0-20	BC343	0-17	BF296	0-21
2N584	0-25	2N3572	0-97	2N5469	0-33	AF142	0-20	BC344	0-17	BF297	0-21
2N591	0-34	2N3702	0-11	2N5470	0-33	AF143	0-20	BC345	0-17	BF298	0-21
2N596	0-15	2N3703	0-10	2N5471	0-33	AF144	0-20	BC346	0-17	BF299	0-21
2N597	0-15	2N3704	0-11	2N5472	0-33	AF145	0-20	BC347	0-17	BF300	0-21
2N598	0-25	2N3705	0-10	2N5473	0-33	AF146	0-20	BC348	0-17	BF301	0-21
2N599	0-25	2N3706	0-10	2N5474	0-33	AF147	0-20	BC349	0-17	BF302	0-21
2N706	0-10	2N3707	0-11	2N5475	0-33	AF148	0-20	BC350	0-17	BF303	0-21
2N706A	0-10	2N3708	0-11	2N5476	0-33	AF149	0-20	BC351	0-17	BF304	0-21
2N708	0-13	2N3709	0-90	2N5477	0-33	AF150	0-20	BC352	0-17	BF305	0-21
2N711	0-25	2N3710	0-90	40050	0-50	BC103	0-15	BC353	0-17	BF306	0-21
2N718	0-21	2N3712	0-95	40251	0-58	BC104	0-15	BC354	0-17	BF307	0-21
2N718A	0-20	2N3713	1-08	40309	0-58	BC105	0-15	BC355	0-17	BF308	0-21
2N720	0-50	2N3714	1-15	40310	0-58	BC106	0-15	BC356	0-17	BF309	0-21
2N721	0-55	2N3715	1-22	40360	0-58	BC107	0-15	BC357	0-17	BF310	0-21
2N914	0-15	2N3716	1-30	40362	0-61	BC108	0-15	BC358	0-17	BF311	0-21
2N916	0-15	2N3717	1-30	40363	0-61	BC109	0-15	BC359	0-17	BF312	0-21
2N918	0-20	2N3718	1-33	40364	0-61	BC110	0-15	BC360	0-17	BF313	0-21
2N919	0-20	2N3719	1-33	40365	0-61	BC111	0-15	BC361	0-17	BF314	0-21
2N929	0-14	2N3720	1-33	40366	0-61	BC112	0-15	BC362	0-17	BF315	0-21
2N930	0-14	2N3721	1-33	40367	0-61	BC113	0-15	BC363	0-17	BF316	0-21
2N1091	0-30	2N3722	1-33	40411	0-58	BC114	0-15	BC364	0-17	BF317	0-21
2N1131	0-20	2N3723	1-33	40412	0-58	BC115	0-15	BC365	0-17	BF318	0-21
2N1132	0-20	2N3724	1-33	40413	0-58	BC116	0-15	BC366	0-17	BF319	0-21
2N1184	1-27	2N3725	1-33	40414	0-58	BC117	0-15	BC367	0-17	BF320	0-21
2N1302	1-18	2N3726	1-33	40415	0-58	BC118	0-15	BC368	0-17	BF321	0-21
2N1303	0-16	2N3727	1-33	40416	0-58	BC119	0-15	BC369	0-17	BF322	0-21
2N1304	0-16	2N3728	1-33	40417	0-58	BC120	0-15	BC370	0-17	BF323	0-21
2N1305	0-20	2N3729	1-33	40418	0-58	BC121	0-15	BC371	0-17	BF324	0-21
2N1306	0-22	2N3730	1-33	40419	0-58	BC122	0-15	BC372	0-17	BF325	0-21
2N1307	0-22	2N3731	1-33	40420	0-58	BC123	0-15	BC373	0-17	BF326	0-21
2N1308	0-25	2N3732	1-33	40421	0-58	BC124	0-15	BC374	0-17	BF327	0-21
2N1309	0-25	2N3733	1-33	40422	0-58	BC125	0-15	BC375	0-17	BF328	0-21
2N1453	0-80	2N3824	0-75	40673	0-30	BC126	0-15	BC376	0-17	BF329	0-21
2N1497	0-20	2N3825	0-75	40674	0-30	BC127	0-15	BC377	0-17	BF330	0-21
2N1613	0-20	2N3826	0-75	40675	0-30	BC128	0-15	BC378	0-17	BF331	0-21
2N1613	0-20	2N3827	0-75	40676	0-30	BC129	0-15	BC379	0-17	BF332	0-21
2N1613	0-20	2N3828	0-75	40677	0-30	BC130	0-15	BC380	0-17	BF333	0-21
2N1613	0-20	2N3829	0-75	40678	0-30	BC131	0-15	BC381	0-17	BF334	0-21
2N1613	0-20	2N3830	0-75	40679	0-30	BC132	0-15	BC382	0-17	BF335	0-21
2N1613	0-20	2N3831	0-75	40680	0-30	BC133	0-15	BC383	0-17	BF336	0-21
2N1613	0-20	2N3832	0-75	40681	0-30	BC134	0-15	BC384	0-17	BF337	0-21
2N1613	0-20	2N3833	0-75	40682	0-30	BC135	0-15	BC385	0-17	BF338	0-21
2N1613	0-20	2N3834	0-75	40683	0-30	BC136	0-15	BC386	0-17	BF339	0-21
2N1613	0-20	2N3835	0-75	40684	0-30	BC137	0-15	BC387	0-17	BF340	0-21
2N1613	0-20	2N3836	0-75	40685	0-30	BC138	0-15	BC388	0-17	BF341	0-21
2N1613	0-20	2N3837	0-75	40686	0-30	BC139	0-15	BC389	0-17	BF342	0-21
2N1613	0-20	2N3838	0-75	40687	0-30	BC140	0-15	BC390	0-17	BF343	0-21
2N1613	0-20	2N3839	0-75	40688	0-30	BC141	0-15	BC391	0-17	BF344	0-21
2N1613	0-20	2N3840	0-75	40689	0-30	BC142	0-15	BC392	0-17	BF345	0-21
2N1613	0-20	2N3841	0-75	40690	0-30	BC143	0-15	BC393	0-17	BF346	0-21
2N1613	0-20	2N3842	0-75	40691	0-30	BC144	0-15	BC394	0-17	BF347	0-21
2N1613	0-20	2N3843	0-75	40692	0-30	BC145	0-15	BC395	0-17	BF348	0-21
2N1613	0-20	2N3844	0-75	40693	0-30	BC146	0-15	BC396	0-17	BF349	0-21
2N1613	0-20	2N3845	0-75	40694	0-30	BC147	0-15	BC397	0-17	BF350	0-21
2N1613	0-20	2N3846	0-75	40695	0-30	BC148	0-15	BC398	0-17	BF351	0-21
2N1613	0-20	2N3847	0-75	40696	0-30	BC149	0-15	BC399	0-17	BF352	0-21
2N1613	0-20	2N3848	0-75	40697	0-30	BC150	0-15	BC400	0-17	BF353	0-21
2N1613	0-20	2N3849	0-75	40698	0-30	BC151	0-15	BC401	0-17	BF354	0-21
2N1613	0-20	2N3850	0-75	40699	0-30	BC152	0-15	BC402	0-17	BF355	0-21
2N1613	0-20	2N3851	0-75	40700	0-30	BC153	0-15	BC403	0-17	BF356	0-21
2N1613	0-20	2N3852	0-75	40701	0-30	BC154	0-15	BC404	0-17	BF357	0-21
2N1613	0-20	2N3853	0-75	40702	0-30	BC155	0-15	BC405	0-17	BF358	0-21
2N1613	0-20	2N3854	0-75	40703	0-30	BC156	0-15	BC406	0-17	BF359	0-21
2N1613	0-20	2N3855	0-75	40704	0-30	BC157	0-15	BC407	0-17	BF360	0-21
2N1613	0-20	2N3856	0-75	40705	0-30	BC158	0-15	BC408	0-17	BF361	0-21
2N1613	0-20	2N3857	0-75	40706	0-30	BC159	0-15	BC409	0-17	BF362	0-21
2N1613	0-20	2N3858	0-75	40707	0-30	BC160	0-15	BC410	0-17	BF363	0-21
2N1613	0-20	2N3859	0-75	40708	0-30	BC161	0-15	BC411	0-17	BF364	0-21
2N1613	0-20	2N3860	0-75	40709	0-30	BC162	0-15	BC412	0-17	BF365	0-21
2N1613	0-20	2N3861	0-75	40710	0-30	BC163	0-15	BC413	0-17	BF366	0-21
2N1613	0-20	2N3862	0-75	40711	0-30	BC164	0-15	BC414	0-17	BF367	0-21
2N1613	0-20	2N3863	0-75	40712	0-30	BC165	0-15	BC415	0-17	BF368	0-21
2N1613	0-20	2N3864	0-75	40713	0-30	BC166	0-15	BC416	0-17	BF369	0-21
2N1613	0-20	2N3865	0-75	40714	0-30	BC167	0-15	BC417	0-17	BF370	0-21
2N1613	0-20	2N3866	0-75	40715							

Sinclair Project 60



Active Filter Unit (A.F.U.)

Built and tested post free
£5.98

The value of an efficient filtering system cannot be over emphasized in these days of very high quality reproduction since there are so often occasions where its use can mean the difference between comfortable and uncomfortable listening. On the low pass side the Sinclair A.F.U. will effectively reduce hiss from radio or tape, cut out heterodyne whistles on A.M. reception, greatly reduce record surface noise and other imperfections; on the high-pass side it will cut out motor rumble and other spurious low frequency intrusion. The unit is for use between pre-amp (including tape pre-amps) and power amplifiers, and operates in two sections, both stereo. The cut-off frequencies are continuously variable, and since attenuation in the rejection band is rapid (12dB/octave) there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is as easy to mount as the stereo 60 pre-amp/control unit which it matches in styling, along with the Stereo FM Tuner.

SPECIFICATIONS

The A.F.U. employs two Sallen and Key type active filter stages, one rumble (high pass) and one scratch (low pass). The two stages use complementary transistors to minimise distortion.

Supply voltage: 15 to 35 volts. Current 3mA maximum.

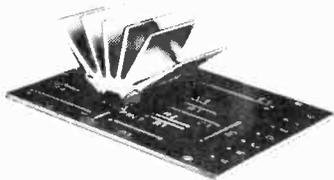
Gain at 1kHz: Filters flat 0.98 (-0.2 dB)

HF cut off: (-3dB) variable from 28 kHz to 5 kHz at 12 dB/octave.

LF cut off: (-3dB) variable from 25Hz to 100Hz at 12dB/octave.

Distortion: at 1kHz (35 volt supply) 0.02% at rated output.

Super IC.12 Integrated circuit high fidelity amplifier



Having introduced Integrated Circuits to hi-fi constructors with the IC.10, the first time an IC had ever been made available for such purposes, we have followed it with an even more efficient version, the Super IC.12, a most exciting advance over our original unit. This needs very few external resistors and capacitors to make an astonishingly good high fidelity amplifier for use with pick-up, F.M. radio or small P.A. set up, etc. The free 40 page manual supplied, details many other applications which this remarkable IC. make possible. It is the equivalent of a 22 tran-

sistor circuit contained within a 16 lead DIL package, and the finned heat sink is sufficient for all requirements. The Super IC.12 is compatible with Project 60 modules which would be used with the Z.50 and Z.30 amplifiers. Complete with free manual and printed circuit board.

SPECIFICATIONS

Output power: 6 watts RMS continuous (12 watts peak). **6-8Ω** **Frequency Response:** 5Hz to 100KHz ±1dB. **Total Harmonic Distortion:** Less than 1%. (Typical 0.1%) at all output powers and frequencies in the audio band (28V). **Load Impedance:** 3 to 15 ohms. **Power Gain:** 90dB (1,000,000,000 times) after feedback. **Supply Voltage:** 6 to 28V. **Quiescent current:** 8mA at 28V. **Size:** 22 x 45 x 28mm including pins and heat sink.

Manual available separately 15p post free.

With FREE printed circuit board and 40 page manual.

£2.98 Post free

Project 605



The easy way to buy and build Project 60

Project 605 is one pack containing: one PZ5, two Z30's, one Stereo 60 and one Masterlink. This new module contains all the input sockets and output components needed together with all necessary leads cut to length and fitted with neat little clips to plug straight on to the modules. Thus all soldering and hunting for the odd part is eliminated. You will be able to add further Project 60 modules as they become available adapted to the Project 605 method of connecting.

Complete Project 605 pack with comprehensive manual, post free **£29.95**

Everything you need to assemble a superb 30 watt high fidelity stereo amplifier without having to solder.

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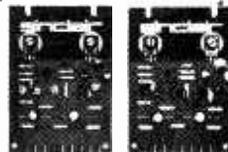
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Z.30 & Z.50 power amplifiers

Built, tested and guaranteed with circuits and instructions manual Z.30 £4.48 Z.50 £5.48

The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to provide unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at 15w (8Ω) and all lower outputs. Whether you use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and are intended for use principally with other units in the Project 60 range. Their performance and design are such, however, that Z.50s and Z.30 may be used in a far wider range of applications.

SPECIFICATIONS (Z.50 units are interchangeable with Z.30s in all applications).—Power Outputs: Z.30 15 watts R.M.S. into 8 ohms using 35 volts : 20 watts R.M.S. into 3 ohms using 30 volts. Z.50 40 watts R.M.S. into 3 ohms using 40 volts : 30 watts R.M.S. into 8 ohms using 50 volts. **Frequency response:** 30 to 300,000Hz ± 1dB. **Distortion:** 0.02% into 8 ohms. **Signal to noise ratio:** better than 70dB unweighted. **Input sensitivity:** 250mV into 100 Kohms (for 15w into 8Ω). For speakers from 3 to 15 ohms impedance. **Size:** 14 x 80 x 57mm.



Stereo 60 Pre-amp/control unit

Built, tested and guaranteed. £9.98

Designed specifically for use on Project 60 systems, the Stereo 60 is equally suitable for use with any high quality power amplifier. Since silicon epitaxial planar transistors are used throughout, a really high signal-to-noise ratio and excellent tracking between channels is achieved. Input selection is by means of press buttons, with accurate equalisation on all input channels. The Stereo 60 is particularly easy to mount.

SPECIFICATIONS—Input sensitivities: Radio — up to 3mV. Mag. p.u. 3mV correct to R.I.A.A. curve ± 1dB 20 to 25,000 Hz. Ceramic p.u. — up to 3mV. Aux — up to 3mV. **Output:** 250mV. **Signal to noise ratio:** better than 70dB. **Channel matching:** within 1dB. **Tone controls:** TREBLE + 12 to -12dB at 10KHz BASS + 12 to -12dB at 100Hz **Front panel:** brushed aluminium with black knobs and controls. **Size:** 66 x 40 x 207mm.



Project 60 Stereo F.M. Tuner

Built and tested. Post free. £25

The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other advanced features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stereo decoder and switchable squelch circuit for silent tuning between stations. In terms of high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with most other high fidelity systems.

SPECIFICATIONS—Number of transistors: 16 plus 20 in I.C. **Tuning range:** 87.5 to 108MHz **Sensitivity:** 7μV for lock-in over full deviation. **Squelch level:** Typically 20μV **Signal to noise ratio:** > 65dB. **Audio frequency response:** 10Hz — 15KHz (± 1dB) **Total harmonic distortion:** 0.15% for 30% modulation **Stereo decoder operating level:** 2μV **Cross talk:** 40dB. **Output voltage:** 2 x 150mV R.M.S. maximum **Operating voltage:** 25–30VDC. **Indicators:** Stereo on; tuning **Size:** 93 x 40 x 207mm



Power Supply Units

Designed specifically for use with the Project 60 system of your choice. Use PZ.5 for normal Z.30 assemblies and PZ.6 or PZ.8 where a stabilised supply is essential.

PZ.5 30 volts un stabilised £4.98
PZ.6 35 volts stabilised £7.98
PZ.8 45 volts stabilised
(less mains transformer) £7.98
PZ.8 mains transformer £5.98

Typical Project 60 applications

System	The Units to use	together with	Units cost
Simple battery record player	Z.30	Crystal P.U., 12V battery volume control, etc.	£4.48
Mains powered record player	Z.30, PZ.5	Crystal or ceramic P.U. volume control, etc	£9.45
12W RMS continuous sine wave stereo amp for average needs	2 x Z.30s, Stereo 60; PZ.5	Crystal, ceramic or mag. P.U., F.M. Tuner, etc.	£23.90
25W, RMS continuous sine wave stereo amp. using low efficiency (high performance) speakers	2 x Z.30s, Stereo 60; PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	£26.90
80W. (3 ohms) RMS continuous sine wave de luxe stereo amplifier. (60W. RMS into 8 ohms)	2 x Z.50s, Stereo 60; PZ.8, mains transformer	As above	£34.88
Indoor P.A.	Z.50, PZ.8, mains transformer	Mic., guitar, speakers, etc., controls	£19.43

F.M. Stereo Tuner (£25) & A.F.U. (£5.98) may be added as required.



Guarantee

If, within 3 months of purchasing any product direct from Sinclair Radionics Ltd., you are dissatisfied with it, your money will be refunded at once. Many Sinclair appointed Stockists also offer this same guarantee in co-operation with Sinclair Radionics Ltd.

Each Project 60 module is tested before leaving our factory and is guaranteed to work perfectly. Should any defect arise in normal use, we will service it at once and without any charge to you, if it is returned within two years from the date of purchase. Outside this period of guarantee a small charge (typically £1.00) will be made. No charge is made for postage by surface mail. Air Mail is charged at cost.

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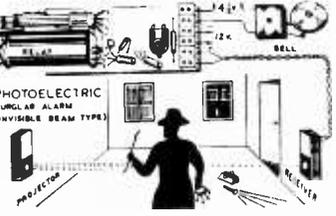
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0Z4	.35	6BW6	.72	6SA7M	.35	1487	.75	6702	EBL21	.60	EL91	.23	PL509	1.30	UY41	.38	AC165	.25	BCY38	.23	OA90	.13		
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1B6GT	.33	6C4	.28	6S17	.35	20D4	1.05	DN	EC92	.94	EM81	.37	PCF89	.43	Y800	.31	U251	.62	AC177	.25	BF159	.29	OA202	.09
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1R4	.22	6CH6	.38	6V8G	.17	20P3	.78	AL60	EC92	.19	EM87	.84	PCF200	.67	QV04/7	VP23	.40	AC180	.25	BF181	.30	OC25	.38	
1U4	.29	6CL6	.48	6V8GT	.27	20P4	.89	ATP4	EC93	.21	EY1	.29	PCF801	.28	R10	.75	VP41	.38	AC181	.15	BF184	.15	OC26	.60
1U5	.48	6CM7	.50	6X4	.20	20P1	1.00	AZ1	EC94	.38	EY81	.35	PCF802	.37	R11	.98	VP71A	.35	AC182	.15	BF185	.15	OC27	.60
2D21	.35	6CUG	.80	6XSGT	.25	25A6G	.29	AZ1	EC95	.38	EY83	.54	PCF806	.55	R16	1.75	VP501	.15	AC183	.15	BF186	.15	OC28	.60
2GK5	.50	6CW4	.63	7B6	.58	25L8G	.20	AZ41	EC96	.38	EY84	.50	PCF802	.68	R17	.88	VP110	.44	AC184	.15	BF187	.15	OC29	.60
3A4	.25	6DE7	.50	7B7	.32	25Y6G	.48	CL33	EC97	.87	EF78	.27	PCL82	.29	R19	.28	VP120	.60	AC185	.15	BF188	.15	OC30	.60
3D6	.19	6DT6A	.50	7H7	.28	25Z4G	.28	CV63	EC98	1.00	EY88	.40	PCL83	.54	SP61	.33	VP120A	.60	AC186	.15	BF189	.15	OC31	.60
3Q4	.38	6EW6	.55	7R7	.65	25Z5	.40	CY1C	EC99	.87	EZ40	.40	PCL84	.32	TH33	.38	VP133	.35	AC187	.15	BF190	.15	OC32	.60
3Q5GT	.35	6F1	.59	7Y4	.60	25Z6G	.45	CY1	EC90	.87	EZ41	.42	PCL85	.35	UBA80	.30	W299	.60	AC188	.15	BF191	.15	OC33	.60
3R4	.28	6F2	.40	7Z4	.40	30A5	.44	DAF91	EC91	.25	EZ80	.19	PCL86	.36	UAF42	.49	X41	.50	AC189	.15	BF192	.15	OC34	.60
3V4	.38	6F13	.38	9BW6	.50	30C15	.55	DAF96	EC92	.64	EZ81	.20	PCL87	.36	UAF42	.49	X41	.50	AC190	.15	BF193	.15	OC35	.60
4C6B	.50	6F14	.40	9D7	.78	30C17	.74	DF91	EC93	.14	ECF804	.2	PCL88	.36	UAF42	.49	X41	.50	AC191	.15	BF194	.15	OC36	.60
5CG8	.50	6F18	.45	10C2	.49	30C18	.58	DF96	.34	2.10	FW4/800.75	PEN4DD	UBC81	.44	UBC41	.45	Transistors	AF186	.55	GET118	.20	OC82	.11	
5T4	.30	6F23	.65	10DF7	.50	30F5	.61	DE76	.28	ECH21	.63	GY01	.75	UBP80	.28	2K404	.18	AF187	.55	GET119	.20	OC83	.11	
5U4G	.30	6F24	.68	10F1	.75	30FL1	.58	DK46	.58	ECH22	.57	EZ40	.48	UBP89	.29	2N2927	.23	BA115	.14	GET120	.20	OC84	.11	
5Y4G	.38	6F25	.51	10F2	.89	30F2	.58	DK46	.58	ECH23	.55	GZ32	.39	UBP89	.29	2N2927	.23	BA116	.14	GET121	.20	OC85	.11	
5Y4GT	.38	6F28	.51	10F18	.85	30FL12	.67	DK96	.85	ECH24	.58	GZ33	.70	UBP89	.29	2N2927	.23	BA117	.14	GET122	.20	OC86	.11	
5Z4G	.38	6F32	.51	10LD11	.85	30FL14	.66	L96	.38	ECH25	.64	GZ34	.47	UBP89	.29	2N2927	.23	BA118	.14	GET123	.20	OC87	.11	
5Z4GT	.38	6G8HA	.50	10P13	.54	30L15	.65	DM70	.30	ECH26	.68	GZ37	.67	PEN4DD	UBC85	.33	2N3121	2.50	BA119	.13	GET124	.20	OC88	.11
6J30L	.53	6GK5	.50	10P14	1.08	30L17	.65	DM71	.38	ECH27	.68	HAB800	.44	4020	.88	PCF80	.31	2N3688	.50	BC107	.15	OC172	.38	
6A8G	.33	6GU7	.50	12A6	.68	30P4MR	.95	DY787	.25	ECH28	.52	HL43DD	.98	PEN46	.20	UC42	.57	A119	.15	BC113	.25	OA9	.13	
6AC7	.15	6H7G	.10	12A6G	.40	30P12	.60	DY782	.29	ECH29	.54	HL43DD	.98	PEN46	.20	UC42	.57	A119	.15	BC115	.25	OA9	.13	
6A08	.25	6H5	.19	12AD6	.40	30P19	.60	ES90C	1.65	ECH30	.54	HL42DD	.98	PEN46	.20	UC42	.57	A119	.15	BC117	.25	OA9	.13	
6A6B	.30	6J6GT	.29	12AE6	.48	30P4	.55	ES91	1.20	ECH31	.58	RN300	1.40	PL33	.38	UCL82	.30	AA129	.15	BC118	.25	OA7	.10	
6A8A	.50	6J6	.18	12AT6	.28	30PL1	.57	ES83F	1.20	EF22	.68	HVR2	.53	PL36	.46	UCL83	.48	AA123	.18	BC119	.23	OA7	.10	
6A8H	.49	6J7G	.24	12AT7	.16	30PL13	.65	ES8CC	.60	EF40	.49	HVR2A	.53	PL81	.42	UF41	.50	AC107	.15	BC120	.23	OA7	.10	
6A05	.21	6J7GT	.38	12AU6	.21	30PL14	.62	E92CC	.40	EF41	.58	KT41	.25	PL81A	.48	UF42	.60	AC112	.25	BC121	.25	OC206	.48	
6AR5	.30	6J8A	.50	12AU7	.17	30PL15	.87	E90A	.30	EF42	.33	KT41	.25	PL82	.28	UF80	.35	AC128	.13	BC122	.25	OC207	.48	
6AT8	.18	6K7G	.10	12AX6	.28	32A2	.48	E189CC1	.00	EF73	.75	KT44	1.00	PL83	.30	UF85	.34	AC127	.17	BC123	.25	OC208	.48	
6AU6	.16	6K8G	.18	12AX7	.21	32L8GT	.42	E1148	.58	EF90	.21	KT66	.80	PL84	.28	UF86	.63	AC128	.20	BC124	.25	OC209	.48	
6AV6	.28	6L1	.98	12BA6	.30	35W4	.23	EA50	.18	EF93	.44	KT81	2.00	PL504/500	UF89	.27	AC132	.20	BC125	.25	OC210	.48		
6AW8A	.54	6L6GT	.39	12BE6	.30	35Z4GT	.24	EA76	.88	EF95	.26	KTW61	.63	UL41	.54	AC134	.25	2-OC82	.48p.	Set of 3-OC83	.65p.			
6AX4	.39	6L7	.38	12BH7	.27	35Z5GT	.30	EAB30	.29	EF96	.27													
6B8G	.18	6L18	.44	12B7GT	.38	35CDDG	.67	EAC91	.38	EF99	.38													
6B44	.19	6L19	1.38	12C15	.50	35D12	.21	EAC92	.38	EF99	.38													
6B8E	.50	6LD20	.48	12K7GT	.34	50EH5	.45	EB34	.20	EF92	.28													
6B8C	.20	6NG7	.40	128C7	.35	50L6GT	.45	EB91	.10	EF98	.25													
6B16	.48	6Q7GT	.43	128G7	.28	85A2	.43	EB41	.48	EF183	.25													
6B7E	.39	6Q7M	.43	128H7	.15	85A3	.40	EB81	.29	EF184	.27													
6BQ7A	.38	6R7G	.35	128J7	.28	90C1	.59	EBF80	.30	EH90	.24													

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50μA	£2-20
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2N1301 0.40	ACY20 0.20	BF196 0.20
2N1302 0.75	ACY21 0.20	BF197 0.20
2N1304 0.25	ACY22 0.15	BF200 0.35
2N1305 0.25	AD140 0.50	BFW87 0.25
2N1306 0.25	AD149 0.50	BFW88 0.23
2N1307 0.30	AD161 0.35	BFW89 0.20
2N1308 0.25	AI162 0.35	BFW91 0.20
2N1309 0.30	ADZ11 1.25	BFX85 0.25
2N1613 0.22	AF114 0.20	BFY19 0.80
2N1711 0.25	AF115 0.20	BFY50 0.25
2N1756 0.75	AF116 0.20	BFY51 0.20
2N2147 0.75	AF117 0.20	BFY52 0.25
2N2160 0.65	AF118 0.25	BSY26 0.20
2N2217 0.30	AF119 0.45	BSY27 0.20
2N2218 0.30	AF127 0.20	BSY28 0.20
2N2219 0.30	AF128 0.20	BSY29 0.20
2N2369A 0.20	AF180 0.35	BSY65 0.20
2N2477 0.65	AF181 0.35	BSY95A 0.15
2N2646 0.60	AF186 0.40	OC16 0.50
2N2905 0.35	AF239 0.40	OC22 0.60
2N2923 0.15	AFZ11 0.45	OC23 0.60
2N2924 0.15	ASV26 0.25	OC24 0.60
2N2926 0.12	ASV27 0.25	OC25 0.35
2N3053 0.25	ASV28 0.25	OC26 0.25
2N3054 0.60	ASV29 0.30	OC28 0.60
2N3055 0.75	ASV54 0.25	OC29 0.60
2N3133 0.30	ASZ15 0.75	OC30 0.75
2N3134 0.30	ASZ16 0.75	OC35 0.50
2N3391 0.25	ASZ17 0.75	OC36 0.60
2N3392 0.15	ASZ18 0.75	OC42 0.20
2N3393 0.15	ASZ20 0.25	OC44 0.20
2N3394 0.15	ASZ21 0.25	OC45 0.15
2N3395 0.20	BC107 0.125	OC70 0.10
2N3402 0.15	BC108 0.15	OC71 0.12
2N3403 0.15	BC109 0.125	OC72 0.25
2N3404 0.35	BC113 0.25	OC73 0.30
2N3414 0.20	BC118 0.30	OC75 0.20
2N3415 0.15	BC134 0.30	OC76 0.20
2N3416 0.25	BC147 0.175	OC78 0.25
2N3417 0.25	BC148 0.15	OC79 0.20
2N3472 0.12	BC149 0.15	OC81 0.15
2N3702 0.12	BC152 0.15	OC81D 0.25
2N3704 0.17	BC158 0.15	OC83 0.20
2N3707 0.15	BC176 0.20	OC139 0.30
2N3709 0.12	BC186 0.25	OC140 0.35
2N3710 0.12	BCY30 0.25	OC141 0.50
2N3819 0.20	BCY31 0.45	OC170 0.20
2N3908 0.20	BCY33 0.25	OC171 0.25
28T02 0.50	BCY34 0.30	OC200 0.30
28T46 0.25	BCY72 0.20	OC201 0.60
AC113 0.15	BCZ10 0.30	OC202 0.65
AC125 0.30	BCZ11 0.40	OC203 0.50
AC126 0.20	BD121 0.65	OC204 0.40

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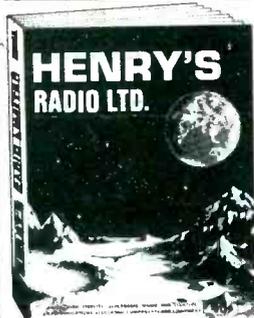
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