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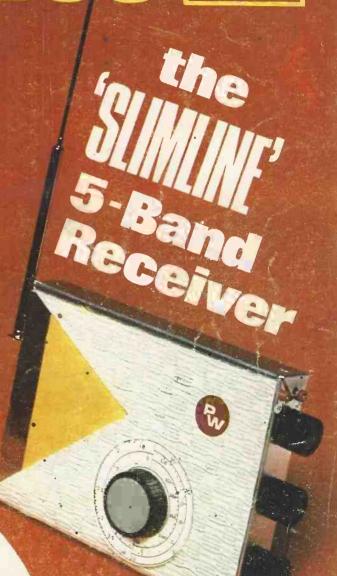
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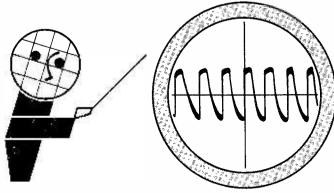
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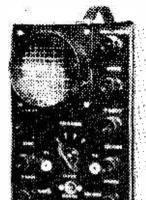
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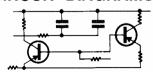
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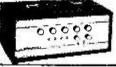
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1R5	. 38	6BZ6	49	68H7	. 44	20P5	1.30	AC/PE	N .98	EC86	٠
184	. 33	6CB6A	.40	68K7GT	. 44	25A6G	. 38	AC2/P	EN/	EC88	
1U4	. 65	6C4	-28	68Q7GT	.38	25L6G	.50	DD	.98	EC92	٠.
1U5	. 90	6C9	1.25	6V6G		25¥5G		AC6PE	IN . 38	ECC33	ı.
	.49	6CD6G	.80	6V6GT		25Z4G	.38			ECC35	•
2GK 5	- 55	6CG8A	.75	6X4	.30	25 Z 5		AL60		ECC40	•
8A4	.42	6CH6	.60	6X5GT	.28	25Z6C		ATP4		ECC81	
3D6	. 19	6CL6	.55	7B6		281)7		AZI	-60		•
3Q4	.49	6CM7	-75	7B7		30A5	.65	AZ31	-60	ECC83	٠
		6CU5	.75	7H7	75	30C15	.75	AZ41	.65		•
	-33	6CM 1	.70		.50	30C17		CL33	1.50	ECC85	
		6DE7	-75	7 Y 4	. 65	30C18	. 73	CAIC	1.00	ECC86	٠
5CG8		6DT6A	-75	7Z4	.80	30F5	. 85	CY31	.45	ECC88	. •
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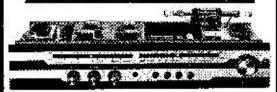
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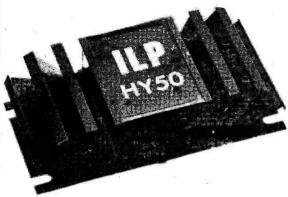
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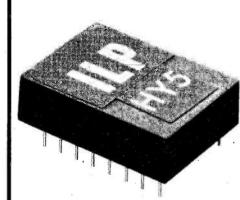
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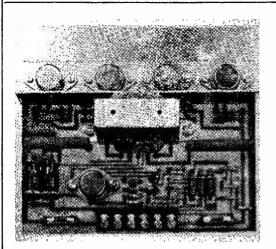
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PS 33	Co-Axial	0.17

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MT50/1		£2 42	35p
MT50/2	2	£3 30	40p

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ACOS GP91-18C. 200mV at 1-2cms/se	ec £1·16
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The E12 Range of Carbon Film Resistors, 1/8th watt available in PAKS of 50 pieces, assorted into the following groups:— R1 50 Mixed 100 ohms-820 ohms 40n R2 50 Mixed 1K ohms-8-2K ohms 40 n 40p

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AL10/AL20/AL30 AUDIO AMPLIFIER MODULES



The AL10, AL20 and AL30 units are similar in their appearance and in their general specification. However, careful selection of the plastic power devices has

selection of the plastic power devices has resulted in a range of output powers from 3 to 10 watts R.M.S. The versatility of their design makes them ideal for use in record players, tape recorders, stereo amplifiers and casettle and cartridge tape players in the car and at home.

Parameter	Conditions	Performance	
HARMONIC DISTORTION	Po = 3 WATTS f=1KHz	0.25%	
LOAD IMPEDANCE	_	8 – 16 Ω	
INPUT IMPEDANCE	f = 1 KHz	100 kΩ	
FREQUENCY RESPONSE Œ 3dB	Po=2 WATTS	50 Hz - 25KH:	
SENSITIVITY for RATED O/P	Vs=25V. Rl=8Ω f=1KHz	75mV. RMS	
DIMENSIONS		3" × 21" × 1"	

The above table relates to the AL10, AL20 and AL30 modules. The following table outlines the differences in their working conditions.

Parameter	AL10	AL20	AL80
Maximum Supply Voltage	25	30	30
Power output for 2% T.H.D. (RL = $8\Omega f = 1 \text{ KHz}$)	3 watts RMS Min.	5 watts RMS Min.	10 watts RMS Min

AUDIO AMPLIFIER

MODULES AL 10. AL 20. AL 30. 3 watts 5 watts 10 watts £2·19 £2·59 £3·01

POWER SUPPLIES

POWER SUPPLIES
PS 12. (Use with AL10 & AL20) 88p
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TRANSFORMERS

T461 (Use with AL10) £1·38 P & P 15p T538 (Use with AL20) £1·93 P & P 15p BMT80 (Use with AL30 & AL50) £2·15

PA 12. PRE-AMPLIFIER SPECIFICATION

The PA 12 pre-amplifier has been designed to match into Frequency response—

12 pre-amplifier has been designed to match into Frequency response—

20Hz-50KHz(-3dB) AL 10, AL 20 and AL 30 audio power amplifiers and it can be supplied from their associated power supplies. There are two stereo inputs, one has been designed for use with *Ceramic cartridges while the auxiliary input will suit most †Magnetic cartridges. Full details are given in the specification table. The four controls are, from left to right: Volume and on/off switch, balance, bass and treble. Size 152mm × 84mm × 35mm.

Bass control—

± 12dB at 60Hz
Trebie control—

Treble control—

± 14dB at 14KHz
*Input 1. Impedance
1 Meg. ohm
Sensitivity 300mV
†Input 2. Impedance
30 K ohms
Sensitivity 4mV

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The STEREO 20

The 'Stereo 20' amplifier is mounted, ready wired and tested on a one-piece chassis measuring 20 cm x 14 cm x 5.5 cm. This compact unit comes complete with on/off switch volume control, balance, base and treble controls. Transformer, Power supply and Power amps. Attractively printed front panel and matching control knobs. The 'Stereo 20' has been designed to fit into most turntable plints without interfering with the mechanism or alternatively, into a separate cabinet. Output power 20w peak. Input 1 (Ccr.) 300mV into 1M. Freq. rex. 25Hz-25kHz. Input 2 (Aux.) 4mV into 30K. Harmonic distortion. Bass control ± 12dB at 60flz typically 0.25% at 1 wait. Treble con. ± 14dB at 14kHz.



50W pk 25w (RMS)

0.1% DISTORTION! HI-FI AUDIO AMPLIFIER

THE AL50

- * Frequency Response 15Hz to 100.000---1dB.
- ★ Load-3, 4, 8 or 16 ohms.
- ★ Distortion-better than .1% at 1 KHz
- * Signal to noise ratio 80dB.

£3-58 each

- ★ Supply voltage 10-35 Volts.
- ★ Overall size 63mm 105mm × 13mm.

Tailor made to the most stringent specifications using top quality component-and incorporating the latest solid state circuitry and ALSO was conceived to fill the need for all your A.F. amplification needs. FULLY BUILT TESTED -GUARANTEED.

STABILISED POWER **MODULE SPM80**

AP80 is especially designed to power 2 of the AL50 Amplifiers, up to 15 wat (r.m.s.) per channel simul taneously. This module embodies the latest component and circuit techniques incorporating complete short circuit protection. With the addition of the Mains Transformer MT80, the unit will provide outputs of up to 1-amps at 35 volts. Size: 63mm x 105mm x 30mm. These units enable you to build Audio Systems of the highest quality at a hitherto unobtainable price. Also ideal for many other applications including:—Disco Systems, Public Address Intercom Units, etc. Handbook available 10p PRICE £3.25

TRANSFORMER BMT80 £2.15 p. & p. 28p

STEREO PRE-AMPLIFIER TYPE PA100

Built to a specification and NOT a price, and yet still the greatest value on the market the PA100 stereo pre-amplifier has been conceived from the latest circuit techniques Designed for use with the AL50 power amplifier system, this quality made unit incorporate no less than eight silicon planar transistors, two of these are specially selected low noise NPN devices for use in the input stages.

Three switched stereo inputs, and rumble and scratch filters are features of the PA100 which also has a STEREO/MONO switch, volume, balance and continuously variable has and trable controls.

bass and treble controls.



SPECIFICATION

Filters: Rumble (High Pass) Scratch (Low Pass) Signal/Noise Ratio

Input overload Supply Dimensions

8KH₂ better than -65dB

+ 26dB + 35 volts at 20mA 292mm × 82mm × 35ton ONLY £13-15

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TRANSFORMERS

Pri. 120/240 V Sec. 120/240 V Centre Tapped and Screened Ref. VA Weight Size cm. P & P
No. (Watts) Iboz 107 20 1 8 7.0 x 6.0 x 6.0 2.32 30
149 60 3 12 9.9 x 7.7 x 8.6 3.45 36
150 100 5 8 9.9 x 8.9 x 8.6 3.79 52 151 200 8 0 12.1 x 9.3 x 10.2 6.45 52 152 250 13 2 12.1 x 11.8 x 10.2 8.41 6.15 153 350 15 0 14.0 x 10.8 x 11.8 11.22 82 154 500 19 8 14.0 x 13.4 x 11.8 16.25 - 155 750 29 0 17.2 x 16.6 x 14.0 22.87 - 156 1000 38 0 17.2 x 16.6 x 14.0 22.87 - 158 2000 60 0 2 16 x 15.3 x 18.1 49.25 -
151 200 8 0 12-1x 9-3 x 10-2 6-45 52 152 250 13 12 12-1x 11-8 x 10-2 8-41 67 153 350 15 0 14-0 x 10-8 x 11-8 11-22 82 154 500 19 8 14-0 x 13-4 x 11-8 16-25 155 750 29 0 17-2 x 14-0 x 10-8 x 11-8 16-25 155 750 29 0 17-2 x 14-0 x 10-8 x 11-8 16-25 155 750 29 0 17-2 x 14-0 x 10-8 x 10
153 350 15 0 140 x 108 x 11-8 11-22 82 154 500 19 8 14-0 x 13-4 x 11-8 11-22 82 155 750 29 0 17-2 x 14-0 x 14-0 z 21-10 156 1000 38 0 17-2 x 16-6 x 14-0 z 29-87
158 2000 60 0 21.6 x 15.3 x 18.1 49.25 -
Ref VA Weight Size on Auro Tobe P.S.P.
No. (Watts) lb oz 113 20 1 0 5.8 x 5.1 x 4.5 0.115-210-240 1.22 22 64 75 2 4 7.4 x 6.7 x 6.1 0.115-210-240 2.40 30 4 150 3 4 8.9 x 7.7 x 7.7 0.115-200-220-240 2.89 36 300 6 4 9.9 x 9.6 x 8.6 5.63 52 67 500 12 8 12.1 x 11.2 x 10.2 8.36 67
113 20 1 0 5.8 x 5.1 x 4.5 0-115-210-240 1 22 22 64 75 2 4 7.4 x 6.7 x 6.1 0-115-210-240 2.40 30 4 150 3 4 8.9 x 7.7 x 7.7 7.115-200-220-240 2.89 36 66 300 6 4 9.9 x 9.6 x 8.6 5.63 52
66 300 6 4 9.9 x 9.6 x 8.6
No. (Watts) boz f p 113 20 1 0 5.8 x 5.1 x 4.5 0.1 5.2 10.2 40 1.22 22 24 75 2 4 7.4 x 6.7 x 6.1 0.1 5.2 10.2 40 2.40 30 4 150 3 4 8.9 x 7.7 x 7.7 0.1 5.2 0.2 2.2 2.2 36 66 300 6 4 9.9 x 9.6 x 8.6 1.5 2.0 2.2 2.2 3.6 67 500 12 8 12.1 x 12.2 0.2 8.36 67 67 500 12 8 12.1 x 12.2 0.2 8.36 67 84 1000 19 8 14.0 x 13.4 x 14.3 15.19 82 82 83 1500 30 4 14.0 x 15.9 x 14.3 21.99 -95 2000 32 0 17.2 x 16.6 x 14.0 28.70 x 27 3000 40 0.2 16 x 13.4 x 8.1 39.17 ** CASED AUTO TRANSFORMERS 15V 500W enclosed transformer, with mains lead and two 15V
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PRIMARY 240-250 VOLTS 12 AND OR 24 YOLT RANGE Ref. Amps. Weight No. 12V 24V boz F & P 111 0-5 0-25 8 4-8 x 2-9 x 3-5 0-12V at 0-25A x 2 1-22 22 213 1-0 0-5 4 6-1 x 5-8 x 4-8 0-12V at 0-25A x 2 1-44 22 71 2 1 12 7-0 x 6-4 x 6-1 0-12V at 1A x 2 1-90 22
111 0 5 6 25
71 2 1 112 7.0 x 6.4 x 6.1 0.12 V at 1 A x 2 1.90 22 18 4 2 2.12 8.3 x 7.7 x 7.0 0.12 V at 2 A x 2 2.68 30 70 6 3 8 8.9 x 8.0 x 7.7 0.12 V at 3 A x 2 3.20 42
71
70 8 3 3 8 89 x 8.0 x 7.7 0 12V at 3A x 2 3 20 42 108 8 4 5 8 9.9 x 8.9 x 8.6 0 12V at 5A x 2 3 60 52 72 10 5 6 4 9.9 x 9.6 x 8.6 0 12V at 5A x 2 4 25 52 116 12 6 6 12 9.9 x 10 2 x 8 6 0 12V at 5A x 2 4 25 52 17 6 0 8 12 12 1 x 9.9 x 10 2 0 12V at 5A x 2 5 10 52 17 6 0 8 12 12 1 x 9.9 x 10 2 0 12V at 5A x 2 6 56 52 17 6 0 0 10 11 8 14 0 x 9.9 x 10 2 0 12V at 10A x 2 8 36 67 187 30 15 15 8 14 0 x 12 1 x 11 8 0 12V at 15A x 2 1540 82 187 4 30 15 15 8 14 0 x 12 1 x 11 8 0 12V at 15A x 2 1540 82
72 10 5 6 4 9.9 x 9.6 x 8.6 0.12V at 5A x 2 4.25 52 116 12 6 6 12.9 9.x 10.2 x 8.6 0.12V at 5A x 2 5.10 52 17 50 0 8 12 12.1 x 9.9 x 10.2 0.12V at 6A x 2 6.56 52 115 20 10 11 8 14.0 x 9.6 x 11.8 0.12V at 10A x 2 8.36 67 187 30 15 15 8 14.0 x 12.1 x 11.8 0.12V at 15A x 2 15.40 82
111 0 · 5 0 · 25
30 VOLT RANGE Ref. Amps Weight Size cm Secondary Tabs P. & P.
112 0.5 1 4 6.1x 5.8x 4.8 0-12-15-20-24-30V 1.42 22 79 1.0 2 4 7.0 x 6.7 x 6.1 1.52 36 3 2.0 3 4 8.9 x 7.7 x 7.7 2.50 36 2.0 3.0 4 8 9.9 x 8.3 x 8.6 3 3.58 42
20 3 0 4 8 9 9 6 8 3 2 8 6 3 58 42 21 4 0 6 4 9 9 2 8 6 8 8 6 4 25 52 55 55 50 6 12 12 12 18 8 6 8 10 2 5 30 52
No.
117 6-0 8 0 12-1 x 9-3 x 10-2, 6-31 52 88 8-0 12 0 12-1 x 11-8 x 10-2, 8-18 67 89 19-0 13 12 14-0 x 10-2 x 11-8, 10-33 67
Ref. Amps. Weight Size cm. Secondary Taps P & P
103 1-0 2 12 8-3 x 7-4 x 7-0 " " 2-80 36 104 2-0 5 8 9-9 x 8-9 x 8-6 " " 3-87 42 105 3-0 6 12 9-9 x 10-2 x 8-6 " " 5-26 52
105 3 0 6 12 9 9 x 10 2 x 8 6 5 26 52 106 40 10 0 12 1x 10 5 x 10 2 6.99 52 107 6 0 12 0 14 0 x 10 5 x 10 8 10 3 6 6 7
No. 102 0.5 i 12 7.0 x 6.4 x 6.1 0-19-25-33-40-50V 1.50 30 103 i 0 2 12 8.3 x 7.4 x 7.0 2.80 36 104 2-0 5 8 9.9 x 8.9 x 8.6 3.87 42 105 3.0 6 12 9.9 x 10·2 x 8.6 3.87 42 106 4-0 10 0 12·1 x 10·5 x 10·2 6.99 52 107 6-0 12 0 14·0 x 10·2 x 11·8 10·35 67 118 8.0 18 0 14·0 x 10·2 x 11·8 10·35 67 118 8.0 18 0 14·0 x 12·7 x 11·8 10·35 67 119 10·0 25 0 17·2 x 12·7 x 14·0 16·93
119 10-0 25 0 17-2-x 12-7 x 14-0 ", ", 16-93 * 60 VOLT RANGE
No. 1b oz f p 124 0.5 2 4 7.0 x 6.7 x 6.1 0.24-30-40-428-69C 1.93 36 126 1.0 3 4 8.9 x 7.7 x 7.7 , , , , 2.70 36 127 2.0 6 4 9.9 x 9.6 x 8.6 , , , 4.25 42
126 1-0 3 4 8-9 × 7.7 × 7.7 2.70 36 127 2-0 6 4 9-9 × 9-6 × 8-6 4-25 42 125 3-0 8 12 12-1 × 19-8 10-2 6-46 52 123 4-0 13 12 12-1 × 11-8 × 10-2 8-36 67
125 3.0 8 12 12 1 x 9.9 x 10.2 6.46 52 123 4.0 13 12 12-1 x 11.8 x 10.2 8.36 67 40 5.0 12 00 14.0 x 10.2 x 11.8 9.85 87 120 6.0 15 8 14.0 x 12.1 x 11.8 9.85 87 120 6.0 15 8 14.0 x 12.1 x 11.8 12.14 82
40 5-0 12 00 14-0 × 10 · 2× 11 · 8 9 85 87 120 6-0 15 8 14-0 × 12-1 × 11 · 8 12-14 82 121 8-0 25 00 14-0 × 14-7 × 11 · 8 13-65 * 122 10-0 25 0 17-2 × 12-7 × 14-0 20-09 * 122 12-0 × 12-0 × 12-0 × 14-0 20-09 * 12-0 × 12-0
123 4-0 13 12 12-1 x 19-3 x 10-2 6-36 52 40 5-0 12 00 14-0 x 10-2 x 11-8 9 8-36 67 40 5-0 12 00 14-0 x 10-2 x 11-8 9 85 87 120 6-0 15 8 14-0 x 12-1 x 11-8 12-14 82 121 8-0 25 00 14-0 x 14-7 x 11-8 13-65 * 122 10-0 25 0 17-2 x 12-7 x 14-0 20-09 * 189 12-0 29 00 17-2 x 14-0 x 14-0 22-49 *
120 6-0 15 8 14-0 × 12-1 × 11-8 12-14 82 12-14 82 12-14 82 12-14 82 12-14 82 12-14 82 13-65 8 12-14 82 13-65 8 12-12 13-65 8 .
Ref. MA. Weight Size cm VOLTS £ p 238 200 2 2.882.682.0 3.0-3 1.31 10 212 1A IA I 4.6.185.884.8 0.6.0-6.6 1.52 22 13 100 4 3.992.662.9 9.0-9 1.12 10 235 330,330 4 4.882.983.5 0.9, 0.9 1.52 10 207 500,500 1.00 6.185.484.8 0.8-9, 0.8-9 2.03 22
212 1A IA I 4 6 1x5 8x4 8 0.6 0.6 0.6 1.52 22 13 100 4 3.9x2 6x2 9 9.0.9 1.12 10 207 500, 500 1.00 6 1x5 4x4 8 0.8.9, 0.8.9 2.03 22 207 500, 500 1.00 6 1x5 4x4 8 0.8.9, 0.8.9 2.03 22
235 330,330
208 1A, 1A 12 7-0x6-1x6-1 0-8-9,0-8-9 2-73 30 236 200, 200 4 4-8x2-9x3-5 0-15,0-15 1-52 10 214 300, 300 14 6-1x5-8x4-8 0-20,0-20 1-60 22 221 700 (D.C.) 8 7-0x6-1x6-1 20-12-012-20 1-41 30
208 A I I Z 7.0 x 6.4 x 6.1 0.8.9 0.8.9 2.73 30 236 200, 200 4 4.8 x 2.9 x 3.5 0.15, 0.15 1.52 10 214 300, 300 4 6.1 x 5.8 x 4.8 0.20, 0.20 1.60 22 221 700 (D.C.) 8 7.0 x 6.1 x 6.1 x 7.7 x 7.0 0.15.20 0.15.20 3.08 36 203 500, 500 2 4 8.3 x 7.0 x 7.0 0.15.20 0.15.20 2.9 x 3.8 2.03 3.00
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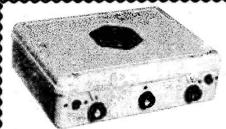
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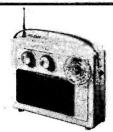
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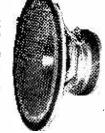
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Calibrator and amplitude Calibrator.
Supplied complete with all accessories
and instruction manual.

OUR PRICE £87.00

LB4 TRANSISTOR TESTER

Tests PNP or NPN transistors. Audio indication. Operates on two 1.5V batteries. Complete with instructions etc. £4.50 P&P 20p

Transistor Tester
27 ranges. 16,700pv.
Overload protected.
Ranges: 0.301900v.
0.5127,320150v.
0.5127,320150v.
0.6127,320150v.
0.6127,320150v.
0.6126,7200mA DC.
Resistance: 0.060
0.6126/620/60/200k ohms/2 Mohms.
Battery operated. Supplied complete with probes, leads and steel carrying case. Size: 115 x 215 x 90mm.
OILB PBIECF £18.50 page 200-

P&P 20p



OUR PRICE £15.00

Model HT100BA MULTIMETER
Overload protected, sheek proof circuits, 9,5uA Meter with mirror scale. Sensitivity 100kV. Polarity change switch, Ranges: 0.5/2.5/1.750/250/500/1.000
Volts DC. 2.5/10/50/250/1.000
Volts DC. 2.5/10/50/250/4/2.5/25/250
mA/10A. AC current: -0-10A. -20 to +62dB. Operates from 2 x 1.5V batteries. Size: 180 x 134 x 79mm.
DIB PBIEF 515.00

OUR PRICE £15.00 P&P 40p

OUR PRICE £17.50

GENERATOR

Carr, paid

OUR PRICE

U4341 Multimeter & Transistor Tester



LB3 TRANSISTOR TESTER Tests ICO and B.
PNP/NPN, Operates
from 9V battery.
Instructions supplied.
OUR PRICE

P&P 20p KAMODEN HM350 TRANSISTOR TESTER

High quality instrument to test reverse leak current and DC current. Amplification factor of NPN, PNP, diodes, transistors, SCR's etc. 4" square clear scale meter. Operates from internal batteries. Complete with instructions, leads carrying handle. current, Ampli-

£3.95

OUR PRICE £12.50

P&P 30p

S100TR MULTIMETER TRANSISTOR TESTER

TRANSISTOR TESTER
100,000pw, Mirror
scale, Overhoad
protection, 0/0, 12/
0.6/3/12/30/120/
0.6/3/12/30/120/
0.7/2/6000V AC.
0/12/600u/A/2/
300mA/6/12A DC
0/10k/1 Meg/
100 Meg.
-20 to +50dB,
Order Dessures Alpha, Beta
and ICO, Omplete with instructions,
batteries and leads.

OUR PRICE £15.95

TE16A TRANSISTORISED SIGNAL GENERATOR

5 ranges, 400kHz to 30 MHz. An inexpensive instrument for Instrument for the handy-man. Operates on 9V battery. Wide easy to read scale. 800kHz modulation. Size: 149 x 149 x 92 with instructions and I

OUR PRICE £8.97 P&P 25p

MODEL TE20 RF SIGNAL

UENEHATOR
Six bands, 120kHz.
260MHz, Dual outparts
Variable audio output
Variable audio output.
Accuracy ± 2%, Audio
output to 8V, Power requirements:
105—125V, 220—240V AC. Size: 193
x 265 x 150mm. Complete with test
leads etc.

OUR PRICE £17.50

ARF 300 AF/RF SIGNAL

GENERATOR
All transistorised
compact fully
portable. AF sinewave 18Hz to 220
kHz. AF square
wave 18Hz to 100k
Hz. Dutput Square/
Sine wave 10V.
P.P. RF 100kHz. to
200MHz. Output
1 maximum.
Coperation
with instructions and leads

OUR PRICE £29.95 P&P 50p

AT201 Decade **ATTENUATOR**

Frequency range 0—200kHz. Attenuator 0—111dB, 0.1dB steps. Impedence 600 ohms. Input power maximum 30dBm. Size: 180 x 90 x 55mm.

OUR PRICE £12.50 P&P 37p

MCA220 Automatic Voltage Stabiliser Input 88–125V AC or 176–250V AC. Output 120V AC or 240V AC 200V/A rating. P&P 501



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PS100B Regulated POWER SUPPLY UNIT

Solid state. Dutput 6, 9 or 12V DC up to 3 Amp. Meter to monitor current. Input 220/240V AC Size: 100 x 82 x 159mm.

OUR PRICE £11.97 PS200 Regulated POWER

SUPPLY UNIT Solid state, Variable output 5–20V DC up to 2 Amp. Inde pendent meters to monitor voltage and current. Output 220/240V AC, Size: 190 x 136 x 98mm.



OUR PRICE £19.95

P&P25p 1137



P&P 25p

OUR PRICE £10.50



EW CLEAR PLASTIC PANEL METERS

USED EXTENSIVELY BY INDUSTRY, GOVERNMENT DEPARTMENTS, EDUCATIONAL AUTHORITIES ETC. Over 200 ranges in stock-other ranges to order. Quantity discounts available. Send for fully illustrated brochure.

CLEAR PLASTIC MODEL SD640 Size: 85 x 64mm

50uA	£3.35	
100uA	£3.30	
200u A	£3.30	- Aug
500u A	£3.25	1 - 1
50-0-50u A	£3.35	90 A0 A
100-0-100u A	£3.30	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
1mA	£3.20	
5mA	£3.20	0.21
10mA	£3.20	1152
50mA	£3.20	
100mA	£3.20	20V DC £3.20
500mA	£3.20	50V DC £3.20
1A DC	£3.20	300V DC £3.20

CLEAR PLASTIC MODEL SW100

50u A 100u A	£4.55 £4.35	3.3
500uA 50-0-50uA 100-0-100uA	£4.10 £4.35 £4.30	A
1mA 1A DC	£3.95 £3.95	N.
5A DC 20V DC	£3.95 £3.95	
50V DC 300V DC	£3.95 £3.95	300V AC VU Meter

EDGWISE MODEL PE70 Size: 90 x 34mm

50uA	£4.15
100uA	£3.95
200uA	£3.75
500uA	£3.50
50-0-50uA	£3.95
100-0-100u A	£3.85
1mA	£3.50
300V AC	£3,50
VU Meter	£4 25



£4.00 £4.75

MODEL ED107 EDUCATIONAL METER Size: 100 x 90 x 150mm including terminals

A range of high quality moving coil instruments ideal for school experi-ments and other bench applications. 3" mirror scale. The meter move-ment is easily accessible to demonstrate internal working. orking.



A DC	 	£6.55		
A DC	 	£6.55		
V DC	 	£6.55	300V DC	£6.55
OV DC	 	£6.55	500mA/5A DC	£7.70
5V DC	 	£6.55	EV/EOV DC	£7.70
OV DC	 	£6.55	5V/15V DC	£7.70
OV DC		F6 55	14/154 00	67.70

CLEAR PLASTIC MODEL 85P

50uA			£4.85
100u A			£4.70
200a A	••	••	£4.45
500u A	•	••	£4.30
50-0-50u 100-0-10	۸.,		£4.70
500-0-10			£4.45 £4.30
1mA			£4.30
		••	£4.30
5mA	••	••	£4.30
10mA	:		£4.30
50mA		::	£4.30
100mA		::	£4.30
500mA			£4.30
1A DC			£4.30
5A DC	::		£4.30
15A DC	••	•••	64.30

POWER RHEOSTATS

ings embedded in vitreous enamel. Heavy duty brush wiper. Continuous rating. Wide range sailable ex-stock. Single hole fixing. X'' diameter shafts. Bulk quantities available.

25 WATT 10/25/50/100/250/500/

50 WATT 10/25/50/100/250/500/1000/2500/5000 Ohms.

100 WATT 1/5/10/25/50/100/250/ 500/1000/2500 Ohms

ALL PRICES

EXCLUDE VAT

Also see previous page

£1.15 P&P 10p

£1.62 P&P 10p

£2.34 P&P 15p

High quality ceramic construction. Windings embedded in

1000 Ohms



21111		-	*****
300V DC 15V AC 300V AC S Meter VU Mete 1A AC 5A AC 10A AC 20A AC 30A AC	 1m/	.: :: :: :: ::	£4.30 £4.35 £4.35 £4.30 £5.00 * £4.30 * £4.30 * £4.30

AUTO TRANSFORMERS

0/115/250V.S	tep up or st	ep down.	
Fully shrouded			
80 WATTS	£2.75	P&P 18p	
150 WATTS	£3.50	P&P 18p	
300 WATTS	£4.50	P&P 23p	
500 WATTS	£6.95	P&P 33p	
1000 WATTS	£9.50	P&P 38p	
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2250 WATTS	£20.95	P&P 50p	
5000 WATTS	£44.95	P&P £1	i

CP110 CHASSIS PUNCH SET



Carefully machined top grade steel. Contains 1/2", 5/8", 3/4", 1" and 1 1/8" punches complete with gripper and accessories.

OUR PRICE £3.00

*Items with asterisk are Moving Iron type, all others are Moving Coil

CLEAR PLASTIC MODEL SD830 Size: 110 x 83mm				
50uA 100uA 200uA 500uA 50-0-50uA		£3.75 £3.70 £3.65 £3.45 £3.75		

200uA 500uA	£3.65 £3.45	where we are
50-0-50uA	£3.75	1 3 4 4
100-0-100u A	£3.70	\
1mA	£3.40	
5mA,	£3,40	
10mA	£3.40	
50mA	£3.40	10V DC £3.40
100mA	£3,40	20V DC £3.40
500mA	£3.40	50V DC £3.40
1A DC	£3.40	300V DC £3.40
5A DC	£3.40	15V AC £3.65
10A DC	£3.40	300V AC £3.65
5V DC	£3.40	VU Meter £3,85

CLEAR PLASTIC MODEL 45P

O120. 30 A	50111111	
50uA		£3.00
100uA .		£2.85
200uA .		£2.75
500uA .		£2,70
50-0-50u A		£2.90
100-0-100	ıA	£2.75
500-0-500L		£2.65
1mA		£2.65
5mA		£2.65
		£2.65
50mA		£2.65
100mA .		£2.65
		£2.65
1A DC .		£2.65
5A DC .		£2.65

No.	7
151	W
300V AC	£2.70

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300V AC S Meter 1mA VU Meter 1A AC 10A AC 10A AC	£2.70 £2.75 £3.00 * £2.65 * £2.65
20A AC	* £2.65
30A AC	* £2.65

CLEAR PLASTIC MODEL 38P Size: 42 x 42mm

ı	OILO: TE A TEIMIN			
	50uA	£2.80 £2.70 £2.65 £2.50 £2.75 £2.65 £2.50	و دامان	
	1mA	£2.50	2	
	1-0-1mA	£2.50	11860	50
	2mA	£2.50	111/02/2005	
	5mA	£2.50	111111111111111111111111111111111111111	
	10mA	£2.50	Control of the Contro	
	20m A	£2.50		
	50mA	£2.50	15V DC	en
	100mA	£2.50	20V DC	£2
	150mA	£2.50	50V DC	£2
	200mA	£2.50	100V DC	£2
	300mA	£2.50	150V DC	£2
	500mA	£2.50	300V DC	£2
	750mA	£2.50	E001/ D0	£2
	1 A DC	£2.50	750V DC	£2.
	2A DC	£2.50	15V AC	£2.
	EA DC	£2.50	50V AC	£2.
	10 A DO	£2.50	30V AL	£2.
	1EA DC	£2.50	150V AC 300V AC	£2.
	204 00	£2.50		£2.
	21/ DC	£2.50	500V AC	£2.
	10V DC	£2.50	S Meter 1m A	£2.

••			£2.50	HINIDA	100
πA	٠.	••	£2.50	1000	
••			£2.50	1111988	
			£2.50	[3][[5]	
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١	••		£2.50		
١			£2.50	15V DC	£2.50
Α			£2.50	20V DC	£2.50
A			£2.50	50V DC	£2.50
Α	••		£2.50	100V DC	£2.50
Α			£2.50	150V DC	£2.50
Α			£2.50	300V DC	£2.50
Α			£2.50	500V DC	£2.50
A			£2.50	750V DC	£2.50
2			£2.50	15V AC	£2.55
3			£2.50	50V AC	£2.55
oc.			£2.50	150V AC	£2.55
C			£2.50	300V AC	£2.55
ю			£2.50	500V AC	£2.55
)C			£2.50	S Meter 1mA	£2.55
x.			£2 50	VIII Manay	20.00

10V DC	:: ::	::	£2.50 £2.50	S Meter 1mA VU Meter	£2.55 £2.90
CLEAR Size: 59	PL × 46	AS7	TIC MO	DEL SD460	
50uA 100uA 200uA 500uA	::	::	£3.10 £3.05 £3.00 £2.80	يبلغ سنري	()
50-0-50u 100-0-10 1mA 5mA	Α Ου Α 	.: ::	£3.10 £3.05 £2.85 £2.85	4	
10mA 50mA 100mA 500mA	:	::	£2.85 £2.85 £2.85 £2.85	10V DC 50V DC	£2.85 £2.85
1A DC 5A DC 10A DC 5V DC	::	:	£2.85 £2.85 £2.85 £2.85	300V DC 15V AC 300V AC VU Meter	£2.85 £3.00 £3.00 £3.20

POSTAGE & PACKING 15p

YAMABISHI VARIABLE

VOLTAGE TRANSFORMERS Excellent quality at low cost. Input: 230V 50/60Hz. Output 0-260V. MODEL \$260 BENCH MOUNTING

1A £10.50 200 2.5A £12.00 35p 5A £17.50 37p 8A £20.35 50p 10A £23.75 75p 12A £29.50 75p 20A £85.00 125p 20A £85.00 125p 40A £12.00 150p MODEL \$260B PANEL MOUNTING

BVD5 Vernier TUNING DIAL

CLEAR PLASTIC MODEL 65P

50uA	£4.10 £3.45 £3.30 £3.30 £3.40 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85	50V AC £3.10 150V AC £3.10 300V AC £3.10 500V AC £3.15 VW Meter 1mA £3.15 VU Meter £4.40
30A DC	£3.10	
EUV DC	£3.20	1A AC * £2.85
5V DC	£2.85	5A AC * £2.85 10A AC * £2.85
10V DC	£2.85	
20V DC	£2.85	
50V DC	£2.85	E0m A AC + C2 OF
150V DC	£2.85	
300V DC	£2.85	
15V AC	£3.10	
DAKELITE M	£3.10	500mA AC * £2.85

BAKELITE MODEL S80 Enlarged Window Size: 80 x 80mm

50u A 100u A 500u A 50-0-50u A 100-0-100u A	£3.85 £3.75 £3.35 £3.75 £3.65 £3.00	إسانتاس
1A DC 5A DC 20V DC 50V DC	£3.30 £3.30 £3.30 £3.30	
300V DC 300V AC VU Meter	£3.30 £3.30 £4.05	

CLEAR PLASTIC MODEL 52P

Size: 60 x 60	mm		
50uA 100uA 500uA 50-0-50uA 100-0-100uA 1mA		£3.85 £3.30 £2.90 £3.35 £3.25 £2.75 £2.75	
10mA 50mA 100mA	-	£2.75 £2.75 £2.75	į
500mA 1A DC 5A DC		£2.75 £2.75 £2.75	SN
10V DC 20V DC 50V DC		£2.75 £2.75 £2.75	1A 5A
300V DC 15V AC 300V AC	 	£2.75 £2.85 £2.85	10. 20. 30.



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,	S Meter 1n	ıA	£2.8
	VU Meter.		£3.9
	1A AC .		* £2.7
	5A AC .		* £2.7
•	10A AC .		* £2.7
	20A AC .		* £2.7
	30A AC .		* £2.7

BAKELITE MODEL 65 Size: 80 x 80mm

			,,,,,,
25uA			£5.05
50u A			£3.90
100uA	•••		£3.30
500uA		••	£3.00
50-0-50u	۸	••	
		••	£3.35
100-0-10	Vu v	٠	£3.30
500-0-50	Ou A	١	£2.85
1mA			£2.85
1-0-1mA	••		£2.85
5mA			£2.85
10mA			£2.85
50m A			£2.85
100mA			£2.85
500mA		••	£2.85
1A DC	•••	••	£2.85
ŽÃ ĐC	••	••	
5A DC	••	••	£2.85
	••	••	£2.85
15A DC	••		£2.85
30A DC			£2.85
50A DC	••		£2.85
5V DC			£2.85
10V DC			£2.85
20V DC			£2.85
50V DC			£2.85
150V DC		••	22.00

150V DC 300V DC



5				- 1
5	30V AC		 * £2.8	5
,	50V AC		 * £2.8	5
5	150V AC		 * £2.8	5
5	300V AC		 * £2.8	5
,	500V AC		 £2.8	5
,	VU Meter	r	 £4.0	ōi
,	1A AC	٠.	 • £2.8	5
•	5A AC		 * £2.8	š
,	10A AC		 * £2.8	
,	20A AC		 * £2.8	5
,	30A AC		 * £2.8	5
•	50A AC		 * £2.8	5 I
•	500mA A	c	 £2.8	5 !
	50mV DC		 £3.2	ŌΙ
	100mV D	C	 £3.2	n 1

2 TRANSISTOR RADIO KIT



No Soldering required. All connect-made with spring clips. Kit includes all parts and wire including ear-piece. Will receive all normal broadcasts on Medium Wave 535-1605kHz. Oper-ates from standard 9V battery or Solar Cell included.

OUR PRICE £1.30

SWR METER Model SWR3 SWH MELEH Model S Handy SWR meter for transmitter antenna align-ment, with built-in field strength meter. Accuracy 5%, Impedence 52' Indic-ator 100uA DC, Full scale 5 section collapsible antenna. Size 145 x 50 x 60mm.

P&P 30p

TRIO JR599 RECEIVER



Nine wave-bands covering 1.8-29.7 MHz, 144-146MHz and 10MHz WWV SSB, CW, AM and FM. AF output is more than 1 watt. S Meter. Squelch control. BFO. Variable AF and RF control. BFO. Variable AF and RF control. BFO. Wariable William 100 Meters of the Control of the

Our Price £132.50 PARP. TRIO 9R590S RECEIVER



Four bands covering 550kHz to 30 MHz continuous and electrical bandspread on 10, 15, 20, 40, and 80 mts. 8 valve plus 7 diode circuit, 4 to 8 ohm output and phone inck. SSB—CW, ANL, variable BFO. S Meter and separate band spread dial. IF frequency 445kHz, audio output 1½ watt. Variable BF and AF gain controls. 115/250V AC, with instructions.

Our Price £42.50 SARR. TRIO TR2200 TRANSCEIVER

TRIO TR2200 TRANSCEIVER
Fully transistorised portable by
Will transmit and
receive on six
channels between
that transmit and
that transm

OUR PRICE £79.50 Carr.paid

BELTEK W5400 CAR TRANSCEIVER



Solid state mobile transceiver for 12 volt DC neg. Transmits and receives on any 12 of 28 channels between 144 and 146MHz. Power output 10W and 1W switchable. Controls: On/off/volume, squelch and channel selector. Internal 3" speaker. Complete of Internal 3" speaker. Complete of Internal 18" power. PTT switch, three volume of the property of the provided of the pr OUR PRICE £75.00



SKYFON 100mW OUR PRICE £24.95 per pair 302 Two Channel 300mW OUR PRICE £52.50 per pair P1003 Three Channel 1 Watt OUR PRICE £71.25 per pair P&P 50p per pair

NB. Licence required for use in UK KE630 3 Station INTERCOM



Master and two sub-stations. Can be used on desk or wall mounted. Comp-lete with cable and batteries **OUR PRICE £5.25**

1138

App. 7:1 ratio planetary drive vernier dial. Log scale 0–180 degrees. Blank scales 1–5. Plai size 128 x 76mm. Overall size 190 x 117 x 41mm. deep including knob and coupling. "diam. shaft OUR PRICE £1.62

1A £10.00 30p 2.5A £12.00 35p

P&P 15p OUR PRICE £4.25

3 P&P 25p



RECORD DECKS

LH02S STEREO HEADPHONES Light weight head-phones with padded ear pieces. 4/16 ohms 20—20,000Hz. Complete with 6' lead and plug.

OUR PRICE £1.97



P&P 30p

TE1018 Deluxe Mono High Impedence Headset. Sensitive magnetic headset with soft ea pads. Impedence 2,600 g ohms (600 ohms DC).

Frequency response: 200-4,000Hz. OUR PRICE £2.25

DH02S STEREO HEADPHONES

performance combined. Adjust-able head band. Impedence 8 ohms 20-12,000Hz. Complete with OUR PRICE £2.25



TE1035 Stereo HEAOPHONES Low cost with exc-ellent response. Foam rubber earcups. Adjust-able headband. 8 ohms impedence. Frequency response 25Hz-18kHz Complete with cable and sterogiack plun

OUR PRICE £2.60

P&P 30p

SH8DV MONO/STEREO HEADPHONES

Volume control for each channel. 4/16 ohms impedence. Frequency response 20Hz – 18kHz. Complete with 10ft. coiled lead and jack plug **OUR PRICE £4.97**



BH001 HEADSET and Boom Microphone

Moving coil. Ideal for language teaching teaching, communications etc. Headphone impede edence 16 ohms. Mic nce 200 ohms. OUR PRICE £5.95

SPECIAL BARGAIN!! PHONIC 10 Two Way Speakers

speakers of unique design. Incorporating a 2" high a 2" high frequency unit & 6" woofer. 8 ohms imped-ence. Size: 348 x 228 x 110mm.



OUR PRICE £8.85 Pair P&P 50p

SPECIAL BARGAIN II

STEREOSOUND SPEAKERS Matched pair of stereo bookshelf speakers. Deluxe teak veneered finish. Size: 368 x 229 x 190mm. 8 ohms. 8 watts RMS, 16 watts RMS, 16 watts RMS, 16



OUR PRICE £12.95

P&P 50p AUDIOTRONIC CRITERION

SPEAKERS SPEAKERS
High quality three way speaker system offering a performance better than more expensive units. Teak finished with dark fronts. Frequency response: 40Hz-20kHz. 8 chms impedence. Maximum power 20 watts. Size: 476 × 232 × 232 mm.

OUR PRICE £27.50 Pr. P&P £1



WE ARE APPOINTED STOCKISTS AT ALL BRANCHES

All kits are complete with compre hensive easy to follow instructions and covered by full guarantee... Post and Packing 15n ner bie

rost and racking 15p per kit.	
AE1 100mW output stage AE2 Pre-amplifier AE3 Diode receiver	£1.65 £1.26 £2.00
AE4 Flasher	£1.09
AE5 Astable multi-vibrator	£1.05
AE6 Monostable multi-vibrator	£1.02
AE7 RC generator	£1.06
AEB Bass filter	99p
AE9 Treble filter	99p
AE 10 CCIR filter	990
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AF25 Mixer	£3.60
AF30 Mono pre-amplifier	£2.61
AF35 Emitter amplifier	£2.27
AF80 0.5W mic. amplifier	£4.22
AF305 Intercom	£9.52
AF310 Mono amplifier	£5.91
AT5 Automatic light control	£2.58
AT25 Window wiper robot	£5.82
AT30 Photo cell switch unit	£5.70
AT50 400W triac light	
AT56 2,200W triac light	£4.80
dimmer/speed control	£6.90
umaner/speed controt	LO.SU

AT50 400W triac light
dimmer/speed control £4.80
AT56 2,200W triac light
dimmer/speed control £6.90
AT60 1 channel light control., £7.80
AT65 3 channel light control, £14.55
GP304 Circuit board£4.94
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for use with 2 x AF310 £21.27
GP312 Circuit board£11.45
GU330 Tremolo unit£7.50
HF61 Diode detector£3.32
HF65 FM transmitter£2.70
HF75 FM receiver £2.87
HF310 FM tuner£15.81
HF325 Deluxe FM tuner £24.12
HF330 Decoder (HF310/325) £9.96
HF380 lw/vhf aerial amplifier £4.94
HF395 broadband aerial amp. £1.77
LF380 Quadraphonic device £11.36
M160 Multi-vibrator £1.71
M191 VU Meter
M192 Stereo balance meter £4.97
NT10 Stabilised power supply
100mA, 9V£6.15
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1139

The Sinclair Cambridge... no other calculator is so powerful and so compact.

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*Uniquely handy package.

Cambridge

The Cambridge - new from Sinclair

The Cambridge is a new electronic calculator from Sinclair, Europe's largest calculator manufacturer. It offers the power to handle the most complex calculations, in a compact, reliable package. No other calculator can approach the specification below at anything like the price - and by building it yourself you can save a further £5.50!

Truly pocket-sized

With all its calculating capability, the Cambridge still measures just $4\frac{1}{2}$ " x 2" x $\frac{11}{16}$ ". That means you can carry the Cambridge wherever you go without inconvenience – it fits in your pocket with barely a bulge. It runs on ordinary U16-type batteries which give weeks of life before replacement.

Easy to assemble

All parts are supplied - all you need provide is a soldering iron and a pair of cutters. Complete step-by-step instructions are provided, and our service department will back you throughout if you've any queries or problems.

Total cost? Just £27.45!

The Sinclair Cambridge kit is supplied to you direct from the manufacturer. Ready assembled, it costs £32.95 - so you're saving £5.50! Of course we'll be happy to supply you with one ready-assembled if you prefer - it's still far and away the best calculator value on the market.

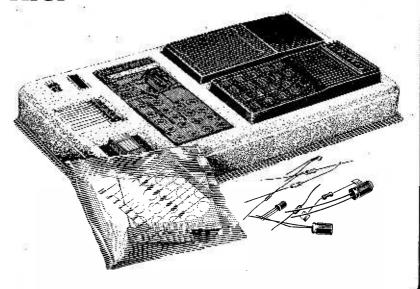


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The kit comes to you packaged in a heavy-duty polystyrene container. It contains all you need to assemble your Sinclair Cambridge.
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- 2. Large-scale integrated circuit.
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- Case mouldings, with buttons, window and light-up display in position.
- 6. Printed circuit board.
- 7. Keyboard panel.
- 8. Electronic components pack (diodes, resistors, capacitors, transistor).
- Battery clips and on/off switch.
- 10. Soft wallet.



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If you just use your Sinclair Cambridge for routine arithmetic – for shopping, conversions, percentages, accounting, tallying, and so on – then you'll get more than your money's worth.

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The reason's simple: only Sinclair – Europe's largest electronic calculator manufacturer – have the necessary combination of skills and scale.

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But that in itself wouldn't be enough. Sinclair also have a very long experience of producing and marketing electronic kits. You may have used one, and you've almost certainly heard of them – the Sinclair Project 60 stereo modules.

It seemed only logical to combine the knowledge of do-it-yourself kits with the knowledge of small calculator technology.

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The Sinclair Cambridge is fully guaranteed. Return your kit within 10 days, and we'll refund your money without question. All parts are tested and checked before despatch – and we guarantee a correctly-assembled calculator for one year. Simply fill in the preferential order form below and slip it in the post today.

Price in kit form: £24.95 + £2.50 VAT. (Total: £27.45) Price fully built: £29.95 + £3.00 VAT. (Total: £32.95)

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ETY FIRS

O encourage safety in the mere presence of electrical, electronic, radio or television apparatus, let alone during their operation, is not only laudable but vital. Hence the British Electrotechnical Approvals Board for Household Equipment (now affectionately BEAB) is extending the BEAB Approval Scheme to include audio and radio products including record players, radios, radiograms, mains/battery portable receivers with (curiously) "continuously rated audio outputs up to 6 + 6 watts stereo or 10 watts mono". Manufactured equipment that is licensed to bear the BEAB approval marking has to be first subjected to some detailed and stringent tests at the BSI laboratory.

The specification for the tests, detailed in BS 415: 1972 (with amendments), highlights for the more casual of the manufacturers, and probably some of the amateur constructor fraternity, areas of potential risk in mains driven equipment that all too often are taken for granted. There are, of course, extreme cases like the ladies' dangling necklace test and the test which inserts artificial fingers into apertures almost in determination to find live contact.

Generally the scheme is an excellent one. In most British equipment, that is designed and manufactured by responsible people, it is unlikely that no thought will be given to hazards such as shock, fire risk, ionised radiation,

implosion and the like.

What has been needed is some form of yardstick by which a known hazard can be measured. Let us not be carried away by any thought that this standard is for manufacturers only. There are frequent cases where more strict attention to detail is needed by everyone who has mains driven appliances or electronic equipment.

We have only one serious complaint: that is the use of graphical symbols to indicate the nature of the supply (a.c. or d.c.) and to indicate live terminals. To the uninitiated layman, technical symbols mean nothing and he will not be inclined to buy BS3939 to find out before operating his

Elsewhere in this issue we have highlighted only a few of the points in BS415 that we feel the general public need to know about. It is stressed that the detailed specification is designed to cover most contingencies of normal operation; we recommend manufacturers, suppliers and users to refer to this for more information.

M. A. COLWELL—Editor.

The May issue of Practical Wireless will include a special pull-out feature to make a handy booklet "Guide to Long Distance Reception of Radio and TV", (useful for locals, too!). Also appearing will be constructional projects: the medium wave "Mini-Pop" (goes in a jacket pocket); an audio booster and power supply to enable you to hear cassette recordings in the car; a frace doubler to enable you to convert a single-beam oscilloscope for four displays. We shall also be giving first details of a super new project that we know will appeal to sports fans all over the world. Don't miss out-order your copy regularly NOW.

(All advanced details are subject to the current national industrial situation).

Further details on page 1167

Export sales of British made Dolby

'N a recent statement Phoenix Videosonic Ltd., of Braintree, Lessex, Europe's only manufacturer of Dolby Noise Reduction Units announced significant export sales to Europe, North

America and Japan.

A Videosonic spokesman stated: "Videosonic leads the world in the technical specification of its equipment: in the PD4 we have introduced a new high level Dolby 'B' circuit providing a unique range of over 95dB between noise and 0.1% distortion. At this time the PD4 represents the ultimate way to take the PSSST! out of tape.

To further extend our lead in the World Hi-Fi market, the PD2b has been introduced as the world's first battery operated Dolby Unit, allowing 'field' use in the most rigorous conditions. The integral microphone pre-amplifier makes this an ideal unit for re-

porter or similar usage.

World recognition of Videotechnical manufacturing competence has been most encouraging, and we can only take pride in our immediate penetration of the Japanese market in the face of very strong local competition. We are advised that our range of Dolby products will be displayed and demonstrated in the top 850 Hi-Fi Retail Shops in Japan, and that local response to date has been very positive. Our first shipment to Japan leaves this week.

Portable Fluorescent Lamp (March P.W.)

7ILL readers please note, that the transformer specified is now no longer available. An improved transformer is available from Messrs G. F. Milward at 77p plus 20p p & p. This includes full modification details and uses fewer components. A 21 in. 13W tube is available at 50p + 20p p & p, and it is claimed that this tube gives a greater light output than the 15W tube. S.A.E. to G. F. Milward for further details.

NEWS...

NEWS...

NEWS...

Bargains galore

F you are in the "Ally Pally" area on March 24th, pay a visit to the Collector's Bazaar which is being held in the Palm Court.

This is a five-bazaar event which includes militaria, vintage post cards, vintage toys, transport relics and, of most interest to our readers, vintage records, horn gramophones, phonographs and probably some items of vintage radio equipment.

Practical Wireless visited one of these bazaars held at St. Johns Wood a few months ago, and it was there that Colin Riches purchased an Edison "Gem" phonograph to be featured in a future "Going Back."

If any readers want to find out the details of hiring a stall at the bazaar (£3.50 for the day) contact the organiser John Carter, Smewins, Shottesbrooke, nr. Maidenhead, Berks, SL6 3SR (Tel. Shurlock Row 539).

Otherwise, put on your cycle clips and pedal along to Alexandra Palace, Wood Green, London N.22, on March 24th. They'll let you in at 1 p.m. but be sure to have your entrance fee of 30p at the ready.

Hi-Fidelity 74

I-FIDELITY 74 is a rival exhibition to the Sonex show. It will be run at the same time and held at the Heathrow Hotel, Bath Road. It's the idea of Malcolm Blockley who is the Hi-Fi Division Sales Manager of Pyser-Britex Ltd.—the sole UK distributor of Marantz, Teledyne and Kensonic equipment.

The organiser states that this show has been arranged because many manufacturers are fed-up with trying to demonstrate their products in small, cramped hotel bedrooms.

Hi-Fidelity 74 will run from March 27th to 31st inclusive but the first two days will be for the trade and press only.

Blast them out!

N order to reduce the effects of interference from an East German station at night, the BBC has increased the transmitting power of the Radio 4 Moorside Edge transmitter to 300kW.

R and TV Components Ltd.

the price of postage and packing for the "Stereo 21" should have read £1 60. Apologies to R and TV Ltd.

Public Address Exhibition

Readers who have an interest in outdoor activities, such as rallies, will be planning events for the coming season. To get up to date on public address installations, it would be worthwhile to visit Sound '74, the international exhibition of the Association of Public Address Engineers. A lecture programme will be held concurrently on p.a. design, building acoustics, microphones, and the financial side of public address work from the practical point of view.

The A.P.A.E. has received more stand space bookings than previously, but there are still a few left for those who wish to come in at a late stage, including suppliers of disco equipment.

Admission is free to all in-

Band IV

Band V

Band VI

(u.h.f.)

(u.h.f.)

(s.h.f.)

terested persons: tradesmen, manufacturers, buyers, and users of public address and allied equipment in the entertainments business. Tickets can be obtained from exhibitors or from the A.P.A.E. Secretariat, 6 Conduit Street, London W1R 9TG.

The scope of activities covered is extended to include audio-visual effects.

Overseas readers will be interested to learn that the A.P.A.E. are exhibiting in Hall 9A at the Hanover Fair from 25th April to 3rd May 1974 and at the L.C.E.T.I.A. exhibition at Melbourne, Australia from 7th to 11th October.

Practical Wireless will be on show at the Hanover Fair.

UK wavebands and frequencies

THE BBC Engineering Department have issued a useful data sheet which shows the frequencies and wavebands allocated to broadcasting in the United Kingdom. Below we give the details from that sheet:

Band		Frequencies	Service
Low frequence (long wave		160–255kHz (1875–1176m)	
Medium frequence (medium w		525–1605kHz (571–187m)	
High frequen	cy (h.f.)	3950-4000kHz (75-m band)	<u> </u>
(short wave	es)	5950-6200kHz (49-m band)	Ì
	•	7100-7300kHz (41-m band)	≻a.m. radio
		9500-9775kHz (31-m band)	
		11700-11975kHz (25-m band)	
•		15100-15450kHz (19-m band)	
		17700-17900kHz (16-m band)	İ
		21450-21750kHz (13-m band)	
	,	25600-26100kHz (11-m band)	j
Band I	(v.h.f.)	41-68MHz (channels 1 to 5)	405-line television
Band II	(v.h.f.)	88-97 · 6MHz	f.m. radio
Band III	(v.h.f.)	174-216MHz (channels 6 to 13)	405-line television

470-582MHz (channels 21 to 34)

614-854MHz (channels 39 to 68)

11700-12500MHz

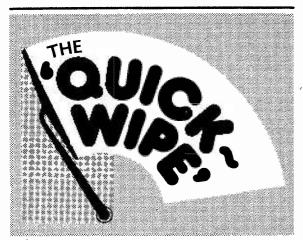
(11.7-12.5GHz)

625-line television

625-line television

Not yet in use for

broadcasting

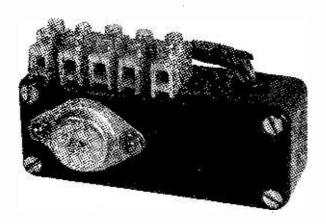


A VARIABLE TIME SWEEP WINDSCREEN WIPER RS

P. S. COLLINS

MAGINE the situation: you are driving your car in drizzly rain, you put on the windscreen wiper. One sweep is sufficient, so you switch it off. Five, ten or fifteen seconds later the windscreen needs another wipe, so you switch on the wiper again for another single stroke. This could go on for some time and tends to be wearisome.

The circuit here described saves this tiresome routine and allows you to relax in the automation of a variable time-sweep wiper. Although the circuit is designed for wiper motors with automatic parking facility, there is some information at the end of the article which will be helpful to those who have wiper motors without this facility.



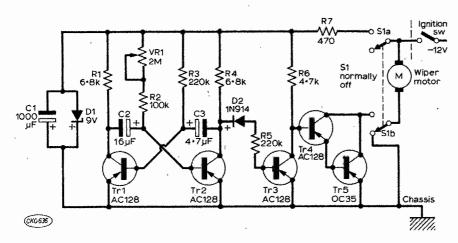
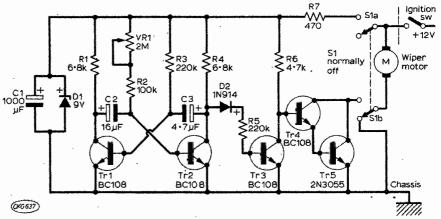


Fig. 1. Circuit of the Quickwipe for a vehicle with a POSITIVE earth system. It is essential to be quite sure which side of the battery is connected to chassis.

Fig. 2. In this circuit for a **NEGATIVE** earth system, different transistors are used and capacitors and diodes are reversed compared to those in Fig. 1.



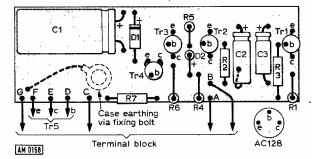
Figures 1 and 2 are the circuits for positive and negative earthed vehicles; the difference lies only with the active components and reverse connection of the polarised ones. The circuit action remains the same. Tr1 and Tr2 form a multivibrator generating a pulse of fixed length with a variable repetition rate. VR1 allows this rate to be varied between approximately 3 and 30 seconds. Tr3. 4 and 5 form a pulse amplifier to drive the wiper motor.

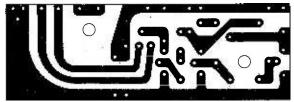
The fixed pulse length is ³₄, second which is sufficient time to drive the motor long enough for its internal switches to take over the drive and thus return it to the park position. Switch SI is centre off. One switch, SIb, switches for continuous operation, earth being directly applied to the motor.

In the other position, S1a, applies 12 volts to the circuit and S1b connects the motor as the load for the pulse amplifier. The vehicle wiper switch may now be regarded as redundant, or left in the circuit, as desired.

CONSTRUCTION

The whole unit can be comfortably housed in a die-cast box measuring 3^{1}_{2} x 1^{3}_{8} x 1^{1}_{8} in. Figure 3





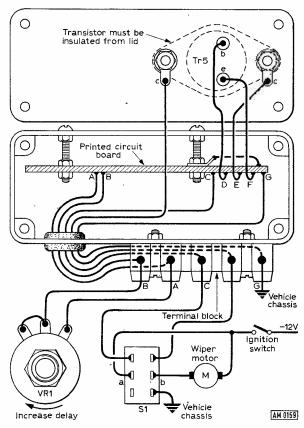
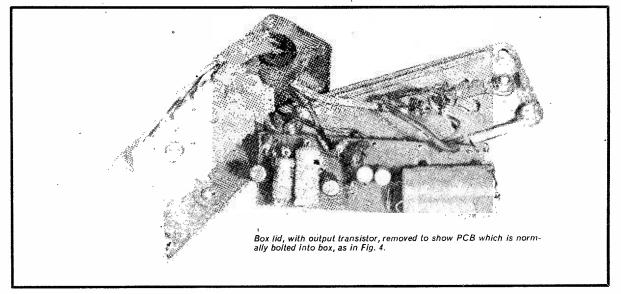


Fig. 3, left, shows PCB actual size and component layout for POSITIVE earth unit. Fig. 4, above, illustrates external wiring of Quickwipe.

shows the printed circuit board. Tr5 is mounted on the lid with insulating washer and bushes. All leads from the circuit board and Tr5 are connected to a five-way terminal strip fixed to the side of the box. This enables easy connection to the vehicle's wiring, as shown in Fig. 4.

Confirm the chassis polarity of the vehicle before constructing the unit, then use Fig. 1 OR Fig. 2 as appropriate.



Resistors

6-8k0 R1 R2 100kΩ

R5 220k() R6 4.7kQ

R3 220kΩ 6.8kΩ

R7 470Ω VR1 2MΩ linear

Resistors 10% 4W except R7 4W

Canacitors

C1 1000 pF 25V C2 16 pF 16 V C3 4 7 pF 16 V

Semiconductors

D1 9V zener 400mW

D2 1N914

Positive Earth Tr1-4 AC128 Tr5 OC35

Negative Earth Tr1-4 BC108

Tr5 2N3055

Miscellaneous

S1, Double pole-double throw switch, centre off. Diecast box (RS Comps.—"Box 992"). Printed circuit board. Insulation kit for Tr5. Five way terminal block

NOTE: It may be possible to arrange the fixed pulse length to correspond with the time taken for the wipers to travel one complete sweep, in the case of wipers without the self-park facility. This could be achieved by altering the values of R3 and C3.

These points are offered only as helpful guides. The author has conducted no tests in this regard and cannot therefore give any facts regarding accuracy or success.

LCHNICK ZZE No. 3 Solution

<u>'U</u>	_	E	<u>'S</u>		٩V	9	B	$^{\circ}R$	A	T	0	8R
	E					M		E		U		E
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^{28}R	0	C	H	Ε	L	L	Ш		²⁹ S	E	T	S

ELEVISION

IN THE APRIL ISSUE

CLOSED-CIRCUIT TV

frext month we start a new series aimed at giving anjessed tally practical account of closedcircuit TV equipment, its use and the servicing techniques required. To start with, the basic element in CCTV work, the vidicon camera lube. is explained along with its basic circuity.

TRANSISTOR FIELD TIMEBASES

Fully transistuated field timebases have been around for some time now, particularly in colour receivers, and have proved to be periorally very reliable. Nevertheless it is time we took a look at common faults and their causes, also at the operation of the class A output stage generally used

THE DIODE DROPPER

The use of a dioge dropper in the heater circuit reduces heat dissipation and is also cheaper. than, using a completely resistive dropper. The action of the diode dropper circuit is attan misunderatood however, which can lead to the use of an incorrect accompanying resistor value. and damage to the valves in the chain. The circuit action will be explained and the procedure for determining the value of the accompanying resistor given, either for designing a new circuit or for working out a diode dropper substitution for an existing set.

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multi-range test meters

H. LEEMING G3LLL

To does not seem many years since test meters were so expensive that, in the radio and TV trade, at least, one was shared between several engineers, the losers having to make do with wet fingers and neon screwdrivers! Test meters are now relatively cheap so that no enthusiast or handyman can really afford to be without one; whether it be for attending to the Hi-Fi system, fixing the car, or even sorting out a fault on the front door bell. Despite their simplicity in operation these meters can deceive the unwary and so it is hoped that a little basic theory will be of practical assistance.

The multi-range test meter commonly contains ranges such as AC and DC voltage, DC current and at least one resistance range. Other functions may be included on the more elaborate instruments but all use the basic meter movement plus the switching of various internal components in or out of circuit.

The DC Voltmeter

The meter movement fitted to most modern test instruments needs a current of something in the range of 1 to 1/100 of a milliamp to move a pointer across the full extent of the scale. The theoretical circuit of the basic meter movement is shown in Fig. 1. The "internal resistance" is not an actual resistor, but is the resistance of the coil of wire in the meter movement. From Ohm's Law, (voltage=current×resistance) this lmA meter movement shown will require a voltage of 0.1 volt for full scale deflection, $(1/1,000\times100/1=0.1$ volt). This basic meter could therefore be used to measure voltages of up to 0.1 volt or currents of up to 1 milliamp—not very useful!

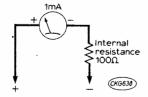


Fig. 1: Representation of meter movement must include resistance of moving coil,

The meter movement is basically a current operated device, but it can be made to read various quantities. A little thought will show that a 1mA meter movement will read full scale if 1 volt is

applied to it through a series resistance which, including internal resistance, totals 1,000 ohms. From Ohm's Law, 1 volt across 1,000 ohms causes a current of 1mA to pass. A voltmeter using a 1mA meter movement is said to have a sensitivity of 1000 ohms per volt.

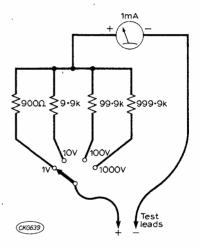


Fig. 2: Series resistors for voltmeter allow for coil resistance. Only of importance on lower ranges.

Fig. 2 shows the meter wired to read four ranges of voltage and it will be seen that the total resistance of the meter is 1,000 ohms for every volt of the range in question. For this reason it is referred to as 1,000 OPV and this would usually be marked on the meter scale.

Such a meter does have its disadvantages and its relatively low resistance can greatly affect circuit voltages as will be shown. In Fig. 3a two 1 ohm resistors are connected across the supply and the voltage between X and Y is measured. If the meter is switched to the 1 volt range it has a total resistance of 1,000 ohms (remember 1,000 OPV) this resistance being shunted across R2. As the meter resistance is very high, compared to R1 and R2, its effect is negligible and the reading is given accurately as 0.5 volts. If, however, the meter is transferred to the circuit in Fig. 3b and another reading is taken the resulting accuracy is quite different. Once again, the reading should be 0.5 volts, but note what happens when the meter is

connected across R2. R2 is shunted by the meter's resistance of 1,000 ohms and the resistance of the bottom half of the circuit drops to around 900 ohms. The voltage divides itself according to the ratio of the resistors and the meter reads just below $0\cdot 1$ volts.

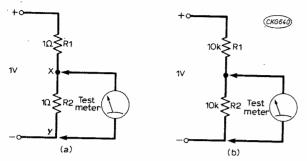


Fig. 3 (a) and (b): to demonstrate effect of meter resistance on high and low resistance circuits.

The meter is not really wrong, it simply reads the voltage that is present when it is connected. Using the same meter a more accurate reading could be taken by switching to the 10 volt range when the test meter's resistance would rise to 10,000 ohms; the meter's resistance in parallel with R2 would then total 5,000 ohms and whilst the voltage reading would still be low at 0.33 instead of 0.5, it would be a little more realistic. Could we take the same argument further and switch to the 100 volt range with a meter resistance totalling 100,000 ohms, and obtain an accurate result? Unfortunately, no, since when the meter was switched to this range the pointer would move so little that we would not be able to take an accurate reading from it.

If we want a more accurate reading in a high resistance circuit the answer is a more sensitive meter movement that will allow us to insert larger values of voltage multiplier resistors. If for instance, we substitute a meter with a 50 micro-amp movement, (0.05mA), we will obtain a sensitivity of 20,000 OPV. Using circuit Fig. 3b we would then obtain, on the I volt range, a reading that was almost correct, (20,000 ohms being shunted across R2), or by switching to the 10 volt range using this higher sensitivity meter we would obtain a reading that was accurate to within all normal requirements.

As has been illustrated, the DC voltmeter can only read the voltage which is present when it is connected. It cannot guess at the voltage which appears when it is disconnected. When using a voltmeter one should get into the habit of comparing the resistance of the range being used with the resistance of the circuit being measured.

In many cases when operating in a high resistance circuit a more accurate reading will be obtained if a higher voltage range is used. If in doubt a reading should be taken on two adjacent ranges of the test meter. With any good quality instrument these readings should be about the same, but if they are not it implies that the meter is loading the circuit on the lower voltage range.

Valved or Transistorised Voltmeters

To obtain higher sensitivities using normal techniques requires very expensive and delicate meter movements. It is not common practice, therefore, to make multi-range test meters with a sensitivity

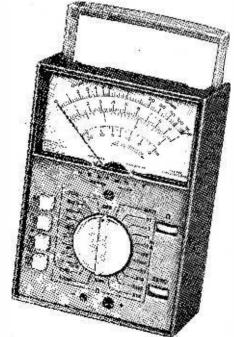
of much over 50,000 OPV. In some circumstances an even higher sensitivity is required, so that test meters of as high a sensitivity as this would be of little use at measuring, say, 0·1 volts in a circuit with resistance of several megohms. To enable higher sensitivities to be obtained, the valve and then the transistorised voltmeter were introduced. In these devices amplification is used so that an input resistance of 10 megohms or more is presented, even on the lowest voltage ranges. Such instruments are essential if tests are to be made in some high impedance transistorised circuits where very small voltages are present.

Frequency Response

Most test meters are basically intended for making tests at the mains frequency and their accuracy often falls off at frequencies in the audio range. One should check the frequency response of a test meter before relying upon it to check audio or bias frequency voltages. In the latter case it should be remembered that high frequency bias voltages can damage the rectifier in some test meters, and also that even if the meter's frequency response is adequate that its loading (possibly only a few hundred OPV) can, in many circuits, much reduce any voltage present. If it is desired to accurately measure voltages at high audio or radio frequencies the valve or transistorised voltmeter is again essential.

The AC Voltmeter

The AC ranges of multi-range test meter function in very much the same way as the DC ranges except that a rectifier is incorporated to enable the basic DC meter movement to function, see Fig. 4. As with the DC voltage section of the meter, the amount of loading on the circuit being tested is indicated by the sensitivity in ohms-per-volt. Rectifiers have a tendency to be non-linear at low current



The Heathkit IM-104 mu timeter, a modern design providing 53 ranges on four scales. Frequency response up to 50kHz on AC voltage ranges. Input resistance of 10 M\(\Omega\) on DC voltage ranges. (Courtesy Heath (Glos.) Ltd.)

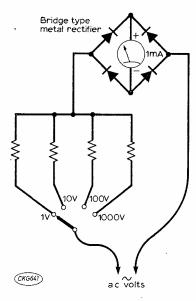


Fig. 4: Incorporation of meter bridge rectifier on AC voltage ranges.

levels and so, in the interest of accuracy, it is common to reduce the sensitivity of the test meter when switched to the AC ranges. The popular Avo Model 8, for instance, has a sensitivity of 20,000 OPV on the DC ranges but only 1,000 OPV on the AC ranges.

The Direct Current Ranges

The basic DC meter movement, as we have seen, will reach full scale when a small current is passed through it. The example shown in Fig. 1 needed ImA for full scale deflection. If it is desired to measure a larger current, some of the current must be by-passed. The circuit with various resistors which are known as "shunts" is shown in Fig. 5. The value of shunt resistor R3, for instance, is calculated so that when the test meter is measuring 1A, 999 milliamps go via R3 and 1mA passes through the meter.

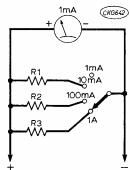


Fig. 5: Switchable shunts to increase current range of basic meter.

It is important to note that when measuring current, some voltage is required to operate the meter, as was shown earlier, when dealing with the DC voltmeter. In this case 0·1 volts will be dropped across the meter terminals. In most cases when making measurements, as in Fig. 6a, this small voltage drop will make negligible difference, being small in relation to the voltages in the circuit. If we try to make a test as shown in Fig. 6b however,

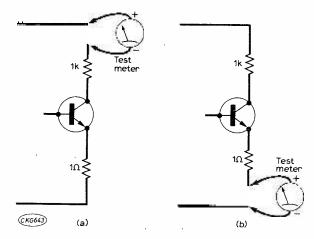


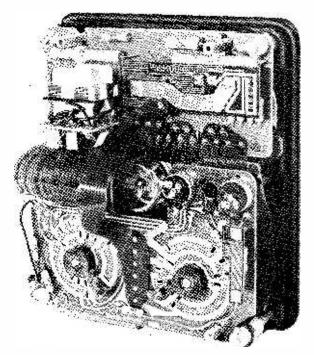
Fig. 6 (a) Correct and (b) incorrect method of inserting meter in transistor circuit.

this is not the case. Here the effect of adding the meter in series with the circuit is to considerably increase the value of the emitter resistor. Increasing this effective value would mean that the current which flowed with the test meter connected would be much less than the current which normally flowed in the circuit.

When checking current flow in low impedance circuits, it is better to measure the voltage across a known resistor and then to calculate the current.

The Resistance Ranges

Figure 7 shows a basic method of resistance measurement. If the test prods are touched together R2 can be adjusted until the meter reads full scale, the current being provided by the battery. As we have seen a 1mA meter when used as a voltmeter



An excellent view of the latest AVO Model 8. It uses printed circuit techniques for shunts and switchboards. (Courtesy AVO Ltd. Dover)

has a sensitivity of 1,000 OPV and here, if the battery is exactly 1.5V, R1 plus R2, plus internal resistance must equal 1,500 ohms, when R2 is set to provide full scale deflection with the test prods touching. If now, instead of touching the test prods together, we connect them to a resistor being tested, of 1,500 ohms, the meter will then read half-scale as an external resistor of the same value as the built-in resistance has been added to the circuit. The centre of the scale would be marked 1,500 ohms and with suitable calibration resistors of between, say, 50 and 50,000 ohms, resistors could be checked using this set-up, with reasonable accuracy.

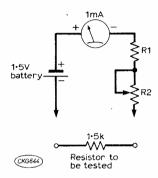
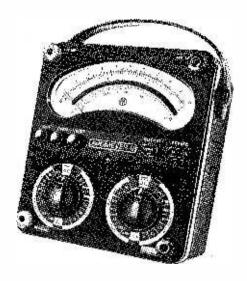


Fig. 7: Basic circuit for measuring resistance.

To divide the range by 10 we can shunt the meter as was done on the current ranges so that the sensitivity of the circuit becomes 100 OPV, enabling R1 and R2 to be reduced to 1/10 of their previous value. Alternatively, we can multiply the range by 10 by fitting a 15V battery and increasing R1 and R2 tenfold. In this way we obtain a meter with a centre scale range of 150, 1,500 and 15,000 ohms on three ranges enabling resistors from below 10 to above 500,000 ohms to be checked with good accuracy.



A large, clear scale with an anti-parallax mirror is the highlight of the latest AVO.

Use of Ohms Range

From the above discussion it will be seen that a current is passed through the component to be tested and that a voltage is also applied across it. In most cases this will do no harm, but it is wise to be aware that voltages of up to 25 or so are possible on the high resistance ranges and that currents in the order of 100mA or more may be found on the low ohms ranges of some test meters. When checking circuits where there is the slightest risk of damage being caused, it is wise to avoid using the highest or lowest ohms range on the test meter and to concentrate tests on the range which applies low voltage and low current. If magnetic devices, such as tape heads, are tested, note that they will be magnetised by the meter current. These tests should not be made, therefore, unless a defluxer is available to remove the residual magnetism.

It should be noted that no checks of resistance can be made unless the circuit which is being tested,

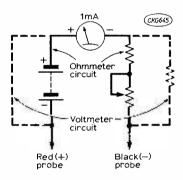


Fig. 8: Illustration of reverse polarity of probes in an ohmmeter circuit.

is completely dead. All voltage sources should therefore be disconnected before tests take place, as, quite apart from giving the wrong results, severe damage can be caused to the test meter and equipment if resistance tests are attempted on live circuits. Devices such as transistors, diodes and electrolytic capacitors are inherently polarity sensitive so the polarity of the voltage output of the test meter should be noted whilst making tests on these devices. As will be seen from Fig. 8 using normal circuit arrangements the polarity of the test prods is normally opposite on the ohms range to that marked on the meter for the voltage and current ranges.

Decibels

Many test meters have a scale marked in decibels marked in + and - values over a total of 15dB's or so. It must be clearly understood that the decibel is **not** an absolute value, such as the ohm or volt, but, as will be seen from the shape of the dB scale, is a logarithmically based system of comparison. Whilst many test meters are calibrated so that 0dB=0.775V this is just an abitrary figure. In practical use, such as measuring the frequency response of an amplifier, the signal level is adjusted so that the output when measured with the test meter set to a suitable range, reads 0dB. If the input frequency is then varied the output variation, and hence the frequency response of the equipment being tested, can be read off directly in decibels.

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	C83	0.45	EL84	0.47	PCH200	0.88	UBCBI	0.70	207.17	0.90
EC	C84	0.55	EL85	0.55	PCL82	0.54	UBF89	0.60	30L17	
EC	C85	0.58	EL86	0.95	PCL83	0.66	UCC85	0 60	30P4MR	1 30
EC	CC88	0.75	EL95	0.70	PCL84	0.59	UCH81	1.00	30P12/PC	801
EC	C189	0.71	EL91	1.31	PCL85	0.63	UCL82	0.70		1.05
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AZ31	0.55	EF85	0 35	PC88	0.80	UF41	0.75	6X4	0.40
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CL33	1.50	EF89	0.28	PC900	0-48	UL84	0 43	7B6	0.75
CY31	0.50	EF91	0.37	PCC84	0.40	UY41	0.48	7B7	0.70
DAF91	0.30	EF92	0.50	PCC88	0.55	U X 85	0 40	7C5	1.30
DAF96	0.50	EF95	0.40	PCC89	0.50	V B 105-30		7C6	0.75
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DL92	0.40	EL36	0.50	PCF805	0.90	1T4 384	0.30	12AT7 12AU6	0.40
DL94	0.48	EL37	2.50	PCF806	0.75	3V4	0·40 0·70	12AU6 12AU7	0.33
DL96	0 55	EL41	0.90	PCF808	0.90	5R4GY	0.80	12AX7	0.38
DY86/7	0.36	EL42	0.90	PCL82	0.35	5U4G	0.40	12BA6	0.45
DY802	0.37	EL84	0 28	PCL83	0.68	5V4G	0.50	12BE6	0.50
EARC80	0.38	EL95	0 40	PCL84	0.45	5Y3GT	0 45	30C1	0.80
EAF42	0.75	ELL80	1.00	PCL85	0.50	524G	0.45	30C15	1.05
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AD140	0.50	BF898 0 25	OC28 0-70	ZTX550	0.18	2N2905A	0.32
AD149	0 50	BFX29 0-28	OC35 0.55	1N914	0.06	2N2906	0.20
AD161	0.39	BFX88 0.22	OC36 0 65	IN4001	0.6	2N2926	0.10
AD162	0.39	BFY50 0.20	OC42 0-40	IN4002	0.7	2N3053	0.20
AF115 AF116	0·25 0·25	BFY51 0-20 BFY52 0-20	OC44 0-18 OC45 0-18	IN4003 IN4004	0.8	2N3055 2N3525	0.60
AF117	0.20	BFW10 961	OC71 0-15	IN 4005	0.10	2N 3614	0.59
AF186	0.40	BY100 0.15	OC72 0-25	IN4006	0.12	2N3615	0.65
AF239	0.44	BY126 0.14	OC76 0 30	IN4007	0.12	2N3702	0.11
ABY27	0 80	BY127 0-15	OC77 0.55 OC81 0.28	1N4009	0.08	2N3703	0.12
ASY28 BA102	0.25	BZX61 series 0.20	OC81D 0.28	1N4148 18921	0.06	2N3704 2N3705	0·14 0·12
BA115	0·25 0·10	BZY88 series	OC81Z . 0-45	182033	0 20	2N3705	0.10
BC107	0.12	0 10	OC83 0 25	182051A	0-10	2N3707	0.13
BC108	0.12	CRS1-05 0-30	OC140 0-65	132100A	0.20	2N3708	0.07
BC109 ·	0·12 0·16	CRS1-40 0-45 CRS3-05 0-40	OC170 0.25 OC171 0.30	183010 2N696	0·25 0·15	2N3709	0.10
BC113 BC117	0 21	CR83-05 0 40 CR83-40 0 55	OC200 0.55	2N 697	0.15	2N3710 2N3711	0·11 0·11
BC143	0 30	MJE340 0.50	OC201 0-80	2N706	0.10	2N3819	0.35
BC147	0.12	MJE370 0-68	OC202 0-90	2N706A	Q·12	2N3320	0.50
BC148	0.10	MJE520 0.65	OC203 0.55	2N1131	0.25	2N3823	0.50
BC169C BC182	0·14 0·12	MJE2955 1.10 MJE3055 0.75	OCP71 1-00 ORP12 0-55	2N1132 2N1302	0 25 0 18	2N3903	0.15
BC182L	0.12	MPF102 0:40	ORP60 0.45	2N 1302	0.18	2N3904 2N3905	0·20 0·25
BC184L	0 13	MPF103 0-36	T1005 0-20	2N1304	0.22	2N 3906	0.16
BCY32	1 20	MPF104 0-35	TIC44 0-29	2N1306	0.22	2N4058	0.15
BCY33	0.38	MPF105 0-46	TIC226D 1-50 TIL209 0-25	2N1306	0.28	2N4059	0.10
BCY34 BCY70	0-45 0-15	NKT404 0.60 OA5 0.60	TIL209 0.25 TIS43 0.26	2N1307 2N1308	0.28 0.28	2N4060 2N4061	0·13 0·13
BCY71	0.20	OA10 6-40	ZTX 107 0 12	2N 1309	0.30	2N4062	0.14
BCY72	0.15	OA79 0-10	ZTX108 0-10		0.20	3N141	0.81
BCZII	0.65	OA81 0-10	ZTX300 0.14	2N1614	0.45	40360	0.40
BD121	1.00	OA91 07 OA200 0.08	ZTX301 0.14 ZTX302 0.20	2N2147	0.75	40361	0.45
BD124 BD131	0 80		ZTX302 0.20 ZTX304 0.24	2N2160 2N2369A	1.00 0.16	40362 40430	0·40 0·85
110101	0.30	0.120x 0.10		241 20 VSA	0.70	40400	0.00
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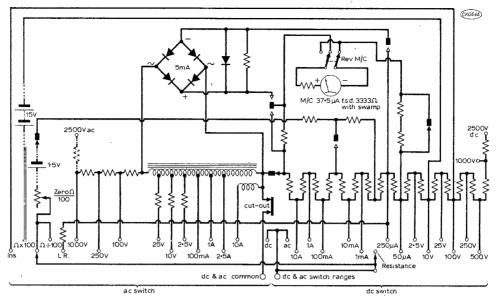


Fig. 9: Basic circuit of the Model 8 Avometer Mk II to show the complexity of a modern multi-meter. (Courtesy AVO Ltd Dover)

To be really useful in making this kind of test the response of the test meter and the output of the audio generator must be flat with frequency, otherwise one is liable to end up in the position of the wheel-tapper who condemned 100 wheels only to find he had a cracked hammer! Remember, it costs next to nothing to print a decibel scale on a meter but it costs pounds to incorporate the response and accuracy needed to make it really meaningful for even simple audio frequency response measurements.

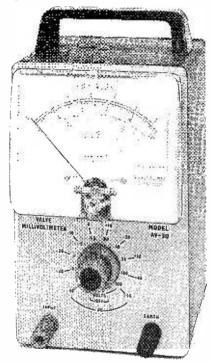
Precautions in use

Multirange test meters are precision instruments which can easily be damaged by over-loading. Whilst many meters have built-in automatic protection, these circuits only give a **limited** protection; they do not cater for gross overloads. A moments carelessness can leave an instrument which is beyond economical repair. To avoid disasters follow the makers' instructions, together with the following suggestions:—

- Always leave the instrument switched to a high voltage range when not in use. Never on a current or ohms range.
- Never connect meter to any live circuit when switched to ohms.
- Be extra careful to avoid short circuits when using the current ranges.
- 4. When measuring unknown voltages or currents switch to the highest range **first**, and only change over to a lower range if less than, say, one third of full scale deflection is registered.

Buying a meter

There is a host of small test meters available, many of which should be more than adequate for the average hobbyist. Aim to get a meter which has a sensitivity of 10,000 OPV or more on the DC ranges and which has a scale which is clear to read. A resistance range coverage of from, say, 1 ohm to 2 megohms, will fill most needs. AC current ranges are not really of any great importance, as



This valve millivoltmeter, type AV-3U, is mains operated and has a sensitivity of 10mV f.s.d. on the lowest range and 300V RMS on top range. (Courtesy Heath (Glos.) Ltd.)

current can always be calculated from resistance and voltage measurements, but a few DC current ranges will be found useful.

When comparing meters it can be advantageous to take along a battery and a few known values of resistors. There is nothing like a practical test to prove whether readings are plain and straightforward or confused and ambiguous. The cost?—£15 will buy a meter which is likely to be more than good enough but look around and testers costing well under £10, which are by no means cheap and nasty, can be found.

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PART 6—GROUNDED EMITTER AMPLIFIERS

AST month's emitter followers were all types of current amplifiers. In every case the output voltage was the same, or slightly less than the input voltage. Many applications require voltage amplification-e.g. raising the output level of a microphone to an extent that when current amplification is applied the resultant signal could drive a loudspeaker. The grounded emitter amplifier will provide a reasonable degree of voltage and current amplification and is, perhaps, the most used type of amplifier stage in the whole of electronics. Because both voltage and current is amplified we call the grounded emitter stage a power amplifier but not necessarily in the sense that you can expect several watts of useful output; specialised power stages are better equipped for the latter purpose and these will be covered later in the series.

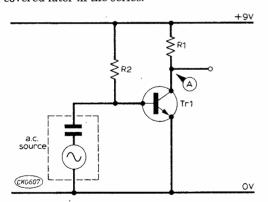


Fig. 42: It is difficult to predict a value for R2 to set the potential at A to mid-rail unless the h_{FE} for Tr1 is accurately known.

Referring to Fig. 42, we know that we can make the voltage at point A go to +9V by ensuring that the transistor is cut off (i.e. by passing zero base current) and conversely we can make it fall to zero volts by passing a certain amount of base current through R2. By knowing an accurate value of $h_{\rm FE}$ for the transistor we could calculate a value for R2 that will cause just sufficient collector current to flow that the voltage drop across R1 will be 4.5V. Theoretically we could hold the voltage at A exactly

mid-way between the two supply rails. At the same time we could connect a source of voltage through a capacitor to the base of the same transistor and (assuming the source voltage was zero at the time) this would not affect our bias condition. However, as soon as we begin to generate a voltage from the source this would cause current to be added or subtracted from the bias current (depending on the polarity of the a.c. signal) and would cause the voltage at A to rise and fall in exact relation—except for the 180° change of phase. Having point A biased "mid rail" allows maximum peak swings of voltage without the transistor clipping (going totally out of conduction) or bottoming (going into saturated conduction) unsymmetrically. In the ideal amplifier the voltage seen at A should faithfully represent that from the source.

In practice the method of obtaining this mid-rail bias shown in Fig. 42 is not very satisfactory because the $h_{\rm FE}$ for the transistor must be accurately known and this can vary widely from one device to another (even though they may be of the same type number).

Base current

A simple way of compensating for this device variation is to use the potential at A as the voltage source for providing the base current—shown in Fig. 43. If the potential at A is too high the base current will be increased, hence the collector potential falls; conversely if A tends to be too low the base current decreases and the potential at A is forced to rise. By careful selection of component values this feedback bias circuit caters well for quite wide variations in the gains of transistors. It is not perfect by any means but is an improved way of getting a mid rail voltage reliably. You can make up the circuit of Fig. 43 on T Dec and try different BC108 devices. The voltage you measure should not fall outside the range of +3.5 to +5.5V. For those interested it is quite easy to arrive at the component values. First of all assume that the collector load is to be $1k\Omega$. For the potential at A to be +4.5V (assuming a 9V supply) the drop of 4.5V across R1 will be caused by a collector current of

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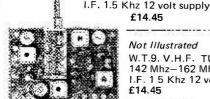
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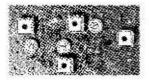
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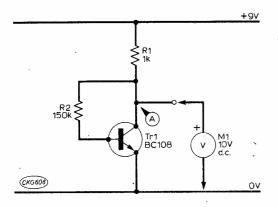


Fig. 43: Using the potential at A as the driving source for base current helps compensate for variations in hff.

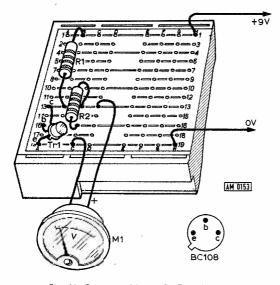


Fig. 44: Component layout for Fig. 43.

4.5mA. If we expect an h_{FE} of around 200 for the BC108 this means that the base current needed to cause 4.5mA collector current is 4.5/200 0.0225mA. The value of R2, to give this current is calculated from the potential difference across 0.6V(potential Α minus the at base emitter drop) divided by the base current $3 \cdot 9/0 \cdot 0225 k\Omega = 170 k\Omega$. The small base current drawn will theoretically modify our original assumption of the potential at A but is so small that it can be ignored. Strictly speaking we should have shown R2 as having a value of $170k\Omega$ but because of other experiments to follow we have made it $150k\Omega$. The effect of this is to cause the quiescent voltage to be slightly less than mid-rail—but near enough for the experiment.

A crystal microphone is a very easily obtainable source of a.c. voltage that is of a capacitive nature and this can be connected straight across the base of Tr1 and ground of our circuit without affecting the bias conditions (see Fig. 45). Note that we have split the value of our original R2 between two resistors (R2 and R3) in series. Initially leave out the capacitor C1 and connect a meter set to a low a.c. range through a capacitor to point A. Most modern

test meters have this capacitor built into them if you use the input socket marked "Output". The capacitor is there so that the meter only responds to a.c. components on top of the d.c. quiescent voltage at A. Whistle loudly into the microphone and you should see a slight movement of the meter (probably IV maximum).

Remember, though, that the output from the microphone is unlikely to be greater than a few tens of millivolts. Clearly there is some form of voltage amplification. If you think about it, though, the a.c. fluctuations at A are being fed back, out of phase, to the base through resistors R2 and R3. This will negate the input signal and the overall gain of the amplifier is going to be considerably impaired. We can, however prevent the a.c. component of the feedback signal reaching the base by connecting a capacitor from the junction of R2 and R3 to ground. Do this while whistling into the microphone and you should see at least a two to one improvement in amplification. We call C1 a decoupling capacitor and it should be of a high enough capacitance to shunt even the lowest frequencies to ground.

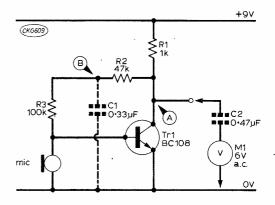


Fig. 45: A signal from a crystal microphone can be superimposed on the bias current but the components have to be slightly modified. Use a meter with an "Output" connection switched to a.c. or alternatively insert C2 when using an a.c. voltmeter.

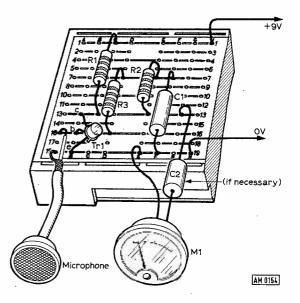
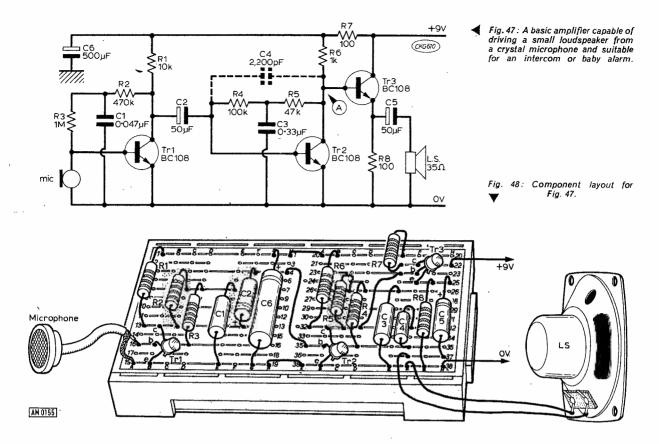


Fig. 46: Component layout for Fig. 45.



The output current from a crystal microphone is very small-because of its high impedance-particularly at low frequencies but there must be quite a reasonable current generated between collector and emitter of the transistor to give rise to the voltage swings we can see at point A. Thus the transistor can be seen to give both current and voltage amplification. The component values in Fig. 45 are not really ideal for coupling from a crystal microphone because we require a fair amount of a.c. base current from the source, and as mentioned earlier, there is not much of this available at low frequencies. The low frequency response of this amplifier would therefore be pretty poor. We can, however, use exactly the same approach to make a stage that needs only one tenth of the input current by increasing all our resistance values by factors of ten (the first stage of Fig. 47. The output from the collector of Tr1 is now coupled as an a.c. signal source to the base of Tr2 which, excluding C4, is identical to the stage we have just described. Before connecting C4 or Tr3 measure the a.c. signal at point A exactly as before; you should see a really high voltage swing (getting on for three or four volts) and more than that, you can get a useful reading for ordinary speech a few inches away from the microphone.

The circuit is clearly providing more voltage gain and has a more useful response at the lower frequency of the human voice. Obviously by increasing the gain at low frequencies we must be overdoing it at high frequencies therefore we insert capacitor C4 which is used, deliberately, to feedback signal from the collector of Tr2 to its base. Because it has a low value it will provide more negative feedback

at high frequencies than at low frequencies and hence helps to linearise the frequency response of the two stage amplifier. Use the "whistle and speech" test to see that the amplitude for the whistle is reduced but the level for normal speech has not been appreciably affected. Because we now have a useful voltage swing at A for speech we can use a current amplifier (an emitter follower) to give sufficient current at that voltage to drive a loudspeaker. This is provided by Tr3.

Note that it is necessary to decouple the power rail between the output stage and the amplifiers by means of R7 and C6. Without these components the current drawn by the output transistor could cause voltage variations on the line which are then seen as a form of signal by the preceding stages and amplified. This leads to instability and the whole circuit would oscillate wildly.

The amplifier of Fig. 47 does not have a particularly good frequency response but is quite adequate for intercom or baby alarm applications. No volume control is provided and in some circumstances you might encounter accoustic feedback (howl-round). This can be prevented by keeping the microphone and the loudspeaker well apart.

A problem with the circuits we have covered, so far, is that the voltage gain is very much dependent on the $h_{\rm FE}$ of the transistor in question. There are other circuits which—at the expense of a little gain—enable us to get what there is under reasonably accurate control.

To be continued



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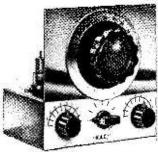
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THE WHYS AND WHEREFORES

C. BUDD

THE concepts of input impedance and output impedance are not really difficult to understand although there is no single rule to cover every situation. What is correct practice depends almost entirely on the individual design requirements.

The most important rule of impedance matching is derived from the maximum power transfer theorem.

The maximum power transfer theorem

If a signal source with a purely resistive output source is required to drive a purely resistive load, maximum power will be transferred from source to load when the load resistance is equal to the output impedance of the source. It should be noted that the theorem assumes that the input and output impedances to be purely resistive, which will rarely be the case in practice, and that to deliver maximum power to the load is the sole requirement.

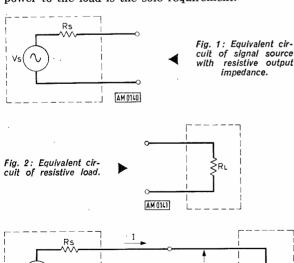


Fig. 3: Equivalent circuit of the source of Fig. 1 driving the load of Fig. 2.

AM 0142

Assuming that our signal source may be represented by an a.c. voltage source in series with a resistance (Fig. 1) and that our load may be represented by a pure resistance (Fig. 2), we can combine the two (Fig. 3) and write some pertinent equations as follows.

Calling the power delivered to the load P

$$V_L = \frac{V_S \; R_L}{R_L + R_S}$$
 by potential divider action

and $I = \frac{V_S}{R_L + R_S} \, \text{where I is the a.c. current flowing}$

$$P = IV_{L}$$

$$\therefore P = \frac{V_{S}^{2} R_{I}}{(R_{L} + R_{S})^{2}}$$

where $V_{\rm L}=$ load voltage, $V_{\rm S}=$ source voltage, $R_{\rm L}=$ load resistance, and $R_{\rm S}=$ source resistance.

Given the source voltage and the source and load resistances we can, with this formula, calculate the power delivered to the load. But we can do more than that. If we assume arbitrary values for $V_{\rm S}$ and $R_{\rm S}$ we can plot a graph of $R_{\rm L}$ against P. The curve obtained will be similar to that in Fig. 4. From the graph it may be seen that the power transferred is at maximum at approximately the point where $R_{\rm L}$ equals $R_{\rm S}$. It may be shown that P reaches a maximum when $R_{\rm L}$ is exactly equal to $R_{\rm S}$.

Maximum power transfer between source and load occurs when the source resistance is equal to the load resistance.

Other considerations

R۱

In practice, however, it is not as straightforward as this because maximum power transfer may not be our only concern. Consider the simple audio output stage shown in Fig. 5. The purpose if T1 is to match the speaker impedance to the output impedance presented by the transistor.

From the maximum power transfer theorem, one could reasonably assume the the "correct" load resistance would be the output resistance of the transistor, but this is not so. In this case maximum

efficiency (i.e. power transfer from amplifier to load) is not our main concern.

Of greater importance is the maximum power that the stage will deliver without distortion due to bottoming (the transistor being turned off by the input signal) or saturation. In fact the load resistance into which the stage will deliver the maximum power without distortion, known as the optimum load, is equal to the supply voltage divided by the quiescent collector current and has nothing to do with the actual output resistance of the stage.

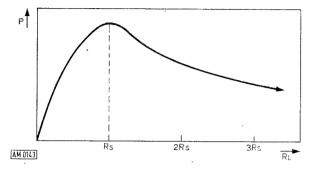


Fig. 4: Sketch graph showing that the power delivered to the load is at a maximum when $R_L = R_S$.

In a practical case the optimum load will generally be higher than the output resistance for an audio power amplifier, and this is the reason that commercial audio power amplifiers, intended to drive load impedances of 3, 8 or 16 ohms, often have output impedances of a fraction of an ohm.

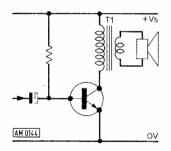


Fig. 5: Simple audio output stage.

Reactive components

An input or output impedance will have reactive components as well as a resistive one. If possible, the reactive element of the source impedance should be cancelled by those of the load impedance. In other words, a source with an equivalent series capacitance should "see" a load with an equivalent series inductance, the reactance being equal, but opposite, to that of the source capacitance.

In this way, the source capacitance and the load inductance form a series-tuned circuit which, ideally, has zero dynamic impedance (zero resistance). Any net reactance in the source-load circuit is undesirable since it reduces the maximum power that can be delivered to the load by the source. Such "reactance balancing" is only possible at a single frequency and in a system of large relative bandwidth (e.g. an audio preamplifier) it is of no use.

At r.f. however, the relative bandwidth will generally be much less and it is usually easy to make the reactive elements of source and load cancel out in the frequency band in use. As an example, one of the functions of the aerial tuning unit in a transmitting system is to cancel out the reactive elements of the aerial impedance.

Equal load and source resistance

Now let us consider another situation in which it would be better to deviate from the rule of making the load resistance equal to the source resistance because maximum power transfer is not our only concern. Fig. 6 shows the equivalent circuit diagram of a typical crystal microphone or ceramic pick-up. The output impedance of such a device consists of a fairly large resistance (typically a few megohms) in series with a small capacitance of perhaps two or three hundred picofarads. If the capacitive element was absent, the transducer drives a pre-amp with an input resistance equal to $R_{\rm s}$ and all would be well.

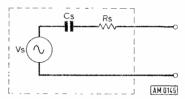


Fig. 6: Equivalent circuit of typical crystal microphone or ceramic pick-up.

However, at the lower audio frequencies, the reactance of $C_{\rm s}$ in a practical transducer becomes large enough to be significant in comparison to $R_{\rm s}$ and attenuation of the bass frequencies would result if the input impedance of the pre-amp were equal to $R_{\rm s}$

Since an inductance in series with the transducer would only cancel the capacitance at a single frequency and would, in any case be ridiculously large, the simplest solution to the problem is to make the input impedance of the pre-amp very large compared to R_s. The reactance of C_s at bass frequencies would then be insignificant compared to the total resistance in circuit and no significant attenuation of the bass frequencies would occur.

High impedance input

The circuit diagram of a crystal microphone driving a pre-amp with an ample input resistance of $10M\Omega$ is shown in Fig. 7. One could reasonably think, from the maximum power transfer theorem, that the large ratio between the resistive component of the source impedance and the load resistance would result in a large loss of available power.

This is the case, but it may be shown that the power gain of a common source f.c.t. stage (and that of a common cathode valve stage) is proportional to the value of the resistor (R1 in Fig. 7) shunting the input, which is roughly equal to the

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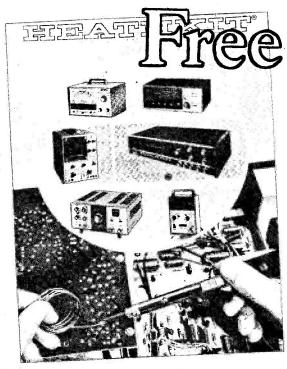
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AUTOMATIC 12V CAR BATTERY CHARGER

Richard Collin

HIS simple automatic battery charger was originally designed for use with the very popular battery operated fluorescent lamp described in the December issue of *Practical Wireless*. Its purpose was to keep the battery in a fully charged state, restoring energy used when mains power is available.

The circuit is of course suitable for charging any 12 volt car battery at a maximum rate of $2\cdot25A$. When the battery reaches full charge ($13\cdot5$ volts) a "crowbar" circuit operates and shuts off the charge current. Interruption of the mains supply restores the crowbar to its off state.

Circuit description

The circuit diagram is shown in Fig. 1. A mains isolation transformer with a 30V centre-tapped secondary winding feeds a full-wave thyristor circuit to provide the charging current. The thyristors are triggered by the d.c. potential applied to the gate electrodes via diodes D1 and D2 and the associated smoothing capacitor C1.

Resistors R1, R2 and R3 limit the gate current together with the indicator lamp LP2. Resistor R1 and lamp LP2 also limit the current through the crowbar thyristor CSR3 when it is 'on'. Resistors

R4 and R5 are connected in parallel. They limit the charge current to 2.25A to protect the transformer, CSR1 and CSR2. Diode D3 is included to stop current flowing back from the fully charged battery into the crowbar circuit once it has triggered.

The crowbar trigger potential is set by the 6.8V zener diode D4 in the gate circuit of CSR3. By using the potentiometer across the circuit output it is possible to adjust the voltage of the output to a predetermined level at which the crowbar circuit 'fires'. The crowbar thyristor 'shorts' the main gates to earth and stops them from receiving gate pulses, so stopping conduction.

* components list

R1 68Ω 5W wirewound resistor

R2, R3 270Ω ½W

R4, R5 1Ω 10W wirewound

R6 1·2kΩ ½W R7 330Ω ½W

VR1 2.2k potentiometer (miniature preset)

C1 640µF 25V

LP1 Mains neon indicator

LP2 6-3V 0-2A lamp

S1 Single pole, single throw toggle

FS1 3A fuse

T1 Mains transformer, secondary 30V centre tapped, 3A

CSR1 2N3228 TO-66 or any 50V 5A thyristor, and

mounting hardware
CSR2 2N3228 TO-66 or any 50V 5A thyristor, and

mounting hardware

CSR3 TIC44

D1 1N4001

D2 1N4001

D3 1N1612R or any 50V 5A stud type (stud is

anode) and mounting hardware

D4 6.8V 1 watt zener diode

Lamp holder (m.e.s.), connecting wire, mains lead, fuseholder, nuts, bolts, etc. Heatsinks (see Fig. 3.)

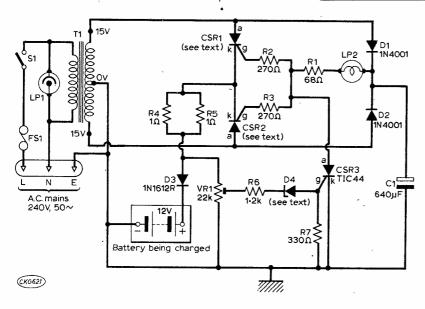


Fig. 1: Schematic circuit of the automatic battery charger.

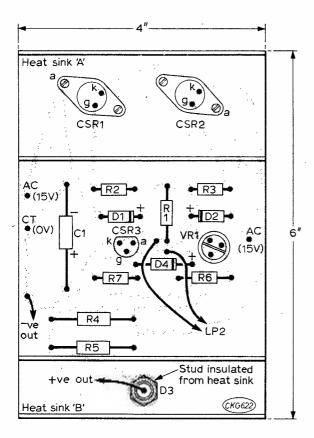


Fig. 2: Printed circuit board and component layout.

The circuit board layout is shown in Fig. 2. All components should be mounted onto the board and soldered up. Ensure that electrolytic C1 is connected correctly and check also the polarity of the thyristor and diode connections. The main thyristors, CSR1 and CSR2 and diode D3 must be mounted with insulators on their respective heatsinks. A smear of silicon grease should be applied to each side of the mica washers to ensure good thermal contact. Resistors R4 and R5 should be spaced clear of the board as they will run quite warm.

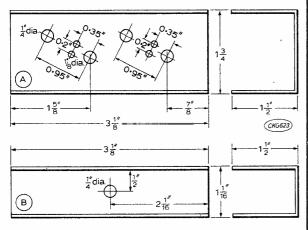


Fig. 3: Heat sink details, in 16 s.w.g. aluminium.

When the board is complete and all wires to the transformer are connected make a final wiring check. Then set VR1 fully anticlockwise, and switch on the mains. Measure the voltage across C1; it should be approximately 20V.

Then connect a fully charged 12V battery (about 13·4V off load) across the output terminals. Advance VRI slowly until the crowbar circuit just operates (lamp LP2 comes 'on'). The voltage measured between earth and R4, R5 and D3 junction should then be about 14V. Do not move the setting of VR1 again—sealing with a dab of glue is a good safeguard. Switch off the unit and disconnect the battery.

Connect a discharged battery to the unit and switch on. If an ammeter is available check the charge rate—about 2·25A. Alternatively measure the voltage across R4, R5; this should be about 1·1V. The crowbar circuit should not operate until the battery is fully charged and reaches 13·4V. Once operated the crowbar cannot be reset unless the mains supply is interrupted.

During power cuts this will be "automatically accomplished.

IMPEDANCE MATCHING—continued from page 1162

input impedance of the stage. Thus, a high input impedance makes for higher power gain and, hence, greater output power from the stage as well as improving the bass response, as it does in this particular application.

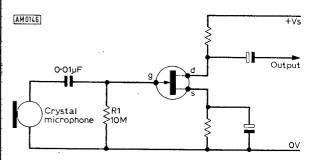


Fig. 7: A crystal microphone driving an audio preamp with a high input impedance.

Power fall-off

There are many such situations in which maximum transfer of power from source to load is not our only concern and load resistance should not be made equal to source output resistance. But the basic principles should be borne in mind. The maximum possible power will be delivered to the load when the input resistance of the load is equal to the output resistance of the source and any reactive components in the source impedance should be cancelled out by equal but opposite reactive elements in the load impedance.

In many practical cases exact equality of source and load resistances is not easy to achieve. It may be seen from Fig. 1 that the power transfer falls off more rapidly with decreasing load resistance than it does with increasing load resistance. Therefore, if it is necessary for a mismatch to occur, it is clearly much better to make the load resistance greater than the source resistance.

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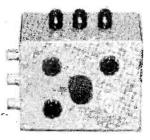
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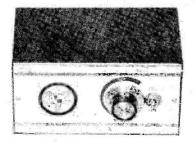
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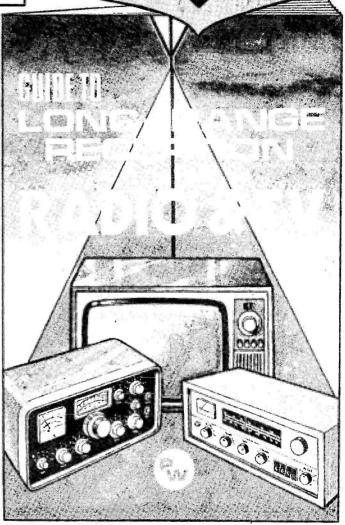


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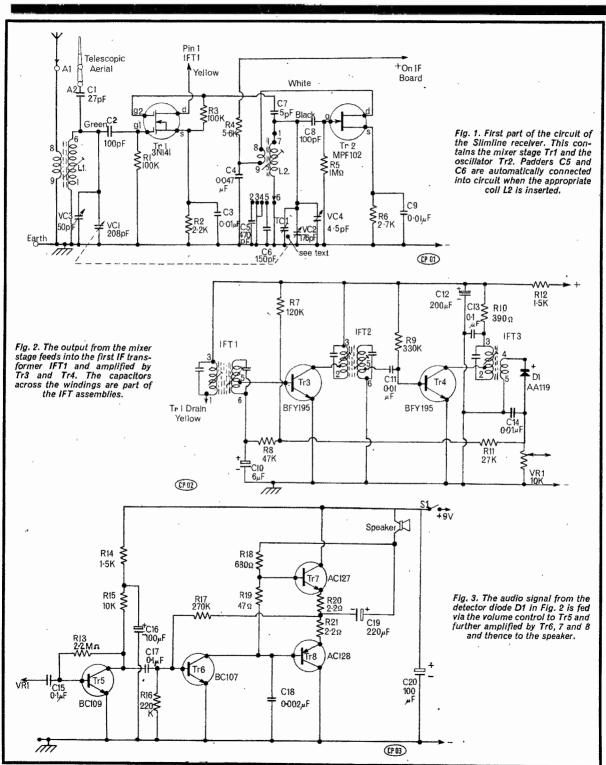
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THE 'SLIMLINE'





Portable Receiver

HIS portable receiver is in a 7×5in. case only lin. deep, though to these dimensions must be added those of the Trimmer, Fine Tuning and Volume/On-Off controls at one end, and the Bandsetting dial on the front. These do not however increase the size very much. The receiver may be operated with its own telescopic rod aerial, with an improved aerial such as a few yards of thin insulated flexible wire or with a conventional aerial.

The coverage of the five bands is approximately as follows:—

Band 1 160---350kHz

,, 2 580—1500kHz

" 3 1·75—4·0MHz

", $4 \cdot 5.9 - 11.5 \text{MHz}$

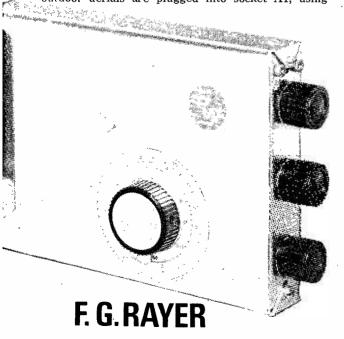
, 5 13—27MHz

The receiver thus has a wide general utility, tuning medium and long waves, if required, in addition to the most popular short wave bands.

Eight transistors and one diode are employed and the receiver is wired and assembled in separate units. A dual-gate 3N141 mixer is used with an MPF102 FET oscillator, followed by two BFY195's and AA119 diode for IF amplification, demodulation and AGC. The audio section has a BC109 preamplifier and BC107 driving an AC127 and AC128 complementary output stage, which provides adequate power for the internal speaker.

CIRCUIT DETAILS

The telescopic aerial, or a **short** wire aerial, is connected to socket A2 Fig. 1, but longer indoor or outdoor aerials are plugged into socket A1, using



the primary coupling winding of the aerial coil L1. This circuit is tuned by VC1 and the panel trimmer VC3 is provided so that this can be peaked for maximum efficiency with any aerial. Signals are taken to gate 1 of Tr1 and gate 2 is coupled by C7 to the oscillator Tr2. The oscillator coil L2 is tuned by the second section of the ganged capacitor VC1/VC2. VC4 is a bandspread tuning control to allow easy tuning on the short wave bands.

L1 and L2 are plug-in coils so there is no need to obtain coils for those bands which are not required. Band 1 is for long wave coverage and may not be wanted in some areas. The extreme high frequency end of this band is not used (above about 350kHz) as instability arises when this stage is tuned near the intermediate frequency, as would be expected.

Band 2 is for medium wave coverage while Band 3 includes shipping and other transmissions, as well as the 160m and 80m amateur bands. Most general short wave broadcasts come in Band 4 and also Band 5.

Capacitors C5 and C6 in Fig. 1 are padders and the correct value is brought into circuit for each coil when it is inserted, by wiring to the appropriate socket pins. TC1 is an integral trimmer on VC2. If VC1/2 is a type without trimmers a separate 30pF or similar small pre-set must be connected here.

Fig. 2 is the circuit of the IF amplifier. IFT1 and IFT2 are double tuned and IFT3 single tuned and these, with the two BFY195's, result in good selectivity and gain. The demodulator diode D1 provides audio signals for the volume control VR1, and automatic gain control bias for the first IF stage. Current for the IF stages is taken from the 9V supply, through R12, the mixer drain circuit being supplied through the primary of IFT1. The on-off switch S1 is incorporated with the volume control VR1.

The circuit of the audio stages is shown in Fig. 3. Tr5 is a low level high gain amplifier with output to the driver Tr6 which drives the NPN/PNP pair Tr7 and Tr8, R17 providing stabilisation of the DC operating conditions. The circuit is intended for an 18 ohm speaker but it will be found that good results are obtained with a 25 ohm or 35 ohm unit.

CONSTRUCTION

Both sides of the mixer/oscillator board are shown in Fig. 4. Plain perforated Veroboard is most suitable, with $0\cdot 15$ in matrix. The resistors and capacitors are inserted as shown and the board turned over and leads soldered underneath. In most places the wire ends of the components are long enough to reach other points. Soldered joints should be small and leads kept near the board, with sleeving on leads which may touch each other. The tag MC is later secured with a 6BA or 8BA bolt, to hold the board clear of the panel and to form a negative or earth return.

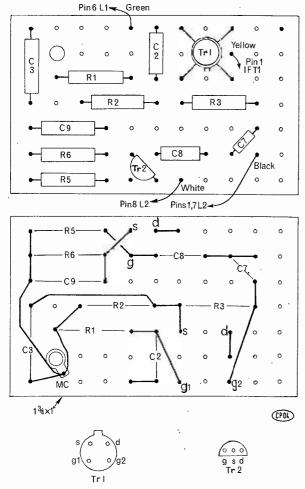


Fig. 4. Layout of the mixer/oscillator board. Veroboard pins can be used where necessary, if component leads are too short.

Important. An insulated gate transistor of the 3N141 type has an extremely high gate internal resistance and it can be destroyed by the static charge of metal or plastic tools, or by touching its leads with the fingers. Despite this, there is virtually no danger to the transistor if it is installed correctly and once R1, R2 and R3 are connected to it, these protect the gate circuits from static charges.

Leave Tr1 until other wiring on this board is finished. Tr1, as supplied, should have a thin spring or loop which short circuits its four leads, to protect it. This is not removed until the transistor is soldered in place. If it has to be unsoldered for any reason, a length of thin, clean wire should be wound round the four leads, under the transistor, before this is done. Spread the leads with a matchstick so that they come through the holes shown in Fig. 4, bend over the wires from R1, R2 and R3, and solder them to the transistor leads.

It is convenient to use colour coded leads for the external connections. These may be green from C2 for VC1 and pin 6 of L1, yellow for the drain circuit, white from Tr2 drain to pin 8 of L2 and black for VC2 and pins 1 and 7 of the holder for L2.

The IF board is shown in Fig. 5. Holes for the IFT pins and screening can tags should be drilled first. The pins are identified by their spacing, and should be arranged as in Fig. 5. A very small round file may

be useful in adjusting the positions of holes, if drilling is not quite correct, so that the IFTs fit without strain on their pins. Holes should also be drilled so that the cores can be reached. Two small tags are secured with the bolts MC, which also fix two angle brackets in place. These brackets allow the board to be fixed to the receiver panel.

Note the polarity of C10, C12 and D1. Proceed with the wiring as for the mixer-oscillator board, with insulated sleeving where required. The wire ends of R12 and C14 can be left projecting, so that other connections can be soldered on later.

The AF amplifier board is built in a similar manner, components being positioned as in Fig. 6. As it is rather difficult to see the transistor lead positions when these are in place, short pieces of coloured sleeving may be put on these wires first to identify them—green for emitter, blue for base

and orange for collector.

Capacitors C16 and C20 are arranged vertically Bolts secure the tags MC and small brackets, as with the IF board. If necessary, these brackets can be cut from a small spare section of flanged universal

* components list

Kesistots			
R1 \cdot 100k Ω	R8 47kΩ	R15	10k Ω
R2 2-2kΩ	R9 330k Ω	R16	220k Ω
R3 100k Ω	R10 390 Ω	R17	270k Ω
R4 5·6kΩ	R11 27k Ω	R18	680Ω
R5 1M Ω	R12 1·5kΩ	R19	47Ω
R6 2·7kΩ	R13 2·2MΩ	R20	$2 \cdot 2\Omega$
R7 120k Ω	R14 1·5kΩ	R21	$2 \cdot 2\Omega$
All resistors 5%	(1 watt		
VR1 10kΩ log.	pot. with switch S	61	

Capacitors

Ċ1	27pF	C8 100pF	C15 0·1µF
C2	100pF	C9 0·01μF	C16 100µF 10V
C3	0·01μF	C10 6µF 4V	C17 0.1µF
C4	0-047μF	C11 0.01µF	C18 0.002µF
C5	470pF	C12 200µF 10V	C19 220µF 6-4V
C6	150pF	C13 0·1µF	C20 100µF 10V
C7	5pF	C14 0.01µF	

VC1/2 208—176pF gang (Jackson 00)
VC3 50pF (Jackson C804)
VC4 4-5pF (Jackson C804)
TC1 30pF trimmer, see text

Semiconductors

Tr1	3N141	Tr4	BFY195	Tr7	AC127
Tr2	MPF102	Tr5	BC109	Tr8	AC128
Tr3	BFY195	Tr6	BC107	D1	AA119

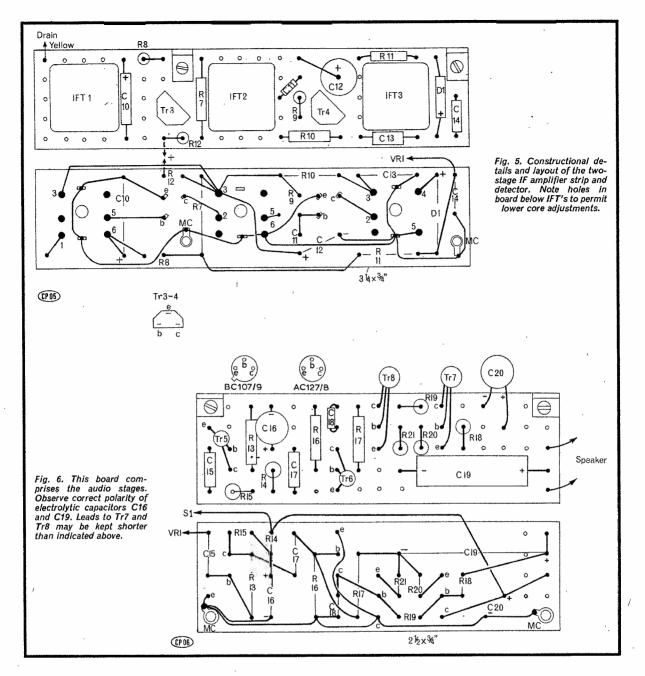
Inductors

IFT1/2 IF Transformer (Denco IFT18/465)
IFT3 IF Transformer (Denco IFT14)
L1/2 Plug-in coils, 9 pin miniature valve type
for ranges required (Denco—'Blue' for
aerial coils and 'Red' for oscillator coils)

Miscellaneous

Speaker, about $2\frac{1}{4}$ in dia., 18 to 35 ohms. Telescopic aerial. Small sockets (2). B9A valveholders, plain (2). Perforated veroboard 0·15in matrix, $1\frac{9}{4}$ x 1in, $3\frac{1}{4}$ x $\frac{3}{4}$ in and $2\frac{1}{2}$ x $\frac{3}{4}$ in. Knobs (4). Perspex for dial.

Casework Plates 7 x 5in (2) (CU168)
Flanged members 7 x 1in (2) (CU54A)
Flanged members 5 x 1in (2) (CU52A)
All from Home Radio.



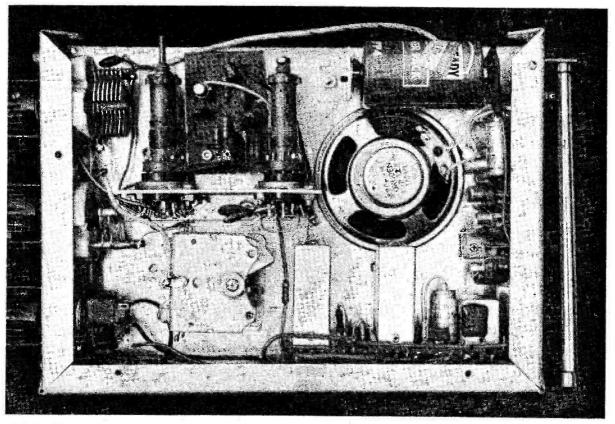
chassis, as used later for the coil holders. Both brackets and insulated board are drilled for 8BA bolts.

A piece of metal with a flange, for mounting the coil holders, is cut $2^3_4 \times 1$ in so that the holders can be fitted as in Fig. 7. A small section is cut away near L2 as shown, to allow the speaker to fit.

The flange is bolted lin. from the edge of the panel, as in Fig. 8. There is little free space so items should be positioned carefully. The flange is held with 6BA countersunk bolts and nuts. The ganged capacitor is held with three 4BA bolts, which must be cut or filed short so that they do not project beyond the thickness of the capacitor's front plate.

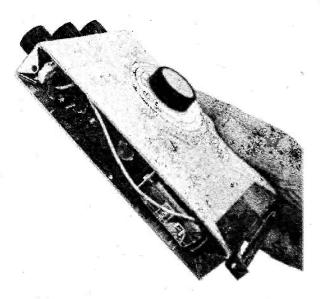
Wiring can then be completed as in the diagrams. The IF, AF and mixer-oscillator boards are held with 8BA countersunk bolts. The one 5×1 in flanged runner is fixed with bolts or self-tapping screws so that VC3, VC4 and VR1 can be mounted, but the other flanged members are left off until later. Leads between units are run against the metal. The speaker is cemented over a 1^3 4in diameter hole and the leads soldered to it. Other connections will be seen in Figs. 7 and 8.

The battery is mounted by a bracket, to which a negative snap connector is bolted. This both holds the battery and provides the negative connection. Two small sockets provide Al and Earth connections. When all wiring is finished, except for the telescopic aerial, the receiver can be aligned. Do not forget to remove the shorting collar or wire from the mixer transistor.



IF ALIGNMENT

As the IFT's are supplied pre-aligned, the cores should not be touched until reasonable results are being obtained. A properly fitting tool must be used, such as that available from the IFT maker, as a wedge-shaped blade may easily break the cores so that they cannot be rotated. Where a signal



Removal of edge panel permits easy coil changing or replacement of battery.

Inside the Slimline receiver. Main components may be identified from Fig. 8.

generator is available, place the output lead of this near the yellow lead (mixer drain) and adjust the cores for best output.

If no generator is available turn the audio gain control to near maximum and tune in a weak but stable signal, such as that obtained from a local BBC transmitter, with no aerial at all in use. With this tuned in correctly, adjust the five cores slightly, as may prove to be necessary, for best volume. An alternative is to connect a high resistance test meter across VR1 (positive to chassis) and use a somewhat stronger signal, so that cores can be peaked for the best reading. When these cores have been adjusted, they should be left alone since their settings are not changed when dealing with the mixer and oscillator circuits.

MIXER/OSCILLATOR ALIGNMENT

If VC1/2 has trimmers, open fully the trimmer on VC1 and screw down the trimmer on VC2 and set VC3 and VC4 about half open. Each range is dealt with separately. Suppose that Range 3 is aligned first. Adjust the core of L2 (Red coil) so that band coverage is approximately correct. Then tune in a signal around 3·5 to 4·0MHz and adjust VC3 for best volume. Leave VC3 at this setting and tune to a signal around 1·9MHz. The core of L1 is then adjusted for best results, after which there is little need for much adjustment of VC3, throughout the band. When VC3 is peaked for best results, it should be neither fully closed nor fully open.

The other ranges are dealt with in the same manner. The cores of L2 are adjusted in that

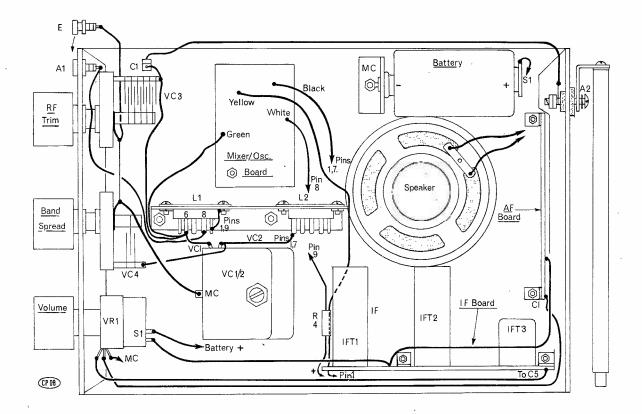
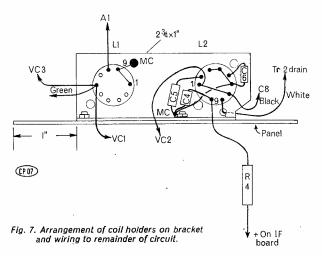


Fig. 8 Location of the three boards and major components. The battery is held in position by the bracket holding the negative clip.

direction which takes them away from the smaller winding for Ranges 1 and 3, otherwise continuous oscillation may prove troublesome at the high frequency end of these bands. This arises from the degree of coupling between L2 and its feedback winding. Should excess oscillation or "squegging" of the oscillator be troublesome, R4 could be increased in value. On the other hand, if Tr2 has somewhat reduced gain the value of R4 could be reduced. However, with the value shown, several MPF102 transistors proved satisfactory, so this should not be necessary.



FINISHING OFF

The aerial is fixed to a small right angle bracket which is pivoted on a 6BA bolt passing through the side of the case. The hole is drilled to take an insulated bush and an insulated washer rests between the bracket and case. A spring washer is placed under the screw head and the nuts locked together so that the aerial can be extended vertically with the case flat or standing upright. A flexible lead runs from the aerial to C1.

The dial is marked on card and is about 2³4in. in diameter. The control knob is a shallow type to which is attached a 2³4in. diameter disc of ¹16in. thick Perspex. This can be fixed with adhesive or self-tapping screws. A line is marked across the Perspex. A disc can be easily cut with an adjustable tank or washer cutter, but if this is not available a pointer knob could be substituted for the disc.

The case is completed by screwing on one 7×1 in member and the remaining 5×1 in member. The 5×1 in members fit inside the 7×1 in members so that the top 7×1 in flanged member can be taken off to change the battery or coils. The back, a 7×5 in flat plate, is permanently attached with self-tapping screws, but only one screw is run into the top member flanges.

There is some opportunity for individual choice in the way in which the case is finished. If left bare or painted, gauze or perforated metal should be fitted over the speaker aperture inside. The case shown was covered at the front with fabric and self-adhesive material as used for shelves, boxes, etc.



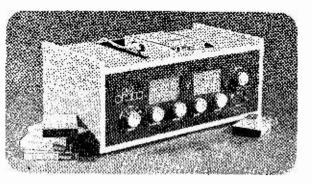


RICHARD COLLIN

POWER AMPLIFIER ASSEMBLY

The first stage in assembly is to mount all components except the plastic power transistors onto the board, ensuring correct polarity of electrolytic capacitors. Solder each joint carefully—do not over heat the components, but make sure joints are properly made. Check that all parts are in the correct position and then cut off all excess lead wires. Note that R13 and C9 are mounted on the speaker sockets not on the printed board.

Next fit the output and driver transistors onto their respective heat sinks ensuring that the mica washers and nylon bushes are correctly located. Check that each device is isolated from the heatsink after assembly. Then form the leads for insertion into the printed board. Do not bend the leads less than ¹8 in from the transistor body. Do support the leads near the body with long-nose pliers whilst forming. Do not radius the bends tighter than ¹16 in.



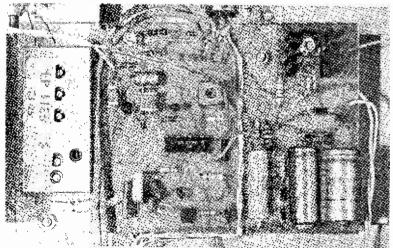
Mount the strip of four output devices onto the circuit board and solder up the connections. Then mount the two driver transistors in a similar fashion. Once soldered ensure that the power transistors are not bent back and forth on their leads—plastic packaged devices can be easily damaged by stressing the lead outs. Once complete the power board should be put away safely until needed later on.

TUNER AND IF CIRCUIT (UNIT 3)

The AM section utilises the Ferranti ZN414 integrated circuit IC1 and a single transistor amplifier Tr1. A small ferrite rod aerial forms part of a double-tuned aerial circuit which is used to eliminate swamping effects of strong local transmissions by improving the selectivity. The circuit and printed board illustrated are for the single-station version. Further channels may be added by inserting a suitable two-pole rotary switch at the points marked "X" and "Y" in Fig. 10 to select additional pairs of trimmer capacitors for each station required.

The ferrite aerial may be insufficient in some areas of poor signal strength. The AM aerial socket, which is loosely coupled to the ferrite rod by two turns of insulated wire, allows adequate reception under such conditions by connection of an external aerial.

In the FM section, a Mullard varicap tuned module type LP1186 feeds an RCA IF amplifier integrated circuit IC2 through a ceramic filter tuned to 10·7 MHz. This integrated circuit requires only one IF coil to provide the audio output for the decoder and also an AFC control voltage.



The prototype Tuner and IF board shown here has some variations in layout from the final version given in Fig. 12

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7404	21p	19v	7460	20p	18p	74154	£2 20	£1.87
7405	21p	19p	7470	33p	27p	74155	£1.65	£1.21
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7409	29p	24p	7475	63p	57p	74161	£2·18	£2.05
7410	20p	18p	7476	55p	51p	74162	£4.84	£4.54
7411	23p	21p	7480	£1.10	99p	74163	£4.84	£4.54
7412	40p	33p	7481	£1.37	£1 26	74164	£2.73	£2.63
7413	31p	29p	7482	£1·10	99p	74165	£2.73	£2 63
7416	49p	47p	7483	£1.32	£1.29	74166	£4.28	£3.94
7417	57p	53p	7484	£1.32	£1.21	74174	£2.78	£2.66
7420	20p	18p	7485	£2.75	£2.64	74175	£1.94	£1.81
7422	60p	58p	7486	49p	41 p	74176	£1-99	£1.87
7423	60p	58p	7489	£4-95	£4·29	74177	£2.75	£2 64
7425	60p	53p	7490	82p	71p	74180	£2.75	£2.64
7426	35p	31p	7492	84p	65p	74181	£6.49	£6.05
7427	55p	51p	7493	82p	66p	74182	£2·16	£2-02
7428	85p	79p	7494	£1.04	93p	74184	£2.69	£2.42
7430	20p	18p	7495	£1 14	£1.03	74190	£3.08	£2.69
7432	42p	33p	7496	£1.25	£1·15	74191	£2:30	£2-24
7433	97p	91 p	74100	£2.75	£2.58	74192	£2-53	£2-30
7437	77p	74p	74104	£1.18	£1.14	74193	£2-53	£2.30
7438	77p	74p	74105	£1-18	£1:14	74194	£3·27	£3.15
7440	20p	18p	74107	48p	46p	74195	£2-42	£2-30
7441	81p	78p	74110		65p	74196	£2·18	£2-06
7442	81p	78p	74111	£1.52	£1.40	74197	£2·18	£2-06
7443	£1.40	£1.32	74118	£1.10	80p	74198	£6.65	£6.05
7444	£1.57	£1.52	74119	£1.64	£1:54	74199	£6.65	£6.05
7445	£2.31	£2·18	74121	47p	42p	74200	£26.40	£21·12
7446	£2:31	£2-18	74122	£1.70	£1.59			

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30)1	DIL		50p	723c	DII
30	1	TO99			723e	TOS
30	1	8 PIN	D1L	46p	741c	8 P
)1A	DIL		69p	741c	14
30)1A	TO99		69p	741c	TOS
	1A	8 PIN	DIL	66p	747c	DH
30)7	$_{ m DIL}$		69p	748c	DH
30		TO99			748c	TOS
30)7	8 PIN	DIL	66p		
30		TO99		6.45p		
30	18A	TO99		6.40p	T⊩	11:
)9e	DIL		35p		R/
70)9c	TO99		31p	ZN414	

99 IN DIL PIN DIL



FERRANTI 35p 31p ZN414 RADIO IC

Electrolytic Capacitors

- upacitois						
4 VO		16 VC		40 VO		
$47\mu F$	6 <u>}</u> p	$15\mu F$	8łp	$47\mu F$	6 <u>1</u> p	
$100 \mu F$	64p	33µF	6½p	100µF	90	
$220\mu F$	6 å p	$150\mu F$	β∦p	68µF	10p	
$330 \mu F$	64p	150µF	8p	$220\mu F$	110	
$1000 \mu F$	13p	$220\mu F$	gn.	470µF	19p	
4700; F	29p	680µF	17p	680µF	25p	
6-3 VC		$1000 \mu F$	17p	1000µF	25p	
		$1500 \mu F$	25p	2200µF	44p	
33μ F	6 <u>1</u> p	$2000 \mu F$	43p		- 1	
$68\mu F$	81p	25 VC				
$150\mu F$	6 <u>∗</u> p					
470µF	11p	10µF	6 ∮p			
$680 \mu F$						
	13p	$22\mu F$	61p	63 VC	LT	
$1500 \mu F$	18p	47μF	6}p			
$1500 \mu F \\ 2200 \mu F$	18p 18p	47μ F 100μ F	6}p 8p	1441	یp	
$1500 \mu F$	18p	$47 \mu F$ $100 \mu F$ $150 \mu F$	6}p 8p 8p	$1\mu F = 2 \cdot 2\mu F$	6 <u>i</u> p	
$1500 \mu F \\ 2200 \mu F$	18p 18p 26p	47μF 100μF 150μF 220μF	6}p 8p 8p 10p	1μF 2·2μF 4·7μF	6½p 6½p	
1500μF 2200μF 3300μF	18p 18p 26p	47μF 100μF 150μF 220μF 470μF	6}p 8p 8p 10p 13p	1μF 2·2μF 4·7μF 6·8μF	6½p 6½p 6½p	
1500μF 2200μF 3300μF 10 VO 22μF	18p 18p 26p LT 64p	47μF 100μF 150μF 220μF 470μF 680μF	61p 8p 8p 10p 13p 20p	1μF 2·2μF 4·7μF 6·8μF 10μF	64p 64p 64p 64p	
1500μF 2200μF 3300μF 10 VO 22μF 47μF	18p 18p 26p LT 6½p 6+p	47μF 100μF 150μF 220μF 470μF 680μF 1000μF	6 p 8 p 8 p 10 p 13 p 20 p 22 p	$^{1}\mu F$ $^{2\cdot 2}\mu F$ $^{4\cdot 7}\mu F$ $^{6\cdot 8}\mu F$ $^{10}\mu F$ $^{22}\mu F$	61p 61p 61p 61p 61p 61p	
1500μF 2200μF 3300μF 10 VO 22μF 47μF 100μF	18p 18p 26p LT 6½p 6½p 6½p	47μ F 100μ F 150μ F 220μ F 470μ F 680μ F 1000μ F 2200μ F	6 p 8 p 8 p 10 p 13 p 20 p 22 p 39 p	1μF 2·2μF 4·7μF 6·8μF 10μF 22μF 68μF	6½p 6½p 6½p 6½p 6½p 6½p	
1500μF 2200μF 3300μF 10 VO 22μF 47μF 100μF 220μF	18p 18p 26p LT 6½p 6½p 6½p	47μF 100μF 150μF 220μF 470μF 680μF 1000μF	6 p 8 p 8 p 10 p 13 p 20 p 22 p	1μ F $2\cdot 2\mu$ F $4\cdot 7\mu$ F $6\cdot 8\mu$ F 10μ F 22μ F 68μ F 100μ F	6½p 6½p 6½p 6½p 6½p 6½p 10p	
1500µF 2200µF 3300µF 10 VO 22µF 47µF 100µF 220µF 330µF	18p 18p 26p LT 6½p 6½p 6½p 10p	47μ F 100μ F 150μ F 220μ F 470μ F 680μ F 1000μ F 2200μ F 5000μ F	6 p 8 p 8 p 10 p 13 p 20 p 22 p 39 p 68 p	1μF 2·2μF 4·7μF 6·8μF 10μF 22μF 68μF 100μF 150μF	6½p 6½p 6½p 6½p 6½p 10p 11p	
1500µF 2200µF 3300µF 10 VO 22µF 47µF 100µF 220µF 330µF 470µF	18p 18p 26p LT 6½p 6½p 6½p 10p	47μF 100μF 150μF 220μF 470μF 680μF 1000μF 2200μF 5000μF	6 p 8 p 8 p 10 p 13 p 20 p 22 p 39 p 68 p	1μF 2·2μF 4·7μF 6·8μF 10μF 22μF 100μF 150μF 220μF	6 t p 6 t p 6 t p 6 t p 6 t p 10 p 11 p 13 p 19 p	
1500µF 2200µF 3300µF 10 VO 22µF 47µF 100µF 220µF 330µF 470µF 1000µF	18p 18p 26p 26p 6½p 6½p 6½p 10p 10p	47μF 100μF 150μF 150μF 470μF 680μF 1000μF 2200μF 5000μF 40 VC	6 p 8p 8p 10p 13p 20p 22p 39p 68p	1μ F $2\cdot 2\mu$ F $4\cdot 7\mu$ F $6\cdot 8\mu$ F 10μ F 22μ F 68μ F 100μ F 100μ F 120μ F 220μ F 330μ F	6 1 p 6 1 p 6 1 p 6 1 p 6 1 p 10 p 11 p 13 p 19 p 22 p	
1500µF 2200µF 3300µF 10 VO 22µF 47µF 100µF 220µF 330µF 470µF	18p 18p 26p 26p 6½p 6½p 6½p 10p 10p 11p 20p	47μF 100μF 150μF 220μF 470μF 680μF 1000μF 2200μF 5000μF	6 p 8 p 8 p 10 p 13 p 20 p 22 p 39 p 6 8 p	1μF 2·2μF 4·7μF 6·8μF 10μF 22μF 68μF 100μF 150μF 220μF	6 t p 6 t p 6 t p 6 t p 6 t p 10 p 11 p 13 p 19 p	

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1 Amp	28p	35p	41p				
3 Amps	44p	50p	60p				
P.I.V.		300	400				
1 Amp		44p	53p				
3 Amps			60p				

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C296 SERIES
400V: 0-001µF, 0-0015, 0-0022, 0-0033, 0-0047 3p, 0-0068, 0-01, 0-015, 0-022, 0-033 3pp, 0-047, 0-068, 0-1 4pp, 0-15 6pp, 0-22 8pp, 0-33 1pp, 0-47 14pp, 160V: 0-01µF, 0-015, 0-022, 0-033, 0-047, 0-068 3pp, 0-1 4p, 0-15 4p, 0-1 4pp, 0-16, 0-22 5pp, 0-33 7p, 0-47 9pp, 0-68 12p, 1µF 14pp, 1-5µF 22p, 2-2µF 24p

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½ watt 5% carbon 1 watt 10% carbon range 10 chus to 4.7 megohms. ½ watt m/o 2%	5% carbon	
range 10 ohms to 4.7 megohms.		
		2
∮ watt m/o 2 %		
	m/o 2 %	

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PET'S.
500 carbon resistors 1, 1, 1, 2 watt.
100 Electrolytic condensers.
250 Ceranic Polystyrene, Silver
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etc. condensers.

etc. condensers. 25 Potentiometers assorted. 250 High Stab 1 %, 2 %, 5 % resistors. 11b Assorted nuts, bolts, washers, spacers, etc. 25 Assorted Switches, rotary, lever, micro, toggie, etc. 50 Preset Potentioneters

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MT111/B	24 volt	·25 amp	£1 35	20p
MT71	12 volt	2 amp .	£1.76	22p
MT71/B	24 volt	1 amp	£1.76	22p
MT18	12 volt	4 amp	£2.47	36p
MT18/B	24 volt	2 amp	£2·47	36p

30 volt transformers								
	-220-240v. S							
12 15, 20,	24, 30v or 12-4)–12v or 15-						
MT112	·5 amps	£1.32	22p					
MT79	1	£1.80	36p					
MT 3	2	£2:96	36p					
MT20	3	£3-30	42p					
MT51	3	£4 84	49p					

50 volt transformers

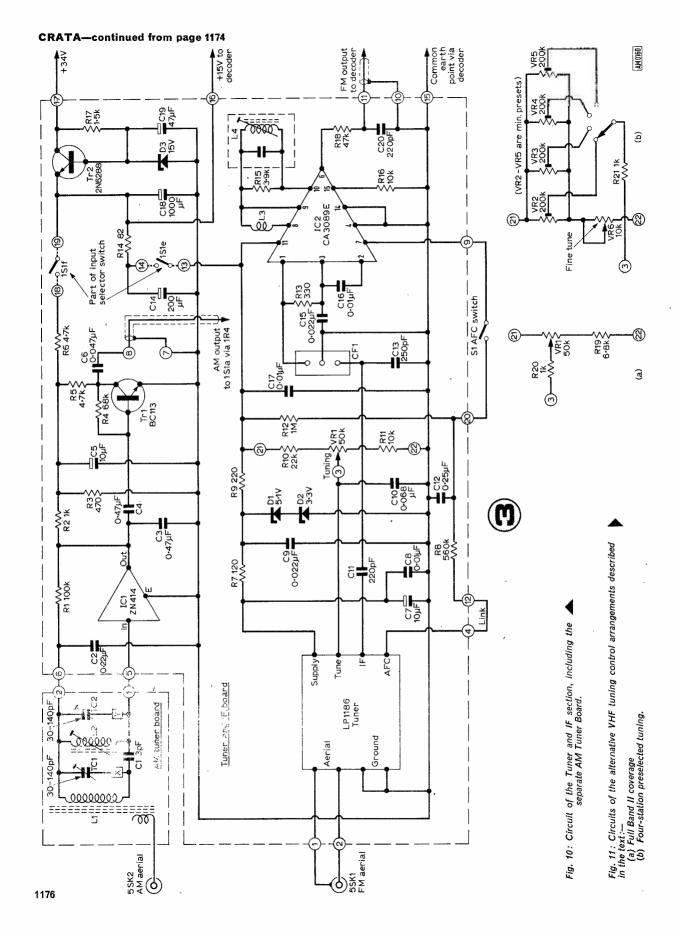
		Secondary	volt. 19,
25,33, 40, 5	50v or 25-0	-25 volt.	
MT102	·5 amps	£1.76	30p
MT103	1	£2.58	38p
MT105	3	£4.84	52p
MT106	4	£6.02	52p

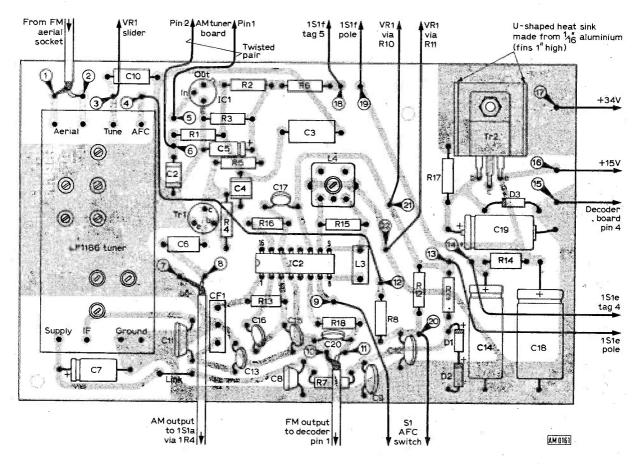
60 volt transformer

i	Prim 200-	220-240 S	econdary 24,	30, 40,
l	48, 60v or	24-0-24v	or 30-0-30v	
i	MT124AT	ama č·	£1.76	38p
i	MT126AT	1	£2.47	34p
ı	34.033.100	- 3	00.00	4.4

	miniature		rmers		
.	Prim 220	volt			
ĺ	BT606	100 mA	6-0-By	98p	15p
	BT909	100m t	9-0-97	98p	15p
i	BT12012		12-0-12v	£1.08	15p
	BT24024	100 mA	24-0 -24 c	£1·95	15p

Transistors/	BC109 11p	BC303 50p	MP8121 33p	TIP32A 78p	Diodes &	
Diodes	BC113 151p	BC304 40p	MP8122 44p	TIP33 £1.05	Rectifiers	
1	BC116 16p	BCY70 17p	MP8123 50p	TIP34A		
AC107 16p	BC125 18p	BCY71 37p	NKT21128p	£1.54	1N914 8p	
AC126 14p	BC126 25p	BCY72 17p	NKT21228p	TIP35A	1N916 8p	
AC127 13p	BC132 16p	BD131 68p	NKT21425p	£2.53	1N4148 8p	
AC128 13p	BC134 16p	BD132 90p	NKT21755p	TIP36A	1844 10p	
AC142K 22p	BC135 16p	BD135 42p	NKT26123n	£3·19	1N4007 22p	
AC141K 20p	BC137 16p	BD136 50p	NKT27120p	TIP41A 79p	1S113 17p	
AC176 15p	BC138 36p	BD141 £1-87	NKT27420n	TIP42A 91p	BA100 16p	
AC187 18p	BC142 33p	BD142 500	NKT27525n	2N706 13p	BA102 25p	
AC187K 20p	BC143 33p	BF159 33p	NKT40371p	2N930 23p	BA115 8p	
AC188 18p	BC144 30p	BF173 29p	NKT40583p	2N1131 22p	Bal44 14p	
AC188K 20p	BC145 26p	BF177 28p	NKY603F	2N1132 28p	BA145 22p	
ACY17 24p	BC147 9p	BF178 29p	66p	2N1613 22p	BA154 14p	
ACY18 21p	BC148 9p	BF179 350	NKT613G	2N1711 26p	BAX13 14p	
ACY19 25p	BC149 9p	BF194 15p	33p	2N2904 40p	BAX16 14p	
ACY20 22p	BC153 16p	BF195 17p	NKT67426p	2N2904A	BAY18 19p	
ACY21 230	BC154 17p	BF244 27p	NKT677G	44p	BAY31 9p	
ACY22 18p	BC157 13p	BF260 29p	24p	2N2905 46p	BY100 19p	
ACY39 68p	BC158 12p	BF329 18p	NKT71332p	2N2924 18p	BY126 16p	
AD140 40p	BC159 14p	BF330 18p	NKT77327p	2N2926 10p	BY127 19p	
AD142 44p	BC167 13p	BF390 37p	OC19 55p	2N3053 26p	BYX10 24p	
AD143 39p	BC168 11p	BFX84 28p	OC20 55p	2N3054 55p	OA5 19p	
AD149 38p	BC169 11p	BFX85 35p	OC23 49p	2N3055 52p	OA10 24p	
AD150 60p	BC177 15p	BFX86 22p	OC25 45p	2N3702 11p	OA47 9p	
AD161 38p	BC179 15p	BFX87 28p	OC28 50p	2N3703 11p	OA70 8p	
AD162 38p	BC182L 10p	BFX88 26p	OC29 50p	2N3704 11p	OA73 11p	
AF114 18p	BC183L 11p	BFY50 21p	OC35 50p	2N3705 11p	OA79 8p	
AF115 18p	BC184L 11p	BFY51 17p	OC36 50p	2N3706 11p	OA81 9p	
AF116 18p	BC186 33p	BFY52 17p	OC44 14p	2N3707 11p	OA85 11p	
AF117 18p	BC212L 11p	BFY64 39p	OC45 14p	2N3708 11p	OA90 8p	
AF118 92p	BC213L 11p	BFY90 72p	OC70 23p	2N3709 11p	OA91 8p	
AF124 27p	BC214L 11p	BSX20 19p	OC71 14p	2N3710 11p	OA95 Sp	
AF139 39p	BC258 9p	C407 22p	OC72 14p	2N3711 9p	OA200 11p	
AF239 41p	BC259 9p	C426 33p	OC81 14p	2N3794 17p		
AL100 77p	BC267 14p	C428 31p	OC83 22p	2N3819 28p		
AL102 66p	BC268 15p	C450 17p	OC94 28p	40361 50p		
AL103 55p	BC300 40p	MP8111 35p	TIP29A 53p	40362 50 p		
BC107 11p	BC301 32p	MP8112 42p	T1P30A 64p	40636 50p		
BC108 11p	BC302 30p	MP8113 35p	TTP31A 64p		'	





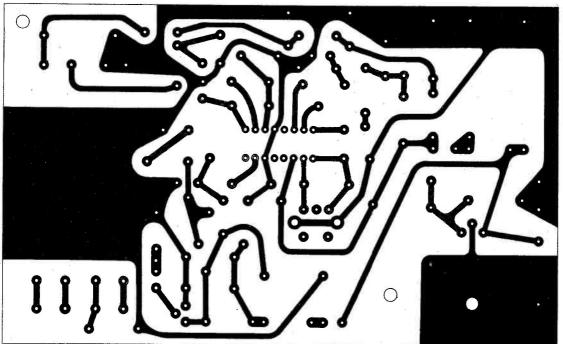


Fig. 12: Component location and printed circuit layout for the main Tuner and IF board. Both drawings are actual size.

TUNER & IF BOARDS Resistors R11 $10k\Omega$ R1 100kΩ R2 1kΩ R12 $1M\Omega$ 470Ω R13 330Ω R3 R4 $68k\Omega$ R14 82Ω R15 3.9kΩ 4.7kΩ R5

4.7kΩ R16 10kΩ 120Ω R17 1.5kΩ R7 R8 560kΩ R18 $47k\Omega$

R9 220Ω VR1 50kΩ lin R10 22kΩ

Note-The alternative VHF tuning arrangements require the following changes in components. (1) Full range continuous tuning (Fig. 11a)

Delete R10 and R11 above and add R20 1k Ω R19 6·8kΩ

(2) Preselected tuning (Fig. 11b)
Delete R10, R11 and VR1 above and add

R21 1kΩ VR2-VR5 each 200kΩ min. preset VR6 $10k\Omega$ lin

All fixed resistors 1W 5% carbon film

Capacitors

C1	3pF ceramic	C11	220pF ceramic
C2	0.22μF ceramic	C12	0·25μF ceramic
C3	0·47μF polyester	C13	250pF ceramic
C4	0·47μF polyester	C14	200μF 25V
C5	10μF 16V	C15	0.022μF polyester
C6	0·047μF polyester	C16	0·01μF polyester
C7	10μF 16V	C17	0·01μF polyester
C8	0·01μF polyester	C18	1000μF 16V
C9	0·022μF polyester	C19	47μF 16V
C10	0.068μF polyester	C20	220pF ceramic
TC1	30-140pF compress	sion t	rimmer
TC2	2 30-140pF compress	sion *t	rimmer

Semiconductors

D3 BZY88 C15

Tr1	BC113	IC1	ZN414 (Ferranti)
Tr2	2N6288 (RCA)	IC2	CA3089 E (RCA)
D1	BZY88 C5V1	D2	BZY88 C3V3

Miscellaneous

L1 55 turns of 30swg enamelled copper wire on 2¼" x 5 dia. ferrite rod

Single-tuned Medium Wave coil RF Choke 15µH Toko 7BA 150J L3

Toko KACS-K586-HM

CF1 Crystal filter Vernitron FM4 or Toko CFS10-7

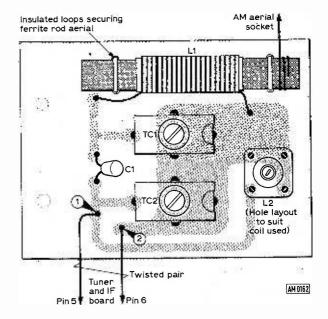
S1 SPST min. toggle switch FM tuning head Mullard LP1186 Tuning drive drum 11/2" dia. Slow-motion cord drive spindle Cord tension spring 1/2 3 small nylon pulleys Printed circuit boards

Notes

1. RCA semiconductors are available from E.C.S. (Windsor) Ltd. (see Part 1 of this project).

2. Toko components are available from Ambit International.

The values given for the tuning control circuit allow coverage of 88-100 MHz. A restricted coverage has the advantage of making the tuning finer and spaces the stations farther apart. The alternative circuit of Fig. 11a provides coverage of the full band 88-104 MHz whilst a four-station preselected tuning arrangement is given in Fig. 11b.



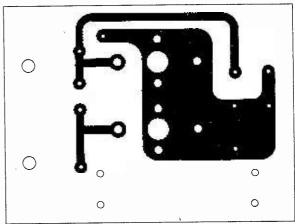


Fig. 13: Location of components and actual size layout for the AM Tuner Board.

Four power supplies are derived from the main 34V rail through a series stabiliser transistor Tr2 and various filter networks.

1. The decoder 15V supply is taken direct from the stabiliser and decoupled via C18.

2. The AM tuner 1.5V supply is provided by a resistive potential divider across the 15V supply R3/R6. Decoupling is provided by capacitor C5.

3. The FM IF and tuner varicap supply is taken from the 15V supply via R14 and decoupled by C14/C17. This supply is 12V.

4. The FM tuner 8V supply is provided from the 12V supply by R9, D1/D2 and R7. Decoupling is provided by C7, C8 and C9.

When assembling the printed board care must be taken not to overheat the integrated circuit pins and also not to short-circuit the adjacent connections as they are fairly close together. Ensure that all electrolytics and diodes are polarised correctly and that the ZN414 leads are correctly positioned. The ceramic filter CF1 may be mounted any way round—the centre pin is earthed and either of the other two pins may be input or output. The series stabiliser transistor Tr2 does not require isolation from either its heatsink or the copper print on the board.



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CRATA—continued

The AFC switch is mounted on the tuner back panel near the aerial sockets—it may be sited on the front panel if required, but do not locate it near to the mains neon and switch.

The AM aerial board, Fig. 13, on which the ferrite rod is mounted should ideally be mounted such that it can be rotated through 90° for maximum signal pickup. Alternatively it may be rigidly mounted in the correct position if the tuner will always be sited in one particular place. The leads between the printed board and the rotary switch in the multistation version should be kept very short. A suitable position for the switch is immediately above the Input Selector.

Due to pressure on editorial space, details of the Storeo Decoder have been held over until our May issue which will also describe the Power Unit and Chassis.

Mciloscope

PART 2 **techniques** ALAN AINSLIE

OSCILLOSCOPE DISPLAYS

The very heart of any oscilloscope is the cathode ray display tube. After all the electronic functions have been executed the ultimate result is displayed, visibly, on the face of the tube. We shall take a look at a few types of CRT and their associated circuitry as applied to oscilloscopes.

The electron beam, produced by an electron gun, passes through a deflecting mechanism and arrives at the screen where it causes the screen material to fluoresce. The whole mechanism is housed in an evacuated glass container and, in an oscilloscope, only the front face is visible. Fig. 1 shows the general arrangement. For oscillographic use we require a bright spot of light, intense but very small.

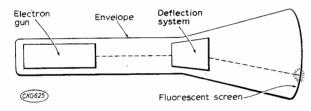


Fig. 1: Main elements in a CRT intended for use in an oscilloscope.

It is the purpose of the electron gun to produce the narrow stream of electrons of high energy to cause local luminescense of the screen. When the beam hits the phosphor screen it causes fluorescence. However, if the beam is cut off suddenly the screen continues to glow with phosphorescent light. It is this phosphorescent light that determines the afterglow of the tube.

ELECTRON GUN

A hot cathode on the axis of the tube produces electrons by thermionic emission, as in a conventional electronic valve. By a suitable arrangement of anodes an electric field distribution inside the tube is created focusing the electrons into a high velocity pencil, arranged to converge on to the screen. A simple gun arrangement is shown in Fig. 2 This type of arrangement is often used and is known as a pentode or five electrode gun.

The cathode is heated to emissive temperature and is surrounded by the grid, in this case shaped like a top hat with a hole in it, known as a Wehnelt cylinder. The grid is maintained slightly negative with respect to the cathode and focuses the space charge around the cathode along the axis of the gun.

The first anode (A1) is positive with respect to the cathode by perhaps a couple of hundred volts. Fig. 3 shows how the electrons are accelerated out of the grid area towards the first anode, and in so doing are focused at Z by the equipotential lines, shown dotted. The diameter at Z is used as an "image" and consequently should be as small as possible for a small spot on the screen. The electron beam enters the first anode diverging and a number of stops are added to keep the beam width small and keep out fringe electrons which impair definition. The diverging electron beam emerging from the first anode now needs to be focused on to the screen, or put another way, an image of Z is projected on to the screen.

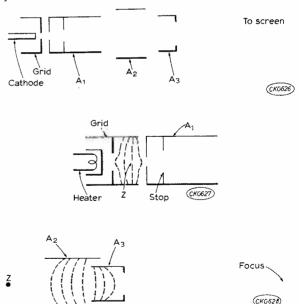


Fig. 2: top, arrangement of electrodes used in a pentode gun. Fig. 3, centre, shows the beam focusing action of the grid and A1. Fig. 4, bottom, the effect of the remaining anodes A2 and A3 in focusing the beam on to the screen.

Fig. 4 shows how the second (A2) and third (A3) anodes accomplish this focusing. The second anode is at a higher potential than A1, and A3, the final anode, is at a still higher potential. Thus the equipotential lines are as shown dotted. The beam of electrons now converges as it crosses the A2-A3 fields and by adjustment of the voltage between A2 and A3 the beam can be focused on the screen of the CRT.

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AD162 36p BC158 14p BFY51 20p 2N3055 60p 40408 40p AFI14 20p BC159 14p BFY52 20p 2N3702 13p ZTX108 15p AFI15 20p BC187 22p BUY105 225p 2N3703 12p ZTX300 15p	Pin insertion tool 52p 52p Spot face cutter 42p 42p Pkt. 50 pins 20p 20p 9V mains power supply. Same size as PP9 battery.
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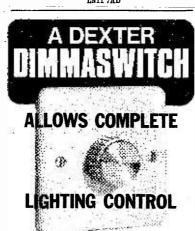
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In simpler types of CRT A2 is omitted giving a tetrode electron gun. The final focusing takes place between A1 and the final anode and geometrically is suitable for a fine spot. However, if focusing is achieved by varying A1 (the final anode potential is fixed as we shall see later) this affects the velocity of the beam because A1 is the primary accelerating anode. The change in velocity changes the position of the point Z and the range of focus is restricted for a good spot size. This situation in practice means that when the grid potential (brightness) or the A1 potential (focus) is altered the other potential must be changed as well, giving restricted focus and brightness range. It is for this reason that the pentode type of tube is almost universally used.

BEAM DEFLECTION

An electron has a negative charge of 1.6×10^{-19} coulombs. This is a very small charge, and conversely any electric field acting on the electron will produce only a very small force. However the mass of the electron is very small and so large accelerations can be produced with only moderate potentials.

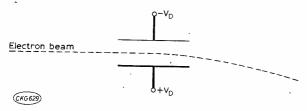


Fig. 5: Effect of the deflecting plates on the electron beam.

If a beam of electrons, focused into a fine pencii, is allowed to pass between two parallel plates as in Fig. 5, the electrons will experience a force towards the positive plate and it can be shown that the deflection is proportional to the deflecting voltage (Vd) and inversely proportional to the accelerating voltage (Va). A purely mathematical outlook shows that electrostatic deflection produces a (theoretically) linear deflection mechanism.

DEFLECTION PLATES

In order to keep the sensitivity as high as possible the tube is physically large and the deflector plates are placed as close together as possible, usually of the form shown in Fig. 6 to permit high deflection sensitivity to be achieved without the beam catching the actual deflector plates. If this occurs (for example if the timebase is overdriven to give X expansion) secondary emission occurs at the surface of the plates, and the low energy secondary electrons can be accelerated towards the screen causing flare and high background illumination. This undesirable

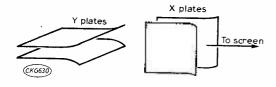
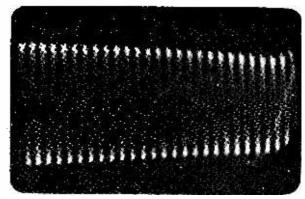


Fig. 6: Arrangement of the X and Y plates, the Y plates being nearer to the gun system.

effect can be avoided by coating the plates with a material of low secondary emission, or providing "beam catchers," small cups that accept the beam when driven off the screen. The X plates are usually mounted nearer to the tube face so that the Y plates have the maximum sensitivity.

To ensure that the electron beam does not become distorted in any way by extra acceleration due to the deflector plates they are arranged to be at the same potential as the final anode. Of course this is only true when the beam is travelling along the axis, but to prevent any gross errors on deflection it is common to provide symmetrical or push-pull deflection. This ensures that the mean electric field is not altered by deflection.



Trapezium distortion on a simple CRT operating with asymmetrical deflection on both axes. The focus and definition make this scope useful only for the simplest applications.

If the plates and final anode were at differing potentials then there would be a deformation of the circular cross-section of the beam (remember it is NOT in focus at this point, only at the screen where the cross-section area should be almost zero) by the plates attracting, or repelling, the outer electrons at opposite sides of the beam. This gives a sausage-shaped spot and the remedy is to make the final anode potential variable so that it may be matched to the Y plates. The X plates are then adjusted to be equal to the Y plate potential (as we shall see in a later section, it would be difficult to alter the Y plate potential). The control for setting the final anode volts is known as the "Astigmatism" potentiometer and is usually a front panel control.



The same CRT displaying a 1kHz square wave. Astigmatism is most noticeable as is the lack of HF response due to the simple deflection amplifier.

Another cause of incorrect spot size and shape is due to the pencil of electrons tending to spread, all being negatively charged. However, in high voltage tubes the velocity of the beam is high enough to keep the electrons in line by the magnetic field that they produce. The mechanism of electrostatic deflection relies on the electron beam being in the field of the deflector plates for a finite time. This means that when a very high frequency, say above 100MHz, signal is applied to the plates the signal may have changed before the electrons have emerged.

If, for example, a beam of electrons takes 10ns to travel through the plates a 100MHz signal will have completed one cycle and the deflection will be zero. In modern high velocity tubes the effect only occurs over 150 or 200MHz and the remedy is to arrange a series of deflectors, linked so that the velocity of the signal down the plates is the same as the velocity of the electron beam. However there are few uses for deflection amplifiers that can produce 200MHz output so this is of academic interest only.

THE FINAL ANODE

In order to produce the high velocity beams that are required to display fast transients, a high accelerating voltage is required. As we have seen, if this is applied to the final anode deflection sensitivity will be reduced so we apply the accelerating potential after deflection, called post deflection acceleration or PDA. Several methods of applying the PDA potential are used but they all aim at not reducing the deflection sensitivity, most important when the deflection amplifiers use transistors having only a limited output voltage swing.

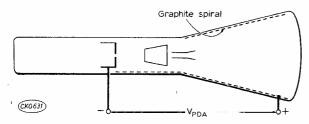


Fig. 7: Location of post deflection acceleration electrode in CRT.

The most popular form of PDA until a few years ago was the form shown in Fig. 7 and used in a lot of Cossor CRT's. The electron gun and tube are as they have been described so far and the beam is accelerated and deflected and focused normally. Around the inner wall of the tube is wound a resistive graphite spiral, connected to the final anode, and at the other end to a few kV positive. The beam is thus accelerated through this field to arrive at the screen with high velocity.

The screen tends to charge negatively at these high energies because more electrons are being gained than lost by secondary emission from the screen. The back of the phosphor is therefore given a very thin coating of aluminium and this conducts the charge to positive PDA, eliminating "screen sticking". This occurs where a local area of screen acquires a negative charge and tends to repel the beam, giving low light output. The aluminium also produces a more axial accelerating field giving better geometry and increased light output by reflecting the light forwards.

The field of the PDA is such as to produce a slightly convergent lens giving a smaller image and also, if it penetrates into the deflector plate region, causes acceleration before and during deflection, decreasing the scan even further. But in spite of this the PDA system offers a distinct advantage of increased trace brightness.

A fine wire mesh can be placed in the path of the beam just after deflection and if connected to the final anode acts as a screen to keep any PDA fields out of the deflection system. This arrangement gives rise to a PDA field that acts as a diverging lens, magnifying the deflection considerably, but also the spot size. Alternatively this mesh can be placed near the screen and PDA applied between the mesh and the screen. This gives very good results without affecting geometry but such tubes are prone to internal flashover.

SCREEN PHOSPHORS

The screen material or phosphor is arranged to give the highest possible light output of the correct colour and persistence. The table shows the range of phosphors used in cathode ray tubes, the most usual being P1 or P5, whilst P7 is sometimes used for medical applications.

Phosphor	Persistence	Fluorescence	Phosphorescence (Afterglow)	Uses
P1	Medium	Green	Green	Scopes (Visual)
P2	Long or Short	Blue/Green	Yellow/Green	Scopes (Visual)
P3	Medium	Yellow	Yellow	
P4	Medium	White	White	Television
P5	Short	Blue	Blue	Scopes (Photography)
P6	Medium	White	White	Television
PŽ	Long	Blue/White	Yellow	Radar
P8	Short	Blue/White	Yellow	
P9	Long	White	White	
P10	Permanent	Magenta	Magenta	Storage Tube
P11	Short	Blue	Blue/Green	Scopes (Photography)
P12	Long	Orange	Orange	Radar
P14	Long	White	Orange	Radar
P15	Short	Blue/Green	Blue/Green	Flying Spot Scanners
P19	Long	Orange	Orange	Radar

Table of phosphor types and principal applications.

Although the trace produced on a tube can be intensely bright, even with only a couple of kV, the contrast between the trace and the background (grey/white) is usually quite small. A filter of about 65% transmission, of the colour of the trace, placed in front of the tube can increase the contrast by a large amount despite a decrease in light output.

GRATICULES

The graticule or measuring scale can be engraved on the filter or a better idea is to cut the graticule into a piece of \$^{1}_{8}\$in. perspex. If the markings are on the front, the observer can move so that the reflection of the line from the back surface of the graticule are in line with the actual lines. This ensures zero parallax when making measurements. The perspex can be lit from the side by a red bulb causing the cuts in the perspex to light up red, although white light is better for photography due to the uneven spectral response of films. Constructors making their own graticules out of perspex must bear in mind that the clearest line, especially with side illumination, is produced by cutting the perspex with a sharp knife and not by scratching.



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4700, 5000 15p; 6800 20p; 8200, 10,000 25p

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Code	Watts	Ohms	1 to 9	10 to 99	100 up
_				e note bel	
Ç	1/20	82-220K	9	8	7.5
CCC -	1/3	4·7-470K	1.3	1.1	0.9 nett
C .	1/2	4 · 7-10M	1 3	1.1	0.9 nett
C	3/4	4 · 7-10M	1.5	1 · 2	0.9 nett
С	1	4·7-10M	3 2	2.5	1.9 nett
MO	1/2	10-1 M	4	3.3	2·3 nett
ww	1	0.22-3.9	9	9	8
ww	3	1-10K	7	7	6
ww	7	1-10K	9	9	8 nett

Codes:
C = carbon film, high stability, low noise.
MO = metal oxide, Electrosil TR5, ultra low noise.
WW = wire wound, Plessey.

Values: All E12 except C ↑ W, C ↑ W, and MO ↑ W. E12: 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and their decades. E24: as E12 plus 11, 13, 16, 20, 24, 30, 36, 43, 51, 62, 75, 91 and their decades.

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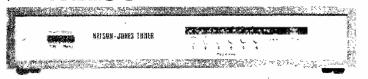
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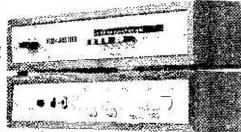
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PHOTOGRAPHY

Photographic film (even so called panchromatic) is most sensitive in the blue region and for this reason blue tubes are best suited to making photographic records. However, fast film (400ASA) together with a wide aperture, f2.8 or better, can give reasonably short exposures from a green tube.

When using single lens reflex cameras, best suited to this type of work, it is important to remember that the image on the film is scanned from right to left (lens inversion) and the direction of motion of the blind could well be from left to right, giving a small vertical exposure if the scope sweep speed is slow. The average shutter takes 1/30 or 1/60 of a second to scan the film and so one must be aware of these difficulties when dealing with fairly slow sweep speeds at fast shutter speeds. For single shot photography it is best to have the shutter completely open before the appearance of the trace.

ABERRATIONS

The ideal characteristics of a cathode ray tube are not always realised in practice due to assumptions in the theory, or plain constructional error (anodes off axis, etc.). One of the most important flaws or "aberrations" is that known as "Astigmatism" and this has already been dealt with, together with its cure.

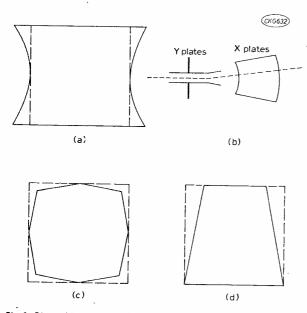


Fig. 8: Pin cushion distortion (a) can be corrected by shaping the plates as in (b). (c) illustrates barrel distortion and (d) trapezium distortion.

Most of the other aberrations are most apparent when the tube is displaying a raster. Ideally such a raster should be capable of being focused into a perfect square of scan lines, all in focus. Some defocusing occurs in deflections due to lens action between the final anode and plates, and between the plates. The effect between the plates is reduced by placing an "interplate shield" between the two sets of plates with a hole for the beam to pass through. This shield is at final anode potential and reduces the defocusing effects.

If the raster takes on the shape of Fig. 8a the distortion is known as pin-cushion distortion and is

caused by the deflected beam travelling through a greater distance between the second set of plates thus arriving at an oblique angle. This can be reduced by making the second pair of plates as in Fig. 8b. Fig. 8c shows barrel distortion caused by loss of extreme scanning sensitivity due to the PDA fields. This can only be reduced by careful design of the PDA spiral. Fig. 8d shows trapezium distortion. This is caused by asymmetrical Y deflection accelerating the beam as the driven Y plate goes positive and decreasing the X sensitivity accordingly. Specially designed plates are available for asymmetrical deflection only.

CRT DEFECTS

Other defects occur in specific tubes and it must be realised that any CRT is a compromise between conflicting factors. Consequently the best instrument tubes as fitted in laboratory scopes can cost several hundreds of pounds, but the home constructor can purchase surplus tubes for just a few pounds and many quite good home-made scopes have been built using these tubes.

With age or abuse cathode ray tubes tend to develop faults the most serious of which is likely to occur at virtually any time, is when the mechanical structure of the electron gun fails. The gun is constructed with tiny spot welds and severe shock or vibration can cause an element to be dislodged. If this happens the tube is almost surely destined for scrap.

Also linked to the mechanical structure of the tube is a fault producing what is known as a "soft" tube. This occurs when a small amount of air leaks into the bulb through an imperfect glass-to-metal seal. This may become evident only after many hours of operation and the symptoms are a diffuse display and a blue glow in the gun assembly. As the pressure inside the tube rises further, tracking occurs in the gun and external circuits can be damaged. In order to avoid this fault occurring it is necessary to take great care when handling the tube and making connections to it. Connections should never be soldered directly on to the tube pins as this is almost certain to break a seal or even crack the envelope, with glass flying everywhere at high velocity.

Perhaps the most common fault, linked directly to old age, is low cathode emission. The cathode surface looses emissivity either by the emissive layer evaporating or becoming poisoned by the remaining gas in the tube. The effect is that in order to see a trace at all the brightness control has to be advanced so far that the beam spot goes out of focus and silvery. The silvery effect is due to the cathode emitting in patches and on some scopes, if the focus control has sufficient range (making focus anode nearly the same potential as final anode), it is possible to produce an image of the cathode on the screen. The image looks a little like the full moon, the dark patches representing areas of low emission.

Sometimes a low emission tube can be improved by deflecting the spot off screen and turning brightness full up for a couple of hours. If this does not work a small transformer supplying $6\cdot 3V+10\%$ can be used to supply the heater (common practice in TV's). However the insulation of such transformers is doubtful over 1kV and a breakdown would make the tube heater/cathode short or damage it in an even worse manner. A small auto transformer is

PRACTICAL WIRELESS

NOVEMBER 1974

25p



HI-FI UNITS

ALSO:-

Section 2 of the P.W. BUYERS' GUIDE

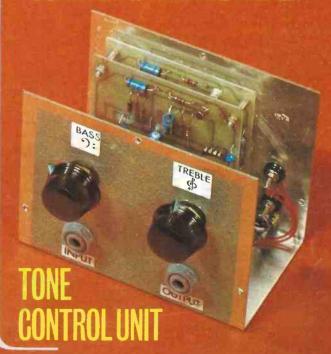
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TONE CONTROL

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Ferrite Rod Aerial for MW and LW. Chronic plated Telescopic aerial can be angled and rotated for peak short ware listening. Push pull output using 600mW transistors. Car aerial and Tape record societs. Selectivity switch. Stransistors plus 3 diodes. Latest 4"2 watt ferrite magnet loudspeaker. Air spaced ganged tuning condenser. Volume/on/off, tuning, wave change and tone controls. Attractive case in rich chestinut shade with gold blocking. Size 9×7×4in. approx. Easy to follow instructions and diagrams. Parts price list and plans 25p (FREE with parts).

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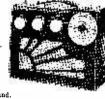
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2 watt Ferrite Magnet
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SW2, SW3, Trawler
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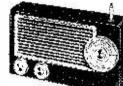
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PRACTICAL WIRELESS

VOL. 50 NO. 7 ISSUE 813 NOVEMBER 1974

BRITAIN'S PREMIER MAGAZINE FOR THE DO-IT-YOURSELF RADIO AND ELECTRONICS CONSTRUCTOR

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STAFF CHANGES

Lionel Howes has been appointed Editor of Practical Wireless and of our associate magazine Television. Eric Dowdeswell has been appointed Assistant Editor of Practical Wireless.

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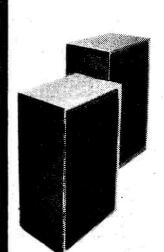
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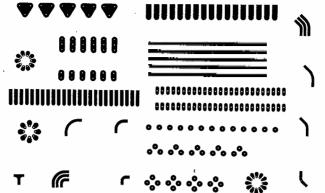
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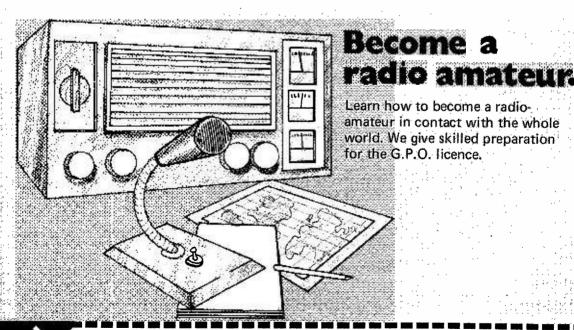
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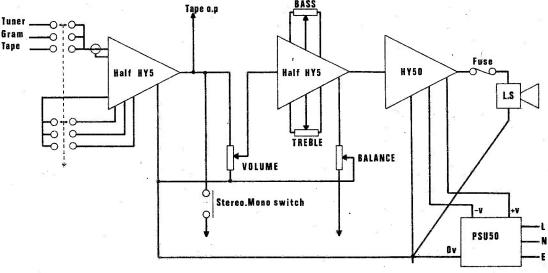
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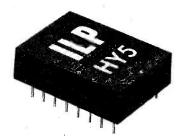
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+18-5VV

The HY50 is a complete solid state hybrid Hi-Fi amplifier incorporating its own high conductivity heatsink hermetically sealed in black epoxy resin. Only five connections are provided, input. output. power lines and earth.

TECHNICAL SPECIFICATION Output Power: 25W RMS into $8k\Omega$. Load impedance: $4^{-1}6k\Omega$. Input Sensitivity 0db (0·775V RMS). Input Impedance: $4^{-1}8k\Omega$. Distortion: Less than 0·1% at 25W typically 0·05%. Signal/Noise Ratio: Batter than 75db. Frequency Response: 10Hz-50kHz = 3db, Supply Voltage: \pm 25V. Size: 105 × 50 × 25mm.

PRICE £5.98

+48p VAT

The PSU50 can be used for either mono or stereo systems

TECHNICAL SPECIFICATIONS
Output voltage: 25V Input voltage: 210-240V. Size: L.70.
D.90, H.60mm

PRICE £4.50 PRICE £5 TWO YEARS' GUARANTEE ON ALL OUR PRODUCTS

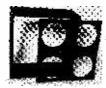
> CROSSLAND HOUSE · NACKINGTON · CANTERBURY · KENT CANTERBURY (0227) 63218

- 40p VAT P. & P. free

CUSTOM CABINETS, 331 High Street, Rochester, Kent. Tel: Medway (0634) 404199 Speaker Cabinets in kit form represent HUGE SAVINGS



2' x 12" Cabinet



4' x 12" Cabinet



Disco Console (includes lid not shown) Takes two slaves

For a long time now a large number of customers have asked us to produce cabinets in kit form, and above we show examples of cabinet styles and these are now available either fully built or in kit form ready for you to produce a professional finish in a very short time!

Kits are available in all specifications and all the kits contain everything you need as follows:-

- 1) 4 sides with handle cutouts, front edges rounded, 1 back with jack socket hole, and 1 baffleboard with speaker cutout
- 2) P.V.C. cut to size for frame and back, plusfalse front and back timbers, white front piping and speaker cloth
- 3) Recessed handles with fixing screws, jack socket, all fixing screws, corner plates, glue, and full instructions!

PRICE & TYPE LIST

Туре	Size	Price manufactured	Kit price
2 x 12" (illustrated above)	'36" x 18" x 13" x ¾	£19.50	£12.50
4 x 12" (illustrated above)	31" x 31" x 13" x ⅔		£17.50
4 x 12" P.A. Column	48" x 27" x 13" x ¾	£30.00	£21.50
1 x 18"	31"x31"x13"x∄	£24.50	£17.50
1 x 15" with two top horn cutouts	36" x 20" x 13" x ⅔	£21.00	£13.50
Mini Disco (state deck cutout BSR, GARRARD etc.)	33" x 20" x 10" x ½	£20.00	£13.00
Maxi Disco (illustrated) (state deck cutout BSR, GARRARD etc.)	42"x20"x10"x½	£25.00	£18.50

Please ask for quotation on any other type or size of cabinet you may require. ALL OUR PRICES INCLUDE VAT AND UK DELIVERY

PC ETCHING KIT

Tyne

Contains 11b Ferric Chloride, 100 sq. ins. copper-clad board, DALO etchresist pen, abrasive cleaner, etching dish & instructions, all for only £3.30

RESISTORS & CAPACITORS

500 assorted resistors £1,35. 2500 £4.70. 150 poly. ceramic, mica etc capacitors 80p.

VEROBOARD

100 sq. ins. assorted sizes and pitches (no tiny pieces) £1.10.

3W TAPE AMPLIFIERS

3W TAPE AMPLIFIERS
Polished wooden cabinet 14, 13 x 9'
containing a sensitive (20,4V) 4 valve
amplifier with tone 4 volume controls. Gives 3 watts output to the 7 x 4" 3Ω
speaker. Also a non-standard tape
deck. Supplied in good working
condition with circuit. Standard mains
operation. £4.50. Suitable cassette
£1.10. Spare head 33D. Tape £2.
£1.10. Spare head 33D. Tape £3D.
Spare head 33D. Tape £3D.
ELEG. ESSO. Amplifier chassis
only, complete and tested (2xECC83,
ELEG. ESSO.) and speaker £3.

VERSATILE POWER UNIT

Contains mains transformer, 2A thermal cut-out and bridge rectifier. Will give 1-7-10-5V output with 2 extra capacitors (supplied) £1.20. Also available as model garage with switch, lamp, lack plug etc. (Used for 'Hot Wheels') £1.70.

LEO III COMPUTER

Arriving late-October. All parts available, including 3000 reels tape, ½" decks, power units, etc.

FERRIC CHLORIDE

Anhydrous technical quality to Mil Spec in 1lb double sealed packs. 1lb 80p, 3lbs £1.65, 10lbs £4.45, 100lbs

PO AMPLIFIER UNIT

Contained in steel case 5½ x 5 x 3½" are 2xGET116 transistors on heat sinks, 3 pot cores, 2 30V zeners, 4 audio transformers, 1% resistors & caps. With circuit diagram £1.

71b BARGAIN PARCELS

Hundreds of new components— Pots, resistors, capacitors, switches, + PC boards with transistors and diodes, and loads of odds and ends. Amazing value at only £2.30.

COMPUTER PANELS

3lbs asstd £1.40, 7lbs £2.55, 56lbs £15. Pack containing 500 components with at least 50 transistors 95p. 12 High quality panels with power transistors, trimpots, IC's etc £2.50. Thousands of boards at shops for callers from 5p. callers from 5n.

SLOTMETER

Ex-Pay TV, takes 10p pleces, has 3 digit mechanical counter, coin counter, Sangamo-Weston impulse movement, nylon gearing, switch, etc. Only £1.20.

MISCELLANEOUS

Transformer, Mains pri 16-0-16V with 9V tap sec 1;A £2. Post office 4 digit counters 50p. Baianced archature earpieces, use as mic or spkr. 20Q impedance 30p. 2N3055 3ks. 80 + 80 + 20µF 350V 15p,10 for £1.15, Multimeters: good range in stock from £3:50.

All prices shown include 8% VAT and postage (mainland only) SAE list, enquiries.

GREENWELD ELECTRONICS (PW8)

Mail order dept., wholesale/retail shop 51 SHIRLEY PARK ROAD, SOUTH-AMPTON. Tel 6703 772591. Other retail shops at 21 Deptford Broadway SE8, Tel 01-692 2009 and 38 Lower Addiscombe Road, Croydon. Callers Welcome.



PRACTICAL WIRELESS

ELECTRONIC IGNITION SYSTEM

This Capacitor-Discharge Electronic Ignition System was described in *Practical Wireless*, and has proved extremely popular.

The kit is supplied with a ready-drilled roller-tinned printedcircuit board and fully machined die-cast case with AMP Electrical Spade Connector Block together with a custom wound transformer, first grade components and full constructional details.

The original circuit employed Germanium Power Transistors for the negative earth version. WE OFFER SILICON P.N.P. POWER DEVICES AT NO EXTRA COST! All components are available separately. Case size $4\frac{3}{4}$ " x $3\frac{3}{4}$ " x 2". Complete assembly and construction manual free with kit, available separately 25p.

SUITABLE FOR 12V SYSTEMS WITH NEG. OR POS. EARTH.

PRICE: £9.50 U.K. ORDERS PLEASE ADD VAT

Quantity Discounts:

Trade and Overseas 1-5 Nett 6-9 less 10% Enquiries Invited 10-49 less 15% 50-99 less 20% Mail Order Only. 100-999 less 25% 1000 up less 30%

PLEASE STATE POS. OR NEG. EARTH WHEN ORDERING

DABAR ELECTRONIC PRODUCTS



98 LICHFIELD STREET WALSALL, Staffs WSI IUZ



SUPERSLIM BSR LATEST

STEREO AND MONO STEREO AND MONO
Plays 12", 10" or 7" records.
Auto or Manual. A high
quality unit backed by BSR
reliability with 12 months'
guarantee. AC 200/250v.
Size 13\frac{1}{2} 11\frac{1}{2} in.
Above motor board 3\frac{1}{2} in.
Below motor board 2\frac{1}{2} in.
With STEREO and MONO KTAL



85p carriage

PORTABLE PLAYER CABINET

Modern design. Black rexine covered Silver front grille. Chrome fittings. £4.50 Post 45p. Motor board cut for BSR deck.

COMPACT PORTABLE STEREO HI-FI



SPECIAL OFFER

Teak finish

Weight 13lbs.

SMITH'S CLOCKWORK 15 AMP TIME SWITCH 0-60 MINUTES

Time SWITCH -06 MINUTES
Single pole two-way.
Surface mounting with fixing
screws. Will replace existing wall
switch to give light for return home,
garage, automatic anti-burgular lights, etc. Variable knob.
Turn on or off at full or intermediate settings. Makers
tast list price 24-50. Brand new and fully guaranteed.
Fully insulated.
OUR PRICE 21-26 Post 25p

WEYRAD PS0-TRANSISTOR COILS

RA2W Ferrite Aerial 85p	Printed Circuit, PCA165p
I.F. P50/2CC 470 kc/s. 40p	J.B. Tuning Gang £1.20
8rd I.F. P50/3CC 40p	Weyrad Booklet10p
Spare Cores 3p	OPT1 65p
P50/IAC	Driver Trans. LFDT4 65p
Persite Dod 8 v Ain 90n 8 v	8 in 90n 8 v 8 in 10n

5 K. ohms to 2 Meg. LOG or LIN. L/S 20p. D.P. 35p. STEREO L/S 50p. D.P. 75p. Edge 5 K.S.P. Transistor 25p Idea 25 & colour 10p vd.

VOLUME CONTROLS | 80 Ohm Coax 5p. yd.

8in & 10 x 6in ELAC HI-FI SPEAKER

Dual cone plasticised roll surround. Large ceramic magnet. 50-16,000 o/s.
Bass resonance 55 c/s.
8 ohm 10 watt. 43.75 Each Post 52p

10 inch 12 watt Twin Cone, 8 ohm £4:50

E.M.I. $13\frac{1}{2} \times 8in$. SPEAKER SALE!

With twin tweeters and crossover, 10 watt, State 3 or 8 or 15 ohm. A4-50 (As illustrated)

With flared tweeter cone and ceramic magnet. 10 watt.
Bass res. 45-60 c/s.
Flux 10,000 gauss.
State 3 or 8 or 15 ohm. Post 25p

BOOKSHELF CABINET Size 16 × 10 × 9 in. teak finish



£6.60 Post 25p

E.M.I. 13 \times 8 in. BASS WOOFER. 20 WATTS 15 Ω RUBBER CONE SURROUND. 25.50 Post 25p.

SPECIAL OFFER

100 ohm 20W Rheostat 2jin. diam. Ceramic Former, screw terminals, jin. diam. spindle. 95p, post 25p.

ANOTHER RCS BARGAIN!

ELAC 9 × 5in. HI-FI SPEAKER. TYPE 59RM. THIS FAMOUS AND WIDELY USED UNIT NOW AVAILABLE AT BARGAIN PRICE 10 WATT, 8 OHM. CERAMIC MAGNET. £2.95

R.C.S. STABILISED POWER PACK KITS All parts and instructions with Zener Diode, Printed Circuit, Bridge Rectifiers and Double Wound Mains Transformer. Input 200/240V a.c. Output voltages available 6 or 9 or 12 or 15 or 18 or 20V d.c. at 100mA or less. PLEASE STATE VOLTAGE REQUIRED. £2.20 Post Details S.A.E. Size \$1 × 11 × 1 in.

R.C.S. GENERAL PURPOSE TRANSISTOR PRE-AMPLIFIER BRITISH MADE

Ideal for Mike, Tape, P.U., Guitar, etc. Can be used with Baitery 9-12v. or H.T. line 200-300V. d.c. operation. Size 11" < 12" × 12" × 12". Response 25 c/s. to 25 Ke/s, 28 dB gain. For use with valve or transistor equipment. 99p Post Full instructions supplied. Details S.A.E.

TEAKWOOD LOUDSPEAKER GRILLS. Will easily fit to baffle board. Size 18½ × 10½in—75p. 10½ × 7¼in—45p.

E.M.I. WOOFER AND TWEETER KIT

Wooter 103 × 6jin. Ceramic Magnet, 44oz. 13,000 lines. Tweeter 3jin. square, 10,000 lines. Crossover condenser full instructions supplied. Impedance 8 chms. Power 12 watts. £5.75 Post 45p.

BRITISH FM/VHF TUNING HEART

88 to 108 M/CS British made, 2 Transistors ready aligned requires 10-7 M/CS I.F. Complete with tuning gang. Connections supplied but some technical experience 10.7 M/Cs IF Strip £4.95 essential Our price £3.95

MAINS TRANSFORMERS	All post
Eagle MT12 12-0-12V 50mA	991
250-0-250 80 mA. 6-8V 3-5A 6-8V 1A or 5V 2A.	£2.50
350-0-350 80 mA 6.3V 8.5A, 6.8V 1A or 5V 2	A£8.00
300-0-800V 120mA, 6 3V 4A C.T.; 6 8V 2A	£4.28
MINIATURE 200V 20mA, 6-3V 1A	£1
MIDGET 220V 45mA, 6-3V 2A	£1.10
HEATER TRANS. 6.3V 1 amp 85p. 3 amp £	1.20
GENERAL PURPOSE LOW VOLTAGE. Trap	ned onimute
at 2 amp. 3. 4. 5. 6. 8. 9. 10. 12. 15. 18. 24 and	POL CASPUS
1 amp. 6. 8. 10, 12, 16, 18, 20, 24, 30, 36, 40, 4	004 20.00
1 amp, 5, 8, 10, 12, 10, 10, 20, 24, 60, 60, 40, 7	0, 00 20 00
2 amp, 6, 8, 10, 12, 16, 18, 20, 24, 30, 36, 40, 4	10, 00 22 0
8 amp. 6, 8, 10, 12, 16, 18, 20, 24, 30, 36, 40,	10, 00 30 00
5 amp. 6, 8, 10, 12, 16, 18, 20, 24, 80, 36, 40,	18, 60 29-70
5, 8 and 18V 5 amp £1.20. 8 amp, 3, 5, 8,	10, 18 and
5.0-5V £1.80, Ditto 5 amp. £1.50; 8-0-8V 5	00mA 90p
9V 1 amp 95p 12V 800mA 75p 12V 500mA 85p	L2V 750mA
95p. 12. 36. 48V 2 amp £2. 20V 3 amp £2.	
AUTO TRANSFORMERS, 115V to 230V or 23	DV to 115V
150W £2 95; 600W £7 50; 760W £10; 1000W £1	
CHARGER TRANSFORMERS. Input 200/250V	
for 6 or 12V, 11 amp £1 50; 2 amp £1 80; 4	
BATTERY CHARGERS, Ready built with least	is and clips
11 ama 90 4 ama 64 5 ama 64.50	_

1; amp £2; 4 amp £4; 5 amp. £4·50. FULL WAVE BRIDGE CHARGER RECTIFIERS; 6 or 12V outputs. 1; amp 40p; 2 amp 55p; 4 amp 85p.

MAINS ISOLATING TRANSFORMER

Primary 0-110-240V. Secondary 0-240V. SA. 720W. Issulated terminals. Varnish impregnated. Fully enclosed in steel case with fixing teet. OUR PRICE £ 12 Carr. Famous make. (Value £19) Can be used as 800W auto transformers 240-110V. IDEAL FOR COLOUR T.V. OR GARDEN TOOLS.

NEW ELECTRO	LYTIC CONI	ENSERS	
2/850V 14p :	100/25V	10p : 60 + 50/800V	50
4/850V 14p	250/25V	14p 350 + 50/325	85
8/350V 22p		20p 32 + 82/350V	
16/450V 25p	1000/25V	35p 82 - 32/450V	
82/450V 35p	1000/50V	47p 32 + 32 + 32/3	
82/500V 50p	8+8/450V	22p + 32 + 32 + 32/	
25/25V 10p	8+16/450V	25p 900/350V	
60/50V 10p	16+16/450V	40p 4700/63V	95

LOW VOLTAGE ELECTROLYTICS

LOW VOLTAGE ELECTROLITICS
1, 2, 4, 5, 8, 16, 25, 30, 50, 100, 200mF. 15V. 10p.
500mF. 12V. 15p; 25V. 20p; 50V. 30p.
100mF, 12V. 25p; 25V. 30p; 50V. 47p; 100V. 70p.
2000mF. 6V. 25p; 25V. 42p; 50V. 57p.
2000mF. 6V. 25p; 25V. 42p; 50V. 57p.
5000mF. 6V. 25p; 12V. 42p; 25V. 75p; 35V. 85p; 50V. 95p. MICRO SWITCH. Single Pole Change Over. 20p. Sub Min

CERAMIC 1pF to 0.01mF, 4p. Silver Mica 2 to 5000pF, 4p. PAPER 350V-0-1 4p, 0-5 13p; 1mF 15p; 2mF 150V 15p. 500V-0-001 to 0-05 4p; 0-1 5p; 0-25 8p; 0-47 25p. TWIN GARG, "0-0" 280pF+176pF, 21-20; 500pF standard 75p; 385-865 with 25+25pF Slow motion drive 50p. SHORT WAVE, SINGLE 10pF 80p; 25pF 55p; 50pF 55p. NEON PANEL INDICATORS, 250V AC/DC Amber 25p. RESISTORS, 'tw, 'tw, 'lw, 20°, 1p; 2W, 5p. 100 to 10M. HIGH STABILITY, 'tw, 20°, 1p; 2W, 5p. 10D to 10M. HIGH STABILITY, 'tw, 20°, 10 ohms to 6 meg., 10p. Ditto 5°, Preferred values 10 ohms to 10 meg., 4p. WIRE-WOUND RESISTORS, 5 wait, 10 wait, 15 wait 10 ohms to 100K 10p each.

TAPE OSCILLATOR COIL, Valve Type 35p.

NEW MODEL "BAKER LOUDSPEAKER" 12in, 50 watt GROUP 50/12 8 or 15 ohm high power full £12.95

BAKER MAJOR 12" £8.50



Post free 30-14,500 c/s, 12in. double cone, woofer and tweeter cone together with a BAKER ceramic magnet assembly having a flux density of 14,000 gauss and a total flux of 145,000 Maxwells. Bass resonance 40 c/s Rated 20 watts. NOTE: 3 or 3 or 15 ohms must be stated.

Module kit, 30-17,000 c/s with tweeter, crossover, buffle and instructions. £10.95 Post free Please state 3 or 8 or 15 ohms.

BAKER "BIG-SOUND" SPEAKERS Post free

TEAK VENEERED HI-FI SPEAKER CABINETS
For 12in, or 10in, dia, speaker 20 × 13 × 6° ± 10-50 Post 259
For 13 · 6in, or 8in, speaker 16 × 10 × 6° 46-69 Post 259
For 8 × 5in, speaker 16 × 8 × 6° ± 495 Post 259
For 6in, and tweeter 12 × 8 × 6° ± 495 Post 259
For 6in, and tweeter 12 × 8 × 6° ± 400 Post 259
LOUDSE EAKER CABINET WADDING 18in, wide, 209 it

EMI 63in. HI-FI WOOFER

Sohm, 10 watt. Large ceramic magnet.

Special Rubber cone surround.

Frequency response 30-12,000
c/s. Ideal P.A. Columns,

Hi-Fi Enclosure Systems, etc.

Suitable cabinet 12 × 8 × 6 24-00.

Suitable cabinet 22 × 8 × 6 24-00.





ELAC CONE TWEETER

The moving coil disphragm gives a good radiation pattern to the higher frequencies and a smooth extension of total response from 1,000 c/s to 18,000 c/s. Size 34 × 35 in. deep. Rating 10 watt, 3 ohm Suitable 21.90 Post 20p ver £1.80 £1.90 Post 20p

MAJOR 100 WATT ALL PURPOSE **GROUP OR DISCO** AMPLIFIER

All purpose transistorised. Ideal for Groups, Disco and P.A. 4 inputs speech and music. 4 way mixing. Output 8/15 ohm. a.c. Mains. Separate trable and bass controls. MAJOR 50 WATT 4 INPUTS. 2-WAY MIXING £39



3-WAY CROSSOVER 950 CPS and 3000 CPS with leads ready assembled

BARGAIN 4 CHANNEL TRANSISTOR MONO MIXER.
Add musical highlights and sound effects to recordings.
Will mix Microphone, records, tape and tuner
4.50
with separate controls into single output, 9 volt. £5.95 TWO CHANNEL STEREO VERSION

BARGAIN 8 WATT AMPLIFIER. 4 Transistor £3.95 and bass controls 18v. DC operation.

COAXIAL PLUG 10p. PANEL SOCKETS 10p. LINE 18p COAXIAL OUTLET BOXES, surface, 35p. BALANCED TWIN FEEDER 300 ohns 7p yard. JACK SOCKET \$td. open-circuit 15p, closed-circuit 23p. Chrome Lead Socket 45p. Phono Pings 8p. Phono Socket 8p. JACK PLUGS \$td. Chrome 20p; 3-mm Chrome 12p, DIM SOCKETS Chassis 3-pin 10p; 5-pin 10p. DIM SOCKETS Lead 3-pin 18p; 5-pin 25p. DIM PLUGS 3-pin 18p; 5-pin 25p. VALVE HOLDERS. 5p; CERAMIC 10p; GANS 5p.

REVERSIBLE 4 POLE MOTOR £2.25 1,400 r.p.m. Reversible 42 Watt, Post 25p spindle 14" × 7₁₃₂", size 34" × 3". As illustrated. With Cooling Fan 240V A.C.

E.M.I. GRAM MOTOR
120v. or 240v. A.C. 2,400 rpm. 2-pole
70mA, Size 2; × 2½ × 2½ in.

COMPONENT SPECIALISTS

337 WHITEHORSE ROAD, CROYDON Open 9-6 Wed. 9-1 Sat. 9-5 (Closed for lunch 1.15-2.30) Buses 50, 68, 159. Rail Selhurst. Tel. 01-684 1665

TRANSFORMERS

SAFETY MAINS ISOLATING TRANSFORMERS Prr. 120/240 V Sec. 120/240 V Centre Tapped and Screened

Size cm

Weight

VA (Watts)

		10. 07 49 50		20 60 00		16 oz 1 8 3 12 5 8		1 9	7.0 x 9.9 x	6·0 7·7 8·9 9·3	× 6	· 0 · 6	£ 2.5: 3.7: 4.13	5 38 9 45
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ŀ	Ref. 238 212 13 235 207	MA. 200 IA I 100 330,		1	2 2 4 6	Siz 8x2 1x5	6x2 8x4	· 8	3-0-	3 0-6	H SC LTS			P 10 30
	13 235 207 208	300,	330 500 IA	10	4 4-	9×2 8×2 1×5	6x2 ·8x4 ·6x2 ·9x3 ·4x4 ·4x6	·5	9-0- 0-9, 0-8-	9 0-9 9. 0-	8-9		1·28 1·42 2·23 3	P 10 10 13 9 10 18
	236 214 221 206	1 A, 200, 300, 700	200 300 (D.C.) I A 500	1 1					0-15	0-2	13 30		I-30 I	9
	206 203 204	IA, 500, IA,	500 1A	2 1	48.	3X/	7x7 0x7 7x7	.0	0-15 0-15 0-15	-20, -27, -27.	0-15 0-15 0-15	-20 -27 -27	3.06 3	8
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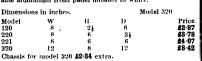
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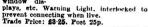
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1	79		2-21	0.38
2	4 3		8-26	0.38
3	20		4 10	0.42
4	21		4-68	0.52
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0-6	0-6	500	500	234	1.80	0.10
0-6	0-6	1000	1000	212	1.98	0.22
9-0-v		100	F10000	13	1.22	0-10
0-9	0-9	330	330	235	1-48	0.10
0-8-9	0-8-9	500	500	207	1.75	0.22
0-8-9	0-8-9	1000	1000	208	2-80	0.36
15-0-15	4-	40		240	1 22	0.10
015	0-14	200	200	236	1-80	0.10
20-0-20		30		241	1.98	0.10
0-20	0-20	150	150	237	1.30	0.10
0-15-20	0-15-26	500	500	205	2.47	0.38
0-20	0-20	300	300	214	1.72	0.22
020		3500	NO SCREEN	1116	3.00	0.40
20-12-0 12 20		700 (D/C	D	221	2.81	0.30
0-15-20	0-15-20	1000	1000	206	8-22	0.38
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1000	84	-15.70	0.75	12:40	0.82
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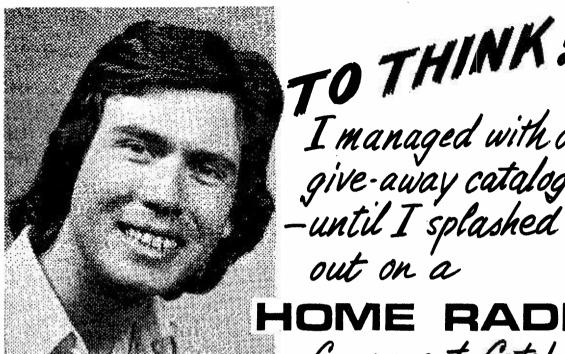
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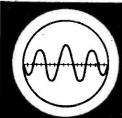
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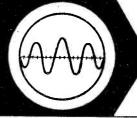
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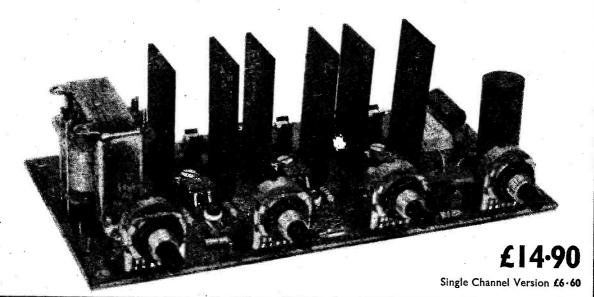
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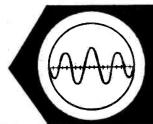
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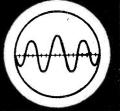
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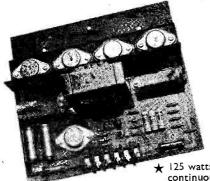


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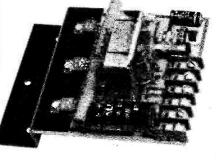
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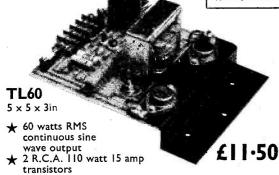
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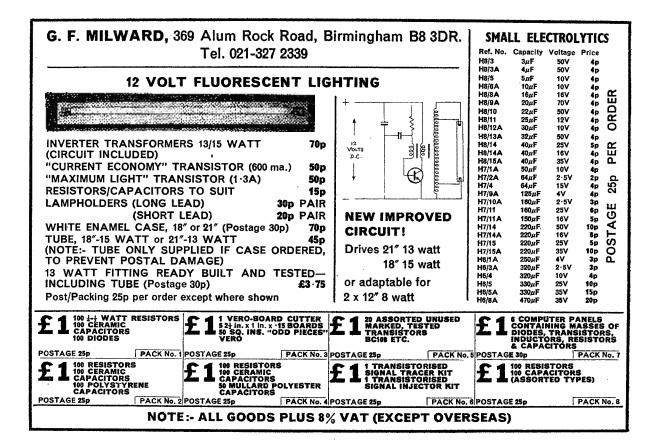
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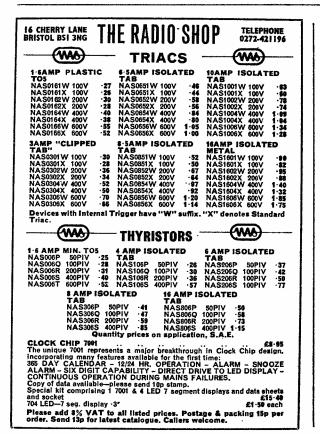
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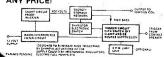
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С	3/4	4 · 7-10M	1.5	1 · 2	0 · 97 nett
С	1	4 - 7-10M	3.2	2.5	1 · 92 nett
MO	1/2	10-1M	4	3.3	2 · 3 nett
ww	1	0·22-3·9Ω	11	10	8 .
ww	3	1-10K	9	8	6
ww	7	1-10K	11	10	8

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1.0	-	_	_	-		11p	_	8p	
2.2	_	_	-		11p		8p	9p	
0·47 1·0 2·2 4·7		-	_	11p	_	8p	9p	8p	
10		_	-		8р	9p	8р	8p	
22 47	_	_	8p		9p	8p	8p	10p	
47	8p	_	9p	8p	8p	8p	10p	13p	
100	9p	8 p	8p	8p	9p	10p	12p	19p	
220	8p	8p	9p	10p	10p	11p	17p	28p	
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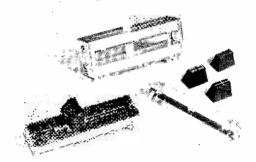
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DIGITAL INTEGRAL CIRCUITS SN7400 20p SN7428 50p SN7473 40p SN74110 50p SN74167 55-25 SN7401 20p SN7432 42p SN74171 44p SN74118 51-90 SN74170 54-10 SN7402 20p SN7432 42p SN7456 SN7456 SN7457 SN7403 20p SN7437 50p SN7457 50p SN74121 50p SN74174 52-90 SN74374 52-90 SN74374 52-90 SN7491 50p SN74176 SN7490 SN7490 SN7490 SN749174 SN7490 SN7490 SN7490 SN749174 SN7490	AB12 3" 2" AB14 7" 5" AB15 8" 6" AB16 10" 7" AB17 10" 44' AB18 12" 5" AB19 12" 8"	1" 44p 2" 70p 21" 84p 3" £1-06 3" £1-22 3' £1-20 3" £1-21	SP F CUTTER 52b 52b 100 PINS SS 30b 30b 100 PINS DS 30b 30b 100 PINS DS 11-20 21-20 Prices Correct June 12
SN7405 20p SN7408 25p SN7401 £1-25 SN74123 £2-70 SN74177 £1-60 SN7407 30p SN7404 20p SN7408 £1-50 SN74102 £1-50 SN74105 £1-50 SN7407 30p SN7404 75p SN7408 £1-00 SN74145 £1-50 SN74101 £1-50 SN7409 SN7404 75p SN7408 5p SN7409 45p SN7404 25p SN7408 45p SN7401 £1-50 SN7401 £1-	ALUMINUM BOKES WITH SLOPII FOR PRE-AMPS, ETC., USING SLI AB20 8° Long 9° Wide 35° High at b With PLS Sorows AB21 As above but 10° long AB22 As above but 10° long V41 VU METER The V41 is calibrated – 20 to – 3 suitable for use as a recording le SenathWhy. 130 u.b. Internal re-	LIDER CONTROLS back . £2-00 ifront . £2-20 £2-40 22-50 3 and 0-100%, making it level meter or as a power	NEW SERIES TRANSISTOR DATA BOOKS DTAS USA Band 3 Transistor Characteristics. Viz. 186285 all 1872 and
SN7417 30p SN7451 20p SN7495 30p SN74160 £2-60 SN74194 £2-50 SN7420 20p SN7433 20p SN7495 £1-00 SN74160 £2-60 SN74195 £1-85 SN7422 48p SN7435 20p SN7495 £1-55 SN74162 £3-40 SN74196 £1-50 SN7425 48p SN7460 20p SN74100 £2-50 SN74162 £3-40 SN74196 £1-50 SN7425 48p SN7470 30p SN74105 £1-45 SN74164 £2-75 SN74197 £1-60 SN7427 20p SN74105 £1-55 SN74196 £2-75 SN74196 £4-60 SN74197 £4	Dimensions: 40 × 40 × 29mm. ALSO STOCKED Electrolytic Capacitors Mullard, Polyester. Polystyrene, Sliver Resistors ‡W-10W Potentiomete Preset. Rectilinear multiturn switches rotary, slide, toggle, etc.	d. Sprague, Lorin etc Mica Capacitors etc lers, carbon, wirewound. Antex Soldering Irons.	Unless otherw V.A.T. all prices are EXCLUSIVE of a T. Please and 8%, to all prices Carriage orders under \$5 - 20p Over £5 post free

AUDIO ACCESSORY SHOP, 17 TURNHAM GREEN TERRACE, CHISWICK, W.4

	MICROPHONES PRICES INC. VAT	•	TWEETERS PRICES INC. VAT		CASSETTES PRICES INC VAT
CM10	Crystal Lapel Microphone with Lead and	CT5	Cone Tweeter. Freq 3000-15000Hz Cross- over freq 3000Hz. Imp. 8 ohms. Suitable for		C60 C90 . C120 BASF LH 88p £1·21 £1·78
CM20 CM73	Plug 60p General purpose Crystal Microphone £1-20 Crystal Stick Microphone with Switch	CT10/8	systems up to 10 watts RMS	£1·98	MEMOREX MROX2 Oxide 99p £1-32 £1-76 CROX2 £1-47 £1-91 —
CO92	Lead and Plug	CT10/16		£2 · 60 £2 · 60	PHILIPS
CO96	shield	DT33	Dome Tweeter Freq. 2000-18009Hz Cross- over freq. 3000Hz Imp. 8 ohms. Suitable for	ar 70	Available in Black or Green; Approx width 54in £1.75 yd.
DD1	Cassette Dynamic Microphone with Plugs for signal and stop/start. 200 ohms £2 · 20	F F2 7	systems up to 40 watts	15.70	HEADPHONES Type H-202 Features Mono/stereo switch, Volume controls on each channel Fred response 20-20,000Hz
DD5 DD6	Electret Paging Microphone, on table stand with gooseneck and switch, 600 ohms £14-89 Lavalier Microphone with Windshield,	FF28	systems up to 30 watts RMS	£6·80	Impedance 4-16 ohms £4-50. TEAK VENEERED SPEAKER CABINETS
	Lavalier Cord. 6 metres Cable, 600 ohms/ 50kΩ	HT15	over freq 3000Hz Imp 8 ohms Suitable for systems up to 20 watts RMS	£8·20	For 8 × 5in Speaker Size $9_{2} \times 13_{2} \times 5_{1}^{2}$ £3.50 8in \pm Tweeter $7_{1}^{2} \times 11_{1}^{2} \times 5_{2}^{2}$ £5.00 13 × 8in $10_{1}^{1} \times 17 \times 6$ £5.75
DM18HL DM73	Dual Impedance Dynamic Microphone with desk stand, 600 ohms/50kΩ £10-50 Omni Directional Dynamic Microphone	HT21	over freq 3000Hz Imp 16 ohms. Suitable for systems up to 30 watts RMS	£4·00	13 × 8:n. + Tweeter 12 × 18 ₇ × 81 £7 • 50 12:n. + Tweeter 15½ × 18 × 82 £9 • 60
	with desk stand, 6 metres Cable and Plug.	H121	Horn Tweeter. Freq 2500-20000Hz Cross- over freq 3000Hz Imp 8 ohms. Suitable for systems up to 40 watts RMS	£6-20	VALVE AMPLIFIERS PRICES INC. VAT
DM81 DM82	Remote Dynamic Microphone, Cassette type with Plugs. 200 ohms	MHT10	Horn Tweeter Freq. 2000-18000Hz Crossover freq 3000Hz. Imp 8 ohms. Suit-		Robust units suitable for most PA/Disco uses 5 watt 2 inputs, Vol. Trebie, Bass Controls . £12-50 15 watt 4 inputs, Vol. Trebie, Bass Controls . £24-50
DM94	with Plugs 200 ohms		able for systems up to 30 watts RMS	£4-00	30 watt 4 inputs, Vol. Treble, Bass Controls 529-50 50 watt 4 inputs, Vol. Treble, Bass Controls 536-25 150 watt 4 inputs with separate vol controls
DM614	with Stide on Windshield and Switch 50kΩ £9-56 Pencil Type Dynamic Microphone with Cable, Lavalier Cord and Base 50kΩ £3-20		CROSSOVERS		plus master vof, treble, bass £75-90 500 watt 4 inputs each with independent vol.
PROM5	Lavalier Capacitor Microphone with Tie Clip 5-8 metres Cable 600 ohms £15-80	CN23	PRICES INC. VAT '2 Way Crossover Network, Imp. 3 ohms.		treble and bass controls plus overall master vol. control
	Omni Directional Capacitor Micro- phone with 6 metres Cable 600 ohms £30-00 Uni-Directional Capacitor Microphone	FF5	Crossover 3000Hz. Suitable up to 15 watts RMS 3 Way Crossover Network Imp 8 chms	£1.70	MICROPHONE MIXERS PRICES INC. VAT
	with 6 metres Cable 600 ohms £32-00 Capacitor Boom Arm Microphone with		Crossover freqs 1000 and 5000Hz. Suitable up to 25 watts RMS	23 - 30	FF1 4 Channel Mono Mixer and Preamplifier with individual slide controls Battery operated £25.60
UD50HL		FF30	3 Way Crossover Network Imp 8 ohms Crossover freqs 1000 and 5000Hz Suitable		FF10 7 Channel Stereo Mixer and Preamplifier with individual slide controls Battery
200C	with Switch. 6 metres Cable and Plug 600 chms/50kΩ £12-00 Slim Line Crystal Microphone with Switch. Cable and Connector £3-80	SN75	up to 25 watts RMS. 2 Way Crossover Network Imp 8 ohms Crossover 3000Hz. Suitable for systems up to 15 watts RMS.	£9-20	operated £34-00 Stereo Frequency Controller and Pre- amplifier, uses five slide controls Battery operated £34-90

All mail order and enquiries to 270 Acton Lane Tel. 01-994 6275

EXHIBITIONS?!

WHAT is happening to the R.S.G.B. National Mobile Rally? This annual event, as many readers will be aware, took place in the grounds of Woburn Abbey during the month of August.

It was not the day of continuous rain that made the exhibition part of the rally a wash-out—attendance was good despite the climatic conditions. Apathy on the part of the organisers and many exhibitors resulted in dismal displays on nameless stalls.

Who were these nameless exhibitors? These people were, in effect, representatives of one of our greatest national activities—Amateur radio and the amateur electronics constructor. The question being asked was, "surely this is not the R.S.G.B. National Mobile Rally? I must have taken the wrong turning!"

Exhibitors displaying new equipment and those displaying 'surplus' gear were intermixed. Yours truly spent a considerable amount of time trying to find the whereabouts of various exhibitors, without avail. Little information was forthcoming—even from the R.S.G.B. stand itself! Well-established and respected manufacturers and distributors were conspicuous—by their absence. Who can blame them?

Someone had better pull up their socks or we may see the rapid demise of what should be, as the title implies, our *National Mobile Rally*.

Do you remember the Radio Communications or Hobbies Exhibitions sponsored by the Radio Society of Great Britain? They were held annually in the London area and were extremely popular. What happened to them.

Practical Wireless and other major organisations, gave their support on numerous occasions and we are justly proud of the part that we contributed by showing our flag, on behalf of the radio and electronic constructor.

This hobby of ours encompasses an exceedingly wide sphere in the field of electronics and it is the responsibility of the Editor and his staff—as a team—to balance the editorial contents of each issue—to cater for many tastes. The satisfaction that the constructor derives from 'switching it on' is extremely gratifying and indeed therapeutic. We are indeed fortunate in that we live in an era of component plethora. Of course, there are shortages in many areas, but we suggest that the pessimists cast a careful eye over the pages of our 1974/5 PW Buyers' Guide to Radio and Electronic Components.

Many new items are included, each month by advertisers in their respective columns. Take a good look at the small print, you could be pleasantly surprised!

We shall be exhibiting at the 1974 International Audio Festival and Fair, Olympia, London. Many PW constructional projects will be on show, including unique constructional designs not yet published in this country. A further exciting development in the PW Tele-Tennis constructional project will also be unveiled.

Members of the editorial and advertising departments will be in attendance to deal with enquiries. We shall also have a limited number of free 'give-aways' to visitors.

Don't forget the PW slogan—Stay tuned to PW for full coverage of the finest and up-to-the minute constructional projects.

A date for your diary—Practical Wireless, Stand B12, International Audio Festival & Fair, Olympia, 28th October—3rd November inclusive.

LIONEL E. HOWES-Editor.

NEWS...

Crofton move

ROFTON ELECTRONICS have moved. Their new address is: 124 Colne Road, Twickenham, Middlesex. (Tel: 898 1569):

A foolproof Electric Lock

OME quite clever ideas have appeared in journals for electronic locks. But our vote goes to a professional approach recently announced which, as far as we can see, is almost fool-proof. The code for this lock is carefully stored in a CMOS shift register memory. When the "electronic" key is inserted, the code in the key is interrogated by the lock which compares it with the code in its memory. If the two codes are identical the lock will open. The key itself contains another shift register with the identical code in its memory banks. Even a small 32-bit memory would provide a possible four million combinations.

When the key is inserted into the lock it activates a microswitch. This causes the lock to transmit a series of pulses which in turn make the "key" enter its code into the lock for comparison.

Because the key does not emit signals (i.e. magnetic or sonic or anything else) it is impossible to "read" the code from the key. Again, any exploratory signals sent into the lock would immediately alter or destroy its memory (fail safe).

One last cunning asset. The speed of operation of the memory circuits in the lock is fast when opening the door with the correct. key. But slow by "logic" standards. If you were to permutate all combinations possible by plugging some sort of pulsing device into the lock instead of the key—it would take well over a year to run through all the possible combinations. Sorry—not available on the market yet and that's all the information we can get at present.

NEWS...

NEWS...

NEWS...

Not to be missed -

THE LATEST Heathkit Catalogue is now available free from: Heath (Gloucester) Limited, Bristol Road, Gloucester, GL2 6EE. Write, or phone Gloucester 29451, for a copy. Or if you happen to be in London or Gloucester, call in and collect one. The London Heathkit Centre is at 233 Tottenham Court Road. and the Gloucester showroom is next to the factory in Bristol Road.

The catalogue contains details of the very large range of electronic kits, many available for the first time in this country.

It talks in detail about kit building "The Heathkit Way" and shows how easy it is to build a Heathkit. Even a complete novice need have no worries as the instruction manual, with the aid of large pictorials and step-by-step instructions, leads you every step of the way.

Its 64 pages give details of many exciting models for home construction, ranging from a large selection of audio and Hi-Fi equipment through electronic calculators, digital electronic clocks, electronic thermometers, an ultrasonic burglar alarm, to test instruments for the electronic hobbyist and home car servicer. Even a 12 inch black and white portable television kit is available.

Heathkit's Catalogue



New kit models include an f.m. tuner with digital readout and computer tuner, a 4 channel SQ amplifier, a battery powered electronic thermometer and a de-luxe digital electronic clock with alarm. All models are available for cash or on extended credit terms through the very popular Heath Money Budget Plan. A free technical consultation service is in operation both before and after purchase.

You have been warned! Don't forget to order your copy of the December issue of *Practical Wireless* . . . look for your Free PW Miniature Screwdriver.

Start building the PW Kempton with our December issue. This is a quality stereo cassette player for your car; build yourself an inexpensive capacitance bridge that really works, and the third section of our 1974/5 PW Buyers Guide to Radio and Electronic Components will also be included in our December issue.

In the January 1975 issue of PW, we start the New Year with constructional series on radio control. Don't forget to place a permanent order with your newsagent, or write to our subscription department.

Further details of the December issue on page 609.

Hi-Fi Accessories by Bib

B IB HI-FI Accessories Limited announce the publication of a comprehensive 16-page full colour catalogue, which illustrates and describes their very large range of hi-fi accessories which now comprises more than 70 products.

The catalogue has been designed so that it can be easily reprinted in foreign languages and arrangements are already in hand to print it in French, German and Italian.

For the UK market a single sheet retail price list is inserted in the catalogue.

Bib Hi-Fi Accessories Ltd., PO Box 78, Hemel Hempstead, Herts, HP2 7EP.

Wolsey's Colour King at sea

ELECTRONICS 7 OLSEY equipment is now being increasingly used marine installations and the most recent of these, through Aerialwork Limited of Southampton, their agents for Southern England, has been the installation of a communal TV and radio system to the officers and crews quarters on the car ferry "Eagle". In order to receive various transmitters whilst at sea, a Wolsey Broad Band "Colour King" u.h.f. aerial and FM411 array were erected with a rotator motor and remote control unit. The aerials and mast were specially treated to withstand exposed sea conditions. The well-proved Wolsey "Mercury' amplifier was fitted and provision was made for a monochrome video cassette recorder and additional outlet points to public rooms should this be required at some future date.

The 11,500 ton "Eagle" which is controlled by one of the P & O Group of Companies—Southern Ferries—is the largest on/off car ferry to use the port of Southampton and operates a regular service to Lisbon, Algeciras and Tangier.

FM AERIAL pre-amplifier

KEITH CUMMINS

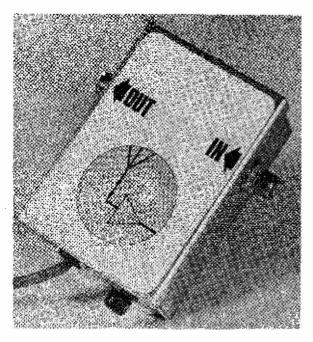
ONG-DISTANCE reception of weak FM signals is possible provided that a high gain aerial is used and that the receiver has high sensitivity. Some older types of receiver lack the sensitivity of their modern counterparts and the use of an aerial amplifier can improve reception considerably.

We have to be careful in the use of such an amplifier however, since high gain is not the only pre-requisite. If the amplifier adds as much noise as it increases the signal, then we are no better off. The amplifier must have a good noise factor, that is, it increases the signal by a much greater amount than it increases the noise.

Another aspect we have to consider is the type of reception we expect, having provided the amplifier. If the incoming signal is very weak indeed than we may be able to improve it, but if it fades away to nothing, no amount of amplification will bring it back again. This situation can exist during fading conditions, when total cancellation of the signal at the aerial occurs because of multipath reception. An amplifier can be useful, however, since it shortens the time during which the signal is unusable. Imagine a threshold level below which the signal must not fall if a satisfactory signal-to-noise ratio is to be maintained; if the amplifier lifts the entire incoming signal, this can fall to a lower level before becoming unsatisfactory.

CROSS MODULATION

The VHF FM band is becoming quite crowded and the weak signals we wish to amplify may be situated very close to a strong local transmission. Unless our amplifier is correctly designed, a strong possibility exists that cross-modulation will occur between the various signals present, due to the high amplitude of the local signals. The signals we wish to receive may then become completely lost in the mess which results. Once this has happened, it is impossible to



separate the signals again, so we must prevent such a thing happening in the first place.

Cross-modulation can not only occur in the amplifier but also in the input stages of the receiver. A valve receiver is far more tolerant of high input levels than its transistor counterpart. Too much amplification before the receiver's RF stage can therefore cause intermodulation and it will be seen that excessive gain can be a real disadvantage. Any aerial amplifier used for FM work should therefore not have so much gain that the local signals will cause cross modulation, have enough gain to substantially improve weak signals, and, itself, have

Fig. 1: The two FETs are connected in a cascode circuit, the first being an amplifier while the second is a buffer or isolating stage.

