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Editorial

We understand that there were good attendances at the Northern Radio Exhibition recently held at Manchester, and that a great deal of interest was shown in the items on display there. Unhappily, the amount of business transacted was somewhat disappointing. This, of course, is only to be expected in view of the trade depression now prevalent in the textile industry, which is concentrated mostly in the area served by the exhibition.

It is under circumstances such as these, when money is “tight,” that the radio constructor scores over the less knowledgable—particularly if he has been wise enough to stock up the “junk box” under favourable conditions. Although there is not nearly so much ex-WW equipment available now as there was a year or so ago, there are still many useful items at reasonable prices for the reader who is prepared to do some searching.

It should not be thought from the above that we advocate the use of surplus components on all and every occasion. We should not, for example, dream of using anything but new, and therefore the most reliable, if more expensive, components when building test equipment—and the same policy applies in many other circumstances. Even so, we must remember that many readers simply cannot afford the higher prices. In that case, obviously half a loaf is better than none.
**Suggested Circuits for the Experimenter**

The circuits presented in this series have been designed by G. A. FRENCH specially for the enthusiast who needs only a circuit and the essential relevant data.

**No. 19—A Phase-Splitting Detector**

In high-fidelity receivers employing push-pull output it is normal practice to use a phase-splitting valve after the detector. An AF amplifying stage may be connected between the detector and the phase-splitter, in which case the phase-splitter usually feeds the output valves directly; or the phase-splitter may be employed immediately after the detector, whereupon several AF amplifying stages in push-pull are usually required to bring the signal to loudspeaker strength.

This month's circuit illustrates an alternative system, by means of which phase-splitting is obtained at the detector itself. Such a system has several advantages, the most important of these being that all the following AF amplification is carried out by push-pull circuits. The circuit is at its most useful when detection occurs at a high RF voltage level. In this case the detected AF has a relatively high voltage, and subsequent AF amplification need consist only of two output valves in push-pull; almost ideal conditions being obtained when these valves are triodes (possibly with negative feedback) giving consequent harmonic cancellation in the speaker transformer.

The provision of a high RF voltage to the detector does not present many problems. Sufficient RF voltage should be obtained on local stations from a frequency-changer and IF stage alone, provided that a good aerial is used and AVC is dispensed with. Two RF stages in a TRF circuit may, if well-designed, possibly give nearly as high a voltage.

**Advantages**

Even when used in a normal AVC-controlled superhet, the circuit still shows its advantages. These are given by the fact that the following AF amplification is in push-pull (as mentioned above), that the necessity for an additional phase-splitting valve is avoided, that the only distortion introduced is that given by a normal diode circuit (this distortion usually appearing only at very low signal levels or on the reception of heavily modulated carriers), and that hum which may be picked up by the cathode of an AF phase-splitter does not occur in this circuit. (Should it be possible for hum to be picked up on the cathode of the diode, the valve should be replaced by a Westector or germanium diode).

The circuit has one disadvantage. This is given by the fact that two volume controls (R5 and R6), are needed, and that these must be fairly accurately ganged. This disadvantage becomes important when the circuit is being put into practical use, as two-gang potentiometers are somewhat difficult to obtain. The problem would probably be met most easily by the use of two identical potentiometers ganged together by a simple mechanical coupling. When the detector is used at a high RF voltage level in the manner mentioned above the potentiometers can be replaced by fixed resistors, volume being controlled in the RF or IF stages.

**Functioning**

The functioning of the circuit is almost self-explanatory. The diode load is made up by the two resistors R3 and R4 in series. By centre-tapping these resistors and arranging the other detection components symmetrically about the centre-tap, phase-splitting is automatically ensured. The tuned circuit feeding the detector should not, of course, be centretapped, and it should be free from earth. If AVC is desired, this may be obtained via R7. The high value shown for this resistor is recommended in order to prevent it upsetting the balance of the circuit. When AVC is not required, R7 and C6 can be omitted.

---

**IN YOUR WORKSHOP**

In which J. R. D. discusses Problems and Points of Interest connected with the Workshop side of our Hobby, based on Letters from Readers and his own experiences.

The enthusiasm of radio amateurs is well known. They have, by reputation, an ability to conjure up the most advanced equipment out of what is, in many cases, a very variegated collection of component parts. And they do this, as well, for a cash expenditure which is often quite small.

Most amateurs make their equipment look pleasing and "professional" as a matter of course. What they build not only works well; it looks well. As they say in Devon: "a proper job!"

However, attention to appearance in finished installations argues the possession of some patience on the part of the builder. Especially is this true when particularly boring and tedious jobs have to be carried out. An example of this occurred recently in the writer's own shack.

Cleating

This shack, in common with many others, has a large number of cables running around the walls. These cables consist of mains leads; power supplies from a main power unit; AF leads for speakers, amplifier, pick-up, etc.; and several others. As these wires have been added to from time to time in the past, their general appearance was more than untidy.

The writer (who has been putting off the job for some time!) finally made up his mind to get them properly cleared away. Lead-covered cable was available for the mains leads, and the AF was carried by screened cables. There would therefore be no objection to running all the wires together side by side. There was one twisted flat lead which could not, of course, be held under metal...
Radio Control of Models

A. C. Gee, G2UK

In the last article in this series, we described a two valve receiver suitable for sequence control. We promised at the end of that article to describe a miniature transmitter for use with the receiver and this installment accordingly deals with the construction of such a unit. That described herewith is the one used by the writer for controlling the receiver previously described.

As can be seen from the circuit diagram, a straightforward push-pull circuit is used, two Mullard DL92 miniature valves being chosen, as these will operate very efficiently with 85 volts HT, which can be conveniently supplied by a Drymax 529 HT battery. The dimensions of this battery are only $6 \times 3\frac{1}{2} \times 2\frac{1}{2}$ inches. Used in conjunction with a Drydex Type H1159 LT battery, the size of which is $4 \times 2\frac{1}{2} \times 2\frac{1}{2}$ inches, these two can be conveniently arranged so that quite a small cabinet can be used as shown in the photographs. This was made for us by Philpots Metal Works Ltd., Chapman St., Loughborough, and measures $6\frac{1}{2} \times 5 \times 5$ inches. The two batteries arranged in the box as shown leave a small space $2\frac{1}{2} \times 3\frac{1}{4}$ into which the transmitter fits. It is built up on a piece of paxolin sheet, which stands on four ‘feet’ 2 inches high. The general position of the components can be seen from the photos. Construction and circuitry are straightforward and need little comment. The tuning coil consists of 12 turns of 22 swg enamelled wire wound on a $\frac{1}{2}$ inch former.

Above: View of completed transmitter.
Below: View of chassis showing tuned circuits.
Simple transmitter for sequence control. See April issue for associated receiver and DL92 base connections.

This coil is split into two sections as shown in the circuit, a space of about 1-inch being left between the two parts. Into this space is wound the aerial coil. Some extra turns may be needed to obtain the tuning of the main tuning coil and the aerial coil just right. In our own unit, three turns proved satisfactory. Too many turns in the main coil create hand capacity effects and poor frequency stability, whilst too few will give a poor energy transfer to the aerial, with consequent unreliable receiver action.

The keying or signal switch is of the push-to-make push-to-break variety and is fitted to the lid of the cabinet. This arrangement helps to eliminate hand capacity effects so often experienced when long leads to the keying switch are used. As the unit is so small, it can be held in the hand or placed conveniently on the ground. The other switch shown on top of the case is the LT on/off switch.

The aerial consists of a 5-ft. length of whip aerial fitted to two stand-off insulators as shown. The lower one of these is connected to one end of the aerial coil, the other end of the coil being earthed to the case. If hand capacity effects are troublesome, the case should be earthed at a fairly stout earth pin, but, as already mentioned, adjustment of the coupling between the aerial and the tuning coil should correct any tendency in this direction. A parallel with each feeder leg coupled to the ends of the aerial coil would very well indeed with this transmitter.

There should be absolutely no trouble at all in getting the transmitter to work. After it is wired and checked, connect up batteries and switch on. Locate the carrier on the receiver (the station receiver) that is. It should show up somewhere around 26 to 28 Mc/s. By means of the variable tuning capacitor, tune it into the 27 Mc/s R/C band and then line up the R/C receiver on to it as has been described before.

The next series on this subject will be contributed by Mr. F. C. Judi, G2BCX, well known as development engineer for "Flight Control." We are very pleased to welcome him to these pages, and we can assure our readers that he will be able to give us the very latest in the field of R/C.

**Book Reviews**


The preparation and publication of a reference book that embraces almost all aspects of radio communication theory and presents such a wide subject in clear and understandable language is, undoubtedly, an ambitious task to which many an author has aspired. In this volume the co-authors have succeeded to a large degree, and are to be commended for their very adequate treatment of basic principles without introducing difficult mathematical formulae. The authors have been careful to apply the vast majority of students who do not like to be tortured with metaphysical hoo-hah.

About one third of the book is taken up by the first nine chapters, in which the reader is gently but firmly educated in those important fundamentals, magnetism, inductance, capacity, properties of A.C. and D.C. circuits, resonance, and kindred subjects. The next three chapters deal with thermionic valves and their application as detectors, amplifiers, and oscillators. From this section of the book the reader can seek and find practically all he needs on such matters, and is given sound knowledge on the interpretation of characteristic curves, audio design, receiver and power supply apparatus, and receiver practice.

There follows some discussion on amplifier-modulated transmitters, transmission lines, aerials and propagation, frequency modulation and detection. The chapter on ultra-high frequency phenomena introduces the reader to the complex problems of the technique, and gives up-to-date information on such things as lighthouse triodes, klystrons and magnetrons, cavity resonators and wave guides.

A chapter on electronic measuring apparatus is devoted to valve-voltmeters, cathode-ray oscilloscopes and Q-meters. A rather short section deals with wave shaping circuits and multivibrators, and a brief chapter on television principles presents a rough idea of the fundamentals of this branch of electronics. The book concludes with a small chapter giving the basic conceptions of radar.

This publication represents good value and can be recommended to those who want to secure a good grounding in essential theory; it forms an admirable introduction to more serious study. It is liberally sprinkled with some 260 problems intended to enable the reader to obtain practice in solving typical design formulae, but as the answers to the questions are not given the student will not be able to check his working. As the book is of American origin, English readers will expect to notice many terms and phrases which at first will be unfamiliar, but these are easily reconciled with the English terms. The type-face and diagrams are particularly clear, and the book is notably free from errors. A useful index, and the sectionalized chapters, are also pleasing features.


The formula used for verifying this book seems to have been the simple process of choosing about a dozen titles of articles that have appeared in the pages of Newnes' monthly journal "Practical Television." One is presented with a general description of how television works from transmitter to receiver, in a manner which is most likely to appeal to readers with very little technical knowledge but who want to learn some of the underlying principles of the technique. They are not taken along a mathematical path.

A fairly clear insight can be obtained of the system of transmission used by the B.B.C., the principles of television engineering, the conversion of the whole into electrical radiations and subsequently reconverted into movnmg images by the television receivers. The receivers are dealt with in some detail, and certain circuits peculiar to them are well described. The pioneer work of the television laboratories, in the specialized fields of stereoscopic and colour television are given note.

The chapter on time bases would have been more complete with the inclusion of some reference to magnetic deflection oscillators and amplifiers; as it is, the chapter concentrates on chrochronoscopes, and readers having familiarity with such circuits will indubitably those given as belonging to the cathode-ray oscilloscope rather than the television set.

D.C. receivers are briefly discussed, and the many types of aerial and their chief characteristics are clearly presented. The chapter on servicing will be of general interest, though it would seem doubtful whether all the person seeking basic knowledge could be the type who might venture to tackle a television receiver fault so early in his career! A few of the many forms of interference, and their causes, are given a few pages; a short chapter on choosing a receiver indicates some of the desirable features to be considered in a television installation.

In Chapters IX and XII, the reader is suddenly confronted with two short constructional articles on a London-Birmingham Converter and a Pattern Generator. They are undoubtedly useful in themselves for those who need them, but these chapters seem rather out of place in a book whose predominating feature is the broad treatment of principles.

Some space is devoted to the recommendations of the Beveridge Report, and the book concludes with a dictionary of television terms which takes up a fifth of the total pages. Although useful as a reference, it nevertheless contains many terms rarely, if ever, encountered in present-day television practice. This last section of the book tends rather to detract instead of adding value to a volume which, having regard for its contents, is priced at a figure that elevates it from the "popular" class to which it seems most fitting.
LARGE SCREEN TV.

THE RADIO CONSTRUCTOR'S 16 inch TELEVISOR

PART FIVE

In this article will be found details of the chassis dimensions and suitable layouts and dispositions for the smaller components.

Readers who have been following this design will at once notice that the valve line-up as seen in the photograph differs from that given in the previous text. Further experiments with the timebases were undertaken, and it was discovered with some satisfaction that for some valve positions alternative types functioned perfectly.

Thus, the 6SN7 replaced the 12AU7, and both the Osram KT61 and the Brimar 6AG6 substituted for the N78 (Note: The N78 was definitely the best for the video stage). For the EHT rectifier the U37 or the R16 were both excellent.
Constructors should therefore determine their final valve line-up before drilling the chassis or before ordering. Those who prefer this arduous task already carried out will find the chassis maker’s name in the list inserted in text.

Returning to the timebase, the screening cans for the line oscillator and the sync separator are necessary. This is because of their proximity to the line output transformer. However, suitable screens are readily obtainable for whatever types of valve are used.

Some “trial and error” experimenting is required with R23. This resistor was found to produce better frame linearity in our model when using a 6.8 kΩ and a 47 kΩ in parallel. The top few lines will be affected and better spacing achieved. A further means of securing control over frame linearity is the addition of a small 500 Ω variable in series with R25.

It was stated earlier that Allen Components Ltd., would be supplying the line output transformer with or without the EHT rectifier valve. Unfortunately, due to packing difficulties this has not been found practicable.

Constructors should observe the high voltage method of soldering in the rectifier, which is attached by its own protruding electrodes.

Short lengths of polystyrene sleeving should be slipped over these, and nicely “blobbed” solder built up to prevent corona discharge.

Your writer has found it a good procedure to paint these joints and sleeving right through to the glass of the valve with polystyrene cement.

C26 was mounted on a small bracket inside the tube installation, close to the front clip, connection to this being made direct from R34. The earth connection for C26 is conveniently available on the seven pin socket at the rear of focus board.

Note: It is not intended that the illustration showing the position of small components under the chassis should be rigidly adhered to, but it will present a fair idea of a reasonable layout. The writer must confess that one resistor and condenser should not have appeared in the photograph; attempts to improve the timebase were continually being made, and the final arrangement has been made known to you. So no bricks, please!

The final chassis arrangement—see cover illustration—comprised three units, timebase, power pack and vision and sound chasses, which were held together by “L” strip. The cabinet, photographed from front and rear, was made to measure for this design, and is a delightful piece of furniture which would grace any home. These cabinets are now available, accurately prepared, to the constructor.

Four holes are provided on the side, and by mounting the four controls on a metal plate, this may simply be screwed on to the interior of the cabinet. These controls are, of course, Focus, Brilliance, Volume and Contrast. Engraved knobs give a finished appearance.

The reader is now in a position to line up and establish a good raster, and it is suggested that the low rail HT voltage be used (see last month’s article). The change-over to higher voltage is effected after establishing linearity and normal scan. Better focusing may be expected, however, when both vision and sound current loads are passing through the focus coil, or by temporarily raising the value of R42 from 500 Ω 3W to 1,000 Ω 3W.
While on the subject of power requirements, your attention is drawn to the Westinghouse mains rectifier type 14A/342. With this, suitable supplies can be economically obtained from the normal 200 to 250V AC mains input. The main consideration is the reservoir condenser.

The accompanying diagram fully illustrates this. A filament transformer for 6.3V at 9-10A, which will also heat the tube, may be purchased at a reasonable price.

The power supply circuit shown is capable of excellent ripple suppression and is perfectly satisfactory for television. In point of fact, the actual residual ripple is approximately 2 to 3 per cent., which may be considered as negligible for practical purposes. The makers of the rectifier, the Westinghouse Brake and Signal Co. Ltd., 82 York Way, King’s Cross, London, N.1, willingly provide any technical information required, and readers resident in areas with peculiar or unusual power supplies would do well to consult them.

Some further considerations are necessary for those who wish to use 9" or 12" tubes for the time being (see last month’s article). One suitable method would be an isolation transformer with tapped primary and a secondary of about 150V. Under these conditions the same rectifier would function well.

Suggested power pack utilizing auto-transformer.
Note: Reservoir condenser should be connected directly after rectifier, and before the fuse—not as shown.

Timebase—Side View.

Still another method, and one with considerable saving in bulk and self-contained heater supply, is the auto-transformer. A suitable circuit is shown, and readers planning to start with a 9" or 12" tube will see at once that there is a 150V tapping—an ideal supply.

One reader has asked if the Brimar RM4 metal rectifier from his “Viewmaster” is satisfactory for this function. The answer is, of course, that it will work perfectly.

Note: Circuits employing auto-transformer or mains metal rectifier should not be externally earthed, and the fusing precautions shown in the diagrams should on no account be omitted. Remember, the chassis is one side of the mains.

Note 2: Allen Components Ltd. have made the necessary centre tap arrangements on the line deflection coils, so that the numbers 1.2/7.3 shown in last month’s circuit will now read 2.7.

Better results have now been achieved by taking the connection marked “C” on the CRT (last month’s issue) to No. 7 on the line output transformer through a 470 kΩ 1W resistor, decoupled with a 0.1 µF condenser, 750V wkg., to chassis. This raises the HT on the CRT second grid to 350V, as against the previous 250V, with a consequent improvement in the operating conditions of the CRT.

Who’s Next?

“Getting out a magazine is fun, but it’s no picnic.

“If we print jokes, people say we are silly. If we don’t they say we are too serious.

“If we clip things from other magazines, we are too lazy to write them ourselves. If we don’t we are too fond of our own stuff.

“If we don’t print contributions, we don’t appreciate true genius. If we do print them, the page is filled with junk.

“Now, like as not, someone will say we swiped this from some other magazine. We didn’t!”

(From the “Model Engineer” who, in turn, extracted it from “The N.Z. Model Railway Journal.”)
THAT PROFESSIONAL FINISH

by A. W. WOOD, B.Sc.

Many otherwise excellent pieces of home-built gear are immediately stamped as an amateur product by the lack of a suitable finish to the bare metal. The purpose of this article is to show how a really beautiful finish can be given to any equipment, to list the necessary brushes and paint, and to enable pitfalls to be avoided. All the tips given here were obtained by experience in finishing a grid dip oscillator and a 19" power pack panel. These are both finished in a glossy grey cellulose paint. This is the type of paint used for spraying on cars, but this particular brand, Brushing Belco, is suitable for brushing on to the surface, so eliminating the necessity for spraying equipment.

The procedure is to thoroughly clean the metal, apply a primer coat, then an undercoat followed by several coats of the glossy finish. The job is then smoothed and polished. The final result is well worth all the trouble involved.

Cleaning The Metal

The directions on the tin state “Clean with turpentine substitute, etc.” This is not enough. The surface must be cleaned until it is bright by means of emery cloth, or glasspaper, so that all grease and any oxide film is removed. Then clean with turpentine or the recommended alternatives, and wipe dry with a clean rag. Now apply the primer.

The Primer

A ¼ pint tin will suffice for several pieces of equipment, and a ½ or 1 pint will be sufficiently large. If the metal surface is flat, lay it in a horizontal plane, supported by small blocks of wood over some sheets of newspaper. The purpose of this is to ensure that the paint, which will run through any holes to a certain extent, will not stick the newspaper to the back of the panel. It is, of course, necessary that all holes and cutouts be mad before any finishing process is started. Also, the term “panel” covers whatever piece of equipment is being celluloised.

Application of the primer is not a tricky business, and the only point to be watched is that it is not laid on too thickly. If necessary, it can be thinned by turpentine substitute.

Lease the panel to dry in a warm, dry atmosphere for at least 16 hours. Clean the brush with turpentine substitute and stand in a jar of water so that the bristles are kept partly immersed.

When the panel has dried, emery paper the surface to smooth out any humps. If the paint was too thick, the humps may cause too much unevenness to be removed without wearing through to the bare metal. If this should happen, apply more primer to these places or, if required, over the whole of the surface.

The Undercoat

Next, the undercoat is applied and, again, a ¼ pint will be enough. The same brush which was used for the primer can be employed again. After use it should be cleaned as before and put into water. There is nothing tricky about the undercoat, either, as both the primer and undercoat are turps based paints. Once again, at least 16 hours should elapse before smoothing with emery cloth.

Finishing Coats

The brush for the glossy finish should be of good quality and have soft bristles. The size will depend upon the subject—for a large panel, a 2" brush will be necessary, but for a smaller article a small, bushy brush is best.

A ¼ pint tin of Light Grey Cellulose is the most suitable size. The paint should be applied with a full brush, using strokes in one direction only, parallel to the shorter edge of the panel.

Do not brush over a part which you have just painted. If there are any “runs” or brush marks, leave them alone; they will smooth out. The reasons for the provisions above are these:

(a) The cellulose dries quickly, so that strips must be applied before the previous strip dries and leaves a noticeable edge.

(b) The action of cellulose upon a previous coat is a very rapid volatilising one. With ordinary paints, the second coat serves to strengthen the first one, but with cellulose, no matter how long the first coat has been on, unless the next coat is applied quickly, and without over-brushing, it will dissolve some of the previous coat. This is a reason why it is essential that many small impurities are visible when the paint dries.

Put on several coats of this glossy finish, smoothing each coat after drying before applying the next. Do not attempt to obtain an absolutely flawless finish by the application of the cellulose alone, because you will not succeed.

The next step is to obtain some “water” paper, or silicon of carbide paper as it is properly termed. This can be purchased from paint dealers or ironmongers for 5d. per sheet, and consists of silicon carbide particles on a waterproof backing. The degree of fineness is indicated by the number on the back of the sheet, the higher numbers indicating finer grades. The two used by the writer were Nos. 280 and 400.

Cut a strip from the coarser sheet to go around a normal sandpaper block, and have a shallow dish of water at hand. Dip the block in the water, and rub evenly over the whole surface of the panel. Use plenty of water. Repeat with the finer paper.

TRADE REVIEW

BURGOYNE TAPE TABLE

(Mail Order Supply Co., The Radio Centre, 33 Tottenham Court Road, London, W.1.)

The Burgoyne Tape Table is a precision model, retailing at £16, 10. 0. It is also available on hire-purchase terms of £6, 10. 0 deposit and 12 monthly payments of £1.

The table employs three motors of a type having negligible stray magnetic fields. The capstan is directly connected to a heavy balanced flywheel, which is driven by a motor through a flexible system allowing the flywheel inertia to maintain a constant tape speed. Fast forward and rewind facilities are available, at a speed of less than a minute for a full spool, of 1,200,000 spools of tape. Pressure pads are used to lock the constant intimate contact between tape and heads, and the latter are set in a single unit to ensure perfect alignment.

Main control is by a pinch roller fitted with a small knob. As this roller is withdrawn, the pressure pads are automatically released, brakes are applied to the tape spools, and the motors are switched off. For fast forward or rewind, the tape is lifted clear of the heads and repositioned and the selector switch set to the desired position. Closing up the pinch roller starts the mechanism.

The tape speed is 7½ per second, and, since the heads fitted are half-track, a running time of one hour is possible with a 1,200-ft reel of tape. The heads are of the high impedance type and are suitable for capacity feed from the tape modulator and direct feed into the playback pre-amplifier. A frequency response of up to 9 kHz is possible with tapes such as Scotch Boy, etc., and a suitable amplifier.

The table measures 16½" x 11½". The maximum projection measurements are 1½" above, and 4" below the table. The finish is hammered stoved brown enamel.
RADIO MISCELLANY

CENTRE TAP talks about

CLUB MAGS – JUNK HUNT – PRICES

Since my recent notes and suggestions regarding Club Magazines and News Sheets, I have been reading copies of those received with much interest. A number, too, have come to light, and a large number of copies which specimen copies have been received. The biggest, both in the number of pages and circulation, is “Monitor,” the organ of the very lively ISWL, but there are also many creditable efforts by local clubs with memberships around the fifty mark. Even these are not only self-supporting, but make a small profit to contribute to the general funds of the group. Sixpence per copy is the usual price.

Generally speaking, the reproduction is good. It’s the way round, but occasional lapses in spelling appear—i.e., articical, volunter etc. The most general weakness is absence of bold headings and the rareness of illustrations. Where are the amateur cartoonists? Pages of typecript look dull unless the matter is attractively displayed, and mere typewritten captions alone need thoughtful planning to enliven a page. Special announcements, etc., are better boxed (set out in a lined border). One magazine failed to do this in an obituary notice, where an extra bold black border should be used. More attention could well be given to the reporting of current club events and local affairs.

Despite these minor points, the general production standard is extremely good, but without exception the amateur editors make urgent appeals for more material from their fellow members, who universally seem reluctant to put pen to paper. I am sure that with mutual co-operation this aspect could be materially improved. For I am putting forward a tentative plan in the hope that it will ease the lots of the harassed editors.

A Central Bureau

Briefly, the idea resolves itself around a central pool of News Sheets, with each editor submitting a small batch of copies of his magazine for distribution from other amateur editors. In return he will receive his quota of copies of other clubs’ efforts, and from these he will be entitled to reproduce any article, or digest of it, which he feels may be of interest to his club members. Permission to reproduce would not have to be specifically sought, as membership of the Bureau would be taken as tacit consent although, naturally, acknowledgment to the source and to the writer would be made.

Incidentally, I discovered that an Amateur Magazine Association once did exist, and it struck me that such an organisation could well serve as the central pool for such a scheme. However, a letter to the last known officer of that association has failed to produce a reply, so it seems there is no other alternative, if the plan finds general favour, than to get the scheme started independently. Perhaps a volunteer organiser will come forward until such time as an elected manager can be appointed.

The pool would be run on the lines of a QSL Bureau, a number of stamped self-addressed wrappers being sent in lieu of the usual envelopes.

It seems probable that a scheme on these lines would provide the stimulus to make many club magazines brighter and even more readable, and may encourage contributors who at present feel that the effort of making a contribution is scarcely worth while when the result is seen by so limited a number of readers.

With sufficient support it may be possible to get someone to donate an annual award for the best magazine standard maintained throughout a given period, points being allocated for reproduction, layout and material interest. The size of the club and the best use of the contents/paper-size ratio would be taken into consideration. An award to the writer of the article, irrespective of its length, which is reproduced in the greatest number of different magazines might also be arranged. Amateur writers and others who have no local club magazine might be induced to send contributions to the central bureau, where they would be available for the use of all affiliated amateur editors.

Amateur editors and others who are interested are invited to send their views and suggestions as soon as possible, even if it is merely a postcard promising support.

Junk Hunt

I recently had a radio-minded friend from Scotland staying with me for a few days, and he was, of course, intent on spending the Saturday on touring the Surplus Shops to look over the diminishing number of bargains. Most provincial readers know the London radio shops pretty well, and make a point of visiting them whenever they come to town—and from further afield than the provinces, for that matter. I remember one continental amateur who had to go to the north of England on behalf of his firm, to see a demonstration of some new mining equipment. On his way back he had a few hours to spare, which he decided to spend in London. It was his first visit, and he was met at King’s Cross by an English friend who mentally planned a lightning tour of the usual sights, Parliament, The Abbey, St. Paul’s, etc., leaving the visitor to choose which to include and which to cut out. Upon his arrival, he duly asked the continental amateur which of the many places of interest he most wished to see, and he was amazed to receive the reply, “The Junk shops.”

It took the friend (who knew nothing of radio) some minutes to guess what he meant and, even when at last it dawned on him, he hadn’t the faintest idea where to look for them. Fortunately, a taxi-driver knew better and took them to Lisle Street, where our English friend waited patiently while the visitor browsed over battered ex-WD gear. No doubt he is still marvelling at the strange ways of foreigners!

Lisle Street was the first point of call for my Scottish visitor and I. We poked around for a long time, but bought nothing. Lisle Street must be losing its grip, for when we moved on to the Edgware Road area we both indulged in an orgy of junk buying. I only wanted a few bits and pieces, myself, and to equalise the load I found myself carrying nearly half of his. He bought an enormous half-striped chassis for a few shillings, just for the sake of the meter, and as he was already fully loaded I had no choice but to offer to help carry it. If I had taken a screwdriver and pliers I might have whipped off a few of the components and shed them on the wayside. In fact, as the time I fervently wished I had. Ex-WD chassis are invariably awkward shapes, and this particular one would have left Euclid simply dizzy.

It was nearing dusk when we got back, hot and dirty, and looking like a couple of itinerant tinkers carrying our stock-in-trade. We were both too ashamed to be seen in our select suburban district in such a state, loaded up as we were like beachcombers after a shipwreck. We hung around taking in a little refreshment, to sneak in after it was dark.
Even then, a horrible clanking of ironmongery heralded our return, which in the quiet of the evening seemed worse than ever.

**Prices**

Among the bits and pieces were some lengths of dural tubing, acquired with the object of making a dummy aerial and boom, as I have been lured back into making amateur talkies. You can imagine the difficulty we had in manoeuvring it through the Saturday shopping crowds. At one time I had a pram hooked on the back end and, in a desperate effort to disengage the front end, I provoked some portly character in the corporation. Perhaps it was his injured feelings or punctured dignity that stimulated his eloquence in telling what we were and what we looked like. No doubt, too, it was his description ringing in our ears that caused us to delay our homecoming until after dark. Happily the dural was undamaged. Nowadays it costs £131/2 a foot! Back in 1946 it was so plentiful that I built a ten metre Plumbers' Delight and had a whole lot left over from five bobs' worth. I suppose the demand for TV aerials has long since swallowed up the surplus. Anyway, the mike boom is a great success and all we want now is a crane. So far I haven't found any one to run the market.

**Whistle While You Work**

Thinking of minds reminds me of just how much whistling into them one hears on the amateur bands. It's a tradition that seems to go back all over the world would seem to use no other form of modulation check than a meter in the mod. output stage. Then if the needle kicks up to show double the plate current as they whistle, the modulation percentage is assumed to be about right.

I use a 'scope myself, and consequently feel most virtuous about it!

It reminds me of an incident which occurred back in about 1930, when the B.B.C. arranged a series of programmes for the early days of amateur talkie. One man taking part in the series felt at the last moment that his carefully rehearsed script needed brightening up. Undoubtedly, he decided to embellish it with a few sound effects. No doubt when he tried it out before his family they warmly approved the additions.

One of the impromptu effects was a whistle, intended to give atmosphere when he came to the part of the programme where the lights went off. Before anyone could stop him, he whipped a whistle out of his breast pocket and let out a long shrill blast right into the microphone.

You can well imagine the effect the sudden surge of current produced in the transmitter. As far as I could discover no one bothered to enquire just what other effects he had up his sleeve. That one put the Daventry transmitter off the air for nearly an hour while the Engineers fitted replacements, and it cost the B.B.C.. over £200. Anyway, it was good work by the Engineers to clear up the shattered transmitter stages so quickly.

I have always heard of the Engineering side, despite my impatience with their top heavy administrative and programme staffs. Readers may well recall the occasion a few months before the War when the Droylsdiet litter was struck by lightning and burnt up. The Daventry aerial, which had then been standing idle for about five years, was quickly pressed into service and radiation continued. The Engineers worked on the Droylsdiet aerial all night with the aid of searchlights, and I believe it was back into service the next day. When your own aerial comes adrift on a dark and dirty night, it will make it just a little easier if you remember the Droylsdiet one has a height of 700 feet.

** Gale Warning**

In a small fishing village where I spend an occasional weekend, there lives an old boy who has a remarkable local reputation for the accuracy of his weather forecasts. In fact, it is said the local farmers consult him regularly around seething and harvest, and visitors planning an outing get great store by his prognostications.

To soothe the fears of a rather nervous XYL before hiring a boat we sought his reassurance as to whether there was a circuit with which storms in the vicinity would not be continued. You can imagine our consternation when he replied “Can’t rightly say. My wireless set’s broke down.”

**The Editor invites**

articles from readers, of a nature suitable for inclusion in this magazine. Articles submitted for publication should preferably be typewritten, but ordinary writing is acceptable if clearly legible. In any case, double spacing should be used, to allow room for any necessary corrections. Drawings need not be elaborately finished, as they will really be redrawn by our draughtsmen, but details should be clear. Photographs should preferably be large (half-plate) but in any case good. Much useful advice to prospective writers is given in our “Hints for Article Writers,” which will be sent free on request.

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**QUERY CORNER**

A “Radio Constructor” Service for Readers

**Dummy Aerial**

In various articles on the design of signal generators, I have noticed that mention is made of a dummy aerial. What is this device used for, and can one be easily constructed?

E. Unwin, Brighton.

When aligning a radio receiver with the aid of a signal generator, it is most important that the receiver is operated under similar conditions to those which exist when it is working normally with an aerial connected. If this condition is not satisfied, it is possible for the alignment and also the sensitivity measurements to appear quite satisfactory on the test bench, but as soon as the normal receiver is operated under normal conditions the results are very different. The reason for this should be apparent if we consider the case of a standard broadcast receiver being aligned with the aid of a signal generator which has a low impedance output. When the generator is connected to the aerial socket of the receiver, its output impedance will be high in comparison to the coupling coil on the first tuned circuit within the set. The most obvious effect of this will be that the tuning of the aerial transformer will be very flat, and it will be impossible to determine the optimum setting of the trimmer. On the other hand, it is impracticable to arrange the output of the generator to be very high because of the difficulty of keeping a check on the output voltage, which would, of course, vary according to the output impedance. Such variations would render the taking of sensitivity measurements an impossible task without the aid of additional equipment.

Thus it is that the arrangement which is generally employed involves the use of a generator having a low impedance output in conjunction with a dummy aerial. This latter is a device which has a loading effect on the receiver which is similar to that of the normal aerial. Also, because the dummy aerial is connected in the lead between the signal generator and the receiver it prevents the generator from loading the circuit with which the receiver and thus introducing the difficulties which have already been discussed. The dummy aerial which is suitable for use on the medium and long wave ranges consists simply of a 200 pF capacitor, a 25μH inductor and a 25 ohm resistor, all connected in series and included in the live side of the generator output lead. Those who do not wish to wind their own coil will be interested to know that the Wearite PO9 coil may be successfully used for the purpose. The dummy aerial is conveniently constructed in a small metal box with flying input and output leads, so that it may be easily connected between the generator and the receiver. Most short wave receivers are designed to have a low impedance input so that a dummy aerial is not necessary, the generator feeding directly into the set.

**Beam Blanking**

About a year ago I completed an oscilloscope using a transistor oscillator as the time base. I have found the instrument extremely useful and satisfactory but for one factor, when the time base is operating on the higher frequency ranges the flyback line on the screen becomes particularly noticeable. This effect can be rather distracting when looking for certain kinds

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**QUERY CORNER**

**Rules**

(1) A nominal fee of 2/6 will be made for each query.

(2) Queries on any subject relating to technical radio or electrical matters will be accepted, though it will not be possible to provide complete circuit diagrams for the more complex receivers, transmitters and the like.

(3) Complete circuits of equipment may be submitted to us before construction is commenced. We will not accept queries where the component values are correct and that the circuit is theoretically sound.

(4) All queries will receive critical scrutiny and replies will be as comprehensive as possible.

(5) Correspondence to be addressed to “Query Corner,” Radio Constructor, 57 Maida Vale, Paddington, W1.

(6) A selection of those queries will be sent to the general interest will be reproduced in these pages each month.
of phenomena. Can you recommend a simple circuit which will enable me to blank out this flyback line?

D. Underwood, Putney.

When designing a time base to operate over a wide range of frequencies it is difficult to maintain a fast flyback time when working on the upper ranges. This effect is particularly marked when a transitron type of oscillator is employed in the time base, and although this type of oscillator is highly satisfactory for use in home built oscilloscopes it does suffer this defect. When working above about 10 kc/s the flyback is often sufficiently long to take several cycles of the signal under examination with the result that the flyback stroke has a tendency to partially obscure the forward or working stroke. This defect can be easily overcome in most oscilloscopes by arranging that the C.R. tube scanning beam is cut off during the flyback period. It is fortunate that the waveform found at the screen grid of a transitron has a negative going flyback pulse which can be applied to the grid of the tube to extinguish the beam during the flyback period. However, as the voltage at the screen does not remain constant during the working stroke, it must undergo some treatment to prevent it altering the trace intensity. This treatment is obtained by means of a simple diode circuit such as is shown in Figure 1. The anode potential of the diode is adjusted by means of the pre-set control R1 so that it does not conduct during the working stroke, but passes the negative going pulse which occurs during the flyback period to the grid of the tube.

Examination of the circuit will show that as this negative pulse is applied to the cathode of the diode it will conduct only during the duration of the pulse. The time constant of the R.C. combination in the tube grid is fairly critical as it affects the speed at which the beam is cut off and again re-instanted at the two ends of the Working stroke. Thus in order that the best results should be obtained over the complete working frequency range of the time base it is necessary that the time constant should have two values which can be selected by means of a switch. This switch is shown as s.l. on the circuit diagram. It may be considered useful whilst incorporating an additional switch on the front panel of the oscilloscope to employ a 4-way single-pole component so that provision can be made to modulate the tube beam from some external source. Such a refinement is advantageous when making certain frequency comparisons with the aid of the oscilloscope, or for inserting marker blips on the trace.

The optimum voltage at the slider of the potentiometer R1 will be determined by the voltage on the screen of the oscillator valve. This potentiometer should be set so that the intensity of the trace during the working stroke remains unchanged, but the flyback is completely blanked out. It will be found to be a simple matter to apply this type of beam blanking arrangement to an oscilloscope which employs a transitron time base oscillator. It is, however, equally suitable for use with other types of oscillator when a negative pulse is available during the flyback back pulse, but minor modifications may be necessary to the circuit constants.
Special Personal Set Offer.

Frame Aerial Covers
Resistors Miscellaneous
Condensers Miscellaneous. To avoid confusion, Type 10 4/4.
B.T.G. Amphenol Valve Holders.
Assembly Instructions.
Battery Stud Connectors pair per kit.
Crystal Microphone.
Output Matching Transformers.

Personal Set for £1. 10s. 0d.

Complete in cabinet as illustrated, this is a 3 Acorn Valve, T.R.F. Circuit which gives quite good results using a short throw-out aerial. Total cost of everything except batteries is 70/-, but it is probable you have some of the parts, so in the first place send 17.3 for cabinet which includes instructions free, or 1/6 for instructions only.

Note this cabinet is one of the following internal dimensions: 64" high x 54" wide x 3" deep, which makes it suitable for the P.W.M. Minifour and other personal sets.

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Beautifully made wooden cabinet complete with punched metal chassis, glass dial, metal supports and clips. 3 knobs and wooden back.

Why not build a few receivers during the summer months and we can supply all the parts for either superhet or T.R.F.?

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The Teletracer.

With the Teletracer signals can be followed through the T.V. to the tube or Loudspeaker. Similarly, powerful indicators can be obtained in and around the sync separator and clip base sections. The Teletracer uses 5 valves and speaker and operates entirely from A.C. and D.C. mains. Send for a free copy of the instruction manual or better still ring time by sending 66/10, plus 7/6 post and insurance for the complete outfit.

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A famous set by a famous manufacturer. Undoubtedly a serious listener's receiver. Among many special features are a P.F. stage and tuning indicator. Tunes up to 11 metre band. We have a few left, less valves and power packs, otherwise in good condition they definitely have never been used. While stocks last; and for this month only you can have one at £6. 19. 6d. plus carriage and packing 15/-, H.P. Terms £2. 6. 6. deposit and nine monthly payments of 12/.

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Except for heavy and delicate items where carriage charge is specified, orders over £2 are post free, under £2 and reasonable amount bearing in mind a 15 lb. parcel costs 2/—. Postable items can be sent C.O.D. additional charge apart. 1/6 ld.

Early closing, Wednesday—Ruislip, Saturday—City.

Precision Equipment.

Windmill Hill, Ruislip Manor, Middlesex, and at
152-153, Fleet Street, London, E.C.4
The following is a brief description of a multi-range AC/DC voltmeter, the construction of which was based on an ex-WD 0–1 mA meter.

The two diagrams will be largely self-explanatory, but a few notes may be of interest.

First, regarding the movement itself, this should have a finely divided scale. That used by the writer had five main divisions, each of these being sub-divided into ten.

The resistors should be of guaranteed accuracy to within a small percentage of the rated value: ± 1 per cent, is ideal and not too expensive. They should also err on the large size as regards wattage rating, in the interests of long term stability. 1W rating is ample.

The switch used was a Dewar type, simply because this was available, but any suitable DPDT switch could be employed. The biased type of switch, where the lever is normally "off" unless pressed over, is a particularly good one to use as one gets into the habit of checking the meter range and connections before taking a reading.

A rotary stud switch could be used for the different voltage ranges, but it was considered that the insertion of the wander plug into the appropriate socket was less conductive to error, thus safeguarding the meter. Incidentally, it is much cheaper.

Great care is necessary when soldering the rectifier connections, as the efficiency of this component will be seriously impaired if it is at all overheated.

Care should also be exercised regarding insulation, as voltages up to 500 may be applied across the input terminals.

If the work is carefully carried out, an accurate and extremely useful instrument will be obtained for a very low cost.

A MULTI-RANGE AC/DC VOLT-METER

by

S. D. DEAN

Circuit of the Multi-Range AC/DC Voltmeter, with values.

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Mainly for the Beginner . . .

HUM

By H. E. SMITH, G6UH

Hum

Apart from insufficient filtering in the power supply, hum may be introduced into the receiver through various other causes. Some of these may be quite well known, even to the beginner, but we will deal with the more common causes and cures. Nothing is more annoying than a hum which cannot be traced, and it is often the more simple causes which prove most difficult to cure. Let us look at some of these more simple ones:

(a) Inductive coupling from the mains transformer or iron cored choke to a neighbouring iron cored transformer or even an RF choke or tuning coil.

(b) The presence of a magnetic field near to a valve.

(c) Induction from the heater wiring to leads carrying RF or leads in any high impedance circuit (i.e., Grid and anode leads).

(d) Long unscreened grid leads in the audio circuits.

(e) Poor heater to cathode insulation in a valve.

(f) Modulation Hum. This is the hum that is only present when the receiver is tuned to a carrier, and may be due to a variety of causes. Some of these are insufficient filtering, poor earthing of the receiver, badly bonded lead-covered cable or conduit carrying the mains supply in the house, no electrostatic screen between primary and secondary of mains transformer, poor filtering of the oscillator anode HT supply. Quite a formidable list, but if attention is paid to certain points during construction, most of these causes may be ruled out. Perhaps the power supply will be a good point to start at, as in many cases this has been found to have been the root of the trouble.

A normal power supply of the type used for the average receiver and capable of delivering between 250 and 300 volts at approximately 100 mA will, if fitted with a 15 Henry choke and two 8 µF electrolytics, produce a ripple voltage of approximately 0.1 RMS. Such a circuit is shown in Fig. 1. This will not be good enough for serious Short Wave work, especially if headphones are to be used, as the hum will be quite noticeable. The ripple voltage may be reduced to something approaching 0.05 V RMS by increasing C2 to 16 µF. The hum will now be barely perceptible, but if a TRF receiver is to be used a threshold hum will be in evidence as the set goes into oscillation.

A far better arrangement is shown in Fig. 2. As will be seen, two 15 Henry chokes are used in conjunction with three 8 µF electrolytics. The ripple voltage drops to some-thing like 0.02 RMS, and there is little chance of any hum being due to a badly filtered power supply. The two 0.1 µF capacitors shown wired across the primary of the mains transformer in Fig. 2 are to prevent modulation hum.

Chassis Wiring

It is most important that the heater leads should always be twisted together, and wherever possible taken along the bend of the chassis and tucked well into the corner, well clear of any other leads carrying RF or grid or anode feeds. Do not rely on a single connection for the earthed heater, earth it at the start and finish of the run.

Take all decoupling capacitors and cathode resistors direct to chassis and never to the earthed heater tag of the valveholder. Where any grid lead exceeds an inch or two, always use a length of screened lead with the screening earthed to the chassis by the shortest route. In the case of grid leads carrying RF, the fitting of a length of screened lead may cause unwanted capacity, and it is always better to completely screen the RF compartment from the rest of the chassis. The volume control is often an unsuspected cause of hum pick-up. Hum is often induced directly on to the carbon track from a nearby transformer. Choose a volume control with a metal back, and solder an earth wire directly to it and earth it to the chassis.

Component Layout

The arrangement of the components on the chassis plays an important part in avoiding hum. When push-pull output stages are to be used, the driver transformer should be carefully positioned relative to the mains transformer, otherwise there will be a risk of severe hum being induced. It is a good plan to use slotted fixings for such transformers, and if any hum troubles are experienced the transformer may be partly rotated to cancel out the field. (Fig. 3).

Arrange that the RF and mixer valves are situated at the opposite end of the chassis to the mains transformer, and never use unscreened coils in any circumstance.
Cures for Modulation Hum

As explained earlier in these notes, modulation hum is easily recognizable as it only occurs when the receiver is tuned to a carrier. This can usually be cured by one or a combination of several of the following methods. The fitting of two 0.1 μF capacitors in series across the primary, with the centre point earthed (these should be rated for at least 750 volts DC working). In some cases, two 0.002 μF capacitors (1000 volts DC working) may be fitted across the secondary with the centre earthed as above.

A good mains filter fitted in series with the mains lead to the receiver will usually take care of any hum due to poor earthing of the conduit or lead covering of the house mains. Cathode/Heater leakage in the mixer valve can only be cured by replacing the valve. Finally, if all else has failed, improve the filtering to the oscillator stage by adding a separate choke and capacitor, at the same time checking that the RF stage is not overloading due to failure of the AVC.

Microphony and “Motor boatling”

The vibrations from the loudspeaker will sometimes set up a noise not unlike a hum. This can usually be quickly identified by tuning the receiver off the station and lightly tapping each of the valves in turn. The gang may also be a source of trouble in this direction. Some commercial receivers have the tuning capacitor assembly mounted on rubber bushes in order to avoid this trouble.

In the case of a valve being found to be causing the trouble, the only real cure is to replace the valve. Shielding with sponge rubber or other material is a makeshift cure, and the loose electrodes which are causing the vibration will remain loose. “Suspect” valves should always be discarded, as they have a habit of misbehaving at the wrong moment.

Motorboating, or audio frequency instability, often takes on the form of a low pitched hum, and is sometimes difficult to distinguish from the hum due to poor filtering.

Adequate decoupling is the answer to this one, especially in the anode circuit of the detector or double diode triode. To avoid trouble, it is always wise to fit an electrolytic capacitor of at least 4 μF as the anode decoupler, and use good quality capacitors for all other decoupling purposes.

How simple awkward jobs can be, if only the right tool for the task is at hand.

Your writer, for instance, has collected them from practically every other occupation. The one to be described here was used by him when engaged on aircraft metal repairs. Such gadgets are often particularly useful at the present time, when the constructor is continually changing, modifying and re-designing ex-WD gear.

One of the “fiddling” things often found necessary is the fitting of a new front panel, which involves the location of fixing holes to match up with those already present in the existing chassis. The tool shown in the sketch is so simple, and does the job so easily, that the writer is astonished that such a thing is not available commercially. The reader will doubtless visualise it in other forms suitable for other applications.

A word of advice regarding construction. This jig will be at its best when made of good materials. The hinge should be stoutly built, and there should be no end-play in particular. Brass could be used, but steel would be better. The top locating bush may be permanently fixed, as it takes only one size of drill which is used to make a pilot hole which is afterwards enlarged to the size required. This bush should preferably be of hardened steel. Next best is mild steel, case-hardened. The bottom bushes are interchangeable. All have the same size centre hole as is used for the top bush, but the spigots are of various diameters to suit the size holes which may be encountered on different jobs. It is, of course, essential that the upper and lower bushes be concentric, and the holes through them be in line.

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"FOUR PLUS ONE"
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PART FOUR

Power with Economy
It is not only your writer who holds the opinion that one cannot even begin to talk about quality in a receiver, unless that receiver incorporates a push-pull output stage.

Figures talk, and whilst a single pentode invariably has a total distortion figure of between 8 per cent. and 12 per cent., two such in push-pull result in only a fraction of this—just 1 per cent. or 2 per cent.

Usually, however, push-pull output is a luxury beyond the price-range of the average receiver. It necessitates the use of more valves and a higher-rated power-pack equipment, as well as greater care in design, and on these accounts, probably, has not been favoured in the commercial field.

Your writer, however, maintains that with careful and correct design, none of these obstacles need exist—that a really first class, sensitive and powerful superheterodyne can be built that will dissipate not more than the usual 80mA of a four-plus-one, yet without an expensive power pack, and giving a full seven watts of undistorted output from the same number of valves.

Such a receiver is shown diagrammatically in Fig. 1.

The Circuit
V1 is a triode-heptode, the heptode section of which functions as combined oscillator (g3-g4, and g1) and mixer.

The IF output is demodulated by a Westector (which also provides AGC) and is then taken to the triode section of the valve, which functions as audio amplifier.

Reaction is taken from the triode anode to a supplementary winding on the IFT.

The reaction largely replaces the IF amplifier (omitted for economy's sake) and may be used to boost weak signals, as a panel control, using a reaction capacitor. Alternatively, and this is the method shown, the reaction may be preset to a convenient level by the preset capacitor C13; if the most is to be made of the receiver quality, however, the former method is preferable, since reaction will not be needed on home transmissions.

The output from V1 is taken to one grid of V2, a double-triode acting as phase splitter. To ensure a well-balanced signal, R18 and R19 should be high-stability resistors, having tolerances ± 2 per cent. of the values.

Two EL32's form the output stage. With the value of R21 given, the valves work in class AB1, i.e., are slightly over-biased, and are capable of giving seven watts output for an average total current (anodes plus screens) of 68mA (minimum 53mA, maximum 73mA).

Negative feedback is taken from the output transformer secondary—make sure the correct side is used—to the cathode of the phase-splitter input triode.

Volume control, not entirely futilie with NFB, is applied at the double-triode input grid, since it is here that overloading is likely to occur.

Applications
Although it would be eminently suitable as a powerful (and delightful) household...
running off vibrator supplies, as a car radio unit. Used as such, the NFB would probably be its most useful function, i.e., the cancelling out of power pack noises, whilst the addition of a shunt resistor as shown in Fig. 4 would render the valves suitable for use in a 12 volt circuit, as well as in a six-volt one.

---

**"Not so Dusty" Vision**

By "TECHNICIAN."

With their noses glued to the "works," how often, alas, are our admirable scientists unable to "see the wood for the trees"!

Take the average television receiver. The amount of brain-wracking that's been done to produce that superb picture transposed into pure energy, would pull a train from Lands End to John O'Groats.

Yet, but twelve months from buying his television, the viewer, too, can't see the "wood"—for the dust in between.

Dust, that invertebrate enemy that provides the world's housewives with the bedrock of their occupation, settles everywhere, and the face of the cathode-ray tube is not an exception. Every day, an insidious layer of the stuff attaches itself to the inside of the protecting glass and to the face of the tube. In three or four months, the three-megacycle bars on Test-card "C" become a thing of the past altogether, and are rapidly followed into dusty oblivion by the two-megacycle bars, the highlights, and all the details that make up enjoyable viewing.

The external face of the glass is easily cleaned, but without the help of a service engineer it's quite impossible, in the majority of receivers, to get at the inside and the tube-face.

---

**SAMSONS SURPLUS STORES**

**USEFUL TUNING UNIT**

*use page 456*

A solidly built variable tapped inductor wound with silver-placed heavy gauge wire. Fitted with vernier dial. 17s. 6d.

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---

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3/16" Dia. Bist Standard Model 22/6

Sole Manufacturers ADCOLA PRODUCTS LTD. Sales Offices and Works: Cranmer Court, Clapham High St., London. S.W.4. (022)
EASILY CALIBRATED SLOW MOTION DRIVE

By NORMAN F. WEBB.

Many radio constructors who have bought one of the TU9B series of tuning units for the cabinet, or the generous metal screening, or the velvet vernier knobs, may have wondered what they can do with the worm-driven slow motion drive, operated by thumbing the rim of a knob marked 0–100. It is such a solid precision-engineered job it seems a pity to leave it lying in the junk box. I have converted this mechanism into a first rate drive assembly, free from back-lash and readily adapted for use where a dial that can be easily calibrated by the constructor is required.

Here’s how it is done:
First, get the drive out of the TU9B. This is easier said than done, but if you paint the grub screws of the flexible coupler (on the condenser side, of course) with amyl acetate (which you can get from the chemists) and go to work with an allen key, it can be done.

The screws that hold the drive to the panel are easily loosened. Save the screws, you’ll need them.

You can use the TU9B panel as a template to mark out the position of the holes needed to mount the assembly on a new panel. Note that the knob is mounted horizontally, not vertically, as on the TU9B. Drill the holes and, with a fretsaw, cut out the space for the knob.

Now we need a holder for a pointer. This is made from a piece of brass (an old condenser plate) or other solderable metal cut to the shape shown in the sketch. The 0–25 graduated metal disk can be used as a template for the three holes needed, one to take the screw, the other two to fix over the little pegs that hold it rigid. Note that the holes have to be drilled in line with the collar of the pointer holder.

The pointer can be a piece of stiff brass wire (or even one of the XYL’s sewing needles, if big enough!).

Now for the “window.” This is made from Perspex. You can get a sheet from the local model shop. Decide how big a window you need, and cut two sheets of Perspex, this size. Clamp the sheets together and drill a fixing hole in each corner.

On the one sheet inscribe a semi-circle just a little bigger than the arc the tip of the pointer will describe.

With a fretsaw, cut out the semi-circle and file the edges smooth.

Put the Perspex over the panel so that the pointer holder and the pointer can travel their full track without fouling the Perspex, mark where the four holes in the corner of the Perspex fall, and drill them out.

Prepare a white card the size of the Perspex and make a hole big enough to clear the pointer holder.

Now to assemble. Mount the drive on the back of the panel. Place the white card over the front of the panel. Screw on the pointer holder. Put on the Perspex sheet with the semi-circular hole. Put the other sheet on top of that. Slip the bolts through the fixing holes and tighten up the nuts. And there’s the dial.

When you are calibrating, you can leave off the top sheet of Perspex. This gives you access to the white card, but does not allow the card to slip about, which is important.

For a signal generator, you can mark the frequencies straight on to the card. For a short wave receiver you can mark on the card where the bands fall by means of thick black lines, and take more exact dial readings from the graduated knob.
Kit and Component Reviews

1. Tuning Unit

Samsions Surplus Stores, of 169/171 Edgware Road, London, W.2., have sent for our inspection a tuning unit which they are offering for 17s. 6d.

This item is a tapped inductor, built on a very solid bakelite framework. The coil consists of some 37 turns of 24" diameter, wound with 12 swg silver plated copper wire. The tapping is continuously variable, good contact being ensured by the use of a spring-loaded plunger. The control spindle is fitted with a vernier dial arrangement to enable accurate re-setting, and the control knob is fitted with a hinged handle to enable quick travel of the plunger from one end of the coil to the other to be obtained.

The unit would make an ideal basis for an aerial tuning unit for use with a low power transmitter. Another use would be to remove the coil and divide this into smaller units as plug-in tank coils for the PA stage of a transmitter, when the bakelite framework would make a very attractive table lamp standard. Other uses will, no doubt, occur to readers of an inventive mind.

2. All-Dry Battery Operated Signal Tracer and Audio Oscillator Kit.

(Henry's Radio, 5 Harrow Road, London, W.2.)

This kit makes up into a most versatile instrument, enabling the progress of a signal to be traced through a faulty receiver from input to output, so that the source of the trouble may be quickly located. Amplifiers may be checked in like manner, and also for distortion. The tracer itself may also be used as an AF amplifier. An audio oscillator is incorporated, and this can be used either separately or in conjunction with the tracer section.

The tracer section consists of a high gain, two stage amplifier using an IT4 followed by an IS4, plus a crystal diode. Resistance capacitance coupling is employed, and a speaker is built in. Automatic bias is applied to the output stage.

The audio oscillator section employs a IT4 valve, triode connected, the necessary feedback from anode to grid being transferred by an AF transformer. The output from this section is taken via a 250 kΩ potentiometer, capacitance coupled to the anode.

The kit supplied is absolutely complete, even to the battery (type B114), cabinet and such small items as wire, screws, solder, etc. The polished wood cabinet is a particularly fine job, with hinged lid giving access to the speaker and controls, and a sliding panel for insertion of the battery.

The cost of the kit is £4.19s. 6d., or it may be obtained fully assembled for an additional charge of 15s. A constructional booklet is available at 1s. 6d., and parts may also be obtained separately at retail prices.

3. Premier 2-Valve AC Medium Wave Receiver

(Premier Radio Co., 207 Edgware Road, London, W.2.)

This receiver, which we have seen in operation, is ideal as a standby or for use in the kitchen, etc. It would also serve as an efficient signal tracer.

Reference to the circuit shown here and to that of the Baby Alarm kit recently reviewed shows that this receiver is exactly the same job except for the tuning section. Premier Radio will, in fact, supply the Baby Alarm kit less microphone and input transformer for this purpose, at 64s. 6d. The only additional components then needed are a two-winding medium wave coil (the Premier Red Spot coil is ideal), a 100 pF fixed condenser, a 30 pF trimmer and a 500 pF tuning condenser. The latter may conveniently be of the reaction type for compactness.

Premier 2-Valve AC Medium Wave Receiver

Component Values

<table>
<thead>
<tr>
<th>Component</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>R1</td>
<td>2.2 MegΩ</td>
</tr>
<tr>
<td>R2</td>
<td>470 kΩ</td>
</tr>
<tr>
<td>R3</td>
<td>3.9 kΩ</td>
</tr>
<tr>
<td>R4</td>
<td>100 Ω</td>
</tr>
<tr>
<td>R5</td>
<td>27 kΩ</td>
</tr>
<tr>
<td>C1</td>
<td>0.005 µF</td>
</tr>
<tr>
<td>C2</td>
<td>0.5 or 1 µF</td>
</tr>
<tr>
<td>C3</td>
<td>0.005 µF</td>
</tr>
<tr>
<td>C4</td>
<td>1 µF</td>
</tr>
<tr>
<td>C5</td>
<td>1 µF</td>
</tr>
<tr>
<td>C6A/B</td>
<td>16-16 µF  350V electrolytic</td>
</tr>
</tbody>
</table>

Volume control with switch.
USES FOR SURPLUS MOTOR GENERATORS

By T. H. O'DELL

There have been, for many years now, a large number of dynamos and small motor generators for sale on the surplus market. These machines are usually converted into AC or DC commutator motors, but there are other uses for them which are, perhaps, not so obvious.

Motors of ratings such as 28V 100A, usually found in connection with the 400 c/s motor alternators, are strangely enough the most useful of all surplus machines for conversion into AC mains motors.

The basic circuit of such a motor is shown in Fig. 1. To convert this machine for AC mains, the brushes are removed and a thick piece of copper braid is wrapped tightly around the armature commutator's segments, and the ends soldered together, thus short-circuiting all the commutator segments to one another.

A better way to do this modification is to remove the rotor and fit a short length of copper tube over the commutator. It is often very hard, however, to remove the rotor due to the tight fit of the frame and ball races.

The conversion is now completed, and the mains are connected to the original 28V input terminals. The motor will run as a 50 c/s induction motor, despite its strange appearance. The spindle speed will be about 2,800 rpm for a two pole machine, and about 1,400 rpm for a four pole one. A 28V 60A motor converted in this manner can develop 1-8-1-4 HP very easily at about a 5 per cent. fall in speed; up to 3/8 HP can be developed for a short period.

A large condenser should be connected in parallel with the motor, to improve the power factor of the machine and to increase its efficiency. A value of 10-20 uF is usually sufficient. Any overheating is usually due to a moans, connection on the commutator shunting braid. This may have to carry up to 30A when starting, etc., so arcing will ensue if the band is at all loose.

The conversion applies only to 28V motors, as a 12V motor would have too small a field reactance. Also, the current rating should be as high as possible, and above 50A, to give high power and efficiency.

Passing, now, to the small dynamos found in surplus units, these may be converted into useful sources of low voltage DC.

A typical circuit is shown in Fig. 2. The only modifications are to break one of the leads going from the field winding to the low voltage commutator and insert a switch, S1. The commutators are then wired in series, as shown, observing correct polarity. The polarity is usually marked on the frame, above the brush holders.

DC is then applied, with S1 open, of the same voltage as the original HT output. When the armature is revolving, S1 is closed and the original motor section will run as a dynamo.

One of the small Command Receiver dynamos, 28V 1-7A input and 270V 70 mA output, when modified in this manner gave a steady 16V at 0.5A, 15V at 1A, and 18V on open circuit. It was run off a small 75 mA metal rectifier as shown in the diagram, Fig. 2.

MORE MNEMONICS

Two readers have responded to the writer's recent paragraph on the subject of radio mnemonics.

W. Jackson of Chester-le-Street, Co. Durham sends in the following useful reminders for circuit relationships:

**Watts**\[W = \text{V} \times \text{I} \times \text{Time} \]

\[W = \text{V} \times \text{I} \]

or

\[W = \text{V} \times \text{I} \times \text{Resistance} \]

**Amps × Volts or IV = WIVout it!**

**Volts = W/IV**

**Amps × Resistance = IR = India Rubber**

Both fractions are, of course, equal to unity.

The other mnemonic comes from S. Holme of Brockley, S.E.4. This one concerns the resistor colour code.

- "Better" Black 0
- Be Brown 1
- Red 2
- Over Orange 3
- Your Yellow 4
- Grid Green 5
- Bias Blue 6
- Values Violet 7
- (for) Grey 8
- Working White 9

Excellent advice and a very useful reminder! Do other readers know any more of these mnemonics? All are welcome, and all will be acknowledged.

J.R.D.

(In Your Workshop).

REGULATORS IN PARALLEL

I was interested to read J.R.D's comment on oscillator stability in his June contribution 'In Your Workshop' and there seems every possibility that his scheme could work. There is one point which, rightly or wrongly I feel might have escaped him, so I hope he will not mind my submitting a few words regarding it. When two neon regulator tubes are connected in parallel there is a danger of only one of them striking when voltage is applied; there is in fact a race between them and the first one home gets the prize. It therefore strikes with great joy, and immediately pulls down the applied voltage to its running value. From there on it's a case of I'm all right Jack—the other tube sitting there looking dark and glum about it all, simply because the voltage is now at running value and below its striking value. In actual fact, Tube No. 1 bites off more than it can digest by being greedy and snatching the lead it also takes unto itself a gross current overload, and consequently can't stand the strain, so just dies. In probability it will, in its death-throes, pass the buck to Tube No. 2—this poor inoffensive being will then have the agonies of its demised partner thrust upon it, so it, too, will take up a hopeless struggle with a death-dealing adversary. Result, two VR.150/30's ready for the dustbin.

Neon regulators are rather temperamental things, and their striking voltage alters somewhat with ageing, so although two tubes may have the same characteristics when new there might be considerable differences after some operation, depending on the actual conditions of use. Both temperature and light (or absence of light) causes changes in striking voltage. There was an article in the December 1950 issue of "Electronic Engineering," by R. E. Harpjohn, in which he discussed some investigations into this matter of parallel operation with particular regard to the STV.280/80 Stabilivolt multi-gap regulator tube, and devised a means of ensuring parallel operation, i.e., simultaneous striking. The circuit developed appears to be capable of adaptation to single-gap tubes of the VR.150/30 type.

I hope our friend J.R.D. will not mind me mentioning this article, and will not think of me as quoting scriptures to add weight to my words here. I appreciate that he put forward this idea for stable voltages as something that readers might like to experiment with—my comments here are intended only to point to a possible pitfall in such work, and not to deny his suggestion or even to deter independent research by readers who may not know about this peculiarity of neon regulators.

Yours sincerely,

W. E. THOMPSON.

(St. Leonards-on-Sea).
Abbreviations, Symbols and Simple Formulae

USED IN RADIO AND ELECTRICAL CIRCUITS

PART 1

Compiled by H. E. Smith, G6UH

(The following data has been compiled at the request of a number of readers, and will, it is hoped, be of assistance to the beginner and to the more advanced reader who has no ready access to all of the information given. The symbols have been grouped in order to provide a quicker reference.)

Commonly used Abbreviations

AC, Alternating Current.
A, Amperes.
AM, Amplitude Modulation.
Ant. or Ae., Aerial.
AF, Audio Frequency.
cm., Centimetre.
CW, Continuous Wave (Telegraphy).
cps or c/s, Cycles per second.
dB, Decibel.
DC, Direct Current.
EMF, Electro motive force.
f, Frequency.
FM, Frequency Modulation.
gnd or E, Earth.
H, Henry.
HF, High Frequency.
if or IF, Intermediate Frequency.
ICW, Interrupted Continuous Waves.
kc/s, Kilocycles per second.
KV, Kilovolt.
KW, Kilowatt.

mm or F, Magnetomotive Force.
mmF, Micro microfarad, (picofarad)
μF, Microfarad.
μH, Microhenry.
μV, Microvolt.
μW, Microwatt.
ma, Milliamperes.
mV, Millivolts.
mW, Milliwatts.
MCW, Modulated Continuous Waves.
P, Power.
PF, Power Factor.
RF, Radio Frequency.
UHF, Ultra High Frequency.
VHF, Very High Frequency.
V, Volts.
W, Watt.
As applied to Valve Circuits
I, Current.
E, Voltage.
C, Capacitance.
R, Resistance (Ohms).
L, Inductance (Henries).

(To be continued)

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