RADIO ELECTRONICS CONSTRUCTOR

MAY 1976

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JUNE ISSUE WILL BE PUBLISHED ON 1st JUNE

Telegrams Databux, London

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MAY 1976

Volume 29 No. 10

Published Monthly (1st of Month)

First Published 1947

Incorporating The Radio Amateur

Editorial and Advertising Offices

57 MAIDA VALE LONDON W9 1SN

Telephone

01-286 6141

Annual Subscription: £5.00 (U.S.A. and Canada \$11.00) including postage. Remittances should be made payable to "Data Publications Ltd". Overseas readers please pay by cheque or International Money Order.

Technical Queries. We regret that we are unable to answer queries other than those arising from articles appearing in this magazine nor can we advise on modifications to equipment described. We regret that such queries cannot be answered over the telephone; they must be submitted in writing and accompanied by a stamped addressed envelope for reply.

Correspondence should be addressed to the Editor, Advertising Manager, Subscription Manager or the Publishers as appropriate.

Opinions expressed by contributors are not necessarily those of the Editor or proprietors.

Production .- Web Offset.

Published in Great Britain by the Proprietors and Publishers, Data Publications Ltd, 57 Maida Vale, London W9 1SN

The Radio & Electronics Constructor is printed by Swale Press Ltd.

3 E !!!! High quality module

OUR PRICE

The 450 Tuner provides instant program selection at the touch of a button ensuring accurate tuning of 4 pre-selected stations, any of which may be altered as often as you choose, by simply changing the settings of the pre-set controls.

Used with your existing audio equipment or with the BI-KITS STEREO 30 or the MK60 Kit etc. Alternatively the PS12 can be used if no suitable supply is available, together with the Transformer T461

The S450 is supplied fully built, tested and aligned. The unit is easily installed using the simple instructions supplied.



 Max Heat Sink temp 90C.
Frequency response 20Hz to 100kHz
Distortion better than 0.1 at 1kHz
Supply voltage ■ Load – 3, 4, 5 of 160hms. ■ Signal to noise ratio 80db ● Overall size 63mm. 105mm. 13mm.

Especially designed to a strict specification. Only the finest com-ponents have been used and the latest solid-state circuitry incorporated in this powerful little amplifier which should satisfy the most critical A.F. enthusiast.

Stabilised Power Supply Type SPM80

SPM80 is especially designed to power 2 of the AL60 Amplifiers, up to 15 watts (r.m.s.) per channel simultaneously. With the addi-tion of the Mains Transformer **BMT80**, the unit will provide out-puts of up to 1.5A at 35V. Size: 63mm. 105mm. 30mm. Incorporating short circuit protection.

Input Voltage: 33-40 V.A.C. Output Voltage: 33V D.C. Nominal Output Current: 10mA-1.5 amps Overlead Current: 1.7 amps approx. **Dimensions:**

105mm x 63mm x 30mm Transformer 8MT80: £2.60 + 62p postage

BUTTO Fitted with Phase Lock-loop Decode

FET Input Stage ☆ VARI-CAP diode tuning Switched AFC ☆

Multi turn pre-sets ☆ ☆ LED Stereo Indicator

Typical Specificatio Sensitivity 34 volt Stereo separation 300 Supply required 20-30 at 20 Ma max.

3. Magnetic P.U. 3mV

P.U. Input equalises to R1A curve within 1dB from 20H to 20KHz. Supply - 20 - 35

299mm x 89mm x 35mi

into 50K ohms

at 20mA. Dimensions:

STEREO PRE-AMPLIFIER o eli:

A top quality stereo pre-amplifier and tone control unit. The six push-button selector switch provides a choice of inputs together with two really effective filters for high and low frequencies, plus tape output.

Frequency response + £dB 20Hz-20KHz

Sensitivity of inputs:

- 1. Tape input 100mV into 100K ohms
- 2. Radio Tuner 100mV into 100K ohms

P&P. 48 MK60 AUDIO KIT: Comprising: $2 \times AL60.1 \times SPM80.1 \times PA100.1$ front panel and knobs. 1 Kit of parts to include on/off switch, neon in-dicator, stereo headphone sockets plus instruction booklet. **COMPLETE** PRICE £27.55 plus 62p postage. TEAK 60 AUDIO KIT: Comprising: Teak veneered cabinet size 16[‡] x 11[‡] x 3[‡], other parts include aluminium chassis, heatsink and front panel bracket plus back panel and appropriate sockets etc. KIT PRICE £9.20 plus 62p postage.



7+7 WATTS R.M.S.

The Stereo 30 comprises a complete stereo pre-amplifier, power amplifiers and power supply. This, with only the addition of a transformer or overwind will produce a high quality audio unit suitable for use with a tape deck, etc. Simple to install, capable of producing really first class mains switch, fuse and fuse holder and universal mounting brackets enabling it to be installed in a record plinth, cabinets of your own con-structor or the cabinet available. Ideal for the beginner or the advanced constructor who requires Hi-Fi performance with a minimum of installa-tion difficulty (can be installed in 30 minutes)



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or stereo, mono and other audio equipment

instructions.

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125 watts R.M.S.



Specially designed for use in: Disco Units, P.A. Systems, high power Hi-Fi, Sound reinforcement systems.

The module has a sensitivity of 450mV and a frequency response extending from 25Hz to 20KHz whilst distortion levels are typically below .1%. The use of 4, 115w transistors in the output stage makes the unit extremely rugged while damage resulting from incorrect or short-circuit loads is prevented by a 4 transistor protection circuit.

SPECIFICATION:

Output Power 125watt R.M.S. Continuous. Operating voltage 50-80. Loads 4-16ohms. Frequency response 25Hz-20kHz Measured at 100

watts. Sensitivity for 100watts output at 1kHz, 450mV.

nput impedance 33kohms.

ONLY £15.95

Total harmonic distortion 50 watts into 40hms, 0.1%. 50 watts into 80hms, 0.06%. S/N radio better than 80dBs. Damping factor, 8ohms, 65. Semiconductor complement, 13 transistors, 5 diodes. Overall size: Heatsink width 190mm, Length 205mm, Height 40mm.

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high gain silicon transistors. It is provided with a standard DIN input socket for ease of connection. Supplied with full, easy-to-follow £2.65

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minimum £1.00

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The AL10; AL20 and AL30 units are similar The AL10: AL20 and AL30 units are similar in their appearance and in their general specification. However, careful selection of the plastic power devices has resulted in a range of output powers from 3 to 10 watts R.M.S. The versatility of their design makes them ideal for use in record players, tape recorders, stereo amplifiers and cassette and cartridge tape players in the home. Harmonic Distortion Po=3 watts (=1KH2 0.25%) Harmonic D f=1KHz 0:25%

10-20-30

书

i=1KHz 0:25% Load Impedance 8-16ohm. Frequency response ± 3dB Po=2 wetts 50Hz-25KHz Sensitivity for Reted OIP - Vs=25V. RL=80hm f=1KHz 75mV. RMS. Size: 75mm x 63mm x 25mm

AL10 3W R.M.S. £2.30 AL20 5W R.M.S. £2.65 AL30 10W R.M.S. £2.95

NEW PA12 Stereo Pre-Amplifier completely redesigned for use with AL10/20/30 Amplifier Modules. Features include on/off volumes. Balance. Bass. Treble controls. Complete with tape output. Frequency Response: 20Hz - 20KHz (-3db) Bess and Treble range ± 12dB Input Impedence 1 meg ohm Input Sensitivity 300mV Supply requirements 24V.5mA Size 152mm x 84mm x 33mm

NEW PA12 Stereo Pre-Amplifier

Power supply for AL10/20/30, PA12, S450 etc. Input voltage 15 – 20v A.C. Output voltage 22 – 30v D.C. Output Current 800 mA Max. Size 60mm x 43mm x 26mm, Transformer T538 £2.30

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Full spec marked	SEMICOND t by Mullard, e	UCTORS	s in stock	BSX20/21 BSY40	13p	OTHER DIODES
AC107 12p	BC184C/LC	9p BF180	/1/2/3 15	BSY95A	9p	1N4148 1.5p
AC128	BC186/7	13p BF184	/5 15	BU105-01	C41 OC44.	Centercel 10p
ACY28 18p	BC261B	10p BF194	A/195C/200 10	ASY63)	7p	BZY61 10p
AD149 40p	BC327/8	10p BF258	3/262/263 20	GE1111	32+p	BB113 Triple Varicap 37p
AF116 12p	BC547/558A	7p BFS28	Dual Mosfet 92	ON222	30p	BA182
AF124/6/7 20p	8C548/557	7/550 90 BFW10	0/11 F.E.T. 26	TIP30	43p	0A5/7/10 10p BZY88 Lin to 33 volt 6p
AF239 20p	BCX32/36	12p BFW5	7/58 . 20	TIS88A FE	т 23р	BZX61 11 volt 16p
ASY27/73 25p	BCY40	60p BFX12		ZTX300	5p	BR100 Diac 19p
BC107/8/9 6p	BD112/3/5/6	40p BFX29	30/84/88 16	2N393/MA	393. 30p	INTEGRATED CIRCUITS
BC108A/B/109B/C 10p	BD131/2/3/5	7/9 30p BFY50	0/1/2 12	2N706	6p	723 reg. 45p
BC147/8/9 6p BC147A/B 8p	BD142. BD201/2/3/4	45p BFY90	0 50 1	2N987		741 8 pin d.i.l. op. Amp 18p
BC148A/B/C, 9B/C/S8p	BD232/4/5	46p BRY3	Unj Junction 31	2N1507/22	19 14p	TAD100 AMRF £1.00
BC157/8/9 6p BC158A/B 11p	BDX/7	10p BSV64	5) 34 1 40	2N2904/5/	6/7 · · · 10p	TAA300 1wt Amp £1.25
BC159B/C,157A 11p	BF167/173	10p BSV79	9/80 F.E.T.s	1 2N2907A		NE555v Timer 40p
BC178A/B/179B 10p	BF1/8/9		Mostet 90	2N3054/30	55(or equiv) 35p	TAA263 Amp 62p
Amp Volt	BRIDGE	Amp Volt		2N3133 2N3704	18p 9p	7400 8p 7402/4/10/20/30 10p
1,600 BYX	10 30p 01-200 20p	0.6 110	EC433 15	P 2N4037		7414 45p
1.4 42 BY16	64 28p	5 400	Texas 75	P 2N5036	/360 31p	7483 200
RECTIFIER	S	OPTO ELE	CTRONICS	2SB135/6	/457 20p	LM300, 2-20 volt 50p
INADOA Amp	Volt	BPX40 65p	Photo transisto	40250	60p	1 74154 67p
IN4004 1	600 J	BPX42 £1.00 BPY10 £1.00	OCP71 30	p Amp Vol	THYP	RISTORS
IN4006 1	800 4p	(VOLTIAC)	BIGL.E.D. 0.2	1 240	BTX18-200	
BY103 1	1,500 15p	BPY68]	2v 50m/A ma	x. 1 400	BTX18-300 BTX30-200	23p
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BYX38-1200 2.5 BYX49-600 2.5	600 34 p	.3" red / segment D.I.L. 0-9 + D.P. di	L.E.D. 14 PAP	AFD 800 V	condenser /olt 30	18SWG 3p per foot
BYX49-300 2.5	300 26p	10m/a segment,	common 1MF	250	volt 15	
BYX49-900 2.5 BYX49-1200 2.5	900 40p	anode	65p 2MFI	D 250	volt 20	ISWG PER YD
BYX48-300 6	300 40p	Infra red transmitt	er £1 4M.FI	250	volt 20	P 20-24 2p
BYX48-600 6	600 50p	One fifth of t	rade I.C. e	xtraction and	insertion	26-42 1p
BYX48-1200 6	1,200 80p	Wire ended glass	neons 5p	TAL CHARG	HU SOCKETS	GARRARD
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DUAL METRONOME

By P. R. Arthur

This electronic metronome employs a very simple circuit and has the unusual feature of providing visual flashes in synchronism with the audible pulses.

Many electronic metronome designs have been published in the amateur electronic magazines over recent years. A number of these circuits are intended to closely imitate the sounds produced by a conventional mechanical metronome. Others, however, are designed more along the lines of a straightforward electronic metronome, with various refinements included to improve their performance.

This metronome circuit falls into the second category and, apart from giving the usual clicking sound, it simultaneously produces a flash from a panel light. This duel output has the advantage that, when playing forte passages where the audible metronome beat may be drowned in the sound of the music, the visual indication can still be followed.

A very simple circuit is used, and only a single active device is employed in the unit. This is the versatile and popular 555 integrated circuit timer. The unit is battery powered and will give many hours use from a PP3 9-volt battery. The current consumption is about 8mA.

The frequency is variable from about 65 to 350 beats per minute.

555 TIMER

The 555 i.c. has quite a complicated internal circuit. It is probably easiest to understand the functioning of the device by considering the operation of each stage, and the circuit breaks down into the constituent stages shown in Fig. 1. The area inside the broken line represents the 555, whilst the components outside the broken line are those needed to enable the i.c. to operate as a simple astable multivibrator.

When the supply is initially connected, CA begins to charge via RA and RB. TRA is turned off and the output from pin 3 of the device is high. The three resistors in the internal resistor chain of the i.c., RD, RE and RF, are of equal value. When the voltage across CA becomes fractionally greater than the voltage at the junction of RD and RE, which is two-thirds of the supply voltage, the output of Comparator 1 alters and changes the state of the flipflop output. TRA turns on and begins to discharge CA via RB until the voltage across CA is less than the voltage at the junction of RE and RF. or one-third of the supply voltage. The output of Comparator 2 then



Fig. 1. Simplified block diagram illustrating the operation of the 555 timer i.c.





changes and resets the flip-flop to its original state. TRA is turned off once more, and CA charges through RA and RB until the potential across it again reaches two-thirds of the supply voltage. The whole procedure then repeats itself, and the circuit continues to oscillate.

Over the period that TRA is turned on the output goes low, with a current being passed by the load, RC.

The time that the output is high is proportional to the time constant of CA and the sum of RA and RB.

COMPONENTS

Resistors

(All fixed values $\frac{1}{4}$ watt 10% unless otherwise stated) R1 56 $\Omega \frac{1}{2}$ watt

R2 680 Ω

R3 100k Ω

R4 2.7k Ω

VR1 470k Ω potentiometer, linear

Capacitors

C1 100 μ F or 125 μ F electrolytic, 10V Wkg. C2 2.2 μ F plastic foil, type C280 (Mullard)

Integrated Circuit IC1 555

Light-Emitting Diode

LED1 TIL209 or equivalent, with mounting bush

Switch

S1 s.p.s.t., rotary or toggle (see text)

Speaker LS1 35 to 80Ω , $2\frac{1}{4}$ to $3\frac{1}{4}$ in. diameter

Miscellaneous

Veroboard, 0.1in. matrix Aluminium box, $5\frac{1}{4} \times 4 \times 1\frac{1}{4}$ in. (see text) Control knob(s), as required 9 volt battery type PP3 (Every Ready) Battery connector The output is low for a duration proportional to the time constant of CA and RB only. During this period, RA plays no active part as its lower end is held close to the negative supply rail by TRA.

PRACTICAL CIRCUIT

The practical metronome circuit is very straightforward, and is shown in Fig. 2.

The 555 has quite a high output current capability, and pin 3 of the device is used to drive both the speaker and the light-emitting diode. R1 limits the speaker current to a satisfactory level, and R2 similarly limits the l.e.d. current.

The charging time of C2 is determined by the values of VR1, R3 and R4. VR1 can be adjusted to alter this time, and it thus acts as a frequency control. The relatively low value of R4 gives a very short discharge time for C2. It is while C2 is discharging that current is passed by the l.e.d. and the loudspeaker.



Fig. 2. The metronome has the very simple circuit shown here A continuous string of audible pulses is thus produced by the speaker, with D1 briefly flashing on at the same time as each pulse. VR1 varies the repetition rate of the pulses and flashes.

C1 is the supply decoupling capacitor and S1 is the on-off switch.

The loudspeaker may be any small type with a diameter of $2\frac{1}{4}$ to $3\frac{1}{2}$ in. and an impedance between 35Ω and 80Ω . In general, the higher the speaker impedance the better the results which are given. The l.e.d. is a TIL209 or equivalent, with a mounting bush or panel holder. It passes a current of around 10mA when it is turned on. The on-off switch may be toggle or rotary, with rotary giving a better appearance to the completed unit. The author employed a miniature multi-way rotary switch with adjustable end stop, no connections being made to the unused tags. A small single pole or double pole 2-way rotary switch could alternatively be used. C2 is a plastic foil non-electrolytic capacitor type C280.

COMPONENT PANEL

Apart from S1, VR1, the l.e.d. and the speaker, the components are wired up on an 0.1in. matrix

Veroboard panel having 18 by 19 holes, as illustrated in Fig. 3. As will be explained shortly, there are two ways of mounting this panel, and with one of these there is no necessity to drill the two 6BA clear holes shown in the diagram.

First cut out a panel of the required size and then, if these will be needed, drill out the two 6BA clear holes. Next, cut the strips at the points indicated in Fig. 3, using a Vero spot face cutter or a small twist drill.

Next, fit and solder the five link wires. These can consist of ordinary tinned copper wire of around 22 s.w.g., and do not need to be insulated. Then, solder on the components. The leads to external components are fitted later.

CASE

The case must be sufficiently large to take the speaker and the Veroboard panel, and that used for the prototype was an aluminium box with front panel type BA4, with nominal dimensions of $5\frac{1}{4}$ by 4 by $1\frac{1}{2}$ in. This box is available from several retailers, including Bi-Pak and Henry's Radio. Other boxes of similar dimensions may be used, the main proviso being, of course, that the parts can be accommodated.



Cut strips at F-6, F-7, F-8 and F-9

Fig. 3. Component layout on the Veroboard panel. Also shown are the connections to components external to the panel





As can be seen from the photograph of the front panel, a grid of small holes is drilled on the left hand side for the speaker. The two controls and the l.e.d. are mounted in a vertical line to the right, with VR1 at the top and the l.e.d. at the bottom. Precise dimensioning is unimportant provided that a neat final appearance is given.

The speaker can be affixed to the panel with nuts and bolts or, as in the prototype, with adhesive. A high quality adhesive, such as epoxy resin, is required. Only a modest amount should be applied to the rim of the speaker, and care should be taken to ensure that none of the adhesive is smeared on the cone or surround.

The component panel is positioned behind S1 and the speaker and, as just mentioned, it can be mounted in one of two ways.

First, it can be bolted to the rear inside of the case with a couple of short 6BA bolts. The mounting position should be such that C2 fits into the space between S1 and the speaker when the two parts of the case are screwed together. Strip 18 is at the top. The component panel must be spaced clear of the rear of the case by insulated spacing washers placed over the mounting bolts between the case and the panel. A layer or two of plastic insulating tape is affixed over the rear



Rear view of the Veroboard component panel and the front panel of the case

case surface beneath the area where the panel is mounted, and this provides additional protection against accidental short-circuits between the case and the connections on the copper side of the Veroboard panel.

Before finally mounting the panel in position, wire it up to the components on the front panel, using 5in. lengths of flexible p.v.c. covered connecting wire.

The second method of mounting the board is slightly easier. It consists of simply wiring the component panel to the components on the front panel of the case by means of short lengths of heavy gauge single strand insulated wire. The component panel is held in approximately the required position during wiring, with C2 between the speaker and S1, the copper strips to the rear and strip 18 at the top. With this method of mounting, the panel is obviously less rigid than when the first method is employed. However, the panel is very light and it stays in place quite satisfactorily.

A layer of plastic insultating tape is spread over the appropriate area of the rear inside surface of the case to ensure that there are no short-circuits to it when the front panel is screwed on.

All the wiring in the unit is shown in Fig. 3, with the exception of the lead connecting one tag of S1 to the positive battery clip. With both methods of component panel mounting, the leads to the battery connector are flexible. The battery fits into the space beneath the speaker and, if necessary, some foam rubber or plastic can be placed in this space to hold the battery in position.

No connection is made to the aluminium case itself.

TESTING

When the metronome has been completed, give the wiring a thorough check for mistakes and, when satisfied that all is well, turn the unit on. After a brief pause, the metronome should produce a continuous succession of simultaneous clicks and flashes. Check that the frequency of these increases when VR1 is adjusted in a clockwise direction.

justed in a clockwise direction. The exact range of frequencies covered will vary somewhat between individual units, but it will be approximately as stated earlier, i.e. 65 to 350 beats per minute. One advantage of using the 555 i.c. is that the frequency does not change significantly with variation in battery voltage. The frequency coverage does not, therefore, alter as the battery voltage falls with age. A simple scale calibrated in beats per minute can easily be marked around the control knob of VR1, if required.

TONE ALTERATION

Metronomes usually produce a fairly high pitched sound, and it is possible to obtain a slightly more conventional and higher pitched pulse from the unit by filtering out some of the bass content. This can be done by connecting an electrolytic capacitor of suitable value in series with the speaker. The modified circuit is shown in Fig. 4.



Fig. 4. A modification which allows pulses of higher pitch to be produced. The value of the additional capacitor is selected to suit the particular speaker employed



A close look at the Veroboard panel

If the second method of mounting the component panel has been used, the capacitor will simply replace the lead connecting hole B16 on the panel to the appropriate speaker tag. The capacitor lead-outs should be covered with sleeving. With the first method of mounting, the loudspeaker lead from B16 can be removed and the capacitor, positioned horizontally, connected between F16 and F11. The loudspeaker lead can then connect to E11. The value required in the capacitor depends to some extent on the speaker employed, and is best found by trial and error. It should be a miniature type, have a working voltage of 10 volts and will probably be 50μ F or a little less. Too low a value will result in greatly reduced volume. The capacitor is wired permanently into circuit after the required value has been determined.

SEQUENTIAL

By T. Miles

It is occasionally desirable to have a push-button circuit in which an initial touch on the button causes equipment to be switched on, whilst a second touch on the button causes it to turn off again. If the button is pressed once more the equipment is again switched on, and so on.

Sequential operation in this manner can be provided by, say, a JK master-slave flip-flop i.c., but such a device could not be used to control a circuit which operated at a relatively high voltage or current. The flip-flop could, of course, control such a circuit by way of a relay. Whereup n one can argue that, if one relay has to be used, why not employ two relays and dispense with the flip-flop!

This article describes a very simple sequential switching circuit which incorporates two standard relays. One of these energises and stays energised when a button is pressed, and it releases and stays released when the button is pressed a second time.

CIRCUIT OPERATION

The circuit of the sequential switch appears in Fig. 1. In this diagram the two relays are shown with the 'detached' method of presentation. Each relay coil is presented as a rectangle alongside which is an identifying letter over a figure. The figure represents the number of contact sets which the relay has, and these are shown, in the de-energised condition, anywhere in the diagram. Thus, Relay A has two contact sets, these being A1 and A2.

Both relays should be of the same type and have the same coil resistance. Those employed by the author were P.O.3000 types with coil resistances of 500Ω .

When the 18 volt supply is initially applied, current flows from the positive rail through the coil of Relay A, the 12 volt zener diode ZD1 and the coil of Relay B to the negative rail. The zener diode drops a voltage of 12 volts whereupon only 3 volts appears across each relay coil. This voltage is not sufficient to operate the relays and they remain in the de-energised state.

If push-button S1 is now pressed, the lower end of the coil of Relay A is connected direct to the negative rail via contacts B1, with the result that Relay A energises. Its contact set A1 closes. The circuit remains in this state during the period when S1 is closed. There is no voltage across the coil of relay B, as this coil is short-circuited by way of S1 and contacts B1.

When S1 is opened, the short-circuit is taken off the coil of Relay B and this energises. Both the relay coils are now in series across the 18 volt supply and both relays are energised. Also, contact set B1 has changed over to the energised position.

RELAY SWITCH

A very simple sequential switching circuit which incorporates two standard relays.



Fig. 1. The circuit of the sequential switch. Relay A successively energises and releases as the push-button is pressed

If S1 is now pressed again, a short-circuit is placed across the coil of Relay A by way of the energised contact set B1. Relay A releases and its contacts A1 open. A circuit is now completed from the positive rail via contact set B1, S1 and ZD1, causing 6 volts to be present across the coil of Relay B. This voltage is sufficient to maintain the already operated relay in the energised state.

SI is next opened whereupon the positive circuit via ZD1 to the coil of Relay B is broken. There is now 3 volts across each relay coil and Relay B releases. The circuit has returned to its initial state and will start another cycle if S1 is pushed once more.

The circuit controlled by the sequential switch is turned on and off by the second set of contacts, A2, of Relay A.

COIL VOLTAGES

The relays employed in the circuit energise reliably at a coil voltage of 9 volts. It will be noted that 18 volts is applied across the coil of Relay A when S1 is initially closed. The use of a voltage which is double the normal energising voltage is quite in order with the relay types employed. On the second part of the switching cycle, Relay B is held energised at a coil voltage of 6 volts and then releases at a coil voltage of 3 volts. This 2:1 voltage change should be more than adequate for reliable relay release. If ZD1 should be on its lower voltage tolerance, or if Relay B shows a little reluctance to release, one or more forward biased silicon rectifiers may be inserted in series with ZD1, as in Fig. 2. These may be type 1N4002 or similar, and each will drop a further 0.6 volt. The writer had no problems in this respect with the prototype, in which the actual zener voltage, as measured, was approximately 12.2 volts. The 18 volt supply should be reasonably well regulated, to say plus or minus 0.5 volt. Current consumption varies between 6mA and 36mA. Although not checked out by the author, there seems little reason to doubt that the basic circuit of Fig. 1 should not cope satisfactorily with relays of a different type and having different coil resistance.

Although not checked out by the author, there seems little reason to doubt that the basic circuit of Fig. 1 should not cope satisfactorily with relays of a different type and having different coil resistance. As already mentioned, both relays should be of the same type and have the same coil resistance. Some experiment may be needed to find the optimum supply and zener diode voltages.



Fig. 2. If desired, the zener delay voltage may be slightly increased by adding one or more silicon rectifiers in series

P.O.3000 relays are fairly frequently advertised on the surplus market. They are also available, made up to customer's specification, from L. Wilkinson (Croydon) Ltd., Longley House, Longley Road, West Croydon, Surrey.

TECHNOLOGY BREAKTHROUGH WITH SINGLE CHIP CALCULATOR



NEWS

A technical breakthrough has been achieved by CBM Commodore Business Machines of 446 Bath Road, Slough, Bucks, with their own "3D" chip. This, for the first time ever in a calculator it is claimed, has all the components *including* digit drivers built into a single integrated circuit.

AND

This chip is being used to up-grade the very popular 776MD to the 796MD. The new model has 8 digits, a memory and percent key and will retail for only $\pounds 6.95$ including VAT.

Kit Spencer, Marketing Manager CBM, commenting on the launch said: "This technical breakthrough by our own design team will help in further establishing our current position of market leadership achieved by our value for money policy with a memory and percent calculator for only £6.95."

RAPID SETTING ADHESIVE FROM KELSEAL

Kelseal Ltd., of Wood Lane End, Hemel Hempstead, Herts., announce the introduction of a range of Rapid Setting Cyanoacrylate Adhesives. Minute quantities can be used for almost instantaneous adhesion to a variety of substrates. Viscosity of the various grades vary making them suitable for application where good spreading or a concentrated amount is required, according to surface condition.

The standard grades available are:

HM22 — A methyl ester of medium viscosity and setting time. Primarily recommended for metals.

HM32 — A methyl ester of high viscosity and medium setting time. Primarily recommended for metals.

HE32 — An ethyl ester of high viscosity and short/medium setting time. Primarily recommended for plastics.

HB11 — A butyl ester of low viscosity and fast setting time. Primarily recommended for rubbers but also plastics.

The adhesive is supplied in three sizes of plastic container, 20g, 45g, and 450g.

Varying applicator nozzles are available to suit the viscosity of the product and application.



RADIO & ELECTRONICS CONSTRUCTOR

COMMENT

TWO HOURS OF HI-FI ON RADIO TEES

"Sounds Superb" is the title of a specialist hi-fi programme on Radio Tees, the Independent Local Radio Station for Cleveland, South Durham and North Yorkshire. The programme is presented by Radio Tees' Programme Controller, Bob Hopton. Bob says, "The programme started life as a means of drawing attention to our VHF transmissions which are, of course, in stereo. However, it has developed since into a programme covering all aspects of hi-fi."

A confirmed hi-fi enthusiast himself, Bob^{*} points out, "That there is no better place to talk about hi-fi and sound than on radio and the reaction has encouraged us to extend the programme by half-an-hour to two hours as from 2 March; this will I believe, make it by far the longest programme about hi-fi sound on radio."

"Sounds Superb" includes a wide range of music from Queen right through Nana Mouskouri and Oscar Peterson to Monteverdi and also includes regular equipment reviews, book reviews, the latest news on equipment and hi-fi developments and a phone-in in which Bob tries to help with hi-fi problems.

"Sounds Superb" happens every Tuesday evening from 8.00 pm-10.00 pm and is on 95 VHF in stereo and also, of course, on 257 metres medium wave.

ELECTRIC BENCH GRINDER



This new top quality machine is designed for the professional and the "Do It Yourself" user. It incorporates a $\frac{1}{4}$ h.p. single or three phase motor with condenser starting and is fitted with two 6in. grinding wheels, one coarse and one fine, a safety pull/push on/off switch, safety plastic eye shields and the whole machine is built on generous and robust lines and is outstanding value for money.

Supplied complete with fixing bolts and delivered in a strong wooden crate.

Price: £35. Plus £3 Packing and Carriage. Plus VAT. Available from: Hadley Sales Services, 112 Gilbert Road, Smethwick, Warley, West Midlands B66 4PZ.

ELECTRONICS SUMMER SCHOOL FOR TEACHERS

The Department of Electrical Engineering Science at Essex University will be holding its annual Electronics Summer School for teachers during the week July 12-16 and, this year, three courses will be run simultaneously. The Linear Circuit Design course is concerned with the use of transistors and operational amplifiers in analogue applications and the basic circuits of a hi-fi amplifier are investigated in detail. The Digital Circuit Design course concentrates on the use of the transistor as a switch and develops design using integrated logic circuits. Small Computer Systems is a new course which aims to introduce a typical small computer, the PDP-8.

Further information on the Summer School can be obtained from R. J. Mack at the Department of Electrical Engineering Science, University of Essex, Wivenhoe Park, Colchester CO4 3SQ.

ANTIQUE RADIO

The collection of antique and wartime radios belonging to Ron Ham, the well known experimenter and radio astronomer, is going on display for 6 weeks as from 1st May at the Horsham Museum. On 10th August the display will move to the Worthing Museum for a similar period.

We hope from time to time to publish short descriptions of some of the equipment in this interesting collection.



"That's right sir — your set was guaranteed for twelve months. Unfortunately this isn't one of them!"

THE 'SUPERALPHADYNE' PORTABLE RECEIVER

Part 1

By Sir Douglas Hall, K.C.M.G.

Employing an ingenious reflex circuit, this receiver offers a high level of selectivity on medium and long waves. There are only three transistors, and an added bonus is an extension of range from the lower medium wave band down to 120 metres. The article will be concluded in Part 2, to be published next month.

Home-constructed radio receivers with single tuned circuits have the great advantages, when compared with superhets, of simplicity and economy of components, this latter point being of considerable importance in these days of rapidly rising prices. Typical single tuned circuit designs use, at the front end, either one or two reflexed common emitter transistors amplifying both at r.f. and i.f. or a single integrated circuit.



The completed receiver, fitted in its case

SELECTIVITY

There are many areas in which either of these types of receiver are perfectly satisfactory but there are others, and the author lives in one, where the proximity of a very powerful medium wave transmission causes its signal to spread over much of the medium wave range. In the writer's locality reception of Radio 1 would be unobtainable as the local Radio 4 transmitter, just 10 miles away, would swamp it right out. It was for areas such as this that the author in troduced his "Spontaflex Super-Alpha" circuit in the May 1968 issue of this journal, and the basic circuit has been developed and used in otherwise widely differing designs several times since. There are, of course, areas with worse conditions than the writer experiences where the local station is so strong that even the "Super-Alpha" receivers are defeated as, indeed, may be the simpler superhets.

may be the simpler superhets. With the present receiver, however, which uses the latest version of the "Super-Alpha" circuit, selectivity and freedom from swamping have been further improved. While the author writes the draft of this article he is listening to a full-blooded signal from Radio 1 without a trace of interference from Radio 4. It may be added that both stations are in the same direction and so no advantage can be taken of the directional properties of the ferrite rod aerial.

There are only three transistors in the receiver, but the author has a choice of seven stations during the hours of daylight and many more after dark, all at full programme value.



Fig. 1. The circuit of the receiver. TR1 and TR2 appear in a reflex configuration and amplify both at radio and at audio frequencies

THE CIRCUIT

The circuit of the receiver is shown in Fig. 1. Tuning is carried out by means of the 100pF variable capacitor, VC1. L2 is wound on a former in which a ferrite rod can be moved, over an inch or so, to one of two positions. In the position where the rod is further out of the coil, and with S1 closed so as to short-circuit L1, tuning is given over a range of 120 to 290 metres. This makes the 160 metre amateur band available and also provides a bandspread tuning effect over the lower wavelength end of the medium wave band from around 190 metres to 290 metres. This setting of the ferrite rod offers extra selectivity at the lower end of the medium wave band, partly because of the reduced pick-up resulting from the ferrite rod not being fully in the coil. When the rod is in its alternative position, where it is fully in L2, and with S1 still closed, the whole of the medium wave band can be tuned by VC1. With the ferrite rod fully in L2 and S1 opened, L1 enters the tuned circuit in series with L2, and the long wave band becomes available. L1 is wound on its own separate ferrite rod. As will be made clearer later, S1 is a home-constructed switch which is actuated by rotating the ferrite rod when it is fully in L2.

COMPONENTS

Resistors (All fixed values 1/4 watt 10%) R1 390 Ω R2 10k Ω R3 47k Ω R4 100 Ω R5 3.3k Ω R6 680k Ω (see text) R7 1kΩ R8 4.7k Ω (see text) VR1 2.2k Ω potentiometer, wire-wound (see text) VR2 22k Ω potentiometer, log, with switch S2 (see text) Capacitors

C1 1,000pF silvered mica or ceramic C2 0.01µF plastic foil C3 1,000pF silvered mica or ceramic C4 64µF electrolytic, 2.5V Wkg. C5 1,000pF silvered mica or ceramic C6 10μ F electrolytic, 2.5V Wkg. C7 1,000µF electrolytic, 10V Wkg. (see text) C8.220pF silvered mica VC1 100pF variable, type C804 (Jackson)

Inductors L1, L2, L3 See text

L4 2.5mH r.f. choke type CH1 (Repanco)

T1 Inter-stage transformer type LT44 (Eagle) T2 Output transformer type LT700 (Eagle)

Semiconductors **TR1 BF167 TR2 BC169C TR3 BC169C** D1 0A10 D2 6.8V zener diode, 400mW

Switches S1 See text S2 S.P.S.T., part of VR2

Speaker

LS1 3Ω elliptical, 8 x 5in.

Battery

9-volt battery type PP9 (Every Ready)

Miscellaneous Ferrite rod, 8 x 3in. (203 x 9.5mm.) Ferrite rod, 6 x §in. (152 x 9.5mm.) 18-way tagboard, 'Standard Group Panel' (Doram) Packet 10 brackets, Lektrokit 2311 (see text) Packet 10 clips, Lektrokit LK2721 (see text) **Battery connectors** 4 knobs (see text) Materials for receiver assembly and case (see text).

It will be seen that the maximum tuning capacitance is 100pF plus strays, with the result that the inductance - capacitance ratio is very high, particularly on the normal medium wave band (ferrite rod fully in L2) and the long wave band. The ratio is lower when the 190 to 290 metre segment is selected and, at first sight, this would theoretically result in



The internal construction of the receiver, as seen from the tagboard side

lower selectivity. In practice, however, the rejection to swamping by a powerful signal is better. It is found that the inductance in L2 when the ferrite rod is fully in tends not to provide as good a bypass effect for unwanted powerful signals when tuning between 190 and 290 metres, and the larger inductance takes on some of the attributes of an r.f. choke.

of the attributes of an r.f. choke. The signal selected by the aerial tuned circuit is coupled to the base of TR1. TR1 and TR2 both act as common collector amplifiers at r.f. and thereby form a 'Super-Alpha' pair having an exceptionally high input impedance. D1, specially chosen for its low forward resistance to match the low output im-pedance at TR2 emitter, detects the signal. TR2, acting at a.f. as a common base transistor, next amplifies the detected a.f. signal and feeds it back to the base of TR1 via R2, L1 (if S1 is open) and L2. TR1 acts as a common emitter amplifier at audio frequencies, whereupon a further amplified a.f. signal appears at its collector. The unbypassed resistor, R4, provides a measure of negative feedback to TR1 and this, combined with the low emitter current of this transistor, provides an adequately high input impedance for TR2 collector, the resistive load for which is the relatively high value component, R3. As will be seen, there is a full reflex operation in TR1 and TR2; the two transistors first amplify the signal at radio frequency and then, operating in completely different modes, amplify the detected signal at audio frequen-

cy. The audio signal at TR1 collector appears across the primary of inter-stage transformer T1, whose secondary feeds into the base of TR3. This is a high gain transistor functioning in à common emitter output stage. Capacitor C8 provides a little treble cut and also bypasses any remanent r.f. signal present at TR3 base. Base bias is provided by R6, and the best value for this resistor may vary between $270 k_{\Omega}$ and $1M\Omega$ according to the exact characteristics of TR3 and the leakage resistance in C6. A value can be chosen which results in a total receiver current of about 12mA with a new battery, the current being measured by inserting a current-reading meter in one of the battery leads. Alternatively, a $1m\Omega$ pre-set skeleton potentiometer may be employed for R6, this being initially adjusted to insert maximum resistance into circuit. The resistance is then carefully reduced until the 12mA reading is obtained. When using the potentiometer great care must be taken to ensure that this does not accidentally insert too low a resistance as this could cause excessive collector current in TR3 with consequent damage to the transistor. However, the value of R6 is not unduly critical and in most cases a $680 \text{k} \Omega$ resistor can be used with confidence or, at least, for initial receiver tests.

VR1 is the reaction control, and positive feedback to L2 via L3 increases as the slider of this control moves towards the track end connecting to C2. A small direct current flows via R8 and R1 through D1 and causes this component to present a lower impedance; it also prevents instability which may otherwise occur at low tuning capacitance settings on the medium wave band. As VR1 is advanced, the d.c. shunting effect of L3 causes the direct current in D1 to reduce, with the result that oscillation occurs more readily. R1 is included to ensure that the detected a.f. signal at the diode is not partly short-circuited at high settings of VR1.

VR2 is a volume control and may be adjusted if necessary for the required volume after a signal has been tuned in and VR1 set just below the oscillation point.

Both VR1 and VR2 should be small in physical size, and those employed in the prototype were obtained from Electrovalue Limited. VR1 is a wire-wound component type CLR1106/11S, and has a body diameter of 0.94in. VR2 is a carbon track potentiometer with switch type P20, and has a body diameter of 0.79in.

CONSTRUCTION

Construction should not be started until the complete article has been read and the photographs studied to see the manner in which the various parts fit together. The dimensions should be suitable for any standard 8 by 5in. elliptical speaker, and it is assumed that this has a magnet which is not greater in diameter than 2in.

First carefully examine Figs. 2 and 3. The piece of Fig. 2(a) appears at the top of the main receiver assembly and is viewed from the underside so that the reader looks directly at the two pieces of springy brass strip which form S1. The brass strips may conveniently be taken from a discarded 4.5 volt flash lamp battery and the author has found that the tinned strips fitted to the more recent Vidor V1289 battery give much better contact in the switch application than do the old plain brass ones. There are two 'brackets, Lektrokit Part No. LK2311, secured to the upper surface of the item of Fig. 2(a), and their positioning depends upon the dimensions of the speaker used. A T-shaped cut-out appears in this item, as also does a 4BA clear hole. The latter will take a 2in. 4BA screw which will hold the battery in position.

Fig. 2(b) gives an inside view of one end piece for the assembly. There are three holes for the mounting bushes of VC1, VR2/S2 and VR1. Also shown is a $\frac{1}{4}$ in. length of wooden dowelling of $\frac{2}{5}$ in. diameter, this being held by means of a $\frac{2}{5}$ in. GBA bolt passing through a hole in the dowelling centre. This dowelling will take the end of the former for L2, L3, whose positioning is shown in Fig. 3. The other end piece is illustrated, again from the inside, in Fig. 2(d). This requires a hole slightly in excess of $\frac{2}{5}$ in. diameter to take the



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Upper view, illustrating the cut-out in the top section of the assembly

ferrite rod which passes into L2, L3. The positioning of the hole should match that of the $\frac{1}{2}$ in. dowelling in Fig. 2(b). The square section cut from the lower right hand corner, as seen in Fig. 2(d), allows the passage of a small wooden mounting block in the case.

Fig. 2(c) shows the base of the assembly, once more as viewed from the inside. This has two further brackets, Part No. LK2311, for speaker mounting, as, well as two spring clips, Lektrokit Part No. LK2721. The latter hold the ferrite rod for L3. It may be possible to secure the brackets and the clips by means of the same screws and nuts, but if the shape of the speaker is such that the coil or ferrite rod would touch it, the clips will need to be mounted separately a little further back.

The manner in which the four items just discussed fit together can be seen from the broken lines in Fig. 2(b) and Fig. 2(d). It will be apparent that, when the item of Fig. 2(a) is secured to those of Figs. 2(b) and (d), the brackets of Fig. 2(a) will be above the brackets of Fig. 2(c). The speaker brackets should be positioned such that the front of the speaker, mounted by its four chassis holes, is very slightly inside the upper edge (as seen in the diagram) of Fig. 2(c). This allows a piece of gauze to be slipped in inside the case later.

The Lektrokit brackets and clips just mentioned are available, each in packets of 10, from Home Radio.

The four pieces may now be cut out. They may then be temporarily assembled sufficiently firmly to allow the bracket and clip positions to be determined with the aid of the speaker to be used. The pieces may then be disassembled again and the brackets and clips mounted.

COILS

The coils are next prepared. They may be wound on sleeves made up from pieces of Fablon. For L1 cut out a piece of Fablon measuring 4 by 3in., leaving on all the backing paper except for a strip $\frac{1}{2}in.$ wide at one 3in. edge. Wrap the Fablon tightly around the 6in.ferrite rod at its centre, the exposed $\frac{1}{2}in.$ strip being wound on last so that it secures the completely rolled tube. A sleeve 3in. long is then given. L1 is wound as shown in Fig. 2(h). The 500 turns' are scramble wound, and the winding should progress gradually along the sleeve to take up an overall length of approximately 2in. A useful approach here consists of marking off $\frac{1}{2}$ in. sections on the sleeve and winding 125 turns at a time in each. The coil ends may be secured with thin pieces of adhesive tape. The sleeve for L2, L3 also consists of a piece of

Fablon measuring 4 by 3in. prepared in the same way as that for L1 to form a tube 3in. long. In this instance, however, the sleeve should be loose enough to allow the 8in. ferrite rod to move freely inside it. L2 and L3 are wound as indicated in Fig. 2(i). Both coils are close-wound.

Instead of sleeves made of Fablon the prototype employed thin-walled s.r.b.p. ('Paxolin') tubes, these being given by a 6in. length of tubing with an outside diameter of $\frac{1}{76}$ in. (Home Radio) cut into two 3in. lengths. The tubing has a nominal inside diameter of $\frac{3}{8}$ in. but some $\frac{3}{8}$ in. ferrite rods will not fit inside it. Because of this, the constructor is advised to employ the Fablon sleeves unless he already has access to the s.r.b.p. tubing and can check this physically with the ferrite rods to be employed.

Next, take up a p.v.c. grommet with a $\frac{3}{2}$ in. hole at its centre and cut it to the cam-like shape shown in Fig. 2(e). After this, cut out the s.r.b.p. piece of Fig. 2(f). This has another $\frac{3}{2}$ in. grommet fitted in its central hole. These two parts are fitted on the 8in. ferrite rod in the positions shown in Fig. 2(g), the $4\frac{3}{4}$ and $2\frac{3}{4}$ in. dimensions from the end of the rod being to the grommet centres. A turn or two of Sellotape may be initially wound on the rod to ensure that the grommets are a tight fit on it. The cam-shape grommet should have its projection pointing upwards when the projection on the s.r.b.p. piece is pointing downwards. A third grommet with a $\frac{3}{4}$ in. central hole is also fitted on



Another view of the completed receiver. The knob shown is fitted over the ferrite rod



Fig. 3. The various parts of Fig. 2 assembled together. Also shown are wiring details which will be discussed next month

the rod and is set up in position later.

The operation of the ferrite rod in conjunction with S1 may now be visualised with the aid of Fig. 2(a), Fig. 2(g) and Fig. 3. If the s.r.b.p. piece has its projection pointing upwards the rod may be moved to right or left, the projection moving in the herizontal (as shown in Fig. 2(a)) slot of the T-shaped cut-out. When the rod is pulled out the lower wavelength band of 120 to 290 metres is selected. When the rod is moved fully in, the standard medium wave band is available. If the rod is now rotated through 180 degrees, the circular section of the s.r.b.p. piece will enter the vertical (as in Fig. 2(a)) slot of the T-shaped cut-out, preventing the rod from being pulled out. At the same time the projection on the cam-shape grommet will depress the left-hand contact of S1, causing it to open. The long wave band is then selected.

These details also give further information on the manner in which S1 operates, and will enable the constructor to make up this switch correctly.

The third grommet in Fig. 2(g) acts as a stop and ensures that the correct band of 120 to 290 metres is selected when the rod is pulled out. It is put to the requisite position on the rod after the receiver has been completed and is held in place by winding on a narrow strip of Sellotape immediately to its left.

MAY 1976

The various parts of Fig. 2 are now assembled, as illustrated in Fig. 3. The left-hand end of the sleeve on which L2 and L3 are wound is fitted over the wooden dowel in Fig. 2(b) and may be secured thereto with a little adhesive. The right hand end of the ferrite rod passes through the hole in the item of Fig. 2(d), and a knob will be fitted to it later. Final adjustments may now be made to the shape of S1 contacts to ensure reliable operation. The speaker tags should be to the right, as indicated, or below the magnet, depending on their positioning in the particular speaker employed.

The 2in. 4BA screw which holds down the battery is omitted from Fig. 3 for clarity, as also are the parts of the speaker apart from its magnet. Some of the later wiring steps are illustrated in Fig. 3, and these will be described in the second part of this article.

NEXT MONTH

The next concluding part will complete the constructional information. The full Components List is published this month, and any outstanding details concerning individual components will be cleared up next month.

(To be concluded)



Now that integrated circuit timers such as the 555 and 556 are available, timing circuits incorporating discrete semiconductor devices are of less interest unless they possess a special feature not given by the integrated circuit timers or employ a small number of inexpensive components.

The timing circuit to be described in this article just falls into the requisite category. It is expressly intended for operation from a 9 volt battery, and draws a very low current between timing periods. Also, it requires few components and employs two low-cost transistors only. It offers timing periods which are continuously variable from about 4 to 75 seconds, and the accuracy of the periods does not alter significantly with falling battery voltage down to some 7 volts.

A small shortcoming is that the relay in the circuit energises momentarily when the unit is initially switched on. If this is considered a disadvantage a further switch can be inserted in series with the relay contacts this being closed after the main switch has been turned on.

CIRCUIT OPERATION

The circuit of the timer is given in the accompanying diagram. In this, Sl(a)(b) is the on-off switch and is shown in the "Off" position. When the switch is set to "On", Sl(a) applies the 9 volt supply to the circuit whilst Sl(b) discussed to the

When the switch is set to "On", SI(a) applies the 9 volt supply to the circuit whilst SI(b) disconnects the 33 Ω resistor, R3, from capacitor C2. The capacitor charges via the relay coil and the forward biased baseemitter junction of TR1, the charging current causing the momentary operation of the relay which has just been mentioned. The capacitor charges



The circuit of the electronic timer. This requires few components and draws a very low current between timing runs

rapidly, and it then has very nearly the full 9 volts of the supply across its terminals.

The charging current turns TR1 hard on and, after C2 has charged, TR1 remains conductive by reason of the current flowing to its base through R1 and VR1. As a result, its collector assumes a voltage above chassis of 0.2 volt or less. This voltage is applied to the base of silicon transistor TR2 which is, in consequence, cut off. No current flows in the collector of TR2, and the circuit is in one of its two stable states.

If push-button S2 is pressed, an energising voltage is applied across the relay coil. Also, the negative terminal of C2 is taken down to the positive supply rail, whereupon its positive terminal is taken 9 volts positive of that rail. TR1 is at once cut off and it draws no collector current through R2, whereupon a base bias current flows via R2 to TR2, and this transistor turns on. The circuit is now in its second stable state, with TR1 turned off and TR2 turned on. The closure of S2 can be very quick as, due to a regenerative effect between the two transistors, it is merely necessary for TR1 base to be taken slightly positive for the circuit to change state.

C2 next discharges via R1 and VR1. After a period of time, which depends upon the setting of VR1, the positive terminal of C2 takes the base of TR1 slightly negative of chassis potential and TR1 commences to conduct, drawing current through R2 and reducing the base bias current available for TR2. There is again a regenerative effect and it results in TR1 being turned hard on and TR2 being cut off. Again, C2 becomes charged to nearly the full supply voltage via the relay coil and the baseemitter junction of TR1.

To sum up, pressing S2 causes TR1 to turn off, TR2 to turn on and the relay to energise. After a time dictated by the setting of VR1, the circuit reverts to its previous state with TR1 on, TR2 off and the relay de-energised. A further timing period can then be initiated by pressing S2.

Observant readers will note that the circuit is really a monostable, or 'one-shot' multivibrator.

DISCHARGE PERIOD

As with a standard multivibrator, the discharge period in C2 following the closure of S2 is approximately equal to 0.7 times the time constant of C2 and the total resistance of R1 and VR1. When VR1 inserts zero resistance into circuit this calculates as 3.8 seconds and, when VR1 inserts maximum resistance, as 74 seconds. In practice, there will be fairly wide divergencies from the calculated values due to tolerances in R1, VR1 and, in particular C2. With the prototype circuit the timing range was approximately 4 to 85 seconds.

The timing period is independent of the negative terminal of C2 is at chassis potential, and if the discharge ends when its positive terminal also reaches chassis potential. In practice the negative terminal is held at about 0.2 volt above chassis by TR2, and the positive terminal rises to about 0.1 volt above chassis at the end of the discharge period. This is one reason why TR1 is a germanium instead of a silicon transistor. A second reason is that the maximum reverse baseemitter voltage rating of the germanium transistor specified for TR1 is 12 volts, whereas most silicon transistors have reverse base-emitter voltage ratings around 5 volts only. Had a sili-con transistor been used a diode would have had to be inserted between its base and the junc-

tion of VR1 and C2 to isolate these two components from the base during the discharge period. Even with a germanium diode the positive terminal of C2 would then have had to rise to some 0.7 volt above chassis level before TR1 turned on, and such a voltage figure would be too high to allow timing periods to be independent of battery voltage. With a germanium transistor in the TR1 position the base voltage at the end of the timing period is, as already stated, 0.1 volt only, and this much smaller figure can be assumed to allow the circuit to be almost completely independent of battery voltage within reasonable limits. The prototype circuit was run a number of times, with VR1 set to the maximum timing period, at supply voltages of 9 and then 7 volts. No discernable differences in period length were observed.

When the unit is switched off, Sl(b) causes C2 to be fully discharged by way of the current limiting resistor R3. In consequence it charges up again via the relay coil and TR1 base-emitter junction after switch-on. If Sl(b) and R3 are omitted, and C1 is left in a charged condition after switch-off, the circuit tends to go through a full timing period when it is switched on again.

A critical feature of the circuit is that, when TR1 is on and TR2 is off, the high level of amplification available causes the circuit to be sensitive to any small positive excursions which may appear at TR1 base; and these can trigger the circuit into its alternate state with TR1 off and TR2 on. A sudden small reduction in supply voltage can cause TR1 base to go positive by way of the relay coil and C2. In consequence it is not recommended that the circuit be run from a simple unregulated mains power supply since reductions in mains voltage could conceivably trigger TR1 off. There are no problems at all in this respect if the circuit is run from a battery or from a voltage stabilized mains supply. C1 is included as a precaution against triggering by transients, as could occur if VRI had a "noisy" contact between slider and track, and were adjusted quickly. It may be found that the circuit is triggered if the armature of the relay is pressed down quickly. Should it occur, this effect is not a fault sympton but merely demonstrates that the relay produces a momentary voltage when its magnetic circuit is suddenly completed.

During the time when S2 is pressed, the negative terminal of C2 is at chassis potential, rising to 0.2 volt above chassis when S2 is released. The small difference between these two potentials should not upset timing accuracy, particularly as S2 is pressed at the start of discharge in C2. The length of time during which S2 is closed is uncontrolled, but it will obviously be much shorter than even the shortest timing period of around 4 seconds.

Turning to components, D1 is the usual diode which is connected across the relay coil to prevent the appearance of a high back-e.m.f. when it releases. The relay used by the author was a "Miniature Open P.C. Relay" with 410 Ω coil which is available from Doram Electronics. Although not checked by the author, any other relay energising at around 6 volts and with a coil resistance between 400 Ω and some 700 Ω should function equally well. If a P.O. 3000 type of relay is used, its somewhat sluggish operation at low energising voltages may prevent it responding to the initial surge of charging current in C2 immediately after switch-on. S1(a)(b) requires a break-before-make action, and this will automatically be given if a d.p.d.t. toggle switch is used here. C2 should be a modern component in good condition, as also

The current drawn from the 9 volt battery when the relay is de-energised is 0.4mA when VR1 inserts maximum resistance into circuit, this rising to 0.8mA when it inserts minimum resistance. The current is approximately 22mA when the relay (if this is of the type employed by the author) energises.

When the circuit has been assembled, several timing runs may be carried out to confirm that operation is correct and to ensure that C2 is fully "formed". Calibration is then carried out by adjusting VR1 to different settings and checking the resultant timing periods with a watch having a sweep second hand.

Dear Mr. Plomley, please send eight more 'Desert Island Discs'. The last lot tasted lovely...



By Frank A. Baldwin

Times = GMT

Whilst listening around the various broadcast bands during each month obtaining material for this article, it quite often happens that one unexpectedly hears an unusual or new signal. A new station perhaps, or an old one on a new channel, a station logged for the first time after months of fruitless effort or even a previously unheard tuning or interval signal. Such an event occurred recently.

Gaberone, Botswana, may be heard on 4845 where it operates from 0400 to 0600 and from 1430 through to 2000 (until 2100 Fridays to Sundays). The station is fairly often reported in the SWL press, usually around the 1800 to 2000 time period, this also apply-ing to my logbook times. Tuning around recently, the dial pointer aligned with the above-mentioned frequency at 0345 at which time a few tinkling bells could be faintly heard. Over the next few minutes the bells became louder in what was obviously a repeated recording. Looking up the information on this frequency elicited the information that this was the interval signal of Gaberone and was in fact cow bells. This signal was heard until 0400 then a choral National Anthem, an announcement by YL in the Setswana language followed by a short prayer by OM in English. What the text book doesn't mention however is that the voice of the heardsman calling his cattle is also to be heard amid the jangle of cowbells!

Any other new signals? Well, the log shows reception of Radio Sana, Yemen, on a measured **4853** since way back in mid-January at which time we had it listed as an unidentified station. It is a relay of the domestic service and the log time entry was at 1629.

Or what about Hanoi on 9839 in parallel with 7512 from 1412 onwards with a programme in Lao to, Laos (where else!) in the External Service.

CURRENT SCHEDULES

TAIWAN

"Voice of Free China", Taipeh, has a programme in English directed to Africa and Europe from 2000 to 2100 on 9510, 11860, 15370 and on 17720.

POLAND

"Radio Warsaw" operates an External Service in which English programmes are provided for Europe as follows — from 0630 to 0700 on 7270, 7285 and on 9675; from 1200 to 1230 on 7285 and 9540; from 1600 to 1630 on 6095, 7125, 7285 and 9540; from 1830 to 1900 on 6095, 7285 and 9540; from 2030 to 2100 on 6095 and 7285 and from 2230 to 2300 on 3955, 5995, 6135, 6155 and on 7285.

HUNGARY

"Radio Budapest" schedules programmes in English to Europe from 1200 to 1240 (not Saturdays or Sundays) on 7155, 7215, 9585, 9833,

Frequencies = kHz

11910, 15160 and on 17715; from 2130 to 2200 on 5965, 6005, 7150, 7220, 9655, 11910 and on 15415.

A DX programme in English is featured on Tuesdays and Fridays from 1515 to 1530 on 6025, 6110, 7200, 7215, 9585, 11910 and 15415.

• ALBANIA

"Radio Tirana" radiates in English to Europe from 0630 to 0700 on **7065** and **9500**; from 1630 to 1700, 1830 to 1900, 2030 to 2100 and from 2200 to 2330 on **7065** and **9480**.

INDIA

"All India Radio", Delhi, broadcasts programmes in English in the General Overseas Service as follows — to East Africa, the U.K. and West Europe from 1745 to 1945 on 7225, 9525, 9575, 11620 and 15080; to North and West Africa, the U.K. and Western Europe from 1945 to 2045 on 7225, 9525, 9755, 9912, 11620 and on 11880; to the U.K. West Europe and Australasia from 2045 to 2230 on 7150, 7225, 9525, 9912, 11620 and on 11740.

• SPAIN

"Radio Nacional de Espana", Madrid, does not present any programmes in English to the U.K. of Europe but schedules some to North America which may be heard here in Britain. The broadcast to N. America is from 0100 to 0400 (Sundays excluded) on 6065 and 11880.

• OMAN

The Domestic Service mainly in Arabic from Muscat is radiated from 0300 sign-on to 2010 sign -off on 6175 and on 11890. There is however a programme in English which is also intended for listeners abroad, this being radiated on 11890 from 0900 to 1100.

AROUND THE DIAL

• CHINA

Foochow on 4975 at 2101, OM in Chinese, military music complete with stirring male chorus. This is Foochow 1 which operates from 0740 to 1600, from 2050 to 0540, additionally radiating a programme directed to Taiwan from 1600 to 1810.

Kunming on a measured 4759 at 1605 with OM and YL alternate in Chinese, signing off at 1620 with a choral version of the "Internationale". Schedule is from 0950 to 1620 and from 2150 to 0800.

Fukien on **3300** at 1553, talk in Chinese, short excerpts of local music. The latest schedule I have of this one is from 1000 to 1902 in Amoy and Standard Chinese in Network 2.

Radio Peking on 7010 at 2056 when signing-off

with the "Internationale" after a programme of Chinese music.

Lanchow on **4865** at 1512 with a Chinese drama production.

Radio Peking on 6645 at 1404, OM and YL in Kazakh in the Domestic Service, this programme being presented from 1400 to 1455, also in parallel on 8565.

Another late winter visitor has been Urumchi on 4970 at 1457, just audible when signing-off with the "Internationale" after the Kazakh programme.

AFRICA

African stations can be quite interesting in programme content, indeed much of the local music and orchestration is barely distinguishable from the modern U.K. pop scene! Some of the African stations are relatively easy to log whilst others are most certainly not in that category, low powers and surrounding commercial interference are, as usual, the enemies.

• ZAIRE

Lubumbashi on 4950 at 1920 with a programme of African music complete with vocals by both OM and YL. This is the Home Service, the schedule of which is from 0400 to 0700, 1000 to 1245 (Saturdays 2100), 1500 to 2100 (Sundays from 0400 to 2000). The power is 10kW. Known to "wander", I once measured this one 4751.5 kHz.

LIBERIA

Monrovia on **3227** at 0639, African music with YL's in chorus. This is Radio Station ELWA (Eternal Love Winning Africa) an evangelical broadcaster, this channel being that for local vernaculars. The schedule is from 0610 to 0800 and from 1805 to 2220, the power is 10kW.

MALAWI

Blantyre on **3380** at 0642 with a programme of local flute music. Schedule is from 0257 to 0520 and from 1700 to 2210 (from May to August 0257 to 1110 and from 1300 to 2210). The power is 100kW and that usually makes this one a fairly easy proposition.

• SENAGAL

Zinguinchor on 3336 at 1958, light music programme with announcements in French. Not so easy to receive, this one has a schedule from 0600 to 0800 and from 1800 to 0000, the power being just 4kW.

KENYA

Nairobi on **4915** at 0548, religious service in Swahili. This is the Home Service, scheduled from 0255 to 0630 and from 1430 to 2015 (Saturdays to 2115). The power is 100kW which also makes for comparative ease of reception.

• NIGERIA

Kaduna on 3396 at 0600, talking drum interval signal, 6 pips, identification in English by YL and then a newscast of local events in English by OM. The talking drum interval signal must be heard to be believed — incredible! During the war with Biafra we often logged this interval signal prior to the news in English and the exhortation "There's a job to be, done, the war must be won."

Ibadan on 3204 at 0625, religious service in

Yoruba. I logged the service the schedule tells me it is in Yoruba! Not so easy to log, Ibadan has a schedule from 0430 to 0730 and from 1430 to 2305 and the power is 10kW.

MALAGASY

Tananarive on **3287** at 0615, recording of local pops. Schedule is from 0230 to 0500 and from 1430 to 1930 (Home Service 1). The power is 4kW.

• **BURUNDI**

Bujumbura on **3300** at 0415, typical African music with YL's in chorus. This is the Home Service 1, scheduled in French and vernaculars from 0330 to 0600 (Sundays to 2100) and from 1600 to 2100. The power is 25kW but this doesn't make it an easy one to receive — the surrounding interference takes care of that!

• NIGER

Naimey on **3260** at 0602, OM with a local newscast in French. Schedule is from 0530 to 0630, 1700 to 2200 (Saturdays from 1700 to 2200 and from 1500 to 2300, Sundays from 1700 to 2130). The power is 4kW.

From all of which may be deduced that one of the best times to listen for those elusive and not so elusive African stations is around 0600 or so.

LATIN AMERICA

Changing the target area and aiming for stations in this part of the world why not set your sights on the rarely reported Voz de los Caras?

• EQUADOR

Voz de los Caras, Bahia de Caraquez, logged at 0418 with a programme of a particular local style of music in which only a guitar and drum are used, this following a clear station identification by OM announcer. We measured the frequency as **4794.5** but Voz de los Caras has been known to drift between the limits **4792** to **4796**. Like the frequency, the schedule can also vary but in general it is from 1100 to 0500.

also vary but in general it is from 1100 to 0500. Radio Cenit, Portoviejo, on a measured **4772** at 0430, local music and songs prior to identification, the National Anthem and sign-off.

Radio Popular, Cuenca, on **4800** at 0618 and still at good signal strength with songs in Spanish after identification.

BOLIVIA

Radio Universo, La Paz, on 5005 at 0425, records of dance music in Euro-style and announcements in Spanish.

• HONDURAS

Radio Progresso, El Progresso, on **4920** at 0440, YL with songs, guitar solo. The evening schedule is from 2200 to 0500 and the power is 10kW.

• DOMINICAN REPUBLIC

Radio Clarin, Santo Domingo, on **4850** at 0434, OM with clear identification then into programme of local songs. Schedule is from 1000 to 0415, obviously on an extended transmission period on this occasion — a practice common with Latin American stations.

• BRAZIL

Radio Gazeta de Alagoas, Meceio, on a measured 3326.2 at 0400, local music and songs then clear identification and sign-off without National Anthem.



I.C. PLI RECI

By A

This is an easily constructed receiver intended for reception on the medium wave band. Its output may be coupled to an earphone or to its own internal loudspeaker. The power is provided by two 1.5 volt HP7 cells in series, from which the current drain is approximately 12mA. In consequence the power input to the receiver is only 36mW and this fact, combined with the use of a very simple Class A audio output stage, limits the output power available for the speaker. However, modern miniature speakers have quite reasonable efficiencies, and the speaker volume should be adequate for bedside listening or for listening in quiet surroundings.

A compact layout incorporating standard components is employed, and the prototype receiver is housed in a case measuring some 155 by 85 by 40mm. (6.1 by 3.3 by 1.6in.). The size could be substantially reduced by the use of sub-miniature components, but this would make construction difficult for the beginner, to whom the receiver will probably have greatest appeal.

THE CIRCUIT

The receiver has an internal ferrite rod aerial, this coupling to an integrated circuit type ZN414 which provides r.f. amplification, detection and automatic gain control. The ZN414 is followed by a 2-transistor a.f. amplifier, in which the second transistor appears in the Class A output stage. The complete circuit is given in Fig. 1.

As can be seen from this diagram, the ZN414 has three lead-outs only, and in fact it has the same size can as a TO18 transistor. Lead-out 3 connects to the lower negative supply rail, whilst lead-out 2 couples to the ferrite rod aerial coil, L1, and its tuning capacitor, VC1. Lead-out 1 provides a detected a.f. output, with R3 functioning as the output load resistor. The supply current required by the integrated circuit also passes through this resistor. The input at lead-out 2 has a high impedance, and the ferrite rod aerial coil can be connected directly to this point without the need for a low impedance coupling coil. A bias current for the i.c. input is provided via R1, and C1 bypasses the earthy end of the tuned circuit given by L1 and VC1 to the lower supply rail at radio frequencies. A simple design offering recept supply demands are very modest earphone or to its own loudspeal



Fig. 1. The circuit of the 'I.C. Plus Two' receiver.

'I.C. PLUS TWO' RECEIVER

By A. P. Roberts

A simple design offering reception on the medium wave band. Battery supply demands are very modest and the receiver offers an output to an earphone or to its own loudspeaker at a low level for bedside listening.



Fig. 1. The circuit of the 'I.C. Plus Two' receiver. This operates from the low supply voltage of 3 volts

RADIO & ELECTRONICS CONSTRUCTOR

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COMPONENTS

Resistors (All fixed values miniature 1 watt 10%) R1 100k Ω R2 2.2k Ω R3 680 Ω R4 100 Ω R5 1.2M Ω R6 3.9k Ω R7 56k Ω VR1 5k Ω potentiometer, log Capacitors C1 0.1µF type C280 (Mullard) C2 0.1μ F type C280 (Mullard) C3 0.01μ F type C280 (Mullard) C4 6.8μ F electrolytic, 10 V. Wkg. C5 0.22μ F type C280 (Mullard) C6 4 μ F electrolytic, 10 V. Wkg. C7 0.1 μ F type C280 (Mullard) C8 100 μ F electrolytic, 10 V. Wkg. CX 0.047 μ F type C280 (Mullard) VC1 208pF variable air-spaced (see text) Inductors L1 Ferrite aerial coil (see text) T1 Output transformer type LT700 (Eagle) Semiconductors **IC1 ZN414 TR1 BC109C TR2 BC109C** D1 0A200 D2 OA200 Switch S1 d.p.d.t. slide Socket JK1 3.5mm. jack socket with break contact Speaker LS1 3 Ω or 8 Ω speaker, 64mm. (2.5in.) round Miscellaneous Plastic or wooden case (see text) Battery holder type BH.2 (Eagle) 2-off HP7 cells Battery connector 2-off control knobs Ferrite rod, 95 x 9.5mm. (see text) Veroboard, 0.1in. matrix Speaker fabric 34 s.w.g. wire, enammelled, d.c.c. or d.s.c. Connecting wire, etc.

The recommended supply potential, at the upper end of R3, is 1.3 volts. A voltage at approximately this level is provided by means of R2 and the stabilizing circuit given by R4, D1 and D2. The latter are two forward biased silicon diodes which each drop a steady voltage of about 0.6 volt. The total voltage across the diodes, plus an additional small voltage across R4, is then approximately 1.3 volts, as is required. C2 functions as an r.f. bypass capacitor.

AUDIO STAGES

The a.f. output from lead-out 1 of the ZN414 is applied, via C4, to the volume control VR1. The signal tapped off by the slider of VR1 is then passed by way of C5 to the base of TR1, which provides most of the a.f. voltage gain in the receiver. It is connected in the common emitter configuration and has R5 as its base bias resistor and R6 as its collector load resistor. C7 filters out any residual r.f. signal which is still present. C6 couples the a.f. signal from the collector of TR1 to the base of TR2 in the output stage.

TR2 is also connected in the common emitter mode, with R7 as its base bias resistor. The collector load is given by half the primary of T1. This transformer is used to match the output impedance of TR2 to the lower impedance of the speaker. It also serves to isolate the speaker from the standing direct current in TR2 collector circuit.

Jack socket JK1 has a break contact which cuts out the speaker when the earphone plug is inserted.

The capacitor shown as CX may be required in order to prevent instability at high volume control settings, and this point is discussed more fully later on. C8 provides supply decoupling, and S1 is the on-off switch.

COMPONENTS

Most of the components are standard readily obtainable items, but a few require some comment.

A manufacturer's surplus air-spaced capacitor was used for VC1 in the prototype, and any reasonably small component having a maximum value of 208pF or a little more may be employed here. An air-spaced capacitor is preferable to a solid dielectric type. A single gang Jackson type 01 capacitor with a value of 208pF is listed by Home Radio and this would be suitable.



Looking into the receiver from the rear. The layout is compact without undue crowding of parts



Fig. 2. Details of the ferrite rod aerial winding

The two HP7 cells are retained in an Eagle BH.2 battery holder, or similar, in which they are fitted side by side. The holder is provided with snap terminals. It is available from several suppliers, including Henry's Radio.

The ferrite rod in the prototype had a length of 95mm. $(3\frac{3}{4}in.)$ and a diameter of 9.5mm. $(\frac{3}{8}in.)$. It is not essential to use a rod of exactly the same length and a 101mm. (4in.) rod of the same diameter may be employed instead.

FERRITE AERIAL

The ferrite aerial coil is wound on the rod by the constructor. This is quite an easy process as only the one winding is required. The coil wire is 34 s.w.g. enamelled, d.c.c. (double cotton covered) or d.s.c. (double silk covered) copper wire, and the coil consists of 75 turns wound side by side. Fig. 2 gives details.

The winding commences 19mm. from one end of the rod, the wire at the start being secured to the rod with plastic insulating tape. The turns are then wound on as neatly as possible in a single layer, after which the winding end is secured with another piece of insulating tape. The two free wire ends should be fairly long, say about 100mm. each. They can be shortened as necessary when the coil is later connected into the receiver circuit.

COMPONENT PANEL

The small components are assembled on a piece of 0.1in. Veroboard having 28 holes by 12 copper strips. The component side of the panel is illustrated in Fig. 3.

Commence by carefully cutting out a panel of the specified size with a small hacksaw. Then drill out the single mounting hole with a No. 41 (0.096in.) twist drill or a drill of similar size. Next, make the seven breaks in the copper strips at the points listed in Fig. 3, using a Vero spot face cutter or a small twist drill.

The single link wire is fitted to the panel, followed by the resistors and capacitors with the exception of CX. The mounting lugs of T1 are bent up at 90 degrees so that the transformer can be positioned flat on the board without having to drill out holes for its lugs. One lug is bent round and under the panel edge, its end being soldered to copper strip L. The other lug may be secured to the board with a little adhesive.



Cut strips at 1-11, J-11, B-6, H-17, F-17, F-24, J-24.

Before mounting the transformer, the three primary leads are threaded through and soldered at holes F20, H20 and J20, and the two secondary leads at F25 and J25. The leads should be cut fairly short, and should be kept under, or close to, the transformer bobbin after mounting. It is in order to connect the unused primary lead at hole F20, as no other connection is made to the strip section concerned.

It must be pointed out that an output transformer other than the LT700 should not be used. The physical layout on the panel has been designed to suit this particular transformer. Also, other transistor output transformers will almost certainly have a much lower primary impedance.

Finally, wire in and solder the two transistors and the integrated circuit. The wires connecting to external components are added later.

CASE AND WIRING

A case for the receiver may be home-constructed, or may consist of a plastic case of the requisite dimensions. It must, of course, be large enough to take the components, including the speaker, and may have the general dimensions mentioned earlier.

A home-constructed case is not difficult to assemble, and it can be made up of thin plywood with simple butt joints. A neat finish is given by covering it, after completion, with one of the self-adhesive plastic materials, such as Fablon.

A metal case must not be employed as this will screen the ferrite rod aerial and prevent signal pick-up.

The general layout and interconnecting wiring of the receiver is shown in Fig. 4. S1 is mounted on the right hand side of the case, as viewed from the rear. It requires a rectangular cut-out, and this may be made with the aid of a fretsaw. Two short 6BA bolts and nuts are employed for mounting the switch. It is a standard d.p.d.t. (double-pole double-throw) type but is used here as an s.p.s.t. (single-pole single-throw) component. In consequence, connections are made to only two of its six tags.



A close-up view of the component panel

Fig. 3. The components are assembled on the Veroboard panel in the manner shown here

The aperture for the speaker may also be cut out with a fretsaw. A piece of speaker fabric is glued behind this, after which the speaker is glued, in turn, to the fabric. Take care to ensure that none of the glue is allowed to get on the speaker cone or surround. The speaker may, alternatively, be bolted in position, assuming that it has mounting holes and that the appearance of screw heads on the front panel of the case is acceptable. Make sure that there is enough space for the battery holder to fit below the speaker magnet.

Most air-spaced variable capacitors are provided with three 4BA tapped holes on the front plate for mounting. The front panel of the case is drilled with a 10mm., diameter hole for the capacitor spindle, and with three 4BA clearance holes for the mounting screws. The positions of the mounting holes may be determined by first holding a piece of paper to the capacitor front plate and marking out the holes on these. The paper may then be used in the manner of a template to mark out the corresponding holes on the case front panel. The mounting screw ends must not pass more than marginally inside the capacitor front plate as they may then damage the fixed or moving vanes. In consequence, short 4BA bolts are required, and it will be found helpful to fit a few 4BA washers over each bolt between the case front panel and the front plate of the capacitor.

The component panel fits below VC1. A piece of 6mm. plywood measuring approximately 25 by 38mm. is glued to the inside of the front panel below VC1, and the component panel is then secured to this by a small woodscrew passing through the hole at D10. A small insulating washer, or a grommet, between the panel and the plywood will ease strain on the panel, and the screw should not be tightened excessively. If the right hand edge (as viewed from the rear of the receiver) of the panel is close to or touches the speaker frame, a further spacing washer or washers may be used. Also, the appropriate surface of the speaker frame may be covered with plastic insulating tape.

VR1 and JK1 are mounted on the left hand side (again as viewed from the rear) of the case. VR1 requires a 10mm. diameter hole. Most 3.5mm. jack sockets require a 7mm. mounting hole. The jack socket shown in Fig. 4 is a type having a closed construction. If the socket to be employed has an open construction, the three leads to it will conrect to its tags as indicated in the inset diagram, the letters X, Y and Z corresponding to the similarly designated wires in the main diagram. The tag layout in the inset is that encountered with standard jack sockets; if any doubt exists here the appropriate tags may be identified by visual inspection and the socket wired up to agree with the circuit diagram of Fig. 1.

A wooden block measuring 12.5 by 12.5 by 25mm. provides a mounting for the ferrite aerial rod. The block has a deep V-shaped groove cut, by means of a hacksaw, along the centre of one of the 12.5 by 25mm. sides. The rod is then glued into the groove and the block, complete with aerial rod, glued to the top inside





Alternative connections to JK₁

Fig 4. Layout of the parts of the receiver inside the case, together with the interconnecting wiring



Another illustration of the completed receiver

of the case. A good quality gap filling adhesive, such as an epoxy resin, is required here. L1 must not be positioned too close to the speaker magnet, or sensitivity may be reduced.

When all the components have been mounted, but before the component panel is screwed down, complete the wiring shown in Fig. 4. Apart from the ferrite aerial coil leads, all the interconnecting wiring should employ thin flexible insulated wire. The lead-outs from L1 connect directly to VC1, as shown. These connections should be of a temporary nature at this stage as it may be necessary to transpose them.

When all the wiring has been completed and checked, the component panel may be mounted. Next fit the control knobs, and connect up the battery holder with cells inserted.

ADDING CX

The receiver may now be tried out. No alignment is required as there is only a single tuned circuit.

If instability should appear at high volume settings, causing a whistle to be produced as the set is tuned across a station, the probable cause is feedback between the speaker and aerial coils. First, check whether the instability can be cleared by reversing the connections from L1 to VC1. If this does not effect a cure, further r.f. filtering in the receiver circuit can be provided by fitting CX to the component panel in the position shown in Fig. 3. There is no need to add CX unless instability at high volume settings is apparent. After this particular check has been carried out, the connections from L1 to VC1 may be made of a permanent nature.

There is a slight possibility that instability at all volume settings may occur with some specimens on the ZN414, and the cure in this case is to slightly reduce its supply voltage by replacing R4 on the component panel with a short link wire. This should only be done if the instability appears as, otherwise, sensitivity will be reduced unnecessarily.

The completed receiver is now ready for use, and the back of the case can be screwed on. As a finishing touch, 'Panel-Signs' legends (available from the publishers of this magazine) may be added to indicate control functions and to show station locations around the knob for VC1. The earphone socket can be used as an output for any of the normal types and impedances of earphone.



IN NEXT MONTH'S ISSUE

FOR 80 METRES

Part 1 (two parts)

In this ingenious receiver design an aerial input is applied direct to the product detector, a Motorola MC1496 integrated circuit. A local oscillator running at carrier frequency then enables demodulation to be given both for s.s.b. and c.w. signals. Due to this direct conversion technique there are only two tuned circuits, one operating at aerial frequency and the other at oscillator frequency. The description of the receiver will be completed in the following month's concluding article.

* * *

NICKEL CADMIUM CELL CHARGER

Rechargeable nickel cadmium cells are becoming increasingly popular in these days of rising battery costs. Because of their low internal resistance they should preferably be charged by constant current sources, and this article describes a unit which is capable of charging up to four 'AA' size nickel cadmium cells. These are similar to standard HP7 dry

* * *

OHMMETER

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AMBIPHONIC ADAPTER

Part 2

by R. A. Penfold

This concluding article completes the constructional information for the ambiphonic adapter. Also described are the processes of setting up and balancing, and of taking the left and right hand input signals from the stereo amplifier.

In last month's issue we examined the basic operation of the ambiphonic adapter, discussed its circuit and then described the first steps in construction. We now continue with the constructional details.

GENERAL LAYOUT

The general layout of the two printed boards, the mains transformer and other components in the adapter can be seen in the photographs. The positioning of the parts is not unduly critical, but, in the interests of obtaining a low hum level, it is best to mount the transformer as far to the left of the chassis as possible and to have the amplifier board at the extreme right of the chassis.

The amplifier board is illustrated, actual size, in Fig. 6, and this diagram may be traced. Note that VR1 and VR2 are miniature 0.1 watt skeleton potentiometers having 0.2in. (5.1mm.) spacing between the two track tags, with the slider tag 0.4in. (10.2mm.) from a line drawn between the track tags. There are two 6BA clear mounting holes in the board, and these may be used to mark out the corresponding 6BA clear holes in the chassis. The board is mounted, later, with these holes to the right on the chassis. 6BA 1in. bolts are employed for this mounting, with $\frac{1}{2}$ in. metal spacers on them to keep the board underside spaced away from the chassis surface. The board takes up its chassis connection by way of these spacers. There are a number of thin flexible flying leads

There are a number of thin flexible flying leads from the board and these may be cut a little longer than is required, being shortened as necessary when they are finally connected to the external components. Components in the right rear channel are identified by the suffix letter "a", as was explained last month. The board is not finally mounted yet. Most of the power supply components are assembled on a second printed board and this is shown in Fig. 7. Again, the diagram is reproduced actual size. The miniature skeleton potentiometer, VR6, has the same tag spacing as VR1 and VR2. There are two 6BA clear mounting holes, which

There are two 6BA clear mounting holes, which may be used for marking out the corresponding holes in the chassis. When mounted, the board has these two holes to the right. Metal spacers are employed to space off the board from the chassis so that the mains lead can pass underneath it. As with the amplifier board, the power supply picks up its chassis connection via these spacers.

The flying leads from the board are made a little longer than necessary, being cut down as required when they are connected. The three leads to the mains transformer secondary are identified to agree with the circuit of Fig. 4 (published last month). The actual transformer tags to which these leads connect were described in Part 1. The printed board is not mounted at this stage.

TRANSISTOR TR3

Transistor TR3 is mounted with its body under the chassis, which acts as a heatsink. Details of the connections to this transistor are given in Fig. 8. The transistor is insulated from the chassis by means of a mica washer and two insulating bushes in the usual manner. The mica washer may initially be employed as a template for marking out the four holes required, and these must be drilled out cleanly with no burrs on the hole edges. A continuity tester or ohmmeter is employed to ensure that the transistor body and its lead-outs are fully insulated from the chassis. If they are not, the power supply can be short-circuited with consequent damage to components.

A solder tag is secured above the chassis at each mounting bolt of transformer T1. The mains earth lead is connected to the left hand tag, and the tone and volume control wiring is earthed to chassis at the right hand tag. The live and neutral mains leads connect to the primary of T1 via switch S1 in the manner shown in Fig. 4.



Fig. 6. Component and copper sides of the amplifier printed board. This is reproduced full size and may be traced





Fig. 7. Details of the board on which the smaller power supply components are assembled. This is also reproduced full size



The chassis as seen from the amplifier board end

Fig. 8. The connections to transistor TR3



Fig. 9. The wiring of the components in the volume and tone control network for one channel. The other channel is connected up in the same manner

The remaining components are wired directly to the volume and tone controls in the manner illustrated in Fig. 9. This shows the wiring for the left rear channel only, the wiring for the right rear channel being essentially the same. The wiring is quite straightforward and should present no problems.

The interconnecting wiring between the two boards and to the volume and tone control networks may now be completed. The connections to the input socket and speaker sockets may also be wired in, the requisite chassis connections being made at the sockets themselves. The non-earthy left and right hand inputs are connected to two pins of the 5-way DIN socket. None of the a.f. wiring needs to be screened but the leads should be kept reasonably short and direct.

When all the wiring has been completed, the two printed boards may be finally mounted on the chassis. Next, after a careful visual check for wiring errors, connect a testmeter switched to a suitable volts range between the emitter of TR3 and chassis, switch the adapter on and adjust VR6 for a reading of 16 volts in the meter.

ADJUSTMENT

Ideally, the adapter shold be fed from the 'Tape' or 'Aux' output of the stereo amplifier, and any such output that will provide 100mV or more into about $20k\Omega$ is suitable. In case of doubt, the availability of a suitable output can be checked from the manufacturer's literature for the amplifier. It is regretted that, owing to the very wide range of stereo equipment which is currently available, it is impossible for the writer or the staff of this journal to advise on the output facilities offered by any particular make and model of stereo amplifier. In the absence of a low level output it is, in any case, possible to obtain a suitable input for the adapter from the amplifier speaker terminals, and the procedure required here is discussed later.

VR1 and VR2 must be adjusted to ensure that the adapter is not overloaded and also to provide balanced inputs. Connect the unit to the stereo amplifier by way of screened leads and plug an 8Ω speaker into each of the adapter output sockets. Set VR1 and VR2 to a roughly central setting and switch the adapter on.

Put the volume controls VR3 and VR3a at maximum then, keeping VR1 and VR2 approximately in step, adjust these so that it is possible to obtain full output from the adapter without major overloading occurring on volume peaks. Note that VR2 is adjusted in an anti-clockwise direction to increase volume, whereas VR1 is adjusted in a clockwise direction for increased volume.

The inputs are then balanced by playing a mono programme or recording through the system. Either VR1 or VR2 is then adjusted for minimum output from the rear speakers. If the input to the adapter is taken from the speaker outputs of the stereo amplifier, it is absolutely essential that the balance control of the amplifier be set correctly before the inputs to the adapter are balanced.

Once the input balancing procedure has been carried out, the adapter may be switched off and the outer casing screwed on. The adapter is then ready for use.

SPEAKER PHASING

In order to obtain the best results from the adapter it is essential that the rear speakers have correct phasing. The two front speakers need the same phasing as for ordinary two channel stereo reproduction, and so will already be correct in this respect.

If the rear speakers are obtained as a stereo pair they should be connected with the same polarity to their plugs. Therefore, provided the two adapter speaker sockets are wired with the same polarity (i.e both flat connectors or both round connectors wired to chassis) of the two possible ways of connecting the rear speakers, one must be correct. The phasing of the speakers can be altered by transposing their connections but, since the outputs of the adapter are in antiphase, a much simpler method consists of simply changing over the speaker plugs in the two adapter speaker sockets. Should this result in what has been referred to in this article up to now as the left rear socket feeding the right rear speaker, and vice versa, all that has to be remembered is that the upper volume and tone controls now apply to right rear instead of to left rear.

When the speaker phasing is correct sounds from the two left hand speakers should blend well together, as should those from the two right hand speakers. When the phasing is incorrect diagonally opposite speakers will blend well together, and this will result in much of the sound seeming to originate from just above the listener's head. A little experiment should



TR3 is mounted under the chassis, which functions as a heatsink

soon reveal the correct method of connection for the rear speakers.

Since the front speakers are reproducing sounds which would come from relatively low down in a concert hall, and the rear speakers are producing sounds which would normally come from comparatively high up, the system will usually sound most convincing with the front speakers on the floor and the rear speakers elevated above head height. This gives a form of three-dimensional sound reproduction.

Improved performance may also be obtained by turning the rear speakers to face the rear wall of the room. The purpose of this is to diffuse the ambience. As treble frequencies tend to be lost during the process of being reflected around a hall to a greater extent than middle and bass frequencies, greater realism may be given by introducing a certain level of treble cut to the rear channels. There is plenty of scope for experiment here, and it is largely a matter of individual taste as to what is considered to produce the most acceptable results.

SPEAKER OUTPUTS

If the stereo amplifier is not fitted with a "Tape' or 'Aux' socket which can be coupled direct to the adapter, the adapter inputs can, as already mentioned, be taken from the speaker outputs of the stereo amplifier. It is necessary to provide input attenuators as, otherwise, it will be very difficult to set up VR1 and VR2.

When the stereo amplifier outputs both have one terminal connected to chassis, the requisite attenuators required are as illustrated in Fig. 10(a). The non-earthy terminal of each stereo amplifier speaker output connects to the upper end of the $39k \Omega$ resistor in each attenuator.

If the stereo amplifier speaker outputs do not have one terminal at chassis potential, additional 1μ F capacitors are added, as in Fig. 10(b). These capacitors block any direct voltages which may be present at the stereo amplifier speaker outputs. The attenuator components of Figs. 10(a) or (b) may be mounted inside the adapter on a small tagstrip positioned near the 5-way DIN socket.

FINAL POINTS

It is not really necessary to have rear speakers of equal quality to those employed for the front channels. The author, for instance, found results were perfectly satisfactory when using two-way speaker





Fig. 10(a). If necessary, the left and right hand inputs for the adapter may be obtained from the stereo amplifier speaker outputs. Attenuators are required in each channel, as shown here (b). Should the stereo amplifier outputs not have one terminal connected to chassis, isolating capacitors are added to block any direct voltages which may be present

systems at the front and dual cone speakers at the rear.

Apart from adding ambience to material produced in a concert hall, the ambiphonic system can make an improvement to the effectiveness of other types of music. A great deal of pop music is embellished with special phasing effects and, as might be expected, these can produce very interesting results when played over equipment of the type which has been described in these two articles.

(Concluded)

BACK NUMBERS

For the benefit of new readers we would draw attention to our back number service.

We retain past issues for a period of two years and we can, occasionally, supply copies more than two years old. The cost is the cover price stated on the issue, plus 11p postage.

Before undertaking any constructional project described in a back issue, it must be borne in mind that components readily available at the time of publication may no longer be so.

We regret that we are unable to supply photo copies of articles where an issue is not available. Libraries and members of local radio clubs can often be very helpful where an issue is not available for sale.

New Products

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uses in electronics.

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ADD-ON

A simple design which enables the output of an f.m. turner or the signal level in an a.f. amplifier to be monitored in terms of volume units.



When making recordings from the radio it is not easy to find the correct settings for the recording level control or controls without some indication of the modulation level being used at the transmitter. This is because the transmitter is lightly modulated for most of the time, with the modulation level only approaching 100% on occasional crescendos. By fitting a VU meter (volume units meter) to the

By fitting a VU meter (volume units meter) to the tuner it would be possible to adjust the recording level meter or meters to match the reading on the VU meter, and so ensure that the correct recording level is used. Unfortunately, though, few tuners are fitted with a VU meter.

The VU meter which forms the basis of this article can prove to be a very worth-while addition when making recordings. The device is constructed as a selfcontained add-on unit, and so it is not necessary to make any connections to the tuner before connecting the meter to it. The meter may also, of course, be employed for indicating volume units in applications other than at the output of a tuner. It is housed in a ready made aluminium case which measures approximately 4 by 2³/₄ by 1¹/₄in. It is battery powered, and its low current consumption of about 2.2mA only from a PP3 battery ensures economy of operation.

R.M.S. OR PEAK READING?

There are two types of VU meter, namely the r.m.s. and peak reading types. As one might expect, the r.m.s. type indicates the relative r.m.s. level of the signal, while a peak reading type has a fast attack and a slow decay, so that the meter shows the relative peak level of the signal. Whilst it is true that the peak reading meter has certain advantages over the r.m.s. type, this circuit is for an r.m.s. meter. Most recorders are fitted with an r.m.s. recording level meter, and it is an obvious advantage to have the same type of meter as is fitted to the recorder.

Resistors (All fixed values + watt 10%)	
R1 4.7k Ω	
$\frac{\mathbf{K}2 \ \mathbf{I}\mathbf{K}\mathbf{\Omega}}{\mathbf{R}3 \ \mathbf{15k}\mathbf{\Omega}}$	1
R4 560k Ω	
$R5 2.2k\Omega$	
$R6 2.7 k \Omega$	
VR1 500k Ω pre-set potentiometer.	miniat
horizontal 0.1 watt (see text)	

ure

COMPONENTS

Capacitors

C1 4.7 or 5μ F electrolytic, 10V Wkg. C2 16μ F electrolytic, 10V Wkg. C3 47 or 50μ F electrolytic, 6V Wkg. C4 16μ F electrolytic, 10V Wkg.

Transistors TR1 BC109 TR2 BC109

Meter

M1 VU meter, 59 x 46 x 35mm. (see text)

Switch

S1(a)(b) d.p.d.t. slide switch with centre "off" (see text)

Miscellaneous

Aluminium box type AB9, 4 x 2³/₄ x 1¹/₂in. 9 volt battery type PP3 (Every Ready) Battery connector Veroboard, 0.1in. matrix. Stereo screened lead Grommet, nuts, bolts, etc.

METER

By P. R. Arthur



THE CIRCUIT

The complete circuit diagram of the add-on VU meter is shown in Fig. 1, and it consists basically of a two transistor amplifier feeding the VU meter movement. The meter movement has an integral rectifier circuit and a series resistor. It is calibrated to take into account the non-linearity of its rectifier circuit and so no overall negative feedback is applied as would be necessary with an ordinary a.c. millivoltmeter.

As the output from most tuners is at a fairly high level, say about 200 to 600mV, and the meter requires about 1.2 volts for a reading at the zero reference level, the amplifier does not need a very high voltage



Fig. 1. The circuit of the VU meter. A simple two transistor amplifier with controlled voltage gain is incorporated gain. On the other hand, if inaccuracies are to be avoided it must have a flat frequency response over the audio frequency spectrum and offer low distortion. Also, if the supply voltage is unstabilized, it must have a gain which is virtually unaffected by variations in supply potential. A further requirement is a reasonably high input impedance, so that the VU meter places a minimum of loading on the equipment to which it is coupled. All these factors are achieved in the present circuit, which incorporates an amplifier having a high level of negative feedback.

Referring to Fig. 1, both transistors are in the common emitter mode, and the signal at the collector of TR1 is directly coupled to the base of TR2. R1 is the collector load resistor for TR1, and R5 the collector load for TR2. R6 is the emitter bias resistor for TR2, with C3 as its bypass capacitor.

The emitter of TR1 is connected to a potential divider, R3, R2, between TR2 collector and the negative rail. This provides the required negative feedback, and the values of R2 and R3 decide the voltage gain of the amplifier. This is given approximately by the sum of R2 and R3 divided by R2. The voltage gain, in consequence, is approximately 16 times.

VR1 functions as a sensitivity control. C1 and C4 are input and output d.c. blocking capacitors respectively, whilst C2 is the supply bypass capacitor. R4 is



All the components appear at the rear of the front panel



The Veroboard panel is mounted between the meter movement and the slide switch

the base bias resistor for TR1, being returned to the emitter of TR2. This bias circuit is very stable due to the high level of d.c. feedback employed.

S1 is a d.p.d.t. slide switch having a central off position. One pole of this connects either the left hand or the right hand channel to the input of the device. The other pole is used to switch the positive supply. The author obtained both this switch and the VU meter movement from M. Dziubas, 158 Bradshawgate, Bolton, BL2 1BA.

The meter movement has dimensions of 59 by 46 by 35mm., and is referred to as a "59mm. VU meter".

CASE DRILLING

The case in which the unit is housed is an aluminium box type AB9. This has a removable lid which is used as the front panel. The drilling and cutting out required for this panel are shown in Fig. 2.' The large cut-outs for the meter and S1 can be

The large cut-outs for the meter and S1 can be made with a fretsaw or coping saw, preferably one fitted with a fine toothed blade. The smaller mounting holes for these two items are made with a No. 31 twist drill, and their positions can be located with the aid of the meter and switch after the large cut-outs have been made. A solder tag is fitted under the lower left mounting nut of the meter, as seen from the rear. The hole for the input cable is fitted with a grommet.



Fig. 2. The holes required in the front panel. The 4in. and 2³/₂in. dimensions are nominal

ELECTRICAL ASSEMBLY

The small components are mounted on a Veroboard panel of 0.1in. hole matrix having 20 by 10 holes. There are no breaks in the copper strips, which run lengthwise.

The component layout on the panel is illustrated in Fig. 3. From this it will be seen that VR1 is a miniature horizontal skeleton pre-set potentiometer having 0.2in. spacing between its track tags, and 0.4in. spacing between the slider tag and a line drawn between the track tags. All the fixed resistors and capacitors are mounted vertically. Because of this it would be advantageous to employ printed circuit type capacitors, with both lead-outs at one end of the body. This is not essential, however, and capacitors with axial lead-outs can alternatively be employed, one leadout being bent down to run alongside the capacitor body.

Fig. 3 also shows the wiring external to the Veroboard. As can be seen from the accompanying photographs, the board is positioned between S1 and the meter. There are two leads from the board to S1, and another two leads from the board to the meter. These consist of a heavy gauge single strand wire (around 16 s.w.g.) covered with sleeving, and they provide the mounting for the Veroboard. The four leads should be kept as short as possible. They should be soldered to the appropriate points on the board after all the other components have been fitted, and should initially be cut to a more than adequate length. They are then cut to the required length just before soldering to S1 and the meter.

The input lead is stereo screened cable with the braiding connected to the earthy meter tag. Its length can be as required and its free end is terminated in a plug or plugs to suit the particular equipment with which the unit is to be used.

There is space for the PP3 battery below the meter. Some foam rubber or plastic may be glued to the inside rear of the case to hold the battery in position when the lid is screwed on.

SETTING UP

The VU meter unit is connected to the equipment being monitored in the most convenient manner available. If the equipment is a tuner having only a single ouput socket, the unit will need to be connected to a single plug in parallel with the recorder input. However, some tuners have additional outputs marked as "Tape", "Aux.", etc., and one of these, if not in use, will probably prove to be suitable.

The only adjustment needed is the setting up of the sensitivity control, VR1. A convenient approach consists of taking advantage of the B.B.C. test transmissions which are sent out from Radio 3 stereo transmitters after the close of programmes on Monday and Saturday evenings. The first test consists of a 250Hz tone in the left hand channel and a 440Hz tone in the right hand channel, each at 40% of maximum modulation prior to pre-emphasis at the transmitter. VR1 is first set to minimum sensitivity (slider fully anti-clockwise) and, with the test transmission accurately tuned in, is adjusted to give a reading of 40% in the meter on either channel. The subsequent tests in the transmission are ignored. Since all B.B.C. transmitters operate to the same standard and since limiting action in conventional f.m. receivers should produce the same audio level for any reasonably



Fig. 3. Layout of components on the Veroboard panel. Also shown is the wiring outside the panel

strong signal, the adjustment will hold good on other B.B.C. stations.

Most stereo decoders have outputs which are closely matched and so, with the unit calibrated for one channel, it should be accurate on the other channel. If there should happen to be a marked discrepancy, then a $100 k\Omega$ pre-set variable resistor can be connected between the input lead for the channel with the greater output and the appropriate tag on S1. The variable resistor may be positioned inside the unit. The unit is then set up on the channel with the lower output, after which the additional pre-set resistor is



Another view of the interior of the unit

adjusted to give the same reading on the other channel.

OTHER USES

If desired, the VU meter unit may be built in a mono version. In this case a single screened input wire is required, this connecting direct to VR1. The 3-way slide switch is replaced by a standard slide switch connected in the positive supply circuit, and which merely functions as an on-off switch.

Another use would be as a VU recording level meter for a tape recorder fitted with a less satisfactory form of level indicator, such as a miniature moving-coil meter or a Magic Eye. In these instances the input to the unit can be taken from a suitable point in the recorder amplifier, probably at the point which feeds the existing indicator circuit. The unit must not be employed with any mains powered equipment which is not fully isolated from the mains supply by a double-wound mains transformer.

If the unit is used as a recording level meter, VR1 is adjusted to read zero VU when the level indicator on the recorder registers the maximum permissable recording level.

No means of measuring the battery voltage is incorporated. The current consumption of the unit is so small that, with normal use, the battery can simply be replaced at about three month intervals.

EDITOR'S NOTE

The outputs of some f.m. tuners contain a small level of the 19kHz pilot tone and its harmonics. No filters are provided in the simple circuit described here and the pilot tone, if present at sufficient strength, could cause inaccuracies at low VU readings, although comparable readings will still be given. This point does not arise when the VU meter is used in other applications.

SINGLE RANGE OSCILLATOR SUPERHET

Part 2

In this concluding article, details are given first of the a.f. amplifier board and then of the complete receiver assembly.

In last month's article the circuit of the receiver was described, as also were the winding modifications for the aerial coil and the construction of the mixer board and the i.f. amplifier. Next to be dealt with is the a.f. amplifier board.

A.F. BOARD

The, a.f. board is illustrated in Fig. 8. The components are assembled on a piece of plain 0.15in. Veroboard having 10 by 19 holes. First, two holes are drilled out 6BA clear to take the two 6BA screws shown. These screws are 1in. long and solder tags are secured under their nuts in the manner illustrated. The projecting parts of the screws will be employed later for securing the board to the chassis.

Wiring is carried out in the same way as for the mixer board. All leads on the underside should be kept close to the board and sleeving should be fitted where necessary. The lead from R13 in the i.f. amplifier is connected to the board just before the latter is mounted. Flying leads from the a.f. board later connect to the output jack socket, to battery positive and to S2 and VR1. R14 is not mounted on the board but appears externally between the slider of VR1 and C9. The appropriate lead of C9 is bent up so that R14 can be soldered to it later.

CASE ASSEMBLY

The case is a "Universal Chassis" measuring 10 by



Looking at the receiver from the rear with the back panel removed. The battery fits on the shelf between the i.f. amplifier assembly and the case side

By F. G. Rayer

6 by 4in. This is shown in the Components List (which appeared last month) broken down into its constituent parts, these being two 10 by 4in. members, which form the front and rear panels, two 6 by 4in. members and a 10 by 6in. metal plate. The "Hardware Kit" which also appears in the Components List, consists of the screws and nuts required for the assembly of a "Universal Chassis".

The two 6 by 4in. sides go outside the front and rear panels, thereby enabling a 10 by 3in. member to be fitted internally and act as a shelf supporting the i.f. amplifier, the a.f. board and the battery. The front panel should be drilled out first before

The front panel should be drilled out first before any assembly work is carried out. The spindle of VC2 is positioned centrally, 14 in. up from the bottom edge. It is mounted by three 4BA bolts which pass through the front panel into tapped holes in the front plate of the capacitor. The bolt ends must not pass beyond the front plate or they may damage the capacitor vanes. In consequence the bolts should be short, and spacing washers may be fitted between the panel and the capacitor front plate. Holes are also required for the tuning drive and its cursor, and these are drilled according to the instructions provided with the drive.

The lower edge of the drive scale is below the bottom of the front panel by about $\frac{1}{2}$ in. and so it is necessary to raise the case to provide clearance. With the prototype a strip of wood 10 by $\frac{3}{4}$ by $\frac{3}{4}$ in. was affixed under the front panel. An alternative approach, which may be used if a second 10 by 6 in. metal plate is attached to the case bottom, is to fit four rubber feet of suitable dimensions.

VC1 is mounted to the left of VC2 and VR1 to the right. Their spindle centres are both 2in. from the bottom of the panel and horizontal spacing is as indicated in Fig. 9. Slide switch S1 is mounted immediately below VC1, and the output jack immediately below VR1. Both are §in. above the bottom of the panel.

The use of a slow motion drive for VC1 is optional. This capacitor is manufactured with a normal spindle or with a spindle incorporating a slow motion drive, although the latter may be difficult to obtain from retail sources. If the standard capacitor without slow motion is used it is mounted to the front panel in the same way as VC2 using three countersunk bolts. The slow motion type has a longer spindle and can be set back by mounting it with $\frac{1}{2}$ in. countersunk bolts, each with two nuts, as in Fig. 9. If a 365pF capacitor with integral slow motion drive cannot be obtained, Home Radio list a 208+176pF capacitor type "00" with slow motion. This could be used instead with both sets of fixed vanes connected together to give a maximum capacitance slightly in excess of 365pF.

A small Perspex cursor with a radial line scratched on it can be affixed to the shaft of VC1 by drilling a





mc-chassis connection

Fig. 8. The component and wiring sides of the a.f. amplifier board

hole in it for a grommet which is a tight fit on the shaft (the slow rotating shaft with the slow motion version). A $1\frac{1}{2}$ in. diameter scale is fitted to the panel behind the cursor.

A rectagular slot can be made for S1 by drilling a few small holes close together then finishing with a small file. The holes for VR1 and the output jack may also be drilled.

The two side pieces may now be secured to the front panel. The left hand side piece requires two small holes for insulated aerial sockets, these being near the position to be taken up by VC1. It also has an insulated mounting, which may be home-constructed from plastic clips or similar, for the telescopic aerial. The aerial can be any type having an extended length of 30in. or more. Further required on the left hand side member is a hole for an earth socket.

The 10 by 3in. chassis member which forms the internal shelf is next fitted between the two side pieces. This takes up the position shown in the photographs and should be set back sufficiently to clear the mixer board. The i.f. amplifier will be mounted on this shelf by two 4BA bolts and nuts with its Veroboard component panel to the front. There should be room on its right hand side for the a.f. board. Three holes are needed in the shelf immediately below the i.f. transformers to allow access to their cores.

The a.f. board will be fitted to the shelf with C9 at the front. Extra nuts on its two 6BA bolts give clearance from the shelf. The two 6BA clear holes needed in the shelf may now be drilled.

INTERCONNECTIONS

Assembly is simplified if the rear panel is not fitted until later. The front panel components may next be fitted. The lead from the aerial coil to VC1 fixed vanes, and the leads to VC1 moving vanes and S1 may now be connected. The i.f. panel is next fitted, the leads from the mixer board to IFTI and the positive supply being connected. These two leads pass through the hole in the shelf under IFTI. Finally, the a.f. board is mounted, this taking up the positive supply lead from the i.f. amplifier.

Fig. 9 shows the interconnections between sections. The two output leads from the a.f. board pass under the board to the jack socket. R14 is connected between the slider of VR1 and C9, and the other wiring to VR1 and S2 is completed as shown. The battery



Fig. 9. Illustrating the interconnections between the sections of the receiver

connectors should be insulated or taped so that they cannot short-circuit to the case metalwork.

The lead from pin 9 of the aerial coil on the mixer board is taken to one of the insulated aerial sockets, this corresponding to socket A1 in Fig 1 (published last month). Trimmer TC1 connects between the left hand fixed vane tag of VC1 and the remaining aerial socket, which now becomes socket A2. The earth socket can be connected to any convenient chassis point.

The rear panel can be fitted when wiring is completed, or left until the receiver has been tested. The same applies to the case top, which is secured with self-tapping screws. There is no real need to enclose the bottom of the case, but another 10 by 6in. metal plate can be used here, if desired.

AERIALS

The telescopic aerial will give reception without the need for an external aerial-earth system. A short length of flexible wire connected to the telescopic aerial is terminated in a plug which can be fitted to socket A2, or removed if a wire aerial is to be plugged in here.

An external aerial is normally plugged into socket A1, but it may instead employ the A2 socket if it is not very long. A long aerial at this socket will cause VC1 tuning to be very flat unless TC1 is set to nearly minimum capacitance. The effects of aerial loading will soon become clear. In general a loose coupling, with the aerial at socket A1 or at A2 with TC1 giving a low capacitance, should be used if this gives enough signal strength.

When an earth connection is available it can be expected to increase the volume of weak signals.

ADJUSTMENTS

The oscillator coverage should be suitable if the 6BA core screw of L7 has 15 threads projecting, but it can be modified by screwing the core in or out. This will have considerable influence on the receiver coverage given by VC2.

A small adjustment of some of the i.f. transformer cores may be needed for the best possible results. The adjustments should be made with a correct trimming tool, such as the Denco type TT5, or the cores may break. Carefully tune in a stable signal, preferably one which gives a low output volume with VR1 well advanced (the aerial can be removed to provide this) and turn each core a little one way or the other for best volume.

It will be found that some short wave signals can be received with VC2 at two widely separate settings. This arises from the way in which the circuit operates, as was described last month. But on the l.f. band the oscillator frequency is above the signal frequency at all times.

Any loudspeaker from 8Ω to 75Ω may be used, an impedance of 15Ω giving best results. Battery drain is lower with a high speaker impedance. With headphones, the falling off in volume encountered with higher impedance speakers is not of importance, and phones of up to 500Ω to $2k\Omega$ will operate satisfactorily. A full headset is recommended and not a single earpiece. Crystal earphones cannot be used.

A PP9 battery is suitable. Current consumption is around 8mA with no signal tuned in or when operating at low volume. Current peaks of 20 to 40mA occur when operating a 15Ω loudspeaker at ample volume.

(Concluded)



This month Smithy the Serviceman takes his assistant on a tour of some of the more illogical premetrication units of length. But this provides only a background to their main discussion: a review of the latest hints received from readers.

"Ah well," said Smithy cheerfully, "I've got an exceedingly technical job to do when I get home this evening."

He raised his disgraceful tin mug to his lips and drank deeply. The crumbs around his feet gave evidence of the lunch he had just consumed. His assis-

looked up at him and swallowed. "Oh yes," he said. "And what's that?"

"I'm adding an extension to our front door bell," replied Smithy. "I can never hear the darned thing if I'm working out in the back." "Blimey," remarked Dick. "You'll

need a circuit diagram and instruc-tions for a project like that." "I think I'll get by," chuckled

Smithy. "However, you could do me a favour when we start work again. There's a drum of cheap low voltage twin flex in the spares cupboard and perhaps' you could measure off a length of it for me." "Okeydoke," replied Dick equably, as he took a last bite at his apple.

READERS' HINTS

Taking careful aim, Dick threw the apple core into the waste bin at the end of the Workshop. There was a metallic clang as it hit the side of the bin, then a rustling noise as it settled down into

the debris inside. "I wish you'd put things like that in

the dustbin outside," complained Smithy. "They encourage mice." "Mice don't eat apples," retorted

Dick. "And in any case, I don't leave half as much mess around me when I eat my lunch as you do. Look at all those crumbs around you. There's enough solid food there to provision a whole regiment of mice. How long do you want it?" "Want what?" "This bit of flex."

"Oh, that. I measured it out last

night and I'll need exactly 20 metres." "Metres?" snorted Dick in disgust. "Why didn't you do it in yards? I'm just about fed up to the teeth with the way everybody's measuring things in metres these days. Grams too, come to think of it." "Well," remarked Smithy mildly.

"We are supposed to have gone over to metrication you know.

"I was always brought up," stated Dick firmly, "to measure things in good and trusty English units. Couldn't you have thought of any units other than metres?"

"I suppose so," said Smithy thoughtfully. "Instead of 20 metres, I could for instance have said 20 million microns. Or even two hundred thou-sand million Angstroms."

Dick glowered at the Serviceman. "Trust you," he said irritably, "to make it more complicated. What I mean is, can't you express that length in proper English units?" "All right," said Smithy. "I'll see if I

can can do a conversion figure for you.

He put down his mug and pulled his note-pad towards him. There was silence for some moments as he scribbled out a calculation. With a grunt of satisfaction he underlined a final number and put his pen down again.

"Well," said Dick impatiently, "what does it come to?"

"That length of 20 metres," stated Smithy happily, "is equal to 3.98 rods!"

"3.98 what?"

"3.98 rods," replied Smithy. "Or, if you like, 3.98 poles or 3.98 perches." "Ye gods," complained Dick. "I've

never met anyone with a brain as devious as yours is." "All right," chuckled Smithy. "I'll

work it out properly for you in a moment. But, in the meantime, there's something else I'd like to mention.'

"It's the fact that we are just about due for another session on readers' hints. Quite a few have come in since the last time.

"Have they?" asked Dick, forgetting his annoyance with the Serviceman's "How about having a go at them right "How about having a go at them right now?" "That," remarked Smithy, opening a drawer in his bench and taking out a

sheaf of letters, "is precisely what I intend to do.

Dick settled himself expectantly on

his stool as Smithy took up the top letter and read it carefully. "Now here," he remarked, "is a

good one for starters. Our correspondent says that surplus and bargain offers of power transistors practically never include insulating sets for moun-ting on a heatsink. If, however, you're prepared to spend a little time at it, it's pretty easy to make up one's own insulating sets using mica obtained from an old electric iron element." (Fig. 1

(a).) "I see," said Dick pensively. "That sounds all right, but my own experience has been that mica is rather difficult stuff to handle." "It is a little," admitted Smithy.

"This letter says that the wastage rate in making the mica washers is high, and that the best tool for cutting it is a sharp pointed modelling knife with the mica placed on a flat metal surface. The mica can be cut out to cover a slightly larger area than the manufactured type would, and it doesn't have to look quite as neat. The holes for the lead-outs and mounting bolts can be cut out with the modelling knife, too. Using a drill to make the holes should never be attempted unless the mica is at least a sixteenth of an inch thick." "What about the insulating bushes?"

"Pieces of plastic insulation taken from 15 amp power cable can be used here," said Smithy. "If you strip off this insulation you get what is effec-tively thick-walled sleeving." "Wait a minute," said Dick, frow-

ning. "There seems to be a snag here. Ah, yes, I've got it! The ordinary manufactured insulating bushes have a flange which ensures that the mounting nuts, or the solder tag which con-nects to the transistor collector, cannot short to the heatsink. You can't have flanges if the insulating bushes consist

of plastic sleeving." "No problem," replied Smithy shortly. "You just use s.r.b.p. insulating washers. Or you can use another idea that's referred to in the letter. This is to cut out a narrow rectangle of printed circuit board and drill two holes in it to take the transistor mounting screws. This is fitted under the securing nuts with the copper side outwards, whereupon you connect to the collector by simply soldering a wire to the copper." (Fig. 1(b).)

DRILLING TIN-PLATE

"Stap me," said Dick, impressed. "That's a crafty scheme." "It is, isn't it?" replied Smithy, put-

ting the letter down and picking up his mug

He drank noisily, then took up a second letter. "Here," he resumed, "is one of those

simple dodges which always turn out to be so useful in practice. This letter states that, when drilling large holes in thin tin-plate for switches and control bushes, it often happens that the drill becomes jammed in the hole. The metal then gets distorted, and the

8BA screw Power transistor 6BA washer Mica Heatsink Solder tag insulated washer Sleeving Fig. 1(a). Using a homemade insulating set for mounting a power transistor. Note that a 6BA washer is employed in conjunction with an 8BA screw

> (a) 0 0 Solder joint on Copper clad laminate copper foil

(b)

LAMINATE CUTTER

Smithy took up another letter and glanced through it.

"Now I've got a really good hint here," he said. "I'll read out what the letter says. 'Recently I had to cut a piece of Veroboard into a number of different sized parts, and got together my junior hacksaw and file. Then I had a different idea. I fished out my Mason-Master Blue Flash tungstencarbide tipped laminate cutter, and tried a few strokes on a scrap piece of board. The result delighted me. My procedure now is to mark the cuts I require with a blue nylon-tip pen on both sides of the Veroboard, then cut down on both sides. The laminate cutter tip makes a V-cut of about 60 degrees, and it is soon quite easy to snap the board through. A quick wipe with the file removes any rough edges, and the fact that the tool cuts the surface layers ensures that there is no flaking of the surface, which can easily be given with the hacksaw. I use a steel rule as a guide straight-edge, and the result has a really professional finish."

Smithy placed the letter on his bench and indicated several sketches in it to his assistant. (Fig. 3(a).)

Dick looked a little blank. "I'm not quite sure," he said reluc-tantly, "what a laminate cutter is." "To be quite frank," confessed Smithy cheerfully, "I wasn't too cer-

tain myself. So I popped round to my friendly neighbourhood ironmonger's and bought a Mason-Master laminate cutter for myself to try out. It's only about 50 pence in price and it certainly does the job."

"Have you got it here now?" "Yes," said Smithy, reaching to the back of his bench. He picked up a small rectangular blue plastic case with a transparent front and passed it over to Dick. "There you are. It comes complete with instructions for cutting ordinary laminate. If you like, you can try it out on some odd bits of Veroboard when we've finished this session. You need to practice a few times to get the hang of it before you start using the cutter for a serious job."

start using the cutter for a serious job." Dick pulled the cutter out of the case and turned it over in his hands. "It looks," he remarked pensively, "as though this could be a useful addi-tion to the Workshop set of tools." "It could well be," averred Smithy. "Now there's another thing you can use it for so far as Veroboard is con-cerned and that is to cut the conner

cerned, and that is to cut the copper strips. With it, you can cut the strips either at a hole or even between holes. To my mind, the gap in the strip after a single cut has been made is rather narrow, and it wouldn't stand up to too much voltage. But you can widen the gap if you like by making several cuts. It's certainly an easier way of cutting the strips between holes than the usually advised method of using a pen-knife." (Fig. 3(b).) "Well," remarked Dick, putting the

laminate cutter back on Smithy's bench. "I've certainly learned something new today. That's a tool I hadn't realised was even in existence:"

"Good," said Smithy, pleased. "And that's precisely the reason why these hint sessions are so useful. There are always new ideas coming up and these will inevitably be of benefit to other people provided they can hear about them. Now, there's another hint in this letter and it concerns the fitting of d.i.l. integrated circuits to 'Soldercon' strips. These are single-line socket strips with 0.1 inch contact pitch, and they have lead-outs at the bottom for soldering into boards with 0.1 inch matrix hole groups. The strips are rather like half an ordinary d.i.l. in-tegrated circuit holder."

"Fair enough," said Dick. "Go on." "Apparently," continued Smithy, "these strips are a bit fiddling to set up for soldering, and the solution consists of holding them in position during soldering by plugging in a dud in-tegrated circuit that would otherwise be thrown away. The dud i.c. need only be 8 pin, even if the final assembly is intended to take a 16 pin job. This approach automatically ensures correct alignment, and a few duffy i.c.'s can be kept on hand for the purpose, having been daubed with cellulose enamel of a distinctive colour to act as a reminder." "I don't seem to recall," said Dick doubtfully, "handling any of these

result is that the hole has to be finished off with a round file."

(b). A narrow rectangle of

printed circuit board with the copper on the outside may be used in place of the

insulated washers. This also enables a connection to be

made to the transistor

collector

"I've bumped into that sort of thing quite often," remarked Dick. "Thin tin-plate.can be pretty vicious stuff at times." "True," agreed Smithy. "Well, 'the

difficulty can be overcome by first drilling a small hole, say an eighth of an inch in diameter, and then using a countersinking tool. This gives a neat round hole without any burrs or distortion of the metal. During the countersinking process, the tin-plate is supported on a wood block with a small hole drilled in it to match the initial small hole in the tin-plate. The writer of the letter says that he has employed this method many times on 2 ounce tobacco tins used for pre-amplifiers, converters and similar small items."

Smithy put down the letter, picked up his mug and drained its contents. After this, he held up the mug in front of him. Dick rose wordlessly, took the mug from him and carried it over to the variegated array of utensils ranged alongside the Workshop sink. Established over many years, the Workshop Tea Ritual was now so automatic as to be beyond comment on the part of either Dick or Smithy. As Dick returned with the filled mug, he was surprised to find Smithy scribbling

the next hint has got something in it that needs working out.'



Fig. 2. A variable voltage power supply which offers equal voltages positive and negative of chassis. The two current overload transistor circuits associated with the 2.7 Ω resistors are based on a design which appeared in the last January issue

single-line socket strips myself."

"It isn't that," replied Smithy. "I've just been sorting that 20 metre length of wire into English units for you." "Good show," said Dick. "What does it come to?"

Dick's eyebrows shot up. "Links?"

"That's right," confirmed Smithy. "As there are 100 links in a chain, you

could also say 0.994 chains." "Links and chains now," moaned Dick. "Couldn't you have thought of

Dick. "Couldn't you have thought of any other outlandish units?" "I can if you like," said Smithy obligingly. "20 metres also works out as 0.00414 of a league!" "How in heck," complained Dick, "can I measure something in leagues?" "You wanted English units," stated Smithy firmly, "and so I've given you English units."

English units.

"I think," said Dick hastily, "that we'd better get on to the next hint." "As you wish," said Smithy,

reaching for a third letter in the pile on his bench. "Now let's see what we have here."



Fig. 3(a). The appearance, and approximate length, of a Mason-Master laminate cutter. This may be employed for cutting out pieces of Veroboard

(b). The laminate cutter can also be used for cutting Veroboard copper strips either at holes or between holes

Smithy read through the letter, then beckoned to his assistant. Dick walked over to him and looked at a circuit diagram in the letter. (Fig. 2). "This circuit," Smithy went on, "is

partly based on the 'Compact Stabilis-



Callers welcome.

ed Power Supply' which appeared in the last January issue of Radio & Elec-tronics Constructor. That power supply had one output only but, as you can

see, this one has two." "What's it for, Smithy?" "It's for powering experimental circuits incorporating op-amps such as the 741," replied Smithy. "What was required was a supply which gave equal voltages positive and negative of earth, these being continuously variable from 5 to 15 volts. Now, the circuit here really consists of two independent power supplies, each run-ning from a separate secondary on the mains transformer, and with the negative output of the upper supply connecting to the positive output of the lower. The crafty bit which brings the circuit up to hint status is that the two $10 \text{ k} \Omega$ output voltage control potentiometers are ganged together as a dual pot, so that adjusting this causes both

output voltages to change in unison." "That's a good idea," commented Dick appreciatively. He looked more closely at the circuit. "The two power supplies aren't identical, though. There's a 240 Ω resistor in series with the track of the voltage control pot in the upper one." "Ah yes," said Smithy, re-

examining the letter which had accompanied the circuit. "That 240Ω resistor wasn't in circuit initially, but it was found that the two output voltages weren't quite equal. This was cleared by inserting the $240\,\Omega$ resistor. Other power supplies made up to the circuit may similarly need a resistor in series with one or other of the pots to make the output voltages equal. Which particular pot requires the resistor, and the value that the resistor needs, are found by ex-periment."

"I heven't seen them referred to in any home-constructor applications," admitted Smithy. "But there are single-line 0.1 inch socket strips in the R.S. Components catalogue. The R.S. version consists of individual 25-way

"At least," commented Dick, "At least," commented Dick, "things like those connection strips are not metricated. Not when they've got a sensible contact spacing of 0.1 inch." "It looks," said Smithy, "as though I still haven't satisfied you with a suitable English convicted to the

suitable English equivalent for that length of 20 metres. Let's have another

He tore the top sheet off his note-pad, then engaged in a further calculation

"Here we are," he said eventually. "I've now worked it out for you." "Thank goodness for that. What's the equivalent?" "A length of 20 metres," grinned

Smithy, "is the same as 10.9 fathoms!" "Stone the crows," spluttered Dick irately. "I want to measure out a length of flex, not pilot the flaming QE2 up the Thames.

But Smithy had already turned his attention to the next letter in the pile. "Here," he remarked, "is a simple

little gadget which should be of particular help to people like Jack de Manio."

He took a small cardboard device-from the envelope and showed it to

Dick. (Fig. 4(a) and (b).) "This gadget," he went on, "simply consists of two concentric cardboard circles with the times from 1 to 12, and from 13 to 24 hours marked on them. A pin through the centres holds them together, and the small circle is free to rotate on this pin."

"I think I get the idea," said Dick. "If, for instance, you want to hear short-wave programmes on G.M.T. whilst the normal time is B.S.T., you can set the inner circle one hour different from the outer one, and this will act as a reminder as to which time

"You've got it," confirmed Smithy. "You can also use it, when listening to short waves, as an aid to working out the different time zones throughout the world. Quite a useful device for the





(b)

Fig. 4(a). A simple device which acts as a reminder for time. differences (b). As may be seen here, the inner circle can be rotated to any desired setting inside the outer circle

2 slots 1.5mm (1/16") width and depth, on 2 sides of tool

7.5mm

Steel or aluminium 13 x 13 x 22 mm (1/2"x 1/2"x 7/8")

Fig. 5. A de-soldering tool for the removal of d.i.l. integrated circuits

keen Dx buff."

"Very good," remarked Dick. "Do you know, Smithy, this is one of the best hint seshes we've had for quite. some time."

Some time." Smithy picked up his mug and again drank avidly.

"We've certainly encountered some good ideas today," he agreed, wiping his mouth with the back of his hand. "And now I'm afraid we have to get down to the last letter. This doesn't mean we're coming to an end all that quickly, though, because this particular letter has no less than three separate hints in it."

DE-SOLDERING TOOL

Smithy took up the last envelope and extracted some sheets of paper from it. There was a sketch on one of these and he showed it to Dick. (Fig. 5).

5). "What we have here," he remarked, "is a de-soldering tool for d.i.l. integrated circuits. It's pretty selfexplanatory, and one important feature is that the large block at the end of the tool must be made of steel or aluminium so that it will not 'freeze' to the printed circuit board if it cools below soldering temperature. The block is heated upon a gas ring or similar, and is then applied to the i.c. connections on the copper side of the board. The large slotted face is employed for 14 and 16 pin i.c.'s. Obviously, the i.c. pin ends fit in the slots, and this helps to give good thermal contact with the solder. After a second or so of steady pressure with the tool, the integrated circuit can be gently eased from the board."

Wooden handle

"Quite a useful gadget," commented Dick. "What's the second hint in that letter, Smithy?"

"It's concerned with rather an interesting approach towards making up an integrated circuit tester," stated Smithy. "The idea was originally conceived for a valve tester quite some time ago, but the principle is applicable for i.c. testing, or indeed for testing other complex devices. There's a sketch here, too."

Dick glanced at the drawing. (Fig. 6).



Fig. 6. A suggested approach towards making up an integrated circuit tester. The program card is a piece of Veroboard to which may be soldered link wires, resistors, rectifier diodes, zener diodes and light-emitting diodes



"It looks," he remarked, "like a piece of Veroboard being plugged into an edge connector." "And that's just what it is," con-

firmed the Serviceman. "Assuming an i.c. tester, most of the contacts of the edge connector are wired up to an i.c. holder in which the i.c. to be checked is plugged. The remainder of the edge connector contacts connect to power supplies, metering circuits and so forth. A Veroboard for a particular type of i.c. is then prepared by fitting link wires, resistors and so on which route the power supply and metering circuits to the appropriate contacts of the i.c. holder. The Veroboard may also have diodes on it to steer currents in particular directions, zener diodes to regulate particular supply voltages and l.e.d.'s to indicate the flow of currents.'

"Why, that's cunning," exclaimed Dick. "What you do is prepare an individual Veroboard panel for each type of i.c. you intend to test. If it's a different i.c. you plug in another Veroboard panel which has been prepared for that type. They're really

"That's a good name for them," said Smithy approvingly. "You can start off with just one Veroboard panel and then make up further Veroboard pan-els as the need for them arises. The great advantage of the system is its flexibility, since it allows you to set up virtually any test circuit in no time at all. Each Veroboard panel is, of course, marked up with the i.c. type that it's programmed for. The scheme can also be adapted for other purposes where the ability to quickly change a complicated test circuit is required."

"I must think about this one later on," pronounced Dick. "The basic idea of having a program card with components on it raises all sorts of possibilities."

"It's certainly worth some thought," concurred Smithy. "Anyway, we must now deal with the last hint for today."

He took a final sheet of paper out of the envelope. This also had its comple-ment of sketches. (Fig. 7(a) and (b).) "This last idea," remarked Smithy,

"is an integrated circuit adapter for fitting to a T-Dec board. It consists basically of a 16-way d.i.l. integrated circuit holder which is soldered to a piece of printed board. This board has two rows of pins spaced at 0.7 inch, the pins themselves being at a pitch of 0.2 inch to conform with the T-Dec matrix."

"I see the idea," put in Dick. "You plug the i.c. into the i.c. holder, and you plug the adapter into the T-Dec." "That's it," stated Smithy. "The

first thing to do is to etch the board and drill out the holes in it. A piece of 0.1 inch Veroboard is useful for aligning the i.c. holder holes, and it's also helpful for the holes at the 0.2 inch inway, which you'll find of advantage when drilling out i.c. holes in any printed board. The i.c. socket is next soldered to the printed board, the



Fig. 7(a). The printed circuit board employed in an adapter for connecting d.i.l. integrated circuits to a T-Dec board. The printed board is reproduced full-size and the diagram may be traced (b). The printed board with the i.c. holder and pins fitted. For clarity, only two of the pins are shown

copper side of the latter being uppermost. This enables the board to lie flat on the T-Dec, and it also assists in the final soldering operation. The board is then placed on the T-Dec with the outer holes over two rows of 8 holes in the T-Dec. Next, 16 clean steel dressmaking pins are passed fully home through the holes into the T-Dec, after which the head of each pin is raised by 2 to 3 mm. The pins are then soldered to the copper of the board.

Smithy paused, and refreshed

himself once more from his mug. "Now," he resumed, "we come to the clever bit. The assembly is raised from the T-Dec until the pins are not quite out of the T-Dec holes. Then, the solder at each pin is melted in turn, it being allowed to cool at one pin before proceeding to the next. This process enables the pins to relax into exactly the positions required for lining up with the T-Dec holes, and the adapter can then be readily inserted into the T-Dec matrix holes whenever it is required.

"Well," remarked Dick. "That's certainly a neat idea." "And just the job," returned Smithy, "for ending this latest session on hints from readers."

SUCCESS AT LAST

Smithy collected the letters

together, then glanced at his watch. "Back to work now," he pronounc-ed. "We've gone nearly quarter of an

ed. "We've gone nearly quarter of an hour past the end of lunch-break." "Fair-enough," said Dick obligingly, as he rose and walked back to his bench. "Now, do stop messing me around, Smithy, and tell me the proper English length for this 20 metres of flex you want." "I'd be happy," stated Smithy promptly, "if you cut it to a length of 17.5 ells."

17.5 ells.

"Blimey, don't you ever give up?" "Or again," said Smithy, "39.4 cubits would be acceptable." "Cubits?" repeated Dick in-

credulously. "Cubits? Where the heck do you get cubits from?"

"They used cubits in the Bible," said Smithy sternly. "What's good enough for the Bible should be good enough for you."

"Well," said Dick uneasily, "I don't want to go against the Bible, but I still can't measure out that flex in cubits."

"If," suggested Smithy, "you had an interest in horses I'd suggest 197 hands. No? All right then, I'll put you out of your misery. A length of 1 metre is equal to 1.094 yards, whereupon 10 metres is 10.94 yards, and 20 metres is 21.88 yards. Cut off 21.88 yards of the wire and I'll be quite content." "That's more like it," replied Dick.

"And how much is 0.88 of a yard?". "Rough check," stated Smithy, "it'll be just over 2¹/₂ feet." "Now," stated Dick in a satisfied

tone of voice, "Those are what I call sensible units of length. Why people want to complicate things by introducing metres, when we have perfectly satisfactory English units to play around with, just about baffles me.

Whereupon Dick, completely forget-ting that nearly all the units Smithy had referred to were representative of present or past English usage, proceeded to measure out the flex required by Smithy in units of twelve inches to the foot and an uncompromising three feet to the yard. Which series, of course, progress to the very first unit offered by Smithy, the redoutable five and a half yard long rod, pole or perch.

EDITORS NOTE

The hints discussed in this episode of 'In Your Workshop' were con-tributed, in the order in which they appear, by H. Kennedy, W. Puffett, G. O. H. Sjogren, James W. Robson, K. Allen and C. P. Finn.

Further hints for this feature are welcomed, and payment is made for all that are published.

TRADE NOTE

SIGNAL TRACER/INJECTOR PROBE

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> We have been asked to point out to readers that the "Super Spark Mk.V" Capacity Discharge Unit supplied by Bi-Pre-Pak Ltd., of Westcliff-on-Sea, and advertised at £7.95 in Kit form and £10.50 complete, attracts VAT at the 8% rate and not 25%.

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With reference to my personal advertisement I would like to con-gratulate you on the effectiveness of your advertising columns.

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Penarth, Glam.

C. Bogod,

MAY 1976

TRANSISTOR LEAD'-OUT LOCATER'

In 1974 I built the "Transistor Lead-Out Locater" by J. R. Davies, in the October and November issues of that year. I find it a great investment, for many transistors have different leads. I find also that, with adjustment to the pre-sets, I can check f.e.t.'s. Normally, the drain and source leads are hard to find.

Another tip concerns making circuit boards. My son has tried masking tape for these, drawing out the pattern and cutting out the part for etching with a masking knife. This works O.K. and the copper is easier to clean.

C. H. Gardener Truro, Cornwall.

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(Continued on page 645)



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