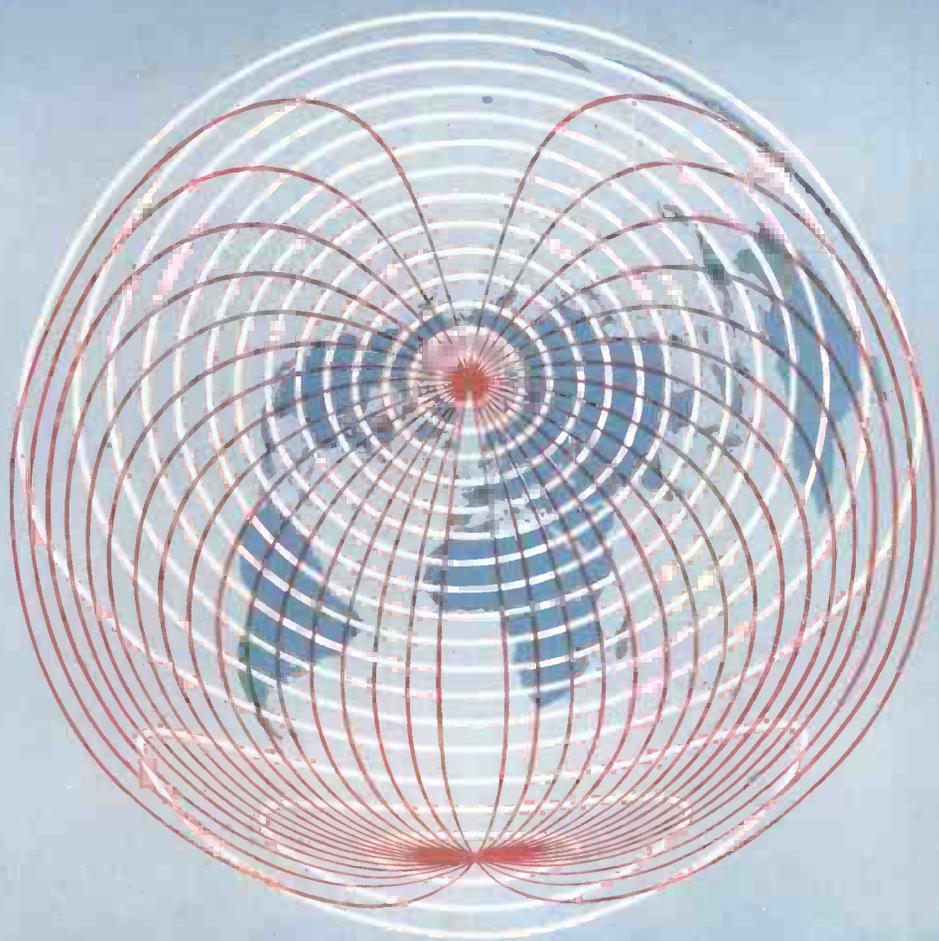
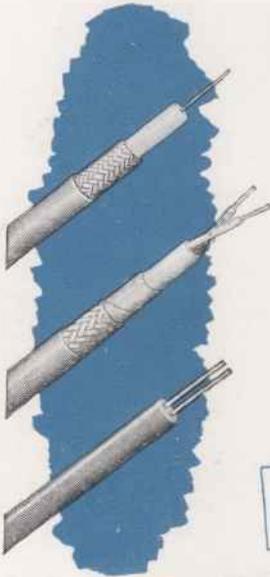


Wireless World

RADIO AND ELECTRONICS



Vol LVI No 11 Two Shillings November 1950



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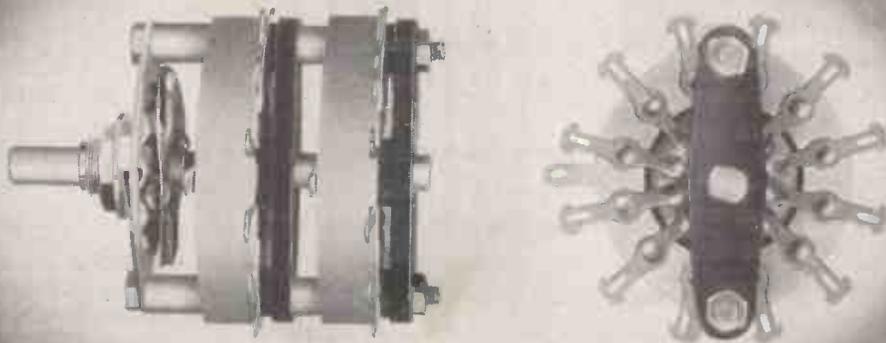
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Important trends in VALVE DESIGN

MULLARD LINE OUTPUT PENTODE TYPE PL81

The line output stage of a television receiver imposes conditions which call for a valve having properties which differ considerably from those of a normal output valve.

The essential requirements for a line output valve are, first, that it shall be capable of supplying a large peak anode current when operated at a low anode voltage, and second, that the insulation of the anode shall be capable of safely withstanding the high voltage peaks, which may amount to 5KV to 7KV, occurring during the fly-back period.

Satisfaction of the first of these requirements is mainly a matter of the geometry of the valve; the second can be assured only by careful mechanical design.

The PL81 is an all-glass power pentode on the B9A (Noval) base, specially designed for use as a line output valve. Its heater is rated at 0.3A, 21.5V, and is therefore suitable for series operation in transformerless receivers intended for A.C. or D.C. mains supply.

It will deliver a peak anode current of 350 mA at an anode voltage of only 70V and a screen voltage of 170V. The efficiency of the valve is thus intrinsically high.

By adopting the booster diode circuit whereby the H.T. line voltage is increased, the required output can be obtained at a still lower anode voltage, so that the already high efficiency of the stage is further improved.

The necessary high insulation resistance to withstand a peak voltage of 7KV has been obtained by special internal construction, and by bringing out the anode connection to a top cap so that the use of a specially insulated valve-holder is not necessary. Even so, the seated height of the valve is only 75mm and the overall diameter 22.2mm—dimensions only slightly larger than those of the voltage amplifying pentode in the same range.

The production of a valve of this output and high insulation in so small an envelope may be counted as something of an achievement.

RATINGS & CHARACTERISTICS

Heater Suitable for Series operation, A.C. or D.C.

V_h	21.5V
I_h	0.3A

Capacitances

C_{in}	14.3 μ F
C_{out}	6.5 μ F
C_{a-g1}	< 0.4 μ F
C_{g1-h}	< 0.2 μ F

Characteristics

V_a	170V
V_{g3}	0V
V_{g2}	170V
V_{g1}	-22V
I_a	45mA
I_{g2}	3mA
g_m	6.5mA/V
μ_{g1-g2}	6

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Wireless World

VOL. LVI. No. 11.

NOVEMBER 1950

Valve Symbols

BRITISH Standard 1409:1947 "Letter Symbols for Electronic Valves," issued some three years ago, was stated to be "based on proposals prepared . . . with a view to standardizing the letter symbols used by valve manufacturers in their catalogues and other technical literature." At the time, *Wireless World*—not unreasonably, we hope—took the publication of this specification as implying a desire that the symbols proposed should be generally adopted by a wider circle. So, in spite of typographical difficulties, we accordingly used the symbols as far as was practicable.

Having gone thus far in the interests of uniformity, it comes as something of a shock to us to see the revised specification B.S. 1409:1950, just issued.* This publication, under the same title as its predecessor, carries on its cover the prominent statement "Mainly for use in valve catalogues and similar technical literature." That seems to put forward a highly undesirable principle: are we to have a state of affairs where users of valves (which means all of us) are to learn two languages—one for use in dealing with manufacturers and another in reading (or writing) technical journals?

Stereophony

OUR correspondence columns bear witness to the widespread interest that exists in stereophonic broadcasting. Stereophony will no doubt attract still more attention next year, as we believe the multi-channel principle is to be used in the sound-reproducing equipment to be installed at the Festival of Britain. That being so, it is a pity that a plea for B.B.C. experimental transmissions on a binaural system, made in this journal last March, was so uncompromisingly turned down. The B.B.C. Chief Engineer, in a letter published in our April issue, pointed out the admitted complications of the system, and expressed doubts as to

whether the Corporation would be justified in spending money on a specialized service of interest to a relatively small number of listeners. The French broadcasting authorities were, however, less pessimistic about stereophony, and staged an experimental transmission a few months later.

We are certain that interest in this subject is greater than the B.B.C. imagines, and venture to suggest the Corporation should make another attempt to find ways and means of staging experiments in which listeners can participate, as they did in France.

Too Many Bosses?

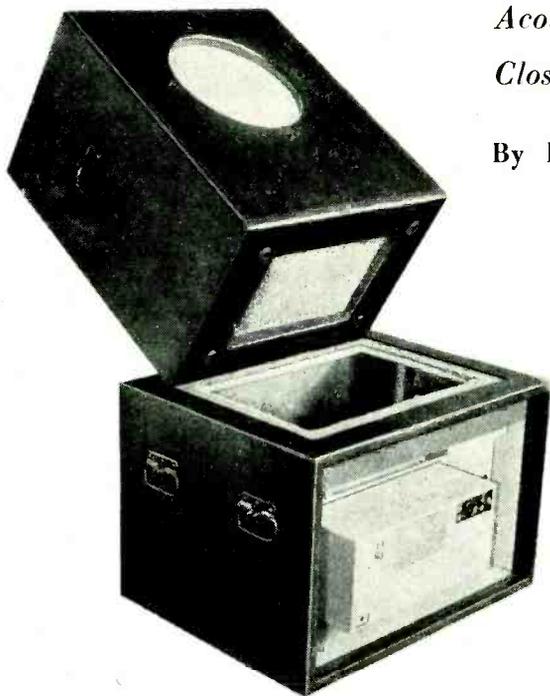
THOUGH the uproar provoked by the withdrawal of the political play "Party Manners" from the B.B.C. television programme was a regrettable and unworthy episode that by now has been largely forgotten, it raised a matter of principle that will, we hope, be borne in mind when the B.B.C. Charter comes up for renewal next year. *Wireless World* does not concern itself with details of programme organization, but we deplore anything that tends to reduce the status of British broadcasting.

As we see it, the B.B.C. attitude over this matter betrayed that weakness against which the Corporation should be most strongly on its guard—timidity. This point of view was admirably expressed in a leading article in *The Times* of 10th November "The listening public will always be behind them [the B.B.C.] in refusing to turn broadcasting into a colourless bore for the sake of this or that crank or fanatic. There would be no intellectual or aesthetic worth in broadcasting if it were controlled to please every shade of minority opinion. Censorship by timidity can be as effective as the blue pencil of a dictator." As things are, the organization of the B.B.C. tends to favour the timorous. Heads of "Programmes" should have sweeping powers, and be discouraged from passing on the responsibility for awkward decisions to higher authority.

[* British Standards Institution, 28 Victoria Street, London, W.1. Price 2s. The revised specification includes a considerable number of extra symbols.]

Sidelights on

Loudspeaker Cabinet Design



Experimental two-section vented cabinet with top half tilted back to show sound-absorbing material covering the communicating window.

IT is not the purpose of the present article to enter deeply into the mathematical treatment of the problems of loudspeaker cabinet design, since this field has already been covered in standard works on applied acoustics as well as in a number of articles in the technical press. Instead, it is proposed to discuss certain aspects of the subject which do not always receive full attention in the literature, and to illustrate these by a few experimental results obtained in the course of development work on cabinets during the period 1938-1947.

Standing Wave Effects

The subject of loudspeaker cabinet design is usually approached by a simplified theory, in which the mechanical properties of the cone unit and the acoustic properties of the enclosure are represented by a set of inductances, capacitances and resistances. Equivalent circuits containing these elements can then be drawn and the basic features of the design calculated.

Clearly, this simplified theory is only valid at frequencies so low that the wavelength of the sound is large compared with the dimensions of the cabinet. At higher frequencies, at which this condition is not fulfilled, the cabinet volume does not behave as a

Acoustical and Electrical Damping in Closed-cabinet Loudspeakers

By D. E. L. SHORTER,* B.Sc.(Eng.), A.M.I.E.E.

lumped acoustic capacity, and standing wave effects may appear unless the enclosure is adequately damped by sound absorbent material.

Unfortunately, the performance of a cabinet at these higher frequencies cannot be readily calculated, and in the absence of facilities for response measurement the degree of damping actually achieved is often in doubt.

The full extent of the standing wave effects in loudspeaker cabinets is not always appreciated. Cabinets intended to give good response down to 50 c/s generally have at least one dimension which is equal to a half wavelength of sound in the frequency range 125 c/s to 250 c/s. Moreover, as some recently published work¹ has shown, that the acoustic impedance presented by the cabinet to the cone may change from a capacitance to an inductance at a frequency of which the wavelength of the sound is some seven times the maximum dimension of the enclosure. In some cases, therefore, the simple theory based on lumped constants may break down even below 100 c/s. Reference to a table of absorption coefficients will show that the effectiveness of any sound absorbent lining of practicable thickness falls off below 500 c/s. It will thus be seen that the frequency band within which standing wave effects are to be expected may extend over some two octaves in an important part of the audio-frequency spectrum.

A practical example will illustrate the foregoing discussion. An experimental closed cabinet (the so-called "infinite baffle" type) was required for a 10-in. cone unit; the resonance frequency of the unit with the cabinet volume was not to exceed 45 c/s.

The suspension of the cone unit had been experimentally modified to give the maximum compliance consistent with mechanical stability, but even so a volume of 8 cu. ft. was found to be required to meet the specification. For reasons connected with high-frequency distribution, the axis of the present loudspeaker was required to be about 3ft. from the floor and this consideration led to the adoption of a design 4ft. high.

Fig. 1(a) shows the free-air axial frequency response obtained with this cabinet, the cone unit being driven by an amplifier of low output impedance. The curve was taken with the cabinet lined with

* Research Department, B.B.C. Engineering Division.
¹ "The Acoustical Impedance of Closed Rectangular Loudspeaker Housings" by Meeker, Slaymaker and Merrill, *Journal of the Acoustical Society of America*, March 1950.

absorbent material of conventional type. Standing wave effects are nevertheless apparent at low frequencies, showing that the internal damping is inadequate.

Damping by Partitions

The ineffectiveness of sound absorbent linings at low frequencies is due to the fact that all the absorbent material lies within a small fraction of a wavelength of the inner wall, which is, of course, a velocity node. Without motion of the air particles, or of the material itself, acoustic power cannot be absorbed and dissipated. Consideration of these facts suggests that the best position for damping material would be somewhere out in the space inside the cabinet, where the standing waves could be caught "on the wing." Theoretically, the material would have to be divided up into many parts, so disposed that at any one frequency there should be an absorbing element in the neighbourhood of a velocity antinode. In practice, however, such a complication has been found unnecessary and effective low frequency damping can be achieved by concentrating the absorbent material into one or two partitions strategically placed across the cabinet. Fig. 1 (b), for example, shows the response of the loudspeaker previously referred to when a single sheet of $\frac{1}{2}$ -in carpet felt was stretched horizontally across the inside of the cabinet at right angles to the longest dimension; the reduction in standing wave effects can be clearly seen.

In this system² of damping by partitions, the cab-

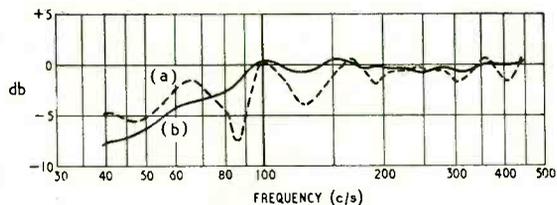


Fig. 1. Axial response below 500 c/s of 10-inch speaker in closed cabinet (a) inner surface lined with absorbent material in conventional manner; (b) with the addition of an absorbent membrane stretched horizontally across the cabinet at right angles to the longest dimension.

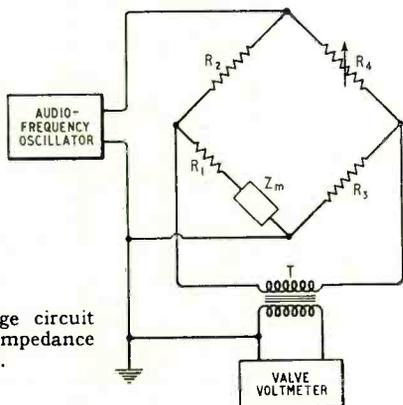


Fig. 2. Bridge circuit for motional impedance measurements.

inet can be regarded as being divided into sections, each so small that any standing wave effects occur at high frequencies, at which the sound absorption of a lining of the conventional type is adequate. It may further be noted that those sections of the cabinet which are separated from the cone by one or more sound absorbing partitions receive little sound at the high frequencies and therefore require very little "acoustic treatment."

The principle of subdivision can be applied in a number of ways to suit different cases. The photograph, for example, shows part of an experimental vented cabinet constructed in two separate sections. The lower of the two sections houses the power amplifier and takes the form of a plinth on which the upper section stands. In the illustration the upper section is tilted to show the underside which has a window communicating with the plinth and covered with carpet felt.

Impedance Test

Reference was made earlier to the strategic placing of absorbent partitions. This operation would appear at first sight to require facilities for measuring the overall frequency response of the loudspeaker. Fortunately, however, it is possible to make the necessary experimental adjustments by quite rough impedance measurements. Fig. 2 shows the circuit used for this purpose. R_1 is the resistance of the speech coil of the loudspeaker which is fed at constant current from an audio-frequency oscillator though a

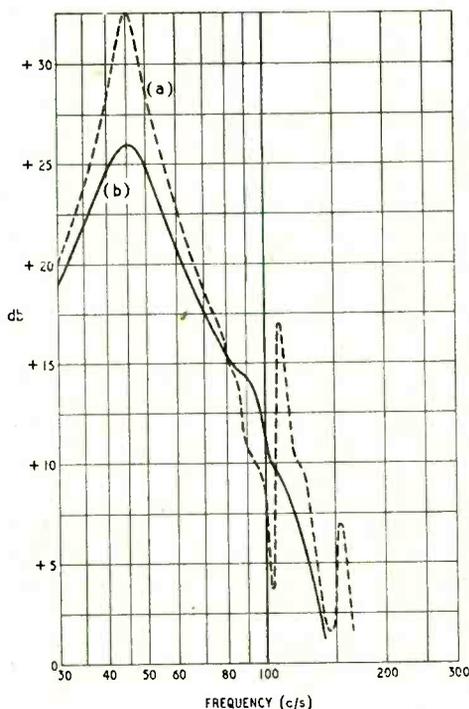


Fig. 3. Typical response curves obtained with the circuit of Fig. 2. Curve (a) is for an undamped cabinet and (b) for the same cabinet with internal damping partition.

² Patent Application No. 2,4528/49

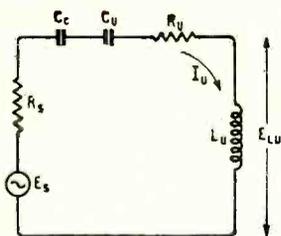


Fig. 4. Equivalent electrical circuit of acoustic elements in a closed-cabinet loudspeaker at low frequencies.

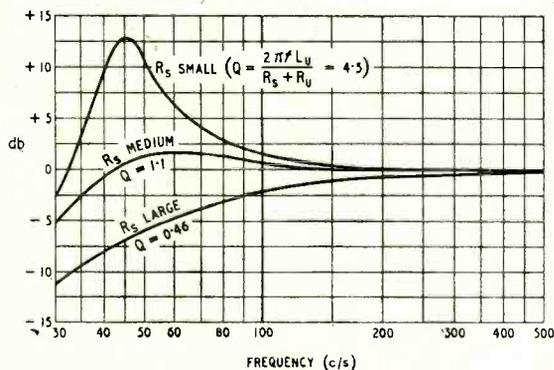


Fig. 5. Response of closed-cabinet loudspeaker for various values of the effective damping resistance R_s .

relatively high resistance R_2 . Z_m is the motional impedance of the loudspeaker, so that the voltage developed across Z_m represents the back e.m.f. generated by the motion of the speech coil when driven by a constant current. Since we are dealing only with the frequency range in which the cone moves as a whole, this back e.m.f. is a measure of the cone velocity. The cone aperture is the only outlet from the cabinet; any internal resonances can only influence the sound output from the system by modifying the motion of the cone, and must therefore reveal themselves by irregularities in the curve of motional impedance against frequency.

In general, the resistance R_1 will tend to swamp all but the largest of these irregularities so that the total impedance of the loudspeaker is not a very sensitive index of cabinet performance. In the circuit of Fig. 2, therefore, the effect of R_1 is roughly balanced out. Resistance R_2 is made approximately equal to R_1 , and the variable resistance R_4 approximately equal to R_2 , the whole circuit forming a bridge, the output of which is taken off through the isolating transformer T to a valve voltmeter. The primary impedance of T should be high compared with the maximum speech coil impedance at low frequencies, a requirement which is generally easy to meet.

To make a test, the speech coil is temporarily prevented from moving, either by disconnecting the loudspeaker field supply or, in the case of a permanent magnet, by carefully inserting small wedges into the gap so as to grip the coil. Assuming complete clamping of the movement, Z_m will now be zero, and in this condition, the bridge is balanced at some convenient frequency, preferably in the 200/300-c/s region, by adjusting the value of R_4 and using the valve voltmeter as a null-indicator. The speech coil is then released and the bridge output, which now represents

the voltage across Z_m (i.e. the back e.m.f. of the speech coil) is read direct on the valve voltmeter and plotted against the frequency of the oscillator. A typical curve of this kind is shown in Fig. 3(a) which was obtained in an ordinary live room with a completely undamped cabinet. The radiation efficiency of the loudspeaker is too low for any room resonances to affect the curve but the internal modes of the cabinet are clearly apparent. Fig. 3(b) shows how these modes are affected by the introduction of a felt partition.

It will be noted that in this test, the speech coil is being driven with constant force. If the cone were mass-controlled, i.e. if the compliance of the suspension were infinite and the effect of the cabinet nil, the speech coil would move with velocity inversely proportional to frequency. In this hypothetical case, the curves of Fig. 3 would be straight lines having a slope of 6 db per octave; and it is sometimes convenient to use such a slope as a standard of reference. If desired, an equal and opposite slope can be introduced into the response of the test circuit (for example, by interposing in the input of the valve voltmeter a small series condenser). With this compensation, the valve voltmeter readings will be confined to a much smaller range, and may be plotted to a more open scale. Small irregularities in the curve may thus be better observed; and the reference line representing the condition of mass control becomes horizontal.

The method of test described above has been used successfully up to about 300 c/s and the accuracy, though limited by the difficulty of ensuring complete clamping of the cone movement, is sufficient to disclose the more troublesome internal cabinet resonances, so that these can be dealt with without recourse to free-air response measurements.

Effect of Source Impedance

Returning to the response characteristic shown in Fig. 1, it will be seen that although the fundamental resonance frequency of the system is at 45 c/s, the acoustic output begins to fall away well above this frequency. For an efficient loudspeaker, driven by an amplifier of low output impedance, this type of response is in accordance with theory. The mechanism of the effect can be explained in the following way.

At the lower end of the audio-frequency band, the wavelength of the sound is large compared with the diameter of the cone, while the polar distribution of the sound output varies only slightly with frequency. It can be shown that in these circumstances the sound pressure produced is proportional to the product of the cone velocity and the frequency. Thus, constant sound pressure will be obtained if the cone moves with a velocity varying inversely as the frequency, while constant cone velocity will give a sound output falling towards the bass. If the cone unit is very efficient, its motional impedance at low frequencies will be high, or, in other words, practically the whole of the voltage across the loudspeaker terminals will be accounted for by the back e.m.f. generated by the motion of the speech coil. If, in addition, the impedance of the driving source is low, the back e.m.f. will be nearly equal to the source voltage, and must therefore remain nearly constant with frequency. In these circumstances, the cone must be moving with nearly constant velocity, and the sound output will therefore fall at the bass. Regarding the matter

from a slightly different viewpoint, we may say that the rise in impedance of the speech coil at lower frequencies produces an electrical mis-match which so reduces the efficiency of power transfer from amplifier to loudspeaker that, however efficient the electro-acoustic power conversion of the system may be, constant overall efficiency cannot be obtained. The higher the magnetic flux density, the further up the frequency range does this effect extend, so that the "infinite baffle" may give disappointing results with the better class of unit. This does not, of course, mean that high efficiency in a cone unit is a bad thing, but that in some cases it is difficult to make full use of it.

It is sometimes suggested that one can never have too much electrical damping of a loudspeaker. The present case, however, appears to suggest the contrary, and in view of the general interest in the subject, it may be worth while to study the electro-acoustic system from yet another view-point.

Fig. 4(a) is a simplified electrical equivalent circuit of the acoustic system of the loudspeaker. For reasons which will appear later, the circuit elements are not placed in quite the usual order. L_U represents the cone mass plus the effect of radiation reactance, R_U the small radiation resistance (which unlike most other resistances, varies with frequency), C_C and C_V respectively the acoustic capacitance of the cabinet volume, and the equivalent capacitance of the cone suspension. R_S is a very important quantity which, nevertheless, is frequently omitted from these equivalent circuits. It represents the effect of the electrical circuit of the loudspeaker and driving amplifier reflected into the acoustic circuit of the loudspeaker in a similar way to that in which the motional impedance is transferred into the electrical circuit. At low frequencies,

$$R_S \propto \frac{B^2}{r_a + r_c}$$

where B is the flux density in the gap, r_a is the output impedance of the driving amplifier (assumed resistive) and r_c is the d.c. resistance of the speech coil. Any internal frictional resistance in the cone suspension

system can, for simplicity, be lumped with R_S which, together with an equivalent constant voltage generator E_s , represents the source of power.

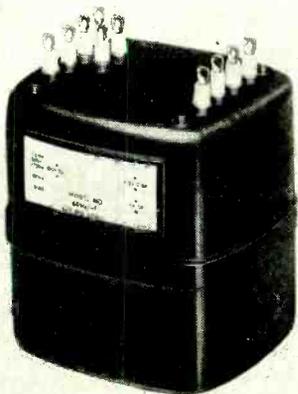
It has already been remarked that at low audio frequencies, the pressure response of the loudspeaker is proportional to the product of cone velocity and frequency. In the equivalent acoustic circuit of Fig. 4 the current I_U represents the alternating air current produced by the cone and is thus proportional to the cone velocity. Hence the acoustic response of the loudspeaker will be proportional to $I_U f$. The voltage E_{LU} is $2\pi f L_U I_U$. Thus E_{LU} is proportional to $I_U f$ and the variation in this voltage with frequency for any one value of L_U gives the frequency response of the loudspeaker. Over the frequency range for which the equivalent circuit is valid and the wavelength is large compared with the size of the cone, the loudspeaker can be reduced, as far as frequency response is concerned, to a half-section, high-pass filter working into open circuit. Small values of R_S , resulting from low flux density or high amplifier output impedance give a resonance peak and bad transient response, while large values of R_S , corresponding to high flux density and low amplifier output impedance can give a serious loss of bass.

The range of possibilities is illustrated by the three curves shown in Fig. 5, showing the variation of E_{LU} for a resonance frequency of 45 c/s with different values of R_S . Curve 3 will be recognised as approximating to the curve of Fig. 1(b), and it will be seen that when standing wave effects are disposed of, the response of the loudspeaker approaches the form predicted by simple theory. Curve 3 corresponds to a Q of 0.46, only slightly less than the figure of 0.5 required for critical damping. Whether critical damping is really necessary is another matter, to which we shall have occasion to refer later; but in the meantime it should be noted that this condition can only be achieved at the expense of a drooping frequency characteristic.

(To be concluded)

Standardized Components

THE Admiralty announce that their range of hermetically sealed transformers and chokes are the first type to qualify as fully Inter-Service Type-Approved Standards. The design comprises "C" core assemblies



Hermetically sealed power transformer to Admiralty design.

accommodated in deep-drawn steel cases, and owing to the many technical improvements which have been incorporated, the new transformers and chokes are as much as 40% smaller and give up to 50% reduction in external magnetic field compared with their counterparts using orthodox laminations.

The contour for each size has been carefully determined to provide the maximum strength, and construction is such as to withstand the severest conditions of vibration and shock, as well as extremes of climate.

Thirty-two sizes are available covering a range of power transformers from 5-VA to 2-kVA, also a range of audio-frequency transformers and power chokes to suit all normal requirements. Thirty-one of these sizes have tapped fixing holes at each end, thus permitting upright or inverted mounting at will.

Although the design of this range is Admiralty property, it may be used freely for commercial purposes by any manufacturer who so desires. Where firms do not wish to tool the range for themselves, they can obtain supplies of cases, internal fittings, etc., from commercial sources. More than twelve firms have already taken advantage of this arrangement, and as their production increases so a greater flow of these standardized transformers and chokes will reach the home and export markets.

Pickup Input Circuits

Compensating for 78 and 33½ r.p.m. Recording Characteristics

By R. L. WEST, B.Sc., A.M.Brit.I.R.E., and S. KELLY

MUCH disappointment can be avoided by a simple understanding of the principles underlying the design and selection of input arrangements for standard 78 r.p.m. and 33½ r.p.m. long-playing records. An exhaustive treatment is not intended, but it is hoped that this article will help the beginner to avoid the commoner pitfalls.

Most pickups fall into two main types—crystal (or piezoelectric) and magnetic—the latter covering ribbon and moving coil, as well as moving-iron armature and "variable reluctance" types. Crystal pickups are always of high-impedance; they are thus suitable for more or less direct connection to a grid circuit. Magnetic pickups are sometimes wound with a large number of turns of wire to generate the relatively large voltage required for the grid circuit; this can introduce electrical resonance (of self capacity and inductance of coil) unless great care is taken in the design. For high-fidelity pickups it is normally more convenient to use fewer turns (only *one* in the ribbon) these produce very small e.m.f.'s but are capable of delivering a much larger current. Since it is voltage and not current that matters at the grid circuit a suitable step-up transformer is normally used. The following remarks assume the use of a transformer where necessary and apply mainly to the high-impedance (secondary) side.

Effect of Load.—The input impedance of a valve is usually very high compared with the generator impedance and can be neglected; the value of the grid leak will therefore be dictated by the load impedance requirements of the pickup.

Magnetic pickups have internal impedance which is principally L and R in series, whereas crystal types

are principally C and R in series and R is usually very small. Fig. 1 shows the effect of load resistance and assumes constant output voltage on open circuit. In each case the dotted characteristic represents the effect of a lower value of load resistance.

Incidental Capacitance.—(i) *Screened lead between pickup (or transformer secondary) and amplifier.*—Again the internal impedance has to be introduced (see Fig. 2). By way of simplification the small resistive component has been omitted from the crystal case but should be included in the event of using very high cable capacities. The slight peak shown in the magnetic case is seldom noticeable since the internal R and the external R (not shown) damp it very thoroughly.

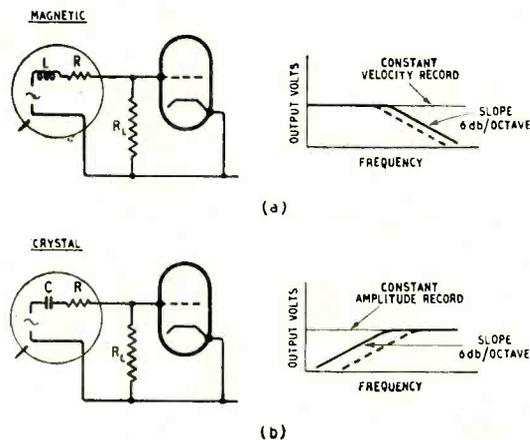
(ii) *Screened lead after the volume control.*—This is a common trap for beginners and is often overlooked by those who should know better! The Fig. 2 (c) shows the effective circuit, and the resulting top loss with intermediate settings of the volume control, which can be very considerable, particularly if a high-value volume control is used. The effect disappears as the slider approaches the "bottom end" and turns into an example of the previous type when the slider approaches the "top end." The use of a compensating condenser C_c as shown sometimes helps a little, but note that a capacity varying between C_L and $C_L/2$ is now permanently across the input, and only when the slider is half way (electrically) is the "compensation" correct! Far better, if enough gain is available, to use circuit of Fig. 2 (d). Here the very low output resistance will "swamp" the capacity of most normal screened lead requirements.

Pickup Resonances.—Low resonances, say under 1,000 c/s, include those due to the tone arm torsional resonance and the effective mass of the whole pickup resonating with the armature mounting compliance. If these are excessive within the working range, the pickup can be considered unsatisfactory, since it will be found that very heavy tracking pressures are necessary to keep the needle in the groove at these frequencies, with consequent increase in record wear. Electrical correction is no remedy.

The most noticeable high-frequency resonance is where the stylus and/or armature flexes. This ranges from about 3,500 c/s in the older pickups to well above audibility in some modern ones. The "height" of the resonance varies, from 12 db or more in the case of an undamped system, down to a barely perceptible rise if sufficient damping is added and in the right place. This is the resonance which, if within the audible range, considerably augments needle scratch. Above this resonance, the output usually falls off very rapidly (see Fig. 3a).

A simple treatment for magnetic types is to use a rather lower load than normal, and so produce top

Fig. 1.—Effect of resistance on output from magnetic and piezoelectric pickups.



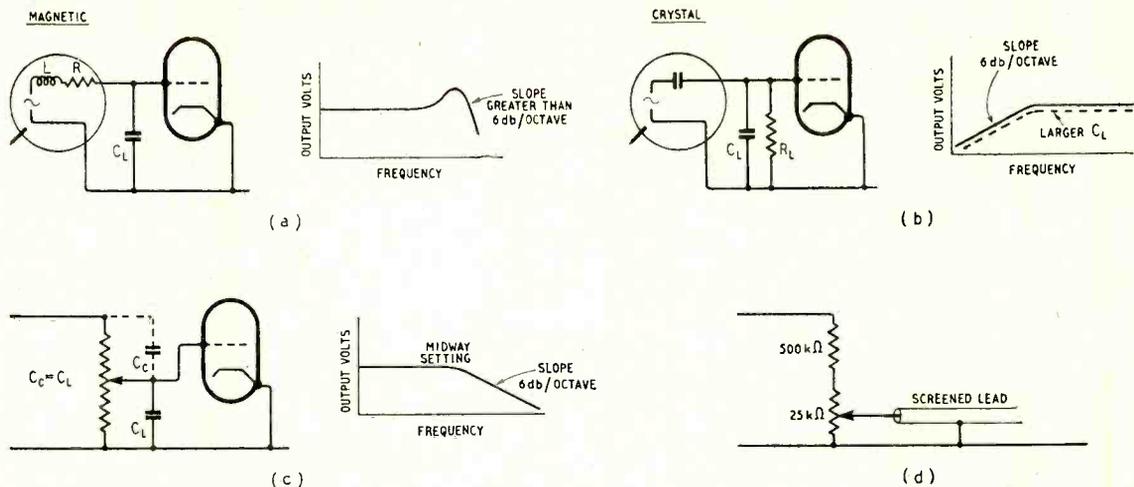


Fig. 2.—Illustrating the effect of external capacitance on the response of magnetic and crystal pickups.

attenuation at the rate of 6 db per octave. This improves the general balance—Fig. 3(b)—and assists the electromagnetic damping.

A more elaborate circuit uses a tuned series filter—Fig. 3 (c). R is seldom needed as the pickup impedance is usually sufficient. As a rule R_L can likewise be dispensed with since there is some resistance in the inductance. It is better to over-emphasise the correction in order to reduce to a minimum surface noise due to the armature resonance. "L" can be an air-cored or dust-cored choke of between $\frac{1}{4}$ and 1 henry. An ordinary laminated core usually exhibits a marked change of inductance with signal strength at these very low operating levels.

The older crystal types usually had an overall output of the type shown in Fig. 3 (d). Here it will be seen that the overall balance is sufficiently good for average domestic use.

Results can be improved by a tuned filter, a parallel-tuned (rejector) circuit is the simplest to use. In Fig. 3 (e), "L" would be the same component as in the magnetic case.

Choice of Load.—In general, the higher the load resistance, the greater the voltage developed by the pickup. For magnetic types the load can be several megohms if the top resonance frequency is very high, the grid circuit capacitance low and no top attenuation desired at this point. The makers' recommendations will have taken these factors into consideration.

For the older crystal types it is usually necessary to use a load under one megohm in order to attenuate the bass response somewhat—unless one is trying to get bass from a small cabinet! Values of $\frac{1}{2}$ megohm to 100,000 ohms are most common.

Hum—Causes and Cure.—There are two main sources of hum—by induction from an alternating magnetic field such as from the mains transformer or gramophone motor, and by electrostatic induction from wiring and components usually connected to the mains or other high voltage a.c. sources.

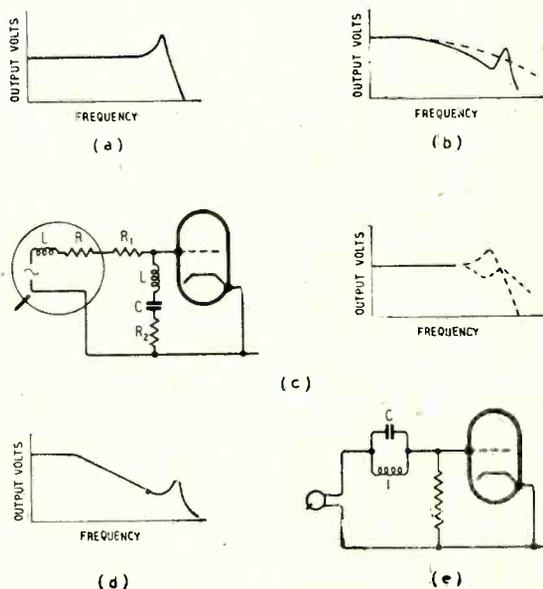
Magnetic hum introduced into the leads and wiring represents only a very small e.m.f., since only one complete turn is involved. This can be troublesome when a step-up transformer follows the lead in question, how troublesome depends on the trans-

former turns ratio and the e.m.f. generated by the pickup.

The best treatment is to twist tightly these low-impedance leads all the way from the pickup coil itself right up to the transformer input terminals. For the secondary connections, ordinary screened leads are sufficient, but it is advisable to keep all these leads as far from stray magnetic fields (including heater wiring) as possible. The transformer hum problem is dealt with later. On the high-impedance side the magnetic and crystal types experience mainly hum from electrostatic induction. The cure is simple—just plain good screening *everywhere*, and this precludes mains switches on volume controls, unless they are well shielded.

Rumble.—This consists usually of vibrations originating from the motor, with the main com-

Fig. 3.—"Top" resonances in magnetic and crystal pickups.



ponents between about 5 to 30 c/s. Magnetic pickups are seldom troubled with rumble since their output is proportional to velocity which falls with frequency for a given amplitude—hence very little output occurs at these low frequencies.

Crystal pickups, on the other hand, usually show up the motor deficiencies on this score, since the output voltage is proportional to amplitude. In a recent design (Acos GP20) a velocity type characteristic has been introduced below about 30 c/s and the trouble is considerably reduced.

Where necessary, a simple high-pass filter, such as that shown in Fig. 4, gives useful rumble attenuation without spoiling the bass response. This attenuates at 12 db/octave and gives a more rapid rate of fall at small values of attenuation than the more usual circuit, having equal capacities and equal resistances. Using the circuit shown, values of

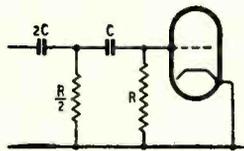


Fig. 4.—Simple "rumble" filter.

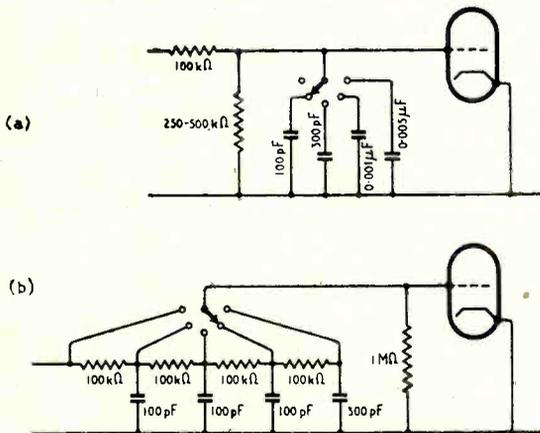
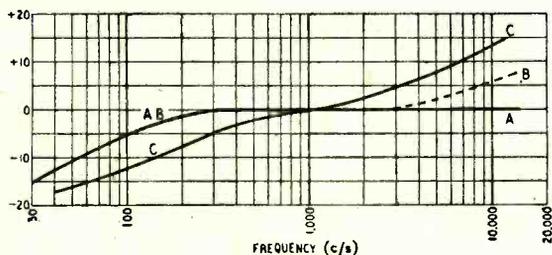


Fig. 5.—Top boost controls (a) with variable cut-off frequency, (b) with variable attenuation slope.

Fig. 6.—Principal commercial recording characteristics plotted on the basis of equal velocity at 1,000 c/s. A, standard 78 r.p.m.; B, Decca FFRR, 78 r.p.m.; C, Decca long playing.



$C = 0.01 \mu F$ and $R = 0.5 M\Omega$ have proved satisfactory.

Pickup Transformers.—(a) *Step-up ratio.*—In general, as high a step-up ratio as practical is used. Suppose the grid leak-cum-load has been chosen as $1 M\Omega$, then the actual load on the pickup will be $10^6/N^2$ where N is the turns ratio. The larger N , the smaller is the load, so one must not make N too large by trying to increase the output voltage too far, or severe top loss will occur. If the d.c. resistance of the pickup is, say, 25 ohms, then its impedance at 1,000 c/s we know must be more than this, say 50 ohms, and the load should be much greater still, say, 100 ohms if minimum top loss is desired. This makes N equal to 100. If top loss is definitely desired N could be increased to, say, 200. This will not quite double the output voltage since the lower load will cause a larger voltage drop (at all frequencies) in the resistive component of the pickup impedance.

(b) *Choice of primary turns.*—For any given ratio and core, two few primary turns, i.e., low inductance, will lead to loss of bass.

At the lowest frequency involved the primary reactance must be equal to or greater than the pickup impedance or load, whichever is the larger. A rough and ready rule, which is liable to err only on the generous side is to put the same number of turns on the primary as there are in the pickup coil, be it one or many.

(c) *Core Material.*—In the interests of minimum distortion (due to hysteresis), at the very low signal levels involved, a nickel alloy such as Mumetal is by far the best material. Not much will be needed, a $\frac{1}{4}$ -in square core section should be ample for any design.

(d) *Screening.*—Enclosure in any earthed metal can will look after the electrostatic component. From the magnetic point of view the best method is to select a spot as far as possible from the mains transformer, smoothing choke and motor. Use a Mumetal can, which should be earthed, care being taken to prevent the transformer core from touching the can, and remembering that the magnetic properties of Mumetal deteriorate if the material is stressed by cold working in any way. Any residual (magnetic) hum can be reduced by orienting the transformer in the can, or the can as a whole. In severe cases, a second Mumetal can, to enclose without touching the first, may be necessary.

Mechanical Feedback.—On occasions, when the loudspeaker is in the same cabinet as the turntable, mechanical feedback will occur when the pickup stylus is in contact with the record. This is usually due to flimsy cabinet construction or to attempting a very large low-frequency output. Each case must be treated on its merits, but trouble of this nature emphasises the desirability of a separate speaker. When this is not practicable cases may be dealt with by rubber or felt mounting for the whole baseboard, stiffening the baseboard, tightening or slackening slightly the motor mounting, or even reducing the bass response at the extreme low frequencies.

Simple Pickup Measurements.—Very little apparatus is necessary to carry out useful checks on frequency characteristics. A standard frequency record, preferably the type with bands of fixed frequency ranging from, say, 30 c/s up to 14,000 c/s or more, a fixed resistor of 5 to 10-watt rating equal to the nominal speaker load, an a.c. voltmeter (rectifier type) of range 0 to 5 V or 0 to 10 V.

Most modern amplifiers employ sufficient feedback

to be virtually flat over the audio range, so, with a resistive load in place of the speaker and the voltmeter across that, they make a very nice valve voltmeter, provided the volume control is not disturbed after the initial setting.

A response curve can then be obtained quite easily by converting voltage ratios to the voltage at, say, 1,000 c/s into decibels by the usual formula: Decibels = $20 \times \log$ ratio—or by referring to decibel tables or abacs if these are available.

Be careful not to overload the amplifier when taking these readings. Knowing the maximum power output of the amplifier and remembering that Watts = V^2/R calculate the highest reading V you can allow to be seen on the voltmeter.

In the absence of an LP test record, the circuit can be checked satisfactorily using a 78-r.p.m. standard frequency record, run at 78 r.p.m. and using the correct stylus. To the readings obtained, when converted to decibels, add the bass-cut figures quoted on the record, then the final curve should look like the inverse of curve C in Fig. 6 if equalization is correct. This method is quite accurate except for the top resonance, if any.

Controls for a Pickup.—Two controls are really sufficient—a top attenuator, preferably switched in 4 or 5 stages, to cover age, origin, and condition of 78-r.p.m. records, and a changeover switch to effect the major 78—LP change. A three-position switch is useful, in the form 78—LP—Radio. The more ambitious might like to expand it to:—78 NORMAL—78 FFRR—LP—Radio, but the extra top of the Decca FFRR can be dealt with quite adequately by the normal top control.

Two top cut circuits are shown. Fig. 5(a) is the conventional one with 6 db/octave attenuation, starting higher or lower in the scale according to the capacity chosen. With the values given attenuation starts, according to the switch position, at frequencies in the neighbourhood of 10, 6 and 3 kc/s and for really bad records at about 300 c/s. Fig. 5(b) varies the slope from 5 to 20 db/octave, with a little variation of the starting point, which is in the region of 1,000-2,000 c/s.

A 78/LP changeover is suggested, rather than using the top and bass controls; this enables the changeover to be made with a single operation. Further, exact equalization of LP recordings is not possible with simple cut/boost controls, and it is in any case desirable that the whole of the variable top and bass control range should be available for special conditions.

78 r.p.m.—(i) *The recording characteristic.*—Fig. 6 shows (A and B) the two recording characteristics produced in this country in terms of velocity against frequency.

(ii) *Correction circuits.*—The magnetic types require a bass-lifting circuit of the type shown in Fig. 7(a). In reality it "attenuates-everything-but-the-bass," a matter of 10 times for both sets of values given, so that adequate gain must be available in the amplifier.

The circuit of Fig. 7(b) for the crystal type is similar in this respect. With the older crystal types it must be used with discretion, though, on account of the rather large high-note resonance. An elaboration of this circuit which was recommended for use with the Acos GP12 is shown in Fig. 8. This pickup followed closely the theoretical amplitude operation of piezo crystals.

With the later types of crystal pickup, such as the Acos GP20, the high-frequency response does not

follow this law, but has an internally-compensated response which approximates to a velocity law at high frequencies when terminated by a resistive load. For those who would like to improve the response, a circuit is shown in Fig. 9.

R ₁	R ₂	R ₃	C
100kΩ	10kΩ	≥ 500kΩ	0.05μF
200kΩ	20kΩ	≥ 1MΩ	0.05μF

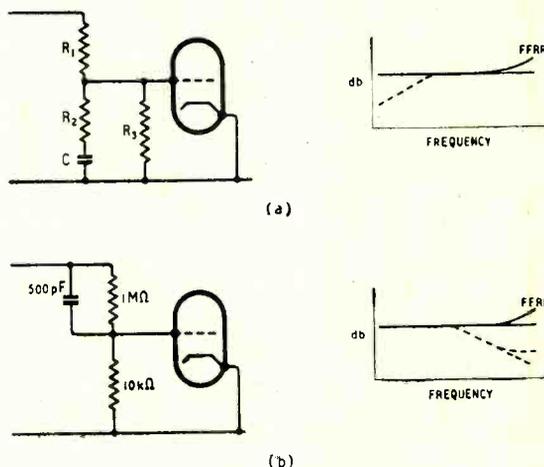


Fig. 7.—Simple compensating circuits for 78-r.p.m. recordings (a) magnetic (velocity) pickups, (b) crystal (amplitude) pickups. The dotted curves indicate voltage output before correction.

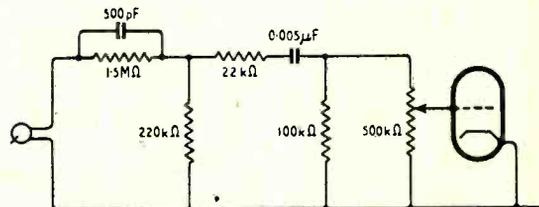


Fig. 8.—Correction circuit for the Acos GP12 pickup on 78 r.p.m. records.

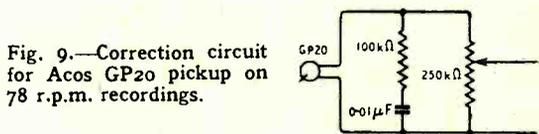
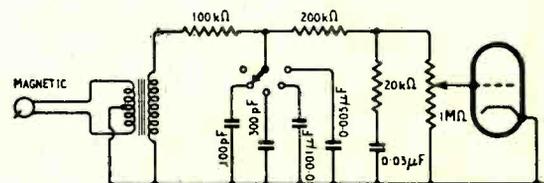


Fig. 10.—Complete compensating circuit (78 r.p.m.) for magnetic (velocity) pickups.



None of these circuits include top correction for the difference between standard and FFRR characteristics, but this will be covered by the suggested top control.

A complete circuit for a magnetic pickup is shown in Fig. 10, and for an Acos GP20 in Fig. 11. This latter includes the anti-rumble circuit of Fig. 4.

Long-playing (33½ r.p.m.).—The successful adaptation of standard pickups for microgroove recording is dependent on the recognition of several factors. If the pickup will not track standard 78-r.p.m. test recordings satisfactorily at 14 grams or less, it is improbable that the same pickup (with a correct radius

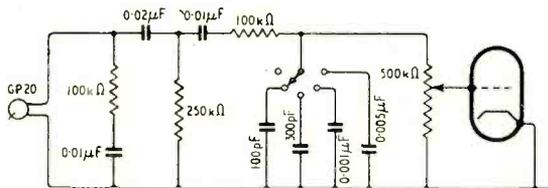


Fig. 11.—Complete compensating circuit (78 r.p.m.) for Acos GP20 pickup.

Fig. 12.—Output of high-impedance Decca Model D2 (3-pin type) moving-iron pickup on 33½ r.p.m. test record ; A, without correction ; B, with equalizer circuit shown inset.

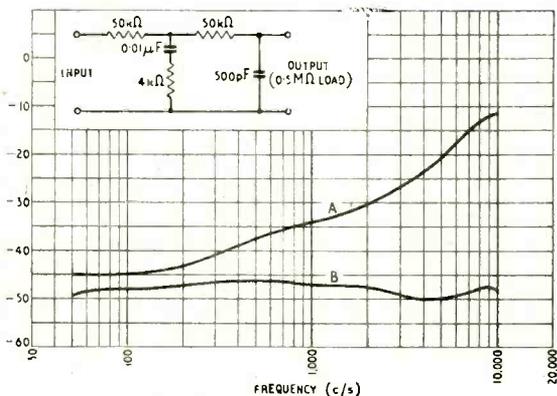
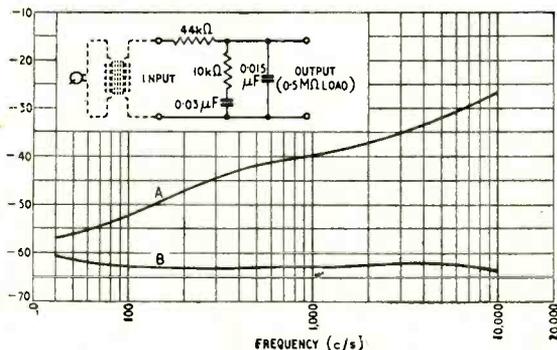


Fig. 13.—Low-impedance Leak moving-coil pickup and transformer on 33½ r.p.m. test record ; A, without correction ; B, with equalizer circuit.



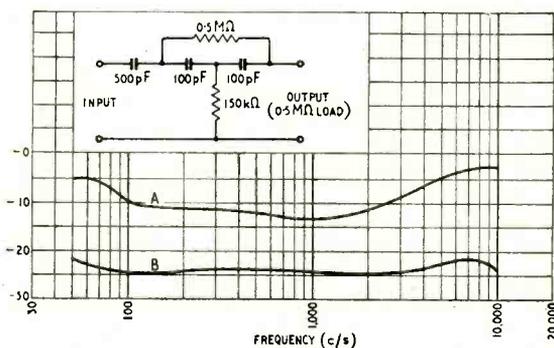
stylus, of course) will track long-playing records at 7 grams. The tracking problem is not only important at the low frequencies, but also at the extreme high frequencies, where the velocity of the microgroove recording approaches that of the standard record, although the tracking weight of the pickup is considerably less and mechanical impedance of the armature is rising rapidly.

Assuming, however, that the pickup is satisfactory in this respect, there is no reason why it should not give satisfactory results on microgrooves, providing it is correctly equalized. It should be noted that the effective resonance frequency of the armature system is usually decreased by about half an octave on microgroove compared with standard records, so that if any resonance is at all apparent in the upper register on standard records it will, in general, be more prominent and at a lower frequency on microgrooves.

Frequency correction.—As examples, two high-fidelity magnetic pickups and a similar type crystal pickup are presented herewith. The open-circuit response characteristic of the Decca Model D2, 3-pin type, magnetic pickup is given in Fig. 12(A). It will be seen that this response, in the mid and lower registers, approximates to the recording characteristic, Fig. 6(C), but in the higher frequencies rises rather more steeply because of the lowered resonant frequency of the armature system. The electrical network, shown inset, corrects the response of the pickup and gives the overall response shown in curve B. Although this final response is not in the "straight line from d.c. to infinity" beloved by the pedants, it is well within ± 2 db. The components in question were radio-tolerance units. It may be pointed out that the 500 pF terminating condenser and the 4,000-Ω resistance may have to be varied with individual pickups to get a satisfactory balance between the middle and upper frequencies. This equalizer has been successfully used with a variety of pickups of up to 5,000 ohms impedance (connected direct or taken on the secondary of the coupling transformer) which normally require a load resistance of quarter to half megohm.

The best of the moving-coil pickups show a resonance of at least 20 kc/s on standard 78-r.p.m. records and even when played on microgroove records the resonance is seldom lower than 15 or 16 kc/s and the pickup response is very nearly that of the record. With care the low-frequency resonance can be below 30 c/s and the low-frequency response will also be

Fig. 14.—Cosmocord GP20 crystal pickup on 33½ r.p.m. test record ; A, without correction ; B, with "bridged T" equalizer circuit.



very nearly that of the recording characteristic. The Leak moving-coil pickup and its transformer are shown as being representative of this type of instrument. The open-circuit response is given in Fig. 13(A); when connected with the appropriate equalizer network the response shown at B is obtained. The high-frequency "roll-off" is controlled by the 0.015- μ F condenser; decreasing it to 0.01 μ F will increase the 10-kc/s response by about 4db. This condenser can be adjusted to meet individual requirements. If the low-frequency end is considered excessive a condenser can be inserted between the transformer secondary and the 44,000 Ω resistor. A value of 0.25 μ F will give a reduction of about 6 db at 50 c/s. The "roll-off" at low frequency can be adjusted to suit conditions by varying the value of this condenser, lower values increasing the attenuation.

The case of the crystal pickup is shown in Fig. 14,

the unequalized response being shown at A and the equalized at B. It will be seen that a modified "bridged T" network is used, and, within reason, the equalizing is independent of the pickup impedance. In all cases the terminating resistance should be 0.5 M Ω . If the input impedance of the amplifier is other than this value, a simple potential-divider matching arrangement should be used.

It may be found, especially with cheaper type turntables or units that have been modified from 78 r.p.m., that motor rumble is excessive. Should this be the case, the high-pass filter unit described earlier may be used successfully, but should be connected between the equalizing unit and its load resistance.

In conclusion, the authors are indebted to Messrs. Decca Radio and Television, Cosmocord and H. J. Leak & Company for information regarding characteristics of records and pickups.

SHORT-WAVE CONDITIONS

October in Retrospect : Forecast for December

By T. W. BENNINGTON (Engineering Division, B.B.C.)

DURING October the average maximum usable frequencies for these latitudes increased very considerably during the daytime, and decreased considerably during the night. These variations were in accordance with the normal seasonal trend.

Daytime working frequencies for long-distance communication were fairly high, though not so high as had been expected. The 28-Mc/s band was sometimes, but not often, usable to the U.S.A., though it was frequently usable in more southerly directions. The failure of the working frequencies to increase as much as was expected was probably due, in part, to the large amount of ionospheric disturbance, and in part to the rapidly decreasing solar activity. Night-time working frequencies were also low, being generally below 9 Mc/s. There was a small decrease in the rate of incidence of Sporadic E, and not much communication on high frequencies occurred by way of this medium.

Sunspot activity was, on the average, slightly higher than during September, but the general level has now fallen by well over one-third since sunspot maximum.

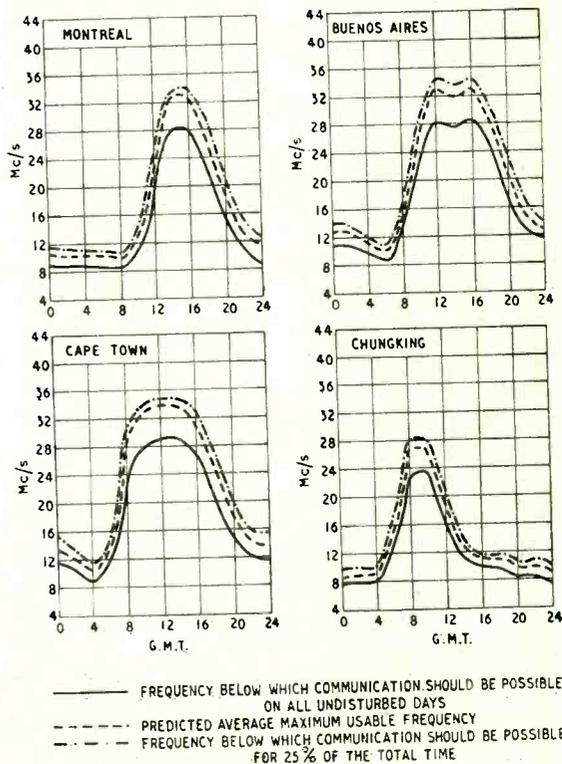
Several severe ionospheric storms occurred during the month, the most disturbed periods being 1st to 8th, 14th to 18th, 23rd to 24th and 28th to 31st. No Dellinger fade-outs have, as yet, been reported.

Forecast.—There may be a small decrease in the daytime m.u.f.s for these latitudes during December, as compared with those for November. Night-time m.u.f.s should also decrease and perhaps reach their lowest values for the present winter season.

As a result of these variations, the long-distance working frequencies should be rather high by day, though the higher frequencies will be usable only for relatively short periods daily. It is doubtful whether 28 Mc/s will be regularly usable over most circuits, though it may well be so on those running in southerly directions. The medium-high frequencies will provide the main means of daytime communication in most directions, and at night 6 to 7 Mc/s should be the highest regularly usable frequencies.

Sporadic E is not likely to be very prevalent and medium-distance communication on high frequencies by way of this medium should be very infrequent. Ionospheric storms are not, as a rule, particularly common during December, but those which do occur are likely to be troublesome, particularly at night.

The curves indicate the highest frequencies likely to be usable over four long-distance circuits during the month.



NEW BOOKS

Aerials for Centimetre Wavelengths (Modern Radio Technique Series). By D. W. Fry and F. K. Goward. Pp. 172+x, figs. 65. Cambridge University Press, 200, Euston Road, London, N.W.1. Price 18s.

THIS is a book of interest primarily to engineers concerned with the design and development of specialized aerials for radar applications at centimetric wavelengths. The authors themselves were concerned at the Telecommunications Research Establishment in much of the early design of aerials of this type. The treatment is not elementary, and a considerable knowledge of transmission lines, wave-guides, and general aerial and radiation theory on the part of the reader is assumed. Nevertheless, the mathematical aspect is not unduly laboured, and mathematical expressions are confined to the minimum necessary for the purpose of theoretical design.

It is in no sense a practical designer's handbook. It describes and catalogues the various types of aerials which have been used or are used for particular radar work, and it discusses in considerable detail the analytical methods of designing a radiating system so as to obtain a specified radiation pattern. Generally a centimetric aerial comprises two principal parts—a primary radiator, such as a dipole or an open-ended wave-guide, which feeds the energy to the secondary radiator, the latter being a reflector, a lens or a horn: primary and secondary radiators are dealt with in separate chapters, which are sub-divided according to the various distinct types.

A large part of the work is concerned with means of scanning, that is, causing the radiated beam to explore continuously a particular area in space. It is shown to be a valuable feature of centimetric aerials that scanning can usually be accomplished at the primary radiator which leads to simpler mechanics and higher scanning speeds than if displacement of the secondary radiator were necessary.

The close resemblance between centimetric work and optical theory is well brought out, and the application of optical methods to the design of centimetric reflectors and lenses is described. Both dielectric and metal plate type lenses are treated, and a note on errors and aberrations in optical systems is given in an appendix.

There are liberal references in the text to relevant literature, all the references being grouped in the form of a valuable bibliography at the end of the book. Printing and production are alike excellent, and the book is a worthy addition to the publishers' "Modern Radio Technique" series. C. G.

Super-Regenerative Receivers. By J. R. Whitehead, Ph.D., A.M.I.E.E. Pp. 169+xiii. Cambridge University Press, 200, Euston Road, London, N.W.1. Price 21s.

BEFORE the war the super-regenerative receiver had gained a reputation for being a tricky and unpredictable device that sometimes gave wonderful results. Published information was considerable in quantity, but generally evasive when it came to clear-cut questions such as: how its signal/noise ratio compared with that of a superheterodyne; how one would design it for a given selectivity; how much gain could be obtained, and what factors determined it; what was the optimum quench frequency and waveform; how the shape of the frequency response curve compared with those of other types of receiver; and so on.

The answers to these and other questions are given in clear and definite terms in the book under review—the first to be devoted exclusively to the super-regenerative receiver. Although it has resulted from work that was done in developing radio and radar equipment for the war, it is by no means a one-sided account of specialized

development. On the contrary, the author has started by getting down to the essential core of any super-regenerative circuit; in fact, of any oscillator—a parallel combination of inductance, capacitance, and conductance. The special feature of super-regeneration—periodical variation of the conductance each side of zero—is then considered. The treatment is therefore perfectly general, and the influence of particular conditions and modes of operation are only brought in when the more general results have been fully established.

The treatment is mathematical and makes use of fairly advanced techniques, but, even if the reader is insufficiently adept to follow all the steps, he should have no difficulty in making use of the results, for the author has arranged his work admirably and has expressed the results clearly in words and in formulae that can be directly applied in design. An appendix contains valuable graphical design data, and the final chapter is devoted to a representative selection of practical circuits, complete with component values.

Most of the pre-war knowledge and use of the super-regenerative receiver were in its logarithmic mode, in which oscillations are allowed to build up to saturation, resulting in strong a.g.c. action, and distortion of deep modulation. So it is only reasonable that special prominence should be given to the linear mode, in which at the cost of some complication of the equipment the distortion is avoided and greater selectivity obtained. The differences between this and the logarithmic and self-quenching modes are adequately covered.

The proof of this attractive-looking pudding was in the remarkable reliability and consistency in performance of 200,000 IFF receivers (to mention only one item of super-regenerative equipment) during the war. The approximations which the author has had to make in order to get anywhere at all with his mathematical treatment seem to be fully justified by the results, within the limits laid down. Confidence in the diagrams is reinforced by a number of excellent oscillograms from actual receivers, in which the various conditions are clearly exemplified.

Errors appear to be confined mainly to incidental results of last-minute changes in the book; for example, what appears as Appendix 2 was presumably at one time No. 3, for several of the references are so numbered. Similarly with Fig. 3.3. And a paper which on p.67 is described as "in the Press" has, by the time one reaches the Bibliography, been published. These are trifling slips. One would wish that every technical book treated its subject so satisfactorily.

M. G. S.

How to Become a Radio Amateur is a 58-page American publication, now in its eleventh edition, and its aim is to show the beginner how to make a start in amateur transmission. It opens by giving a very brief account of basic radio theory.

The main body of the book is devoted to the choice of apparatus for the beginner with emphasis placed on construction as being the surest way of getting to know how things work. The most ambitious receiver described is a 4-valve communications superhet. V.H.F. apparatus is included.

The book, which is published by the American Radio Relay League, West Hartford, 7, Connecticut, U.S.A., is well illustrated with diagrams and photographs and in the U.K. is obtainable through the Radio Society of Great Britain, New Ruskin House, Little Russell Street, London, W.C.1. It is delivered direct from the U.S.A. in from four to five weeks and the price is 4s.

Variable Filter Tuning

(Concluded from p. 358 of the previous issue)

2.—Design Procedure for R.F. and I.F. Stages

By A. B. SHONE, B.Eng., A.M.I.E.E.

IN the earlier part of this article we established in Fig. 3 the general shape of the receiver response characteristic at which we intend to aim.

It is possible to obtain such a response in the long-wave band by any of the three alternative circuits which were given in Fig. 9. Considering the case of the long-wave Droitwich station, the response required is shown in Fig. 10, i.e., sensibly flat from 195 kc/s to 205 kc/s and heavily attenuated at 191 kc/s and below and at 209 kc/s and above. Using filters, this would require sections introducing a heavy attenuation at 1.02 times the cut-off frequency (i.e., 209/205 kc/s). As will be seen in the curves given later, this is quite practical.

In the medium-wave band it is not really practical to obtain such characteristics directly by any of the three methods compared, and a superheterodyne type of circuit becomes almost essential.

It is in choosing a suitable intermediate frequency that the filter-tuned receiver begins to depart from normal practice. If the delineation of the response is to be divided between the high-frequency filter and the intermediate-frequency filter, then it is reasonable, if not axiomatic, to suppose that the minimum number of sections will be required when the work is shared equally between the two filters.

Referring to Fig. 11: If f_k represents the carrier frequency of the wanted transmission and f_i and f_l the extremes of its sidebands, if f_p represents the carrier of the second channel and f_o and f_s its objectionable sidebands and if f_c represents the intermediate frequency with f_b and f_d being the sidebands it is desired to receive unattenuated and f_a and f_g being the adjacent stations carriers it is required to reject, then we can set down this equation if the two filters are to be of equal sharpness:—

$$\frac{f_o}{f_l} = \frac{f_g}{f_a}$$

or

$$\frac{f_k + 2f_c - 5 \text{ kc/s}}{f_k + 10 \text{ kc/s}} = \frac{f_c + 9 \text{ kc/s}}{f_c + 5 \text{ kc/s}}$$

Taking the worst position in the medium-wave band i.e. when $f_k = 1,500$ kc/s, we get $f_c = 56$ kc/s approximately. This intermediate frequency will require filters whose sharpest sections introduce a heavy attenuation at 1.06 times their cut-off

frequency (i.e., $\frac{56 \text{ kc/s} + 9 \text{ kc/s}}{56 \text{ kc/s} + 5 \text{ kc/s}}$) and the high-frequency filters will require sections of equal sharpness.

Bearing in mind that the high-frequency filter has to be variable over the medium-wave band, i.e., from 600 kc/s to 1,500 kc/s, whereas the intermediate-frequency filter is a fixed filter (or, at the most complicated, a filter with small percentage changes to give the variable characteristics found desirable in Fig. 3), it may be desirable to reduce slightly the high-frequency filter and, at the same time, increase the intermediate frequency filter by raising the

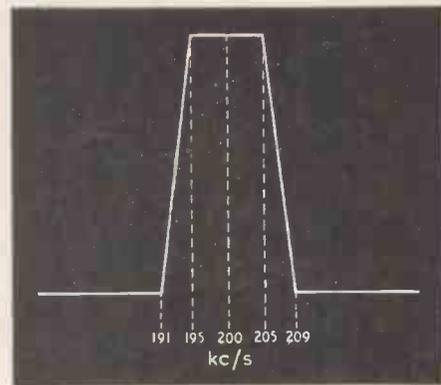
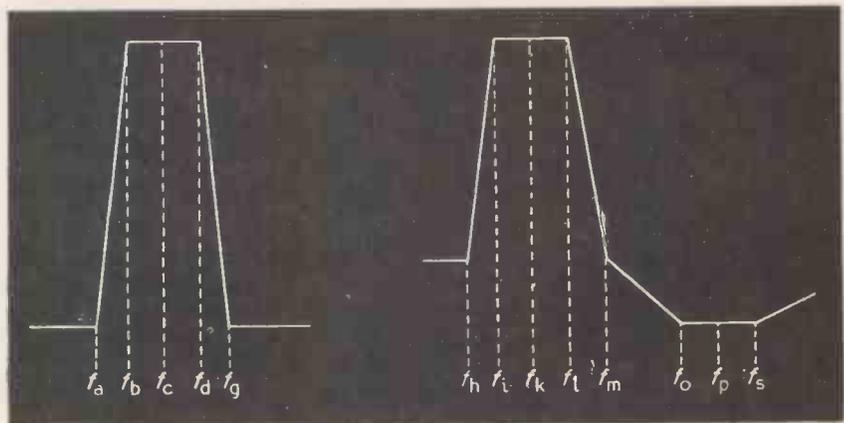


Fig. 10. Wanted and unwanted bands in the Droitwich long-wave case.

Fig. 11. Wanted and unwanted bands in the superheterodyne case.



intermediate frequency slightly. If it is increased to 80 kc/s, the sharpest sections in the high-frequency filter become 1.09 (i.e., $\frac{1,500 \text{ kc/s} + 160 \text{ kc/s} - 5 \text{ kc/s}}{1,500 \text{ kc/s} + 10 \text{ kc/s}}$) while the sharpest sections in the intermediate frequency filter are correspondingly reduced to 1.047 (i.e., $\frac{80 \text{ kc/s} + 9 \text{ kc/s}}{80 \text{ kc/s} + 5 \text{ kc/s}}$). However, as will be seen below, this process should not be carried too far as the very sharp filter sections become relatively inefficient.

Considering now the actual filter sections available, the filters can be built in the form of high- and low-pass filters in tandem, the former having a lower cut-off frequency than the latter. Taken together, they jointly form a bandpass filter. This arrangement, although requiring a few more components than conventional bandpass filters, is preferable as the component values are in general much more convenient.

The sections we can use are tabulated in Fig. 12, together with the relevant formulae for calculating component values expressed in terms of R the terminal impedance of the filter, f_c the cut-off frequency, and a term m . The latter term is evaluated

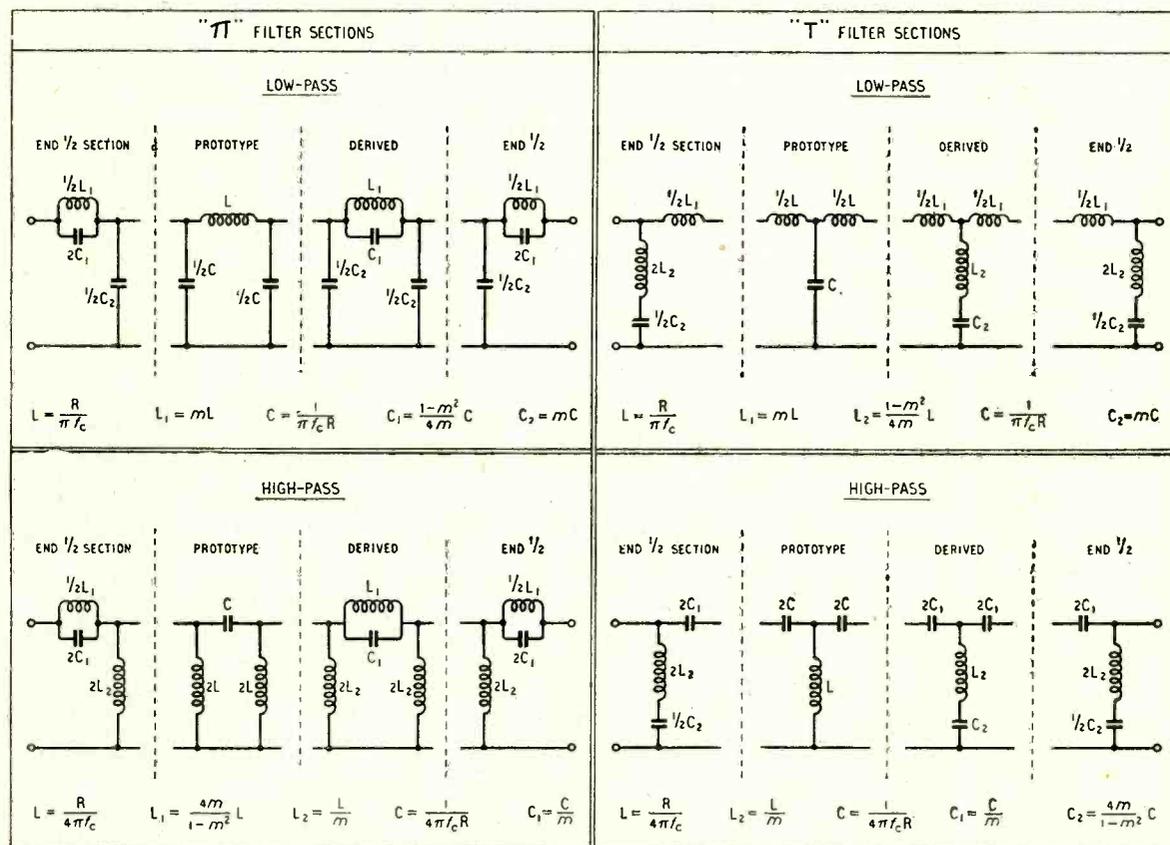
by the formula $m = \sqrt{\frac{a^2 - 1}{a}}$ where a is the ratio of the frequency of maximum attenuation to the cut-off frequency of the filter section. We can use either the "π" form of the section of the "T" form, whichever is

the more convenient. As we want to keep the variable condensers down to a minimum, we shall in general use the "T" form of the low-pass filter and the "π" form of the high-pass filter.

In each case there are two main sections, the prototype sections and the derived sections. (In each case the filter ends in half a derived section.) The prototype section begins to attenuate at the cut-off frequency and continues with steadily increasing attenuation all the way to infinite frequency in the case of the low-pass filter (or to zero frequency in the case of the high-pass filter). The derived sections, however, are arranged to give their maximum attenuation at some frequency between infinite frequency (in the case of the low-pass filter or zero frequency in the case of the high-pass filter) and cut-off frequency. Between these limits we can make the frequency of maximum attenuation of a derived section what we like, and we describe the section by the ratio of this frequency to its cut-off frequency in the case of the low-pass filter or the inverse in the case of the high-pass filter. This ratio is usually known as the "a" of the sections and a is always greater than 1. (We can, in fact, now describe the prototype section as being merely a special case of the derived section where $a = \text{infinity}$.)

The attenuations obtainable with sections having various values of a are shown in Fig. 13 where f_c is the cut-off frequency. In these curves it is assumed that the coils used have a ratio of reactance to resistance (Q) of 100 which should be quite practical at

Fig. 12. Filter design formulae.



these frequencies. (The coils should be either wave-wound or wound on dust cores using formers with at least four slots in order to keep down their capacitance.)

The characteristic impedance of various sections—by which is meant the impedance looking into such a section when terminated with an infinite train of similar sections—will vary with frequency, and only equals the value R at zero frequency in the case of the low-pass and at infinite frequency in the case of the high-pass sections. For all values of a the derived sections quoted in Fig. 12 have the same characteristic impedance as the prototype sections, and therefore the two types can be connected together without introducing any impedance mismatch. But the mid-section impedance of a derived half-section, when correctly terminated with its characteristic impedance, will not be equal to the characteristic impedance of the whole section, but will vary with a as is shown in Fig. 14 where the mid-section impedance is expressed in relation to R . For certain values of a around 1.25 the ratio is constant over a large portion of the pass band of the filter. Such a half-section is therefore very useful for terminating a filter, as its mid-section impedance is approximately a constant resistance.

An inspection of the curves of Fig. 13 shows the relative inefficiency of the sections having low values of " a ," for not only do they put in less attenuation at their resonant frequency but they require to be used in conjunction with other sections of higher value of " a " if the filter is to maintain its attenuation in the stop range. For instance, it becomes necessary to follow a section having $a = 1.02$ by a section of $a = 1.09$, if the attenuation is to be maintained beyond the cut-off frequency. Similarly, a section of $a = 1.09$ will require to be followed by a section having an " a " of about 1.6 and so on. There are, of course, an infinite number of values of " a " which might be chosen, but as it is impossible to give a complete set of filter tables in an article such as this, the above values for " a " have been chosen as being representative. These particular values are advantageous because $a = 1.02$ gives $m = 0.2$, $a = 1.09$ gives $m = 0.4$, while $a = 1.6$ gives $m = 0.8$. As these three values of " m " are each double the previous value, it will be seen from the formulae given in Fig. 12 that using such values there will be a great deal of similarity in the component values of the various sections. Similarly $a = 1.06$ gives $m = 0.33$, $a = 1.35$ gives $m = 0.66$ and $a = \infty$ gives $m = 1$, and again using these sections together we may expect to get a certain similarity in component values.

A further inspection of the formulae in Fig. 12 will reveal that in the formulae for the prototype low-pass filter

$$L = \frac{R}{\pi f_c} \text{ and } C = \frac{1}{\pi f_c R}$$

Eliminating R we get,

$$LC = \frac{1}{(\pi f_c)^2} \text{ or } f_c = \frac{\sqrt{LC}}{\pi} \quad \dots \quad (1)$$

From this we see that we can vary the cut-off frequency by altering either L or C or both.

Eliminating f_c we get,

$$\frac{L}{C} = R^2 \quad \dots \quad (2)$$

From equations (1) and (2) we see that if we alter both L and C maintaining the ratio $\frac{L}{C}$ constant, we can

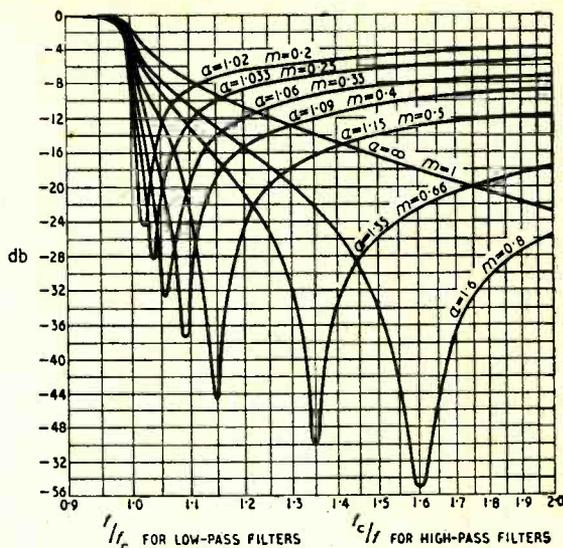


Fig. 13. Attenuation curves of typical filter sections.

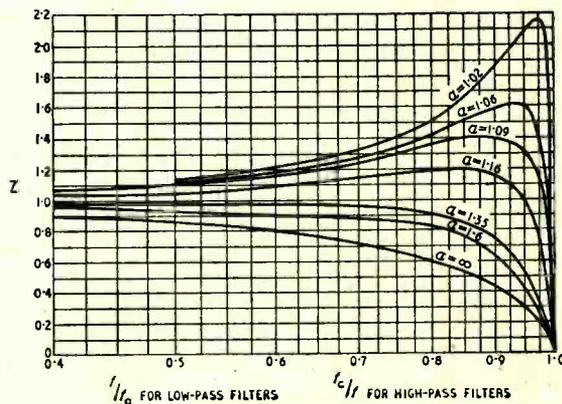
alter the cut-off frequency of the filter and at the same time keep R constant, and this is, in fact, what is generally done.

If, however, we are prepared to let the value of R vary according to equation (2), then by equation (1) we can vary the cut-off frequency by altering either C or L . In practice it is easier to alter C , as ganged condensers are readily available commercially.

Considering the medium-wave band, the frequency range is from about 600 kc/s to 1,500 kc/s, or a ratio of 2.5. By equation (1) this will require a change of L or C by 2.5^2 and this in turn will cause R to alter by a ratio of 2.5. To be absolutely correct we could make the termination of the filter a variable resistance and adjust it to the right value for the particular cut-off frequency. In practice this is not necessary, and if it is made a fixed resistance of $\sqrt{2.5}$ its correct value when the filter is adjusted for a cut-off of 600 kc/s, then the error introduced is not serious and we need not worry about it.

If it is chosen to alter the cut-off frequency by varying C (keeping L constant), then the " π " type

Fig. 14. Mid-section impedance of derived sections expressed relative to R , plotted against frequency relative to f_c .



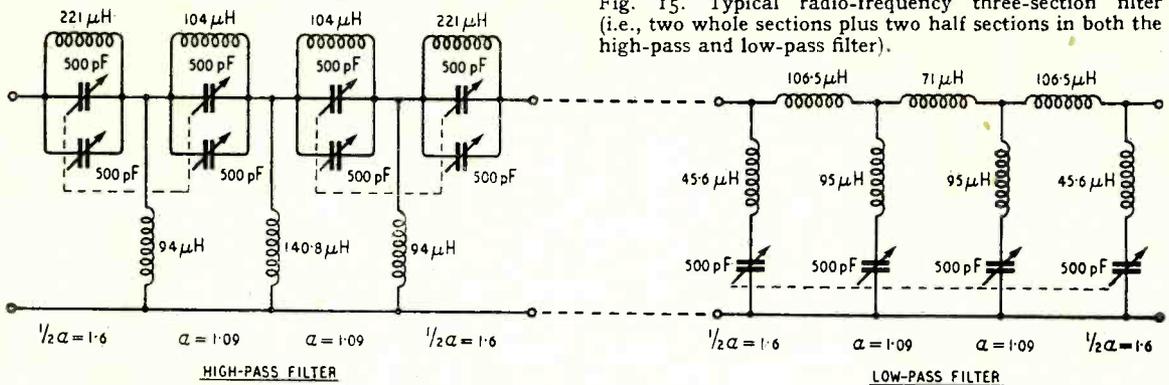


Fig. 15. Typical radio-frequency three-section filter (i.e., two whole sections plus two half sections in both the high-pass and low-pass filter).

of low-pass filter and the "T" type of high-pass filter should be avoided, as the derived forms of these sections call for two variable condensers of different value, which are not readily available in ganged form.

By way of an example, let us consider the design of a high-frequency filter with a cut-off ratio of 1.09. Using the "T" form of the low-pass filter, we can keep all the condensers to the same value if all the sections are derived and the half sections at the end have an "m" of double the middle sections, i.e., if the middle sections are $m = 0.4$ ($a = 1.09$) and the half sections at the end are $m = 0.8$ ($a = 1.6$), then all the condensers in the filter are 0.4 of the value of the condenser in the prototype section, which is

$$C_{lp} = \frac{0.4}{\pi f_{lpc} R} \dots \dots \dots (3)$$

where f_{lpc} is the cut-off frequency of the low-pass filter.

Again, using the "π" section of the high-pass filter, we can keep all the condensers in the filter to the same value if all the sections are derived and if the

half sections at the end have an "m" of double the middle sections. Again, using $m = 0.4$ ($a = 1.09$) for the middle sections and $m = 0.8$ ($a = 1.6$) for the half sections at the end, the condensers are $\frac{1}{0.4}$ of the condenser for the prototype section, which is

$$C_{hp} = \frac{I}{4\pi f_{hpc} R} \times \frac{I}{0.4} = \frac{I}{1.6\pi f_{hpc} R} \dots \dots \dots (4)$$

where f_{hpc} is the cut-off frequency of the half-pass filter.

Bearing in mind (Fig. 3 of previous instalment) that we required f_{hpc} to be 0.8 of f_{lpc} , we get

$$C_{hp} = \frac{I}{1.6\pi \cdot 0.8 f_{lpc} R} = \frac{0.8}{\pi f_{lpc} R} \text{ (approx.) } \dots \dots \dots (5)$$

From the above it will be seen that we have now got all the condensers in the low-pass filter the same and all the condensers in the high-pass filter equal to and double the value of those in the low-pass filter. This was another important reason in the choice of these particular values of "a" as it means that standard condensers can be used throughout, the only difference between high- and low-pass filters being that each condenser in the former is built by putting two condensers in parallel.

The above completes the design considerations for the high- and low-pass filters except to give an idea of practical values. If a commercial $0.0005 \mu F$ ganged condenser is made the basis of the design, then putting $C_{lp} = 0.0005 \mu F$ when $f_{lpc} = 600 \text{ kc/s}$ in equation (3), we get $R = 400 \text{ ohms}$ at 600 kc/s .

As already explained, a

Fig. 16. Calculated characteristic of radio-frequency filter as in Fig. 15 for position where all variable capacitors are set to $0.0002 \mu F$.

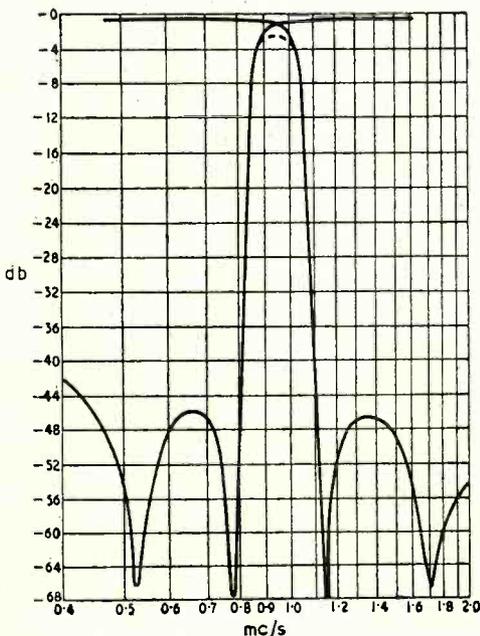
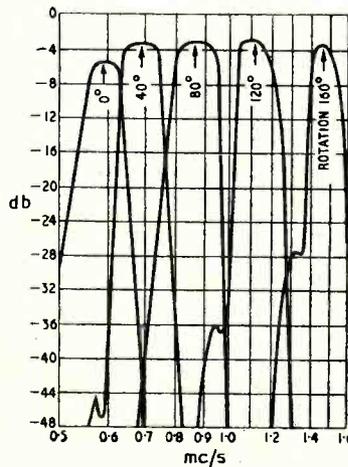


Fig. 17. Measured attenuations for various capacitor settings of radio-frequency filter as in Fig. 15.



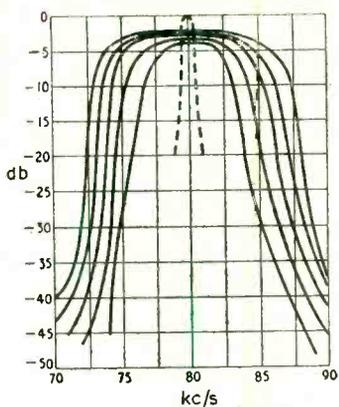


Fig. 18. Measured characteristics of variable intermediate-frequency filter for various capacitance settings.

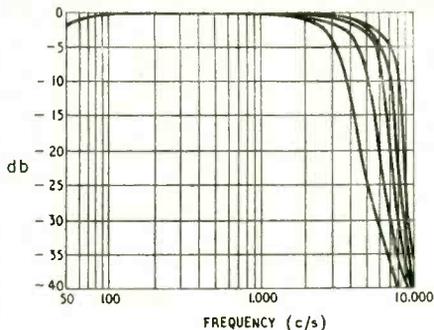


Fig. 19. Overall a.f. response of the receiver for various positions of the variable i.f. filter.

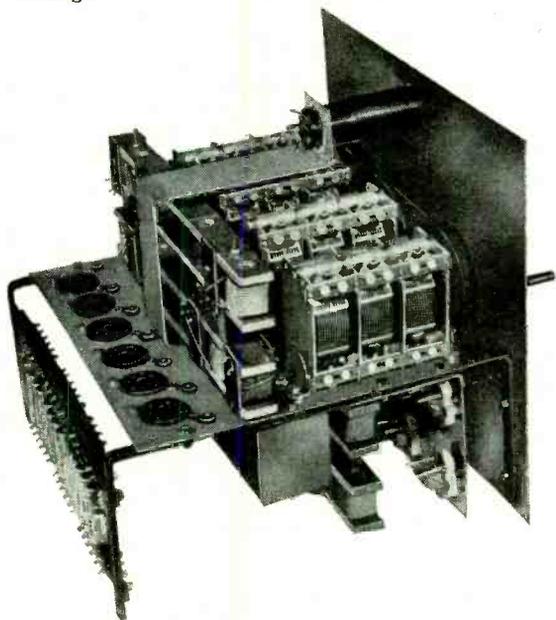
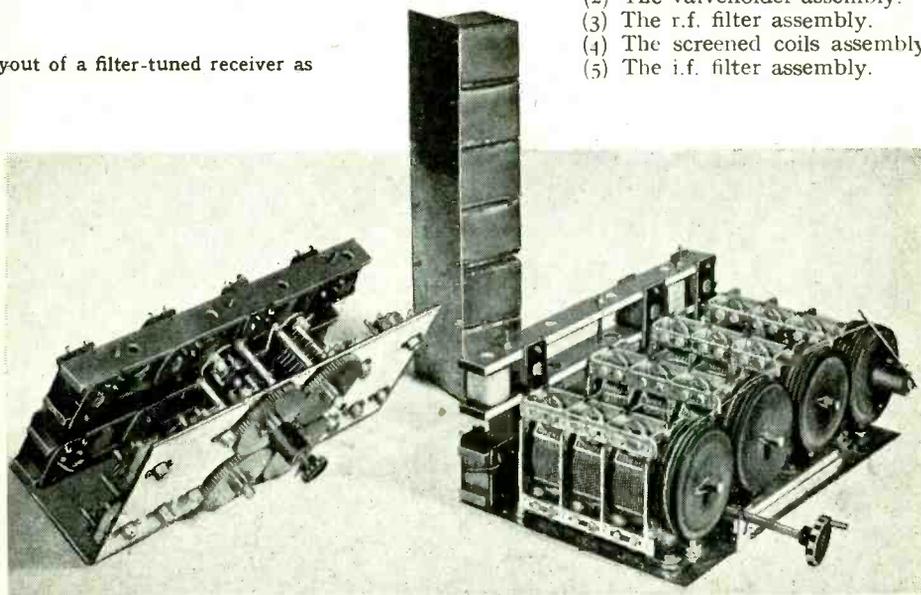


Fig. 20. Practical layout of a filter-tuned receiver as seen from the back.

Fig. 21. The three main assemblies. (Left) the i.f. filter, showing the ten fixed capacitors (air-spaced trimmers are used for convenience) and the eight variable condensers (four "split stator" condensers were used for convenience) connected by gears. (Centre) the screened coil assembly and (right) the r.f. filter showing the wire and drum drive.



suitable mean terminating resistance would be this value multiplied by $\sqrt{2.5}$, i.e., 650 ohms.

The circuit of the above filter is given in Fig. 15, its calculated characteristic is given in Fig. 16 and its measured characteristic at various points on the medium-wave band is given in Fig. 17.

The above is a typical r.f. filter. The i.f. filter follows on similar lines but from consideration of component values and in order to work at a suitable intervalve impedance, it is designed with a characteristic impedance of 12,000 ohms. In addition the con-

densers are not made completely variable, but consist of a fixed portion and a 10 per cent variable portion: further the variable portions in the high- and low-pass sections of the filter are connected in opposition in such a way that the cut-off frequency of the one rises as the other falls and finally the ratio of the high- and low-pass variable condensers is chosen to be such that for any movement of the condensers both filters change their cut-off frequency by the same amount in cycles per second.

Overall A.F. Response

The measured characteristic of this filter for various positions of the condenser shaft is shown in Fig. 18. (The dotted curve represents the characteristic of a sharply-tuned circuit which is in the "magic eye" circuit and enables the receiver to be tuned to the centre of its i.f. characteristic—an important requirement in such a receiver as this.) The audio-frequency response of the receiver for various positions of the i.f. condensers is shown in Fig. 19.

In its simplest form the practical design of such a receiver is shown in Fig. 20 which is a back view. It contains five sub-chassis namely:—

- (1) The decoupling resistor and condenser assembly.
- (2) The valveholder assembly.
- (3) The r.f. filter assembly.
- (4) The screened coils assembly.
- (5) The i.f. filter assembly.

The last three assemblies are shown removed in Fig. 21 which indicates the method of ganging the condensers in the r.f. and i.f. filters. In the former case a wire and drum drive is used, and as two of the condensers are above earth potential they are mounted on a sheet of Paxolin and the drums are made of ebonite: no difficulty is experienced in ganging the condensers if the grub screws in the drums are tightened when all the condensers are maximum. The condensers are not likely to get out of gang if suitable wire is used, but if they should they can quickly be re-ganged by slackening off the grub screws, setting all the condensers to maximum and then retightening the screws.

In the case of the i.f. filter, air dielectric trimmers have been used for the fixed portion of the capacitances and the variable portions are coupled together by means of gears, though a wire and drum drive could equally well have been used.

Space has precluded giving complete details of the receiver design but it is hoped that enough has been given to show the general lines of approach. The resulting receiver has much to recommend it, particularly its relative freedom from noise and its variable i.f. filter, which can be adjusted continuously and without introducing clicks or noise of any kind until the best position is found. It is,

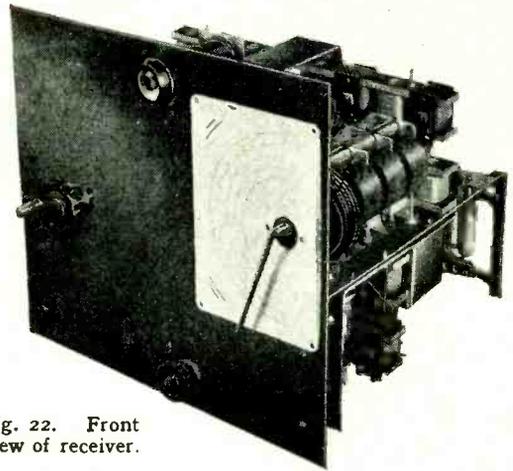


Fig. 22. Front view of receiver.

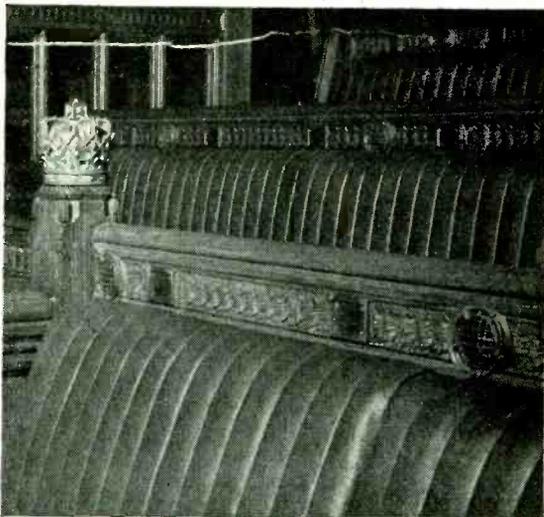
however, a complicated design and cannot be built without adequate test equipment. Furthermore, when built it is still only a compromise solution. In the author's opinion, it is the best compromise possible in modern listening conditions.

HOUSE OF COMMONS S.R.E.

A PART from the general interest in the sound reinforcing system in the new Chamber of the House of Commons this low-intensity installation is of particular interest in that it has been designed to ensure that all members can hear and, if desired, be heard without having to leave their seats.

To achieve this a large number of low-intensity loudspeakers have been installed in the woodwork at the back of the seats—one unit for two members—and six uni-directional microphones have been suspended from the ceiling over the front benches and three each side, mounted on cantilever arms, over the back

Loudspeakers behind bronze grilles in the carved oak rail above members' seating in the new House of Commons.



benches. The selection of the microphones during debates and the general supervision of the installation is undertaken by an operator in a cubicle overlooking the chamber.

To obviate "howl" caused by acoustic feedback when microphones and loudspeakers are in close proximity, the reproducers are arranged in groups which are co-related with the pick-up area of the microphones. When a microphone is brought into circuit the reproducers in the immediate vicinity are muted and in certain cases the input to those in adjacent areas is attenuated.

The main equipment comprises fourteen microphone pre-amplifiers with stand-by units. After pre-amplification, frequency and volume correction, the signals are passed through a "buffer" amplifier to raise the level sufficiently to energize the power amplifiers. There are eighteen of these, plus spares, and each one provides power for one loudspeaker zone, the input to which is connected through two relays and attenuators to provide, automatically, the correct degree of muting or volume reduction associated with the microphone employed in each particular zone. Separate amplifiers are provided for operating db volume indicator meters, which provide visual indication of output signals at the main operating position and at the alternative control position below the floor of the House. A periscope is provided at this position to enable the operator to view the chamber and select the appropriate microphone.

In addition to the microphones and loudspeakers already referred to there is a microphone above the Speaker's chair and another on the Table of the House. It should be pointed out that the reproducers on the tables in the Press Gallery and in other galleries are operated at a constant level.

The entire installation was undertaken by Tannoy Products (Sound Rentals, Ltd.).

WORLD OF WIRELESS

International Vision Standards ♦ Short-Wave Broadcasting ♦ R.T.E.B.
Exam. Results ♦ Training Opportunities ♦ Television Relay Service

European Television

DETAILS of the standards drawn up by the Television Study Group of the International Radio Consultative Committee (C.C.I.R.), following the investigation of systems at present in use in France, the U.S. and the U.K., have been published by the European Broadcasting Union, and we give below a summary of them:—

The width of the channel is to be 7 Mc/s (U.S. standard is 6 Mc/s and the British 5 Mc/s) with the vision carrier 5.5 Mc/s below the sound carrier—in this country, of course, it is 3.5 Mc/s below.

There are to be 625 lines per picture with interlaced scanning. The line and frame recurrence frequencies are 15,625 c/s and 50 c/s, respectively. The British line frequency is 10,125 c/s. The aspect ratio of the picture is that now used in this country—4:3, horizontal to vertical.

The lower sideband of the vision channel is to be partially suppressed, and, as in the U.S., negative modulation will be used. The pedestal level (normal black level) will be represented by a definite carrier level independent of light and shade in the picture, and this will be transmitted at 75 per cent—with a tolerance of $\pm 2\frac{1}{2}$ per cent—of the peak carrier amplitude. Peak white will be at least 10 per cent of the full carrier amplitude.

It is recommended that frequency modulation be used for the sound transmission. No reference is made in the recommendations to the polarization of the transmissions.

H.F. Broadcasting

WHEN the Hague Radio Conference, due to have opened in September, was called off (see page 318, September issue) the delegates to the International High-Frequency Broadcasting Conference, which had been in session, first at Florence and then Rapallo, since April 1st, decided by 39 votes to 13 (with 4 abstentions) to conclude their deliberations. This was on August 19th. The main reason for discontinuing all work on preparing a plan for h.f. broadcasting was that such a plan, based on the new bands allocated at Atlantic City (1947), could be implemented only if another Conference, such as that planned for the Hague, made available other frequencies to the

services at present occupying these bands.

The Conference was convened to draw up plans for the allocation of frequencies (between 5.95 and 26.1 Mc/s) to the world's short-wave broadcasting stations on the basis of time sharing and simultaneous channel sharing. These plans were based on the various phases of the sun-spot cycle.

Being unable to produce the plan envisaged, the Conference, at its final meeting, made a number of recommendations which are included in the September 15th issue of the European Broadcasting Union *Bulletin*. To encourage the use of the higher frequencies for broadcasting and thereby reduce the congestion in other sections of the h.f. band, it is recommended that the frequency coverage of receivers should be extended to include the upper limits of the band.

Servicing Examinations

THE result of the first Television Servicing Certificate examination held last May by the Radio Trades Examination Board, which was restricted to the London area, shows that of 30 entries 16 passed and 12 were referred in the practical examination. Of the 264 candidates who entered for the Radio Servicing Certificate examination, also held in May, 137 were successful and 45 were referred in the practical tests.

Application forms for the next examinations, to be held in May, 1951, may be obtained from the R.T.E.B., 9, Bedford Square, London, W.C.1. The closing date for entries for the Television Certificate is January 15th and that for the Radio Certificate is February 1st.

Frequency Control

THE need for a simple method of quoting frequency stability was stressed by C. F. Booth, the new chairman of the I.E.E. Radio Section, in his inaugural address on "The Evolution of Frequency Control." A proposed method, that he felt was worthy of consideration, is to express frequency stability in terms of the common logarithm of the reciprocal of the frequency variation when the latter is expressed as a fraction; for example, an oscillator subject to frequency variations of 1 in 10^6 would have a stability of 6 stability units, or, say, 6 S.U.

Technical Experience Abroad

OF the 1,672 University and College students who, through the International Association for the Exchange of Students for Technical Experience, gained experience in industry overseas during the summer vacation this year, 353 were from Great Britain, 204 from France, 197 from the Netherlands and 184 from Sweden. Twelve countries, including, for the first time, the U.S.A. and Germany, took part in the exchange scheme. Great Britain and Sweden headed the list of countries receiving students with an intake of 368 and 344 respectively.

The third Annual Report of the Association records that there was an increase of 436 on the exchanges made in 1949. About a dozen British radio firms received overseas students under the scheme.

Particulars of the Association, which, it is stressed, organizes these exchanges on a reciprocal basis, are obtainable from the General Secretary, J. Newby, Imperial College, South Kensington, London, S.W.7.

B.B.C. Changes

FOLLOWING the much-talked-of resignation of Norman Collins as Controller of B.B.C. Television, the politics of which we will not enter into, George Barnes, who has been B.B.C. Director of the Spoken Word since the creation of the post in 1948, has been appointed to the new post of Director of Television. Norman Collins has stated that he has left the Corporation because of the principle which was being adopted in the development of television—its merger "into the Colossus of sound broadcasting."

T. W. Chalmers, Controller of the Light Programme, has been seconded for three years to become head of the new Nigerian Broadcasting Service (see "In Brief") and has been succeeded by Kenneth Adam.

Electronics Scholarships

TO meet the growing need for technicians in the research and design sections of E.M.I. a scholarship scheme for a special four-year course in electronics has been provided by E.M.I. Institutes.

The scheme provides for a grant of £50 p.a. to each successful applicant towards the £400 course and a

maintenance grant of at least £50 p.a. Candidates, who must be between 16 and 18 years of age, and preferably of Higher School Certificate standard in science, must enter the company's service for four years after the satisfactory completion of the course.

Application forms and particulars of the course, which provides for three years at the Institute and one year's practical experience in the company's factories and workshops, are obtainable from the Principal, E.M.I. Institutes, 10, Pembroke Square, London, W.2. The first course commences on January 17th.

It is stated that, in normal circumstances, students will receive a deferment from National Service during the period of the course.

News in Morse

SINCE the publication of the schedule of the morse transmissions of the London Press Service in our May issue, a number of changes have been introduced, and we give below a revised list. In addition to the morse transmissions listed, the speed of which is between 20 and 27 w.p.m., a large number of bulletins are transmitted by Hellschreiber.

G.M.T.	Call	Freq. (Mc/s)	Areas
0030-0130§	MIK	9.725	1
	GPJ	10.885	2
0045-0230*	MIK	9.725	1
	GPJ	10.885	2
0130-0230§	MIK	9.725	1
	GPJ	10.885	2
0130-0300*	GDI	7.780	3
	GAH	8.065	4
0130-0300	GCV	8.920	5
0945-1045*	GCV	19.365	6, 8.
1100-1200†	GCV	19.365	6, 8.
1115-1215	GAG	17.105	7
1300-1300	GCF	19.005	5
1215-1315‡	GAG	17.105	7
1600-1700*	GCF	19.005	5
	GBI	10.865	6, 8.
1600-1800*	GIB	11.980	7
1700-1800	GBI	10.865	6
1815-1930	GBG	9.395	7
	GBI	10.865	6, 8.
1845-1945*	GIM	12.857	3
	GBO	13.665	4
1945-2215*	GDT	8.925	6, 8.
	GBG	9.395	7
2045-2200†	GBG	9.395	7
	GDT	8.925	6, 8.
2100-2200*	GBO	13.665	5
2251-0030*	GPX	11.646	1
	GPJ	10.885	2
2330-0030†	GIB	11.980	5

- * Weekdays only.
- † Sundays only.
- ‡ Mondays only.
- § Mondays and Saturdays only.
- || Alternate Fridays.

The number in the fourth column of the table denotes the area for which the transmissions are destined: 1, N. America; 2, S. America; 3, Distant Europe; 4, Middle East; 5, Africa; 6, N.E. Asia; 7, S.E. Asia; 8, Australasia.

There is no restriction on the reception of these transmissions, which are radiated by Post Office stations, and the use of their contents outside the United Kingdom.

National Exhibition

THE Radio Industry Council has announced the date of next year's National Radio Show—August 28th to September 8th. As already stated, the show—the 18th in the series—will be at Earls Court, London, and not Olympia, so that the well-established title Radiolympia will not be applicable.

Greenwich Time Signal

A MEAN time signal is now being transmitted twice daily from the Royal Greenwich Observatory, Abinger Common, Surrey, in addition to the present rhythmic signal. The schedule is:—

G.M.T.		
	h m s	
to 00 54 00		Preamble: "GBR GBR TIME" (4 times) followed by tuning dash.
00 55 00		
to 10 00 00		Mean time signal: Seconds dots, lengthened to dashes at the minutes.
10 01 00		
to 10 06 00		Rhythmic signal: Dots spaced 61 to the minute, lengthened to dashes at the minutes.
10 06 05		
to 10 06 15		Tuning dash.

This sequence is repeated from 1754.

The morning transmission is radiated by GBR, 16 kc/s; GIC, 8,640 kc/s and GIA, 19,640 kc/s, and the evening transmission by GBR, 16 kc/s; GIC, 8,640 kc/s and GKU3, 12,455 kc/s.

The duration of each dot is approx. 0.1 sec, and that of the dashes at the minutes is approx. 0.6 sec. The beginning of each dot or dash is the timing reference point.

Hotel Television

A TELEVISION relay service has been installed in each of the 940 bedrooms in the Cumberland Hotel, London, W.1. The hotel was already equipped with an a.f. distribution system giving a choice of four programmes, and the same wiring is used for television.

A four-element aerial is employed on the roof of the building to minimize the pick-up of interference and its output is fed to seven amplifiers, of which one is a spare. With a maximum gain of 55 db they provide an output of 2 V r.m.s. in 75-ohm feeders.

The audio wiring of the hotel is carried out in 63 vertical ducts each feeding about 16 rooms. The r.f. television signal is fed by 75-ohm balanced cable to the tops of these ducts, each amplifier feeding 9-12 ducts. They are there connected by resistance hold-off pads to the audio wires which are used in a quad phantom circuit. A $\lambda/4$ stub is connected a quarter-wavelength beyond the junction to prevent r.f.s. passing back to the a.f. source.

Resistive stopper pads are in-

cluded at the loudspeaker for the audio channel to divert the television r.f. signal to the outlet socket. Standard television receivers are used and the hotel charges 3s a night for the service.

The equipment was installed by British Relay Wireless.

Television Components

IN preparation for the expected demand for television receivers when the projected stations open in Montreal and Toronto, the Canadian Government has authorized the release of U.S. dollars to fifteen Canadian set manufacturers for the purpose of buying components in the U.S.A. Attention having subsequently been drawn to the availability of television components in the U.K., the Canadian Department of Trade and Commerce has agreed, in principle, that where practicable the components should be secured in this country. British manufacturers who are represented in the Dominion, and wish to bring their components to the notice of the Canadian set manufacturers, should send catalogues and price lists in duplicate to E. J. McWilliams, Assistant Director, Emergency Import Control Branch, Department of Trade and Commerce, Ottawa. Firms without agents in Canada may like to use the services of the Board of Trade to secure representation, in which case communications should be sent to the Commercial Relations and Export Department, Thames House North, Millbank, London, S.W.1, quoting reference C.R.E. 5902/50.

IN BRIEF

Consol.—The second edition of the Ministry of Civil Aviation publication "Consol—A Radio Aid to Navigation" (M.C.A.P. 59), which has been published by H.M. Stationery Office, price 1s 6d, contains complete details of the service and coverage of the existing Consol stations at Bushmills, Stavanger, Lugo and Seville and also of the service to be provided by the new station at Plonéis, near Quimper, Finistère (France), which will be brought into use in the near future.

Amateurs and Distress Calls.—In contrast with the facilities provided by American amateurs for a network of stations in cases of emergency, such as forest fires, floods, etc., which were tested during a recent nation-wide exercise, the Ministry of Transport has declined the offer made by the Radio Society of Great Britain for British amateurs to place themselves at the disposal of the appropriate authority for receiving distress messages from vessels at sea.

M.F. Air Navigation.—It is pointed out by the Ministry of Civil Aviation that, while every effort is made to assign to m.f. navigational facilities frequencies from the aeronautical bands (255 to 285 kc/s and 315 to 405 kc/s), it is not always possible to do so be-

cause of the congestion within those bands. Use is, therefore, made of broadcasting stations as non-directional beacons and of other non-directional beacons operating on frequencies outside the aeronautical bands but within the limits of 200 to 1,750 kc/s.

Netherlands F.M.—According to information issued by the European Broadcasting Union, the Netherlands Government is planning the erection of a network of 12 f.m. stations operating on frequencies between 92.5 and 94.7 Mc/s.

Suppressing the ignition system of motor vehicles is dealt with in one of the chapters of the fourth edition of "Automobile Electrical Equipment," by A. P. Young and L. Griffiths, which is issued by our Publishers for our associate journal *Automobile Engineer*. This 386-page book, which deals exhaustively with electric lighting, starting and ignition as applied to the internal combustion engine, costs 25s.

Multitone.—The results of investigations, using the "Optimeter," in the volume requirements of five hundred hearing-aid users are given in the article "How Loud Should I Listen?" included in the first issue of *Hearing Aid News* which will be issued at irregular intervals by the Multitone Electric Co.

Hearing Aids.—The National Institute for the Deaf has issued a booklet, No. 481, giving approved lists of manufacturers and suppliers of hearing aids in the United Kingdom. Makers of mechanical as well as electronic aids are listed and those supplying group hearing aids are indicated.

Christmas lectures "adapted to a juvenile auditory," which will again be given at the Royal Institution this year, will be on "Waves and Vibrations," by Prof. E. N. da C. Andrade, D.Sc., F.R.S. This 121st course of six lectures, the fee for which is 10s 6d for children between 10 and 17 years of age, will be given on December 28th and 30th and January 2nd, 4th, 6th and 9th at 3.

"**The Use of Radar at Sea**" is the provisional title given to a textbook on the operational use of marine radar, which is in course of preparation by the Institute of Navigation. The book will contain contributions by twelve authors and will deal with every aspect of the subject. This is announced in the annual report of the Institute for the year ended June 30th, 1950, in which it is reported that the membership is now over 1,100.

"**Decca News**" is the title given to the recently introduced journal of the Decca Navigator Company, which at present is issued bi-monthly. Descriptive articles on both radar and Decca Navigator installations are included.

Post-graduate Training.—Twenty-eight university graduates and technical college students recently commenced a special training course at the New Southgate Works of Standard Telephones and Cables. The course, which lasts a year and is the fourth since the commencement of the company's present post-graduate training scheme, is designed to provide opportunities for candidates to relate their theoretical and practical training to the whole field of activities within the Standard organization.

Convention Cancelled.—The Radio Section of the I.E.E. had proposed to hold a convention covering "Current Researches in Electron Valves" during the Festival of Britain, but having been advised that to hold such a convention in prevailing circumstances might not be in the National interest, it has been decided not to proceed with the arrangements.

Interference Suppression.—The television-conscious motorist who fits Lucas suppressors to his car ignition system will be easily identified by a transparency bearing the words "This car has been suppressed," which is being fixed to windscreens. At both the recent Motor Shows in London the firm demonstrated the effects on television reception of suppressed and un-suppressed car ignition systems which, according to the Radio Industry Council, are responsible for 85 per cent of the interference caused. Lucas have recently produced a prototype of a distributor incorporating a carbon brush of resistive material which acts as a suppressor.

Nigeria, which at present relies on a wired-wireless distribution system for radio programmes, is to be served by six broadcasting stations to be erected at a cost of about £350,000, which is being shared by the Nigerian Government and the U.K.

Instrument Show.—Scientific and industrial instruments are to have an exhibition of their own in London next year. Among the supporting organizations of the exhibition, which will be held at Olympia from July 4th-14th, is the Scientific Instrument Manufacturers' Association.

Television in Industry.—The use of television to permit the remote observation of dangerous industrial processes was recently demonstrated when the English Electric Co. employed it to show the operation of high-power switch gear. Standard 405-line Marconi apparatus was used.

Blind Technicians.—The Report of the National Institute for the Blind records that an experimental training scheme has been arranged with Electric and Musical Industries to ascertain to what extent the blind can be instructed to undertake receiver repairs. This has necessitated the provision of circuit diagrams in relief and Braille-calibrated test equipment.

"**Broadcast News**," which is published by the Radio Corporation of America and is devoted almost entirely to descriptions of transmitting equipment for sound and vision, is now available to subscribers in this country from RCA Photophone, 36, Woodstock Grove, London, W.12. It is published at two-monthly intervals and the subscription rate is £2 for twelve issues.

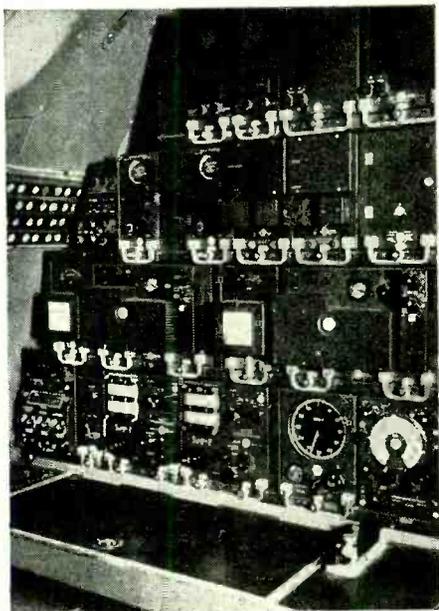
Vox Populi.—The International Short-Wave Club has announced the result of a census taken among its members in all parts of the world to ascertain the most popular short-wave broadcasting station. Leopoldville (OTC) comes first with 609 votes, Radio Australia second with 446 and Switzerland third with 435, followed by Canada (419), B.B.C. Overseas Service (401), Hilversum (388), The Voice of America (380) and many other stations with fewer votes.

Sound Letters—magnetically recorded messages on metallized paper tape—have been introduced by the Welfare Council of the Norwegian whaling fleet for use by the men working on the factory ship and their relatives. They are regularly flown to and from the Antarctic whaling grounds.

B.I.F.—Next year's British Industries Fair will be held from 30th April to 11th May, at Olympia and Earls Court, London, and Castle Bromwich, Birmingham.

Institute of Physics announces an increase in its membership of some 200 during 1949.

Airborne Television.—A Marconi image-orthicon camera and 30-watt "suitcase" transmitter were used by the B.B.C. for the first television broadcast from the air which was radiated from the London and Sutton Coldfield stations on October 1st.



COMET RADIO.—The Marconi radio installation in the de Havilland "Comet" jet air liner. The equipment shown includes intercom. units, direction finders (duplicate control units for which are in the cockpit) and high-power transmitters.

BUSINESS NOTES

Rural Radio.—The Persian Government is considering the purchase of 50,000 radio receivers for use in rural areas. They should be battery-operated, six-valve sets, fitted with "magic eye" tuning and covering the 60 to 120-metre and 180 to 360-metre bands. Interested firms should communicate with Esfandiar Bouzourg-

mehr, Director, Government Propaganda Department, Tehran, forwarding details, and prices of their products. It is stated by the Board of Trade that it will be appreciated if copies of correspondence are sent to the Counsellor (Commercial) British Embassy, Tehran.

R.T.S.—We understand that it is only the stock and plant of the *transformer* business formerly operated by R.T.S. Electronics which has been acquired by EARL Services and to which reference was made in our last issue. R.T.S. are continuing the manufacture of the "Motoradio" car set and the "Mimicomm" intercommunication equipment.

I.A.L.—Consequent on the withdrawal of the R.A.F. from Hargeisa Airfield, British Somaliland, International Aeradio, Ltd., will provide an Airport Controller for service in the Protectorate.

A contract for the supply of Decca navigational radar gear to be installed in ships of the Royal Navy has been received by Decca. The company states that orders to equip nearly five hundred naval and merchant ships have been received during the past twelve months.

British Radar for Japan.—The first Japanese ship to be fitted with British marine radar equipment is a whale-oil refinery vessel which was equipped by Cossor Radar prior to leaving for the Antarctic.

Marconi Marine Radio gear, including two transmitters, two receivers, direction finder and echometer, is being installed in the new 28,000-ton turbine tanker *Verena* under construction for the Anglo-Saxon Petroleum Company. The radio-communication and navigation equipment installed in the new Argentine liner *17 de Octubre* has also been supplied by Marconi's.

Trawler Radar.—Ten trawlers now under construction in this country for the Icelandic Government are to be equipped with Decca radar gear, Type 159A.

Pakistan.—Seven more ships of the Pakistan merchant fleet are being fitted with radio equipment by the Marconi International Marine Communication Co., Ltd.

Plessey announce the resignation of Wing Commander G. C. Cunningham, O.B.E., who was the company's communications sales manager.

Aerialite, Ltd. of Stalybridge, Cheshire, announce that O. E. Trivett, M.Brit.I.R.E., A.M.I.E.E., has been appointed personal assistant to the Managing Director. Before taking up this appointment he was concerned with the setting up of a plastics extrusion and radio factory in India in conjunction with General Electric of America.

Ersin Multicore Solder is being exported to an increasing number of countries; among the latest are Brazil, Argentina, South Africa, Syria and Mexico. In addition agents have recently been appointed in Iceland and Iran.

Oldham & Son, the battery manufacturers, are to establish a factory in Madras, India, which is to be managed by Oldham & Son, India, Ltd.

Denco announce that, following the recent resignation of D. W. Heightman from the Board, A. W. Allwright has rejoined the company as Managing Director.

I.M.R.C.—The Brazilian Navy training ship *Almirante Saldanha*, recently refitted at Barrow, has been equipped with m.f. and h.f. transmitters by the International Marine Radio Company. The vessel was equipped by I.M.R.C. when built in 1934.

Sobell Model 610, six-valve superhet has been tested by the School Broadcasting Council for the United Kingdom and approved for use in schools.

E.E.G. Exports.—Edison Swan have recently received orders from Spain, Poland, Egypt and Ceylon for their Mark II electro-encephalograph.

E. K. Cole announce that Bentley Jones has resigned from the position of sales manager of the company's radio division. He has joined Thorn Electrical Industries as commercial director of the Ferguson television and radio division.

Dubilier Condenser Co. announce that F. H. McCrea, Managing Director, is undertaking an extensive business tour of Canada and the United States.

The Electrical Apparatus Co., of St. Albans, announce that J. de Gruchy has been appointed Head of the Instrument Department which at present is concentrating on the production of moving-iron and moving-coil meters.

NEW ADDRESSES

British Standards Institution has opened an office at 12, Hilton Street, Manchester, 1 (Tel. Central 4856), where a complete set of British Standards may be consulted and copies purchased.

Marconi's have recently established an Inspectorate at Mombasa providing radio and radar maintenance for vessels calling at ports in the area.

Depots are being opened by Aerialite, Ltd., at 343, Deansgate, Manchester, 3 (Tel. BLA. 3524); and 50, Cathay, Redcliffe, Bristol (Tel. 26130).

Southern Radio Supply, Ltd., have moved from 46, Lisle Street, London, W.C.1, to 11, Little Newport Street, London, W.C.2 (Tel. Gerrard 6653).

MEETINGS

Institution of Electrical Engineers

Radio Section.—"Crystal Diodes," by R. W. Douglas, B.Sc., and E. G. James, Ph.D., and "Crystal Triodes," by T. R. Scott, B.Sc., at 5.30 on December 6th.

Discussion on "Have Post-War Broadcast Receivers taken Full Advantage of Wartime Development?" opened by R. B. Armstrong, B.Sc., at 5.30 on December 18th.

The above meetings will be held at 5.30 at the I.E.E., Savoy Place, London, W.C.2.

Cambridge Radio Group.—"A Review of some Television Pickup Tubes," by J. D. McGee, M.Sc., Ph.D., and "The Design of a Television Camera Channel for Use with the C.P.S. Emitron," by E. L. C. White, M.A., Ph.D., and M. G. Harker, B.Sc. (Eng.), at 6 on December 5th at the Cambridgeshire Technical College.

North-Eastern Radio Group.—"Electronic Counters and Some Applications," by R. B. Conn B.Sc., at 6.15 on December 18th at King's College, Newcastle-on-Tyne.

Sheffield Sub-Centre.—"Some Electromagnetic Problems," by Prof. G. W. O. Howe, D.Sc., LL.D., at 6.30 on December 13th at the Grand Hotel, Sheffield.

North Lancashire Sub-Centre.—"The General Aspects of Television," by A. J. Biggs, Ph.D., B.Sc., at 7 on December 20th at the Harris Institute, Corporation Street, Preston.

South Midland Centre.—"Generation and Flow of Harmonics in Transmission Systems," by S. Whitehead, M.A., Ph.D., and W. G. Radley, C.B.E., Ph.D.(Eng.), at 6 on December 4th at the James Watt Memorial Institute, Great Charles Street, Birmingham.

Reading (Berks) District.—"Television Engineering," by D. C. Birkinshaw, M.B.E., M.A., at 7 on December 11th at the Great Western Hotel, Reading.

British Institution of Radio Engineers

London Section.—Discussion on "Progress in Loudspeaker Design," opened by R. L. West, B.Sc., at 6.30 on December 15th at the London School of Hygiene and Tropical Medicine, Keppel Street, Gower Street, W.C.1.

North-Eastern Section.—"A Survey of Television Development and its Problems," by H. J. Barton Chapple, B.Sc., at 6 on December 13th at Neville Hall, Westgate Road, Newcastle-on-Tyne.

Scottish Section.—"Vacuum Engineering Applied to Electronics," by D. Latham, B.Sc., at 6.45 on December 7th at Heriot-Watt College, Edinburgh.

North Western Section.—"High Fidelity Reproduction," by H. J. Leak, at 6.45 on December 7th at the College of Technology, Manchester.

British Sound Recording Association

"The Application of Magnetic Coatings to Film Stock," by G. F. Dutton, Ph.D., D.I.C., at 7 on December 6th at E.M.I. Studios, Ltd., 3, Abbey Road, St. John's Wood, London, N.W.8 (Joint Meeting with the British Kinematograph Society).

"Modern Recording Technique," by C. E. Watts at 7 on December 13th at the Central Library, Guildhall, Portsmouth. Demonstrations from 5 p.m. (Joint Meeting with the Institution of Electronics).

"The Crystal Pickup With Particular Reference to Long-Playing Records," by S. Kelly at 7 on December 20th at the Royal Society of Arts, John Adam Street, London, W.C.2.

Television Society

Engineering Group.—"Television Transmission for the Amateur" by M. Barlow (Hon. Sec. British Amateur Television Society), at 7.0 on December 14th, at the Cinema Exhibitors' Association, 164, Shaftesbury Avenue, W.C.2.

Institution of Electronics

Midlands Branch.—"Electronic Instruments for Temperature Measurements and Control, and for Safeguarding Combustion," by H. A. Stevenson and C. Smith at 7 on December 5th at the Warwick Room, Imperial Hotel, Temple Street, Birmingham, 2.

Tolerances and Errors

"CATHODE RAY" Explains How They Add Up in the Final Result

SOMEONE has written to me to ask: what about tolerances? And to make his point clear he proceeded to fire a number of diverse examples in rapid succession. Some of these concerned combinations of resistors, and he ended by asking "Is there a 'tolerance arithmetic' for simple series/parallel networks?" To tell the truth, I hadn't given the matter much thought, but after having done so I can answer with a definite "yes."

The subject of errors, even if confined to the field of measurement, is a very large one, and to the mathematically-minded a very attractive one. Large and excessively learned books have been written on it. But they concentrate on the question of *probable* error, which must be clearly distinguished from *maximum* error or, as it is called in engineering, tolerance. The tolerance is so important in connection with radio components that the colour code applicable to them has one unit devoted to indicating it.

So when one buys even such a simple thing as a resistor one must be prepared to answer the question "Yes, sir; what tolerance?"—or look a fool. It is not merely an academic question; it has more to do with the price, apparently, than anything else. The reason lies in the fact that the manufacture of resistors (of the ordinary composition type) is rather like shooting at a target from a considerable distance. The resistances no more come out all exactly the right value than all the bullets go through a single hole exactly in the centre. In the absence of any special trends, the distribution of bullets relative to the centre of the target, and of resistances relative to the nominal value, is found to follow what is referred to in the learned books as a normal (or Gaussian) error curve, Fig. 1. Over a narrow range on each side of the nominal value the quantities are distributed almost evenly. Those falling within 5% of the nominal value are picked out and marked " $\pm 5\%$." From the remainder, those falling within 10% are picked out and marked " $\pm 10\%$." Similarly for the $\pm 20\%$. Those not within 20% of one nominal value come within 20% of another nominal value and can be marked accordingly. So, on this plan, buyers of $\pm 10\%$ resistors are unlikely to find them within 5%, and the usual assumptions made by the "probable-error" school of thought fall down.

If all were offered at the same price, the makers would have no sale for the 10% and 20% stocks, so the prices are graduated to equalize the demand.

Generally one does not buy a resistor as a self-contained unit, to be preserved for ever in complete isolation. It is intended to be used in conjunction with other components, to achieve some desired result. Even if it is wanted as a single fixed standard of resistance, the ultimately important matter is not the maximum error in that resistance but the error in the results of measurements based on it. So one ought to have a clear idea of how tolerances in components affect the maximum possible error in the final result. It is because I suspected that one does

not have this clear idea that the subject struck me as being just the thing for considering here.

The sort of question one ought to be able to answer can be indicated by an example: We want to pass a current of $50 \text{ mA} \pm 7\frac{1}{2}\%$ from a 200-V supply and we have a $6.8 \text{ k}\Omega$ resistor with a tolerance of 5%. This resistance is too high, because what is wanted is $4 \text{ k}\Omega$; but a $10 \text{ k}\Omega$ in parallel would do the trick (within about 1%); what tolerance can this $10 \text{ k}\Omega$ be allowed?

Series Combinations

Let us, then, tackle resistance networks, or at any rate those whose overall resistance can be calculated by the two simple principles of series and parallel addition. Before starting there are one or two things we ought to be quite clear about.

When a resistor is marked " $200 \Omega \pm 10\%$ " (read as "200 ohms plus-or-minus 10 per cent") it means that if its actual resistance is anything between 180Ω and 220Ω you have to be satisfied; but if it is outside those limits you can claim your money back. Dimensions in engineering drawings are sometimes marked with unequal positive and negative tolerances; but we shall exclude them, or (if you insist) alter the main dimension so as to divide the tolerance equally. We make this assumption so that we can simplify our calculations by using + signs for all tolerances, except where a positive overall error is contributed to by a negative tolerance, as for example in the effect of shunt resistance on meter current.

If we had been interested in *probable* errors we would have had to take account of the fact that when two quantities are combined, each having random variations from the nominal value, there is a lucky chance that the errors will tend to cancel one another out, as well as the unlucky chance that they may add up. So the most probable error is less than the sum of the two. But here we are taking a sternly engineering attitude, leaving nothing to chance, and (whatever we may secretly hope) being prepared for the worst. So we shall assume in every case that the tolerances combine in the worst possible way.

If in an unguarded moment one were to be asked

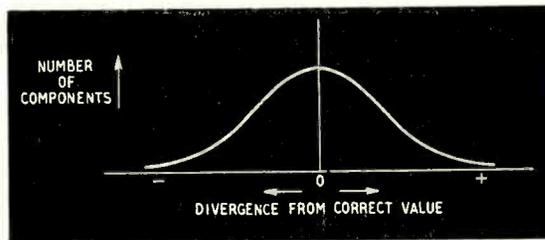


Fig. 1. If the components in a very large batch are arranged according to their departure from the nominal value, their quantities tend (theoretically) to follow a curve something like this.

about the overall tolerance when two equal $\pm 5\%$ resistances are connected in series one might (without thinking) answer " $\pm 10\%$ " But this would be confusing percentages (or proportional errors) with absolute errors. If the two resistors were each $1,000\Omega$, each would have a tolerance of 50Ω , so the tolerance in the combination would be 100Ω , it is true. But relative to the resistance of the combination, $2,000\Omega$, this would still be 5% . One can go further and say that in any combination of resistances having equal percentage tolerances the overall percentage tolerance is the same as that of the components. The proof, if one is wanted, will emerge as a special case of the less obvious problem of any-value tolerances.

This problem can be solved by at least three methods: by common sense, by simple algebra, and by differential calculus. I am leaving out of account a fourth method—by arithmetic—because that solves only one example at a time, and I assume that anybody reading this article is more interested in getting to the root of the matter.

The common-sense method is to argue that in a combination of any number of resistors in series the tolerances in ohms add up together, just like the nominal resistances, but when they are expressed as percentages of the whole combination they affect it only in proportion to the individual resistances. For example, if a 20% resistor comprises one quarter of the resistance of the combination, its contribution to the overall tolerance will be one quarter of 20% . Similarly for the other resistors.

Simple algebra reaches the same result by denoting the resistances by symbols and subjecting them to the ordinary arithmetical operations. Suppose there are two resistances, nominally R_1 and R_2 (Fig. 2), and their respective tolerances, expressed in the same units as R_1 and R_2 , are r_1 and r_2 . The corresponding percentage tolerances, p_1 and p_2 , are therefore $100 r_1/R_1$ and $100 r_2/R_2$. The nominal value of the combination, which we shall denote by R , is of course, $R_1 + R_2$; and according to the rules we have just laid down the tolerance of the combination (call it r) is $r_1 + r_2$. What we want to find is p , the percentage tolerance of the combination. It is, of course

$$p = \frac{100r}{R} \\ = \frac{100(r_1 + r_2)}{R_1 + R_2}$$

Since $p_1 = 100r_1/R_1$, r_1 must be $p_1 R_1/100$. So

$$p = \frac{100\left(\frac{p_1 R_1}{100} + \frac{p_2 R_2}{100}\right)}{R_1 + R_2} \\ = \frac{p_1 R_1 + p_2 R_2}{R_1 + R_2}$$

If we had had three resistances, it would have been

$$p = \frac{p_1 R_1 + p_2 R_2 + p_3 R_3}{R_1 + R_2 + R_3}$$

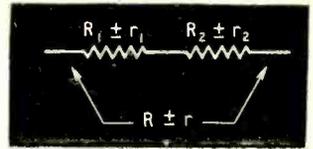
and so on.

This just puts in symbols what we have already said in words. Perhaps this would be made clearer if we rewrite the formula thus:

$$p = \frac{p_1 R_1}{R} + \frac{p_2 R_2}{R}$$

etc. Example: A $200\text{-}\Omega \pm 10\%$ resistor is connected in series with a $500\text{-}\Omega \pm 5\%$ resistor; what is the overall percentage tolerance and the contribution

Fig. 2. Two resistances in series, the nominal values being indicated by capital letters and the tolerances by small.



of each resistor? The first contributes $10 \times 200/700 = 2.86\%$, and the second $5 \times 500/700 = 3.57\%$; total 6.43% .

As a matter of fact it is rather silly to give this answer to two decimal places, because the resistor sorters certainly do not work to that degree of precision. Another reason is that in general the accepted methods of calculating tolerances are only approximate. As it happens, however, this simple case of adding two quantities is an exception, thanks to the custom of reckoning tolerances relative to the nominal values. You can check this by taking an extreme case: suppose the tolerance of the $200\text{-}\Omega$ had been 1% and that of the $500\text{-}\Omega$ had been 60% . Then with positive errors the components would have been 202Ω and 800Ω respectively, so R_2 would have been nearly four times R_1 . With negative errors they would have been 198Ω and 200Ω , making R_2 and R_1 almost equal. So it would seem as if the proportions in which each error contributed to the overall result would be greatly influenced by the errors themselves. And so they would, if they were reckoned on the actual values, or if the errors interacted on one another (as would be indicated if there were terms containing both p_1 and p_2). Check it with the example if you like; the maximum error (positive or negative) is 302Ω , which relative to the nominal value of the combination (700Ω) is 43.15% . The calculated contributions are $1 \times 200/700 = 0.29\%$ and $60 \times 500/700 = 42.86\%$, which add up to 43.15% .

But what about the differential calculus method? In this case it offers no advantage whatever; in fact, it only tells us what we have already accepted as obvious, namely that $r = r_1 + r_2$. But it is quite otherwise with more complicated cases, which by simple algebra are usually unbearably tedious.

And Now in Parallel

Even such an apparently simple situation as two resistances in parallel is bad enough. The nominal value R , according to the well-known formula, is $\frac{R_1 R_2}{R_1 + R_2}$. We can see that a positive error in either leads to a positive error in the combination, so $+$ signs throughout are in order, and the maximum value of the combination is

$$R + r = \frac{(R_1 + r_1)(R_2 + r_2)}{(R_1 + r_1) + (R_2 + r_2)}$$

and r is obtained by subtracting R from this. As before, $p = 100r/R$. Now you can go ahead and work it out, on the same principle as for resistances in series. But make sure you have plenty of paper! The result, in spite of a considerable amount of boiling down and tidying up, is the rather unpleasant

$$p = \frac{p_1 R_2 \left(1 + \frac{p_2}{100}\right) + p_2 R_1 \left(1 + \frac{p_1}{100}\right)}{R_1 \left(1 + \frac{p_1}{100}\right) + R_2 \left(1 + \frac{p_2}{100}\right)}$$

But provided that the tolerance percentages are

reasonably small, one can get a sufficiently good approximation by neglecting them where they are divided by 100; thus:

$$p \approx \frac{p_1 R_2 + p_2 R_1}{R_1 + R_2}$$

This is rather interesting, because it is the same as for resistances in series, except that each tolerance contributes in proportion to the *other* resistance. Which fits in with common sense, because if 100Ω is shunted by 10,000Ω the 100-Ω resistance is thereby affected only very slightly (being reduced to about 99Ω) and the effect of small tolerances in the 10,000Ω is quite negligible. On the other hand, the tolerance in the 100Ω is practically the same as that of the combination. In the parallel connection, then, the two tolerances are not independent of one another; the effect of varying one resistance depends on the value of the other.

Having neglected $p_2/100$ in comparison with 1, we should not expect to find this formula very accurate if applied to our 500-Ω ±60% resistor. In parallel with the 200-Ω ±1% resistor, the result is (by exact calculation) 142.8Ω +12.9% or -30.2%. (Note how much smaller the positive tolerance is than when they are in series, because the greater part of the current flows through the 1% resistor. This is much less so with the negative tolerance.) According to the approximate formula, p is ±17.86%.

I have made rather a lot of this difference between the two cases because it forms an interesting analogy with intermodulation in amplifiers. If an amplifier is perfectly linear, then the effect of amplifying two signals at once is equal to the sum of the effects of separate amplification. But if, as is always more or less so, there is non-linearity, the signals intermodulate. And while this may be negligible when the amplitudes (relative to the steady valve current) are small, it will probably not be when they are large. The tolerances or errors correspond to the signal amplitudes.

The differential calculus method is a considerable help with the parallel circuit. Normally, for the benefit of readers who look on it as something much too intellectual, I keep the calculus out of these pages; but this time, for the benefit of those who have learnt the elements of it and are looking around for something not too hard to practise on, I will just stop to point out the way. It is based on the assumption that over the range of variation represented by the tolerance the "curve" is linear. In other words, exactly the same assumption as we make in most valve calculations. Using the same symbols as before, one can write it

$$r = r_1 \frac{\partial R}{\partial R_1} + r_2 \frac{\partial R}{\partial R_2} + \dots$$

which means that to find the contribution of r_1 to the overall error one multiplies it by the rate at which R changes when R_1 is varied; and similarly for any number of resistors *connected in any way whatsoever*. One only needs to know how R is related to the component resistances and how to differentiate with respect to each of these.

With two resistances in parallel the result of the differentiation is

$$r = r_1 \left(\frac{R_2}{R_1 + R_2} \right)^2 + r_2 \left(\frac{R_1}{R_1 + R_2} \right)^2$$

and when the substitution has been made for p , etc., the result is the same approximate formula as before.

The more complicated the problem, the greater the saving by using the calculus.

By one method or another we now have formulae for dealing with both series and parallel arrangements, and with these can solve any resistance network that can be reduced to such arrangements. And remembering that capacitances in series are calculated as for resistances in parallel, and vice versa, we can deal with them, too; which is rather useful when designing oscillator circuits for superhets.

In practice, one may have to take into account temperature tolerances as well as manufacturing tolerances; but the methods are the same.

Meter Tolerances

When one comes to meters there is more need to consider the causes of the errors. Meter tolerances are generally stated as a percentage of full-scale reading; in other words, as a constant amount regardless of reading. For instance, if a 0-500 volt-meter is said to have an accuracy of ±1%, it means that the readings are (or should be) reliable within 5 V. If one tries to read 10 V on such a meter, p is ±50%, which is not very good. Moral: use a lower range. The only sort of error I can think of that would strictly follow this law is a faulty adjustment of the zero-setting device, and that doesn't count! Most of the inherent errors of the instrument—temperature, lack of balance, non-linearity of field and spring, etc.—have some sort of proportionality to the deflection; but it is not necessarily simple proportion, so to be on the safe side the maker quotes a full-scale error everywhere.

When using multipliers and shunts the plot thickens. Presumably any errors arising from uncertainty in the resistance of the meter are not included in the quoted inaccuracy and have to be added. So the question "A meter ±1% f.s.r. is used with a shunt ±2%; what is the accuracy of the reading?" is less simple than it looks. Assuming that the ±1% refers to the meter used unshunted, we would have to know the maximum error in the specified or measured value of the meter resistance.

Fig. 3. Symbols used in working out the shunting error due to tolerances in the shunt and meter resistances.

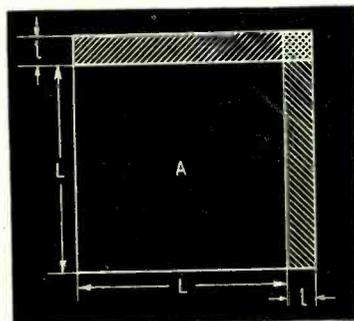
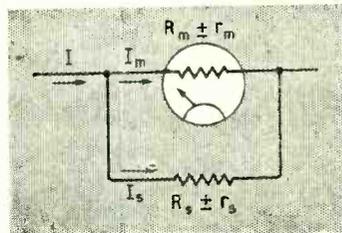


Fig. 4. Showing how a tolerance in a dimension is approximately doubled when the quantity is squared.

This would enable us to calculate the corresponding figure for the meter current in relation to the total current to be measured. We assume that this total current is unaffected by inserting the meter; otherwise that error would have to be calculated, too. The 1% meter error is additional to the shunting error.

The symbols in Fig. 3 are, I hope, self-explanatory. A shunting-error formula can be obtained in much the same way as the parallel-resistance formula, but the starting point is different:

$$I_m = I \frac{R_s}{R_s + R_m}$$

The result, either by straightforward algebra, neglecting terms divided by 100, or by short-cut calculus, is

$$p \approx (p_s - p_m) \frac{R_m}{R_m + R_s}$$

This shows that if both meter and shunt resistance are high or low by the same percentage, the shunting error is nil (which is what one would expect).

An important thing to know is that if the value of a component has to be squared to give the answer, the overall tolerance is doubled. Similarly, cubing multiplies the tolerance by 3; a square root by $\frac{1}{2}$; and so on. This is another of the rules that is a good approximation for small tolerances only. It is very obvious to anybody who has absorbed the first stages of the differential calculus; and can be demonstrated to others by the simple diagram Fig. 4. The area A of a square is of course equal to L^2 . If L is increased by a small amount, l , A increases in the same proportion in two places, plus a little corner piece. If the

corner is neglected, the area therefore varies twice as fast as L.

The same sort of game can be played with a cube, but beyond that it is difficult.

If there is still space I would like to refer to a formula quoted on page 358 of Scroggie's "Radio Laboratory Handbook" (5th edn.) as an example of a type that should be avoided for its insidious error-multiplying nature. It refers to the method of measuring the total initial capacitance of a tuned circuit by noting the frequencies f_1 and f_2 , to which it resonates when two known capacitances, C_1 and C_2 , are added. The formula is

$$C_0 = \frac{C_1 f_1^2 - C_2 f_2^2}{f_2^2 - f_1^2}$$

Unless you have some time on your hands I don't advise working out the maximum error formula for this; but having done so I would like to give a typical example, assuming these values:

$C_1 = 200\text{pF} \pm 0.5\%$; $C_2 = 400\text{pF} \pm 0.5\%$;
 $f_1 = 1,000 \text{ kc/s} \pm 0.1\%$; $f_2 = 733 \text{ kc/s} \pm 0.1\%$.
 Anybody using these figures might imagine that the data were pretty accurate; nevertheless, he would not be justified in relying on the answer to better than 20%. Yes; decidedly a method to be avoided.

Answer to Introductory Example

Apart from the 1% by which the nominal value of the parallel combination fails to fit the exact requirement, the tolerance in the 10-k Ω resistor could be (calculated by substitution in the given formula) 11.2%. So a $\pm 10\%$ resistor would do.

APPLIED ELECTRONICS

Brit.I.R.E. Presidential Address

"SELLING" electronics to industry, the dissemination of technical information, aeronautical radio and the possibilities of employing vertically radiated transmissions in an endeavour to accommodate more stations within the limits of the h.f. broadcasting bands are some of the matters dealt with by Paul Adorian in his recent Presidential address to the British Institution of Radio Engineers.

He suggested that in order to stimulate interest in, and secure the acceptance of, electronic methods in industry and medicine, papers should be presented, not only to radio engineers but to those engaged in fields of research to which the techniques are applicable.

In regard to the problems associated with broadcasting, Mr. Adorian summarized the difficulties, so far as medium- and long-wave stations are concerned, by saying that, allowing for a 9-kc/s separation between channels, it would be necessary to use each available channel twenty-five times to cover the world's land mass with one programme.

On the question of h.f. broadcasting, he outlined a system employing aerials which radiate a large proportion of their power vertically, giving relatively short-range reflections from the Heaviside layer. The system, using the wavelength of 30 metres, has been used in Trinidad since 1947 and has given satisfactory reception throughout the island in daylight, but at

night interference is caused by stations operating in different parts of the world on the same wavelength but with aerials radiating considerable power at low angles. Another station using the system has recently been opened in Jamaica.

RCA Receiving Tube Manual

A NEW and completely revised edition of this useful reference book has recently been announced by the RCA Tube Department. It contains general information on valves, ranging from elementary theory to descriptions of the latest applications of receiving valves, and has some new features reflecting developments in electronics. The section on valve and circuit theory has been expanded and includes formulæ and examples for the calculation of power output, load resistance and distortion for several classes of amplification, as well as information on the design of cathode followers. New designs for receivers and amplifiers have also been added, and there is a complete section on resistance-coupled amplifiers.

In addition, the manual provides technical data on more than 460 RCA receiving valves and television picture tubes, including many discontinued types. For quick and easy reference there is a classification chart which groups together the types having similar characteristics and the same filament or heater voltages.

Single copies of this new edition, RC-16, can be ordered from RCA Photophone Ltd., 36, Woodstock Grove, London, W. 12, price 5s 6d, post free.

Long Range Television

Review of Propagation Conditions

Prevailing During Reception in South Africa

By T. W. BENNINGTON (B.B.C.) and R. MORRIS (Panorama Receiving Station, S.A.B.C.)

REGULAR reports on reception of the Alexandra Palace 41.5-Mc/s sound channel have been sent since 13th March, 1949, to the B.B.C. from the Panorama Receiving Station of the South African Broadcasting Corporation, near Johannesburg. At this station from 5 to 7 observations are made daily throughout the year on this frequency, covering both the forenoon and afternoon transmitting periods. The results of the observations are reported in a 5-figure code, in which the first figure designates the signal strength on a scale of 0-5, while the remaining figures indicate respectively the fading, noise, interference and overall merit. In this review we are concerned with the propagation conditions and so the signal strength figure only has been used. During all observations when it is not possible to allot a figure of 1, or greater, to the reception, either "Nil" reports are given, or else the designation "BNL" (Below Noise Level) is used, both of which classifications are taken to mean that the signal strength is, in fact, zero.

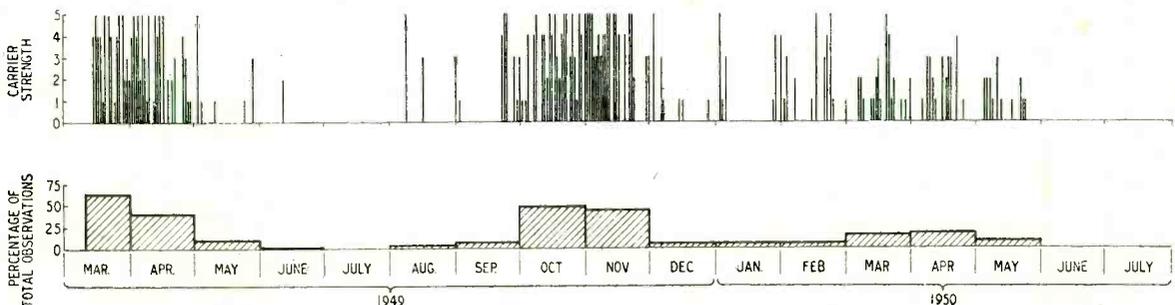
The reports have here been analysed for the period 13th March 1949 to 31st July 1950. In the upper section of Fig. 1 are shown the days on which reception was obtained. On each of these days the observation giving the strongest signal of the day was taken and the results are plotted as vertical lines on the scale 0-5. During 1949 reception was far more frequent, and signals were, in general, stronger during the months of March, April, October and November than during the other months of the year. It should be noted, however, that had observations been made during the early part of the year, frequent reception might have been had during February. Reception conditions were the most favourable in the early spring and late autumn, though mid-winter produced occasional reception. During the

summer conditions were particularly poor and on one day only during June, and on not a single day in July, was reception obtained, though just as many observations were made then as during other months. In 1950 signals were heard on several days during mid-winter, though it again tended to increase towards the vernal equinox. It is again significant that not a single case of reception was obtained between 24th May and 31st July when our record finishes. It is to be noted that reception during the early spring of 1950 was much less frequent than during that of 1949, due, no doubt, to the decreased solar activity and the consequent fall in the ionization of the F_2 layer.

In the lower section of Fig. 1 there are given, in histogram form, the total number of cases of reception at strength 1 or greater, as a percentage of the total number of observations made during the month. Reception on 41.5 Mc/s was most frequent during March 1949, when 65 per cent of the observations produced signals, and it was least frequent during June and July 1949, while June and July 1950 were completely blank months. It will be noted that in the late winter/early spring period reception peaked during the equinoctial month of March, whereas at the late autumn/early winter period the equinoctial month of September did not produce a notable increase in reception, which reached its seasonal peak in the following month. It would be expected that reception would peak just after and just before the mid-winter period rather than at the equinoxes, and it is difficult to assign a reason for this asymmetry in regard to the peak reception months of 1949, particularly as sunspot activity during April and September was at similar levels.

It seems reasonable to assume that the best conditions for reception tended to occur towards both

Fig. 1. Graphical records of reception of Alexandra Palace 41.5 Mc/s sound signals in Panorama South Africa. Day-to-day signal strength is given in the top half, the lower showing the monthly reception as a percentage of the observations made.



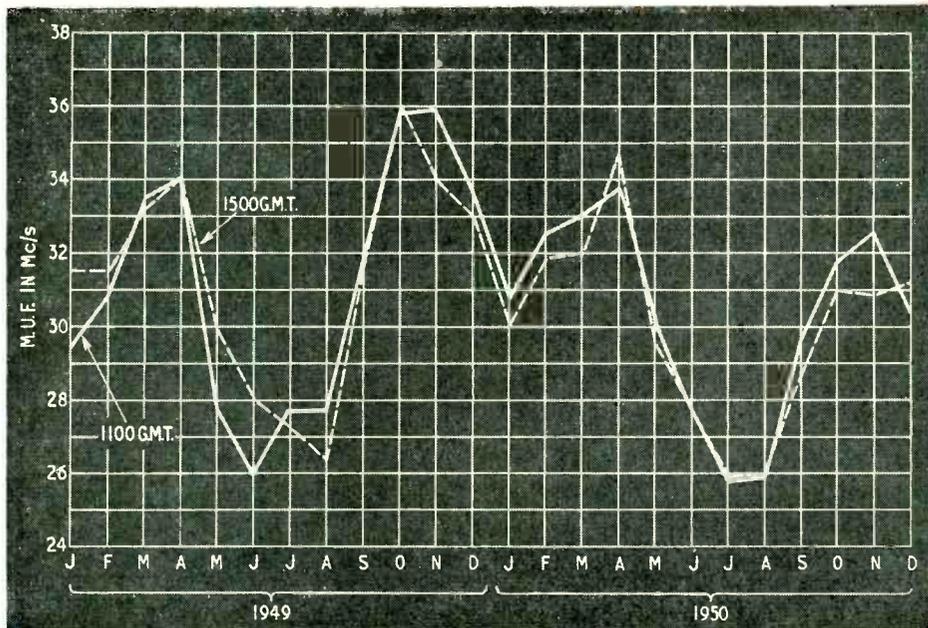


Fig. 2. Predicted monthly m.u.f.s for the Daventry/Johannesburg path at 1100 and 1500 hours G.M.T. during 1949 and 1950.

vernal and autumnal equinoxes. Again in March and April 1950 there occurred an increase in reception, followed by a sharp decrease in June. The level of reception in the spring of 1950 was very much less than in the same months of the previous year, which may be accounted for by the fact that the sunspot activity (as indicated by the monthly sunspot numbers) has decreased by approximately one-third as between March/April 1949 and March/April 1950.

Comparison with Ionospheric Data

It is not feasible to compare these results with any measured m.u.f. (maximum usable frequency) data, because no such charts are published, and there do not exist enough measured critical frequencies over this path on which to estimate the results with the predicted m.u.f. for the path, as obtained from the world ionospheric contour charts, which are compiled on the basis of past measured data supplied by the world network of ionospheric measuring stations.

It is not to be expected that, because reception was obtained on a few days during any particular month, the mean m.u.f. for that month would reach 41.5 Mc/s. It is known that there is a very considerable day-to-day variation about the monthly mean value, and so it might be possible to receive 41.5 Mc/s on several days during the month when the mean m.u.f. for the path was much lower. Nevertheless, when reception was obtained on 50 per cent, or more, of the observations made, it would indicate that the mean monthly m.u.f. for the path must have been near 41.5 Mc/s.

In Fig. 2 are plotted, for 1100 and 1500 G.M.T., the predicted monthly m.u.f.s for the path for 1949 and 1950, as obtained by the use of world ionospheric contour charts. It will be seen that there is a large seasonal variation in the predicted m.u.f. for the path, such that low values are to be expected in the summer, highest values before and after the mid-

winter period and medium - high values at mid-winter. The general trend of the seasonal variations in m.u.f. thus agrees exactly with the observed results at Panorama, in that the seasonal periods when no reception was obtained occur when the predicted m.u.f. was lowest, the most frequent reception when it was highest and occasional reception when it was less than the highest expected. It is to be noticed that there is a general fall in predicted m.u.f.s with time, in accordance with the decrease in sunspot

activity, so that the late winter/early spring peak in m.u.f. in 1950 is lower than either peak of 1949, and this agrees with the decreased amount of reception in the late winter/early spring of 1950 as compared with the peak reception periods of 1949. Actual values of predicted m.u.f. would appear to be somewhat lower than those which must have prevailed, for during no month did the predicted mean exceed 36 Mc/s, whereas during several months 41.5 Mc/s was received frequently.

In conclusion we can summarize:—

(1) Reception of 41.5 Mc/s over the London/Panorama transmission path was obtained; (a) frequently during the late winter/early spring and late autumn/early winter periods, (b) occasionally during the mid-winter period, and (c) not at all during the summer period.

(2) The seasonal variation thus disclosed is in exact accordance with the expected variation of m.u.f. over the path, as indicated by the predicted m.u.f. values. There is strong evidence, however, that the predicted m.u.f.s were somewhat lower than the actual frequencies for the path, at least during the equinoxes.

(3) Reception during the late winter/early spring period of 1950 was much less frequent than during both periods of peak reception of 1949, due to the general fall in sunspot activity and the consequent decrease in the ionization of the F_2 layer.

INTERFERENCE MEASURING SET

THE Electrical Research Association has recently designed for the Admiralty a portable interference measuring set in conformity with the requirements of BS1597 (suppression of marine installations) and BS727 (general measurement of radio interference). Sets to this specification, which are equally suitable for marine or land use, are being made by E.M.I., though the Admiralty states other civilian organizations may use the design without change. Further information may be had from the E.R.A., Perivale, Middlesex.

Phase-Shift Oscillators

New Circuit Giving Constant Amplitude

By W. G. RAISTRICK (Pye, Ltd., Cambridge)

THE circuits to be described are all based upon the phase-shift oscillator shown in Fig. 1. In order to produce self-sustaining oscillation in this arrangement two conditions must be satisfied. First, the voltage introduced from the output of the amplifier must be in phase with that fed back to the input, and, secondly, the voltage gain in the amplifier must be rather greater than the loss in the resistance-capacitance network.

A further requirement, important when a variable-frequency oscillator is considered, is that the sum of the amplifier-gain and the network loss should be constant over the whole of the frequency range in order that the voltage output may remain constant and the amplifier valve work always on the same part of its characteristic. The success or otherwise depends very largely upon how accurately one can maintain the system in a condition when it oscillates only very gently, and in practice most oscillators of this type embody some form of automatic amplitude control. The design of this control is greatly simplified if the amplitude variation in the first place is only slight.

If we make the assumption that the valve-amplifier gives a constant voltage-gain and a constant phase-shift of 180° over the whole range of frequencies to be considered, then we are left with the problem of designing a phase-shifting network which gives a phase change of 180° and a constant loss over the frequency range.

In the circuit of Fig. 1 it is not feasible to obtain a phase shift of more than 60° in each resistance-capacitance section so that the minimum requirement for oscillation is three sections. If the network loss is to remain constant then either all the capacitors or all the resistors must be varied simultaneously and it is this latter feature which has led to the comparative neglect of this type of oscillator for generating variable-frequencies.

Three-gang potentiometers are not easy to obtain, and if the normal type of tuning capacitor of 500-600 pF, is pressed into service then at least two will be required for each section, if frequencies of the order of 20 c/s are contemplated, otherwise the associated fixed resistors become of so high a value that the valve grid is extremely susceptible to hum pick-up. A further consideration is that the loss in the network decreases with the number of sections. It is $1/29$ for a three-section network and $1/18$ for a four-section one, necessitating valve voltage gains of rather more than 29 and 18 respectively. This is one reason why some of the oscillators described in the past have had as their tuning elements two four-gang capacitors coupled together.

By employing the more elaborate phase-shifting circuit of Fig. 2 it is possible to obtain a phase-shift

per stage of approximately twice that obtained with the simpler circuit. As is well-known, the virtues of this particular phase-shifting circuit are that the phase may be changed from 20° to 160° without any appreciable change of amplitude at the output terminals, so long as no attempt is made to draw power from the circuit, and it thus becomes possible to design an oscillator with only two stages of phase-shifting. Also, only one variable element is required although, as will be pointed out later, it is not always advisable to avail oneself of this characteristic.

Phase-splitting Valve

In all the oscillator circuits which have so far been tried by the author the centre-tapped transformer of Fig. 2 has been replaced by a phase-splitting valve. Each phase-shifting section then becomes as in Fig. 3.

For a first analysis we may neglect the effects of the valve anode resistance, the input impedance of the succeeding stage and the cathode-bias resistor.

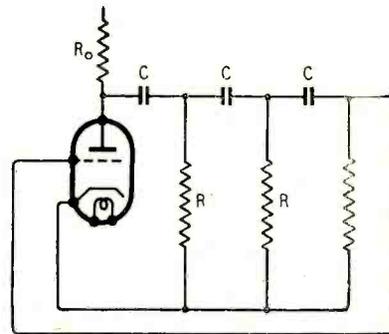


Fig. 1. Conventional phase-shift oscillator.

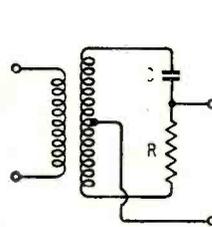


Fig. 2. Constant-amplitude phase-shift circuit with transformer input.

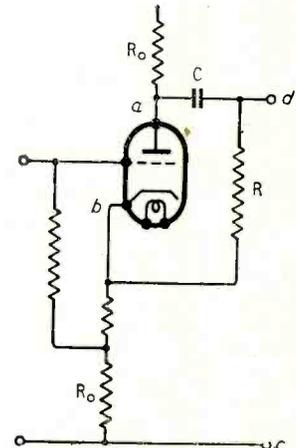


Fig. 3. Push-pull phase-splitting circuit which can replace the transformer of Fig. 2.

The equivalent circuit is then that of Fig. 4(a). If now a sinusoidal voltage of amplitude E is applied between terminals ab , then the current through

the resistive branch becomes $\frac{E}{2R_0}$, and that through the RC branch

$\frac{E}{R + 1/j\omega C}$. The resulting voltage

distribution is shown in the vector diagram of Fig. 4(b); note in this that the angle adb will remain a right angle as C or R is varied assuming C to be a capacitor of low power factor, so that the point d will describe a semicircle about the centre c , and cd will always be equal to both ac and cb since all three are radii of the same circle. The voltage cb , the cathode voltage, is in phase with the input voltage to the valve grid, and cd is the output voltage, so that the phase angle θ between input and output voltages is the angle bcd . By the process of completing the parallelogram, Fig. 4(c), and bisecting angle θ by the perpendicular cf , it can easily be seen by inspection that the tangent of half

this angle is: $\tan \frac{\theta}{2} = \omega CR$. Now

$\tan 2x = \frac{2 \tan x}{1 - \tan^2 x}$ from which

$$\tan \theta = \frac{2\omega CR}{\omega^2 C^2 R^2 - 1} \dots \dots (1)$$

Fig. 5 depicts an oscillator constructed by associating two such phase-shifting stages with a valve-amplifier V_3 . If we denote the phase shift obtained in the second stage by

$\phi = \frac{2\omega C_1 R_1}{\omega^2 C_1^2 R_1^2 - 1}$ then oscillation will be obtained when $\theta + \phi = 180^\circ$.

Now $\tan(\theta + \phi) = \frac{\tan \theta + \tan \phi}{1 - \tan \theta \tan \phi}$ and substituting from (1)

$$\tan 180^\circ = 0 = \frac{2\omega CR}{\omega^2 C^2 R^2 - 1} + \frac{2\omega C_1 R_1}{\omega^2 C_1^2 R_1^2 - 1} \div \left(1 - \left(\frac{2\omega CR}{\omega^2 C^2 R^2 - 1} \cdot \frac{2\omega C_1 R_1}{\omega^2 C_1^2 R_1^2 - 1} \right) \right)$$

From which $\omega^2 = \frac{1}{R C R_1 C_1}$

And $f = \frac{1}{2\pi \sqrt{R C R_1 C_1}} \dots \dots (2)$

It now can be seen wherein lies the disadvantage in having only one tuning element, for assuming we decide to allow the resistance R to fulfill this function then $C = C_1$ and the expression for oscillation frequency becomes $f = \frac{1}{\sqrt{R} \cdot \sqrt{R_1 C}}$; in other words the

frequency becomes proportional to $\frac{1}{\sqrt{R}}$ and a linear control will give an extremely cramped scale if a coverage of the order of 10:1 for each range is considered. In order to obtain an approximately

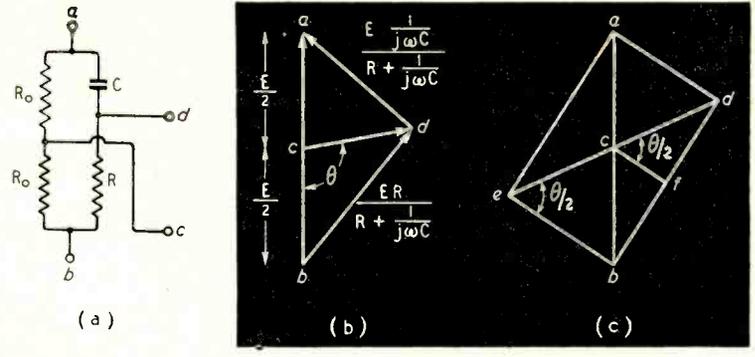
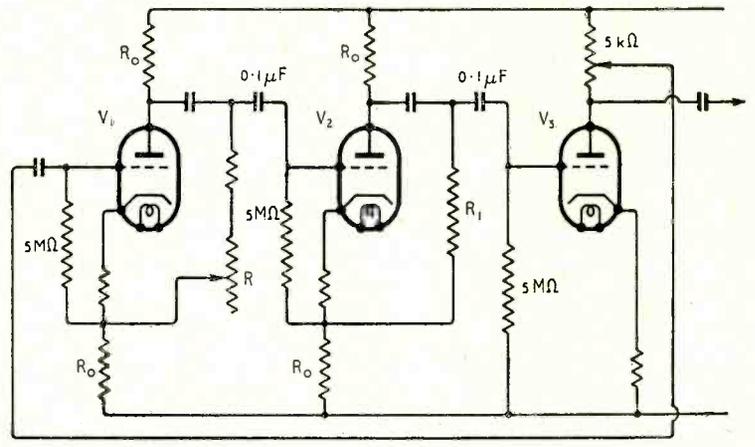


Fig. 4. Basic phase-shift circuit alone (a) and vector diagram of voltages (b). The parallelogram is completed in (c).

Fig. 5. Circuit of complete oscillator with two phase-shift and one amplifier stages.



logarithmic scale then a logarithmic potentiometer will have to be used and unfortunately logarithmic wire-wound potentiometers are not obtainable in large ohmic values.

However, when extreme accuracy and permanence of calibration are not important, quite useful instruments can be assembled around the ordinary carbon-track volume control with a log or semi-log law. A practical design along these lines would proceed somewhat as follows. The minimum value of R should not be reduced below about 5 kΩ, and from (2) it can be seen that the maximum value is equal to $(f_1/f_2)^2 R_{min}$ where f_1/f_2 is the ratio between maximum and minimum frequencies on any one range. For decimal scales this ratio is, of course, 10, and R_{max} becomes 0.5 MΩ. R could conveniently be a fixed resistor of 5 kΩ in series with a 0.5-MΩ potentiometer. R_1 should be a fixed resistor equal in value to

$$\sqrt{\frac{R_{max}}{R_{min}}} \cdot R_{min} = 5 \times 10 \text{ k}\Omega, \text{ and } C \text{ would equal } C_1,$$

and be simultaneously switched for each range, increasing in capacitance in multiples of 10. It will be found that sufficiently good multiplication will be obtained over the whole frequency range to enable a single calibration to be used, and the range-changing switch used merely as a multiplier, labelled $\times 1$, $\times 10$, $\times 100$, etc., so long as sufficient care is taken over decoupling arrangements at the lower

frequencies. The coupling capacitors preceding the phase-splitting stages need not be embarrassingly large even for quite low frequencies as the input impedance of the particular type of phase-splitter used is high. A value of $0.1 \mu\text{F}$ is adequate for frequencies of the order of 20 c/s.

The anode and cathode load resistors R_0 should be of fairly low value—something between 2 and $5 \text{ k}\Omega$ will be found suitable. The "gain" of each phase-shifting stage is that which is normal for this type of phase-splitter and should not be less than 0.8 or 0.64 for the two together; thus the gain of the amplifier V_3 need not exceed 1.6 and its design becomes very simple.

No provision for automatic amplitude control is made in the circuit of Fig. 5. The feedback is controlled by the $5\text{-k}\Omega$ potentiometer and, once set, it will be found that reasonably constant output will be obtained over the frequency range without further adjustment. When the output is required to be as free from harmonic distortion as possible, then it must be set at the lowest possible setting consistent with reliable oscillation, and under this condition the total harmonic content can easily better 1 per cent.

Readers who prefer to embody some kind of amplitude limiting in their designs can use any of the usual arrangements. In this connection it may be mentioned that both valve-operated control circuits and temperature-controlled devices, such as Thermistors,

have been used by the writer with good results. Enough has been said to indicate that the use of the valve phase-shifter* principle makes available a RC oscillator allowing fair flexibility of design. A single- or a double-element control may be used as desired, and this control may be either resistive or capacitive; for instance the circuit of Fig. 5 could have employed a single capacitor as the tuning control with a range of 3.16 to 1, covering the audio-frequency band of 20-20,000 c/s in 6 switch-positions. Alternatively a twin-gang potentiometer can be made to give a range in excess of 30:1 in one sweep, and in all cases the output remains constant.

These advantages are secured at the expense of two extra valves, but this is not so great a complication when it is remembered that both phase-shifters can be sections of one of the popular small twin-triodes, and V_3 can be another section of a further valve of the same type. The complete oscillator plus output stage need therefore have no more than two "bottles." With the circuit of Fig. 1 the valve must nearly always be a multigrid type in order to obtain the necessary gain. In addition a cathode-follower is commonly added, so that the RC network may be fed from a low-impedance source, and two glass envelopes are still required, for the oscillator alone.

*British Patent No. 3516/1949.

B.B.C. REPORT FOR 1949/50

A COMPREHENSIVE account of the work and progress in the operation of both the sound and vision services of the B.B.C. during the year ended last March is given in the Annual Report of the Corporation, which is published by H.M. Stationery Office.

After dealing with the engineering developments of the year, the section devoted to the technical aspects of the Corporation's activities, concludes with some notes on the television research undertaken. In order to obtain data concerning the probable mutual interference which would be experienced with synchronized television stations working on the same wavelength (which will, of course, be necessary as there are only five channels available and ten stations are planned) six recording posts were in almost continuous operation during the year and an unbroken record was kept of reception from experimental transmitters over long distances. Recordings were also made of the Alexandra Palace transmissions in Scotland and of the Sutton Coldfield transmissions in the London area.

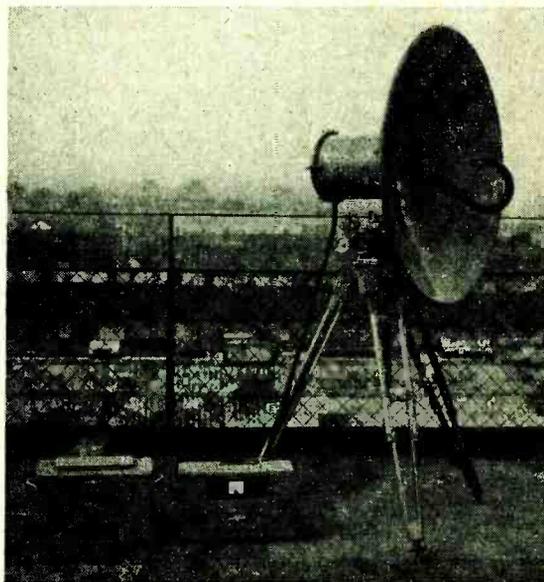
As a long-term project to appraise the relative merits of different systems, it is stated in the Report that preliminary experiments are being made on systems using higher standards of definition and on colour television. To facilitate work of this kind, a new flexible television transmitter designed to operate at will on standards of definition from 400 to 900 lines, has been constructed for use in the laboratories.

On the financial side, the Report records that although the Treasury retained 15 per cent of the licence revenue— $\pounds 1,753,926$ —and the Post Office received $\pounds 814,111$ for expenses of collection and interference investigation, the Corporation's net licence income was $\pounds 9,938,917$ —an increase of $\pounds 494,445$ on the previous year. Of this amount $\pounds 272,747$ was derived from the additional $\pounds 1$ charged for the combined sound and television licence. The revenue from the sale of publications was $\pounds 1,039,464$. It is noteworthy that 25.3 per cent of the year's expen-

diture on the Home and Television Services is classified as "engineering."

One of the best reproductions of an end-of-tube picture—showing Their Majesties at the Royal Opera House, Covent Garden—is among the illustrations in the Report, which costs 3s.

TELEVISION O.B. LINKS.—Six centimetre-wave transmitters, similar to that illustrated, are to be supplied to the B.B.C. by Marconi's to provide radio links for television outside broadcasts.



Communications on 460 Mc/s

Suitability of the Decimetre Waves for Mobile Services

By E. G. HAMER, B.Sc. (Eng.) (Hons.), A.M.I.E.E., Ass.Brit.I.R.E. (G.E.C. Research Laboratories, Wembley)

A FEW years ago it was thought that the frequency spectrum between 70 and 100 Mc/s would be wide enough to accommodate most of the necessary radio services, particularly short-range fixed links and mobile communication. The demand for frequencies in this band for use in essential services such as police work has, however, been so heavy that additional allocations are not now readily available. Higher frequencies were therefore sought for some less essential services, including taxis and the press, and, at the 1947 Atlantic City conference, the International Telegraph Union allocated the band between 156 and 184 Mc/s for this type of user. Here again, since only part of this band is available for commercial fixed link and mobile services, it appears that the congestion in this new band will shortly be the same as it is now between 70 and 100 Mc/s. All the available frequencies are rapidly being allocated and the next logical step will obviously be to move yet higher up the frequency spectrum to the range between 460 and 470 Mc/s, which was allocated at Atlantic City to fixed and mobile stations, and is used in America for "citizens' radio."

Previous work has shown that frequencies in the 700-100-Mc/s band give slightly better results than those between 156 and 184 Mc/s when used for mobile types of service. For frequencies of the order of 460 Mc/s, however, the performance has not been so accurately known. The various conflicting reports made in the past had led to the assumption that the usefulness of such frequencies for mobile communication largely depended on the location of the fixed station aerial.

Mobile Station

In order to obtain more precise information on this point and, further, to investigate the behaviour of the received signals under non-"line-of-sight" conditions, an extensive programme of tests was undertaken in the London area. During these tests, the opportunity was taken of measuring the field strengths received at the mobile station and comparing these measured values with those predicted from theoretical considerations.

The tests were made using various fixed station sites, roughly corresponding to sites in open country, together with a site in the centre of a built-up area. The receiver was installed in a car, which was used as the mobile station and, in some of the tests, the transmitted power and the receiver sensitivity were adjusted to a value likely to be obtained with "walkie-talkie" type of equipment.

The transmitter consisted of a low power r.f. unit giving a frequency modulated signal at a frequency of about 115 Mc/s. This unit was used to drive a series of doubler and earthed-grid

amplifier stages. A power output of 30 watts was obtained from the final amplifier and, with the length of the feeder in use, gave a radiated power of 6 watts from a simple vertical dipole aerial fitted with a quarter wave co-axial stub standing wave suppressor. The immense loss of power in the feeder with this arrangement was due to the unavoidably large separation between the transmitter and its aerial. No attempt was made to increase the all-round aerial gain, although at these frequencies an aerial array is very attractive owing to its small physical size.

A normal frequency modulated receiver was used in the car and operated on a frequency of 40 Mc/s. This receiver was preceded by an extra frequency changing unit. Figure 1 gives a block schematic diagram of this arrangement, which consists of a capacity-loaded line connected to a silicon crystal valve used as a frequency changer. The local oscillator frequency is provided by a quartz crystal oscillator, followed by a chain of multiplier valves. An additional stage of amplification at the first i.f. of 40 Mc/s is included between the mixer head and the normal receiver. Such an arrangement gave a minimum receiver sensitivity for an intelligible output of 4 μ V input across 70 ohms. A complete receiver designed in accordance with the latest practice might be expected to have a sensitivity of the order of 1-2 μ V across 70 ohms. The aerial fitted to the car consisted of a quarter wave whip aerial mounted above a metal sheet acting as an earth plane. Again, no attempt was made to use an aerial array to give an increased gain.

Communication from the car to the fixed station was provided by normal v.h.f. equipment with a transmitted power of 10 watts and a receiver sensitivity of 1 μ V across 70 ohms. This circuit was operated at a frequency of 100 Mc/s, so that an indirect comparison with the performance of the 460-Mc/s equipment was obtained by noting the areas in which signals to and from the car could not be received.

The characteristics of the equipment used can be

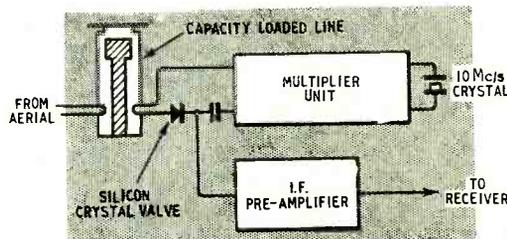


Fig. 1. Schematic layout of the experimental 460-Mc/s receiver.

summarized as follows: (a) transmitter; radiated power 6 watts; peak deviation ± 45 kc/s; operating frequency 466 Mc/s; (b) receiver; sensitivity (for usable signal) $4 \mu\text{V}$ across 70 ohms; bandwidth ± 160 kc/s at 3 db points.

For the first series of trials, the fixed station aerial was located on top of a water tower near Ealing, 120 feet above local ground level and some 200 feet above the surrounding terrain. The mobile set in the car was taken to a number of places, including non-"line-of-sight" locations behind near and distant hills. Field strength measurements were also made at selected sites, for subsequent comparison with the calculated values. The non-"line-of-sight" positions can be described as: (a) behind a long range of hills seven miles away; (b) behind a local hill two miles away; (c) behind a large hill four miles away, also partly screened by another hill between it and the fixed station.

The approximate service area for continuous reception had a radius of about eight miles, comparing very favourably with the 100-Mc/s signals. On good receiving sites, of course, much greater ranges were obtainable.

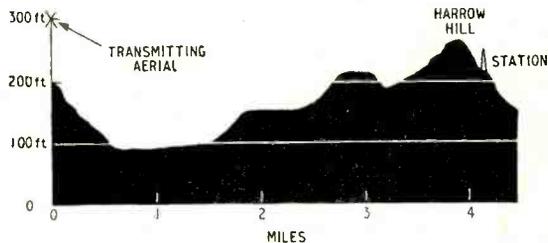
The second series of trials was made with the fixed station in the centre of London, the aerial being mounted 30 feet above roof level, the aerial height above ground level being 130 feet. Mobile tests were again conducted in and about the City of London, and field strength measurements were taken behind Hampstead Hill. Reliable communication in this instance was obtained up to a range of seven miles, and within a radius of two miles the effects due to fading of the signal were negligible.

Some Comparisons

The results obtained in the two series of tests described above gave rise to the following conclusions: communication results obtained during mobile working on a frequency of 460 Mc/s are, in general, inferior to those experienced using a frequency of 100 Mc/s. In isolated instances in built-up areas the 460-Mc/s frequency may give a better service owing to standing wave effect. As is usual with v.h.f. and e.h.f. installations, there is a variation in field strength depending on multi-path propagation and, as a car moves through the resultant field, a fluctuation in field strength is encountered causing the strength of the received signal to vary. The rate of flutter is greater at 460 Mc/s than at 100 Mc/s since the wavelength involved is shorter. When frequency modulated transmissions are used, and provided the receiver has good limiters, the effect on intelligibility is of the same order as when using 100-Mc/s equipment. If, however, the limiting action of the receiver is poor, or the a.g.c. time-constant incorrect, this rapid flutter fading may give rise to an effect which is similar to a superimposed low frequency modulating the speech intelligibility. The effect is to mar the speech quality badly and to reduce the intelligibility.

During both trials the equipment operating on 460 Mc/s did not give as great a range as that used on 100 Mc/s. The difference between the two values was, however, usually small, being of the order of 10 to 20 per cent. It was also interesting to observe that, during communication to a heavily wooded country area, the trees appeared to cause more

Fig. 2. Ground contour of typical site used for field strength measurements.



attenuation of the 460-Mc/s signal than of the 100-Mc/s signal. This effect was more pronounced when the trees were wet, although the presence of wet buildings in a built-up area appeared, if anything, to improve the 460-Mc/s communications.

The effect of operating the mobile station under trolley-bus wires and bridges was negligible, unless the bridge was of metal and, at the same time, very low and wide. Even in a town in very heavy traffic, the amount of ignition interference experienced was very small, despite the use of an intermediate frequency of 40 Mc/s and a relatively poorly screened experimental receiver. Good signals were obtained in the centre of the City of London about 2 miles from the fixed station, even in very narrow "canyon"-like streets, and again the effects of passing traffic caused very little alteration in the signal. In particular, it was found that, in these narrow streets, there appeared to be no significant difference in signal level between adjacent streets which were radial and circumferential to the fixed station.

A further series of tests was carried out to simulate the conditions likely to be obtained using "walkie-talkie" type of equipment, and in some instances the receiver used was of the simple super-regenerative type. The transmitted power was 0.25 to 0.5 watt, and the minimum receiver sensitivity for a usable signal was $30 \mu\text{V}$ across 70 ohms. From a high site the range to the sensitive receiver ($4 \mu\text{V}$) was $2\frac{1}{2}$ miles in open country and 1 to $1\frac{1}{2}$ miles in a built-up area. With the super-regenerative receiver the range was reduced to 400 yards in a built-up area. In another instance the transmitter aerial was placed about 3 feet above ground level, adjacent to and outside the wall of a brick and steel building, halfway between the two ends of the wall. When using the super-regenerative receiver inside the building the range obtained was between 60 and 100 yards, depending on the type of obstructions inside the building and upon the floor level on which the receiver was used. Outside the building (which was approximately 100 yards square) signals were received along the side where the transmitting aerial was located and along the adjacent sides, but they were not received on the opposite side of the building.

As a general rule the simple "walkie-talkie" equipment gives service, when used in the open, over a range of 200-400 yards, depending on the location of the aeriels. When used inside a building the range is reduced to 60-100 yards. It should, however, be remembered that at present it may not always be possible to achieve such performances using filament type battery valves.

An approximate analysis was made of the anticipated field strength in the areas where the field strength had actually been measured. This analy-

sis was based on the nomograms published by Bullington.* For the non-"line-of-sight" position, the field strengths were calculated at the crest of the intervening hill to determine whether smooth earth or free space conditions should be used. The appropriate shadow loss and, if necessary, the grazing loss were taken into account.

Figure 2 shows the ground contour of a typical site tested. Allowance is made for the grazing loss over the intermediate hill, and for the shadow loss due to the principal hill. The calculated transmission loss is 119db, which is in satisfactory agreement with the measured loss of 124 db. A series of some 40 readings were made and the results were found to be consistent for any transmitting station site.

The results obtained with the transmitter on an open site show very close agreement with the results calculated by the Bullington method, the two values usually being within 3 db of one another for a simple non-"line-of-sight" path. This may, to some extent, be fortuitous in view of some of the assumptions made, particularly in regard to the gain or loss of the aerials and feeders. Using identical equipment in a built-up area, it was found that there was an extra loss of some 10db in the measured values. This loss may be accounted for by the indeterminate extra "grazing" loss due to the roofs of surrounding buildings. Such extra indeterminate losses can be regarded as being a function of the transmitter aerial height above roof level rather than of its actual height above ground level. Small increases in aerial height are therefore likely to give much greater signals, while the converse is also true.

It can therefore be stated that, where a high transmitting aerial is situated in the open, the propagation loss may be evaluated to a fair degree of accuracy, even under non-"line-of-sight" conditions. In a built-up area, however, an extra fixed loss must be added to the calculated loss. This extra fixed loss may vary in any given direction depending upon the heights and types of building near to the fixed station aerial.

The general conclusion drawn from the entire series of tests was that frequencies in the 460-470-Mc/s band could be used for many mobile radio services. A satisfactory service would definitely be obtained, although the service area would be slightly less than when using frequencies in the 70-100-Mc/s band. The service area could be increased by the use of aerial arrays giving omni-directional gain, these aerials being physically small, and might then be comparable with the 100-Mc/s service area. This general statement may not, however, be applicable in extremely rugged terrain so that, as when lower frequencies are used, exploratory tests on the actual site are desirable under such conditions.

* K. Bullington, Radio Propagation at Frequencies Above 30 Mc/s. Proc. I.R.E., 35, 1122-1136 (October, 1947).

Presenting Pickup Characteristics

THE need for a standardized presentation of audio-frequency response curves, to facilitate comparison, has long been recognized, and, as a first step, the Gramophone Equipment Panel of the Radio and Electronic Component Manufacturers Association have recommended their members to adopt a scale ratio of 38 db per octave. Graph paper on this basis (actually 3 inches per octave of frequency and 1 centimetre to 5db of vertical scale) has been prepared and is obtainable

from H. K. Lewis & Co., 136, Gower Street, London, W.C.1. The chart includes a useful ruled panel for relevant data.

Nomenclature: Standard Terms

SEVERAL supplements to British Standard 204:1943 ("Glossary of Terms used in Telecommunication") have recently been issued by the British Standards Institution, 28 Victoria Street, London, S.W.1.

Supt. No. 2: Glossary of Terms used in Radio Propagation.—Terms connected with radio propagation through the ionosphere and troposphere. Price 2s.

Supt. No. 3: Fundamental Radio Terms.—Definitions of the terms used for the various applications of radio in communication and location, with a chart showing the relation between the various methods. Price 1s.

Supt. No. 4: Glossary of Terms used in Radar.—Price 2s.

CLUB NEWS

Basingstoke.—The secretary of the Basingstoke District Amateur Radio Society advises us that owing to lack of support it has been decided to discontinue the Club's activities. Sec.: L. S. Adams, "Rosien," 16, Brambllys Drive, Basingstoke, Hants.

Belfast.—Two 150-watt transmitters, one 'phone and one c.w., are now in use at the headquarters of the City of Belfast Y.M.C.A. Radio Club, Wellington Place, under the call sign G16YM. Morse classes are held on Wednesdays—the club night—and Thursdays. Sec.: S. H. Foster (G13GAL), 51, Belmont Park, Belfast.

Birmingham.—At the meeting of the Slade Radio Society in the Parochial Hall, Broomfield Road, Erdington, on December 8th at 7.45, W. H. Yeates (G.P.O.) will speak on "Telephone Transmission Systems." Sec.: C. N. Smart, 110, Woolmore Road, Erdington, Birmingham, 23.

Bournemouth.—Meetings of the Bournemouth Radio and Television Society (G3FVU) are held on the first and third Thursdays of each month at 7.30 at the Cricketer's Arms, Windham Road. Sec.: F. G. Hamshere, 99, Elmes Road, Winton, Bournemouth, Hants.

Brighton.—Membership of the Brighton and District Radio Club is now about 80 and meetings are held every Tuesday evening at 7.30 at the "Eagle Inn," Gloucester Road. The club station, G3EVE, is operated on alternate Tuesday evenings on 80 metres (c.w. and 'phone). Sec.: L. Hobden, 17, Hartington Road, Brighton, Sussex.

Chester.—Morse classes are held for an hour prior to the weekly meetings of the Chester and District Amateur Radio Society (G3GIZ) which are held at 7.30 on Tuesdays in the Tarran hut in the Y.M.C.A. grounds. Sec.: R. C. Windsor, 17, Hough Green, Chester.

Coventry.—Fortnightly meetings of the Coventry Amateur Radio Society are held on alternate Mondays at 7.30 at the B.T.H. Social Club, Holyhead Road. On December 4th demonstrations will be given of aids to reception. Sec.: K. G. Lines (G3FOH), 142, Shorncroft Road, Coventry.

Dorking.—Weekly meetings of the Dorking and District Radio Society (G3CZU) are held at the H.Q., 5, London Road on Tuesdays at 7.30. A lecture on valve technique will be given on December 19th. Sec.: J. Greenwell, G3AEZ, 7, Sondes Place Drive, Dorking.

Gravesend.—Weekly meetings of the Gravesend Amateur Radio Society are held on Wednesdays at 7.30 at the club headquarters, 30, Darnley Road, Gravesend. Sec.: R. E. Appleton, 23, Laurel Avenue, Gravesend.

Malvern.—Meetings of the Malvern and District Radio Society are held on the first Wednesday of each month at 7.45 at the "Foley Arms Hotel." A lecture on "Microphones and Loudspeakers" will be given at the December meeting.

Wakefield.—The Secretary of the Wakefield and District Amateur Radio Society will give members of the club "An Introduction to Frequency Modulation" at the meeting at Service House, Providence Street, at 7.30 on December 13th. Sec.: W. Farrar (G3ESP), "Holmcroft," Durkar, Wakefield.

Walworth.—Meetings of the Walworth (Men's Institute) Radio Club are being held each Wednesday and Friday from 7 to 9 at The Avenue School, John Ruskin Street, London, S.E.5. Sec.: J. Gibbs, 22, Caspian Street, Camberwell, S.E.5.

The Hall Effect

Its Application to the Measurement of the Flux Density of Magnetic Fields

IN Clerk Maxwell's time it was thought that the distribution of current in a network of wires or a fixed solid conductor was unaffected—apart from initial transient induction effects—by the application of a constant external magnetic field. Explanations of the failure of experiments to disclose any movement of the current itself, in spite of the very considerable forces experienced by the conductor, were usually sought in terms of the "incompressible fluid" theories then current. They did not entirely convince E. H. Hall,¹ working in John Hopkins' University, U.S.A., who held that even if the incompressible fluid entirely pervaded the conducting material, a lateral pressure, if not a flow, should be detectable.

His early efforts to detect changes due to a magnetic field in the equipotential points at the sides of metal strips carrying longitudinal current (Fig. 1) were inconclusive until, at the suggestion of Prof. Rowland, he tried extremely thin conductors (gold leaf on glass). These gave positive results and he was able to show that the lateral galvanometer current was, in fact, proportional to the product of the main current strength and the magnetic field. Later the effect was shown to be inversely proportional to the thickness of the material. Thus the lateral change can be expressed $V = RIH/t$. Where R is the "Hall coefficient" of the material, I = longitudinal current in amperes, H = magnetic flux density in gauss and t = thickness of conductor in centimetres.

Theories of Conduction

According to modern theories of conduction in simple metals (e.g., copper and silver), in which the current is due to a drift of electrons from atom to atom under the influence of an external field, the effect is explained if we assume that the electrons travel in straight lines under the electric field, but describe curved paths under the influence of the perpendicular magnetic field. There is a corresponding distortion of the equipotential lines which gives rise to a potential difference at the side contacts. (Fig. 1 (b).)

In other metals and semi-conductors the polarity of the Hall voltage may be of opposite sign, indicating that the current-carrying elements have the equivalent of a positive charge. These elements are not necessarily particles, but may be "holes" in the structure of a crystal lattice which are temporarily unfilled by electrons. When an electron moves into a vacant site, a "hole" is left in an adjacent part of the structure and this vacancy can travel through the material until it reaches the negative point of connection, when it will be filled by an electron. At the other end electrons are extracted, thus keeping up the supply of "holes."

The Hall effect in germanium is very high and the ratio of Hall coefficient to specific resistance, upon which the deflection of any current-indicating meter

connected to the lateral terminals will depend, is about 200 times that of copper. G. L. Pearson² has shown that it is suitable for the direct measurement of flux densities up to 20,000 gauss, and has described a simple instrument, involving only a $4\frac{1}{2}$ -V battery, a

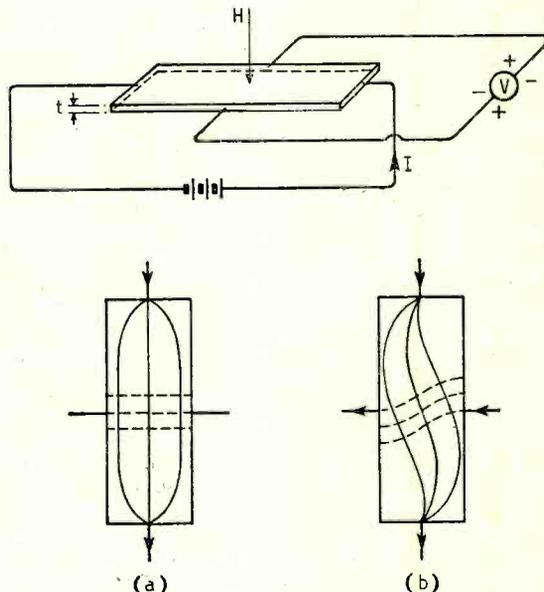
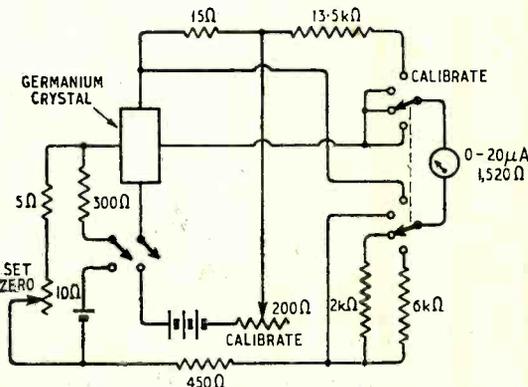


Fig. 1. Illustrating the Hall effect. Current distribution (a) without magnetic field (b) with field perpendicular to the paper. Transverse equipotential lines are shown dotted.

Fig. 2. Typical circuit for measuring field strength by means of the Hall effect in germanium.



¹ *American Journal of Mathematics*, 1879, and *Phil. Mag.*, 1880, Series 5, Vol. 9, p. 225.

² *Rev. Sci. Instr.* Vol. 19, No. 4, April, 1948.

microammeter and resistances, which can be used in conjunction with a thin slip of germanium crystal for measuring, for example, the flux in loudspeaker magnet gaps.

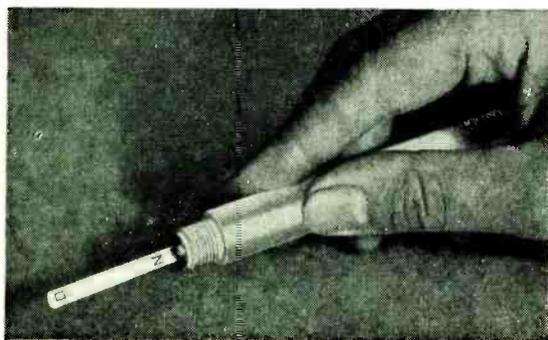
The circuit used by Pearson is given in Fig. 2. Ranges of 5, 10 and 20 kilogauss are provided and the fourth position on the range switch is used to connect the meter across a 15-ohm series resistor to check the main crystal current against a calibration mark. A potentiometer ("set zero") is used to offset any residual lateral current arising from the difficulty of soldering the leads accurately to spots of equal potential.

In Commercial Form

In this country a similar type of instrument has been produced commercially by the British Thomson Houston Company, Rugby, and is known as the Type G gauss meter. A five-way rotary switch gives ranges of 5, 10 and 25 kilogauss and has "Off" and "Calibrate" positions; there are separate calibration and zero-setting controls. The germanium crystal is in the form of a probe and is protected by a non-magnetic sheath having external dimensions of 0.14 x 0.035 x 1.25 inches; longer probes are available. The polarity of the transverse field corresponding to positive meter readings is marked on the probe.



B.T.H. gauss meter, Type G, and (below) close-up of the probe, which is protected by a non-magnetic sheath.



"RADIO LABORATORY HANDBOOK"

NEW EDITION

VALUABLE information on all aspects of test and measurement is given in the fifth, revised, edition of this popular book, recently issued from our publishers at 15s. The author, who is well-known as a consulting engineer and as a contributor to *Wireless World*, writes knowledgeably from a long and varied experience of radio. He does so in a way that will appeal to the amateur and to the professional radio man alike, for he is concerned not only with commercial laboratory apparatus but with keeping down expenditure by constructing and improvising one's own equipment. After dealing with the principles of correct measurement, he goes on to describe at length the various types of instruments and how they are used, then makes helpful suggestions on the most suitable apparatus for equipping a laboratory. Considerable space is devoted to particular methods of measurement on components, amplifiers and receivers, and special attention is given to v.h.f. work. There is also a chapter of useful reference information, together with an appendix on the construction of bridges.

This edition has been revised and new material has been added. In particular, the pages on oscillators have been re-written to include the latest developments in RC oscillators, additional information is given on thermistors, valve-voltmeters and cathode-ray oscilloscopes, and the reference section is up to date.

MANUFACTURERS' LITERATURE

Microphones and associated sound equipment described in a set of leaflets from Lustraphone, Ltd., 84, Belsize Lane, London, N.W.3.

Electric Motors of the more popular ratings in an abridged list from Higgs Motors, Ltd., Witton, Birmingham, 6.

Television Aerials and accessories described in an illustrated pamphlet from Validus Aerials, 69, Hornsey Road, London, N.7.

Coilpacks are catalogued and suitable receiver circuits given in a brochure from Osmor Radio Products, Ltd., Bridge View Works, Borough Hill, Crowdon, Surrey.

Midget Paper Capacitors, type W99, described in a "Hunt's News" leaflet issued by A. H. Hunt, Ltd., Garratt Lane, London, S.W.18.

Television Components illustrated catalogue, available to manufacturers from the Plessey Company, Ltd. (Components Division), Ilford, Essex.

Communications Receiver, Eddystone "740" general-purpose model described in a leaflet from Stratton & Co., Ltd., Eddystone Works, Alvechurch Road, Birmingham, 31.

"**Noise and Vibration in Industry**," a booklet dealing with noise-measuring instruments, from A. E. Cawkell, 7, Victory Arcade, The Broadway, Southall, Middlesex.

Sound-level Recorder, high speed, and **pH Meter**, Type 1900, described in leaflets from Dave Instruments, Ltd., 130, Uxbridge Road, Hanwell, London, W.7.

Schering Bridge specification in a bulletin from Muirhead & Co., Ltd., Beckenham, Kent.

Intercommunication system; the Ediswan Mark II Loudspeakerphone described in a brochure from the Edison Swan Electric Co., Ltd., 155, Charing Cross Road, London, W.C.2.

Receivers and Radiograms for 1951; short specifications in a catalogue from Pye, Ltd., Radio Works, Cambridge.

Television Receiver, Model TU142; a descriptive leaflet from E. K. Cole, Ltd., Ekco Works, Southend-on-Sea, Essex.

Sound Heads for magnetic recorders; brief details in a leaflet from Bradmatic, Ltd., Station Road, Aston, Birmingham, 6.

Earth Analyser for detecting earthing faults on electrical apparatus; a leaflet from Runbaken Electrical Products, 71-73A, Oxford Road, Manchester, 1.

Dark-Screen Television

Use of Tinted Implosion Guards

IN a television picture, the "blacks" are actually the colour of the unexcited portions of the phosphors on the face of the cathode-ray tube as they appear in the particular conditions of external lighting which exist at the time of viewing. Consequently, if the external lighting is fairly high, considerable loss of contrast is noted in the picture, because the light reflected from the face of the tube gives a greyish look to the phosphors.

The obvious way of preventing this loss of contrast is to eliminate external light altogether, but this is often impracticable or undesirable. When the picture must be viewed under conditions of high external lighting it is possible to maintain an adequate degree of contrast by using a suitably tinted transparent light-filter in front of the cathode-ray tube to cut down the light reflected from the face of the tube.

Such a neutral-tinted filter in the form of acrylic sheet is now quite often used in television receivers and it fulfils a double function. In addition to improving the contrast of the picture when viewed in a room not completely blacked-out, its strength in the appropriate thickness gives adequate protection to the viewer should the tube collapse.

The increased contrast is due to the fact that external light in the room passes through the filter, strikes the face of the cathode-ray tube and is reflected back through the filter again, whereas the radiations of the tube phosphors pass through the filter once only. This considerably reduces interference by reflected light.

At first sight it would seem that to obtain a picture of comparable brightness when using a filter to that obtained on a set with the ordinary clear guard, the tube brightness would have to be turned up considerably to make up for the light absorbed in the filter. This is true to a certain extent, but in practice the actual colour of the filter is not a true "straight line" neutral and although the overall transmissions of the colours used are on the average about 50-55 per cent, their transmission curves show a considerable increase in transmission in the blue and red ranges. Transmission curves for the three "neutrals" which have been specially developed for this application are given in Fig. 1, and show that the transmission rises in the blue to about 70 per cent and in the red to over 80 per cent. As the visible light from the excited phosphors of the average cathode-ray tube also peaks in the blue and red, the filter transmits about 70 per cent of the phosphor radiations as against only about 50 per cent of daylight or other external lighting.

A further point which must be remembered is that any type of clear guard of glass or plastic transmits at the best only about 90 per cent of the light from the cathode-ray tube falling on it, so that the com-

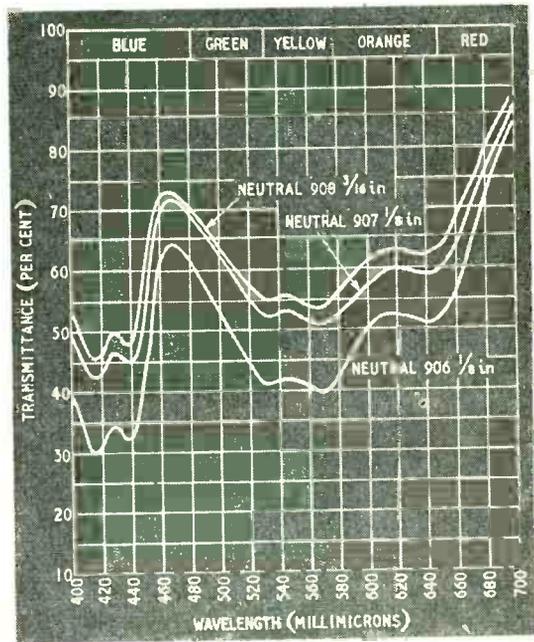
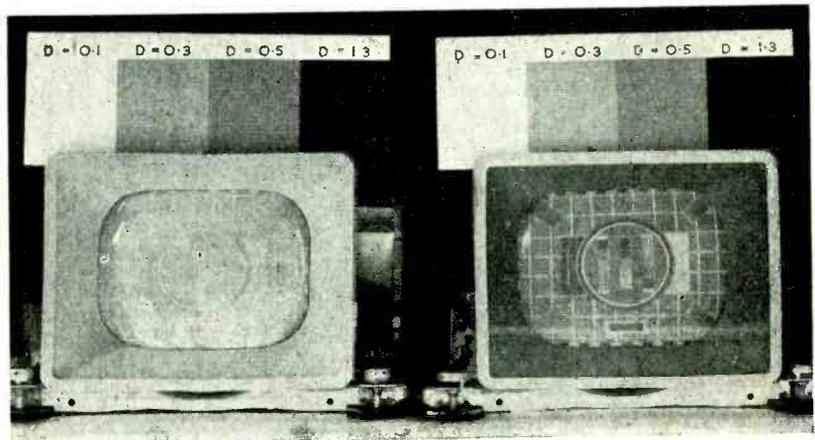


Fig. 1. Light transmission of "Perspex" acrylic sheet television implosion guards. The spectrum colours are indicated approximately against the wave-length scale.

This photograph shows identical sets under conditions of fairly high external illumination. The left-hand set has a clear guard and gives a picture of poor contrast; the right-hand set has a neutral tinted "Perspex" filter and produces a picture of good contrast.



parison of transmission of a tinted to a clear filter is about 70:90 and not 70:100.

A further effect of the coloured filter is that it completely alters the "dead pan" appearance of the cathode-ray tube and mask.

The photograph—taken in the Pye development laboratories, Cambridge—shows two identical sets operating side by side under conditions of fairly high external illumination. The left-hand set, which has an ordinary clear guard, demonstrates a picture

of poor contrast. The right-hand set, which has a neutral tinted "Perspex" acrylic filter, manufactured by I.C.I. Plastics Division, England, shows good contrast. Behind the sets are exposure squares ranging in colour from white to black which demonstrate that the photograph shows the effect as nearly as possible as it is observed by the eye. These sets were, of course, individually adjusted to give as good a picture as possible under the existing circumstances.

Radio in Germany

Broadcast Receivers and Sound Reproduction at Dusseldorf

FORMING an opinion of the broadcast receivers on show at the first German post-war radio exhibition, held at Dusseldorf in August, was not made any easier by the scarcity of circuit diagrams, but in spite of this one gained the impression that modern German design techniques are much the same as ours, and no unusual principles are involved. In outward form the sets compare very favourably with models from other countries, and have neat and attractive cabinets without too much emphasis on originality of appearance. At the same time, there is a tendency in some quarters to camouflage receivers as objects of furniture. One superhet, for instance, takes the form of an easy chair, with controls fitted on the arms and a loudspeaker in the back facing outwards. The built-in frame-aerial gives somewhat directional reception, so the chair is provided with wheels to permit easy positioning. Another example is the "Straight Three Bedside Lamp," which has nothing in its outward appearance to reveal that it is a receiver, except that the station names are printed on the shade and a shadow line indicates the station to which the "lamp" is tuned.

Most of the medium-priced German receivers now have an e.h.f. band (86.5 Mc/s to 101 Mc/s approx.) incorporated in the design, and if not, arrangements are made for adding a separate e.h.f. unit by plug-and-socket connection. Some makes also provide for f.m. reception, as there are several f.m. transmitters in use now, in Bavaria and N.W. Germany.

Interest in Tuned Circuits

When judging the merits of a receiver, the German public is interested not only in the number of valves that go with it (usually five or six) but in the number of tuned circuits in the r.f. stages, and this habit of counting tuned circuits (an i.f. transformer counts as two) is reflected in all the sales literature. "Seven tuned circuits" is a sales point, so that a dealer wishing to do business with only three has a difficult time. However, the importance of the properties of the tuned circuits is also appreciated, and quite a few receivers at the exhibition had resonant circuits with adjustable characteristics—variable bandwidth, for instance. With some models, the bandwidth auto-

matically contracts on reception of a weak signal—thereby giving selectivity and an adequate signal-to-noise ratio in exchange for a loss in quality—and then expands again when a strong station is tuned in. Other sets are fitted with a manual bandwidth control, and one manufacturer has combined this with a tone control.

The average price of broadcast receivers in Germany is much the same as in this country, but the lowest prices are well below those charged here. For instance, a straight a.c./d.c. set for reception of local stations can be bought for 65 Deutsch-Marks (just over 5 guineas), whilst the "Straight Three Bedside Lamp" mentioned above costs about the same. These low prices may be partly accounted for by the fact that the number of German manufacturers producing receiving sets has greatly increased since 1939 and competition is more intense.

Unusual Recording System

Among the exhibits of the German Federal Post department, the most up-to-date equipment on show was a telephone amplifier using germanium crystal triodes, or transistors. Compared with the 8 watts of non-utilized power consumed by an equivalent valve amplifier (for heater supplies, standing anode current, etc.) this amplifier required only 0.16 watt—a saving in power or efficiency of 98 per cent.

In the acoustics section, a long-playing gramophone recording system was displayed, giving a smaller average spacing between grooves than is normally possible. With conventional systems of recording, the width of the grooves and the spacing of any two neighbouring grooves is kept large enough to accommodate any sound amplitude—that is, any lateral needle swing—that *may* be necessary in a recording, but in this new system the width and spacing are arranged to be dependent on the amplitudes which actually do occur in the individual grooves and neighbouring grooves. The result of this more economical method of "packing" is that more grooves can be got into the space available, and it is claimed that this gives an average increase in playing time of 100 per cent. Speech recordings would probably allow a greater increase in playing time than would musical performances.

M. L. T.

Manufacturers' Products

New Equipment and Accessories for Radio and Electronics

Miniature Three-Range Coil Pack

A THREE-RANGE coil pack measuring $2\frac{1}{2}$ in \times $2\frac{3}{4}$ in \times $1\frac{1}{8}$ in and intended for use in small superheterodynes without r.f. stage has been introduced by British Distributing Co., 66, High Street, London, N.8. When tuned by 0.0005-mfd capacitors the three ranges available are: 16 to 50m, 190 to 550m and 1,000 to 2,000m respectively.

The six coils have dust-iron cores. The pack is inductance-trimmed in the factory, and the only adjustments needed after its assembly in a receiver will be to the six trimmer capacitors accessibly mounted on top of the unit. With the single hole fixing and simple wiring, assembly takes only a few minutes. It is designed for an i.f. of 465kc/s. The Bridisco sub-miniature coil pack is priced at 30s 6d.

Quality Amplifiers

A RANGE of quality amplifiers costing approximately £1 per watt has been introduced by the Broadcast and Acoustic Equipment Company, Tombland, Norwich. Resistance-capacity coupling is employed with a paraphase-coupled push-pull output stage.

In the 12-watt amplifier, 6V6 or 6L6 valves are used in the output stage and a 120mV input is required for full output. Feedback is applied over three loops, and the response is flat within 2½ db between 20c/s and 15kc/s. Variable

bass and treble boost is included with maximum lifts of 20db. The price is £12 10s, or £8 10s without power pack.

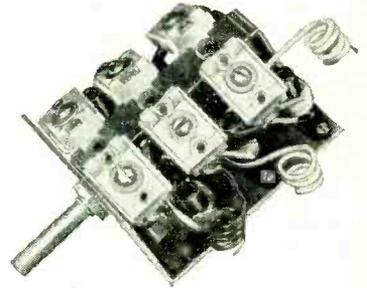
The 15-watt model has 6L6 or 807 output valves and the overall sensitivity is higher, being suitable for use with a microphone or photocell. The frequency range is 40c/s to 20kc/s within 1.8db. Bass and treble tone controls are included and the price is £15 10s or £10 10s without power pack.

Breeze Plug and Socket for heavy-duty applications has two 100-amp pins and one 19-amp pilot pin, in a brass housing that is waterproof when screwed together. All three socket inserts and the two 100-amp pins can be removed for soldering. The makers are The Plessey Company, Ltd., of Ilford, Essex.

High-Voltage Adaptor, Model 341, has been introduced by Taylor Electrical Instruments Ltd., 419-424 Montrose Avenue, Slough, Bucks, to extend the voltage range of their Model 170A Electric Testmeter up to 10kV.

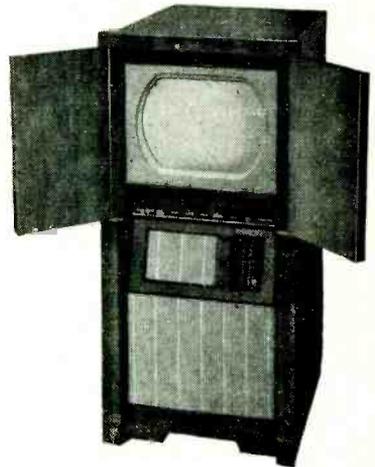
Television Receivers. Suitable for viewing in normal room lighting is the 600A table model projection television receiver produced by Philips Electrical, Ltd., of Century House, Shaftesbury Avenue, W.C.2. It has a flat screen measuring $13\frac{3}{4}$ in \times $10\frac{1}{2}$ in with lenticular rulings on the black face to give a wide horizontal angle of view, and is fitted with safety devices to prevent damage to the projection tube should either of the deflecting circuits fail. In a walnut cabinet, the set costs £91 9s 8d with a table-stand or £88 14s 6d without.

Ferranti, Ltd., of Hollinwood, Lancs, have introduced a new range of sets by adding to their console



Bridisco sub-miniature coil pack.

Ferranti Model T1505 combined radio and television receiver, with self-contained radio aerials.



receiver T1205 two more 12-in models, the T1405 table model, and the T1505 combined radio and television receiver. There will be two versions of each model available, and Ferranti will incorporate converter units, free of charge, in all Sutton Coldfield models which may have to be converted as a result of the forthcoming opening of the Holme Moss transmitter.

Two-speed Gram Motor. Coinciding with the recent offer to the public of long-playing records, Small Electric Motors, Ltd., Eagle Works, Churchfields Road, Beckenham, Kent, have produced a two-speed gramophone motor operating at 78 and $33\frac{1}{2}$ r.p.m. The complete motor assembly, which is of the rim drive type, is compact and suitable for mounting direct on to a metal or wooden baseboard. Although at the moment the standard unit is for use only on 50-c/s a.c. mains, a 60-c/s unit can be offered for the export market.



12-watt gramophone amplifier (Broadcast and Acoustic Equipment). The underside shows a simplified sub-assembly for coupling components.

UNBIASED

By FREE GRID

Radio and Road Hogs

RECENTLY I was telling you about a small radio transmitter installed in my car which, without infringing the law, enables me, a mile or so from home, to flood the house with light, warmth, music and the smell of sizzling kippers.

A reader who signs himself "Autophile," which, on the face of it, sounds like another name for Narcissus but probably means a car lover, has written to tell me that there is a far more necessary use for a short-range e.h.f. car transmitter than pandering to the soul-destroying sybaritism in which I indulge. He is apparently troubled by the number of inexperienced drivers and experienced road hogs who hurtle along dark country roads at night with dazzling headlamps which they haven't, respectively, the savvy or the courtesy to dip when passing other road users; in fact, according to him, night driving has become a regular battle of headlights. I cannot confirm or deny his words from my own experience as I am at the present time far too engrossed in trying to navigate my car solely by

radio beam from an approaching car was picked up by a simple fixed-frequency receiver which would operate the necessary switch by a relay.

Time Gentlemen, Please

NATIONALIZATION of coal is a burning topic, but, being politically controversial, is naturally barred, together with discussions of other nationalization matters, from the pages of *Wireless World*. I do think, however, that the Editor may make an exception when I call attention to the shameless manner in which the Government's own servants are deliberately sabotaging its most cherished monopolies. I refer to Time, which has had the offices of its control board at Greenwich since vesting day. Wireless, and in particular the B.B.C., has made us all conscious of the boon and blessing of this particular piece of nationalization.

Yet one need only go into any nationalized railway refreshment room to see B.P.T. (British Pub Time) still rigidly observed and the Government's wishes flouted by its

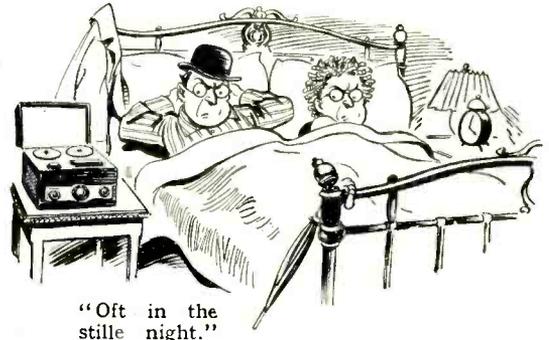
of the self-contained type using a magnetic wire or tape from which the programme can be easily and quickly wiped out when desired. I have for a long time used a home-made one of this type and I make a regular habit of recording certain B.B.C. programmes just for the pleasure of wiping them out without listening to them.

However, as I have said on a previous occasion, the real function of these instruments, in my opinion, is to record programmes which we cannot otherwise hear. Next year during the Festival of Britain when, as we have all been bidden, we are devoting all our energies to enlightening the overseas visitors on "this realm, this England," we shall have still less time to listen. We shall, in fact, have to bottle not only the B.B.C.'s day-time programmes but the evening ones as well for consumption in what we shall with literal truth be able, with apologies to Thomas Hood, to call "The Stille Night."

It is possible, of course, to bottle any programme at will by means of an ordinary receiver, a time switch and a recording unit. We can, in



Night driving difficulties.



"Oft in the stille night."

its radar screen and accordingly I leave lighting and all such matters to Mrs. Free Grid, but possibly my correspondent's information explains the presence of the ex-A.A. searchlight that I notice has recently been mounted on the car roof.

Briefly, my correspondent's idea is that headlamps should all be made illegal and the latest type of overhead lighting installed on all roads throughout the land, the capital cost being met partly by the money saved by not manufacturing headlamps and partly by one of the Chancellor of the Exchequer's once-for-all levies. Running costs, represented chiefly by the huge current consumption, could be virtually wiped out by using radio since the lights on any particular furlong of road would not come on until a

own lackeys who fling thirsty electors out on to the cold hard platform five minutes before the legally appointed time. This five-minutes-fast rule must irritate teetotallers also, for after gulping down Government tea and the very aptly named rock cakes, they rush out on to the platform only to find to their chagrin that they have plenty of time to get sedately into the third-class accommodation for which they have paid instead of flinging open the door of a moving first-class compartment and collapsing breathlessly into its cushioned comfort.

Home-bottled Programmes

I AM glad to see that more and more home recorders are coming on to the market, especially those

fact, select and bottle all our listening for a week ahead for consumption at our leisure. I am able, by this means, to keep a car full of guests cheerful and free from the vice of backseat driving when rolling home in the small hours long after the B.B.C. has closed down.

I have little doubt that by doing this I am not only infringing copyrights galore but also transgressing against the rights of innumerable recording companies; I trust they will all send along the necessary writs to the Editor who will accept service on my behalf. I can only think that it is this question of copyright and recording rights that prevents manufacturers putting forward an all-in-one receiver-cum-automatic recording unit. Can some of you legal luminaries enlighten me?

LETTERS TO THE EDITOR

The Editor does not necessarily endorse the opinions expressed by his correspondents.

Resistor Colour-coding

IS it not time that the manufacturers of colour-coded resistors made up their minds as to the meanings of the colours? There is great confusion between Black for Nought and Brown for One—I have before me two resistors with orange body and tip, and brown spot; on a bridge they are 33 ohms and 330 ohms respectively! Green Black Black is shown on the bridge to be 50 ohms—how would 5 ohms be marked, then? Among a batch of 50,000-ohm resistors, the honours are about even between Black and Brown for the tip colour. Surely, if Black means Nought, when it appears as body or tip it must mean *Not Even a Nought* (a simple explanation becomes a little Irish, but you must see what I mean).

Worse is to come—with certain high-stability resistors a fourth stripe appears for the tolerance and bears its correct colour (in place of the familiar gold and silver of the humdrum resistor). Some resistors have a black moulded body; here is one with brown tip and yellow spot; it measures 100,000 ohms, using the body colour for the initial ONE. But here is one with black body and two red stripes; it measures 2,200 ohms, showing that this time the black body forms either the intermediate or final colour, according to taste; finally, a brown moulded body with three stripes, Red Red Brown; this measures 220 ohms, showing that the body colour is now disregarded—you have my sympathy if you thought that this was a 1,200-ohm 1 per cent resistor.

No wonder one manufacturer takes no chances and places round his colour-coded product a label bearing the value in clearly printed figures!

PETER D. DAW.

London, S.E.1.

Stereophonic Broadcasting

IN your issue of September, 1950, I read an article about improved stereophony in which E. Aisberg started his article with the following words:

"The first broadcast of stereophony, the system in which sources of sound are restored to their relative positions in space, took place in France on June 19th, 1950."

Although I understand the feeling of stating something new, in this

case there is a *deus ex machina* in Holland.

On June 15th, 1946, there was a stereophonic transmission with a specially constructed artificial head, equipped with two condenser microphones, that broadcasted a concert given by the Dutch Radio-Philharmonic Orchestra.

Also the manifold publications of our industry—Philips, Eindhoven, about stereophony (Dr. K. de Boer), were not mentioned at all in this publication.

J. J. GELUK,

Netherlands Broadcasting Union,
Hilversum, Holland.

THE article by E. Aisberg in your September number was of considerable interest to me, having had experience of an opposite problem during the earlier stages of the late war with acoustic locational apparatus for aircraft.

In his seventh paragraph he mentions the differential intensity of sound being responsible for the binaural effect. Although the intensity effect exists over short periods with human ears, it was always my experience that it was the phase differential aspect which predominated in any locational exercise or practice. To be equipped with tubes and receiving horns extending the aural sound base from 6in to 8ft and to centre these upon a stationary sound source produced a remarkable effect in that the nodal point of no phase difference travelled recognisably round the back of the cranium. This, of course, operated in one plane only for one "listener."

For perfection we will need a wall in which are positioned 5 loudspeakers (the middle one to take up slack) and two listeners, one sitting normally to recognize what is going on in the horizontal plane, and one prone to follow the vertical movements of those who climb staircases or rise upon piano wire, or to hear, for example, the gravitational descent of "Les Larmes du Diable."

M. F. L. FALKNER.

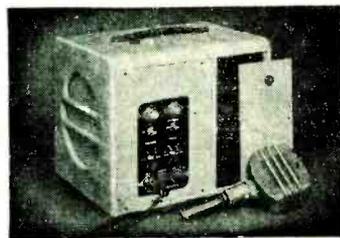
Holmes Chapel, Cheshire.

YOUR contributor's account (September issue, page 327) of the recent French broadcast over two channels does not, to my way of thinking, make a clear enough distinction between true binaural stereophony (in which two microphones mounted in an artificial head

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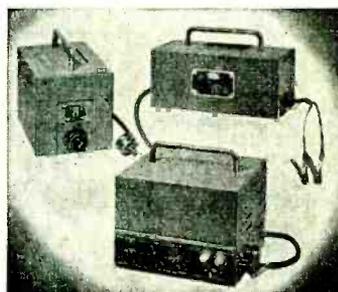


Portable Model B 65 (open)

Can you provide a public address system at a moment's notice? With a B65 it is simple—just place the equipment in a suitable position and switch on. Incorporated within an easily portable case are the amplifier complete with loudspeaker, rotary transformer, 6-volt unspillable accumulator and microphone with cable. Power output is approximately 5 watts. The equipment is a most useful outfit for political meetings, religious gatherings, auctioneers, etc., and numerous other applications where no electric supply mains are available.

Price complete £32 10 0

An external speaker can be attached if desired.



Portable Battery Mains Amplifier B 69

Operates on 12-volt battery or by means of separate plug-in adaptor unit, on A.C. mains. Power output approximately 16 watts.

Full details of these models and others in the large Trix range of equipment available on request.

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AMPLIFIERS · MICROPHONES · LOUDSPEAKERS

are used at the source, and headphones are used at the receiving end) and other systems which simulate directional effects.

Neither is it true to say that the appreciation of acoustic *depth* is essentially a product of binaural hearing. Distance between sound source and microphone in a studio is readily judged in a single-channel system by the ratio of direct to reverberant sound. The inclusion of a reverberation chamber in the system described suggests that the designers are well aware of these facts, and, together with two-channel control of volume, they have placed at the disposal of producers a versatile medium of expression. I believe that Bernhart and Garrett describe their work as "directed" stereophony, which seems a happy phrase. HENRY MORGAN.

Hindhead.

WITH reference to the article in the September *Wireless World*, I note that there is no reference to the effect of phase displacement in the location of a source of sound.

I had understood that whereas amplitude formed the chief discriminating factor in the case of the high notes, phase discrimination was important in the lower register where amplitude differences are less marked.

(This is physiologically possible since at low frequency the nerve impulses are synchronous with the sound waves. Note that this does not involve phase discrimination between waves of different frequency.)

If this is so Fig. 1 (a and b at least) will preserve the original phase relations intact, provided the channels are balanced, but Fig. 2 ought to introduce a certain amount of distortion unless the faders can be made to introduce the correct phase displacement, a problem of no small magnitude in an electrical circuit.

H. R. A. TOWNSEND.
South Cerney, Glos.

Hint to Manufacturers

WHEN buying a television set its position in the home should be in a room different from that in which a wireless set is kept. This is obviously desirable when only one wireless set is available, as a member of a family may well wish to hear a particular sound programme during television transmitting hours. It is also desirable in these days of flats and small rooms which quickly tend to become overcrowded. At the same time sound broadcasting is sometimes required in the room used for tele-

vision. The answer, of course, is an extension speaker, but this not only adds to the overcrowding, but is an additional expense. In the television set, however, there is a loudspeaker which is idle for a large part of the day. May it be suggested to television manufacturers that a simple switching apparatus be incorporated in television sets (other than combined sound models, of course) so that the speaker may be used as an extension speaker from a wireless set. The speaker could be wired for use when the television set is installed. D. R. BRAY.

London, N.22.

Raising E.H.T. Voltage

I FEEL the greatly improved brightness and focus of modern receivers is due to using voltages of 6 to 10kV whereas it was quite common in older types of receiver to use from 3 to 4kV.

The obvious method of changing the e.h.t. transformer for one of higher voltage might be considered too costly in an old receiver. The only alternative is to use line flyback e.h.t. but it will usually be found that the line output transformer is unsuitable for this purpose and with a simple half-wave system would only provide about 2 to 3kV. But if this voltage could be added to the existing system the e.h.t. could then be 6 to 7kV or more. Unfortunately, however, the straightforward connection of a rectifier and condenser would not work as the cathode of the rectifier would be at a higher positive potential than the flyback pulse feeding the anode. The best way of adding the voltages is as shown in my diagram. This circuit might seem a bit puzzling until it is realized that the extra components V_2, C_2, R are really the top half components of the usual voltage doubler system sometimes used in flyback e.h.t. systems.

During the forward scan C_2 will be charged up through R to the same potential as C_1 . When the

flyback pulse comes along these two voltages will be added and will be applied to the anode of V_2 , thereby charging C_3 and C_1 to the combined voltage. So therefore with the simple addition of two condensers, a resistor, and a rectifier, almost double the e.h.t. voltage could be obtained. This would naturally mean that increased scanning power would be required and whether this is within the capability of the set is another matter, although I have found this just possible in most cases.

It would be rather more difficult using the voltage doubler system with the existing mains transformer as one side is usually earthed and must remain so. In any case, much larger capacitors would be required whereas with the above method C_2 and C_3 need only be 0.0003 μF ; R is 2 M Ω .

It would be better to use a metal rectifier for V_2 and no heater voltage would then be required.

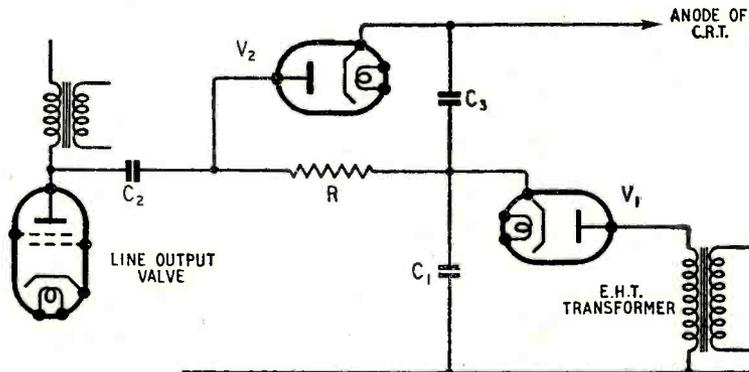
L. J. HILLS.

Belvedere, Kent.

American Insularity

HAVING read with interest the correspondence on the above subject in your journal, I felt it would be interesting to analyse the footnotes and references in a typical American publication. This I have done for the excellent collection of articles entitled "Electronics Manual for Radio Engineers" (Zeluff and Markus; Pub. McGraw-Hill). This book contains 872 pages of text, covering 289 "all-time-great articles" from *Electronics* 1940-48.

The total numbers of separate references are as follows: American, 466; British, 38; others (mainly German), 14; (A few references are of doubtful origin and may have been added to the wrong list). Of the 38 British references, 6 are to O. S. Puckle's "Time Bases," 5 to *Wireless World* and 3 to *Electronic Engineering*, leaving a paltry 24 to



represent the remainder of British brains.

A further analysis shows that of 77 pages of microwaves (did we do any radar work in this country?) there are 3 British references, and of 75 pages on television, only 1! In an article on the "Phantastron," although it is admitted that the circuit originated at T.R.E., there are no British references and 3 American references.

It is important to realize that these figures are not taken from one isolated case, but represent the attitude of 270 different authors to the efforts of workers outside their own country.

Although I have not made a similar count in any British publications, a quick check through 3 copies of *Wireless World* and 3 of *Electronic Engineering* shows that more than 50 per cent of references are to American literature.

A. T. COLBECK.

Talgarth, Brecon.

Names and Titles

AS an "old timer" in the world of wireless I have been giving some thought to nomenclature and titles.

The first refers to v.h.f. radio-telephony between private vehicles, tugs and the like, offices, etc., with, at present, the unwieldy designation of "Business Radio." It is extraordinary how difficult it is to arrive at a suitable name covering this application of the art. Of course there is R/T, but this encroaches upon service terminology and in any case is still not a word. RADIO-PHONY appears to cover it, but it would be interesting to have opinions of your many readers.

My second search has been for a suitable title covering the 1951 Radio Exhibition, observing it cannot be held at Olympia. RADIO-SHOW is what it is, but RADIO-BRITAIN seems to cover the special occasion. Again, what do your readers think?

H. ANTHONY HANKEY.

London, W.4.

"Television In Your Home," a new booklet written for the layman by W. E. Miller in clear non-technical language, provides all the information a viewer needs to know before and after purchasing a receiver. The confirmed televiewer also will find here answers to some of the questions which may have cropped up during his viewing experience. After describing the television service and sketching the basic principles of television, the booklet gives useful advice on the choice, installation and correct operation of a receiver, and ends with a comprehensive list of questions and answers. Copies can be obtained from all bookstalls, price 2s, or direct from our Publishers, price 2s 2d.

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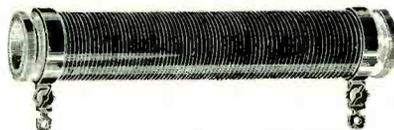
6W Size, 1½" × 1½" φ



10W Size, 1¾" × 1½" φ

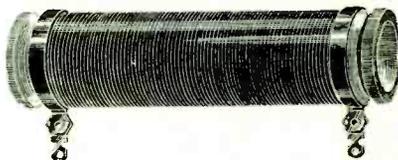
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RANDOM RADIATIONS

By "DIALLIST"

Big Tube or Projection ?

INTERESTING TO NOTICE that television receivers seem to be developing along quite different lines in this country and in the United States. Viewers in both countries want big images: here the tendency is to provide them by projection methods; on the other side of the Pond they are all in favour of the monster c.r.t. I don't know of any model amongst this year's British receivers with a tube bigger than 15 inches, nor are there many such; but in America there are quite a few with 19-inch tubes and for all I know some may use even larger ones. One reason, I suppose, for our different approaches to the problem of the big image is that America, with an output that runs into quasi-astronomical figures, can turn out c.r.t.s a good deal more cheaply than we can. We, on the other hand, seem to have advanced rather further in the technique of making reasonably long-lived, small, super-brilliant projection-type tubes.

Direct Comparison

Not all comparisons are odious, despite the old saying. I recently had the opportunity of making one that can't have been possible to any vast number of people, and, far from being odious, it was surprisingly interesting and instructive. Briefly, I watched the simultaneous display of a whole television programme by projection and big-tube methods. The images were of the same size—about 16 by 12 inches—and the two screens were side by side. The big tube was provided with optional spot-wobble; that is, the "spot-wobbulator" could be switched on or off at will. The first thing to strike one was that, even at short range, no lininess was apparent in the projected image, though it was very much in evidence in that on the large tube when the spot-wobble was not applied. The reason, presumably, is that in small high-voltage tubes one cannot obtain a focus that is relatively as sharp as that of a high quality tube of large diameter. In other words, the spot on the small tube has sufficient spread to cover up the effects of lininess. One might expect this to lead to a rather

poorly-defined image; but I cannot honestly say that it had this effect. My general impression was that though the projected image might be a little lacking in depth when directly compared with the other, it was distinctly more pleasing (and less tiring) to the eyes than an un-wobbled image on the big c.r.t.

Passing Thought

It must be no mean job to design and manufacture very large cathode-ray tubes. It wouldn't be so bad if the business end could have a pronounced convex curve, for this would have a much better chance of standing up to the strains resulting from a vacuum within and an outside atmospheric pressure of getting on for 15 lb to the square inch, but the end of the television c.r.t. must be as nearly flat as possible. Take a 20-inch tube to make calculations nice and easy, and you have a surface area for the screen of 314 square inches. That multiplied by 14.5 gives a total air pressure on the screen of 4,553 lb, or a little over 2 tons—the combined weight of 32 average men and women.

Nomenclature

SOMEHOW, I am not attracted by F. B. Rudd's suggestion in the September *Wireless World* that what we now know as the intermediate frequency should be styled henceforward the resultant frequency. For one thing, you could not abbreviate it to r.f., for that is already in use for radio frequency. Our frequency designations are a pretty bad muddle, anyhow. The main reason is that so many of the terms are used sometimes with a relative and sometimes with an absolute meaning. What, for instance, is a high frequency or a low frequency? Glance through disquisitions by various writers on the amplification problems in different parts of the receiving set and you will see what I am driving at. Myself, I would like to see a standardization on the following lines. Let the three main classes of frequency met with in a receiver be named respectively signal, intermediate and audio frequencies—s.f., i.f., and a.f.; divide each of these into three degrees:

upper, middle and lower. All the three class terms are relative, for s.f.s may be anything from a few kilocycles to thousands of megacycles, i.f.s have a smaller but similar possible range and a.f.s run from frequencies below the limits of human hearing to those a long way above those limits, but, as applied to the receiving set they are perfectly clear.

Still They Come

THERE CAN BE no doubt that television has caught on as a national hobby. By the time that this is printed the number of licences will probably have passed the half-million mark, which means that, despite raw material shortages and production difficulties, a very considerable proportion of the homes in which reception is possible will have television sets. Between them the London and Birmingham service areas have a population of some 18 millions. Allowing an average of four persons to each household gives a figure of 4.5 million homes in the areas. For one reason or another television reception is probably impossible in at least half-a-million of these. Hence, just about one home in every eight in which reception is possible now has the necessary equipment. What will the saturation figure be? Higher costs—initial, maintenance, running and replacement—will naturally make it much lower than the figure for sound broadcast receivers, which are now part of almost every home. For television I predict it will turn out to be somewhere between one home in four and one home in five.

Terminals

THE TERMINAL (*Americè*: binding post) as we know it to-day and have known it for umpteen years is definitely not a satisfactory electrical device. There are only two main types. In one of these a nut clamps the wire or wires to a non-moving base. In the other the base is again fixed, but the clamping is done by the point of a screw. The trouble in either case is that the moving part of the clamping system rotates and in so doing grinds, bruises and even cuts the wires. We're all only too familiar with defects due to the eventual breaking of wires—particularly flex—at the point of compression in the terminal. What is urgently wanted is a terminal in which a straight push, without any twisting action, is exercised on the wires.

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All owners of the "Avo" Valve Characteristic Meter who have returned the Registration Form supplied with the instrument will receive a copy of this publication free of charge. Future purchasers of the "Avo" Valve Characteristic Meter will receive their copy automatically. As, however, it also contains data and information for use with the original "Avo" Valve Tester and a comprehensive treatise on the technique of valve testing, it has been decided to make the book generally available at 15/- post free.



CORRECTION

In our advertisement in the September issue of "Wireless World", it was stated in error that the new "Avo" Valve Data Manual is being supplied free with the "Avo" Electronic Test-meter. The Book in question is, in fact, supplied free only with the "Avo" Valve Characteristic Meter.

FREE INFORMATION SERVICE:

An important feature is the **FREE INFORMATION SERVICE**, to the end of June, 1952, whereby supplementary data, to cover new valves as they are introduced, will be mailed from time to time. These supplementary items will be issued on perforated adhesive sheets so that they can be easily detached and inserted in the book in their correct alphabetical and numerical positions.

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Please send me a copy of the "Avo" Valve Testing Manual, for which I enclose P.O./Cheque 15/-

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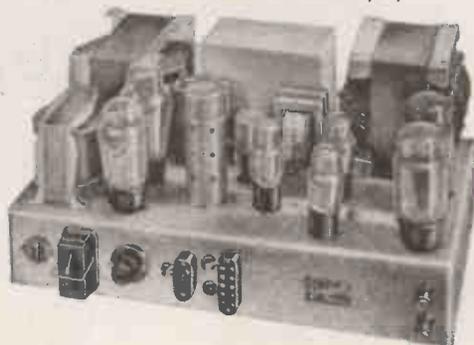
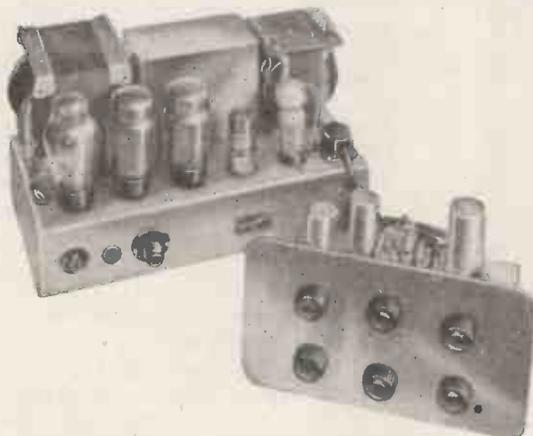
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Price £15/15/- . P. Tax £3/10/-.

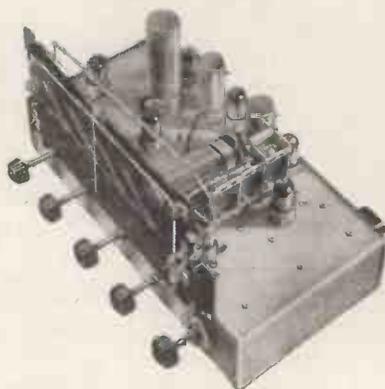
With wide range tone control, additional L.F. stage and extra 6dB per octave valve correction circuit on gram input only.

Suitable to drive Williamson amplifier.

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A.

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If, by sitting with your ear in a loudspeaker fed from an audio frequency oscillator, you hear something when the dial is set at 30 cps and something when it is set at 20,000 cps, then you can, presumably, with a semi-transparent, if not clear, conscience say

that the speaker has a response of 30-20,000 cps. Whether this information is of any

use or not depends upon whether you want the loudspeaker to listen to or talk

about. By these standards a poor loudspeaker looks as good on paper as a good one, which is why we try to refrain from sticking

our necks out and say as little about the performance of our speakers as possible.

When it comes to listening tests however, we find quite a lot of people choose our models, and

only a few refuse to believe their ears and insist on knowing what the speaker looks

like. If you *must* know, even our sceptical

ears can hear 30 and 15,000 cps signals on the Klipschorn Reproducer at a

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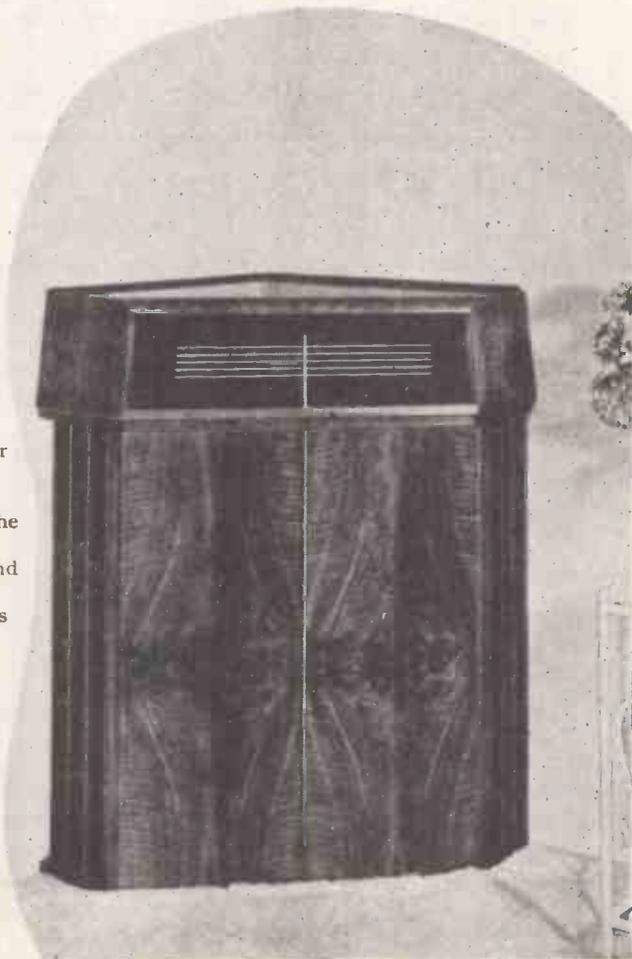
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The demand for "AERIALITE" Television Aerials increases daily—WHY? Simply because Aerialite are alive to the exacting requirements of an aerial under all conditions. Here are a few of the models from our wide range, all proved sellers.

MODEL 67 (Illustrated)

This model is another recent addition to the Aerialite range of TV aerials. It is easily adjustable to all channels and gives excellent results. It can be fixed to window-sills or adjacent brickwork and is fully proofed against climatic conditions. 27/6.

MODEL 55

This is the well-proved and popular Aerialite "H" array. It is robustly constructed, corrosion proofed inside and out and is supplied with a 10ft. x 2in. alloy mast which will withstand 100 m.p.h. gales. Model 55, 125/-.

Model 55X Aerial only, 65/-.



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Two new indoor models for skirting board of window fitting. The 65 has one telescopic and flexible section, whilst the 66 has two flexible sections. Each complete with five yards of coaxial* cable for receiver connection. The range of both these easily fitted aerials can exceed 20 miles. Model 65, 28/6. Model 66, 16/6.

* Models 65A and 66A. As above but supplied with balanced twin feeder. (Cat. 387).

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This aerial is intended for erecting in lofts and can be mounted in a variety of positions. It gives excellent results and requires only the connection of the cable for immediate operation. Price 25/-.

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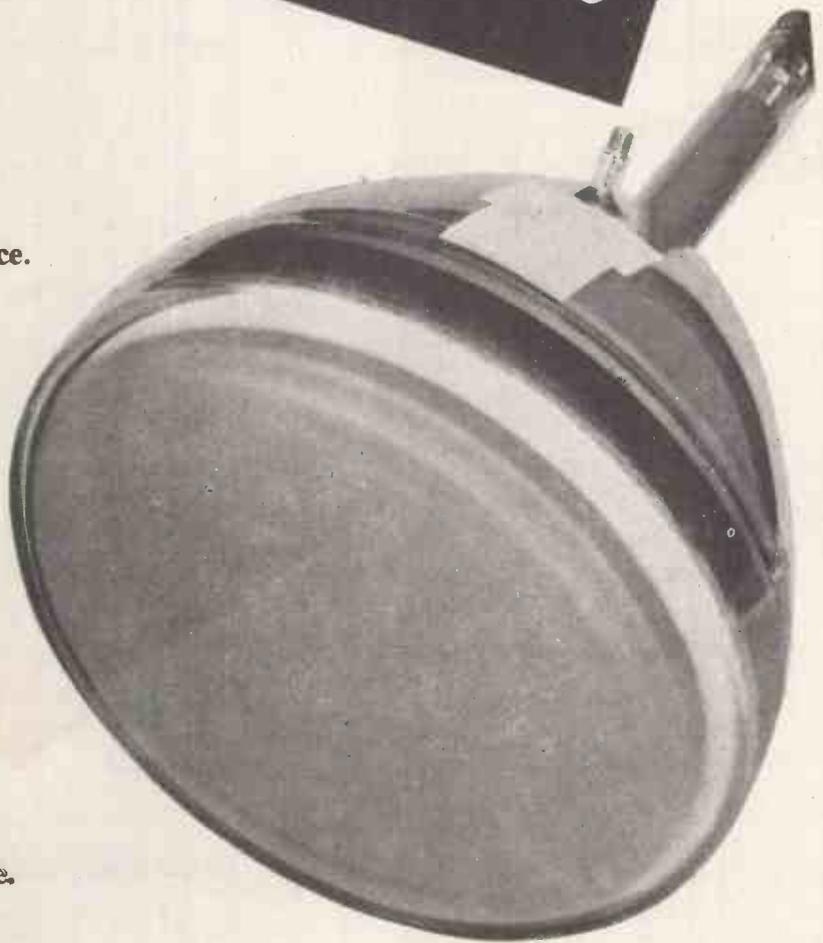
It has a specially flat face.

**It gives a bright,
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image.**

**Ferranti reliability
ensures long life.**

**It gives freedom
from ion burns.**

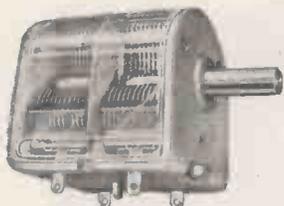
The price is reasonable.



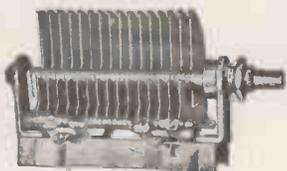
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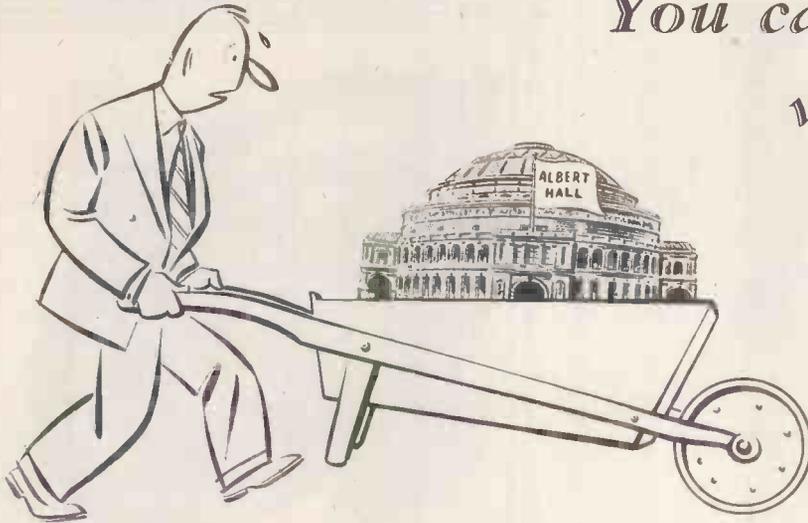


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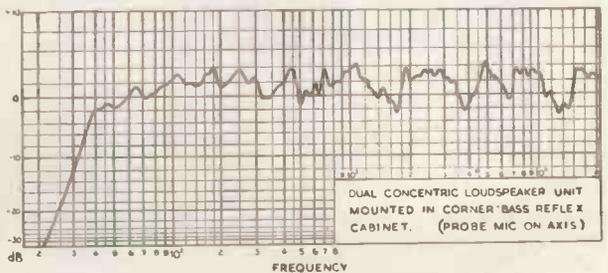
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This loudspeaker system is offered in the 15 inch size at £26.5.0. We will be glad to send full technical specifications on receipt of a postcard, or to arrange a demonstration in our showrooms at West Norwood.

Also available in 12 inch size at £19.0.0 complete with cross-over network on separate chassis. This speaker is identical in every way with the 15 inch model, except in size and power handling capacity.



15in. Dual Concentric Unit showing cross-over network.



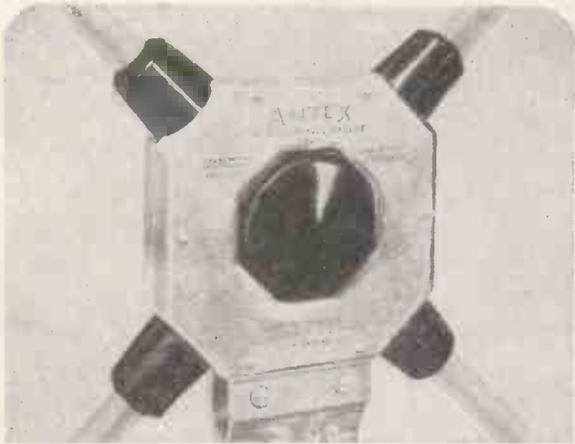
Frequency curve of 15in. unit.

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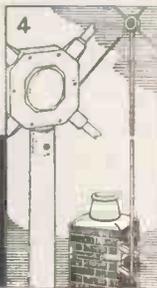
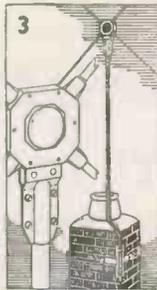
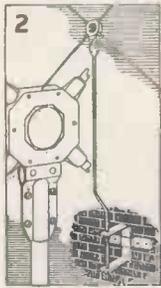
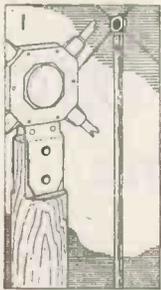
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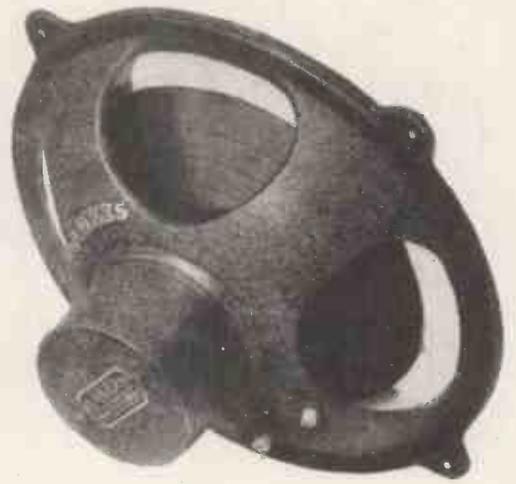
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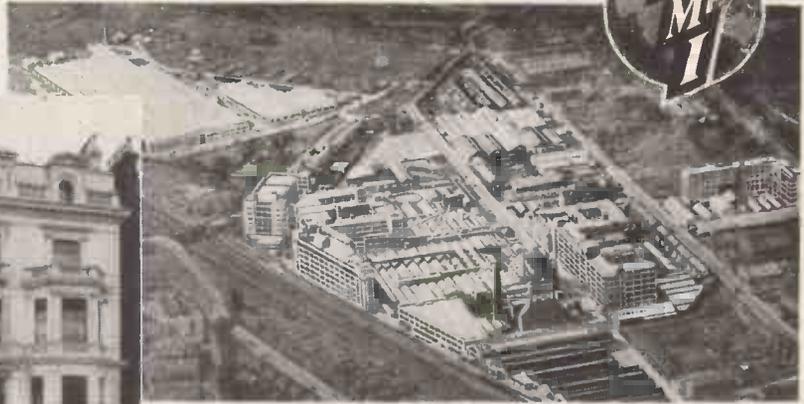
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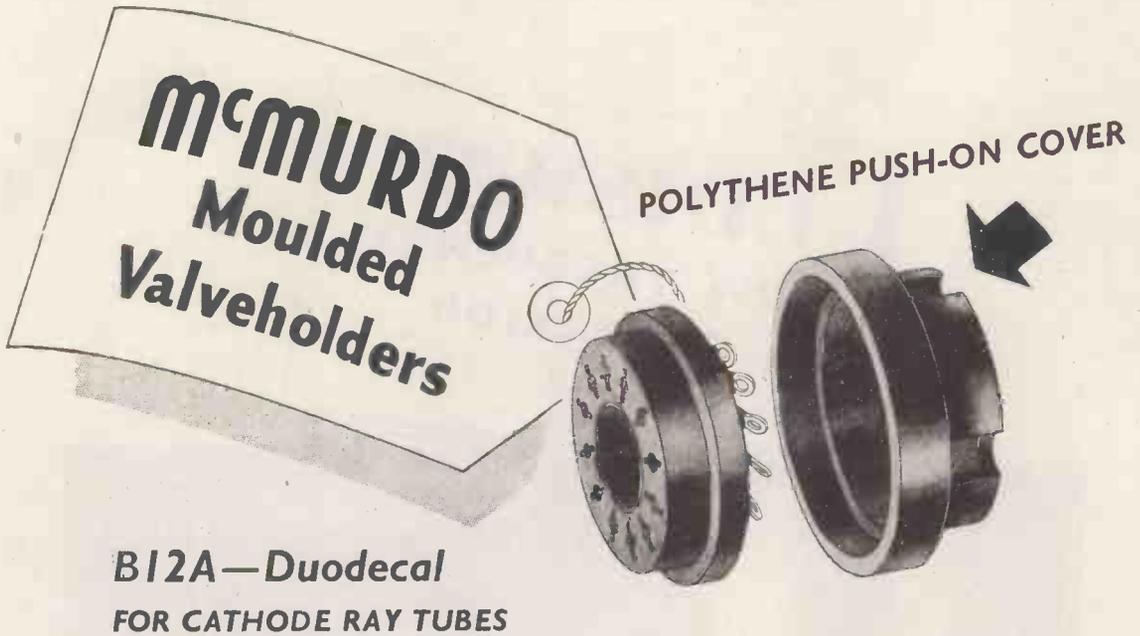
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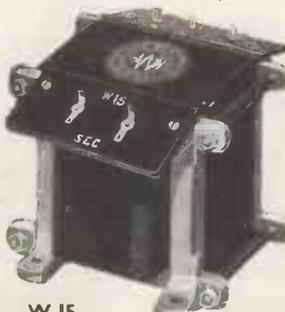
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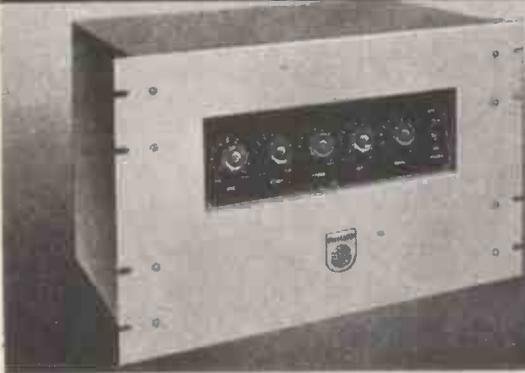
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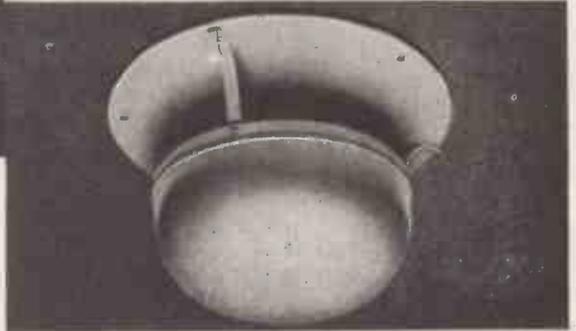


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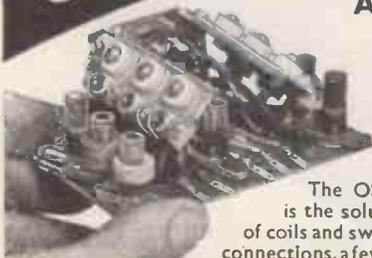
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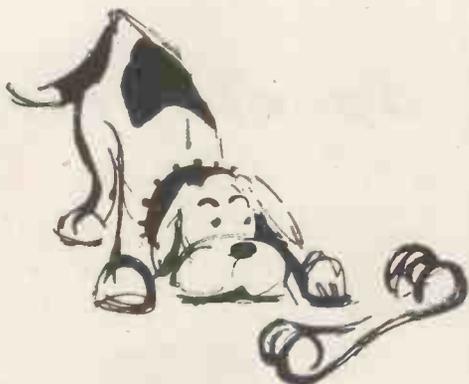
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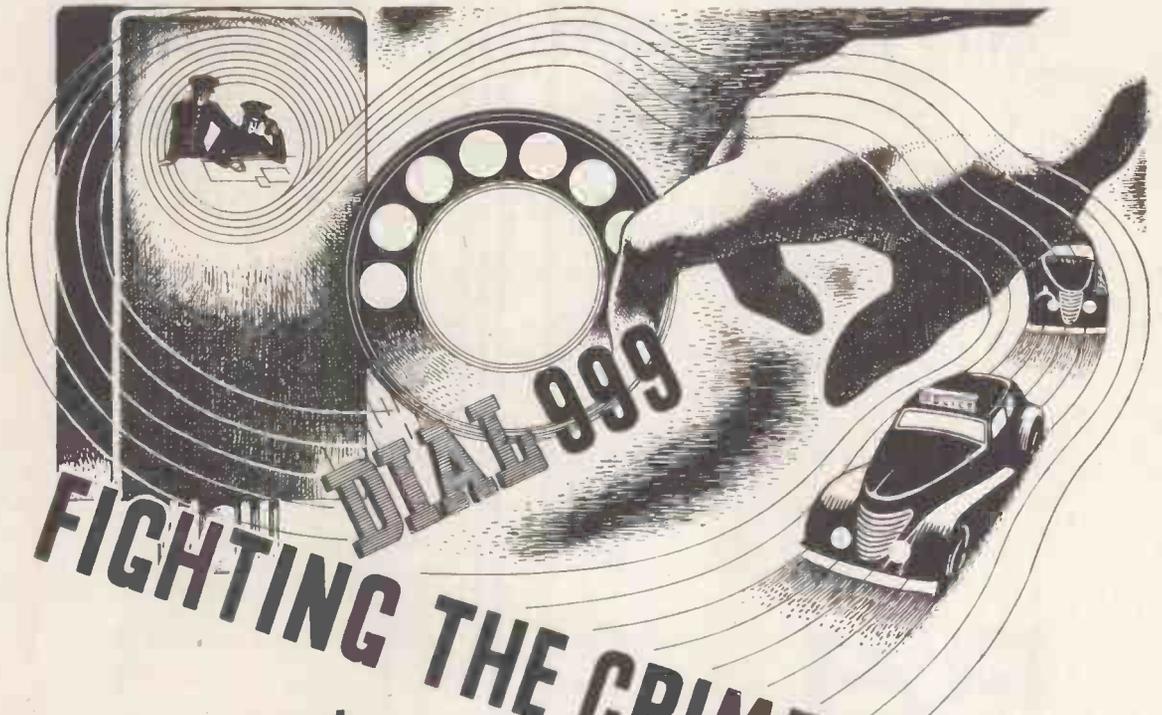
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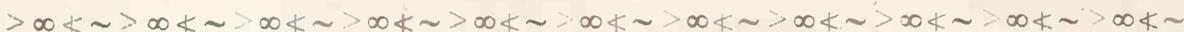
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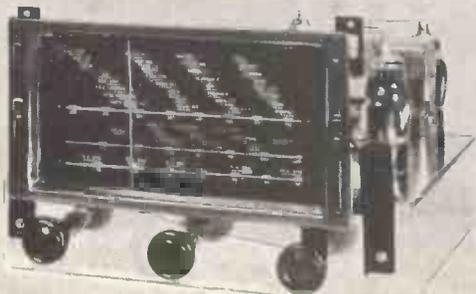
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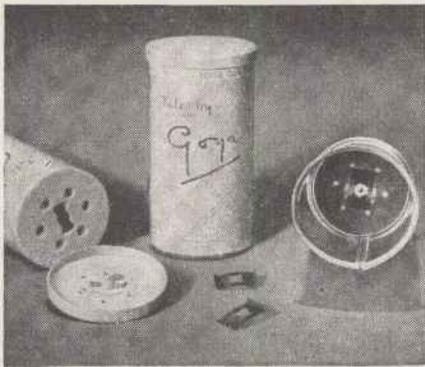
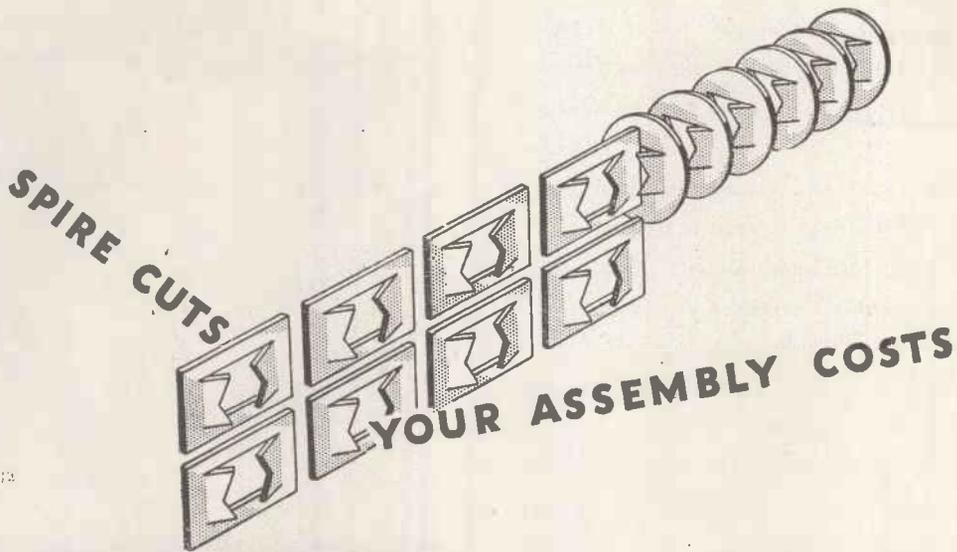
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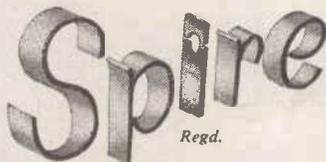
Secure top of talc container so that it can be rotated under spring tension for alignment of sifter holes.

SOLUTION:

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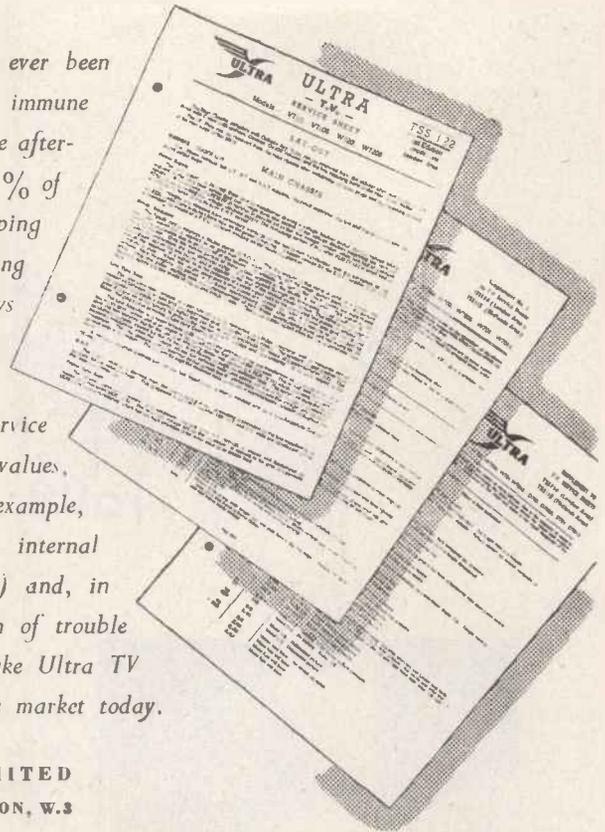
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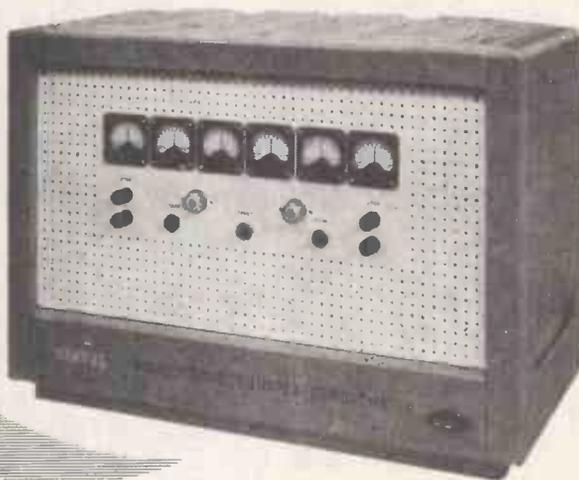
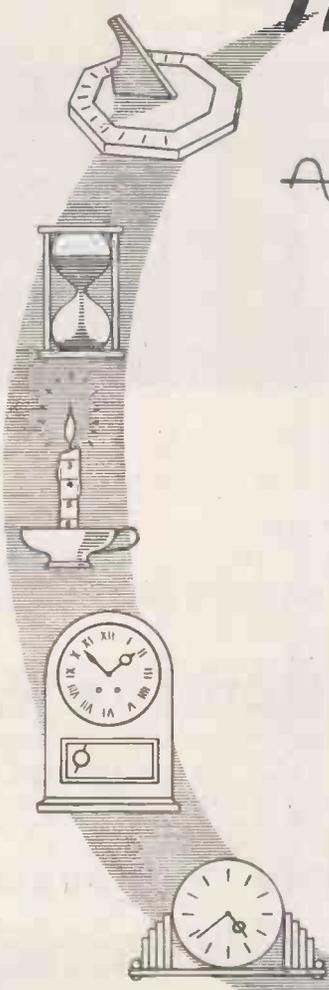


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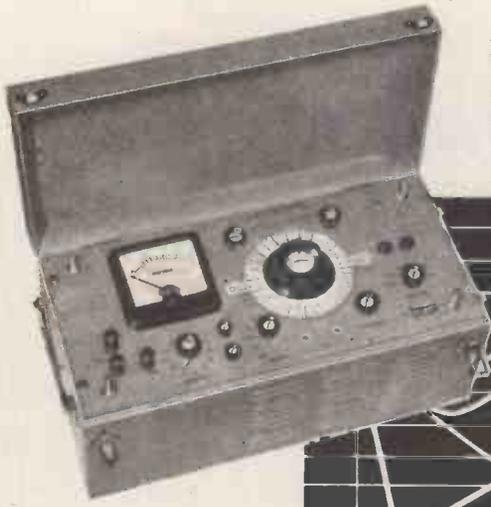
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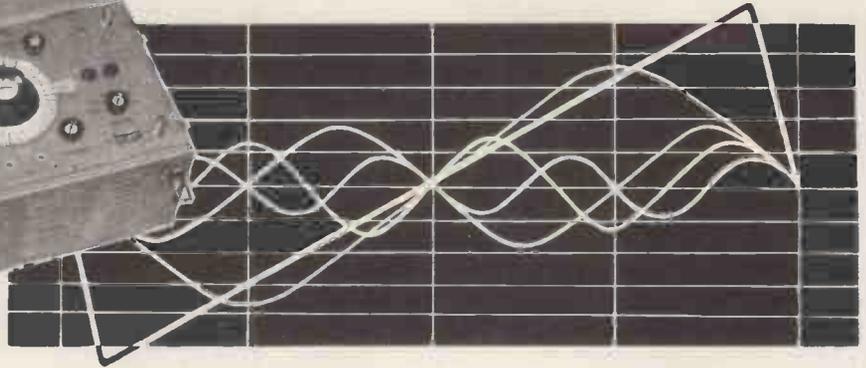


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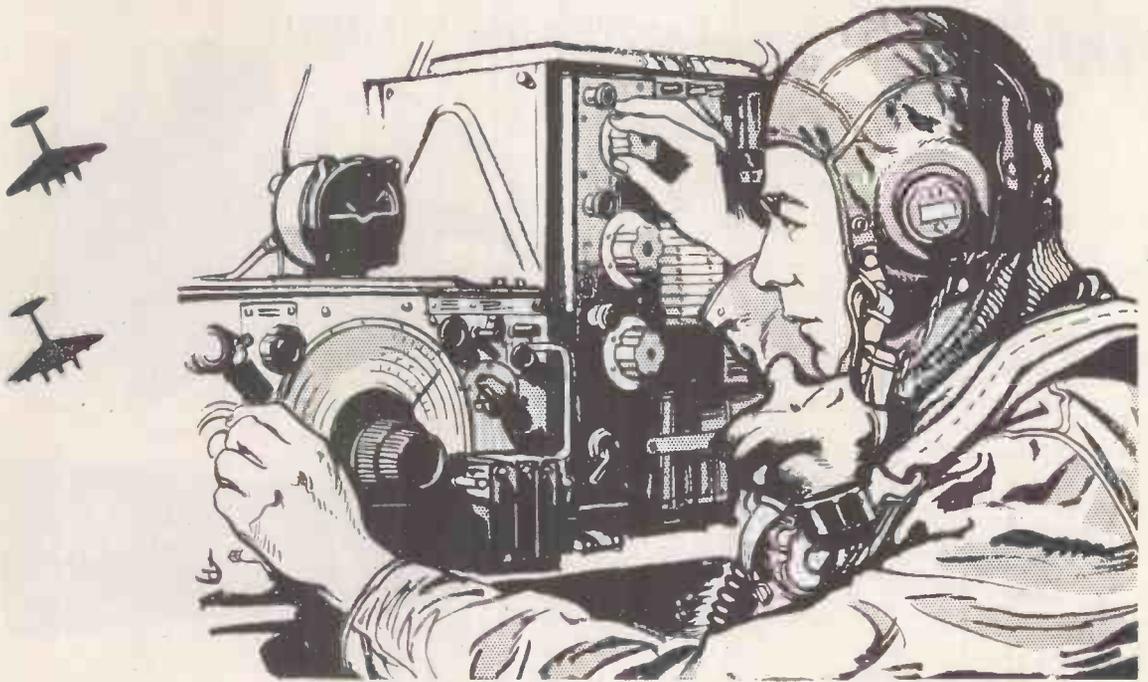
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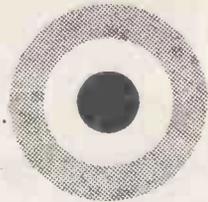
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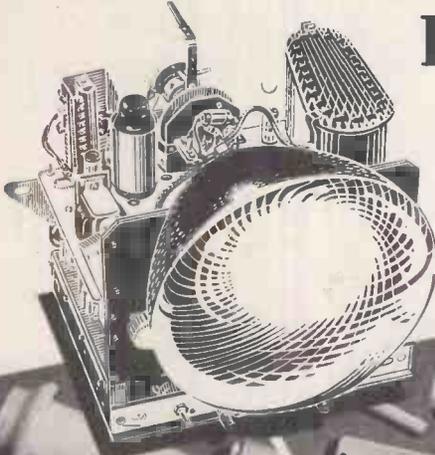
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FS160X. Output 350/0/350v. 160 m/a., 6·3v. 6 amps, 6·3v. 3 amps., 5v. 3 amps. Fully shrouded.....	37/6
FS43X. Output, 425/0/425v. 250 m/a. 6·3v. 6 amps. 6·3v. 6 amps. 5v. 3 amps. Fully shrouded.....	57/6
HS6. Output, 250/0/250v. 100 m/a. 6·3v. 6 amps. C.T. 5v. 3 amps. For receiver RI 355. Half shrouded.....	24/6
HS150. Output, 350/0/350v. 150 m/a. 6·3v. 3 amps. C.T. 5v. 3 amps. Half shrouded.....	25/9
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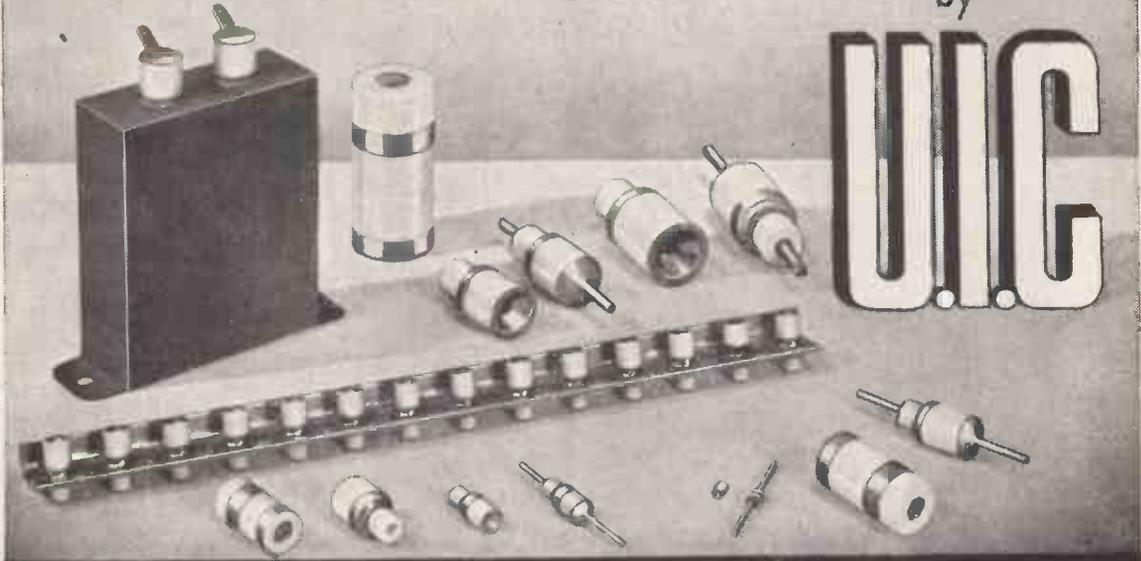
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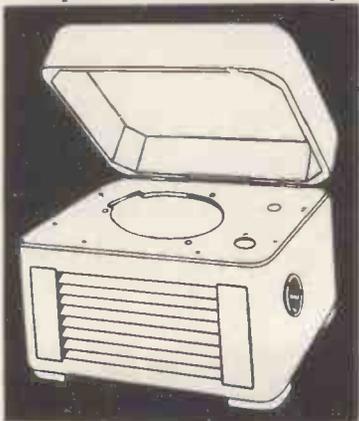
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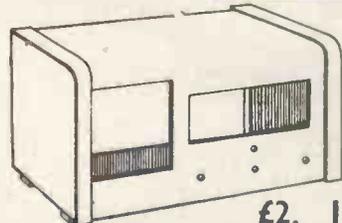
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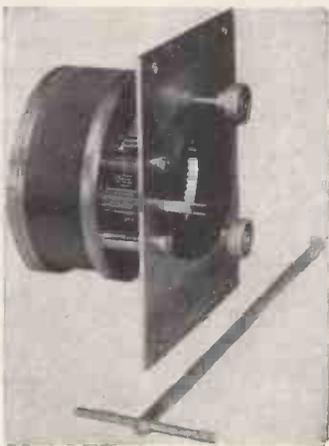
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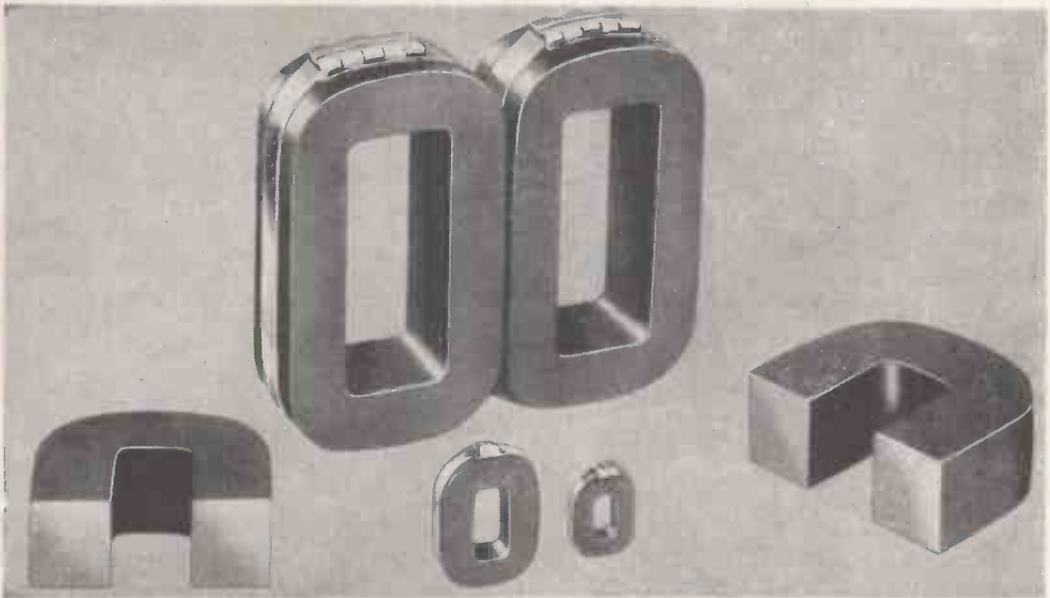
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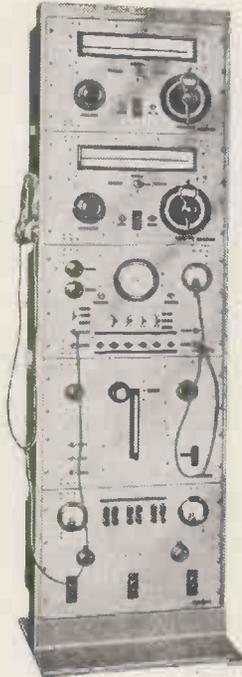
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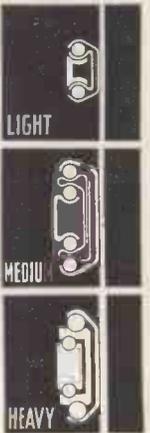
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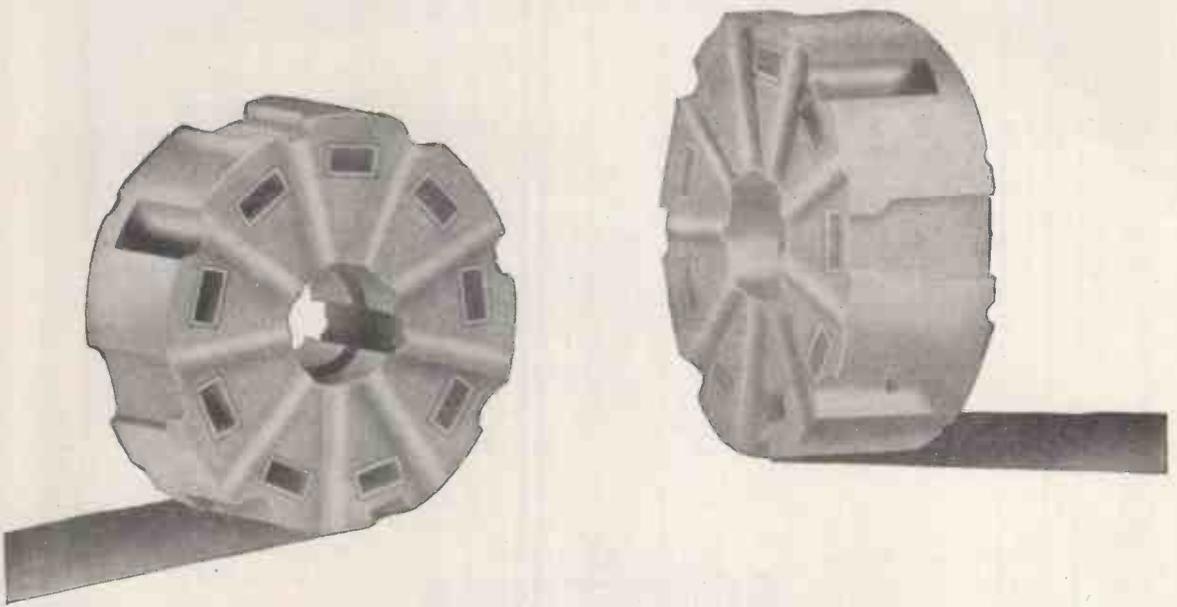


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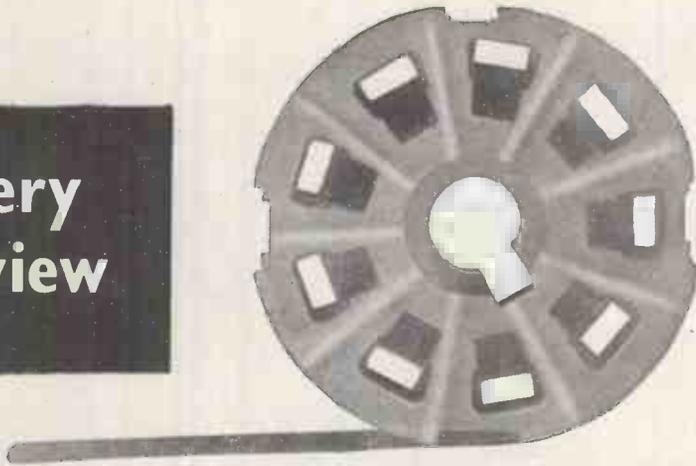
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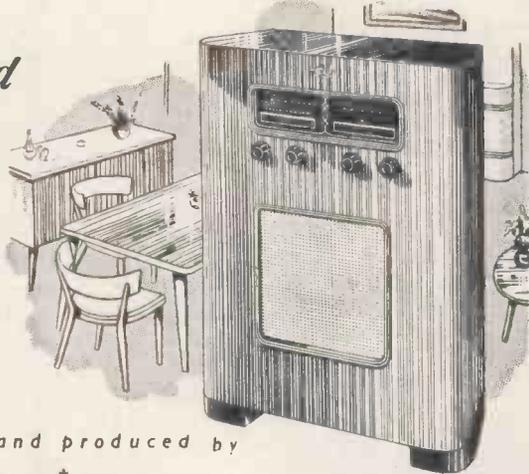
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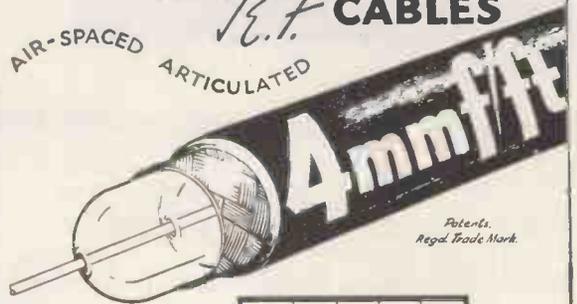
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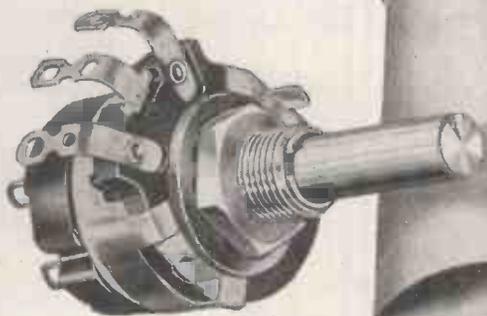
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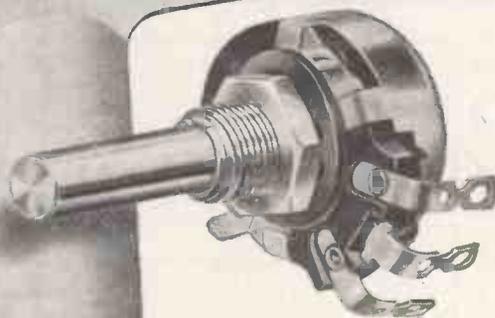
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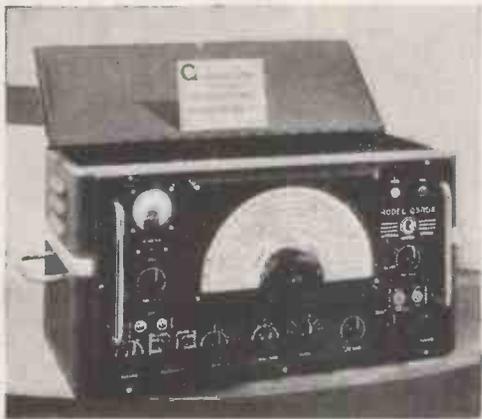
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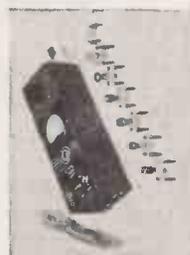
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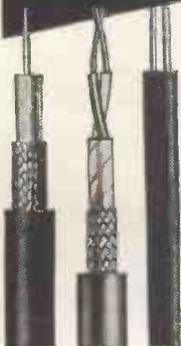
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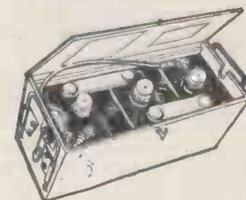


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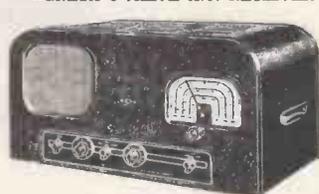
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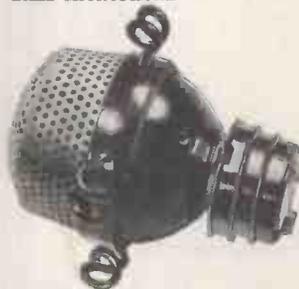
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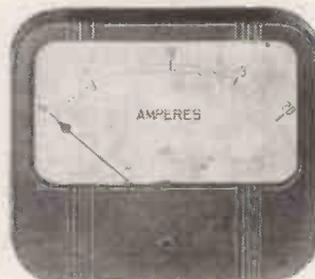
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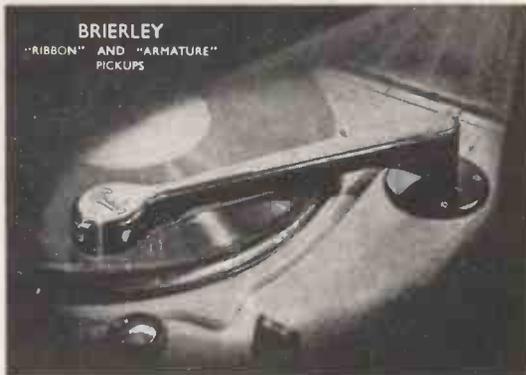


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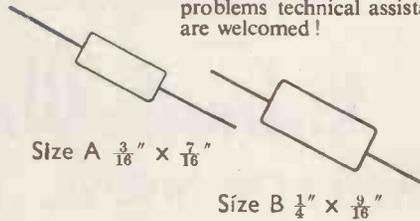


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		B
350 D.C.	0.001 to 0.003	A
		B
600 D.C.	2.5 μ F to 0.0005	A
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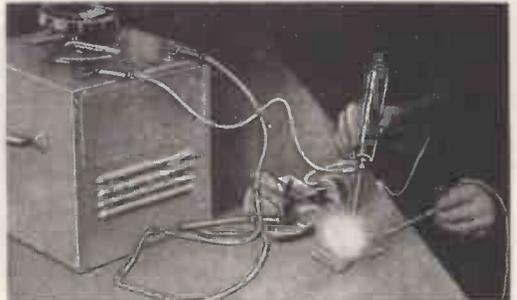
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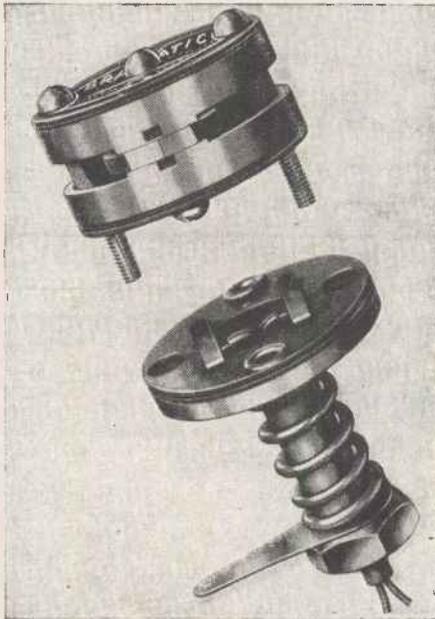
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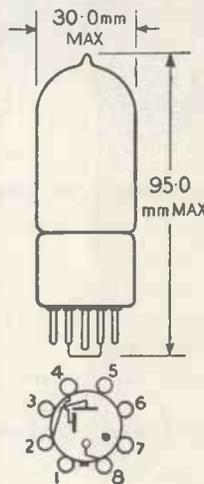
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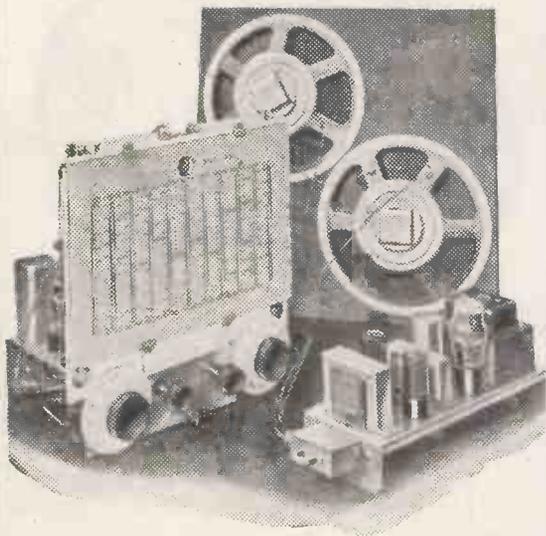
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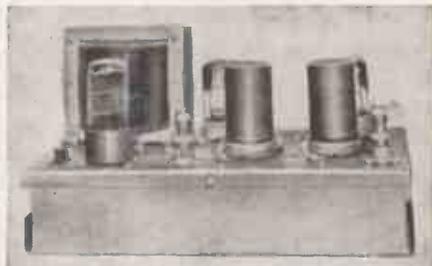
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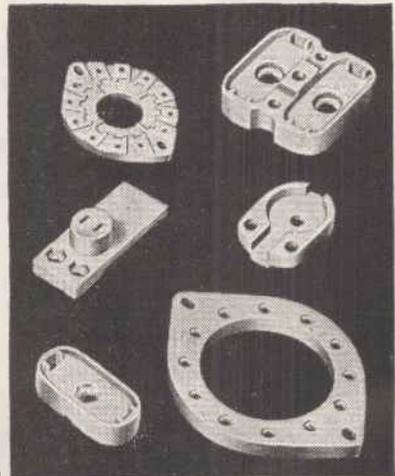


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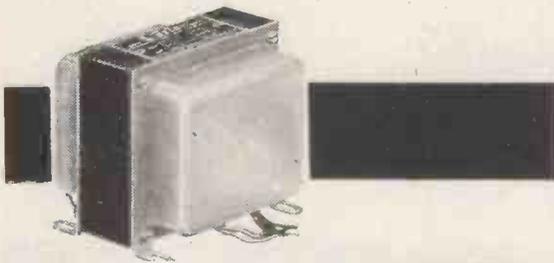


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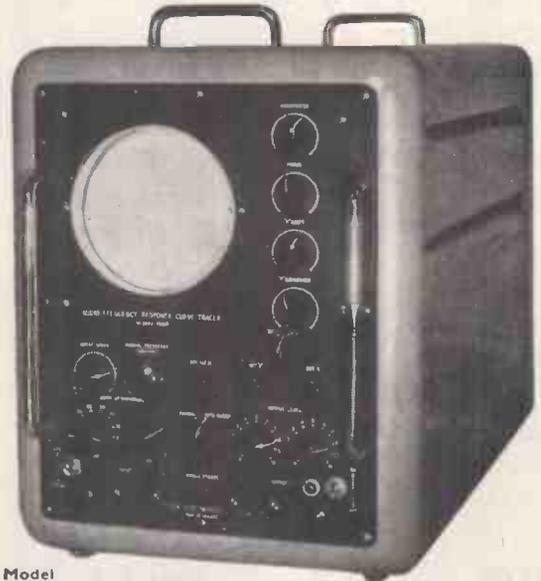
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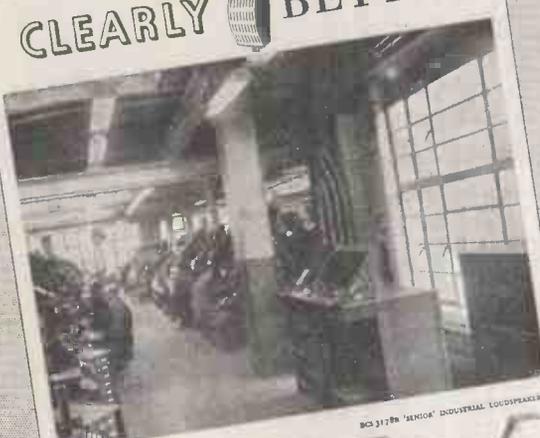
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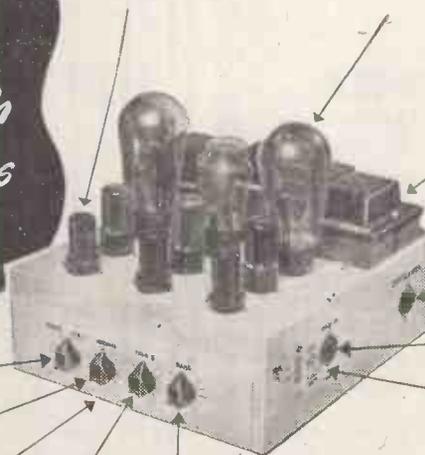
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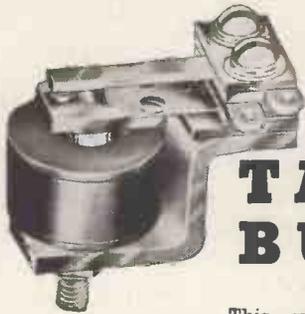
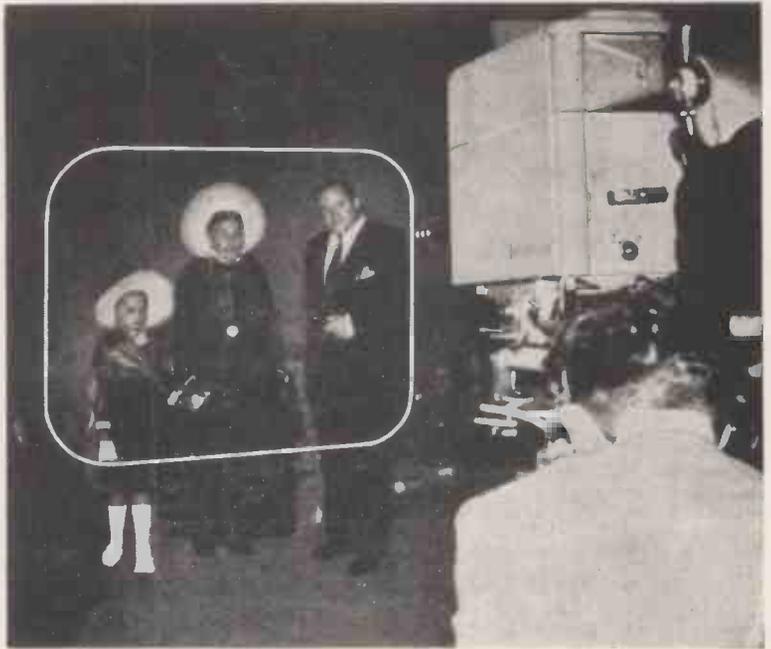
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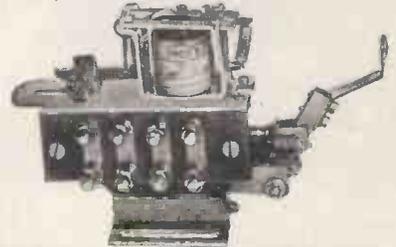
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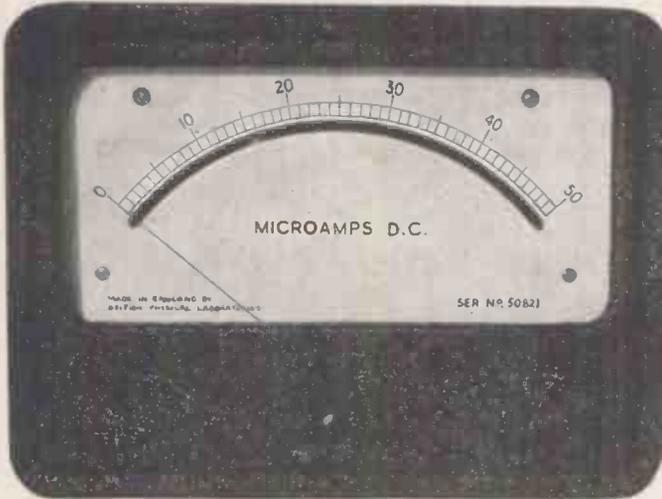


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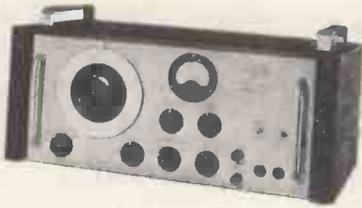


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AS ONE MAN
SAID TO ANOTHER



Dear Sirs,

A short time ago a friend of mine in Massachusetts purchased one of your transformers. His enthusiasm knew no bounds so I am sending you an International Money Order on this date for one of these transformers. I might add that I am looking forward to doing business with you after the recommendation that I have received.

Sincerely yours,

The New Model Type 2B36B, Primary 10,000 Ω centre tapped, incremental inductance over 100 henrys. Secondary impedances 1-25 Ω , 2-8 Ω , 5 Ω , 7-8 Ω , 11-3 Ω , 15-3 Ω and 20 Ω . Leakage reactance under 15 millihenrys. Size : 5 $\frac{1}{2}$ " \times 4" \times 6". F.C. 4 $\frac{1}{8}$ " \times 3 $\frac{1}{4}$ " \times 2BA. Weight : 12 lbs

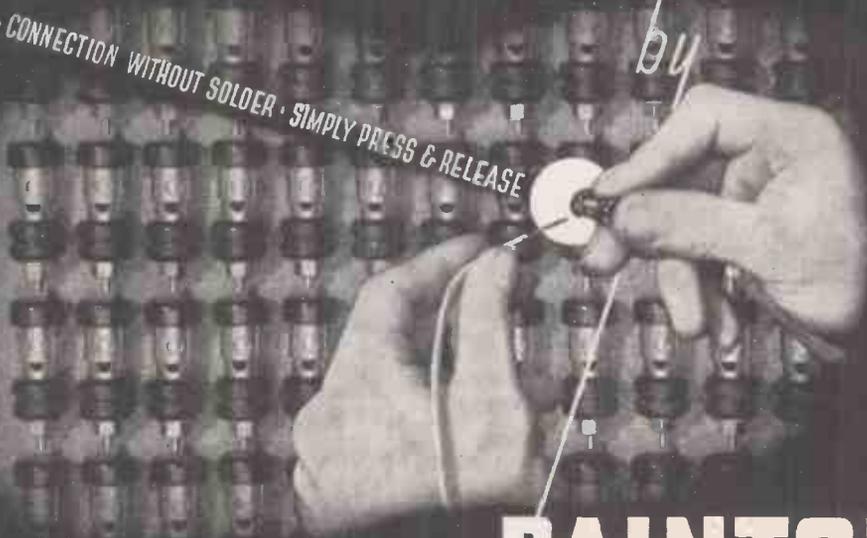
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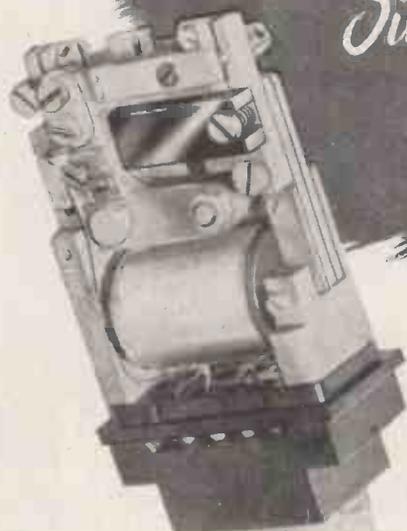
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Ceramic, Amphenol, Paxolin, all types

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**12 v D.C. to 230 v A.C. 50 cycles Rotary
Converters**, 150 watts. Complete with
300 v A.C. Meter and D.C. Input Regulator.
£7/10/0, plus carriage.

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Retail price without pickup - - - - - £13 15 0
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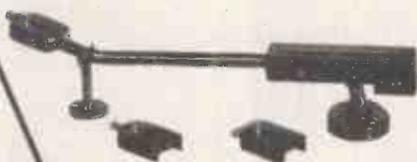
SUPER LIGHTWEIGHT PICKUP for standard and microgroove recordings.

The interchangeable heads are fitted with an easily replaceable armature system complete with a semi-permanent sapphire. Armature mass 20 milligrams. Extremely low mass at needle point (4/5 m.g. only) allowing for reduction in downward pressure to 10/12 grams for standard recordings, and 5/7 grams for microgroove recordings.
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THE CONNOISSEUR Varigroove Recording Unit. 33.1/3 and 78 r.p.m. 100 to 300 GROOVES PER INCH continuously variable, MOVING COIL CUTTER HEAD of entirely new design. Patented method of suspension allowing use of large magnet system, producing sensitivity and response hitherto unobtainable. All patterning effects eliminated, allowing microgroove recordings to be made with ease.
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LESS THAN 5 WATTS required to fully modulate.
Price £130 0 0

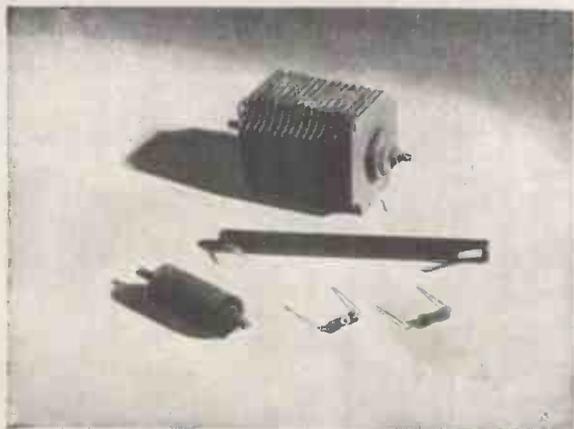
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- Special tone control circuit, with independent bass boost and cut, and treble boost and cut.
- Built-in vibrator.

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40th YEAR OF PUBLICATION

In This Issue

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Editor: H. F. SMITH

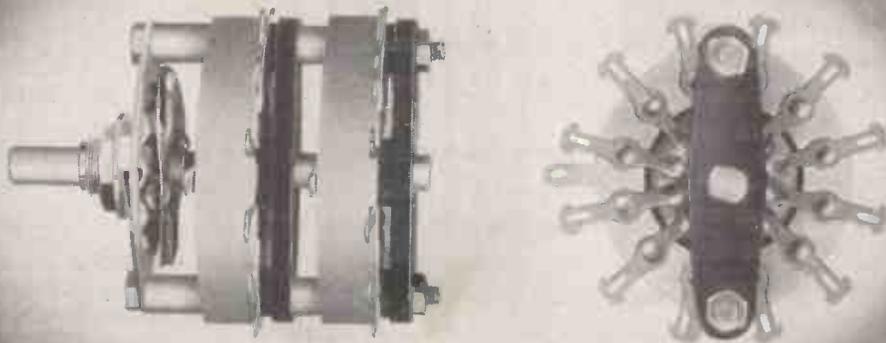
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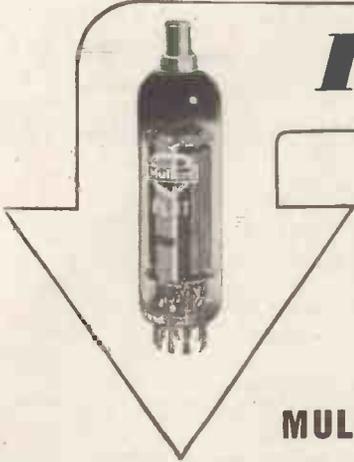


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Important trends in VALVE DESIGN

MULLARD LINE OUTPUT PENTODE TYPE PL81

The line output stage of a television receiver imposes conditions which call for a valve having properties which differ considerably from those of a normal output valve.

The essential requirements for a line output valve are, first, that it shall be capable of supplying a large peak anode current when operated at a low anode voltage, and second, that the insulation of the anode shall be capable of safely withstanding the high voltage peaks, which may amount to 5KV to 7KV, occurring during the fly-back period.

Satisfaction of the first of these requirements is mainly a matter of the geometry of the valve; the second can be assured only by careful mechanical design.

The PL81 is an all-glass power pentode on the B9A (Noval) base, specially designed for use as a line output valve. Its heater is rated at 0.3A, 21.5V, and is therefore suitable for series operation in transformerless receivers intended for A.C. or D.C. mains supply.

It will deliver a peak anode current of 350 mA at an anode voltage of only 70V and a screen voltage of 170V. The efficiency of the valve is thus intrinsically high.

By adopting the booster diode circuit whereby the H.T. line voltage is increased, the required output can be obtained at a still lower anode voltage, so that the already high efficiency of the stage is further improved.

The necessary high insulation resistance to withstand a peak voltage of 7KV has been obtained by special internal construction, and by bringing out the anode connection to a top cap so that the use of a specially insulated valve-holder is not necessary. Even so, the seated height of the valve is only 75mm and the overall diameter 22.2mm—dimensions only slightly larger than those of the voltage amplifying pentode in the same range.

The production of a valve of this output and high insulation in so small an envelope may be counted as something of an achievement.

RATINGS & CHARACTERISTICS

Heater Suitable for Series operation, A.C. or D.C.

V_h	21.5V
I_h	0.3A

Capacitances

C_{in}	14.3 μ F
C_{out}	6.5 μ F
C_{a-g1}	< 0.4 μ F
C_{g1-h}	< 0.2 μ F

Characteristics

V_a	170V
V_{g3}	0V
V_{g2}	170V
V_{g1}	-22V
I_a	45mA
I_{g2}	3mA
g_m	6.5mA/V
μ_{g1-g2}	6

Reprints of this article together with additional data may be obtained free of charge from the address below



MULLARD ELECTRONIC PRODUCTS LTD.
TECHNICAL PUBLICATIONS DEPARTMENT
CENTURY HSE, SHAFTESBURY AVE. W.C.2

These Valves make News!

MINIATURE AMERICAN TYPES

for AC/DC EQUIPMENT

A complete range of miniature B7G valves is now available for 110 volt or 240 volt AC/DC equipment. All these valves bear American type numbers.

TYPE 50C5

OUTPUT TETRODE for 110v. Supply

Heater Rating	50.0 volts 0.15 amp
Mutual Conductance	7.5 mA/V
Power Output	1.9 watts

Price: **15/6** plus P. Tax

TYPE 19AQ5

OUTPUT TETRODE for 240v. Supply

Heater Rating	19 volts 0.15 amp.
Mutual Conductance	4.1 mA/V
Power Output	4.5 watts

Price: **13/-** plus P. Tax

TYPE 35W4

HALF WAVE RECTIFIER

Heater Rating	35 volts 0.15 amp.
R.M.S. Input	240 volts max.
Rectified Current	100 mA. max.

Price: **10/6** plus P. Tax

DIMENSIONS:—Seated Height 2½" max.
Diameter ½" max.

TYPE 12BE6

SPECIAL HEPTODE

Supply Voltage	110 volts	250 volts
Heater Rating	12.6 volts 0.15 amp.	
Anode Impedance	0.5	1.0 meg.
Osc. Mutual Conductance	7.5	7.5 mA/V
Conversion Conductance	0.40	0.48 mA/V

Price: **16/-** plus P. Tax

TYPE 12BA6

VARI Mu R.F. PENTODE

Heater Rating	12.6 volts 0.15 amp.	
Anode Impedance	0.25	1.5 meg.
Mutual Conductance	4.3	4.4 mA/V

Price: **13/-** plus P. Tax

TYPE 12AT6

DOUBLE DIODE TRIODE

Heater Rating	12.6 volts 0.15 amp.	
Voltage Gain	33	42

Price: **12/-** plus P. Tax

DIMENSIONS:—Seated Height 1½" max.
Diameter ½" max.

BRIMAR

WRITE NOW TO DEPT. 4530
for data sheet on the above valves.

TECHNICAL ADVICE SERVICE

STANDARD TELEPHONES AND CABLES LIMITED, FOOTSCRAY, SIDCUP, KENT.



AN APOLOGY

The inconvenience and annoyance caused to the public and to our friends in the trade occasioned by the delay in delivery of *acos* microcell pick-ups is a matter that causes us the gravest concern. It is in the main due to the unprecedented demand for these pick-ups which has outrun the supply of certain raw materials and also made our factory space inadequate. Commitments to manufacturers made prior to the general announcement of the pick-ups have still further aggravated the position.

Happily, the raw material problem should shortly be solved and plans for greater production facilities are being urged forward. In the meantime, we are doing all we can to meet existing orders, but regret that delivery on new orders will be subject to about three months' delay.

We can only express our regrets for the circumstances that have made this announcement necessary, and trust that our trade friends and the general public will bear with us in view of our assurance that all possible steps are being taken to meet the situation and to reduce delay to a minimum.



COSMOCORD LIMITED · ENFIELD · MIDDLESEX

THE "BELLING-LEE" PAGE

Providing technical information, service and advice in relation to our products and the suppression of electrical interference

Apologies to the B.B.C.

In the September issue of the "Wireless World" on this page we stated that the B.B.C. altered the frequencies of Sutton Coldfield a fortnight before the station opened.

This was a mis-statement for which we do not hesitate to apologise. Something happened, but at this distant date we cannot recall the details, but B.B.C. Engineering Division tell us that they first published the Sutton Coldfield frequencies on 20th September 1948 and that they were never altered. We agree that nothing should be said or written which might cause uneasiness in the minds of the trade or the public.

While we do our best to be accurate in this page, when we do "drop a brick," the quality of those who come back at us is ample evidence that our page is read by the right people.

Rationalisation of Television Aerial Numbering

Most "Wireless World" readers know that eventually there will be eleven television transmitters operating on five frequency channels, and therefore the sooner we stop talking about the London and Midland transmitters the better. The transmitters should be referred to by their official channel number—London—Channel 1, Midland—Channel 4, etc.

All aerial manufacturing members of the Radio and Electronic Component Manufacturers' Federation have agreed to indicate the television frequency by the official channel number following a stroke, incorporated immediately after the list number of the particular aerial.

It has also been agreed to standardise a colour code for each frequency channel, but this may not be used by everyone immediately.

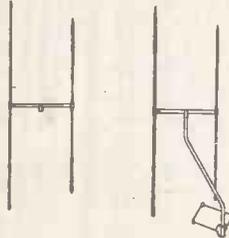
So far as all this concerns "Belling-Lee" a complete new list of television aerial numbers has been built up, and became operative on Sept 1st.

At first all aerials are being despatched from the factory labelled on the outside with the old and the new numbers, and using the following colour code:

Channel No.	Cat. suffix	Colour Code
1. London	1	Yellow
2. North England	2	Light Blue
3.	3	Red
4. Midlands	4	Green
5.	5	Dark Blue

In each "Belling-Lee" case the first figure group before the stroke will indicate the list number,

the first suffix the channel on which the aerial will operate (-/1 London, -/4 Midland, etc.) and the second suffix shows either the type of mounting (-/L chimney lashing, -/W wall mounting, -/9 9 foot mast and lashing) or the type of feeder supplied (-/B balanced, -/U unbalanced).



L802/1 or 4/C. L802/1 or 4/L.

Comparison of Aerial Prices

"Belling-Lee" aerials may appear dearer than some but we do ask those interested to make certain that when they are thinking or talking aerial prices that they are clear in their minds what they are getting for their money. "Belling-Lee" have made a practice of stating the price of a complete aerial, whereas some other manufacturers feature a price which is in fact the price of the cross-arm and elements only, pole, if any, and lashings are extra. Because of this, one is apt to consider that "Belling-Lee" aerials are more expensive than they really are.

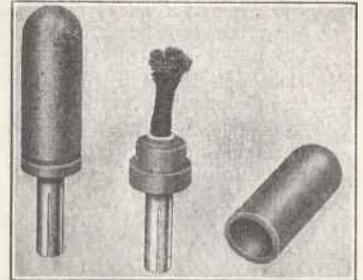
Suppression of Motor Car Ignition Interference.



It is very gratifying that some interest is at last being taken in this subject and it is possible that a lot will be done voluntarily before legislation takes place. The A.A. give it its blessing, then the B.B.C. are helping by their film on Television and by demonstration on Sound Broadcast, neither are they always preaching to the already converted. There must be many television viewers whose cars are still a source of annoyance to others. The selfish owner never sees the trouble his own car makes, unless his wife drives too, and then it is only for a minute while the car is put in its garage. It is the duty of every viewer to suppress his own car and to persuade all those who see his television to do likewise. Many garages have been slightly hostile towards the fitting of suppressors, so we are grateful to the

"Motor" for the excellent article they published recently. This, together with the fact that one of the greatest names in car electrics now recommend and market suppressors, must do a great deal to break down uninformed opposition.

An Amateur testifies on behalf of the "Coronette" silent aerial discharger.



This is an extract from a letter dated July:

"The past week or so has given ample opportunities for studying the effects of the device on 'coronary discharge' interference with the reception of short and medium wave broadcast reception.

I am using an R.C.A. 'AR.77E' Communication Receiver and can now listen in comfort to the most distant continental medium wave transmitters during heavy and protracted rain storms. It is only after half an hour's torrential rain that a slight background 'hiss' manifests itself, and this is a remarkable improvement after my experience before fitting the Discharger, when, as you know, immediately rain started any programme, other than North Regional or Light, was blotted out by terrific 'static' of the shrieking variety.

I am happy to say that the expense incurred in taking down and re-erecting the aerial consequent upon fitting the 'Silent Discharger' has been more than repaid in increased listening pleasure over the last two week-ends.

I might add that I seem to get all-round quieter performances since fitting your Company's device, and am very grateful to you for all the trouble and interest you have taken in the matter."

NOTE: The "Coronette" discharger is designed to fit "Skyrod" aerials only and is unsuitable for other makes of Vertical aerials.

BELLING & LEE LTD
CAMBRIDGE ARTERIAL RD., ENFIELD, MIDD., ENGLAND

An amAZing new amplifier.

Factual Figures

FROM A-Z, FROM PICK-UP TO SPEAKER, including Tone Control Circuits
NOT MERELY A LABORATORY MEASUREMENT OF AN AMPLIFIER ONLY, BUT THE
WHOLE STORY OF THE "A-Z", AS IT WILL PERFORM UNDER USERS' CONDITIONS

NATIONAL PHYSICAL LABORATORY REPORT

ON TESTS OF AMPLIFIER (MARKED : TYPE A-Z, SERIAL No. A50/1, SOUND SALES)

TESTED FOR :—SOUND SALES LTD., WEST STREET, FARNHAM, SURREY

REFERENCE :—LETTER, RNW/DES/AZ, DATED 31.8.50

The instrument was tested for sensitivity at various frequencies between 20 and 25,000 cycles per second. The total harmonic distortion was measured at 60 c/s and 1,000 c/s ; the hum and noise output voltage and the output impedance were also determined.

The supply to the instrument was at 230 volts and 50 c/s ; the connection to earth was independent of the mains supply and made directly to the instrument.

The input was in all cases made to the lead provided, with the controls set as follows :—LF cut, 0 ; volume 12 (maximum) ; Bass, 0 ; Treble, 0. A load resistance of 15.0 ohms was connected to the output of the amplifier by means of the leads provided.

TABLE I
8 WATTS OUTPUT

Frequency, c/s	Input, volt
20	0.100
60	0.101
1,000	0.102
3,000	0.102
5,000	0.102
10,000	0.102
15,000	0.102
20,000	0.102
25,000	0.102

SENSITIVITY

The input required to develop an output of 12 watts in the load at 1,000 c/s was 0.125 ± 0.002 volt.

The input required to develop an output of 8 watts was measured at several frequencies ; the results obtained are given in Table I

HARMONIC DISTORTION

The harmonic distortion was measured with an output of 12 watts at 60 c/s and 1,000 c/s. The second and third harmonics of the fundamental, in about equal proportions, were found to predominate. The total harmonic voltage expressed as a fraction of the fundamental is given in Table II.

TABLE II
12 WATTS OUTPUT

Input Frequency	Ratio, Total Harmonics/ Fundamental
60 c/s	0.002
1,000 c/s	0.002

HUM AND NOISE

The hum and noise output voltage was measured with the input lead short circuited and found to be 0.005 volt.

OUTPUT RESISTANCE

The output resistance was measured at a frequency of 1,000 c/s for output powers of 3 watts and 12 watts in a load resistance of 15.0 ohms.

The results obtained are given in Table III

TABLE III

Power Output, watts	Output resistance, ohm
3	0.50 ± 0.05
12	1.2 ± 0.1

Date 5th October 1950.

Reference E.488.18.

Passed by L.M.F., C.H.R.

E. C. BULLARD, Director.

L. HARTSHORN,

for Superintendent, Electricity Division.

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In each case the speaker is damped by a minimum of 12 times at audible frequencies to prevent speaker resonance, and the crossover is very fast, approximately 28 db for the first octave. A control is provided to vary the power applied to the treble speaker, to compensate for its efficiency compared with the bass speaker, and a frequency record reveals the absence of dip or rise in output at crossover frequencies.

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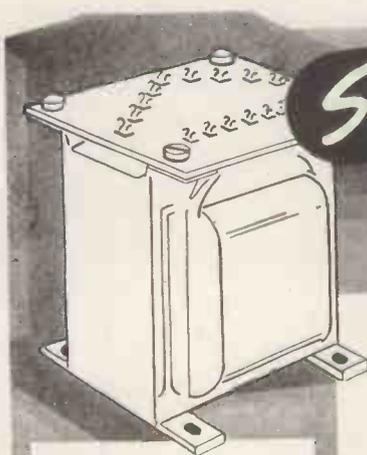
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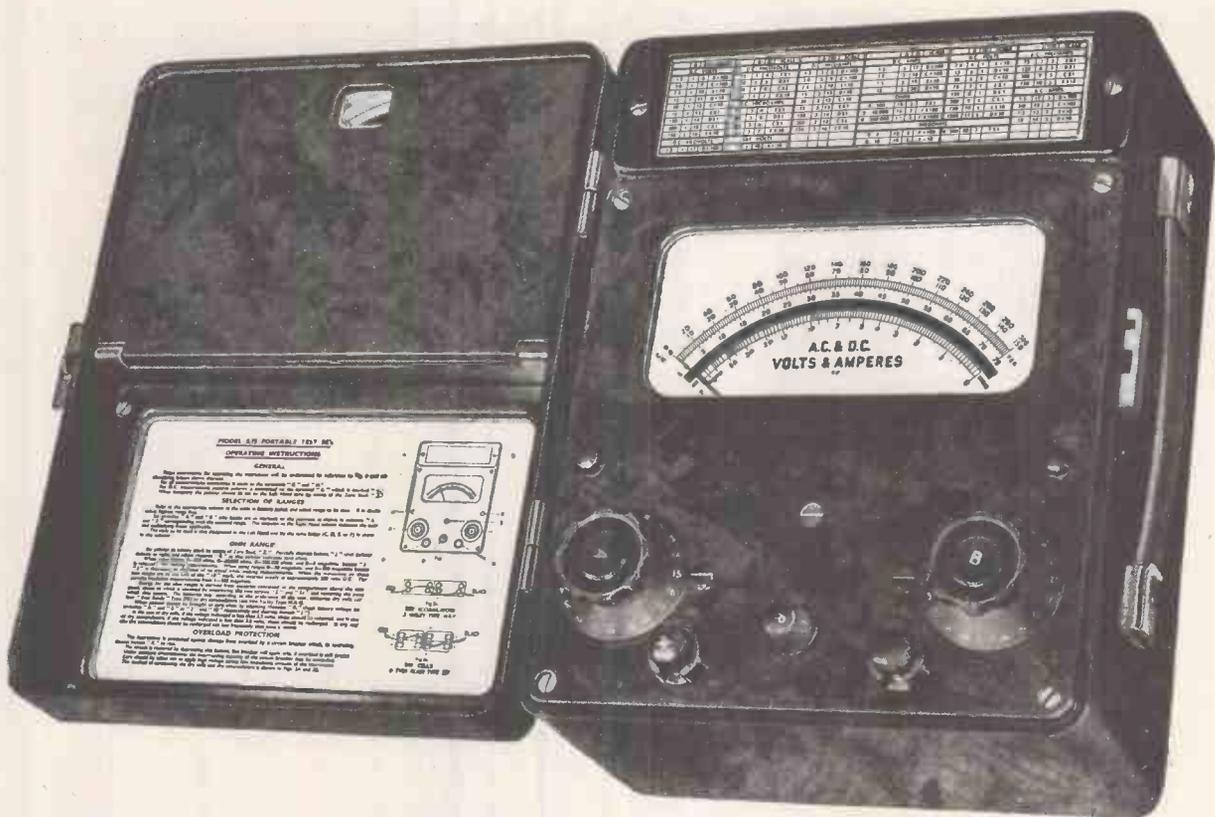
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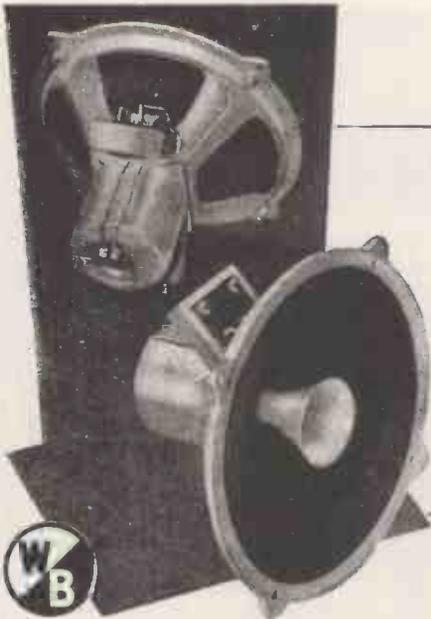
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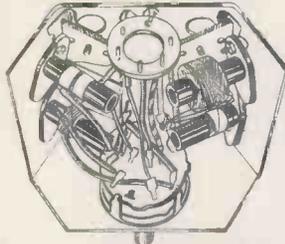
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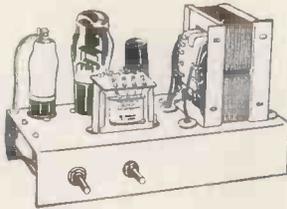
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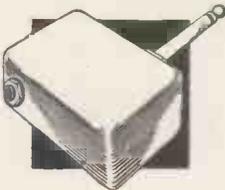
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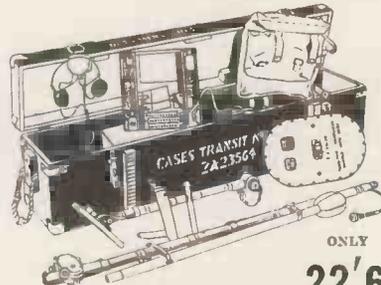
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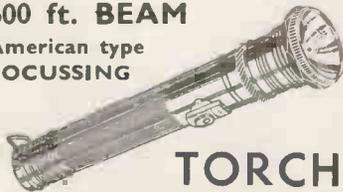
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Two specially designed chokes with three smoothing condensers with circuit diagram. Cuts out all mains noise. Can be assembled inside existing receiver. 6/- complete.

CO-AXIAL CABLE.

Super quality cable, consisting of a centre copper core, a polyvinyl resin type insulator, a flexible screen, a weather-proof P.V.C. outer cover. Just the thing for Television lead-in, super mike cable, etc., 80 ohms impedance. Cat. No. C.755, 3d. per foot.

THE PREMIER 1950 CATALOGUE

contains all the newest TV Kits, Components, Aerials, Tubes, etc., in addition to thousands of Radio Bargains.

Price—6d.

T.V. WHITE RUBBER MASKS.

We can now supply a specially designed White Rubber Mask for 6in. C.R. Tubes at 7/6 each.
9in. White Masks, 9/6. 12in. White Masks, 15/-.

SUPER QUALITY TELEVISION MAGNIFYING LENS.

To suit 5 1/2 in., 6 in. or 7 in. Tubes. Increase picture size considerably, 25/- each.

PERMANENT MAGNET FOCUS POTS.

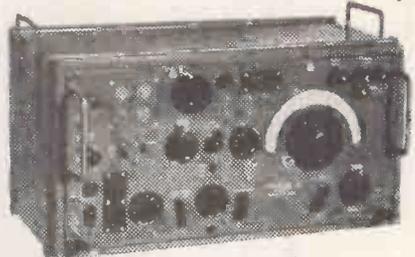
Available for all Tubes, 15/-.
Please state Tube used.

MOVING COIL METERS.

All 2 1/2 in. outside diameter. 1 mA., 7/6; 5 mA., 5/-; 50 mA., 8/6; 150 mA., 8/-; 20 amp., 7/6; 40 amp., 7/6; 20 v., 5/9; 40 v., 5/9; 500 microamps, 7/6. All 3 1/2 in. outside diameter. 1 mA. 15/11; 30 mA., 10/6; 200 mA., 8/6; 500 microamps, 19/6; Thermocouple meters, 2 1/2 in., 2.5 amp., 5/-; 3 amp., 5/-; 3.5 amp., 5/-; 3 1/2 in., 2 amp., 8/6; Electrostatic 3 1/2 in., 2 v., 25/-.

THE LAST FEW R 107 RECEIVERS.

ONE OF THE ARMY'S FINEST COMMUNICATIONS RECEIVERS. (See "W.W." August, 1945.)



9 valves, R.F. amp. osc. Frequency Changer, 2 I.F.s, (465 kc.), 2nd Detector, A.V.C. Af. amp. B.F.O. A.C. mains, 100-250 v. or 12 v. accum. Frequency range 17.5 to 7 Mc/s, 7.35 Mc/s to 2.9 Mc/s, 2.0 to 1.2 Mc/s. Monitor L.S. built in. Complete. Write for full details. Price £12/12/-, plus 21/- carriage and packing.

NEW

A.C. ALL-WAVE SUPERHET KIT.

7 valves (plus rectifiers) for 200-250 v., 40-60 cycle A.C. mains.
4 Wavebands, 13.6-52, 51-190, 190-540 and 900-2,100 metres.

Pick-up input. Uses 6K7, 6K8, 6K7, 6B8, 6J5 and 2-6V6 in push-pull, giving an output of 10 watts. Specially designed QF transformer to match 6V6's to 3 and 15 ohm speakers.
Negative feedback is applied over 3 stages giving a high fidelity output. Tone control is incorporated. £14/5/-.

Also available for A.C./D.C. Mains. Specification as above except that valve line up is 6K7, 6K8, 6K7, 6Q7, 6J7, 2-KT38C. In Kit form at £13/8/10.

FURTHER EXPANSION!

ALL POST ORDERS SHOULD NOW BE SENT TO OUR NEW HEAD OFFICE AT 740 HIGH RD., TOTTENHAM, N.17.

Telephone: TOTTENHAM 5371.

PREMIER MIDGET RADIO KIT



Redesigned and easier than ever to build. Includes an attractive walnut or cream plastic cabinet 12 in. x 5 in. x 6 in.

The valve line-up is 6K7, 6BH7 and beam power output (CV1510) in the A.C. model and 6K7, 6BH7 and 12A6 in the A.C./D.C. model. Both use metal rectifiers and are for use on 200-250 volt mains. The dial is illuminated and the receiver presents an attractive appearance. Medium and long waveband coverage. Complete kit of parts with valves, speaker, cabinet and point-to-point diagrams.

Please state if A.C. or A.C./D.C. **£4.19.6** inc. P.T. is required.

NEW 3-BAND MIDGET SUPERHET KIT

Redesigned to cover the short, medium and long wavebands (16-50, 190-540, 1,000-2,000 metres) A.C. valve line-up, 6K8, 6K7, 6Q7, CV1510 Beam power output. A.C./D.C. valve line-up is the same excepting output valve is 12A6. Both use metal rectifiers and are for use on 200-250v. mains.

In cream or walnut cabinet as illustrated. Illuminated dial. An attractive and powerful receiver. Complete kit of parts with Valves, Speaker, Cabinet and point-to-point diagrams.

Please state if A.C. or A.C./D.C. **£6.19.6** inc. P.T. is required.

CATHODE RAY TUBES. ALL NEW AND PERFECT.

CV. No.	Civil'n No.	Dia. in inches	Focus	Defn.	E.H.T.	O.K. for T.V.	Price	Roll pkg. and Inset
254	—	9	E.S.	Mag.	8kv.	Expmtl.	40/-	10/-
2719	—	2.75	E.S.	E.S.	1450	Expmtl.	10/-	2/6
600	5CPI	5	E.S.	E.S.	2kv.	Yes	25/-	2/6
601	5BPI	5	E.S.	E.S.	2kv.	Yes	27/6	2/6
602	3API	3	E.S.	E.S.	1.5kv.	Yes	15/-	2/6
790	2API	2	E.S.	E.S.	1kv.	Yes	15/-	2/6
817	3EPI	3	E.S.	E.S.	2kv.	Yes	15/-	2/6
1112	VCR112	5.25	E.S.	E.S.	3kv.	Yes	15/-	1/6
1131	VCR131	12	E.S.	E.S.	4kv.	Yes	80/-	12/6
1138	VCR138	3.5	E.S.	E.S.	1200v.	Yes	10/-	2/6
1140	VCR140	12	Mag.	Mag.	4kv.	Yes	90/-	12/6
1879	ACR2	5 1/2	E.S.	E.S.	8kv.	Yes	15/-	2/6
1381	ACR3	5.25	E.S.	E.S.	3kv.	Yes	15/-	1/6
1384	—	11.3	E.S.	E.S.	4kv.	Expmtl.	40/-	10/-
1395	—	6.25	E.S.	E.S.	3kv.	No	17/6	2/6
1811	VCR511	11.75	E.S.	E.S.	4kv.	Expmtl.	60/-	11/6
1816	VCR516A	9	Mag.	Mag.	3kv.	No	40/-	10/-
1521	VCR521	3.5	E.S.	E.S.	4kv.	No	5/-	1/6
1522	VCR522	1.75	E.S.	E.S.	800v.	Yes	15/-	1/6
1593	VCR517	5	E.S.	E.S.	2kv.	Yes	20/-	2/6
2880	KM14/1	3	E.S.	E.S.	800v.	Yes	17/6	1/6
3776	—	5.25	E.S.	E.S. Mag.	4kv.	Expmtl.	20/-	2/6

TRANSMITTING AND SPECIAL PURPOSE VALVES

866A	10/-	8012	10/-	708A	10/-	EHT7(CV19)	20/-	MR300/ECV3558	15/-
837	10/-	843	5/-	2E32	7/6	V868(CV168)	8/6	U19(CV187)	6/6
860	5/-	3623	5/-	3B24	7/6	EL266(CV15)	40/-	N82(CV1199)	5/-
872A	10/-	713A	6/6	V869	7/6	VT30(CV1030)	7/6	CV87(Kinatron)	5/-
830B	10/-	XEL15	6/6	GDT4C	6/6	U17(CV1113)	5/-	GU50(CV1072)	7/6
878	10/-	807	6/6	DET5	10/-	PT25R(CV1046)	5/-	1628(CV1755)	3/6
861	20/-	AC27	10/-	282A	10/-	VU33A(CV354)	8/6	BL63(CV1102)	6/6
832	10/-	2X2	2/6	327A	15/-	ADM(CV1314)	6/6	G11(CV1262)	6/6
803	10/-	9002	3/6	958A	2/6	DQC(CV1141)	8/6	V1906(CV20)	6/6
803	10/-	9003	3/6	958	2/6	717A(CV3594)	6/6	E1359(CV76)	40/-
705A	10/-	9004	3/6	CV1510	6/6	BL11(CV1197)	5/-	931A	30/-
1616	5/-	—	—	—	—	EL114B(CV3505)	6/6	Base for 931A	2/6

152-153, FLEET STREET, E.C.4. Phone: CENTRAL 2833—and at—207 EDGWARE RD., W.2. Phone: AMBASSADOR 4033

207, Edgware Road is open until 6 p.m. on Saturdays.

Terms of Business: Cash with order or C.O.D. over £1.

Send 6d. stamp for list.

PREMIER RADIO COMPANY

MORRIS & CO. (RADIO) LTD

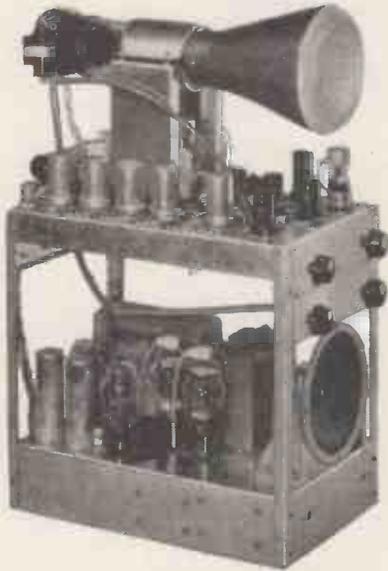
NEW LONG RANGE TELEVISOR KITS

FOR THE LONDON OR BIRMINGHAM FREQUENCIES

— £17 - 17 - 0 —

As is usual in Premier Kits every single item down to the last Bolt and Nut is supplied. All chassis are punched and layout diagrams and theoretical circuits are included.

FIVE EASY-TO-ASSEMBLE KITS ARE SUPPLIED :—



A well-made walnut finish PEDESTAL CABINET is available from stock at £5/10/0, plus 7/6 carriage and packing. Working models can be seen during transmitting hours at our Fleet Street and Edgware Road branches.

VISION RECEIVER with valves, carriage 2/6.....	£3 13 6
SOUND RECEIVER with valves, carriage 2/6	£2 14 6
TIME BASE with valves, carriage 2/6.....	£2 7 6
POWER SUPPLY UNIT with valves, carriage 5/.....	£6 3 1
TUBE ASSEMBLY , carriage and packing 2/6.....	£2 18 6

This unit includes the VCR97 Tube, Tube Fittings and Socket and a 6in. P.M. Moving Coil Speaker with closed field for Television. The Instruction Book costs 2/6, but is credited if a Kit for the complete Televisor is purchased.

Any of these Kits may be purchased separately ; in fact, any single part can be supplied. A complete priced list of all parts will be found in the Instruction Book.

20 Valves are used, the coils are all wound and every part is tested. All you need to build a complete Television Receiver is a screw-driver, a pair of pliers, a soldering iron and the ability to read a theoretical diagram.

The following sensitivity figures prove that the Premier Televisor Kit is capable of reception at greater distances than any other standard commercial ki. or receiver whether T.R.F. or Superhet.

		VISION RECEIVER.
Sensitivity	...	25 μ v for 15v peak to peak measured at the Anode of the Video Valve.
Sound Rejection	...	Better than 40 db.
Adjacent Sound Rejection	...	Midland Model Better than 50 db
		SOUND RECEIVER.
Sensitivity	...	20 μ v. Vision Rejection, better than 50 db.

NEW PRE-AMPLIFIER FOR FRINGE RECEPTION AREAS With sensitivity better than 35db.

We can supply the complete kit of parts to make this wide band width Pre-Amplifier, using 2 717A Pentodes. With all parts, valves, chassis, diagrams, etc., **27/6**

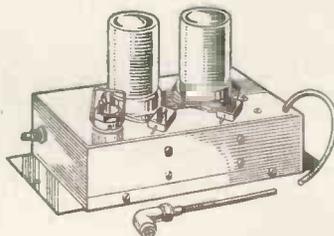
All parts available separately.

SEPARATE POWER SUPPLY KIT

for use with this Pre-Amplifier can be supplied for **21/-**
(H.T. output 130v., 20mA. L.T. 6.3v., .4A.

When ordering Televisor kits

PLEASE STATE IF THE LONDON OR BIRMINGHAM MODEL IS REQUIRED



207, EDGWARE RD., W.2 Phone : AMBassador 4033 (Open till 6 p.m. Satur
AND AT **152-153, FLEET STREET, E.C.4** Phone : CENtral 2833

Terms of Business : Cash with order or C.O.D. over £1. Send 6d. Stamp for list.

ALL POST ORDERS to our new Head Office : 740 HIGH ROAD, TOTTENHAM, N.17. Phone : TOTtenham 5371.

BRANCH

PREMIER RADIO COMPANY

MORRIS & CO. (RADIO) LTD.

Now being Delivered!

PREMIER TELEVISOR KITS

FOR LONDON AND BIRMINGHAM

USING 9" OR 12" MAGNETIC C.R. TUBES

£19.19.0 *including all parts, valves and loud-speaker, but excluding C.R. TUBE*

(Carriage and Packing 15/-)

CIRCUIT DETAILS

The Vision Receiver consists of 4 R.F. stages (EF54's) which are followed by a Diode Detector and Noise Limiter (6H6) which is directly coupled to the Video valve (EF54). Complete Kit with valves, £3/16/0. Carriage and packing 2/6.

The Sound Receiver comprises 3 R.F. stages (6SH7's) followed by a Double Diode Triode (6Q7), which acts as Detector and L.F. Amplifier. A Noise Limiter (EA50) is also incorporated. The output valve (6V6) drives a 10in. P.M. Moving Coil Speaker with closed field magnet, which is included in the Time Base Kit.

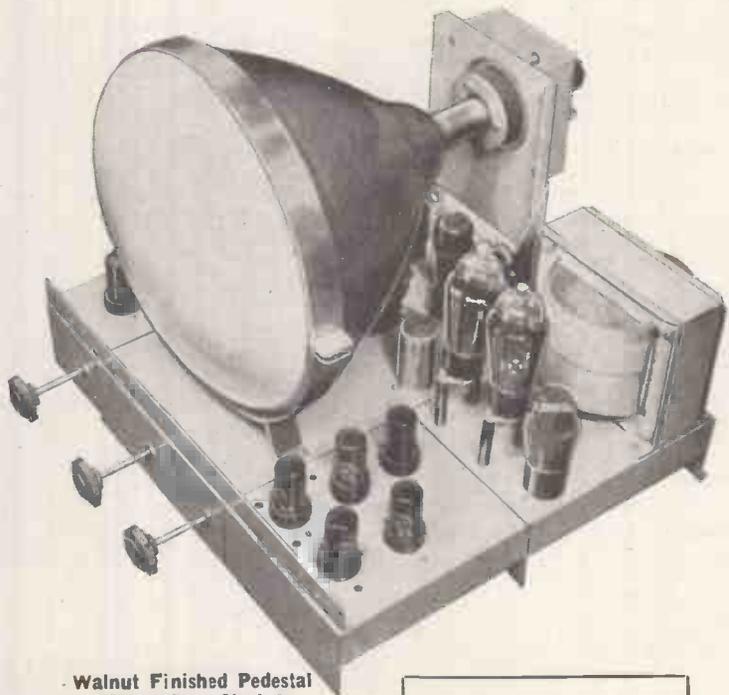
Complete Kit with valves, £3/1/0. Carriage and packing 2/6.

The Time Bases employ blocking oscillators on both Line (6SH7 and 807), and Frame (VR137 and 6V6). E.H.T. (Non-lethal) is taken from the Line Output Transformer through a voltage doubler employing two valves (VU111). The Sync separators are 6H6 and 6V6.

Permanent Magnet Focusing. Complete Kit with valves, £8/5/6. Carriage and packing 5/-.

The Power Supply is from a double wound mains transformer completely isolating the receiver from the mains. The H.T. Rectifier is a 5U4G.

Complete Kit with valves £4/16/6. Carriage and packing 5/-.



Walnut Finished Pedestal Cabinets from Stock for
 9in. Tubes £6 15 0
 12in. Tubes £8 8 0
 Carriage and Packing 7s. 6d.

EACH KIT OR INDIVIDUAL PART AVAILABLE SEPARATELY

The following sensitivity figures prove that the Premier Televisor Kit is capable of reception at greater distances than any other standard commercial kit or receiver whether T.R.F. or Superhet.

VISION RECEIVER

Sensitivity : 25 μ V for 15V peak to peak measured at the Anode of the Video Valve
 Sound Rejection : Better than 40 db.
 Adjacent Sound Rejection : Midland Model. Better than 50 db.

SOUND RECEIVER

Sensitivity : 20 μ V. Vision Rejection : Better than 50 db.

"MAGNETIC"
 CONSTRUCTION

BOOK

3/-

7, EDGWARE RD., W.2 Phone: AMBassador 4033 (Open till 6 p.m. Saturdays)
 AND AT 152-153, FLEET STREET, E.C.4 Phone: CENTra: 2833

Terms of Business : Cash with order or C.O.D. over £1. Send 6d. Stamp for list.

ALL POST ORDERS to our new Head Office : 740 HIGH ROAD, TOTTENHAM, N.17. Phone: TOTrenham 5371.

DON'T MISS THESE BARGAINS

MAINS TRANSFORMERS

Ordinary—E.H.T.—Special.

All transformers are suitable for 200-250 v. 50 cycle mains, are fitted with primary screens, fully impregnated and complete with all necessary clamps, etc.

300-0-300 at 80 mA. 6.3 v. at 4 amp. 5 v. at 3 amp. Half shrouded drop through, 14/6.

260-0-260 at 60 mA. 6.3 v. at 3 amp. 5 v. at 2 amps. Half shrouded drop through. Price 13/9.

350-0-350 at 80 mA., 4 v. at 6 amps. 4 v. at 3 amps., drop through or upright mounting, a useful replacement type for old-type receivers. 16/6.

350-0-350 at 100 mA., 6.3 v. at 5 amps., 5 v. at 2 amps. Fully shrouded upright mounting, 19/6.

260-0-260 at 60 mA. 4 v. at 4 amps. 4 v. at 3 amps. Half shrouded drop through. Price 13/9.



235-0-235 at 60 mA. 6.3 v. at 3 amp., 5 v. at 2 amps. Fully shrouded upright mounting, 15/-. Primary has an additional tap for 110 v.

Filament Transformer, 6.3 v. 1½-2 amps, upright, 6/-.

350-0-350 at 160 mA., 5 v. at 3 amps., 6.3 v. at 6 amps., 6.3 v. at 3 amps. Fully shrouded upright mounting, 36/-.

250-0-250 at 100 mA., 5 v. at 3 amps., 6.3 v. at 6 amps., 27/6.

2,500 v. at 5 mA., 4 v. at 1.5 amp., 202 v. at 2 amp., 27/6.

4 KV. at 5 mA., 2 v. at 2 amp., potted with insulators, 67/6.

Special combined transformer designed to be suitable for Television or oscilloscope using a 6in. tube VCR97, etc. 400-0-400 at 150 mA., 2.5 KV. at 5 mA., 6.3 v. at 6 amps., 6.3 v. at 6 amp., 6.3 v. at 2 amp., 4 v. at 1 amp., 4 v. at 2 amps., 5 v. at 3 amp., 70/-.

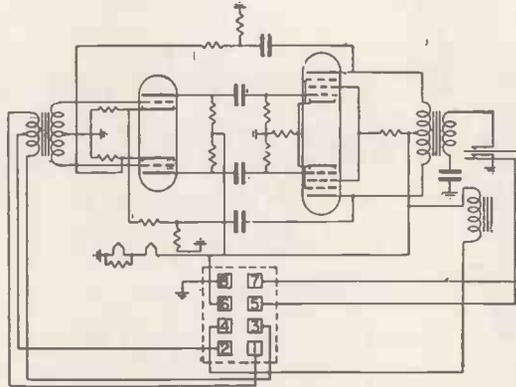
SPECIAL

6.3 v. at 2 amps.,
60 v. at 200 mA.,
tapped 200/220, 230/250,

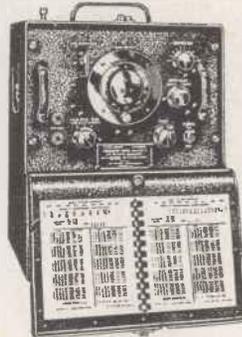
7/6

PRE-AMPLIFIER

MODEL K



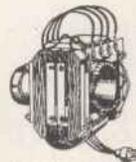
The above is the circuit diagram of pre-amplifier model K. You will notice that the circuit includes two double valves, push-pull input, and push-pull output transformers, a relay, a choke, and numerous small resistors and condensers. The whole thing is complete with valves wired up and enclosed in a metal case size approximately 5½in. x 4in. x 4in. You will readily appreciate that this little unit will fit in almost any cabinet, including table models. These units are very well-made by a famous American company, originally intended for Forces use, to increase the output of low gain microphones and pick-ups. We have a fair quantity available, all new and unused, the price is 17/6 each and as this is the equivalent of a 4-valve push-pull amplifier, it is of course enormous value. We anticipate a big demand, so please order by return.



FREQUENCY METERS BC221

American Manufacture. Accuracy .005%. Frequency range k/cs 20 mc/s. Crystal controlled and temperature compensated. Makes an excellent V.F.O. without impairing its use as a frequency meter. Complete with instruction book. Used, in good condition. Carriage paid, £25.

PARTS FOR TELEVISORS



FRAME AND LINE COIL ASSEMBLY

Perfectly made by a very famous maker, for standard type magnetic tubes, 9in., 10in., 12in., or 15in., we have a limited number only, the price is 16/6, and cannot be repeated once these are cleared, so please act quickly.

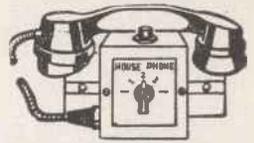
PERMANENT MAGNETIC FOCUSING UNITS. No current drain—for all makes of tubes—patented method of adjusting the gap, giving really clean pictures and even focus of whole of the tube free. Price 16/6 each.

P.M. FOCUSING
for
clear pictures

R. F. E. H. T.
Non-Lethal

R.F. E.H.T. We were so pleased with the quality of this unit that we have taken up the entire output of the manufacturer, the voltage can be adjusted to make it suitable for working 9in., 12in. or 15in. tubes, the unique design and vacuum impregnation combine to give a trouble-free unit which will give years of satisfactory service, and, of course, the big point about the R.F. E.H.T. is that it is not lethal, the size is only 4½ x 3½ x 4in., price complete, ready to operate, 65/-.

HOUSE TELEPHONES



Desk or Wall Mounting

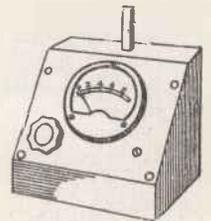
Suitable for intercommunication between offices, workshops, stores, garages, big houses, kitchens, etc. Each station consists of normal size Bakelite handset and desk or wall mounting cabinet with built-in selector switch, buzzer and push. All stations can communicate with one another independently. Each installation is absolutely complete and internally wired. 3-station installation complete with 50 yards 5-core cable 16/10/-. 4-station installation, complete with 50 yards 6-core cable, 18/10/-. 2-station installation, complete with 25 yards 4-core cable, 13/17/6.



ELECTRIC HEATERS

Heavy cast iron framework totally encloses the elements, so these are 100%

safe even in confined spaces, just right for your radio den, garage, office, shop, etc. 900 watt (heavy) model, 23/6, plus 5/6d. carriage. Other models available are: 750 watt, 500 watt, 250 watt, all these are 23/6 each, plus 4/6 each carriage. The 250 watt model used as a foot-warmer keeps legs and body warm for less than a farthing per hour.



SHORT TURNS COIL TESTER

You know that it is almost an impossibility to test for shorted turns in I.F. Transformers, Coils, L.T. Transformers, etc., with an ordinary ohmmeter. Our mains-operated shorted turns coil tester will reveal these faults in a second. An essential instrument in all coil-winding shops as it will test for continuity at the same speed. 16/10/-.

MISCELLANEOUS ITEMS

8 kv. sleeving, 3/- doz. yds. B7G ceramic valve holder, 10d. Ditto, EF50, 9d. Pax EF50, 6d. Int. Oct. Valve holder Amphenol, 6d. Pax, 4d. Miniature 100 K pots, 1/6.

DEPENDABLE SPARES. Unless otherwise stated none of our spares is Government Surplus. Prices do not include postage, for details of this see bottom of this page.

ELECTROLYTIC CONDENSERS

4 mfd. 450 v.	1 6	8 mfd. x 8 mfd. at 450 v.	3 4
8 mfd. 150 v.	1 3	8 mfd. x 16 mfd. at 350 v.	2 6
8 mfd. 350 v.	1 6	8 mfd. x 16 mfd. at 450 v.	3 6
8 mfd. 450 v.	1 11	16 mfd. x 16 mfd. at 350 v.	3 0
8 mfd. 500 v.	2 6	16 mfd. x 16 mfd. at 450 v.	3 9
16 mfd. 450 v.	1 11	16 mfd. x 8 mfd. x 24 mfd. at 450 v.	4 2
16 mfd. 450 v.	2 8	25 mfd. x 25 mfd. at 200 v.	3 11
16 mfd. 500 v.	3 6	16 mfd. x 8 mfd. at 350 v.	2 6
32 mfd. 350 v.	2 8	16 mfd. x 8 mfd. at 500 v.	4 6
32 mfd. 450 v.	3 6	250 mfd. at 12 v.	2 3
10 mfd. 25 v.	1 0	16 mfd. x 32 mfd. at 350 v.	3 4
25 mfd. 25 v.	1 0	12 mfd. at 50 v.	1 3
50 mfd. 12 v.	1 0		

P.M. SPEAKERS

All speakers are by very famous makers such as Rola, Celestion, Goodmans, etc.

Size.	With Trans.	Less Trans.
2½in.	—	10 6
3½in.	—	10 0
5in.	12 3	10 6
6½in.	12 6	10 6
8in.	13 6	11 6
10in.	18 6	16 6
12in.	—	39 6

ENERGISED SPEAKERS

6½in. with 700 ohm field and hum buckler, price 9/- . 8in. with 2,000 ohm field, hum buckler and output transformer, 15/6.

I.F. TRANSFORMERS

465 kc/s, iron dust cored very high "Q" fitted in standard size can, 6/9 per pair, 465 kc/s iron dust cored very high "Q" fitted in midget size can, 12/6 per pair. 465 kc/s air cored, medium size can, 6/9 per pair.

L.F. CHOKES

Heavy duty types suitable for power packs and mains smoothing. These are mostly Government Surplus.

200 mA. 10 henry	10 0	120 mA. 9 henry	6 6
200 mA. 3 henry	5 0	80 mA. 10 henry	4 6
Midget-type inductance		80 mA. 5 henry	4 0
unknown	3 6	40 mA. 5 henry	3 6

OUTPUT TRANSFORMERS

Midget pentode matching to 3-5 ohm	3 6
Standard pentode matching to 3-5 ohm	3 9
Medium pentode matching to 3-5 ohm	3 3
Standard size multi-ratio	4 6

VOLUME CONTROLS

All have full-length spindle and are complete with fixing nuts. We stock full range of values between 2,000 ohms and 2 megohms. prices are less switch, 2/6 each; single-pole switch 3/9 each.

TUNING CONDENSERS

2-gang .0005 mfd. with long spindle	5 6
Ditto, but fitted with trimmers	6 6
4-gang with built-in trimmers fitted into a screening compartment but easily removable	4 9
Single-gang .0005 standard size with medium-length spindle	2 9

LIQUIDATOR'S STOCK



Polished walnut radio cabinet size 20 x 12 x 7½in. complete with L., M. and S. dial, size 7 x 6½in. and backplate with magic eye cutout, also with drilled chassis and hardboard back. You will find it quite a simple matter to complete this into a very handsome receiver of the £15 class. Limited quantity, price 32/6, plus 2/6 carriage for the 5 items.

FOR YOUR LABORATORY

You many times have felt the need of a device which would enable you to put resistance or capacity or a combination of these two quickly into a circuit. We have a small quantity of resistances and capacity boxes which, by the simple manipulation of plugs, will enable you to do this. With these boxes you can put in 1 ohm, 2 ohms, 3 ohms, 4 ohms, and so on, in steps of 1 ohm, right up to 6,000 ohms. In a similar way capacity can be put into circuit by small amounts, thus making it simple for you to find optimum working conditions. These boxes made for Government Laboratories, are available while they last at 19/6 each plus 1/6 post and packing. Don't delay—order by return.

BREAK-DOWN UNIT

At present day prices the spares in this unit would cost at least £5. Here is a list of the main contents:

- 3 two-metre coils;
- 3 tuning condensers, split-stator type;
- 4 two-watt carbon resistors, useful values;
- 1 tapped 20 watt resistor, vitreous covered;
- 6 paper condensers, .05 mf. 1,000 v. working;
- 3 paper condensers, .1 mf. 1,000 v. working;
- 2 H.F. chokes;
- 4 paper condensers, .1 mf. 450 v. working;
- 2 paper condensers, .15 mf.;
- 5 bakelite moulded mica condensers .001;
- 1 paper condenser, .01 mf. 3,000 v. working;
- 24 rubber grommets, assorted sizes;
- 6 resistors 1 watt, all useful values;
- 6 resistors ½ watt, all useful values;
- 40 resistors ¼ watt, all useful values;
- 40 silver mica condensers assorted values, including: 10, 15, 20, 40, 50, 100, 150, 300, and 500 pf. types;
- 4 English octal valve holders;
- 2 English 5-pin valve holders;
- 1 E.F.50 type valve holder;
- 3 diode valve holders;
- 1 louvered casing, size 12 x 7 x 4½in.;
- 1 heavy metal chassis size 12 x 7 x 2 in.;
- 8 condenser clips assorted sizes.

Also an assortment of nuts, bolts P.K., self-threading screws, tag boards, chassis mounting tag connectors, screened grid caps, plain grid caps, levers rollers, connecting rods, outputsockets, etc., etc. ALL THIS COLLECTION OF PARTS FOR 6/6 only, plus 1/9 postage and packing.

TWO SUPER SPEAKERS

The first is a beautifully made 10in. P.M. speaker, a real precision product made by a very famous speaker firm. It is undoubtedly a 10in. which reproduces with all the quality of a 12in. It has three special features (1) a solid diecast frame (2) a special speech coil suspension which gives wider frequency response (3) dustproof cone assembly. Speech coil is normal 2.3 ohms. Price is 16/6 plus 2/6 post and insurance. The second is the 8in. P.M. speaker made by the same firm whose name incidently we are not allowed to mention but you will recognise it immediately. This again has normal 2/3 ohm coil. Price is 11/6 plus 1/9 post and insurance.

—THIS MONTH'S SNIP—

RADIOGRAM UNIT BY A VERY FAMOUS MAKER. Comprising centre drive induction motor with speed regulator, auto stop and magnetic pick up, all mounted on a full size unit plate. Brand new in manufacturer's cartons. The motors are 78 R.P.M. type, but we understand that as they are governor controlled, their speed can be reduced to 33 R.P.M. or they can be made into dual speed motor by quite a simple modification. We have no precise details of this modification at the moment, but if these come to hand we will gladly supply free of extra charge to purchasers. Only a limited supply of these radiogram units are available at this month's Snip price of £5 5s. ea. (this is almost half proper price) so order by return. If not calling enclose 3/6 extra for packing and insurance.



Orders under £2 add 1/6, under £1 add 1/-. Postable items can be sent C.O.D., additional charge approx. 1/-. Good stock of all items at time of going to press. List 6d. Telephone: Ruislip 5780

PRECISION EQUIPMENT (2) ELECTRON HOUSE, Windmill Hill, RUISLIP MANOR, MIDDX.



FIRST AGAIN!

12" TELEVISION AT THE LOWEST PRICE

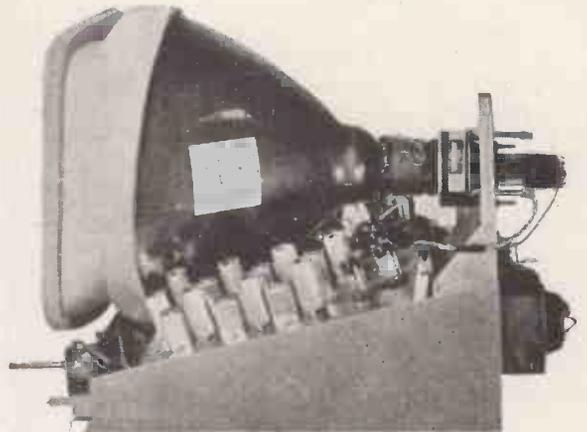
First Time Offered

**T.V. CHASSIS - LONDON or BIRMINGHAM
RECORD VALUE**

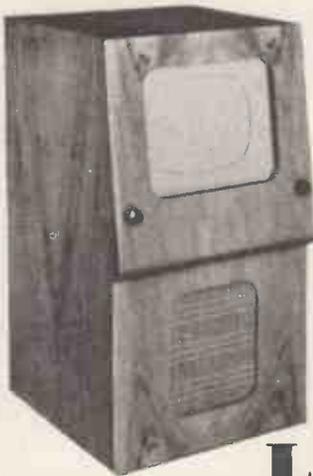
15 valves. Large 12in. black and white picture. **BRAND NEW AND UNUSED.** This is not a kit but a factory built job. Fully assembled and tested, made by well-known manufacturer. Sound and vision RF. unit uses latest type miniature valves, 6 of 6AM6 and 2 of 6AL5. Permanent magnet focussing. Complete with all valves. Any type of 12in. c.r. tube can be used. High quality sound with Elac 8in. p.m. speaker. Closed field. Hard valve time bases on frame and line, uses 2 7C5 and 1 62BT. Line fly back E.H.T. 7-8 Kv., non lethal using EY51.

**LASKY'S
PRICE £23 0 0**

Complete with 15 valves, but less cathode ray tube.
Carriage and insurance 37/6 extra.



Power supplies 200-250 volts 50 c.p.s. Auto wound mains transformer, with two 6 volt, a 2 volt and 5 volt windings for valve heaters. 53KU rect. Dimensions: 15½in. wide, 15½in. deep, 10in. to top of tube support. Make no mistake, this is no Ex-Government lash up, but a new television receiver, complete in every detail, and when fitted with a cathode ray tube it is ready to function. Mount it in a cabinet of your own choosing, in a wall or any location that meets your requirements. Complete working and circuit diagrams, for future reference supplied with each receiver. Write for further details. Better still call and view. "SEEING IS BELIEVING."



A beautiful walnut console television cabinet, suitable for use with either our 10in. or 12in. receivers. It is fitted with a shelf for easy fixing of the chassis, speaker grill and fret, metal castors. Undrilled.
LASKY'S PRICE £8 . 10 . 0
Carriage 12/6 extra.

**WHY VIEW IN THE DARK
ELIMINATE EYE STRAIN.**

Filters.	Filter Lens
9in., 13/6.	9in. or 10in.
10in., 18/-.	Price 50/-.
12in., 21/-.	

Clear lens. 9in. or 10in. Price 45/-,
All the above post free.

CATHODE RAY TUBES. NEW AND GUARANTEED.

9in. Mullard, Mazda, Brimar ..	£11 6 10
10in. Cossor, E.M.I.	£12 12 0
12in. Mullard, Mazda, Brimar..	£15 2 5
12in. aluminised Brimar, G.E.C.	£16 1 4

Carriage extra.

TELEVISION AERIALS by K.A.
Combine lightness with extreme rigidity.

U/D. Universal dipole.	30/-.
W/DR. Wall fitting dipole and reflector.	60/-.

Carriage free.

(Please state London or Midlands.)

LASKY'S RADIO

370 HARROW ROAD, PADDINGTON, LONDON, W.9

Telephone: CUNningham 1979

Write for a copy of our current Bulletin giving full details of our stocks of new manufacturers surplus components, valves, transformers, etc., also Ex-Government equipment. Enclose a 2½d. stamp, with your name and address, for a copy by return.

AT LAST IT'S HERE!

A Portable Analyser at a Price You Can Afford



THE L.S.L. VALVE AND CIRCUIT ANALYSER

MODERN SERVICING METHOD

- ★ Saves time and trouble.
- ★ Portable. Can be used on the bench or in the home.
- ★ Simple to operate.

In carrying case, black crackle finish, with leather handle. Size 12" x 12" x 7". Almost half usual price.



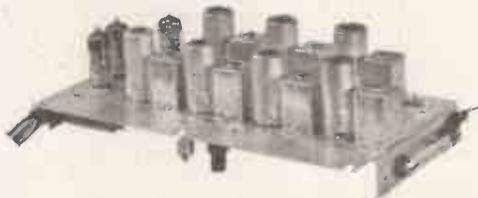
Six important features:—

1. The resistance of the meter is at the rate of 2,000 ohms per volt.
2. Used as an external meter it has a total of 30 ranges of voltage, current and resistance readings.
3. It is the only universal meter on the market which employs two moving coil meters on the one panel, thus giving a simultaneous indication of current and voltage reading.
4. The meter is extremely useful in locating difficult and intermittent faults by leaving it in circuit in the stage suspected on a "soak" test, the meter automatically indicating incorrect readings when they occur.
5. It is the only meter on the market possessing an internal switch whereby "zero end" can be carried out on the three resistance ranges by a flick of the switch and without the bother of holding two external wires together.
6. There is a current reversing switch included which is particularly valuable in measuring grid bias.

LASKY'S PRICE £10 19 6. With leads and adaptors. Carriage and insurance 10/- extra.

AND NOW A TELEVISION/SOUND VISION UNIT. NEEDS NO CONVERSION

Model A—London. B—Birmingham. By well-known British manufacturer. Uses 10 of the latest type miniature valves. Specification and line up: Vision: 3 R.F. stages with 6AM6's. Det. and int. suppr. 6AL5. Syn. Sep. 6AM6. Video output 6AM6. Sound: 3 R.F. stages with 6AM6's. Det. and int. suppr. 6AL5. Sound output 6AM6. Size of unit: 10in. x 4½in. x 1in. Circuits and full data supplied with each unit. Remember these are brand new manufacturers surplus and not Ex-Government. **COMPLETE WITH VALVES.** **LASKY'S PRICE £6 19 6.** Carriage 2/6 extra.



MAINS TRANSFORMERS.

Primary 200-250 volts 50 c.p.s.
 MBA/3. 350-0-350v 80 m/a.,
 6.3v 3a., 5v 2a.
 Both filament windings tapped at 4v.

PRICE 18/- Post Free.



SBT/1. 300-0-300v 80m/a.,
 6.3v 3a., 5v 2a.

PRICE 15/- Post Free.



ANTENNA RELAY UNITS TYPE GBY/29125

Contains 0.5 m/a m/c meter, relay insulators 0.75 amp heating element and switch. Also 50 pf. 5 Kv vacuum condenser. In black crackle metal case as illustrated.

LASKY'S PRICE:
 NEW BOXED - - - 12/6
 SOILED 7/6 POSTAGE 1/6

CONDENSER CORNER. By famous Manufacturers.

All new goods fully guaranteed.

2 mfd.	350 v.w.	1/-	25 mfd.	25 v.w.	1/6
4	350	1/3	50	12	1/-
4	500	2/-	64	450	5/11
8	350	2/-	8 x 8	150	2/6
8	500	2/6	8 x 8	500	4/6
12	50	1/-	8 x 16	450	4/3
16	500	3/-	8 x 16	500	4/11
20	12	1/-	16 x 32	350	4/11
			32 x 32	350	4/11

GARLAND BROS

AMPLIFIER ACIII: We are pleased to announce that we are now using a Varley Mains Transformer, specially wound for us, and a Varley D.P.47 Hi-Fi Output Transformer in this popular kit. Specification: 7 valves (incl. rectifier). Push-pull Output up to 10 watts (2 x 6V6G) to 3Ω or 15Ω Speaker (state which). Supply available for tuner unit, etc., 280 v. 30 mA approx. High and Low Gain Inputs. Separate Bass and Treble controls. Negative Feedback. Complete kit, with circuits and instructions (incl. circuit of suitable quality local-station tuner). £7/17/6.

"OSMOR" GLASS DIAL ASSEMBLY: 3-colour, 3-wave, 7in. x 7in., with drive mechanism. 25/-.

"OSMOR" "Q" COILPACKS: A selective high-Q coilpack of miniature size (1½in. x 3½in. x 2½in.) with easy one-hole fixing. Type HO, Long, Medium and Short, 33/- plus 7/4 P.T. Type LM, Long, Medium and Gram., 28/- plus 6/4 P.T. Type TB, Medium, Long and Shipping, 35/- plus 7/10 P.T. Type EX, Medium, Short and Short, 35/- plus 7/10 P.T. Type B, Long, Medium and Short Battery with frame aerial, 37/6 plus 8/4 P.T. Type T.R.F. Long, Medium for T.R.F. Receivers, 30/- plus 6/8 P.T.

"OSMOR" H.F. STAGES: Designed for use with above coilpacks. For HO, TB and EX Coilpacks, 15/- plus 3/4 P.T. For LM Coilpack, 13/- plus 2/10 P.T.

I.F. TRANSFORMERS: 465 k.c., standard size, capacity-tuned. Made for us by a leading manufacturer. Per pair, 12/6.

T.R.F. COILS: M. & L. wave, with reaction winding. Per pair, 6/6.

WEARITE "P" COILS: Full range in stock. Each 3/-.

MAINS TRANSFORMERS: Pri: 0-200-220-240 v. Sec: 350-0-350 v. 80 mA. 0-4-6.3 v. 4A. 0-4-5 v. 2 A. Electrostatic screen. Tag connections. Universal winding. A truly all-purpose transformer. Each 16/6.

MAINS TRANSFORMERS: Pri: 0-200-220-240 v. Sec: 250-0-250 v. 80 mA. 0-4-6.3 v. 4A. 0-4-5 v. 2A. Electrostatic screen. Tag connection. Universal winding. Each 16/6.

BALANCED ARMATURE HEADPHONES: Type DLR2. With wide, comfortable double metal headband, lead and plug. The most sensitive low resistance phones made. Boxed. Per pair 5/-.

TRIMMERS: Miniature ceramic air-spaced 3-30pF 5d. each, 4/6 per doz. Philips Concentric type: 3-30 pF, 6d. each, 5/6 per doz., £3 per gross. Ceramic air-spaced 75pF 1/- each. Compression Ceramic type: 50pF 6d. each, 100 + 100 pF, 8d. each, 250 pF, 1/- each, 500 pF, 1/3 each, 1,000 pF, 9d. each.

ALADDIN COIL-FORMERS: Type F804, with iron-dust cores, 5d. each, 4/6 per doz., 48/- per gross.

THERMALLY OPERATED MICRO-SWITCHES: Normally "on." Break at approx. 100° C. (adjustable). Control 10 A, 250 v. Each 3/6.

ELECTROLYTICS: By leading makers. All new and guaranteed, 1/350, 2/6; 2/200, 1/-; 2/350, 1/6; 4/200, 1/3; 4/450, 2/6; 8/350, 2/6; 8/450, 3/-; 8/500, 3/3; 16/350, 2/6; 16/450, 3/6; 16/500, 4/-; 4/9; 5/-; 32/350, 3/-; 32/450 (T.V.), 6/-; 8-8/450, 3/6; 8-8/500, 4/8; 8-16/450, 4/6 and 5/-; 8-16/500, 6/-; 16-16/350, 4/-; 16/16/450, 6/-; 16-32/350, 3/-; 32-32/450, 6/6; 60-100/350, 6/-; 12/50, 1/9; 20/12, 2/6; 25/25, 1/9; 50/12, 1/9; 50/25, 2/-; 50/50, 2/3.

OIL TEMPERATURE INDICATORS: A sensitive moving-coil movement, F.S.D. of which is approx. 120 μA. Centre-tapped moving coil. Calibrated 0-120. Ideal as indicator in bridges, signal strength meter, valve-voltmeter movement, or can be modified as sensitive relay. 3/- each, 30/- per doz.

EHT CONDENSERS: .0015 mfd., 8 kV wkg. Ideal for EHT from line flyback. 2/6 each. .01 mfd. 50kV wkg. 1/6 each.

RESISTORS: ½ w., 3d.; 1 w., 4d.; 1 w., 6d.; 2 w., 9d.; Wide range of values in stock.

WIREWOUND RESISTORS: 6 watt, 2, 2.4, 4, 5, 14, 14, 31.5 ohm, 1/- each. 12/15 watt, 100, 1k, 7.5 k, 9 k, 11 k, 12.5 k, 30 k, ohm, 1/6 each. 45 watt, 80 ohm, 18 k, 2/3 each. 100 watt, 800 Ω, 1k, 10 k, 20 k, 3/- each. 200 watt, 430 ohms, 4/- each.

HEADPHONES, TYPE DLR1: Low Resistance, with headband, lead and plug. New and unused. Special offer at 3/9 per pair, or 42/- per dozen pairs.

CONDENSERS: Ceramic, silver mica, moulded mica, in following values (all pF's). 2, 4, 10, 15, 20, 22, 25, 47, 50, 100, 170, 200, 220, 250, 300, 330, 500, 1,000, 6d. each, 5/- per doz.

TOGGLE SWITCHES: D.P. on-off, laminated bakelite, 1/6. D.P.D.T., black bakelite, 2/6. D.P. on-off, black bakelite, ex-equipment, 1/-.

NEONS: 85 v. striking, no resistor in cap. With holder, 2/- each, 21/- per doz.

CLIX 5A SINGLE PLUGS: Per doz. 2/6.

RUBY LAMP HOLDERS: To take M.E.S. bulb, 1/- each.

ALL GOODS NEW AND UNUSED UNLESS OTHERWISE STATED. GOODS SHOWN AS EX-EQUIPMENT HAVE BEEN FULLY TESTED AND ARE IN GOOD WORKING ORDER. PLEASE ADD POST OR CARRIAGE ON ALL ITEMS.

We maintain a very complete and comprehensive stock of valves, cathode tubes and components for radio, television and electronics. Our shop hours are 9 a.m. to 6 p.m. on Monday, Tuesday, Wednesday, Friday and Saturday, and 9 a.m. to 1 p.m. on Thursday, during which times we are always pleased to welcome callers. Post orders to Garland Bros., Chesham House, Deptford Broadway, S.E.8.

"CLEAREX" TELEVISION LENSES: For 9in. tube, 50/-, with filter, 55/-; For 12in. Tube, 70/-, with filter, 75/-.

TELEVISION FILTERS for 9 in. tube 18/-; For 12 in. tube 21/-.

STABILIZING VOLTS: Type NSL. Voltage stabiliser and divider. Operating voltages 280 v., 210 v., 140 v., 70 v. Max. electrode current 80 mA. Each 10/-.

MICROPHONE TRANSFORMERS: Individually boxed. Each 2/6.

METER OFFER: 2½in. Meters, FSD 50 μA D.C. Tropicalised. Brand new and unused. Few only at 30/- each.

JUNEERO TOOL: Bends, shears, punches and threads. For all the little jobs that waste your time. As reviewed in this journal. Each 18/6.

XACTO SLIDE GAUGE AND PROTRACTOR. For use with above Juneero tool 7/6.

EXTENSION SPEAKERS: Fitted Sin. Plessey P.M. Speaker in bakelite cabinet, with perforated back. Also ideal for intercom. Each 19/6.

AERIAL RODS: Heavily copper-plated steel, one foot long. Fit into one another to make any length aerial. Per doz. 2/-.

PLUGS AND SOCKETS: Pye angle, 1/-; Pye straight, 1/3; B. & L. 5 pin, 1/6; B. & L. 7 pin, 1/9; B. & L. 10 pin, 2/-; Jones 6 way, 1/6; Jones 8 way, 1/9; Jones 10 way, 2/-; Jones 12 way, 2/6; E.H.T. Single, 1/-.

The above prices include plug and socket in all cases. Octal Plug and Socket (Valveholder), black bakelite, 1/9. Jack plug with Igranic socket, 2/6. Pye T-pieces, 6d. Pye connectors, 6d.

OVERLOAD CUTOUPS: Adjustable from 50 to 100 mA. Ex-equipment, 4/- each.

MURKHEAD DIALS: As used on G-units and R.1224A. Each 6/6.

"VIEWMASTER" TELEVISION: Instructions, 5/-.

Components supplied separately, or in kits as follows: Whiteley, 125/-; T.C.C. London, 135/-; Midland, 140/-; Westinghouse, 62/6; Morgan-ate (incl. V/C's) London, 35/9; Midland, 35/-; Plessey, 112/6; Colvern, 19/3. Wearite Coils, London, 22/-; Midland, 30/-.

"ELECTRONIC" TELEVISION: London Handbook, 2/6. Wiring diagram, 2/6. Midland Handbook and Wiring Diagram, 4/6. Chassis, with valveholders, coil formers, etc., mounted: Vision, 22/6; Sound, 22/6; T/Base, 17/6; P/Unit, 25/-; Gantries, etc., 9/-.

Designer approved components: Coils and chokes, London, 15/-; Midland, 17/6. (Please specify London or Midland.) Focus, 30/-; Scanning, 25/6. L/O Transformers, 25/6. Mains Transformer, 90/-; 4kV Transformer, 67/6. 5kV Transformer, 72/6.

L.F. CHOKES: 350 ohm 40 mA, 4/-; 5H 80 mA, 4/6; 10H 80 mA, 7/6; 3H 200 mA, 4/6; 20H 80 mA, 8/6.

P.M. SPEAKERS: New and unused, by leading manufacturers. Sin., 11/6; 6½in., 13/6; 8in., 15in., 10in., 19/6. All 3.

THROAT MICROPHONES: Magnetic, suitable electronic musical instruments. 1/9 per pair.

MAINS DROPPERS: 2 amp, 3/3; 3 amp, 4/6; Vitreous enamelled or cement-coated.

VARIABLE CONDENSERS: 50 pF S.G., 1/-; 100 pF S.G., 2/-; 160 pF S.G., 2/3; 200 pF S.G., 2/6; 500 pF Two Gang, 6/6; 500 pF Three Gang, 7/6. Split Stator 100 + 100 pF 2/-; Split Stator 250 pF with worm gear and switch, 2/6.

MAT RESISTORS: 100 ohm 250 watt, 1/6; 300 ohm 250 watt, 1/9.

VIBRATORS: 6volt non-synchronous (4 pin UX), 5/-; 6 v. synchronous (6 pin UX), 7/6.

SELENIUM RECTIFIERS: 140 v. 600 mA (bridge) or 280 v. 300 mA half-wave, 10/-; 24 v. 1.2 A (American), 12/6; 12 v. 4A (bridge), 15/-.

METERS: 2½in 0-150 v. A.C. (M.I.) American, 6/6; 2in. 50 mA D.C. (M.C.) square flush, 6/-; 2in. 200 mA D.C. (M.C.) square flush, 6/-; 2in. 500 μA D.C. (M.C.) 7/6.

WIREWOUND POTENTIOMETERS: 50Ω, 200Ω, 250Ω, 1 kΩ, 5kΩ, 8kΩ, 10kΩ, 20kΩ, all 5 w. bakelite case, 2/6 each. 100Ω, 500Ω, 5k, miniature 1 w. preset, 1/6 each. 50 Ω 25 w. 4/6 each. 17kΩ 100 w. toroidal ceramic, 6/6 each. 20 kΩ 10 w. De Jur Amisco Precision, 4/6 each.

CARBON POTENTIOMETERS: 500Ω, 3kΩ, 10kΩ, 25kΩ, 50kΩ, 100kΩ, 250kΩ, 500kΩ, 1 mΩ, 2 mΩ, 3 mΩ, 1/6 each.

ANTI-VIBRATION MOUNTINGS: To take 56lb. weight, 1/- each.

MINIATURE 24 v. D.C. MOTORS: 2½in. x 1½in. x 1½in. each 10/-.

MICA T/X CONDENSERS: 500pF, 1.5 A at 4-7.5Mc/s. Test 5,000 v. A.C. for ten minutes. 6 for 5/-.

VALVES T/X AND SPECIAL PURPOSE: 803, 805, 10/-; 8012, CV296, 7/6; VU111, VU120A, CV66 6/6; VU133, CV54, 5/-; 7193, 3/6.

GARLAND BROS

GARLAND RADIO

ALLEN & GOULD

CHESHAM HOUSE, DEPTFORD BROADWAY, S.E.8

5, OBELISK PARADE, LEWISHAM, S.E.13

TELEPHONE: TIDEWAY 4412/3

TELEPHONE: LEE GREEN 4038

D. COHEN

RADIO & TELEVISION COMPONENTS

MAINS TRANSFORMERS

Primary 200-250 v. P. & P. on each 1/6 extra.

250-0-250 100 mA., 6 v. 3 amp., 5 v. 2 amp., Upright mounting, 17/6.

250-0-250, 60 mA., 6 v. 4 amp., (to be used on common heater chain with 6x5 rectifier), 13/6.

280-0-280, 80 mA., 6v. 3 amp., 4 v. 2 amp., drop-through, 14/- Same as above, but 350-0-350 14/-.

Drop thro' 350-0-350 v. 70 mA., 6 v. 2.5 amp., 5 v. 2 amp., 13/6.

Semi-shrouded, drop-thro' 280-0-280, 6v. 3 amp., 5v. 2 amp., 15/-.

Semi-shrouded, drop-thro' or upright mounting 280-0-280 80 mA., 4 v. 6 amp., 4 v. 2 amp., 12/6.

Auto-wound H.T. 280 volts at 360 mA., 4 v. 3 amp., 2 v. 3 amp., or 6 v. 3 amp. Separate 4v. 3 amp. rectifier winding (upright or drop-thro'), 10/6.

Heater Transformers Pri. 200-250 v., 6 v. 1 1/2 amp., 6/-; 2, 4 or 6 v. 2 amp., 7/6. P. & P., each 9d.

ELECTROLYTIC CONDENSERS

50 mfd. 50 work. 1/9.

16.24 mfd. 350 work. 3/3.

100 mfd. 12 v. work. 1/3.

16-16 mfd. 450 work. 4/-.

50 mfd. 12 v. work. 1/1.

25 mfd. 25 v. work. 1/2.

16x8 mfd. 450 work. 3/9.

8 mfd. 450 v. work. 1/11.

250 mfd. 12 v. work. 1/3.

8 mfd. 500 v. 2/9.

16 mfd. 500 v. 3/6.

8x8 mfd., 450 work. 3/6.

32 mfd. 350 work. 2/-.

32+32 M.F.D. small tube tag ends 200 v. work. at 2/-.

P.M. SPEAKERS

Size	with trans.	less trans.
3 1/2 in.	—	9/-
5 in.	13/6	—
6 1/2 in.	13/6	10/-
8 in.	15/6	13/6
10 in.	19/6	17/6

P. & P. on each of above 1/- extra

ENERGISED SPEAKERS

8 in. 2,000 ohm field with O.P. trans., 5,000 ohm imp., 15/6.
5 in. 1,000 ohm field with O.P. trans., 13/6.

Post and packing 1/-.

MIDGET BAKELITE CABINET, 7 in. x 5 1/2 in. x 5 in. c/w. 5-valve S/H. chassis med./long wave scale and back (Takes std. twin gang condenser and 3 1/2 in. speaker), 15/-.

EXTENSION SPEAKER, 4 in. wide x 4 1/2 in. high x 3 in. deep at base tapering to 2 1/2 in. c/w. 3 1/2 in. speaker. 15/-.
Colours of both the above: Cream, walnut, black and maroon. State second choice when ordering.

LINE AND FRAME COIL ASSEMBLY. Frame coils wound but not fitted (full instructions supplied). High impedance frame; low impedance line matching 5-1. 7/6.

6 1/2 in. SPEAKER (P.M.) specially made for Television with closed field, complete with O.P. transformer. 11/6.

CONSTRUCTOR'S PARCEL

Comprising 5-valve superhet chassis with transformer cut-out, size 13 1/2 in. x 6 in. x 2 in., with L.M. and S. scale, size 7 in. x 5 in. Back plate two supporting brackets, drive drum, pointer, two-speed spindle, twin gang condenser. Mains transformer 250-0-250 v. 60 mA., 6 v. 4 amp. Pri. 200-250, 6 1/2 in. speaker and 6x5 rect. 28/- Plus 2/- post and packing.

28/-

6-STATION SWITCHED SUPERHET COIL UNIT, by famous manufacturer. Ideal for Car Radio or Radio set. Range coverage Pos. 1, 200-300 m.; 2, 250-360 m.; 3, 250-360 m.; 4, 320-460 m.; 5, 400-550 m.; 6, 1,100-1,850 m.; no oscillator required for lining up, complete with Circuit and medium and long wave frame aerial. 21/-, post and packing, 1/-.

PRE-ALIGNED MIDGET 465 Kc. Q.120 made for the above Coil Unit. 8/6 per pair, post 6d.

CHASSIS TO FIT COIL UNITS AND I.F.s, size 11 1/2 in. x 5 1/2 in. x 1 1/2 in. 2/6

MAINS TRANS. TO FIT ABOVE CHASSIS. Pri. 200/250 volt. Sec 250-0-250 v. 60 mA., 6 v. 4 amp., 13/6, post and packing, 1/-.

CONSTRUCTOR'S PARCEL, comprising:

Chassis 10 1/2 in. x 5 1/2 in. x 2 in. with speaker and valve holder cut-outs, R. and A. 6 1/2 in. P.M. with transformer, twin gang with feet, pair medium and long wave iron cored T.R.F. coils. Four International Octal valve holders, wave-change switch and Erie 20k pot. with switch, 25/-, plus 1/6 post and packing.

CONSTRUCTOR'S PARCEL, comprising chassis 10 1/2 in. x 5 1/2 in. x 2 in. with speaker and valve holder cut-outs; Rola 5 in. P.M. with O.P. trans.; twin-gang with trimmers; pair of T.R.F. coils; Four International Octal valve holders; wave change switch and Erie 20k pot. with switch, 19/6, plus 1/6 post and packing.

CONSTRUCTOR'S PARCEL, comprising Midget twin-gang with slow-motion drive; pair midget 465 Kc. I.F.s; frame aerial; medium wave osc. coil and layer type H.T. and L.T. batteries 90 v. + 1 1/2 v., 21/-, plus 2/- post and packing.

STANDARD 465 KC. I.F.s. Iron cored Q.120, 7/- per pair.

MINIATURE 465 KC. I.F.s. Type M400B. 12/6, plus 6d. post and packing.

MINIATURE 465 KC. I.F.s (slightly larger than the above item), Q.120. Per pair 10/-.

IRON CORED 465 KC. I.F.s. Q.130, 2 1/2 in. x 1 1/2 in., per pair 6/-.

IRON CORED 465 KC. WHISTLE FILTER, screened, each 2/-.

VALVE HOLDERS, Paxolin International octal. 4d. each. Moulded International octal, 6d. each. EF50 ceramic 7d. each. Moulded BTG slightly soiled 6d. each.

LINE CORD. 3-way 0.3 amp., 180 ohm per yard. 11d. per yard. 3-way 0.2 amp., 300 ohms per yard, 1/-.

CERAMIC P.F.S. 3 each of the following: 330, 220 180 and 82, 2/6.

VOLUME CONTROLS, by famous manufacturer. Long spindle and switch, 1/2, 1 and 2 meg, 3/6 each. 20, 25 and 50 k., 3/- each. Post and packing 3d. each.

VOLUME CONTROLS, by famous manufacturer. Long spindle less switch, 5 k., 50 k., 500 k., 1 meg., 1/9 each. Post and packing 3d. each.

5-VALVE A.C. MAINS, 200-250 v., 3 wave-band superhet chassis. 1,000-2,000, 200-550 and 16-50 metres. By very good manufacturer, complete with valves. 6K8 6K7 6Q7 6V6 and 5Z4. Size of chassis 11 1/2 in. x 7 1/2 in. x 2 in. Size of glass scale 8 1/2 in. x 7 1/2 in. with pick-up sockets (takes 8 in. P.M. with trans.). TAX PAID. £8/18/6. Post and packing 2/6.

CONSTRUCTOR'S PARCEL, comprising: 5-valve superhet chassis with I.F. trans. and V/H. cut-outs, 13 1/2 in. x 6 in. x 2 in. with L.M.S. scale 7 in. x 5 in., back plate and two supporting brackets. Drive drum, spindle and pointer, mains trans. G.E.C. 350-0-350 70 mA., 6 v. 2.5 amp., 5 v. 2 amp., and Plessey 8 in. M. energised 2,000 ohm field with 5,000 ohm impedance, O.P. trans., 29/6. Post and packing 2/-.

CONSTRUCTOR'S PARCEL, comprising: 5-valve superhet chassis with I.F. trans. and V/H. cut-outs, 13 1/2 in. x 6 in. x 2 in. with L.M.S. scale 7 in. x 5 in., back plate and two supporting brackets. Drive drum, spindle and pointer, 6/6. Post and packing 1/6.

CONSTRUCTOR'S PARCEL, comprising: twin gang with feet, pair long and medium iron cored T.R.F. coils, 4 octal V/H., 3 pole 2-way switch Erie 20k. pot. w/s., heater trans. 220-240 v. 1 amp., 2 yds. flat silk flex, 3 black knobs, chassis 10 1/2 in. x 5 1/2 in. x 2 in. with speaker and V/H. cut-outs, metal rectifier 60 mA., 230 v. and 32+32 mfd. 200 v., 19/6, post paid.

GOVERNMENT SURPLUS. Removed from equipment but guaranteed: Metal Rectifier, 230 v. 60 mA., 4/-.
Metal Rectifier, 230 v. 80 mA., 5/-.

Post and packing on each, 6d.
8 mfd. metal cased, 450 v. work, with clip, 1/- each.

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.2 amp. 717 ohms, tapped 100 ohms. 1/6.

.3 amp. 520 ohms, tapped 2/6 each.

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3-pole 2-way, 1/2.

4-pole 4-way, and 4-pole 3-way 1/9.

1-pole 12-way, 2/6.

3-pole 12-way, 4/6.

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White Rubber. 9 in. with glass, 10/6.

WE ARE ABLE TO OFFER THE FOLLOWING:—

Heater transformer fully interleaved and impregnated and guaranteed. 6.3 v. 1 amp., max. input 220/240 volts, 3/6, post paid.

THIS MONTH'S OUTSTANDING OFFER

CONSTRUCTOR'S PARCEL, comprising chassis with V.H. and transformer cut-out, size 13 1/2 in. x 6 in. x 2 in. with s.c.a. size 7 in. x 5 in. Back plate, two supporting brackets, drive drum, pointer and spindle. Mains transformer input 200-250 v. H.T. 280 v. 4 v. 3 amp. and 3 valves, 2 Octal H.F. pentodes, and 1 output valve, all ex-Govt.

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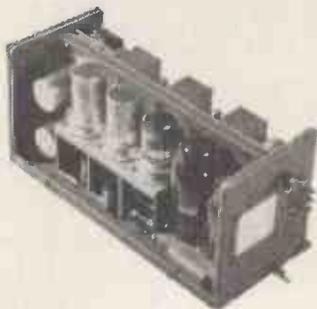
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YOU TOO ! CAN GET GOING ON "144."



The P40 VHF superhet receiver provides yet another basis for that 2 metre rig. Transmitters prove comparatively simple to build but the receiver is another story, but let us explain—We can supply you with this STRATTON built receiver which can be modified for use on "2." The set in its present state can be tuned to any spot frequency between 85 and 95 Mc/s by means of a crystal controlled oscillator stage which should not prove unduly difficult to alter, and pruning the coils is quite simple. REMEMBER ! The P40 would make a FB mobile receiver for "144." Employing an I.F. of 2.9 Mc/s, the valve line includes : 1/EF54 RF, 1/EF54 MIXER, 1/EC52—2/EF54 OSCILLATOR & MULTIPLIER STAGE, 2/EF39 IF, 1/EB34 DET & AVC, 1/6J5 1st audio, and a 6V6 output. The complete unit is enclosed in a die cast frame with a louvered cover. Dimensions 1 1/4 x 5 1/2 x 4 1/2 in.

CLYDESDALE'S PRICE ONLY **£3.19.6** each POST PAID

POWER FOR THE P40 RX.

THE POWER UNIT S-451-B designed for use with the P40 receiver proves to be an extremely handy little unit in any "HAMS" shack, in that it has an LT output of 12 volts, a supply which is often needed for powering Ex-W.D. surplus equipment.

The S-451-B built by STRATTON is complete and ready for use on an A.C. mains supply of 200/250 volts 40/60 cy.

The outputs are 12.5 v. at 2.5 amps and 175 v. at 60 M/a. with double choke smoothing and condenser input.

The power unit is completely enclosed in a die-cast metal frame with a louvered cover. Dimensions 1 1/4 x 5 1/2 x 4 1/2 in.

CLYDESDALE'S PRICE ONLY **39/6** each

POST PAID.

FOR MARINE USE.

The CRV 46151 is a 6-valve superhet suitable for shipping, with a frequency coverage of 195-9050 kc/s 1 RF., and 3 I.F. stages, plus an audio output stage. The 3rd I.F. stage provides C.W. Osc.

VALVE LINE-UP : 4/12SF7, 1/12SA7, 1/12A6 and 1/991 stabiliser.

H.T. power is derived from a 28 v. dynamotor mounted sub-chassis, which has an output of 260 v/70 Ma. The valves are wired in series/parallel providing a 24 v heater circuit. Complete in metal case 15 1/4 x 8 1/2 x 7 1/2 in. Weight 23.8 lb.

CLYDESDALE'S PRICE ONLY **£5.19.6** each

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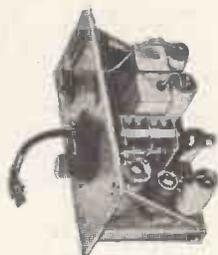
THE 40 METRE RX YOU CAN TAKE WITH YOU.

The receiver unit of the No. 18 WALKIE TALKIE provides an extremely compact set for operation on "40" During tests on 7 Mc/s the 18 Rx proved extremely sensitive and requires only a 2v. accumulator and a 90/120v. H.T. supply with about 1 1/2 v. of bias. The 18 Rx is a 4 valve superhet with regeneration for use when C.W. reception is required, by increasing the L.F. gain control to almost MAX the receiver is in a state of oscillation. The I.F. is 465 Kc/s.

The valve line-up includes 1/ARPI2 R.F., 1/ARPI2 Mixer, 1/ARPI2 I.F., and 1/AR8 2cd DET & AVC and AUDIO OUTPUT. The output jacks are provided for headphone use. Circuits and details are available as required.

CLYDESDALE'S PRICE ONLY **17/6** each.

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HOT NEWS TIP FOR THE COMMERCIAL RADIO CONSTRUCTOR

WALNUT WOODEN CABINETS.

A professionally built finely finished walnut wooden cabinet with inside dimensions 15 1/2 x 8 1/2 x 7 1/2 in. complete with a finished dial aperture in the front 5 1/2 x 3 1/2 in. and a speaker aperture 5 1/2 x 4 1/2 in. Three holes are drilled symmetrically below the dial aperture. This is the type of cabinet which will make want to build that new house set. Refer H394.

CLYDESDALE'S PRICE ONLY **£15.0** each

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DIAL GLASS (Graduated) H 410.

A three WAVEBAND DIAL GLASS to suit the cabinet detailed above, completely graduated with station names and wavelength. Dimensions 6 x 4 in.

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CONTROL KNOBS.

IVORY CONTROL KNOBS 1 1/2 in. diam., 3/4 in. deep with serrated edges suitable to fit 1/4 in. spindle with flat side. Knob complete with spring clip. Refer H403.

CLYDESDALE'S PRICE ONLY **9d.** each POST PAID.

H404, as above but finished in BROWN

CLYDESDALE'S PRICE ONLY **8d.** each POST PAID.

LOUDSPEAKERS.

H396 BRAND NEW 8 inch PM MOVING COIL LOUDSPEAKERS complete with matching transformer. These speakers are standard replacement types and ready for installation, in original makers cartons.

CLYDESDALE'S PRICE ONLY **17/6** each POST PAID.

CONDENSERS.

H399 TWO GANG variable tuning condenser less trimmers. 00035 Mfd. nom. with 1/4 in. spindle 1/4 in. long. Dimensions 2 1/2 x 2 1/2 in.

CLYDESDALE'S PRICE ONLY **7/6** each POST PAID.

MEDIUM and LONG WAVE PADDERS. 150 and 400 Pf. respectively. These two trimmers are mounted in a single ceramic block fitted with a small bracket for mounting purposes.

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H400 8 Mfd. 450 v. Wkg. Ali-can Electrolytic condenser 2 1/2 x 1 1/2 in. diam.

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H400A Mounting clips for the above condenser CLYDESDALE'S PRICE ONLY **4d.** each

H401 16 x 24 Mfd. 450 v. Wkg. Ali-can Electrolytic condenser 2 1/2 x 1 1/2 in. diam.

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H401A Mounting clips for the above condenser.

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An inexpensive 1/2 H.P. motor—modified from the TYPE 29 MOTOR GENERATOR for use on 200/250 Volts A.C. mains. This motor makes an ideal buff, or light tool grinder—or a static drilling machine, a drill chuck can be easily fitted to the end of the lin. spindle after the existing fan has been removed. Motor size 11 in. x 5 1/2 in.

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EX-R.A.F. INDICATOR UNIT TYPE 62. Containing VCR-97 CRT with mu-metal screen; Xtal Unit and valves 16/VR65 (SP61) 2/VR54 (EB34) 2/VR92 (EA50), etc., etc., two deck chassis in metal case. 18 x 18½ x 11½ in. New condition. 67/6 each. Plus 7/6 packing and Carriage.

INDICATOR UNIT TYPE 198. Containing VCR 138A 3½ in. tube 3 VR65, 1 VR54, 1 VR92, 2 high-speed relays, volume controls and 101 res. and condensers. Absolutely brand new. Carriage paid, £2.

BAKELITE RECEIVER CABINETS. An extremely advantageous purchase, enables us to offer the following:—Attractive brown bakelite cabinet, size 15 in. x 8½ in. high x 7½ in. deep, complete with chassis drilled for standard five-valve superhet, back, 3-wave glass dial and back plate. Chassis and cabinet are designed for 6½ in. speaker, and all standard components. Price complete is 25/- only. Limited quantity.

WAVE-FORM GENERATOR TYPE 34. Ex. A.M. Including 6 SP61, 4 EF36, 2 EB34 and one CV116. Also relays, transformers, pots., condensers and resistors. The whole contained in metal box size 11½ x 11 x 8 in. In clean condition, an absolute bargain at 25/-, plus 3/6 packing and carriage.

A.M. RECEIVER UNIT, TYPE 161. Comprising RL37, 2 EF54 and EC52. Coils, relay and many condensers and resistors. The whole in metal box size 8½ in. x 6½ in. x 3½ in. New, a bargain at only 15/- Carriage Paid.

SPECIAL PURCHASE. Brand new H⁴/200 E.H.T. pencil rectifiers, 2,400 v. 3 m.a., only 15/- each. Also RECTIFIERS. J50 (new, ex-Govt.), 7/6 each. Westinghouse 36 EHT 35, 17/4; 36 EHT 100, 26/6.

SLIDER POTS. As used in all the latest T/V sets. A bank of four, comprising 2 or 10K, 100 ohm and 500 ohm. Only 6/- the set. Easily split up.

MIDGET .0005 mfd. TWO-GANG TUNING CONDENSER. Size only 2½ in. x 1½ in. x 1½ in. Capacity guaranteed, standard length ½ in. spindle, complete with mounting bracket, less trimmers, 6/6, or complete with "built-in" trimmers, 7/6. Each plus 6d. post.

RECEIVER TYPE 21. The receiver portion of the W/S 21 operating from 4.2-7.5 Mc/s. Double superhet from 18-30 Mc/s. Incorporating B.F.O. and crash limiter. Valve line-up 7-ARPI2 (VP23) and 2-ARB (HL23DD). Absolutely brand new, complete with circuit. Only 45/- complete. Vibrator Power Unit for above, brand new, 17/6 only.

I.F. TRANSFORMERS. Manufacturer's surplus. Iron-cored. 455 kc/s. Size 4 in. x 1½ in. x 1½ in. Per pair 8/6 whilst they last!

FREQUENCY CONTROL CRYSTALS. By American G.E. Co.—Oxal base fixing. Following frequencies only: 2,500 kc/s. 3,500 kc/s. 4,600 kc/s. 6,200 kc/s., 8,000 kc/s.—at only each 7/6. New Condition.

SPECIAL COIL PACK OFFER. Limited quantity of brand new manufacturers' surplus, 3-wave-band, superhet coil packs. Iron cored. Size 4 in. x 3½ in. x 2 in. deep. Complete with circuit, a bargain at 25/- only.

SPECIAL VALUE IN MAINS TRANSFORMERS. 250-0/250, 90 m/a 6.3 v. 3 a., 5 v. 2 a., half shrouded, drop through type. Electrostatic screen. Price 15/- only, plus 9d. post. Limited quantity.

RECEIVER TYPE 21. The receiver portion of the T/R 1196. Covers 4.3-6.7 Mc/s., and makes an ideal basis for an all-wave receiver, as per "Practical Wireless," August, 1949 issue. Complete with valves types EF36(2) EF39(2), EK52 and EBC33. Supplied complete with necessary conversion data for home use. Only 22/6. Chassis only, 8/6.

6½ in. WAFER SPEAKERS. Special offer of the above well-known speaker, listed at 25/- . Limited quantity available, brand new, at 15/- each, Post Free.

931A. PHOTO-CELL MULTIPLIER AMPLIFIER UNIT COMPLETE. Incorporating 931A photo-cell, 2 valves type 6AC7, 6AG7, etc., etc. Can be adapted for use in window lighting, warning systems, locating foreign bodies in liquids, flaws in textiles, burglar alarms, circuit switching by relays, etc., etc. Panel size 9½ in. x 3½ in. Circuit diagram not available. Price 45/- complete, post free.

R.3515 I.F. STRIP. A complete I.F. Unit, comprising 6 SP61 I.F. Stages, tuned to 13.5 Mc/s., 1 EA50 diode detector, and 1 EF36 or EF39 output or video stage. A few modifications only are required to adapt this unit, which will give pictures of extremely good quality. Price, complete with valves, and foolproof modification instructions, is 45/-, plus 5/- carriage and packing. Limited quantity only.

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R.C.A. ET-4336B COMMUNICATIONS TRANSMITTER, 2-20 mcs. Height 57 in., width 17 in., depth 24 in., 9 valves: 4/866, 2/805, 2/813, 1/807. New. Comprehensive booklet and photographs available on loan against deposit of £1 returnable. Crated and carriage paid, £60 each.

Q MAX B4/40 TRANSMITTER. Listed £75. Shop-soiled only £50. Full details on request.

AR88 LF. Equal to brand-new, £45. Crated and carr. paid.

1155 RECEIVERS. Brand-new, in transit cases, complete with valves. Without a blemish. Aerial tested, £9/10/-, plus 7/6 carriage.

R107. The well-known Army Communications receiver. Few only, £12/10/-, carr. paid.

CANADIAN NO. 58 TRANS/RECEIVERS, 33-50 metres, complete with mikes, phones and 2 batteries (1 spare). Each complete unit, 10 gns. Guaranteed brand-new.

1155 POWER PACK AND OUTPUT STAGE (U50 and KT61) to "Wireless World" specification, in neat black crackle case size 12 in. x 8 in. x 5 in., with 5 in. L.S. built in. Just plug into 1155 and set is instantly all A.C. operated without any modifications. Price £5/19/6, plus 3/6 carriage.

TANNOY AMPLIFIERS. Rack type audio amplifiers fitted with 10 valves: 4/163, 4/KT66, 2/U18. Used ex-Govt., but fine condition, £6/10/- . Without valves, £3. 6ft. rack free of charge to purchasers of 4 amplifiers with valves. This is a unique offer.

TELEVISION PRE-AMPLIFIERS. Makes a blur into a clear picture. Really sensitive. Fitted with EF50. Very compact. Power requirements 6-3 v. L.T. and 200/250 H.T. Ready for instant use. No modifications. State for London or Birmingham. Price 15/-, plus 1/- post and packing. A snip.

TU6B Tuning Units, 3000, 4500 kc/s, less outer case. New condition, 10/-, carriage 1/6.

BC306 Aerial Tuning Units, ceramic switch, slow-motion drive, etc. Size 16 in. x 8 in. x 8 in. Brand-new in cartons. The last few dozen. 10/- each, carriage 1/6.

12-volt Car Radio. Comprises an ex-Govt. 6-valve Command receiver expertly modified to tune medium wave band. Complete with separate 5 in. loudspeaker. Excellent performance (definitely not available for 6 volts), price £5/10/-, carr. paid.

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PAMPHONIC PA LOUSPEAKERS. 10 in. high flux unit. Handsome, Maroon Cellulose, Metal Cabinet, 20 x 9 x 13 in. Impedance 3 ohms. Brand-new. In cartons. Not surplus. Less than half price, 55/-, carr. paid.

Command Receiver Triple Controllers. Brand-new, in cartons, 8/6, post paid.

Medium Wave Coils for converting BC453/4/5 to MW., 10/- each. State which required. Tuning spindle and knob for same, 2/6. EF50 ceramic valve holders, 5/- doz. (minimum). Morse keys, new, ex-Govt., brass, fine job, 3/6, post 6d.

AMPLION CRYSTAL PICK-UPS, brand-new, in cartons, 26/9, post paid. Type 25 receiver, with 6-6 v. valves, 22/6, carr. paid. NEW.

CONDENSERS, waxed tubular. 50 for 10/-, 25 of .1 1000 v. and 25 of .25 mfd. 500 v.

Lexington Junior Moving Coil Pick-up. One only 70/-, post paid. All offers subject to goods being unsold.

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COMMUNICATIONS RECEIVER TYPE R1155.

This famous receiver needs no description, but for those not familiar with the set we can supply full circuit details, etc., for 9d. post free. All sets are air-tested before despatch and are supplied complete with 10 valves. We will gladly demonstrate any set to callers. Brand new, £9/10/0, or despatched in maker's transit case for £9/19/6, carriage paid. A.C. mains power pack and output stage for R1155 receiver enables this receiver to be operated direct from A.C. mains. Just plug in! Price £3/10/0, carriage paid.

MEDIUM WAVE COMMAND RECEIVER.

Frequency range 200-600 metres. Valve line up: 12SK7 R.F., 12K8 F.C., 12SK7 I.F., 12SK7 I.F., 12SR7 Det. B.F.O. and 12A6 output (all metal valves). Needs only 50 k. pot. for volume control purposes to be fitted and ten minutes work and receiver is all ready for operation as either a car radio or domestic radio. Note: this receiver is the original medium-wave set with the correct I.F. for the job and not a bodged-up conversion. Unused and in excellent condition, only £3/19/6. Circuit details supplied free with set.

RECEIVER TYPE 18.

A four valve battery superhet receiver. Uses standard iron-cored 465 kc/s. I.F. transformers. Complete with all valves. Frequency range 6-9 mc/s. Circuit diagram provided. Brand new. Only 17/6.

RECEIVER TYPE 1147B.

A 7-valve UHF receiver, range approx. 200 meg. Particularly suitable for conversion to 144 mc/s. Valve line-up: two EF50, two EF36 and one each of EBC33, RL7, RL16. This receiver is beautifully constructed and fitted with micro-condenser drive. Contained in black metal case size 8 x 7 x 6 in. BRAND NEW IN USEFUL TRANSIT CASE which might have been designed as a tool box! ONLY 30/-, carriage paid.

RECEIVER UNIT 25/73 (TR1196).

Valve line-up: two EF36, two EF39, one EK32 and one EBC33. Easily and rapidly converted to a very fine superhet receiver. (See "Practical Wireless" August 1949.) Supplied complete with circuit and conversion data. In very good condition indeed and offered at 22/6, post paid.

RECEIVER UNIT TYPE 6.

Housed in case size 10 x 8 x 7 in. Frequency range 3-7 mc/s. Valve line-up: five of EF50, and one each of EBC33, and EF36. The dial is exceptionally well geared and calibrated. Slightly soiled condition externally but perfect inside 29/6. Callers only.

R1355 RECEIVER.

New, but slightly store soiled. 49/6, plus 5/- carriage.

45 MC/S PYE STRIP.

A ready made vision receiver! (London frequency). Uses six EF50 and one EA50. Complete circuit data provided. All brand new. Less valves, 39/6, with valves 62/6.

MODULATOR TYPE 67.

This unit is essentially a heavy duty mains power pack for 230 volts A.C., 50 cps. operation. It contains a heavy duty mains transformer with two 6.3 volt outputs, 5 volts and the H.T. is 345-0-345 volts. Heavy duty choke appropriate smoothing condensers, rectifier, etc. In addition there are sundry SP61's, etc., which we haven't listed. Don't miss this bargain at only 52/6, plus 5/- carriage.

WIRELESS SET NO. 48. Transmitter/Receiver.

Brand new ex-U.S.A. equipment. Frequency coverage 6-9 mc/s. A complete station. All brand new in six cartons. Comprises 1 transmitter/receiver type 48, complete in case, with ten valves and one 1-mc/s. crystal. Two satchels, one ground aerial, spare valve case, complete with ten spare valves, one key assembly, one hand microphone, two headsets, one hand generator together with mounting tripod, two battery boxes and all necessary interconnecting cables and comprehensive instruction manual. Special offer for one month only at less than scrap price. Only £9/19/6, plus 10/- carriage. Inland only. Extra for Eire and Overseas.

BRAND NEW AMERICAN MADE 19 SETS.

This is a transmitter/receiver covering 2-8 mc/s. on phone, C/W. and MC/W. It also comprises UHF transmitter/receiver and an intercomm. amplifier. Supplied complete with 15 valves. Only £15, plus 10/- carriage.

INDICATOR UNIT 116H.

Brand new and contained in manufacturers original wooden crates. A more up-to-date version of the famous 6A. The contents include VCR97 tube, four EF50, three EB34 and innumerable other useful components. Price only 79/6, plus 7/6 carriage and packing.

RECEIVER TYPE 21.

A battery operated superhet receiver covering 4.2-7.5 Mcs. and 19-31 Mcs. Operates as a double superhet on the 10 metre band. Complete with nine 2 v. valves. Circuit diagram supplied. In new condition. 45/- carriage paid.

6 V. VIBRATOR PACK.

Suitable for use with the above set. With circuit diagram. Output 150 v. at 40 mA fully smoothed and rectified. Only 17/6 post free.

ADMIRALTY RECEIVER B36 OR B21.

A superb communications receiver made by Marconi's Wireless Telegraph Company. Valve line-up: two R.F. stages, freq. changer, three I.F. stages, double diode triode, BFO and output pentode. Freq. coverage 1-20 Mc/s. (15-300 metres) in 4 unbroken bands via turret coil change. "S" meter and valve check meter incorporated. Sensitivity for 10 db signal to noise ratio—better than 1 microvolt! Filament transformer for 230 v. AC operation is included but the H.T. supply is required. Necessary valves are: International Octal types two of KTW61, two of X65, three of KTW63, one of DH63 and a KT63. In new and unused condition. Complete with circuit diagram. Supplied less valves. £12/10/-, carriage paid. Only 20 of these high grade receivers in stock. First come first served!

INDICATOR UNIT 62A.

Contains twelve EF50, four of SP61 (CV118), two of EB34, three of EA50, 13 pots and a VCR97 tube. The finest Indicator Unit of them all. Unused condition but chassis slightly soiled. Offered to callers only. Price £4/19/6.

LOUDSPEAKERS.

Plessey 10in. p.m. type. ALNI magnet. Suitable for T.V. Brand new and boxed. Only 17/6 post paid.

MICROPHONES.

M.C. microphone by Vitavox. With on/off switch. 30 ohm impedance. Brand new and boxed. 30/- post paid.

LOOK! Marconi/Ekco Signal Generators type TF114G. Marconi/Ekco valve voltmeters. Call for details.

HEAVY DUTY 6 V. ACCUMULATORS.

Size 12 x 9 x 7 in. Brand new. Capacity 85 ampere hours. In teak case. Only 59/6. Exceptional value.

METAL RECTIFIERS.

Selenium full wave bridge 12 v. 5 amp., 15/- each.

MAINS TRANSFORMERS.

350-0-350 volts 80 m/a., 6.3 v. tapped 4 v. at 3 amps., 5 v. tapped 4 v. at 2 amps. Top chassis mounting. Fully guaranteed. 18/6, plus 9d. postage.

250-0-250 volts, 130 m/a., 6.3 v. at 6 amps., 5 v. at 3 amps. Fully shrouded top chassis mounting. A quality job. Guaranteed. 27/6.

E.H.T. Transformer for VCR97 or VCR517 tubes. 2,000 volts, 4 v. for tube heater and 4 v. tapped at 2 v. for E.H.T. rectifier. 30/- All the above transformers have standard primaries, 200/250 volts 50 cycles.

SPECIAL OFFER.

Mansbridge condensers. 4 mfd. 750 v. wkg. All brand new. Six for 10/6, post paid.

SPECIAL BARGAIN FOR CALLERS. UHF RECEIVER TYPE 1481.

Frequency range 65-86 mc/s, 6 in. slow motion drive, 11 of 6.3 v. valves as follows: four of EF39, one of EK32, four of SP61, one of P61, one of EB34. I.F. is 12 mc/s. B.F.O. etc. Brand new with circuit. £3/10/0.

Full range of valves, C.R. tubes, components, etc., at very attractive prices. Many, many bargains for the caller. Large quantities of resistors, condensers, valves, etc., for EXPORT AND TRADE DISPOSAL.

THE "EASYBUILT" TELEVISOR

COMPLETE DETAILS OF A FULL SIZE MAGNETIC TELEVISOR IN BOOK FORM. DETAILED INSTRUCTIONS, WIRING DIAGRAMS, ETC., A MINE OF INFORMATION FOR ONLY 2/6, POST FREE.

Inexpensive Television data booklet No. 4. Fully revised and brought up to date. Describes the 45 mc/s. "Pye" strip as well as the R1355 and other well-known government surplus units. Only 2/6, post free.



CHARLES BRITAIN (Radio) Ltd.

11, UPPER SAINT MARTIN'S LANE,
LONDON, W.C.2 TEM 0545

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Shop Hours: 9-6 p.m. (9-1 p.m. Thursday). Open all day Saturday



FROM EVERY POINT OF VIEW —A VAST IMPROVEMENT

The Magnavista Lens is not just a "magnifier"; it is an optical instrument, designed by optical scientists. For perfect clarity, and to avoid distortion, different receivers need different lenses. There is a Magnavista Model specially designed for your set. Here is real television progress which you can see for yourself.

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NEW

R.C.A. TELEGRAPH AND TELEPHONE COMMUNICATIONS TRANSMITTERS TYPE ET. 4336.

Designed and produced by the Radio Corporation of America, the Type ET.4336 is outstanding in the exceptional quality of construction, versatile operation with rapid band selection and adjustment, and the embodiment of modern advantageous features not generally found together in one equipment. The transmitter is designed for communications service in the high frequency range of 2,200 to 20,000 kilocycles, and any desired operating frequency within this range may be quickly selected, using ordinary crystals. All controls employed in tuning the transmitter to any frequency within the overall range are mounted upon the front panel. Shift from telegraph to telephone operation is switch controlled, and high speed keying is permissible. Two transmission power levels of 250 or 350 watts are available, however the actual outputs obtained are somewhat in excess of these values at 20 mc/s, and increase with decreasing frequency to values in excess of 300 and 450 watts respectively at 3 mc/s.

GENERAL FEATURES.

The complete transmitter is housed in a tall console cabinet, superbly finished, and has a very attractive appearance. Side and rear panels are removeable, and electrical interlocks are fitted as a safety feature. Stylish panel controls are conveniently grouped, and clearly identified. Five Meters are employed to read Aerial, Plate and Grid currents, and Filament voltages. A modulation and keying indicator of the vapour column type is mounted on the front panel. The Type MI-19468 Crystal Multiplier, which we supply with the transmitter, slides into an aperture which is normally concealed by a removeable panel. When employing this unit, the oscillator stage in the transmitter functions as an intermediate P.A. stage, or frequency multiplier, and whilst employment is optional, transmission over the entire transmitter frequency range, using low frequency crystals, is a distinct operational advantage.

CIRCUITRY.

Valves Type 807 are employed in the Crystal Multiplier Unit and the Transmitter Crystal Controlled Oscillator. The Power Amplifier stage utilizes two Valves Type 813 operating in parallel, and the Modulator stage uses two Valves Type 805 operated in a Class B arrangement. Plate and screen voltages for all stages are obtained from a mercury-vapour rectifier comprising four Valves Type 866A, connected in a full-wave parallel circuit. An Antenna Coupling and Matching system is provided, and is so designed to allow the use of various feeder arrangements.

ELECTRICAL CHARACTERISTICS.

Type of Modulation ...	Class B, high level,
Audio-Input Impedance ...	500 ohms.
Audio-Input Level for 100 per cent. Modulation ...	20 vu.
A-F Resonance ...	±5 db from 400 to 7,500 cycles.
A-F Harmonic Distortion ...	5 per cent r.m.s.
Power Input :	
Telegraph, Low Power ...	1.25 kW.
Telegraph, High Power ...	1.46 kW.
Telephone, 100 per cent Modulation ...	1.82 kW.
Power Supply Requirements ...	115-230 v., 1 phase, 50-60 cycles.
Regulation (Maximum) ...	5 per cent.

DIMENSIONS. Height, 58in. Width, 17in. Depth, 24in.

WEIGHT. 500 lb.

CONDITION. New and perfect, as ex-factory. Our Guarantee and Individual Test Certificate is supplied with each transmitter.

We offer immediate delivery of the above equipment to home and overseas buyers; complete and with all valves, at an exceptionally low price. Full specification and further particulars are promptly available on request.

LAWRENCES

61, BYROM STREET, LIVERPOOL, 3.

Telephone : CENTRAL 4430.

Experienced Export Shippers.

A GUARANTEE OF SATISFACTION WITH EVERYTHING WE SELL.



Moving Coil Speakers. All new 2/3 ohms P.M.: 3in., 1 1/8"; Rola 16 8; 4in. 18/-; 5in. 10/- (with Trans. 14/6); 4 1/2in. 11/6; 5in. 12/6; 6in. 12/6; 7in. 12/6; 8in. 12/6; 10in. 22/6; 12in. Rola 39/6 and Celestion 75/-.

Potentiometers. New Centralab: 2K, 5K, 10K, 25K, 50K, 100K, 1, 1 and 2 meg., less switch, 3/9, with switch 6/-. Midget Type 2/6. Midget with switch, 1, 1 and 2 meg., 6/-.

Surplus Potentiometers. All standard size with extended spindles: 5K, 10K, 15K, 20K, 26K, 50K, 100K, 250K 500K, 750K, 1 meg. 2/6 each.

Coils. Denco Maxi "Q" High "Q" with miniature size Poly Styrene Formers with adjustable Iron Dust Cores. Aerial, H.F., or Oscillator for 465 kc or 1.6 mc. Range covers all wavebands from 3.6 to 2,000 metres. Wiring diagram. Prices: Chassis Mounting, 3/9 (with Rect. 4/9) Octal fitting pin base, 4/- (with Rect., 5/-). Denco T.R.F. Matched pair Medium and Long Waves, 6/6 pair. Weymouth T.R.F. Matched pair M. and L. Waves, 9/6 pair. Superhet Matched pair M. and L. Waves, 8/9 or 11/4 pair. All types Wessite "P" 1/4 dia., Iron Core, Aerial, H.F. or Osc., 3/6 each.

Electrolytic Condensars. B.E.C. Midget Can Tubular, 8 mfd. 450 v. (1 1/2in. x 1/2in. dia.), 2/6; 8.8 mfd. 450 v. (1 1/2in. x 1/2in. dia.), 4/-; 16.8 mfd. 450 v. (1 1/2in. x 1/2in. dia.), 3/2 mfd. 450 v., 5/-; 16.16 mfd. 450 v. (1 1/2in. x 1/2in. dia.), 4/6; Dablier "Drillite" Card Tubular, 4 mfd. 500 v., 3/6; 8 mfd. 500 v., 4/-; 16 mfd. 500 v. 5/6; B.I. Can, standard size, 8 mfd. 500 v., 3/6; 8.8 mfd. 500 v., 5/-; 16 mfd. 500 v., 4/3; 16.16 mfd. 500 v., 5/3; 32 mfd. 500 v., 5/-; All New Stock. Dablier mica. 001 mfd. 5,000 v., 2/6.

Denco E.F. Lines for accurately lining-up 465 kc./or 1.6 m.c./f. channels. Pre-tuned circuits, battery operated and completely self-contained. Price 42/- (incl. P.T.).

Coil Packs. Osmor Midget Coil Pack. Size 3 1/2in. x 2 1/2in. x 1 1/2in. covering 8. M. and L. Waves. Coils wound on Polystyrene Formers with adjustable Iron Cores, ensures efficient performance. Factory wired and aligned. Price, including full circuits for Superhet 483 kc. Unit, 33/- Plus 7/4 P.T. Weymouth Midget 3 1/2in. x 2 1/2in. x 1 1/2in. covering 8-M-L W/Bands, for 465 kc. employing Matched Iron Cores Coils on each W/Band. 42/10. Wessite Superhet Type 706 and 706, size 4 1/2in. x 3 1/2in. x 1 1/2in., covering two Short Wave and one Medium W/Band or 8-M-L Wavebands, 465 kc., employs Iron Cores Coils 37/10. All of the above Coil Packs include Switching, Padding and Trimmer Condensars.

Output Transformer—Stern's. Midget 1 1/2in. x 1 1/2in. x 1 1/2in. ratio 50-1, 3/9 (or ratio 90-1, 3/9). Stern's Multi-ratio (over 12 ratios, some C.T.), 5/6 watts 8/6. Stern's Heavy Duty Multi-ratio, all C/T, handled handles 13 watts and suits P.X.4s, 6L6s, etc., 29/6. Rola Multi-ratio, 5/6 watts, 10/6.

L.F. Chokes. Midget 10 henry 250 ohm 40 mA, 3/6; 20 henry 250 ohm 60 mA, 8/6; 30 henry 300 ohm 100 mA, 11/9; 5 henry 50 ohm 250 mA, 18/6; 20 henry 250 ohm 120 mA, 18/6; 9 henry 250 ohm 150 mA, 8/6.

Aluminium Chassis. Substantially made of gauge 16 S.W.G. with four sides, 7in. x 4in. x 2in., 3/3; 5in. x 5in. x 2 1/2in. 4/-; 10in. x 6in. x 2 1/2in. 4/11; 10in. x 8in. x 2 1/2in. 5/6; 12in. x 9in. x 2 1/2in. 6/8; 14in. x 9in. x 2 1/2in. 6/11; 16in. x 8in. x 2 1/2in. 7/3; 16in. x 8in. x 3 1/2in. 8/6.

I.F. Transformer, 465 kc. New well-known manufacturer's surplus 1/2in. x 1/2in. x 1 1/2in. Iron Core, 9/- each. Denco Iron Core, 465 kc./or 1.6 m.c./f. 1 1/2in. x 1 1/2in. x 3/16", 16/6 pair. Wessite Stand Cap, Tuned, 465 kc./or 1.6 m.c./f. New Surplus 465 kc./or 1.6 m.c./f. 4in x 1 1/2in. sq., 10/- pair.

Meter Resistors. Westinghouse 250 microamp., 11/6; 1 mA., 10/8; 5 mA., 4/9.

Selenium Rectifiers. H.T./H. wave. 250 v. 60 mA. 5/6; 250 v. 100 mA. 7/6; 250 v. 170 mA. 13/6.

F. Wess Bridge Rectifiers for Battery Charging or Models 2, 4 or 6 v., 1 1/2 amp., 7/6; 6 or 12 v. 1 1/2 amp., 11/6; 6 or 12 v. 3 amps., 19/6; 6 or 12 v. 5 amps., 23/-; 12 or 24 v. 3 amps., 23/-.

Variable Resistor to control charging (or model speed) up to 3 amps rating, 13/6. Suitable METER, 5/8.

Charger Transformers. Suitable for use with above Rectifiers. Each has input of 230 volts. Outputs (a) 24 volts tapped 16 v., 9 v. and 4 v. at 3 amps., 22/9; (b) 30 volts tapped 15 v. and 9 v. at 3 amps., 22/9; (c) 15 volts tapped 9 v. at 3 amps., 18/6; (d) 12 volts, 1 1/2 amps., 11/3; (e) 15 volts tapped 9 v. at 6 amps., 21/6; 15 volts tapped 9 v. at 1 1/2 amps., 13/6. A Battery Charger Wiring Diagram is included with purchase of Charger Transformer and Rectifier.

NEW SURPLUS ! ! FOSTER TRANSFORMERS. PRIMARY 230 VOLTS. SECONDARY 12 VOLTS, 9 AMPS. 21/-.

Filament Transformer. Inputs 230 volts, outputs 6.3 v. 1 1/2 amp., 8/3; 4 v. 1 1/2 amp., 7/6; Input 200/250 v., output 4 v. (C.T.) 1 1/2 amp., 4 v. 2 amp., 6.3 v. 2 amp., 19/6. Input 230 v., output 6.3 v. (C.T.) 4 amp. 18/6.

Westinghouse Rectifiers. (a) H.T.51. Rated 350-0-350 volts 100 mA., 35/-; (b) H.T.52. Rated 350-0-350 v., 200 mA., 37/6; (c) H.T.53. Rated 500-0-500 v., 200 mA., 50/-; (d) Type 18H.T.56, 17/9; (e) Type 36E, H.T.25, 11/9; (f) Type 36E, H.T.35, Rated 2.5 kV., 1 mA., 17/6; (g) Type 36E, H.T.100, Pulse rating 5/6kV., 28/8.

Mains Transformers. All New Stock with Primaries tapped for 200-250 volts. Secondaries: (a) 250-0-250 volt, 80 mA., 6.3 v. (Tapped 4 v.) 4 amp and 6 v. (Tapped 4 v.) 2 amp., 18/6 (also available with 350-0-350 volt at 15/6). (b) Stern's 350-0-350 volt, 150 mA., 6.3 v. (Tapped 4 v.) 4 amp. and 5 v. (Tapped 4 v.) 2 amp., 38/6; (c) 350-0-350 v. 250 mA., 4 volt, 8 amp., 4 v. 3 amp. (Tapped 2 v.), 2 amp., and 6.3 v. 6 amp., 72/6, and many to other ratings.

Heater Auto Transformers: (a) Tapped 2v., 4 v., 5 v., and 6.3 volts 3 amp., 9/6; (b) 4 v., 3 amp. to 5 v. 2 amp. Reversible 6/-; (c) 4 v. 3 amp. to 6.3 v. 2 amp. Reversible, 6/-.

Power Potentiometers. Buign adjustable slider type, max. 6 ohms 60 watt, or 14 ohms 60 watt, 13/6 each. Ex-Govt. Rotary Adjustable 50 ohms 60 watt 5/9.

A 4 Station Pre-set Tuner. A complete self-contained unit from which any 3 Medium W/Band and 1 Long W/Band Stations may be pre-selected, and then individually selected by turn of Rotary Switch. No Tuning Condenser required, only 4 connections are necessary, price 40/-.

Adjustable Mains Droppers. 1 1/2in. dia. x 2 1/2in.: (a) .15 amp., 1500 ohms, 5/-; (b) 2 amp., 1,000 ohms, 4/-; (c) 3 amp., 600 ohms, 5/-.

6 Volt Vibrator Transformers, secondary 300-0-300 volts, 55 mA., 8/6.

KITS OF PARTS AND CONSTRUCTORS ASSEMBLY OUTFITS

"MAINS or BATTERY PERSONAL KIT"

A complete KIT OF PARTS to build our new MIDGET 4-VALVE SUPERHET PERSONAL SET, covering MEDIUM and LONG WAVES and designed for MAINS or BATTERY operation is now available.

This 2 Waveband Superhet Receiver is designed to operate on A.C. mains 200/240 volts, or by an "All-Dry" Battery, either method being selected by means of a Rotary Switch. It is so designed that the Mains Section (size 4 1/2in. x 3 1/2in.) is supplied as a separate kit, which may be added at any time. The kit therefore can be supplied either as an "All-Dry" Battery Personal Set, or as a Midget Receiver for combined Battery/Mains operation.

The circuit incorporates Delayed A.V.C. and Preselective Audio Feedback. A Rola 4in. P.M. Speaker with generous size Output Transformer ensures excellent quality reproduction. Ready Wound Frame Aerial, Fully aligned I.F. Transformers, and a Drilled Midget Chassis are included. Valve line up:—I.R.5 (F.C.), I.T.4 (I.F. Amp.), I.R.5 (Diode Det and Audio Amp.) and 3 B.4 (Output Tube).

The Set is quite easily built from the very detailed assembly instructions supplied, which include a practical component layout, with point to point wiring, and a circuit diagram for both the Set and the Mains Unit.

Price of COMPLETE KIT (less Mains Unit), £8/13/9. Price of COMPLETE MAINS UNIT KIT, £1/17/6. EVER READY Type B134 BATTERY, 9/7.

An attractive Walnut Finished Cabinet, size 9in. x 5 1/2in. x 5 1/2in., of the hinged lid type and suitable to house the combined set is available for 19/6.

THE COMPLETE ASSEMBLY INSTRUCTIONS mentioned above can be supplied separately for 1/9.

A Midget T.R.F. Battery Portable "Personal" Kit. A complete Kit of Parts to build a Midget 4-valve All-dry Battery Personal Set. Consists of Regenerative T.R.F. Circuit employing 8V Tuned Frame Aerial, with Denco Iron Dust Cores Coil, thereby ensuring maximum gain for Single-Tuned Stage covering Medium Waveband.

Valve line-up: IT4 (R.F. Ampl.), IT4 (Detector), 185 (1st A.F.), and 384 (output). Includes latest Rola 3in. Moving Coil Speaker, and a Chassis already drilled and shaped. A consumption of only 7 mA. ensures long battery life. The Kit is designed for a cabinet, minimum size 6in. x 4 1/2in. x 3in. Detailed Building Instructions, with Practical Layout and Circuit included with Kit make assembly easy. Price for Complete Kit, £3/18/9 (plus 16/7 P.T.). Suitable unpainted Cabinet 6in. x 4 1/2in. x 3in., 12/9. Ever Ready B114 Battery, 9/7. Building Instructions, Circuit, etc., supplied separately, 1/-.

A Complete Kit of Parts to build a Midget "All-Dry" Battery Eliminator, giving approx. 60 volts H.T. and 1.4 volts L.T. This Eliminator is suitable for a Personal Set, requiring H.T. and L.T. voltages indicated above. The Kit is quite easily and quickly assembled and is housed in a Light Aluminium Case, size 4 1/2in. x 1 1/2in. x 3 1/2in. It

car therefore be accommodated inside most makes of Personal Sets. Price of Complete Kit, £1/17/6.

"Wireless World" Midget A.C. Mains 2-Valve Receiver. We can supply all the components, including valves and M/Coil Speaker to build this set as specified in the March issue at a total cost of £3/5/0. Reprint of detailed assembly instructions and circuit supplied separately for 8d.

"Wireless World" Midget A.C. Mains 3-Valve Receiver. Covering Long and Medium Wavebands. We can supply all the Components, including Drilled Chassis, Valves, Moving Coil Speaker, etc., to build this set, as specified in the Feb. issue, at a total cost of £4/10/0 including a reprint of the complete Assembly Instructions and Circuit (this is available separately for 9d.) and Practical Components Layout with "point-to-point" connections. An attractive Walnut Finished Cabinet is now available for this W/World 3-Valve Set at 21/-, or it can be supplied with a complete Dial and Drive Assembly which includes the latest Station Name Dial and Dial Escutcheon, and a Combined Switch/Volume Control to effect very slight modification. Inclusive price, 35/- (Dial and Drive Assembly with Switch/Vol. Control supplied separately for 14/-).

We can supply all the Components, including Valves, M/Coil Speaker, etc., to build a Midget A.C./D.C. Mains T.R.F. 3-Valve (Plus Metal Rectifier) Receiver as designed and specified by a popular Technical Magazine, at a total cost of £4/17/6. A reprint of the assembly instructions, and layout available for 9d.

An Entirely Complete 3-Valve Amplifier Kit of Parts. Operating on A.C. or D.C. mains 200-250 volts. Has an output of max. 4 watts, with valve line-up 25A6, 6J7 and U51. A matched 6in. Moving Coil Speaker is supplied. Price, including Wiring Diagrams 75/- (or less M/Coil Speaker, 59/6).

"ELECTRONIC" VALVE VOLTMETER. We can supply the COMPLETE KIT OF PARTS, including the Valve, Diode and Meter, etc., to build this instrument, as published in the January issue of 'Electronic Engineering', complete with a reprint of the wiring diagram and assembly instructions (supplied separately for 8d.) at a total cost of £3/15/-.

TELEVISION ! ! The "Viewmaster" Television assembly instructions showing Wiring Diagram and Practical Component Layout available for 5/-. We have the specified Components, including the T.C.C.—Buign—Morgan—W.B.—Westinghouse—Plessey—Colvins, etc., outside in stock. We can supply this Television by the individual stages (as published with the instructions) or by separate Components. Complete price details can be obtained on application.

THE "EAS BUILT" TELEVISION. Full constructional data now available in book form, showing Wiring Diagram, Practical Component Layout and "point-to-point" connections, make this one of the most suitable Televisions for the Home Constructor to build. The specified Components are all available at very reasonable prices, enabling the set to be completely built for approx. £20—£23 including Valves, but excluding C.R.T. Price of complete Manual 12/6.

★ Send 3d. stamp for our Comprehensive Stock List. When ordering please cover packing and postage.

STERN RADIO LTD, 109 and 115 FLEET STREET, E.C.4

Telephone: CENTRAL 5814 and 2280

UNSURPASSED PERFORMANCE

The new "RD Baby De-Luxe" amplifier is ideal where an output not exceeding 7.5 watts is required.

Performance Figures

Amplifier : Output, 5 watts with less than .5 per cent total harmonic distortion ● Frequency response ± 1 DB 30-20,000 cps. ● Multiple loops which employ a total of 24 DB feedback, and include all stages and output transformer ● Sensitivity .75 v. for 5 Watts output ● Hum 85 DB below 5 watts output ● Complete stability with inductive, resistive or capacitive load. ● "Woden" iron cored components employed throughout. Pre-amplifier : Sensitivity, pick-up 90 m/V, radio 425 m/V. ● Noiseless switched bass and treble controls, providing compensation for Decca, H.M.V., and L.P. record characteristics, ● Detachable, to operate at a distance from main amplifier.

Prices : Amplifier £10/10/-. Pre-amplifier £4.

The following firms in London now stock and demonstrate the "RD Baby De-Luxe" amplifier : Webb's Radio Ltd., The Gramophone Exchange Ltd., Tele-Radio (1943) Ltd.

Full details of the above units will gladly be forwarded on request

Trade enquiries invited

ROGERS DEVELOPMENTS CO.,

"RODEVCO HOUSE," 116 BLACKHEATH ROAD, GREENWICH, S.E.10

Telegrams: RODEVCO, GREEN, LONDON.

QUALITY SUPERHET

By courtesy of the General Electric Co. Ltd., Kingsway, London, we have pleasure in introducing a new pre-tuned superhet, as described in their technical publication TP4. This receiver is ideal for use with amplifiers such as the "Williamson"; where reception conditions are unfavourable to a "straight" type of receiver.

Outstanding Features

- Four pre-selected wavelengths. 3 medium. 1 long.
- Two positions of selectivity. Bandwidth 6 kc/s. and 16 kc/s.
- Very efficient 9 kc. whistle rejector, with approximately 40 DB rejection.
- Variable switched bass and treble controls.

Model RD/TP4 : to G.E.C. specification, including extra bass and treble positions for L.P. record characteristics. Ample gain for lightweight pick-ups. Very low overall distortion.

Price : £18. Purchase Tax : £4/4/-.

Model RD/TP4A : as RD/TP4 but not including tone controls and pick-up input.

Price : £14. Purchase Tax : £3/5/4.

All individual components for the above units available.

1 KW TELEGRAPH TRANSMITTERS. Two HF 300's output. Operation 3.5 mc to 16 mc.

HALLICRAFTERS BC £10's. Complete with speech amplifier, antenna tuning unit; exciter units and coils for all bands.

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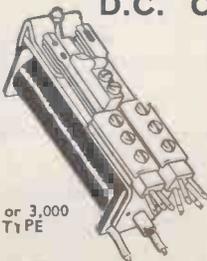
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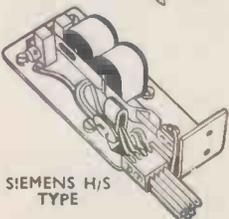
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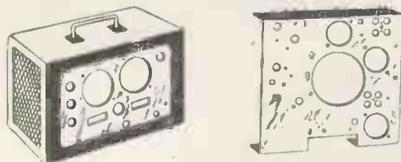
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Readers are warned that Government surplus components which may be offered for sale through our columns carry no manufacturers' guarantee. Many of these components will have been designed for special purposes making them unsuitable for civilian use, or may have deteriorated as a result of the conditions under which they have been stored. We cannot undertake to deal with any complaints regarding any such components purchased.

NEW RECEIVERS AND AMPLIFIERS

UNIVERSAL ELECTRONIC PRODUCTS, 36, Marylebone High St., London, W.1. Welbeck 4058

SPECIALISTS in the design and manufacture of high fidelity reproducing equipment from 5-100 watts for domestic or industrial purposes. Our new twin channel amplifier (type U.E.57), with independent bass and treble outputs, provides the most satisfying standard of reproduction we have yet experienced. It is now being demonstrated in our showrooms daily (we close Thursday 1 p.m., Saturday 4.30 p.m.), and we invite those who seek perfection from recorded music to hear this superb instrument. We also offer tuning units or complete chassis designed and constructed to individual requirements.

12-watt high quality amplifiers, bass and treble boost; £12/10; lists.—Broadcast & Acoustic Equipment Co., Ltd., Tombland, North. [0005]

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C.J.R. ELECTRICAL & ELECTRONIC DEVELOPMENT, Ltd., Hubert St., Birmingham, 6 (Aston Cross 2440) the Midlands specialist manufacturers of high fidelity sound reproduction equipment, for the world-famous Williamson amplifier and associated accessories including tone control stages, loudspeaker crossover units, distortionless contrast expanders and radio feeders; send for details and prices. [0105]

TELRAD ELECTRONICS, 70, Church Rd., Upper Norwood, London, S.E.19.—Designers and manufacturers of Telrad quality amplifiers; established as the most outstanding value in high-quality amplifiers, thanks to faithful reproduction at unrivalled price, these unique amplifiers are the first choice of the enthusiast; built to satisfy the discriminating ear; bass and treble independent controls, providing widest possible variation to suit all recordings and varying acoustic properties of one room with another; £18 complete; full details on request.—Write, call or phone Lytchstone 4879. [0019]

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RECEIVERS, AMPLIFIERS—SURPLUS AND SECONDHAND

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EDDYSTONE 358X, 150cc/s, 31mc/s, ex-W.D., £12/10, or nearest offer.—Box 7152.

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PHILIPS P.C.R. communication receiver, with ac power pack, £12.—31, Alexander Terrace, Douglas, I.O.M. [6139]

COMPLETE 30-watt amplifier, 4 K.T.6s in parallel push-pull switching for mic. gram. or radio, £18/10.—Mit., 316/10.—[6096]

SOUND sales 456 amplifier, P/P PX4bs, 5 watts 3 db, 20c-20kc; offers.—Waters, 152, Stifford Long Lane, Grays, Essex. [6020]

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Can be used for soldering aluminium, magnesium, duralumin and other metals which form refractory oxides.

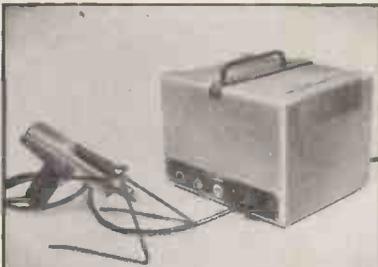


The soldering iron has a nickel silver bit driven by a magnetostriction transducer. The transducer is arranged to run at its natural resonant frequency by a feed-back system. A conventional low voltage winding heats the soldering bit.

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A small electronic amplifier supplies the ultrasonic power. There are no controls, apart from the mains switch, to operate. Unskilled workers can use the apparatus without discomf, since the ultrasonic frequency used is inaudible to the human ear. Full information about the Mullard Ultrasonic Soldering Iron—the only commercial model in the world—is available on request.



The Mullard Ultrasonic Soldering Iron and Amplifier. The unit operates from A.C. mains and is robustly made to suit workshop conditions.

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(M1340B)

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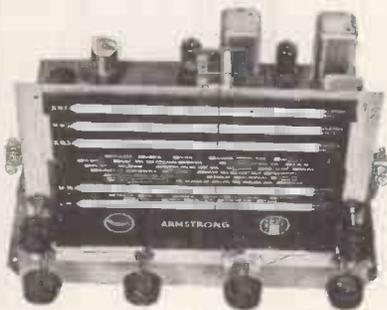
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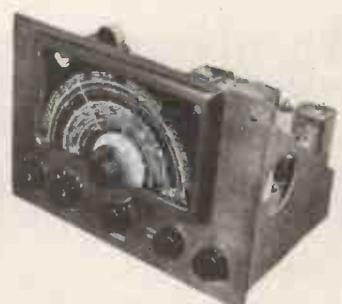
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425-0-425 v. 200 ma., 6.3 v. 4 v. 4 a. C.T., 6.3 v. 4 v. 4 a. C.T., 0-4-5 v. 3 a. ... 42/6
ELECTROLYTICS. 8 mfd. 450 v. Small Met. Tubes, 1/11 ea.; 16 mfd. 350 v. Small Cans, 2/3 ea., 18/6 doz.; 8-16 mfd. 450 v. Cans, 3/6 ea., 35/- doz.; 8-16-32 mfd. 450 v. Cans, 4/9 ea.; 50 mfd. 12 v., 8d.
SMOOTHING CHOKES. 40 ma. 10 h. 360 ohms, 3/3; 60 ma. 15 h. 400 ohms, 4/3 ea., 42/- doz.; 80 ma. 12 h. 350 ohms, 5/3 ea., 45/- doz.; 100 ma. 10 h. 100 ohms, 200 ma. 5 h. 100 ohms, 7/6 ea., 66/- doz.; 250 ma. 10 h. 100 ohms Potted, 11/9 ea.
OUTPUT TRANS. 6V6 to 2-3 ohms (Small), 1/11; Push-pull 10 w. 6V6, PX4, 6L6 to 3-5-8-15 ohms, 15/-. Williamson type, exact to author's spec., 63/-.
TERMS. C.V.O. or C.O.D. over £1. Post extra under £2. Full list 3d. Special List for Trade, 3d.

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DROP THROUGH TYPE. TO? SHROUD

(a) 250-0-250 v. 60 mA., 6.3 v. 3 a., 5 v. 2 a.	15/6
(b) 250-0-250 v. 60 mA., 4 v. 4 a., 4 v. 2 a.	15/6
Following types have Universal L.T. windings.	
6.3-4-0 v. 4 a. C.T., 5-4-0 v. 2 a.	
(c) 250-0-250 v. 80 mA.	17/6
(d) 300-0-300 v. 80 mA.	17/6
(e) 350-0-350 v. 80 mA.	17/6
(f) 250-0-250 v. 100 mA.	19/6
(g) 300-0-300 v. 100 mA.	19/6
(h) 350-0-350 v. 100 mA.	19/6

FULLY SHROUDED UPRIGHT TYPES

(i) 350-0-350 v. 150 mA., 6.3 4.0 v. 6 a. C.T., 5-4-0 v. 3 a.	39/-
(j) 425-0-425 v. 180 mA., 6.3 v. 4 a. C.T., 6.3 v. 4 a. C.T., 5 v. 3 a.	42/6
(k) 425-0-425 v. 180 mA., 4 v. 8 a. C.T., 4 v. 4 a. C.T., 4 v. 4 a.	44/6
(l) 425-0-425 v. 180 mA., 6.3 v. 4 a. C.T., 4 v. 2 a. C.T., 4 v. 2 a. C.T., 5 v. 3 a.	47/-

Note.—Model (j) above is suitable for Williamson Amplifier.

Williamson Pre-Amp Mains Transformer
325-0-325 v. 20 mA., 6.3 v. 6 a., 6.3 v. 1.9 a. ... 19/6

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Built to Author's specification 1.52 secondaries. Approved type ... £3 12 6

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High class radio feeder units with R.H. stage. Switched pick-up sockets. Glass scales. Completely aligned.
MODEL A. Covers 16/50, 190/50 and 900/2,000 metres. Price, including Purchase Tax, ... £10 8 6
MODEL B DE LUXE. Covers 43/145, 190/50, 900/2,000 metres and six ranges of band spread. Price, including Purchase Tax ... £18 7 6
MODEL E. As Model A, but with Variable Selectivity and infinite impedance detector. Price, including Purchase Tax £12 15 0

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POLISHED ALUMINIUM CHASSIS, 16 S.W.G., 4 SIDES, 3 in. DEEP

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Comprehensive range in enamelled cotton and alk covered copper wires from 16 S.W.G. to 40 S.W.G.
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PACKARD BELL PUSH-PULL PRE-AMPS. In sealed cartons with accessories and two valves, 6SL7 and 28D7 ... 16 6

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SITUATIONS VACANT

E.M.I. INSTITUTES.

PRINCIPAL: Professor H. F. Trewhman, M.A. (Cantab.), M.I.E.E., M.I.Mech.E., M.Brit.I.R.E. APPLICATIONS are invited for two full-time posts as lecturers in Electrical, Electronic and Telecommunications Engineering to students on two, three and four year courses. For one post applicants should have a good degree in Electrical Engineering, with Telecommunications. For the other post, a graduate Telecommunications Engineer is required, preferably with Post Office experience. Applicants for both posts should be under 30 years of age, and are required to possess industrial and good instructional experience.

THE commencing salary depends on experience and will be in the range of £450-£600 per annum.

APPLICATIONS, stating age, qualifications, and experience, with the names and addresses of three persons to whom reference may be made, should be sent, within fourteen days after the appearance of this advertisement, to The Principal, E.M.I. Institutes, Ltd., 10, Pembroke Square, London, W.2. [6057]

CROWN Agents for the Colonies.

RADIO Engineer (development) required by the Government of Fiji for one tour of three years in the first instance, for duties in connection with the installation and maintenance of small H.F. radio stations and the general planning of an enlarged radio-telephone network commencing salary according to qualifications and experience in the scale £P80 rise to £P960 a year (£F111—£100 sterling); free passages; gratuity on satisfactory completion of service at the rate of £P25 for each period of 3 months' service; candidates must have had 3 years' practical experience of installing and maintaining radio stations, administrative experience of the organisation required for operating a group of stations, and experience of international procedure and frequency allocation; a knowledge of the special requirements of meteorological and aeronautical radio services an advantage; apply at once by letter, stating age, full names in block letters, and full particulars of qualifications and experience, and mentioning this paper to the Crown Agents for the Colonies, 4, Millbank, London, S.W.1; quoting M/N/25777(3B) on both letter and envelope; the Crown Agents cannot undertake to acknowledge all applications and will communicate only with applicants selected for further consideration. [16000]

CROWN Agents for the Colonies.

RADIO Officer required by Nuerla Government Posts and Telegraphs Department (for aeronautical wireless stations) for one tour of 18-24 months in the first instance, with prospect of permanency; salary according to age and experience in scale £660-£850 a year (including gratuity), plus temporary allowance between £51 and £65 a year according to salary; outfit allowance £60; free passages; liberal leave. Candidates should preferably hold a Postmaster-General's Certificate in radio-telegraphy or an air operator's certificate, should have had a thorough grounding in I.C.A.O. codes and procedures, and recent experience in operating wireless and direction finding stations used for aeradio services. Experience in radio-telephone procedure and knowledge of manual V.H.F.D/F would be an advantage.—Apply at once by letter, stating age, full names in block letters, and full particulars of qualifications and experience and mentioning this paper to the Crown Agents for the Colonies, 4, Millbank, London, S.W.1; quoting M/N/25824(3B) on both letter and envelope. The Crown Agents cannot undertake to acknowledge all applications and will communicate only with applicants selected for further consideration. [16046]

YORKSHIRE ELECTRICITY BOARD.

RADIO and Television Assistants (Vacancy No. 59/50).—A Specialist Assistant is required for the Radio and Television Section in each of the Sub-Areas of the Board at Bradford, Huddersfield, Sheffield, Leeds, Wakefield, Hull and Grimsby. Salaries in accordance with the National Joint Council Agreement, Grade 5 £570/20/£630 per annum. Applicants must have had a sound training and experience in the maintenance and repair of various makes of radio and television sets and the duties will include supervision of the Sub-Area Radio Service Depots carrying out installation, repair and maintenance of apparatus, and will also include responsibility for the training of radio mechanics. The possession of a qualification will be an advantage. Applications, stating the above vacancy number, age, qualifications, experience, and indicating the Area to which they wish to be appointed, should be forwarded to the Secretary Yorkshire Electricity Board, Wetherby Road, Scarcroft, Leeds, within fourteen days of the appearance of this advertisement. [16074]

RADIO television engineer, first-class only; accommodation available.—Box 7036. [16140]

RADIO service assistant engineer; knowledge T.V. an advantage; write.—Robert Bennett, Ltd., 73, Stroud Green Rd., N.4. [16076]

RADIO service engineer required to take charge of workshop; television experience essential; able to drive; good prospects for right man.—Bruce Moore, 109, York Rd., West Hartlepool. [16040]

RADIO engineers, experienced, required for work on communication receivers, D.F. equipment, work in N. London or S.W. area of London; write giving particulars of experience. —Box 6961. [16097]

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The words "twin-units," "cross-over," "feed-back" exercise so magical a fascination these days that we feel it is not amiss to point out that the Barker patent drive is in fact the equivalent of a very efficient twin unit with its own built-in cross-over, plus an extremely high degree of self-adjusting feed-back found in no ordinary speakers, twin or otherwise.

Further, the Barker patent cone corrugations provide a smoothly varying effective cone area which radiates adequately over the full audio range. Nor does it exhibit any break in quality or space since its material and treatment are homogeneous and continuous.

These facts are well known to many hundreds of our friends who find constantly recurring pleasure in the way their Barker speakers bring out the essence of good performances, new experiences in music, speech, and even in noise!

Send now for details of the 148a and 150, twelve inch units, and the new 501 cabinets.

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SITUATIONS VACANT

WOOLWICH POLYTECHNIC, London, S.E.18.

THE Governing Body invite applications for the post of lecturer in the department of Physics and Telecommunications to teach chiefly electrical subjects to the standard of the Intermediate B.Sc. examination and the Higher National Certificate in Telecommunications. Candidates will be preferred who have a degree in physics and a knowledge of some branch of telecommunications, but a candidate with a suitable degree in electrical engineering will be considered.

BURNHAM technical scale salary £300-£15-£555 plus London allowance and graduate additions.

Starting salary according to industrial and teaching experience. Maximum possible is £708. FULL particulars of the post and application forms may be obtained from the Clerk to the Governors, to whom they should be returned within two weeks of the date of this advertisement.

HIS MAJESTY'S COLONIAL SERVICE—MALAYA.

A VACANCY exists for an Engineer in the Department of Broadcasting, Malaya, to install and manage broadcasting studios, recording channels, and transmitters on a salary scale of £460 to \$1,065 per month (equivalent to £644-£1,491 per annum). In addition a cost of living allowance is payable, and varies from £210 per annum for a single officer to a maximum of £525 for a married officer with children. Income tax is at a low rate. The appointment is permanent and pensionable but subject to a probationary period of 3 years. Free passages are provided for the officer, his wife and up to 3 children on appointment; and for the officer and his wife in respect of each tour, while assistance is given towards children's passages. Furnished quarters are provided if available, at rates varying from \$20.5 to \$71 per month (equivalent to just under £29-£100 per annum). Vacation leave will be granted at the rate of 4 days per month of resident service in a tour of duty. Free medical attention. CANDIDATES, between the ages of 23 and 35, should have an Engineering Degree, Graduate-ship of the Institute of Electrical Engineers or equivalent, and at least 2 years' general experience with an organization handling studio and transmitter equipment. The successful candidate will later be required to pass an examination in Malaya.

CANDIDATES should write for an application form, stating age, experience and qualifications, to the Director of Recruitment (Colonial Service) Colonial Office, Secretary, Great Smith Street, London, S.W.1. reference No. 27326/39. [6073]

SENIOR television engineer required for research dept. of McMichael Radio, Ltd.; applicants should write stating age, experience and salary required, to—Personnel Officer, Wexham Rd., Slough. [6015]

CAPABLE man of high intelligence and integrity as personal assistant to owner-manager of soundly established London retail radio business; state age and full details of career.—Box 6788. [6025]

TELEVISION testers and radio testers required for firm of radio manufacturers; top rates, plus bonus; good conditions and prospects.—Apply, Hale Electric Co., Ltd., Talbot Rd., West Ealing, W.13. [5999]

INTERNATIONAL company has vacancy for radio technician, South America; should have experience ground installation, maintenance navigational aids and good command Spanish.—Box 6782 [6007]

E. K. COLE LTD. (Malmesbury Division), invite applications from electronic engineers for permanent posts in development laboratories engaged on long-term projects involving the following techniques:—

1. PULSF generation and transmission.
2. SERVO mechanisms.
3. CENTIMETRIC and v.h.f. systems.
4. VIDEO and feedback amplifiers.
5. V.H.F. transmission and reception.

THERE are vacancies in the senior engineer, engineer and junior grades; candidates should have had at least 3 years' industrial experience in the above types of work, together with educational qualifications equivalent to A.M.I.E.E. examination standard; commencing salary and status will be commensurate with qualifications and experience; excellent opportunities for advancement are offered with entry into pension scheme after a period of service.—Forms of application may be obtained from Personnel Manager, Ekco Works, Malmesbury, Wilts. [5974]

PILOT RADIO, Ltd., requires immediately fault finders, testers and mechanical inspectors for radio and television alignment experienced in factory production, five-day week with good rates of pay. APPLY or write to:—Park Royal Rd., London N.W.10. [6179]

RADIO and electrical engineer, preferably single, aged 26/32, required by British Company trading Middle East; salary according experience, pension scheme, cost living allowance, etc.—Apply Box 6777 [5992]

ELECTRICAL inspector for mains and audio transformers test department. Previous similar experience essential. N.W. London. Write with full details of age and salaries earned to Personnel Manager Box 6792 [6038]

TESTERS for pre-production assembly; must be experienced in electronic and radar equipments and be able to work on own initiative with minimum supervision.—Apply giving full details, to the Personnel Manager, E.K. Cole, Ltd. (Development Department), Malmesbury, Wilts. [6085]

**SOLONS FOR YOUR
SOLDERING JOBS!**

Types available—65 watt oval tapered bit,
65 watt round pencil bit,
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125 watt round pencil bit,
240 watt oval tapered bit.



**HENLEY
SOLON**
ELECTRIC
SOLDERING IRONS

These five models will satisfy practically every soldering demand whether for the occasional household job or continuous soldering under workshop or factory conditions. With the Solon the heat is in the bit itself... continuously... hour after hour; all connections housed at end of handle away from heat. Each model complete with 6 feet Henley 3-core flexible. Now available from stock. Write for folder Y.10.

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Constructor's Envelopes (4/3 Post Free G.B.)

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TAPE MECHANISMS & RECORDERS SOON!
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The finest tuner unit in existence for quality reception (T.R.F. & Superhet) No complications in connecting to any well known amplifier.

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Lowther House, St. Mark's Road,
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Offer the following Clearance Lines:—

100 K/C Crystals, Bliley and R.C.A., 12/6 each. Selenium Rectifiers, full wave, 24 v. 4 amp., 25/- each; 12 v. 4 amp., 15/- Ex.-U.S. Tuning Units. Range C. and D. enclosed in Black Cracked Case 12in. x 9 1/2in. x 8 1/2in. with handles, 15/- each.

New Transformers. Input 220-240 volts. Output 350-0-350, 80 mA., 6.3 and 4 volt, 5 amp., 5 volt 2 amp., 16/- each.

Ferranti 0-500 Micro-Ammeters, 2 1/2in. Flush Type. New and Boxed, special offer, 16/6 each. Modulation Transformer, D a' in cut and Output 360 watts and 12 watts. Mktl tapped primary, totally enclosed, 7in. x 7in. x 7in. Weight 30 lb. 25/- each. Choke. 10 henry, 650 mA. Totally enclosed 7in. x 7in. x 7in. Weight 30 lb. 25/- each. Swinging Choke. 3.6 to 4.2 H., 250 mA. Totally enclosed 4 1/2in. x 3 1/2in. x 4in. Weight 7 1/2 lb. 7/6 each. American Loran Indicator. Lens Valves and Tube. Contains a host of components, including 24 Ceramic Valves, Holders, High Voltage Condensers, Switches, etc. 17/6.

Receiver Type 78. 5 Valve Superhet, with 100 k/c crystal, E.C.H.35, E.F.39, 6J5, VR91, VR92. Good condition. 35/- each.

Transformer, 230 volt, 50 cys. input. 115 volts, 500 v.A., 35/-.

Eddystone Power Unit. 200-250 volt, 50 cys. input, 300 v 200 mA D.C., 12.5 volts 3 amp. A.C. and 4 volt D.C. smoothed for microphone output. £2/5/0. Test Set.

Type 74. Input 230-250 volts, 50 cys. Tube 139R. Valves VR135, 5Z4, VU120, 6J5, 6Q7, 5VR, 65s. Good condition. Ideal for conversion to Scope. £3/5/0. Sperry Bomb Sight Computer, as advertised at £3/15/0. Brand new in transit case. Our price £2/10/0. A gift to the model maker.

All prices include Carriage or Post. Cash with Order and please write name clearly.

SITUATIONS VACANT

MINISTRY OF SUPPLY invites applications from electronic engineers and physicists for unestablished appointments in the Experimental Officer Class at Research and Development Establishments in the South Midlands.

CANDIDATES should possess at least Higher School Certificate or equivalent qualification, but special consideration would be given to applicants who have such additional qualifications as a full apprenticeship in light electrical engineering or electronics, or a degree in physics or electrical engineering; experience of radar or radio gained in the Services or in industry, of electronic techniques, particularly in the U.H.F. range or of wave development, would also be an advantage. **SALARY** according to age, qualifications and experience within ranges: Experimental Officer (min. age 28), £495-£645; Assistant Experimental Officer, £220-£460; rates for women somewhat lower.

APPLICATION forms obtainable from Ministry of Labour and National Service, Technical and Scientific Register (K), York House, Kingsway, London, W.C.2, quoting D.253/50-A. Closing date 14 days after date of appearance of this advertisement. [6090]

JUNIOR engineering and laboratory assistants with knowledge of radar or radio wanted for interesting work in Luton.—Graduates or ex-radar or radio mechanics should write giving full details mentioning ref. HAE to Box 6952. [6062]

ELECTRONIC engineers and physicists are invited by the Ministry of Supply to apply for unestablished appointments in the experimental officer class at Research and Development Establishments in and near London.

MINIMUM qualification Higher School Certificate; applications also invited from candidates holding Higher National Certificate in light engineering including electronics, or higher qualifications; experience in the following fields is desirable: electronic measurements in connection with field trials; radio and electronic circuitry; high speed electrical transients; electronic development; general experimental research requiring some mathematical facility. **SALARY** according to age, qualifications and experience within ranges: experimental officer (minimum age 28), £525-£675 (London); £495-£645 (provincial); assistant experimental officer £230-£490 (London); £200-£460 (provincial); rates for women somewhat lower.

APPLICATION forms obtainable from Ministry of Labour and National Service, Technical and Scientific Register (K), York House, Kingsway, W.C.2, quoting A.296/50-A. Closing date 14 days after the appearance of this advertisement. [6101]

ADMIRALTY invites applications for unestablished appointments as technical author in various naval establishments; the duties are to prepare technical publications and handbooks on electronic equipment used in H.M. ships.

THE posts will be graded in one or other of the ranges: £625-£750 or £500-£625 according to qualifications and experience; rates outside London will be a little lower. **CANDIDATES** should have had experience in the production, maintenance and/or operation of radio and radar equipment or electronic control systems; in addition, they should either have completed an engineering apprenticeship or equivalent training and possess technical knowledge to the standard of Higher or Ordinary National Certificate, or alternatively, have had extensive experience in one or other of the appropriate technical and specialist branches of the Royal Navy; preference will be given to those who have had previous experience in technical writing.

WRITE quoting D.49/50-A to Ministry of Labour and National Service, Technical and Scientific Register (K), York House, Kingsway, W.C.2, for application form which must be returned completed 14 days after appearance of this advertisement. [6114]

RADIO and television, experienced men required for the design, construction and/or operation of radio and television sets at present 35d per hour; N.J.I.C. conditions.—Apply Midlands Electricity Board, 31, Kingsway, Stoke-on-Trent. [5966]

ELECTRICAL engineers or physicists required with experience in the theory and practice of servo mechanisms and analogue computers for interesting new development work near London.—Apply, mentioning ref. DEF, to Box 6252. [5866]

TELEVISION/RADIO service engineer, fully qualified to be able to drive; permanent position with excellent opportunities; full particulars, references and salary required to W. J. F. Holt, Ltd., Howardsgate, Welwyn Garden City Herts. [5880]

RADIO engineer, able to drive, required by motor agents in west of London suburb; must have sound experience of car radio, electrical systems and mains wiring; write stating age, experience and wage required to—Box 6778. [5994]

SALES engineer required by the Edison Swan Electric Co., Ltd., 155, Charing Cross Rd., London, W.C.2, for department engaged in the sales of heavy duty thermionic valves. Technical qualifications essential. State also age and experience in detail. [6042]

YOUNG man, 21/22, required as service/sales engineer for London area by well-known manufacturer of industrial high frequency equipment; starting salary £400 per year and expenses; write stating if car owner or driver (not essential)—Box 6964. [6112]

QUALIFIED engineer or physicist required, with experience in design of electronic instruments; salary £550 or more according to age and experience.—Reply with full particulars to P.D. Research Division, A. C. Cossor, Ltd., 22, Highbury Grove, N.5. [6079]

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MANUFACTURERS' & BANKRUPT STOCKS LIMITED SUPPLIES ONLY

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Resistors 1/2, 1, 1 1/2, 2 and 3 watt. ALL VALUES

16 foot sectional aerial in Canvas carrying bag.

2 Volt Accumulator suitable for Radio or Model Driving, House Lighting, etc. Heavy Mass Type Plates. Pre-charged. Only need filling. Size: 7in. x 2in. x 2in.



Receivers: R1155, 1355 and 184 Brand New in original cases. Dinghy Radio Transmitter SCR 578.



Celluloid (R.A.F.) Portable 2 v. lead. Acid Accumulators 7 amp. H.R.S. Size: 3 1/2in. x 3 1/2in. x 1 1/2in.

Charging Control Boards with Auto-cut out, 3 amp. 220 v.

Magnifying Lens, Rubber Mask, Burgoyne Solder Guns, Bakelite Accumulators, Ex-Govt. S.W. Condensers. All types. Meters, Switches, Toggle and Yaxley. Headphones, L/R and H/R, Vibrators, 6 and 12 v. Speakers all types. Volume Controls. Output Transformers. Chokes. Crystals—Valves Type CV.101.

Storage Secondary Portable Canadian Hart Batteries, 6 v. 100/125 amp.

6 v. 125 amp "Globe" Car Batteries.

Brand New Accumulators 6 v. 85 a. Size: 12 x 9 x 7in. Weight 45 lb. British Made.

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OSCILLATOR UNIT. Constructed on small chassis suitable for sub-assembly, provides r.f. for erase and bias at 45 kc/s. Requires 250v. h.c. and 6.3v. for operation. Complete with 6V6 valve, £3/6.

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GENERAL assistant manager required specialising in radio and electrical departments in old-established music, radio and piano business; accommodation available.—Apply with full particulars and references to Morlings, Ltd., The House of Music, Lowestoft. [6022]

SALES engineer required by the Edison Swan Electric Co., Ltd., 155, Charing Cross Rd., London, W.C.2 for department engaged in the sales of electronic and light electrical instruments; technical qualifications essential. State also age and experience in detail. [6043]

E. K. COLE, Ltd., have vacancies for testors at their Electronics Division—experience in the testing of radar, communications or electronic equipments, to Ministry specifications, essential.—Full details in writing to the Personnel Manager, Malmesbury, Wilts. [5805]

FOREMAN for assembly of radio and electronic equipment in factory located South Wales; wide experience in Government contract work desirable; apply giving full details of experience to—Personnel Department, Murphy Radio, Ltd., Welwyn Garden City. [5983]

ASSISTANT metallurgist required for employment in Essex with knowledge of physical testing and heat treatment; age 24-30, and preferably in possession of at least H.N.C. in Metallurgy or L.I.M.—Apply, giving full details, mentioning reference HAD, to Box 6958. [6083]

TESTING engineers required for design and manufacture of apparatus for production testing of radar, communications and electronic equipment according to qualifications and experience.—Full details to the Personnel Manager, E. K. Cole, Ltd., Malmesbury, Wilts. [6037]

A WELL-KNOWN electrical manufacturing company in North London requires test foreman for large department producing wide range of h.f. and l.f. coils and transformers; good standard of technical knowledge required; state experience and salary required to "P.M." Box 6775. [5989]

DRAUGHTSMAN required for radio technical handbook work; ability to produce first-class diagrams from rough notes is essential; good prospects, permanency and superannuation scheme.—Apply, stating age, qualifications, experience and salary required, mentioning ref. ABC to Box 6793. [6039]

DESIGNER of mains and audio transformers required, experience of commercial design work necessary, must be able to produce full manufacturing and test specifications, interesting position; N.W. London area.—Write, stating experience, age and salaries earned, to Personnel Manager, Box 6791. [6037]

MECHANIC required for the construction and servicing of industrial electronic apparatus, maintenance of electro-mechanical transducers, etc.—West London area.—Forward details of education, experience and salary required to Box A.E.151, Central News, Ltd., 17, Moorgate, London, E.C.2. [6154]

REQUIRED for original and interesting design work on magnetic recorders, a design engineer capable of undertaking a complete project; location South Bucks; convenient for West London; reply stating qualifications, experience and salary required to Box No. M.1795, Haddons, Salisbury Sq., London, E.C.4. [6092]

RADIO engineers required; the General Electric Co., Ltd., are expanding their radio development laboratory at Coventry, and a number of vacancies for senior and junior engineers exist at present and a further considerable number of vacancies will occur during the next few months in the new laboratory.

APLICATIONS are invited from development engineers with experience of microwave radio or radar techniques who are capable of developing equipment and components to service specifications.

WRITE, quoting Ref. CHC.(3), to Personnel Officer, General Electric Co., Ltd., Radio & Television Works, Spion Kop, Coventry. [6079]

A TELEVISION receiver manufacturing company in the North West requires a chief engineer; only experienced engineers interested in the design and progressive development of a range of high quality receivers for quantity production need apply; write giving full details mentioning ref. DDG to—Box 6785. [6011]

A NUMBER of senior and junior vacancies for radio, radar, electronic, television etc., development, service engineers, draughtsmen, wiremen, testers, inspectors, etc., urgently required 30 television service engineers.—Write in confidence, Technical Employment Agency, 179, Clapham Rd., S.W.9. (Brixton 3437). [0103]

YOUNG men, with knowledge and experience of radio required by large manufacturer to fill certain vacancies in radio and television manufacture; applicants should have civilian or Forces radio experience and should possess adequate technical knowledge.—Kindly state full details of experience, with age, to Box 6782. [6024]

CHEMIST (aged 28/35) with good honours degree required for Industrial Research Laboratory at Chelmsford; familiarity with analytical techniques is looked for, particularly in metallurgy, together with good experience in the physical chemistry field.—Write, giving full particulars mentioning ref. HAJ, to Box 6951. [6060]

BELLING & LEE, Ltd., Cambridge Arterial Road, Enfield, Middlesex, have a vacancy for an assistant for television aerial research; applicants must hold a Grad. I.E.E. or equivalent qualifications and should preferably have had previous experience of V.H.F. aerial problems.—Apply in writing giving age, qualifications, and full details of experience and salary required. [6069]

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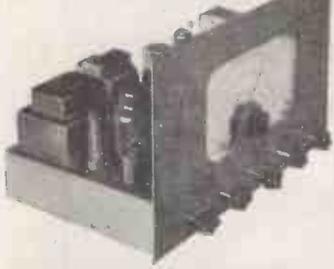
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SITUATIONS VACANT

RADIO engineer required by manufacturer's service department in North London area; applicants should give full details of education, which should not be below School Certificate Standard, technical training and experience, age and salary required to—Box No. 450, c/o Era Publicity, Ltd., 7 Fitzroy Square, London, W.1. [5995]

THE General Electric Co., Ltd., radio and television works, Coventry, have vacancies for senior-junior mechanical designers, design and detail draughtsmen accustomed to the design and layout of electronic apparatus. Applicants should state fully their experience, age and salary required to the Personnel Manager. [6127]

DRAUGHTSMEN.—Several vacancies exist in West London for mechanical and electrical draughtsmen and designers with well-known engineering group; experienced switchgear and electronic men are required, but men with sound mechanical or electrical D.O. experience will be considered.—Apply quoting ref. AAB to Box 6785. [6016]

PHYSICIST or electronic engineer required for the development of apparatus for physical measurements; preferably honours degree standard, or equivalent, with several years industrial experience; full particulars, age, qualifications, experience, salary required, etc.—Box A.E.94, c/o Central News, Ltd., 17 Moorgate, London, E.C.2. [6001]

CHARGE hand required for radio coll-winding section; must have had 2 1/2 years' experience; good prospects for keen young man capable of handling female labour; the ability to plan winding capacity, fix piece rates, etc., an advantage; pleasant working conditions; close to sea.—Weymouth Radio Manufacturing Co., Ltd., Weymouth. [6100]

DRAUGHTSMEN (electrical) with experience of schematic or detail wiring diagrams, are invited to apply for progressive positions in the Drawing Offices of the English Electric Co., Ltd., Liverpool.—Write, giving full particulars quoting ref. 140, to Central Personnel Services, English Electric Co., Ltd., 24-30, Gillingham Street, London, S.W.1. [6059]

YOUNG man aged about 20 (or less if not subject to National Service) required by progressive and well-known Croydon firm, to learn coll-winding, testing, etc.; intelligence and good practical knowledge of radio essential; write stating age, experience and salary required (5-day week)—Osmer Radio Products, Ltd., Borough Hill, Croydon. [6098]

E. K. COLE, Ltd., have vacancies in their electronics division at Malmesbury, Wilt., for senior and intermediate draughtsmen in the Development Drawing Office, for work on radar, communications and electronic projects; previous experience in this field desirable but not essential.—Apply in writing to the Personnel Manager, Ekco Works, Malmesbury, Wilt. [6086]

APPPOINTMENTS of two assistant foremen in the test department, will shortly be made; knowledge of electrical work essential, experience and technical standard of radio electrical work desirable, but not essential; 5-day week and all welfare conveniences.—Apply Personnel Superintendent, The Edison Swan Electric Co., Ltd., Cosmos Works, Brimsdown, Enfield. [6109]

ANORTH Midlands firm requires electronic engineers experienced in maintenance and design of electronic equipment, to work on the measurement of vibrations of engines, etc.; some mechanical knowledge, strength of materials, etc., an advantage; Higher National Certificate minimum qualification; salary £400 to £500 p.a., according to experience.—Box 5787. [6021]

ELECTRONIC development engineers.—Senior and junior electronic engineers required for design and development work on interesting new projects, degree or higher national certificate essential; good salary and excellent prospects, pension scheme.—State age, qualifications and experience to Personnel Manager, Falrey Aviation Co., Ltd., Hayes, Middlesex. [6050]

ELECTRICAL component manufacturers, situated in W. London, require intelligent person to take charge of special test section; applicants should possess either B.Sc. or equivalent, have previous experience of test and measuring equipment and be capable of maintaining accurate records.—Write, stating age, experience and salary required, to Box 6796. [6160]

SERVO engineers for experimental work are required by prominent central concern; applicants, preferably under 35 years of age, must be educated technically to degree standard and have experience in the design of one or more of the following: hydraulic systems, servo amplifiers, small electrical mechanisms.—Apply stating age, experience and salary required to Box 6954. [6068]

TECHNICAL assistant required by large firm in N.E. London suburb for experimental work in connection with the industrial application of electronics (di-electric heating, process control, etc.); applicants should have fulfilled liabilities under the National Service Act and have a good degree (or near equivalent) in electrical engineering or physics and some practical engineering or radio experience, a knowledge of radio frequency oscillators, transmission line theory and radio frequency measurement is essential; the post offers good scope, interest and experience; commencing salary will be in the region of £400 to £450 per annum according to qualification and experience; successful applicant would be required to join staff pension scheme.—Write giving full details of training and experience to Box 7156. [6174]

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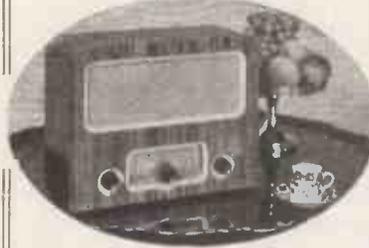
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ENGINEERS required for electrical design of radar apparatus and also for laboratory work in connection with radio and television. Applicants must have sound basic training, preferably a degree in physics and some experience in industrial design laboratories.—Write, stating age, experience and salary required, to Personnel Dept., Murphy Radio, Ltd., Welwyn Garden City, Herts. [6058]

UNIVERSITY COLLEGE, London, has a vacancy in the Department of Psychology for a Grade I technician; experience in construction and maintenance of electronic and electrical apparatus and metal work; salary scale £390-£415-£481; family allowance scheme.—Application forms from the Secretary, University College, London, Gower St., W.C.1, quoting 'S70009/2'. [6152]

WAYNE KERR have vacancies in their laboratory for a senior development engineer and a development engineer to undertake design and development work covering a wide field of electronic applications and measurements; applicants should apply in writing to—The Chief Development Engineer, Wayne Kerr Laboratories, Ltd., Sycamore Grove, New Malden, Surrey. [6120]

DEVELOPMENT engineer (electronics) required by old-established company, to be responsible for the design and development of specialized radar and electronic instruments; applicant should have good circuitry experience in time-base, pulse and C.R.T. techniques; preferably conversant with Service design requirements; state age, experience and salary expected.—Box 6965. [6113]

READAR, radio and/or electronics senior development engineer wanted for work on important defence project in special English Electric Co. laboratory; salary £600-£900 p.a. according to experience; write giving details of qualifications and previous experience to Personnel Services, English Electric Co., Ltd., 24/30, Gillingham St., London, S.W.1. [6105]

AN experienced valve design or production engineer required by the English Electric Valve Co., Ltd., at Chelmsford, aged 25-35, with previous experience on the manufacture of large receiving valves and small transmitting valves.—Apply giving full details and present salary, quoting reference 497A, to Central Personnel Services, English Electric Co., Ltd., 24-30, Gillingham St., London, S.W.1. [6095]

READAR technicians are required by a well-known firm of radio manufacturers for a factory in South Lancashire; experience in the service and/or installation of radar equipment essential; persons who have had experience in this type of work in the Services would be particularly suitable; good salaries, according to experience; write giving full details, mentioning Reference HAA to Box 6959. [6099]

MINISTRY OF SUPPLY invites applications from electronic engineers and physicists for unestablished appointments in the Scientific Officer and Experimental Officer Classes at the Royal Aircraft Establishment, Farnborough, particularly in the fields of radio communication, including microwave techniques, circuit design and measurements, servo mechanisms and measurement of flight parameters.

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APPLICATIONS obtainable from Ministry of Labour and National Service, Technical and Scientific Register (K), York House, Kingsway, W.C.2, quoting D.220/50-A. Closing date 14 days after the appearance of this advertisement. [6091]

DESIGN draughtsmen are required by Wayne Kerr for work covering a wide range of electronic applications, measurements and radio communications; applicants should have had several years of experience in this class of engineering; write giving full details of qualifications and experience to—The Senior Project Engineer, Wayne Kerr Laboratories, Ltd., Sycamore Grove, New Malden, Surrey. [6121]

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SITUATIONS VACANT
INTERNATIONAL AERADIO, Ltd., require immediate applications for appointment of radar specialist, Middle East, to take charge installation and training; experience required electronic ground and air radar equipment, in Chinese, American, Typ. 21, Eureka, Pass, Rebecca, I.F.F.; monthly salary £4,000; free state accommodation; passage free; free passage—Apply Personnel Officer, 40, Park St., W.1.

An experienced valve engineer is required for employment at Glemsford; applicants should be 25-35 years of age, qualified engineers and preference will be given to applicants with previous design or production experience of small transmitting valves; write giving full details of previous experience mentioning ref. 4918 to Central Personnel Services, English Electric Co., Ltd., 24-30, Gillingham St., London, S.W.1.

BELLING & LEE, Ltd., Cambridge, require a tele-communication service engineer aged 20/25, to be trained in the suppression of electrical interference and to handle the relative correspondence; applicants should possess City and Guilds certificates in Radio Communications 1 and Tech. Elect. 1, and must be prepared to work for finals; written applications to state age, experience and salary required. (599)

ENGLISH ELECTRIC require a technical representative for the Birmingham area; candidates should have good experience of industrial electronic equipment and be resident in the Birmingham area; previous commercial experience in this field is desirable; car provided; write giving full details of previous experience quoting ref. 5362 to Central Personnel Services, English Electric Co., Ltd., 24-30, Gillingham St., London, S.W.1. (5932)

URGENTLY required for employment in the Swindon area personnel experienced in the maintenance and repair of radar fire control equipment; salary £3,000 p.a. to £5,000 p.a.; opportunities for advancement; applicants must give full details of age, practical experience and technical qualifications held.—Replies quoting Swindon Vacancies should be addressed to D.M.M., 2 A.A. Group, Barossa Barracks, Aldershot, Hants. (6155)

THE General Electric Co., Ltd., radio and television works, Coventry, have vacancies for senior-junior development engineers for broadcast radio receivers, television receivers, H.F. and V.H.F. communication transmitters and receivers.—Applicants who should preferably be graduates of a university and experienced in one or more of the above fields should write stating age, experience and salary required to 16126 Personnel.

ELECTRONIC engineer; fully experienced electronic engineer required (grad. I.E.E. or equivalent qualifications) for work in a large Birmingham light engineering company; the work will be closely connected with laboratory work and development departments and will consist of all kinds of electronic apparatus; applicants should state age, experience, qualifications and salary required.—Box 6962. (6110)

MANAGER required to take charge and develop service department of home company trading in British Central Africa, handling radios, refrigerators, typewriters and sewing machines, etc.; sound electrical and radio knowledge essential; preliminary training will be given in other service requirements before departure; four years' contract with passage, housing, paid leave, etc.; good salary and prospects.—Address, 1,301, Wm. Porteous & Co., Glasgow. (6070)

REQUIRED, radio and radar superintendant preferred for British Shipping Company's Hong Kong Office, with first-class technical qualifications and experience, and good administrative capacity; starting pay £800 p.a. plus fluctuating high cost of living allowance (at present £360 p.a.), plus £20 married home leave; provident fund and pension scheme; excellent prospects for right man.—Reply giving full qualifications and references, to Box 6957. (6033)

HIGH frequency induction heating applications engineer required by progressive and expanding company specializing in the manufacture of high frequency equipment; experience in induction heating essential and a good knowledge of metallurgy would be considered as an additional qualification; the position offers excellent opportunities for advancement to a really energetic man having the requisite experience; write giving experience and salary required.—Box 7037. (6141)

American services equipment.—London firm of manufacturers, stockists and exporters of radio radar and signal equipment have vacancies for (a) radio-electrical engineer fully conversant U.S.A. Services radio, radar and signal equipment, required practice in installation, operation and maintenance; previous experience an advantage, excellent prospects for right applicant; (b) technical assistant to export director, familiar with American equipment.—Box 7149. (6157)

MARCONI'S WIRELESS TELEGRAPH Co., Ltd. require staff for their modern development laboratories at Chislehurst, Essex, to undertake important development work on interesting radar projects; qualified electrical engineers and physicists with experience of radar are required at various levels; there is also scope for young men without experience, including those who possess the highest academic attainments; where necessary a period of training will be given at the Marconi College.—Please send full details indicating present salary level, quoting Ref. 474, to Central Personnel Services English Electric Co., Ltd., 24-30, Gillingham St., London S.W.1. (5783)

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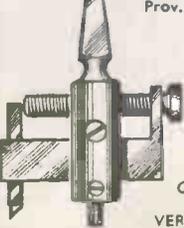
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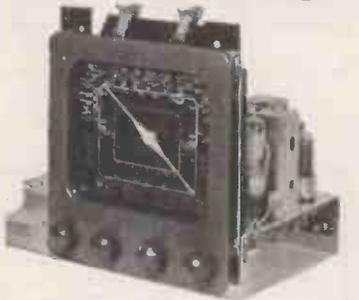
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SITUATIONS VACANT

REQUIRED at once, by the Plessey Co., Ilford, young engineers of British birth with several years' experience of radio communication, radar, or electronic development work; applicants should preferably have a degree in physics or engineering, but this qualification is not essential; the posts involve work on interesting long term development projects and are permanent and pensionable; please state full particulars with age and salary required to Personnel Manager. [6106]

MICHAEL RADIO, Ltd. require senior project engineers in their Equipment Division Development Laboratory at Slough; training and experience in the field of Applied Electronics (including communications) and experience of working with Government departments, are the chief qualifications required; salary will be commensurate with ability; write stating age and full details of training, qualifications and experience, to the Chief Engineer, Equipment Division, Michael Radio, Ltd., Slough, Bucks. [6080]

NELSON RESEARCH LABORATORIES, ENGLISH ELECTRIC Co., Ltd., Stafford, require draughtsmen for development work on vacuum devices, including industrial type electronic valves; must have flair for design of jigs and fixtures for assembly and processing of components and be familiar with modern shop techniques in this field; salary according to qualifications and experience.—Apply, mentioning reference 143A, to Central Personnel Services, 24-30, Gillingham St. London, S.W.1. [5881]

SEVERAL draughtsmen with electronic experience are required by an old-established firm at their research laboratories, Borehamwood; applicants must have experience of the design and detailing of modern electronic equipment; please state full details of experience, age and salary required; there are also several vacancies for juniors to train as electronic draughtsmen; an experienced electronic clerk (male) for office records and photo copying is also required, age 40-55 years.—Apply Box 6784. [6012]

ATTRACTIVE staff vacancies for draughtsmen exist at Chelmsford and in London with Marconi's Wireless Telegraph Co., Ltd.; continuing expansion of the company's work calls for increased D.O. output and electrical or mechanical draughtsmen are invited to apply for these permanent staff positions on the design and development of radio and radar equipment.—Write, giving full details, quoting reference 142A, to Central Personnel Services, English Electric Co., Ltd. 24-30, Gillingham St. London, S.W.1. [5769]

A NUMBER of senior radio development engineers are required by the Research Division of the Plessey Company to work on interesting long-term radio communication projects; candidates must be British-born, between the ages of 25-35, and should have some years' experience in the design of radio communication equipment; the posts are permanent and pensionable.—Apply to Plessey Co. Ltd., Ilford, giving full particulars of age, education and experience. All applications will be treated in confidence. [6075]

RESEARCH and Development engineer for work on electronic switching, control and computing apparatus required by N.W. London firm of repute manufacturing a variety of electrically controlled light mechanisms and extending their development in the electronics field; position offers good remuneration and permanency; candidates should have good theoretical background of wire and tape recording principles and a practical experience in development work. Kindly submit details of experience, age, salary required, etc., to Box 7035. [6137]

A VACANCY exists with a well-known radio engineering firm near London for a technical writer; duties will be to originate technical sales literature of all kinds, to deal with printers and typographers, and to liaise with design engineers within the company; experience gained would range over the company's many products and would be invaluable to a young engineer; applicants should have a good general knowledge of telecommunications, be between 21 and 30 years of age, and have an ability for this special kind of writing.—Apply giving full details, mentioning Ref. BGH to Box 7031. [6125]

A NUMBER of interesting vacancies have arisen for physicists and engineers for experimental and design work in research teams at the Research Laboratories of the General Electric Co., Ltd., East Lane, North Wembley, Middlesex. A variety of problems are being investigated and applications will be considered from men with both general and specialised training and experience in the fields of physics and light mechanical or electronic engineering. Details of openings will be sent to all selected candidates who send particulars of their qualifications and experience to the Personnel Officer (Ref. GBCL/35/4). Replies will be sent to all letters. [6027]

APPLICATIONS are invited by the Marconi's Wireless Telegraph Co., Ltd., for their post of project engineer in the broadcasting division; applicants should have a university degree in electrical engineering or equivalent qualifications and have had experience in the installation, operation and maintenance or design of transmitting or studio equipment; the successful candidate must be able to assist in the planning, organisation, co-ordination and control of the development, sales production, distribution and installation of all television equipment handled by the company.—Write, giving full details mentioning ref. 465, to Central Personnel Services, English Electric Co., Ltd., 24-30, Gillingham Street, London, S.W.1. [6051]

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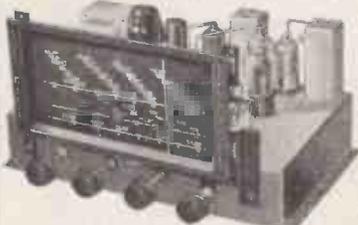
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SITUATIONS VACANT

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E.M.I. ENGINEERING DEVELOPMENT, Ltd. offer outstanding opportunities for experience in interesting development in many branches of electronic engineering, including radar, radio communication, television receivers, audio-frequency engineering and magnetic recording; applicants will be welcomed from men with engineering or physics degrees or the equivalent, with design experience; salaries according to age and experience.—Applicants should write, giving full details, to Personnel Department, E0/21, E.M.I. Engineering Development, Ltd., Blyth Pond, Hayes, Middx. [6081]

UNIVERSITY OF GASKOW requires, for work in the physiology department, a technician (grade A) with experience in building electronic devices; he will be required to construct to specification high-gain L.F. amplifiers, stabilised power supplies, time bases, etc.; a good standard of workmanship is expected; a knowledge of physiology is not essential, but a successful applicant would be expected to learn physiological laboratory technique; salary scale: £350.—Applications, showing experience and qualifications, should be sent to the Senior Administrative Assistant, The University, Glasgow, W.2, from whom further particulars may be obtained. [6054]

LABORATORY technician required for electroencephalography department of mental hospital; applicants should possess technical training in electronics and servicing of amplifiers; workshop practice essential; previous E.E.C. experience not essential. Preference will be given to graduateship of British Institution of Radio Engineers, Institute of Electrical Engineers, or equivalent qualification. Salary scale £370, rising by 4 increments to £435 p.a., plus London weighting allowance according to age.—Application forms, to be returned within 14 days of the appearance of this notice, from the Secretary, Institute of Psychiatry, Maudsley Hospital, S.E.5. [6045]

MARCONI'S WIRELESS TELEGRAPH Co., Ltd., have vacancies for two engineers for work on VHF development, applicants for the first post must have good practical knowledge and experience on VHF low power transmitters; for the second post experience on multiplex channelling audio and/or video is required; applicants must be familiar with problems on linearity, distortion, etc., and a knowledge of centimetric techniques would be an asset; salary will be not less than £650 per annum, and may be higher for candidates with outstanding qualifications and experience; the company has a staff pension fund.—Please apply giving full details, quoting Ref. 322, to Central Personnel Services, English Electric Co., Ltd., 24-30, Gillingham St., London, S.W.1. [6178]

ADMIRALTY—Vacancies exist for electrical and/or mechanical engineering draughtsmen in Admiralty research and development establishments located in the vicinity of Weymouth, Portsmouth, Teddington (Middlesex) and Baldoock, Herts. Draughtsmen experienced in light current, electro-mechanical, precision mechanical and electronic equipment are particularly needed. Candidates must be British subjects of 21 years of age and upwards, who have had practical workshop experience (preferably an apprenticeship) together with drawing office experience. Appointments will be in an unestablished capacity, but opportunities may occur for qualified staff to compete for established posts. The salaries offered, depending on age, experience, ability and place of duty, will be within the range £283-£510 p.a. Exceptionally well qualified candidates may be considered for appointment in a higher grade within the salary range £470-£610 p.a. Hostel accommodation is available at some establishments.

APPLICATIONS, stating age and details of technical qualifications and apprenticeship (or equivalents) and workshop and drawing office experience, should be sent to Admiralty (C.E.11, Room 89), Empire Hotel, Bath. Original testimonials should not be forwarded with application. Candidates required for interview (at London or Bath, whichever is nearest) will be advised within two weeks of receipt of application. [6134]

MARINE radar engineer required by major British oil company for service at a Middle East port; applicants must not be over 35 years of age, and must be Associate Members of the Institute of Electrical Engineers, or possess comparable academic qualifications, coupled with a wide knowledge and experience of post-war Mercantile Marine radar equipment; maintenance, general knowledge and some experience of marine radio communication systems would be an advantage; the successful applicant will be required to institute a small maintenance depot capable of offering emergency service to ships fitted with a variety of radar equipments; he would also be required, as a secondary commitment, to service marine radio communication systems, including V.H.F. radio telephone equipment; the post carries an attractive salary commensurate with the above, plus a generous allowance in the local currency; there is a pension scheme and terms and conditions of service are good.—Write, giving personal particulars and details of qualifications and experience, quoting Department F.205, to Box 2908 at 191, Gresham House, E.C.2. [5883]

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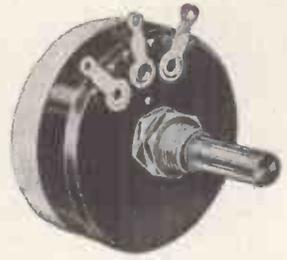
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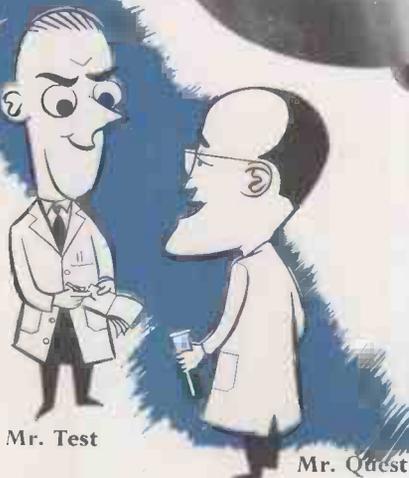
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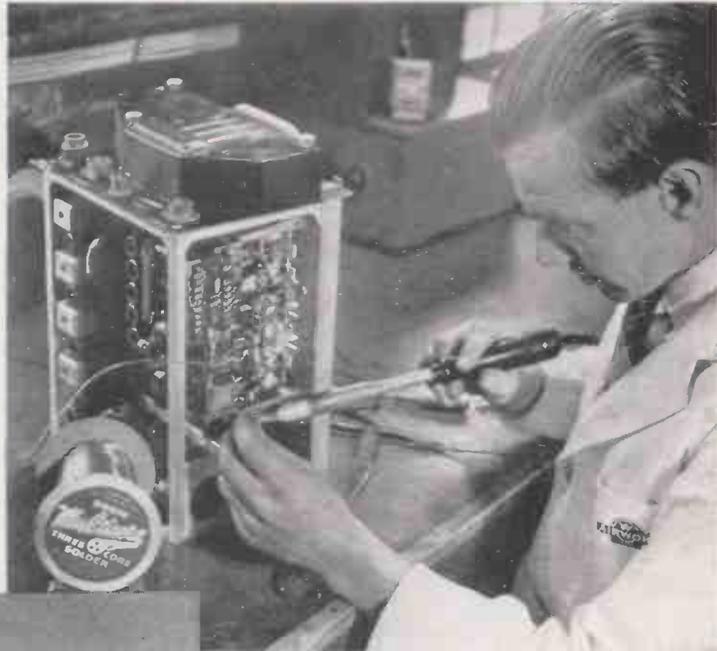
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