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RADIO, TELEVISION
AND ELECTRONICS
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41st YEAR OF PUBLICATION

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## VALVES...and their Applications

## R.F. VOLTAGE AMPLIFYING

INDIRECTLY-HEATED VALVES FOR BROADCAST RECEIVERS

The I.F. Stage

The I.F. stage requires a valve capable of providing a large gain with the desired bandwidth. It must give stable operation under all conditions, and its characteristics must be suitable for the application of A.V.C. A.V.C. must not, however, cause serious variations in the response curve of the stage, and the valve must be capable of handling input and ontput voltages over a wide range of signal levels without undue distortion. All these requirements are met by the Mullard EF41 and UF41 medium-slope, high impedance variable-mu pentodes.
The anode-to-control-grid capacilance of these valves is sufficiently small to ensure stable operation with normal I.F. transformers, provided that reasonalle care is taken with the wiring layout.
Using critically-coupled I.F. transformers having a single circuit impedence of $0.2 \mathrm{M} \Omega$, gains in the order of 200 are obtainable when the following stage is of high impedance. When, however, us is usual, a single I.F. stage is followed by the detector and A.V.C. diodes, the damping imposed by these diodes limits the gain from the grid of the I.F. valve to the detector input to about 100 , assuming a detector load of $0.5 \mathrm{M} \Omega$.
In normal 4-valve receivers where the detector is followed by an A.F. amplifier and high-sensitivity output pentode, the input required at the detector for full output can easily be obtained from the J.F. valve with moderate input signals. In order to reduce the risk of overloading on strong signals where the A.V.C. circuit is supplying a large hias voltage, the A.V.C. characteristics of the EF41 and UF41 are so matched to those of the corresponding frequency changers that, when the same A.V.C. voltage is applied to hoth stages, the gain of the I.F. valve with sliding screen voltage is reduced more slowly than that of the frequency changer.
The signal voltages on the I.F. valve are therefore not allowed to become excessive, and modulation distortion in this stage is small.
These valves may also be used as R.F. amplifiers before the frequency changer stage. For this application the screen voltage should be ohtained via a potentiometer


THE COMPLETE SERIES

|  | FREQUENCY <br> CHANGER | R.F. or I.F. <br> AMPLIFIER | DET., A.F.AMPLIFR. <br> \& A.V.C.DIODE | OUTPUT <br> PENTODES | RECTIFIERS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6.3 Heater | ECH42 | EF41 | EBC41 | EL41; EL42 | EZ40; EZ4I |
| 0.1 AHeater | UCH42 | UF41 | UBC41 | UL41 | UY41 |

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## Uses of Metremance Broadeansing

THIS journal is concerned with the means and not the end of radio communication. To us, the urgent messages of life and death, the outpourings of contraltos, comedians or symphony orchestras are, like the impassioned oratory of politicians and the gyrations of ballet dancers, just " signals" or "modulation." Their interest lies not in their information or æsthetic content, but in the way they can be transmitted and reproduced by loudspeaker or on the television receiver screen.

But perhaps all this can be carried too far. Of late there has been much discussion on the technical means for a proposed metre-wave broadcasting system for this country, but practically nothing has been said in our pages, and very little elsewhere, on the way in which such a service would be used. Though it is not strictly our concern, it is essential to know what kind of audiences would be served if the best possible technical decisions are to be reached.

So far as the proposed extension of the B.B.C. service is concerned, the matter is relatively simple. In all probability the new service would be used very largely to fill in the gaps and to give better signals to the very large number of listeners who at present stand in need of them. There would also be the opportunity of providing signals of wider audiofrequency range. We doubt very much if the B.B.C. would decide to use the new channels for programmes different to those radiated on medium and long waves.

In considering the "independent" (non-B.B.C.) stations envisaged in the Beveridge Report and tentatively accepted in the Government White Paper, we move into much more controversial realms. It has been suggested that a multiplicity of small local stations conducted by public bodies would prove widely acceptable to listeners, and so would stimulate general interest in broadcasting; in addition, a valuable element of competition with the B.B.C. service would be introduced. Those who hold these views point to the success of small local stations in

America. But can we accept American experience as a guide? We believe in that country local patriotism or the community spirit is much more highly developed than here; even so, the small stations independent of national networks do not seem to be on the increase.

Coming to more materialistic considerations, who in Great Britain could afford to pay for the running of such stations? We must assume, of course, that the present ban on advertising will be maintained. No doubt, certain " pressure groups" with wealthy supporters will apply for licences, but would the propaganda programmes certain to be sponsored by such societies be likely to have a wide acceptance among listeners? Similarly, we may guess that some of the richer educational foundations would enter the field, but probably none of them could afford full national coverage, and anything much less would probably be thought unattractive. However, a group of educational bodies might well set up a network of stations, with a system of time-sharing for individual members.

In the present age of austerity we cannot visualize a stampede on the part of municipalities and the like to set up stations, nor that the ratepayers would approve of the use of their money for running them. And, even if this view is wrong, would there be a steady supply of acceptable programme material? In fact, is there any real future for "parish pump" broadcasting? No doubt, the average citizen would like to have a ready source of information on important local happenings and also on minor local disasters such as interrupted train services, gale and frost warnings, and the like. But, to derive full benefit from such a service, he would need an elaborate receiver with a calling device--a relatively expensive matter.

So we come back to the question of economics, which, in this matter at least, seems to outweigh most technical considerations. Much as we want to see independent stations licensed, if only experimentally, we must not be blind to the difficulties.



## f. M. Receiver

1.-.Simple, Inexpensire Set for
the $90 \mathrm{Mc} / \mathrm{s}$ Band

By J. G. SPENCER

' Research Department, B.B.C..

ONE of the points which has often been discussed when comparing amplitude modulation and frequency modulation for v.h.f. sound broadcasting is the relative cost of receivers for the two systems. It has been suggested that f.m. receivers will be more costly to manufacture, and that tuning is more difficult to achieve and maintain than for the corresponding a.m. receiver. On the other hand it is generally accepted that a wide-deviation f.m. system will result in a much better signal-to-noise ratio than a.m.

The design of the receiver described in this article was undertaken in order to find out whether it is practicable to obtain satisfactory performance from a receiver employing simple circuits and inexpensive components. It was designed for v.h.f. reception only and was intended to be comparable in cost and complexity with a medium priced domestic broadcast superheterodyne, but to realize the improvement in audio bandwidth which is possible at v.h.f. and the reduction in background noise of a wideband f.m. system. A total of seven valves is employed, their functions being, r.f. amplifier, frequency changer, i.f. amplifier, limiter, combined discriminator and first audio amplifier, output valve and rectifier. This is rather more than the medium-wave counterpart, but is largely offset by the absence of a ganged tuning

This top view of the receiver shows the position of the valves, mains equipment and controls. The chassis used measures 14 in $x$ 3 in $\times 2 \frac{1}{2}$ in and the panel 14 in $\times 8$ in. There is a $\frac{5}{8}$-in spacing between panel and chassis to accommodate the cord drive for the tuning cafocitor.

assembly and the simple construction of the r.f. and i.f. coils.
Circuit.-The receiver is designed for an f.m. system employing $\pm 75-\mathrm{kc} / \mathrm{s}$ deviation and $50-\mu \mathrm{sec}$ pre- and de-emphasis and covers a frequency band of $87.5 \mathrm{Mc} / \mathrm{s}$ to $95 \mathrm{Mc} / \mathrm{s}$. The circuit is given in Fig. 1.

The first stage is a pentode r.f. amplifier $\left(\mathrm{V}_{1}\right)$, which is followed by a triode-hexode oscillator and mixer $\left(\mathrm{V}_{2}\right.$. ) The r.f. circuits are not continuously tuneable as the frequency coverage of the receiver is only some 8 per cent of the mid-band frequency and the increased sensitivity at the ends of the band which could be obtained by employing continuous tuning would not justify the difficulties involved in ganging. No lumped capacitance is used in these circuits, since by tuning with stray capacitances only, the L to C ratio is kept high, thus reducing the $Q$ and giving a sufficiently uniform pass-band response while maintaining a high tuned impedance.
A.G.C. is applied to the mixer stage, the control voltage being derived from the limiter grid, to prevent the limiter being over-run by large carrier inputs.

The oscillator is a conventional tuned anode circuit, one point of interest being the frequency drift compensating device $\mathrm{R}_{10}$ and $\mathrm{C}_{19}$. This is a high negative temperature coefficient ceramic capacitor

Fig. 1. Theoretical circuit diagrom of the receiver. Although provision is mode for o.m. reception, this focility is not for direct comparison between a.m. and f.m., but merely becouse an a.m. signal will apfear on the limiter $\left(V_{4}\right)$ grid when receiving an a.m. transmission.
which is heated by a resistor connected across the valve heater supply. Its function is to correct for the rapid initial drift of local oscillator frequency which occurs immediately after switch-. ing on due to heating in the oscillator valve.

The i.f. amplifier is a single high slope pentode $\left(\mathrm{V}_{3}\right)$ and is followed by a pentode limiter stage $\left(\mathrm{V}_{4}\right)$.

Provision for a.m. reception is made by utilizing the limiter grid as a detector, and the audio output is fed to $V_{5,}$ through the i.f. filter $\mathbf{R}_{11}, C_{3,9}$ and the a.m./f.m. switch $S W_{\text {. }}$.

To facilitate accurate tuning on f.m., a spring-loaded pushbutton switch $\mathrm{SW}_{1}$ is provided, which when pressed, injects into the limiter grid circuit an a.c. voltage derived from the cathode of the rectifier $V_{7}$. This amplitude modulates the carrier and if the receiver is incorrectly tuned gives an audible hum in the output. When the receiver is correctly tuned however and the i.f. carrier is at the mid-frequency of the discriminator, the latter does not respond to amplitude modulation and the hum is at a minimum.
$\mathrm{V}_{5}$ is a triple-diode-triode, functioning as a Foster-
View of the underside of the chassis showing the general loyout and the annotation will enable most of the visible components to be identified.


Seelcy phase discriminator and first audio amplifier. Only two of the diodes are employed but a normal double-diode-triode cannot be used as the two diodes must have separate cathodes.

The output stage is a single tetrode with negative feedback from the output transformer secondary applied to the cathode of $\mathrm{V}_{5}$.
Construction.-Winding data and diagrams for the coils are given in Table 1 and Fig. 2. All the i.f. coils should be lightly brushed with polystyrene varnish after winding, to prevent any subsequent movement of slack turns.

TABLE 1.

| COIL | WINDING DETAILS |
| :---: | :---: |
| $\mathbf{L}_{1}$ | 1 turn 20 s.w.g. insulated wire interwound with $\mathrm{L}_{2}$. |
| $L_{2}$ | 6 turns 20 s.w.g. spaced to occupy ${ }^{3}$ in on Neosid former Dwg. 351/8BA with Dwg. 500 dust core grade 901. |
| $\mathrm{L}_{3}$ | 6 turns 20 s.w.g. spaced to occupy ${ }_{8}^{3}$ in Former and core as Le. |
| $\mathrm{L}_{4}$ |  |
| $\mathrm{L}_{i j}$ | 3 turns 20 s.w.g. spaced to occupy ${ }_{6}^{5}$ in on former as L. . No core. |
| ${\stackrel{L}{L_{7}}}_{\mathrm{L}_{7}}$ | Each consists of 40 turns 38 s.w.g. enamelled wire close wound with $10-\mathrm{mm}$ spacing between adjacent ends of coils. Both coils to be wound in same direction and connections made to pin numbers shown in Fig. 2. Aladdin former Type PP5937 and PP5939 with cores grade "A," Type PP5839. Can, John Dale Ltd. Type DTV1. |
| $\begin{aligned} & \mathrm{L}_{8} \\ & \mathrm{~L}_{9} \end{aligned}$ | Each consists of 35 turns 32 s.w.g. enamelled wire close wound with $6-\mathrm{mm}$ spacing between adjacent ends of coils. Former, cores, can and winding direction as $L_{6}$ and $L_{7}$ with similar pin connections. |
| $\mathrm{L}_{1.1} \mathrm{I}_{\text {i }}$ | 22 turns 32 s.w.g. enamelled close wound. <br> 26 turns 32 s.w.g. enamelled close wound in two layers of 13 turns each, one layer outside the other, and centre-tapped (see text). Spacing between adjacent ends of $\mathrm{L}_{10}$ and $\mathrm{L}_{11}$ is 5 mm Former, cores and can as $\mathrm{L}_{6}$ and $\mathrm{L}_{7}$. Connections as in Fig. 2. |

fip. 2. Sketch of i.f. (a) and discriminator (b) transformers. The pin numicrs refer to the numbers stamped on tha hase of the Aladdin formers.



Schematic layout of the cord drive located behind the panel. A $2 \frac{1}{8}$-in drum is used for the capacitor and one of $2 \frac{3}{4}$-in, running loose on a spindle fixed to the ponel, corries the pointer. The driving head is the J.B. Type A.

Insulated sleeving is called for in the grid coil of the oscillator assembly, as there is a potential difference of 100 V between the two windings. The overall diameter of the sleeving used should not be too large in order that it may be interwound with the anode coil when the latter is wound with turns equally spaced and filling the specified winding length.

The i.f. transformers are quite straightforward, to facilitate adjustments of coupling, should they be necessary, the primaries are not wound directly on the former, one turn of adhesive cellulose tape is put on first, adhesive side outward, and the primary is wound over this. Provided the coil is not wound on too tightly it will then slide quite easily along the former.
The i.f. tuning capacitors $\mathrm{C}_{12}, \mathrm{C}_{13}, \mathrm{C}_{23}$ and $\mathrm{C}_{24}$ are mounted inside their respective cans.
The secondary of the discriminator transformer, $L_{11}$, is centre-tapped. In order to minimize reakage inductance and to ensure symmetry of the two halves about the centre tap, which is essential for correct operation, it is wound in two layer form. The suggested winding procedure is as follows:-Start the first ayer about $\frac{1}{4}$ in up from the base of the former, wind on 13 turns and cut off the wire, leaving an inch or so for connecting and securing the two ends of the coil temporarily with cellulose tape. Next wind on a few turns of cellulose tape cut down to a width of $\frac{1}{8} \mathrm{in}$, hard against each end of the coil. This will provide two end cheeks between which to wind the second layer and will prevent the end turns of the latter from " spilling " over. Put one turn of cellulose tape, cut to the required width, over the first section to provide a smooth base for the second layer and then wind on the second section, starting again at the base end of the former and winding this time in the reverse direction. Finally connect together the ends of the two sections remote from the base of the former to make the centre tap. Great care should be taken that both halves are identical, with no loose turns or gaps in the winding, to ensure that the coil is symmetrical about the centre tap.

The discriminator primary, $L_{10}$ is wound in the same way as those of the i.f. transformers to allow for coupling adjustment. Capacitors $\mathrm{C}_{29}, \mathrm{C}_{30}$ and $\mathrm{C}_{31}$ are mounted inside the discriminator can.
If the specified chassis layout is adhered to, little difficulty should be experienced with the construction of the receiver.

Enlarged view of the r.f. and oscillotor portion of the receiver. The mojority of the components are onnotated and con te identified by reference to the circuit diagrom.

All decoupling circuits should be returned to the same earth point for each valve to avoid the possibility of coupling through common chassis paths. In the case of the r.f. circuits the decoupling point is the cathode pin of the valve holder, as shown in the circuit diagram. This is particularly important because the impedance of even a short length of wire is appreciable at the signal frequencies involved.

For the same reason all wiring in the r.f. section of
 the receiver must be as short and direct as possible ; $\mathrm{C}_{16}$, for example, is connected directly between the moving vane contact of the tuning condenser and the low potential end of the oscillator anode coil. Any lead of excessive length
here will appreciably lower the oscillator frequency, and may make it impossible to tune to the top end of the band.

An earthing clip must be provided at the socket

of the frequency changer to earth the metal can of the X81. Any of the retaining devices which grip the base of the valve are satisfactory.

For the frequency drift compensating network, $\mathrm{C}_{19}$ and $R_{t 0}$ are mounted in physical contact with each other in a small spring clip of the type used for mounting vitreous wire-wound resistors. The construction of this assembly is shown in Fig. 3.

To minimize oscillator frequency drift it is important that the components in the oscillator circuit should be of the types specified in the list of parts.

Small changes of wiring in this part of the circuit may alter the effect of the drift compensating network. This can be adjusted by changing the capacitance of $\mathrm{C}_{20}$. Increasing this capacitance will increase the upward movement of frequency during the warmingup period and vice versa.

Ventilating holes should be provided in the chassis deck above the oscillator section and in the cabinet base below it to facilitate ventilation.

The tuning condenser $C_{1 ;}$, used in the prototype receiver was a Raymart type MC151)X, nominal capacitance 5 to 15 pF , with one stator vane removed. Thus modified it gives a range of 3 pF to 11.5 pF and any component of similar physical size and with this capacitance range can be used. The tuning range obtained with this variation of capacitance is from


Fig. 3. Details of the frequency drift compensating unit which is described in the text.
$86.5 \mathrm{Mc} / \mathrm{s}$ to $96.0 \mathrm{Mc} / \mathrm{s}$, which is somewhat wider than the normal requirements for this band.

Screened wire is used for the lead from the gain control $\mathrm{R}_{28}$ to the grid of $\mathrm{V}_{5}$ to avoid hum pickup and low capacity cable should be used to prevent attenuation of the upper audio frequencies. Coaxial r.f. cable is ideal for the purpose.

The values of the resistors $\mathrm{R}_{30}$ and $\mathrm{K}_{31}$ are chosen for an output transformer designed for a 3- $\Omega$ load. Should a transformer with a different ratio be used these values should be adjusted for the correct voltage feedback.
(To be concluded)

# Ringing-Choke E.H.T. Systems 

Part I-Malf-wave Rectifier

By W. T. COCKING, m.t.e.

IT has now become almost standard practice to derive the e.h.t. supply for a television receiver from the line flyback. There are, however, cases where it may be desirable to use some other system and one of the most convenient of these is the so-called ringing-choke method. It is, in fact basically the same as the ordinary flyback method but because the e.h.t. and scanning circuits are quite separate each can be of optimum design for its own needs and, in particular, a simple voltage-regulating system can be provided.

Like the flyback system, the ringing-choke circuit depends on the interruption of current in an inductance or, rather, since capacitance is never negligible, in a tuned circuit. The circuit oscillates as a result and the voltage waveform is a damped oscillation. In the scanning circuit such oscillations cannot be permitted or must be confined to a single half-cycle within the flyback period. In the e.h.t. system they can be allowed.

The basic circuit is shown in Fig. 1, where R represents the circuit losses and $C$ the total stray capacitance. If the $Q(=R \sqrt{ } C / 2)$ is reasonably high the natural frequency of oscillation is very nearly $f=1 / 2 \pi \sqrt{ }$ LC.

If the valve is suitably biased and a large saw-tooth voltage is applied to the grid, its anode current will remain cut-off for a considerable part of the cycle.

This grid voltage is shown in Fig. 2 (a), in which the cut-off voltage is indicated by AB, and the resulting anode current has the form (b). The current rises more-or-less linearly to a maximum value $i_{0}$ in the period $\tau_{e}$ and is then suddenly cut-off. This kicks the tuned circuit into oscillation and the resulting anode-voltage waveform is like Fig. 2 (c).

It is not difficult to show that the magnitude of the first positive peak of voltage is, very nearly,

$$
\begin{equation*}
V_{m}=i_{n} \sqrt{x} \mathbf{L} / \mathbf{C} \tag{1}
\end{equation*}
$$ where $x$ is the fractional current overshoot in $L$ and is equal to $\epsilon^{-\pi / 20}$. The first negative half-cycle has the value $-i_{p} \sqrt{ } x^{3} \mathrm{~L} / \mathrm{C}=-x V_{m}$. Thereafter each positive half-cycle has a peak value $x^{2}$ times its previous positive peak and each negative peak is $x^{-2}$ times the previous negative peak. The number of cycles which occur before the train of oscillations becomes negligibly small depends on the damping. In practice, when the valve starts to conduct, its a.c. resistance damps the circuit and the oscillations to not usually persist for more than a cycie or so after it has started to conduct. Although the valve is a pentode, the rype normally used has quite a low a.c. resistance for a pentode-of the order of $20,000 \Omega$ only. The valve can, therefore, damp tine circuit quite heavily.

The e.h.t. supply is obtained from these oscillations by applying them to a rectifier which can be
a half-wave type or a voltage-multiplier. For a halfwave rectifier, the output cannot exceed $\mathrm{V}_{m}$ and will usually be some $10 \%$ less.

The foregoing relation between the amplitudes of successive peaks holds only in the absence of rectifiers. When these are present they extract energy from the circuit and the following cycle is consequently of smaller amplitude. An exact analysis is quite difficult. A fairly exact one has been made for a halfwave rectifier, ${ }^{1}$ however.

Consider a train of damped oscillations as shown in Fig. 3. They are produced by the sudden interruption in the supply of a current $i_{p}$ to L-the current being supplied by the valve of Fig. 1. The initial energy stored in L is $\mathrm{L} i_{n}{ }^{2} / 2$. With no rectifier, the energy is transferred to the capacitance when the current has fallen to zero and the amount stored in it is then $\mathrm{CV}_{m}{ }^{2} / 2$. This energy is less than that originally stored in L because some has been lost as heat in the circuit. From (1) $\mathrm{CV}_{m}{ }^{2} / 2=x i_{n}{ }^{2} \mathrm{~L} / 2$ and so the lost energy is $(1-x) L i_{p}{ }^{2} / 2$; it is from this relation that equation (1) is obtained.

Now with a half-wave rectifier the circuit becomes Fig. 4. For simplicity we assume a perfect rectifier which is an open circuit when the voltage across $C_{1}$ is less then the voltage on the tuned circuit and a short circuit when it is greater. We assume also that $C_{1}$ is so large that the voltage across it cannot change appreciably in any time interval under consideration. Let $C_{1}$ be charged to a voltage $V_{1}$ less than $\mathrm{V}_{m}$. When the voltage actoss C reaches $\mathrm{V}_{1}$ the rectifier conducts and $C$ and $C_{1}$ become in parallel. The voltage across both is then held at $\mathrm{V}_{1}$ and the current in L flows into $\mathrm{C}_{1}$, except for some, $V_{1} / R$, in the shunt damping resistance. When the total current in L has fallen to $V_{1} / \mathrm{R}$ the voltage can no longer be maintained and falls, so that the rectifier open-circuits to disconnect $\mathrm{C}_{1}$. This capacitance has gained energy during the conductive period of the diode and it gives this out again in its turn to the load circuit.

The circuit is left with energy $\mathrm{CV}_{1}{ }^{2} / 2$ in C and the voltage $\mathrm{V}_{1}$ across it. The difference, $\mathrm{Li}_{\mathrm{p}}{ }^{2} / 2-\mathrm{CV}_{1}{ }^{2} / 2$, has been partly expended as heat in the circuit resistance and partly passed to $\mathrm{C}_{1}$. In effect, a new cycle of oscillation now commences with initial energy $\mathrm{CV}_{1}^{2} / 2$. The second positive peak can have an amplitude of only $x^{2} V_{1}$ and must always be less than $\mathrm{V}_{1}$. The rectifier thus cannot become conductive again on any positive half cycle after the first. The rectifier action is entirely confined to the first positive half cycle.

## Basic Energy Relations

Precise relations for finite damping were given in the article already referred to. If the circuit losses are low enough to be ignored, however, it is very easy to derive some simple relations which, if only approximate, have the great merit of showing the important factors. If losses are negligible, the initial energy $L i_{>}{ }^{2} / 2$ in L and the energy stored in C at the peak, $\mathrm{CV}_{m}^{2} / 2$ are equal.

When the diode conducts the energy in C is $\mathrm{CV}_{1}{ }^{*} / 2$, the difference $L i_{p}{ }^{2} / 2-\mathrm{CV}_{1}{ }^{2} / 2$ is passed into $\mathrm{C}_{1}$. Now during the whole time $\mathrm{C}_{1}$ is delivering a constant current $i_{0}$ to the load circuit; it delivers an output power $i_{0} \mathrm{~V}_{1}$ and so during one complete cycle of dura-

[^0]tion $r$ (the interial between successive interruptions of $i_{p}$ ) it loses energy $i_{0} V_{1} \tau$. In the equilibrium condition the energy gains must equal the energy lost and so
\[

$$
\begin{equation*}
i_{n} V_{1} \tau=\mathrm{C}\left(\mathrm{~V}_{n}^{2}-\mathrm{V}_{1}^{2}\right) / 2 \tag{2}
\end{equation*}
$$

\]

If the output energy $i_{0} V_{1} r=W_{0}$ and the energy initially stored in the tuned circuit ${ }_{2}^{1} \mathrm{Li}, .,{ }_{2}^{1} \mathrm{CV}_{m}{ }^{*}$
Ws the above equation can be written in the very simple form

$$
\begin{aligned}
& \frac{\mathrm{V}_{1}}{\mathrm{~V}_{m}}=\sqrt{\left[1-\frac{W_{0}}{\mathrm{~W}}\right]} \\
& \approx 1-\frac{\mathbf{W}_{\mathrm{w}}}{2 \mathrm{~W}_{s}} \text { when } 1 \quad W_{11} \mathbf{W}_{s .}
\end{aligned}
$$

For constant stored energy, $\mathrm{V}_{m}$ is also constant. and so we find that the output voltage $V_{1}$ falls as the output energy increases. The meall current taken by a cathode-ray tube varies with the mean picture

Fig. I. Basic circuit of ringing-choke e.h.t. supply unit withour the rectifier system.

Fig. 2. Waveforms in the circuit of Fig. l; (a) grid voltage. (b) anode current and (c) anode voltage.


Below: Fig. 3. Damped oscillation forming the anode potential of the drivitig value.

brichtness and unless the voltage stays constant both focus and deflection sensitivity vary in some degree. The voltage regulation of the supply is, therefore, an important matter,

It may be expressed in several ways. One is to take the ratio of the voltage change from full load to no load to cither the full-load or the no-load voltages [that is, $\left(V_{m}-V_{1}\right) / V_{1}$ or $\left(V_{m}-V_{1}\right) / V_{m}$ ]; the figure is the fractional voltage regulation or, if multiplied by 100, the percentage voltage regulation. Another method is to express it as an equivalent resistance by dividing the change of output voltage by the change of output current which causes it [that is, $\mathrm{R}_{4}=$ $\left.\left(V_{m}-V_{1}\right) / i_{0}\right]$; it is in some ways a good method, but means little unless the voltage is stated also. However, the other way also means little unless the change of current is stated.

In this article the change of current used is always $100 \mu \mathrm{~A}$, and is from zero to that figure. The regulation is then $\left(V_{i n}-V_{1}\right) / V_{m}=1-V_{1} / V_{m}$ and can be obtained directly from equation (3). As long as $W_{0} / W_{0}$ is small compared with unity

$$
\begin{equation*}
\frac{\mathbf{V}_{m}-\mathrm{V}_{1}}{\mathbf{V}_{m}}=\frac{\Delta \mathbf{V}_{1}}{\mathbf{V}_{m}}=\frac{1}{2} \cdot \frac{\mathbf{W}_{0}}{\mathbf{W}_{n}} \tag{4}
\end{equation*}
$$

If it is des'red to express the regulation in the form of an internal resistance, this is readily done, for

$$
\begin{aligned}
\mathbf{R}_{1} & =\frac{\mathbf{V}_{1}}{i_{0}} \approx \frac{\mathbf{V}_{m}}{i_{0}} \cdot \frac{1}{2} \frac{\mathbf{W}_{0}}{\mathbf{W}} \\
& =\frac{\mathbf{V}_{1} / i_{0}}{2 \mathbf{W}_{n} / \mathbf{W}_{0}-1}
\end{aligned}
$$

Here $V_{1 / i 0}$ is, of course, the resistance of the external load circuit.

This expresses the regulation of the system due to the LC circuit and assumes a perfect rectifier. With any practical rectifier the regulation will be poorer. The relation is very important for it shows that, apart from the rectifier, the regulation depends only on the ratio of the output to the stored energy and that good regulation requires a large stored energy which, in its turn, naturally means a large power input to the stage.

## Required Voltage Regulation

Since the deflectional sensitivity of a magnetic c.r. tube is proportional to $1 / \checkmark V_{1}$ it is necessary for the regulation to be $2 \%$ if the picture width and height are to change by only $1 \%$ for a change of beam current of $100 \mu \mathrm{~A}$. On a 10 -in picture this means a change of 0.1 inch. In practice a bigger change is often tolerable because changes of picture brightness from black to peak white are rare. Normal brightness changes are probably no more than $25 \%$ of the maximum possible, and then a regulation of $8 \%$ will not alter the picture size more than $1 \%$. Because of this, a regulation of $8-10 \%$ is often considered satisfactory and one of $4-5 \%$ is thought to be good. Since the effect of the rectifiers is not included in the present discussion it is desirable to make the computed regulation around $2 \%$.

As equation (4) shows, this demands $W_{0} / W_{0}=0.04$; that is, the stored energy must be 25 times the energy supplied to the load. If the circuit of Fig 4 is driven at line-scan frequency the period $t$ is nearly $100 \mu \mathrm{sec}$. If the output voltage of $V_{1}$ is 10 kV and the current $i_{0}$ is $100 \mu \mathrm{~A}$, the output power $\mathrm{P}_{0}$ is 1 watt and the output energy is $10^{-4}$ joule. The stored energy must then be 0.0025 joule, and as it must be supplied afresh every scanning cycle $(10,000 \mathrm{c} / \mathrm{s})$, the power needed is

25 watts. This is apart from losses, such as the anode dissipation of the valve.

Referring to Fig 2 (b) the anode current of the valve is of triangular waveform and rises more or less linearly to $i_{D}$ in the period $\tau_{c}$. Assuming the rise to be actually a linear one, the mean anode current of the valve and the back e.m.f. across $L$ are

$$
\begin{align*}
& i_{a}=\frac{i_{p}}{2} \cdot \frac{\tau_{c}}{\tau}  \tag{5}\\
& \mathbf{E}_{\mathrm{L}}=\mathbf{L} i_{p} / \tau_{c} \tag{6}
\end{align*}
$$

In practice it is necessary for the h.t. supply voltage to be greater than $E_{1}$, by the minimum permissible anode voltage $\mathrm{V}_{a}$ of the valve, usually $60-100 \mathrm{~V}$.

## Turns Ratio

One minor difficulty arises. Any practical valve has a peak anode voltage rating which must not be exceeded. In the circuit of Fig 4, $V_{m}$ must not exceed this figure, and so the output is limited. This is easily overcome, however, by tapping the anode down the coil, as shown in Fig 5. If the ratio (turns 1-3) (turns 1-2) is $n$, then the equations already given still apply if all currents and voltages pertaining to the valve are multiplied and divided respectively by $n$. That is, design is carried out for a unity ratio and. then the ratio is chosen to bring the conditions within the limits of the value and to the most convenient values.

Because of leakage inductance and stray capacitance, the performance is affected in other ways, and if it is to be reasonably close to calculation $n$ must be restricted. It is inadvisable to make $n$ more than about 1.5 for an air-core coil or about 2.5 for an ironcore component. Greater ratios can be used, but more experimental work in the determination of final values will be needed.

As an example of the procedure, let us now consider the example which has already been taken; that is, of a supply of 10 kV at $100 \mu \mathrm{~A}$ with a regulation of $2 \%$. As we have seen, the stored energy $W_{s}$ is 0.0025 joule.

It is hardly safe to take the self-capacitance of the coil as less than 10 pF and a metal rectifier for e.h.t. will add about 15 pF , so 25 pF is abut the minimum safe value to take for C . A valve rectifier would add less, in itself only about 1 pF . The filament winding would increase it considerably above this, however, and it is a very troublesome matter for the experimenter to adjust a filament winding correctly.

Now since $W_{n}=\frac{1}{2} \mathrm{CV}_{\mathrm{m}^{2}}{ }^{2}$ and for $2 \%$ regulation $V_{m}=10.2 \mathrm{kV}$, we find $C=2 \times 0.0025 / 1.02^{2} \times 10^{8}$ $=4.8 \times 10^{-11} \mathrm{~F}=48 \mathrm{pF}$. This is the capacitance required to store the necessary energy at 10.2 kV . It is greater than our assessment of the minimum practical value, and so capacitance sets no limit and we can proceed on the basis of $C=48 \mathrm{pF}$.

The value of $L$ required depends on the peak current which the valve can provide, and we need to know the turns ration. A valve such as the PL81 is rated fur a peak voltage of 7 kV positive or 5 kV negative. It is necessary to take the lower value because the anode voltage does swing negative on the second half cycle of oscillation. For this valve, $n$ must be 2, at least. With an EL 38, the peak rating is 8 kV and no restriction is placed on the sign of the voltage. With this valve $n$ need be 1.3 only. Assume this; then $i_{0}$ for the valve is 150 mA and in the circuit is $150 / 1.3=115 \mathrm{~mA}$.

Since $W_{8}=\frac{1}{2} \mathrm{Li}^{2}{ }^{2}$ we have $\mathrm{L}=2 \times 0.0025 / 0.115^{2}$
$=3.76 \times 10^{-1} \mathrm{H}=376 \mathrm{mH}$. The natural frequency of oscillation is $1 / 6.28 \sqrt{ } 0.376 \times 48 \times 10^{-12}=10^{6} / 26.5$ $=3.78 \times 10^{4}=37.8 \mathrm{kc} / \mathrm{s}$. The time of one cycle is $26.5 \mu \mathrm{sec}$. This frequency is rather low, for if $\tau_{c}$ is made $50 \mu \mathrm{sec}$ there is time for something less than two cycles of oscillation only during the non-conductive period of the valve. If we arbitrarily take $\tau_{e}$ as $50 \mu \mathrm{sec}$, the back e.m.f. across L is $\mathrm{E}_{\mathrm{L}}=0.376$ $\times 0.115 / 50 \times 10^{-6}=870$ volts. On the valve this becomes $870 / 1.3=670 \mathrm{~V}$. The h.t supply must, therefore, be around 750 V The mean anode current is $z_{a}=\frac{150}{2} \cdot \frac{50}{100}=37.5 \mathrm{~mA}$ and the power drawn from the h.t. supply is $760 \times 0.0375=28.5 \mathrm{~W}$. The anode dissipation of the valve is $28.5-25=3.5 \mathrm{~W}$.

There are two features about this design which are unsatisfactory, apart from the large total input power ; they are the low frequency of oscillation and the very high voltage needed for h.t. The latter can be reduced only by increasing the current, and this may entail the use of valves in parallel.

If poorer regulation can be tolerated the power can be reduced by operating with less stored energy. This entails a reduction of capacitance, and so there is a limit to the amount by which the stored energy can be reduced, a limit set by what it is practicable to achieve in capacitance.

It was earlier estimated that the capacitance was likely to be 25 pF as a minimum. Taking it as 24 pF for convenience (one-half of 48 pF ), the stored energy is halved and so the regulation becomes $4 \%$. The inductance is halved and becomes 188 mH for the same current. The natural frequency is four times as great ( $151.2 \mathrm{kc} / \mathrm{s}$ ) and the number of cycles permissible for $\tau_{c}=50 \mu \mathrm{sec}$ is nearly eight. The tapping point on the coil, being set by the peak voltages remains unchanged. Since L is halved and the current is unaltered, $\mathrm{E}_{\mathrm{L}}$ is halved and becomes 355 V so that the h.t. supply drops to about 425 V . The valve currents are unaltered and the input power falls to $425 \times$ $0.0375=16 \mathrm{~W}$.

This is a considerable improvement, but the power is still high. If we could again halve the capacitance the regulation would become $8 \%$ and the back e.m.f. on the valve would drop to 167.5 V , so that an h.t. supply
of 257.5 V would suftice. The power input would become 9.75 W . This is a reasonable condition and by varying the tapping point on the coil to change the ratio of valve voltage to current we could modify the conditions over a small range to suit a particular h.t. supply voltage.

It is almost certainly pcssible to achicve a capacitance of only 12.5 pF by careful design when a valve rectifier is used. It is very doubtful if it is possible with existing types of metal rectifier. A regulation of $8 \%$ would be tolerable for some purposes, and a system of this basic regulation or worse can be made to have any required improvement by the addition of a voltage regulator. It is possible in this way to obtain an improvement of the order of $5: 1$.

## Repetition Frequency

So far no mention has been made of the effect of varying the repetition frequency of the saw-tooth driving waveform, and it has been assumed that it will be at line-scan frequency, some $10 \mathrm{kc} / \mathrm{s}$. This is usually the most convenient frequency, since the e.h.t. supply unit can then be driven from the line time base.

If $\tau$ is increased, by lowering the frequency, the output energy $W_{0}$ required per cycle is increased in proportion. For the same voltage regulation the stored energy $W_{s}$ must also be increased in proportion. This stored energy has to be supplied anew only $f(=1 / \tau)$ times as often, so that the input power remains unchanged. If the conductive period of the driving valve is increased in proportion, so that $\tau_{c} / \tau$ is constant, $\mathrm{E}_{\mathrm{L}}$ will be inversely and $i_{a}$ directly proportional to $\tau$. The voltage/current ratio in the driving valve will change, which may or may not be convenient. Generally speaking, therefore, the frequency of the driving wave is not very important, and there is usually no point in departing from the time-base frequency.

For the same regulation, therefore, there is usually no point in making the driving frequency different from the scanning frequency. Generally it is a disadvantage to make it different because a special generator of the driving waveform becomes necessary whereas, if operation is at line-scan frequency, the valve can be driven from the line time base. Moreover, if the frequency is appreciably reduced, a larger reservoir capacitance must be used.

If the regulation is not kept unchanged, however, conditions are different. If $W_{s}$ is kept constant while $\tau$ is increased the regulation varies as $1 / \tau$ and as ${ }^{\prime}{ }^{\prime}$, has to be supplied $1 / \tau$ times a second, the input power varies as $1 / \tau$ and falls as $\tau$ is increased.

The whole point of using a regulator with a circuit of this type is to enable the input power to be reduced without affecting the regulation. Now at a driving frequency of $10 \mathrm{kc} / \mathrm{s}$ it does frequently happen that it is impossible to make C small enough for the regulation to be worse than $5 \%$ or so. The input power is then still large and cannut be reduced by adding a regulator. However, by increasing $\tau$ (lowering the frequency) the regulation is made worse and the input power reduced and the regulator is worth while. Because of this there are cases where a lower driv ng frequency is an advantage and frequencies down to $1 \mathrm{kc} / \mathrm{s}$ are used commercially; e.g., in the Mullard $25-k V$ e.h.t. unit for projection telev s on. As will appear later, the use of a voltage-multiplying rectifier offers an alternative and more coaveni nt solution, and for the rest of this article a $10-\mathrm{kc}$ 's driviag wave will be assumed.

# Aircrait Radio on Show 

Suppressed Aerials, Latest Radio, Radar and Navigational Aids

THE higher speeds now attained by passenger aircraft has given the radio engineer a new set of problems to tackle and not the least of these is the installation of aerials. Even if it carries only a portion of the many radio aids to navigation now available a modern airliner may require up to a dozen different aerial systems, for on long distance routes, m.f. and h.f. communications, d.f., v.h.f. and some of the many homing and position finding systems, and possibly a radio altimeter, will be essential equipment.

In very few cases can one aerial be used for more than one service and the problem is how to fit all those required on a thoroughly streamlined aircraft without introducing "drag" and so impairing its flying efficiency.

The latest technique is to build the aerials into the body of the aircraft and this is a matter that must be decided at a very early stage in the construction of the 'plane, and preferably at the drawing-board stage. Some examples of this practice were seen at the recent flying display and exhibition held by the Society of British Aircraft Constructors at Farnborough, Hants. The installations designed for the English Electric Canberra and the De Havilland Comet and Ambassador were shown by the Marconi Company and a few other examples were seen elsewhere. An account of some measurements made on various types of these "suppressed" aerials, as they are called, was given in Wireless World of December, 1949.

Typical of the way in which the actual structure of the aircraft is being used as a radio aerial is that of the tail fin of the Comet. This is a metallic structure and is insulated from the body of the aircraft by a 4 -in section of insulation (fibreglass is used in
this case). The metal skin of this fin is used as an aerial for h.f. and m.f. communications and in the top part, under a dome of fibreglass, is a wide-band v.h.f. aerial designed to cover the aircraft band of 118 to $132 \mathrm{Mc} / \mathrm{s}$.

Doors enclosing retractable landing gear; body inspection covers and so on are also pressed into use to accommodate some form of radio aerial.

A new type of radio altimeter, or terrain clearance meter, made its appearance this year. Two firms were showing it and both employ the same basic principle. It is a frequency-modulated system and in the case of the Standard Telephones design, the Type STR30, operates in the $4,300-\mathrm{Mc} / \mathrm{s}$ band. A klystron-type oscillator is used for the transmitter, the output circuit being a section of waveguide two wavelengths long. Inside this is a tuning device resembling the vane of a variable capacitor and it is rotated by a small motor giving a sweep of $100 \mathrm{Mc} / \mathrm{s}$ or of $10 \mathrm{Mc} / \mathrm{s}$ as required, the former being used for the low altitude range covering $0-500 \mathrm{ft}$ and the latter for the high, covering $0-5,000 \mathrm{ft}$. Separate indicating instruments are used for each range with the view to preventing ambiguity in reading and also to enable the most suitable type of scales to be employed, in this case logarithmic for the low and linear for the high. The lowest height marking is 5 ft and the accuracy is said to be $\pm 2 \mathrm{ft}$ or $\pm 3$ per cent, whichever is the greater.

Separate aerials taking the form of small horns for recessed mounting in the aircraft are used for transmitter and receiver and these can be mounted as close as 1 ft apart, measured centre to centre.

The other radio altimeter was shown by Salford Electrical. It has been produced to Ministry of Supply requirements and is a single-range instrument covering $50-5,000 \mathrm{ft}$ with a required accuracy of 3 ft $\pm 3$ per cent. Present indications are that readings below 50 ft will be quite reliable and the upper limit probably better than the specification. It also embolies a frequency modulated system employing a mechanical means of sweeping the frequency


Above: Stondard Telephones radio altimeter Type STR30; the two horn "aerials" are on the right and the remote control unit with one height indicctor on the left. Right: Recessed iron cored loop (inner) and sense aerial (outer) of the Marconi Type AD7092A automatic direction-finding equipment.


Left : Plessey Type PTR61, v.h.f. transmitter-receiver fitted with remote control attachment. The equipment provides 6 channels send and receive, for immediate operation. Right : Redifon Type Al45 airborne passeiger announcement system showing pilot's control (left), amplifier unit, steward's control and microphone and one of the 13 loudspeakers.
over a band of $50 \mathrm{Mc} / \mathrm{s}$ and it operates at a mean carrier frequently of $1,630 \mathrm{Mc} / \mathrm{s}$. Slot aerials are used and mounted in weatherproof boxes designed for fitting flush with the skin of the aircraft.

The most up-to-date types of v.h.f. airborne radiotelephone equipment can be divided into two main categories. In the one are those sets capable of providing, at the turn of a switch, any one of the full number of radio channels available in the 118- to 132$\mathrm{Mc} / \mathrm{s}$ band and in the other sets which provide immediate selection of a limited number of channels and facilities for changing to any of the others by fitting the appropriate crystals.

Two firms, Marconi and Standard Telephones, have multi-channel sets of the first kind and both provide a complete coverage of the available channels with 24 crystals only and this includes both send and receive.

Basically, the principle of operation is the same in both sets but there are many differences in carrying out the idea. Two oscillators are used in the Marconi AD115 equipment, one, the major oscillator, has 14 switchable crystals whose frequencies are adjusted so that after a pre-determined multiplication a carrier output on each of the whole numbers of the working frequencies is obtained; e.g., $118,119,120$ and so on to $132 \mathrm{Mc} / \mathrm{s}$.
'The other, or minor, oscillator is also crystal controlled and provides an output which when mixed with the major oscillator's output adds the required decimal portion of the frequency, for example, 0.1, $0.2,0.3 \mathrm{Mc} / \mathrm{s}$ and so on.

At present the band 118 to $132 \mathrm{Mc} / \mathrm{s}$ is operated with $200-\mathrm{kc} / \mathrm{s}$ channel spacing and so 70 channels only are usable but future requirements will be for $100-\mathrm{kc} / \mathrm{s}$ spacing and then the 140 channels will be required. This equipment gives $15-20$ watts output, has full remote control and operates on telephony or m.c.w.

In the Standard Telephones STR12C equipment 70 channels with $200-\mathrm{kc} / \mathrm{s}$ spacing are provided, but it is a simple matter to double this number when the need arises. A small remote control unit contains 24 miniature crystals and three oscillators, but two only are in use at any one time. It carries also two frequency selecting switches, one for whole numbers the other for the decimals, on-off switch and telephony or m.c.w. telegraphy switch. The carrier output is 15 watts.

Typical of the sets in the second category are the
two Ekco models CE40, 11 channels, and CE58, 22 channels; Murphy MR60 and MR80, 5 and 23 channels respectively and Plessey PTR61 with six channels. The majority of the equipments in this category are low power sets being intended mainly for privately owned and light aircraft, where the requirements are a limited number of channels immediately available and facilities for changing to others, if necessary, in the air.

Some of the larger passenger aircraft now hav several cabins, each seating 12 or more people and. although interconnected, dividing bulkheads-isolate them to some extent. In these aircraft are now being fitted passenger announcement loudspeaker systems, generally under the control of the steward of stewardess but with over-riding control from th: pilot's or navigator's positions.
An amplifier for an installation of this kind is made by Redifon; it is the Type A145, gives 15 to 20 watts audio output and is capable of operating 13 loudspeakers distributed throughout the aircraft. It fits the standard aircraft racking and has all cabling brought in at the back via plugs and sockets to simplify servicing.
Wide-band aerial amplifiers designed to do away with the forest of aerials which distinguish most ground stations working long-distance point-to-point and ground-to-air communication services were seen at the S.B.A.C. show. Plessey has developed one, the Type PV14, covering $2-25 \mathrm{Mc} / \mathrm{s}$ and which will operate up to ten communications receivers from a single aerial without mutual interference. The amplifier consists of two identical sections each having two EF91 valves in parallel and feeding five ECC.91 valves operated as cathode followers. Each supplies a separate receiver. A modification of this amplifier is available for dual diversity reception, each half operating up to five receivers from two separate aerials.

Another example of a wide-band amplifier is the Redifon Type MCU1. It is designed to operate up to eight receivers from a single aerial. The input from the aerial is taken through a band-pass filter which accepts all signals within the band $2-20 \mathrm{Mc} / \mathrm{s}$ but heavily attenuates those outside this band. Following the filter are eight EC91 triodes operating as cathode followers and each feeding into a separate output for the eight receivers.

One of the latest secondary radar navaids, the interrogator-responder systern known as DME (Dis-
tance Measuring Equipment) was shown by Ferranti. This operates in the $1,000-\mathrm{Mc} / \mathrm{s}$ band and provides the pilot of an aircraft with continuous visual information of the distance, and any deviation from the direct line of flight, to a selected ground beacon. Its effective range is about 200 nautical miles. Both ground and airborne equipments were on view.

- Another navigational system well represented was Dacca, which firm had a model of an anti-static aerial for aircraft consisting of a vertical streamlined and insulated mast with its leading edge cased in metal and acting as a shield for the aerial fitted in the centre of the mast. It is claimed that the earthed metal shield
protects the aerial from charged rain and other static effects and provides a better signal-to-noise ratio than the usual unprotected aerial. This firm also included the latest Mark VII airborne Decca receiver designed for use in fast flying civil aircraft. It operates on a wider "lane" spacing than hitherto and includes a local oscillator which is locked to the master station's signals so that the operation of the set is not dependent entirely on the continuous reception of the master station. Complete interruption of several seconds' duration does not affect the operation or reliability of the system as a navigational aid. Including the control unit it weighs under 401b.


# SHORT-WAVE CONDITIONS 

## September in Retrospect : Forecast for November

By T. W. BENNINGTON*

DURING September the average maximum usable frezuencies for these latitudes increased by day and decreased by night, which variations were in accordance with the normal seasonal trend. Daytime work ng frequencies did not, however, appear to increase, and $17 \mathrm{M} / \mathrm{cs}$ remained about the highest regularly usable frequency for east/west paths, though those up to $22 \mathrm{Mc} / \mathrm{s}$ were sometimes usable. Over north/south paths $24 \mathrm{Mc} / \mathrm{s}$ remained about the highest regularly usable daytime frequency. At night only the lower short-wave frequencies ( $6-7 \mathrm{M} / \mathrm{cs}$ ) were generally usable, due mainly to the disturbed conditions which generally prevailed.

There was a sharp decrease in the amount of Sporadic E recorded. Dutch and German stations on freouenc'es around $94 \mathrm{Mc} / \mathrm{s}$ were frequently received during the first

half of the month, and on isolated days towards the end, their signals being presumably heard due to tropospheric propagation.

The average sunspot activity was considerably higher than during the previous month.

The month was notable for the very large amount of ionospheric storminess which occurred. Although the equ noctial months of March and September are generally badly disturbed, this September was exceptional for the long duration of the disturbed periods. In fact the whole period from the 9 th to 28th was more or less severely disturbed, this being probably due to several different ionospheric storms following each other in quick succession, and poss.bly connected with the central meridian passages of sunspots on the 9 th, 15 th and 20 th . There were accompanying magnetic disturbances of severe intensity and on several occasions aurora was observed in this zountry. The height of the disturbance occurred on the 25 th, when the aurora was widespread and the magnetic disturbance reached the intensity of a "great magnetic storm." In the afternoon and evening of this day short wave reception was very poor and there was severe flutter fading with a "rumbling" background on nearly all stations. Both the rapid fading and the " rumble" were not ced even on medium wave reception later in the evening.

Five Dellinger fadeouts were reported during the month, those at 1057-1230 on 7th and 1500-1700 on 15th being of severe intensity.
Forecast: During November the daytime in.u.f. for these latitudes should continue to increase, whilst that for the night-time should continue to decrease. Working frequencies should, therefore, be relatively high by day, and on east/west circuits those up to $20 \mathrm{Mc} / \mathrm{s}$ should be regularly usable. It is unlikely, though, that those above $26 \mathrm{Mc} / \mathrm{s}$ will become usable over such circuits, except, perhaps, on one or two isolated occasions. Over north/ south circuits frequencies up to $26 \mathrm{Mc} / \mathrm{s}$ should remain regularly usable, and those up to $32 \mathrm{Mc} / \mathrm{s}$ occasionally so, during the daytime. Medium-h:gh frequencies will have to be used for an increasingly large proportion of the daily time, owing to the continued decrease in the hours of daylight. At night very low frequencies will have to be employed, and $6 \mathrm{Mc} / \mathrm{s}$ should be about the highest regularly usable frequency over most circuits.

Sporadic E capable of propagating very high frequencies is unlikely to be prevalent. Medium-distance communication will be controlled by the $F_{2}$ layer, and should therefore be possible on medium-high frequencies during the day, and only on the lowest short-wave frequencies at night.

The curves indicate the highest frequencies likely to be usable over four long-distance circuits from this country during the month.

# Ignition Interierence Suppressor 

Suggestion for an Improved Tolevision Limiter Circuit



ONE of the difficulties encountered in receiving televised images is that of removing the "blobs" produced by unsuppressed car ignition systems. These are due to spot defocusing caused by intense positive or negative interference pulses (depending on whether grid or cathode modulation is used) being applied to the cathode ray tube.
There are two kinds of suppression systems ir use and each depends on a clipping action on the waveform. The first, shown in Fig. 1, is a limiter with manual adjustment (applied to a cathode-drive modulator). If adjusted correctly this undoubtedly gives the better overall results, but it has the disadvantage that adjustment of the contrast control alters the threshold of clipping. At first sight this may seem irrational until it is realized that every adjustment of contrast requires a corresponding adjustment of brightness-which means a change of black level and peak white level.

Unless one resigns oneself to a constant contrast setting this can become a nuisance, so various attempts have been made to devise self-setting suppressors. A simple circuit used by home constructors and in certain commercial receivers is shown in Fig. 2. It gives extremely efficient suppression as the effect is augmented by instantaneous negative feedback from anode to grid. Although in theory the $0.1-\mu \mathrm{F}$ capacitor should charge to a value equivalent to peak white, it actually reaches a value somewhat below this level and tends to clip highlights. Images above a certain brightness therefore lack detail and this is particularly noticeable when the relevant object is against a dark background.

The writer has attempted to devise a simple circuit (Fig. 3) which will combine the merits of both these methods and at the same time minimize their disadvantages as far as possible. It will be seen that a manual control is supplied, which can be set for optimum results on a normal picture. If, however, the contrast level is reduced (and brightness increased) the circuit self-biases itself to highlight level. This works out very well, in the writer's experience, because at low contrast there is little likelihood of a gloomy background, and, what is more important, over a long period of use it has been found that resetting is quite unnecessary under any circumstances. This in spite of repeated trials to see if the setting could be improved.

The method of setting recommended is simple. Choose a programme consisting of a fairly mixed range of contrasts (newsreels are probably as good as anything in this respect). Then reduce the value of the variable resistor until the highlights begin to be affected and lose detail. Finally adjust the setting so that no effect can be detected, just beyond this point.

In fringe areas, where more or less severe variations of signal take place, it may be found preferable to connect the 5-MI2 resistor to h.t. + rather than to the anode. The connection shown, however, has been
found better for normal conditions of steady reception, since the anode connection supplies a small amount of d.c. level to the diode and reduces any tendency for loss of highlight detail when receiving exceptionally dark pictures such as night scenes.

F.g. 1. Simple limiter with manual adjustmen:.


Fig. 2. Self-bias limiter acting by negative feedbock.


Fig. 3. Limiter combining manual setting with automatis self bias. Note that the $2-M S 2$ contro! may be connected by long wires because of the 0.1 -nt copacitor acting as a filter.

# Sensitive T.R.F. Receiver 

3- Valve Circuit with Amplified A.G.C.

By S. W. AMOS, * B.Sc.(Hons) and G. G. JOFNSTONE, * B.Sc.(Hons)

THE 3-valve receiver descibed in this article was designed to use the amplified a.g.c. circuit described in last month's issue. It uses a t.r.f. circuit, chosen because such circuits are easier for home constructors to align than superhets. Nevertheless the perfomance of the receiver compares very favourably with that of a 3 -valve superhet with a frequency-changer, i.f. amplifier and double-diodepentode output; in fact the sensitivity and a.g.c. performance are better than that of the superhet. The selectivity is inferior but permits interferencefree reception of 12 medium-wave signals during daylight in London, threc of the signals being between the Home Service ( $908 \mathrm{kc} / \mathrm{s}$ ) and the Light Programme ( $1214 \mathrm{kc} / \mathrm{s}$ ).

It is unusual to apply a.g.c. to a t.r.f. receiver because the gain is not normally adequate to make its application worthwhile. If the receiver has to operate at maximum gain to give adequate output from an aerial signal of, say, 1 mV amplitude, the a.g.c. can do nothing to maintain the output when the signal fades below 1 mV ; applied to such an insensitive receiver, a.g.c. is only useful in levelling the output from comparatively strong signals, though it may also serve to prevent detector overloading on strong signals. To make the best use of a.g.c. as a means of reducing fading, high sensitivity is essential and is obtained in this receiver by the use of high-slope pentodes as r.f. amplifier, detector and output valve. With such valves it is possible to obtain ser.sitivity of the order of $10 \mu \mathrm{~V}$ as will be seen from the following calculations.

An EF50 or SP61 is used as an output valve with a load of $20 \mathrm{k} \Omega$; with a $g_{m}$ of $6 \mathrm{~mA} / \mathrm{V}$ (a practical figure) the gain is 120 . A similar valve is used as detector with an anode load of $300 \mathrm{k} \Omega$; the working mutual conductance is much lower but the gain is still approximately 100. In the r.f. stage a dynamic anode load of $30 \mathrm{k} \Omega$ or higher is used giving a gain in the region of 200 . With an aerial circuit gain of 5 (a conservative figure) the overall r.f. gain is $10^{3}$ or better, and the total receiver gain from equivalent aerial generator to final anode is in the region of $10^{7}$. With the output-valve anode load assumed, the anode voltage swing is 31.6 volts r.m.s. for the standard 50 mW output, and the r.f. aerial generator output necessary (at 30 per cent. modulation) to produce this output is approximately $10 \mu \mathrm{~V}$. The sensitivity realized in practice is slightly less than this calculated value and is approximately $20 \mu \mathrm{~V}$.

The provision of such high gain introduces a number of design difficulties. One, already

[^1]mentioned, is that of detector overloading and is most effectively overcome by the a.g.c system Overloading ${ }_{6}$ is also possible at the grid of the r.f. amplifier since "straight" pentodes of the EF50 type overload with signal inputs greater than approximately 1 volt. To prevent this, provision is made for the introduction of a wavetrap tuned to the strongest signal. Further, and most important, high gain is an embarrassment unless the receiver has high selectivity ; this point is illustrated by the following calculation. Assume that it is intended to receive a relatively weak signal ( $100 \mu \mathrm{~V}$ amplitude) displaced by $50 \mathrm{kc} / \mathrm{s}$ from a powerful neighbour operating at $1 \mathrm{Mc} / \mathrm{s}$ with a signal amplitude of 10 mV . From universal selectivity curves ${ }^{1}$, the rejection of the strong signal given by a single LC circuit with a Q of 100 tuned to the weak signal is 20 db . Thus to give a signal/interference ratio of 20 db , three tuned circuits are necessary.

In practice conditions even more difficult than this may easily be encountered. To cope with such conditions a wavetrap tuned to the Home Service frequency and providing a further degree of selectivity, is necessary. This not only helps station separation, but also prevents overloading of the r.f. stage. Such a wavetrap is incorporated in the receiver described (which is used in the London Area) but it should be realized
"See for example "Radio Receiver Design," by K. R. Sturley l'art I, p. 124 (Chapman \& Hall).

Top of chassis viewed from the bock, showing trimming adjustments.

that it will not be necessary in areas of generally low field strength, and should not in every region be tuned to the Home Service for the best results. For example in the Daventry area, it may be most advantageous to tune the wavetrap to the Third Programme on $647 \mathrm{kc} / \mathrm{s}$. Some idea of the value of the wavetrap can be gathered from the fact that the receiver in Central London and without interference receives clearly three stations, Hilversum ( $1007 \mathrm{kc} / \mathrm{s}$ ), West of England Home Service (1052kc/s), and Midland Home Service (1088kc/s) between the London Home Service and the Light Programme ; it certainly cannot do this without the wavetrap.

The three tuned circuits are best arranged as a single circuit and two coupled circuits acting as a bandpass filter. Experiments showed that best results are obtained when the single circuit is connected between aerial and r.f. valve and the coupled circuits between r.f. valve and detector.

## The Circuit

The full circuit diagram of the receiver is given in Fig. 1. V1 is the r.f. amplifier (an EF50) with a.g.c. voltage applied to the suppressor grid, V2 is an anode bend detector (SP61 or EF50) and V3 is an audio output stage (SP61 or EF50).

The aerial input circuit is quite conventional and uses Wearite PA1 and PA2 coils. The cathode of V1 is maintained at a potential of 100 volts (approximately) above earth by high-value cathode resistors, $\mathrm{R}_{3}$ and $\mathrm{R}_{4}$. This cathode provides the screen potential for V2 and for this reason it is decoupled by a $16 \mu \mathrm{~F}$ capacitor $\mathrm{C}_{7}$. The grid leak of V1 is returned to a tapping point on the cathode resistor chain, $\mathrm{R}_{2}$ acting as the bias resistor. The wavetrap previously mentioned is also included in the cathode circuit and provides negative current feedback at the rejection frequency. It was decided to place the wavetrap in the cathode rather than the aerial circuit for two reasons; first, it avoids the mistuning effect of aerial waverraps; secondly, it avoids the marked changes in receiver sensitivity over the waveband caused by aerial wavetraps. This

latter effect has been discussed in an earlier article:The design of the wavetrap in this set depends on local conditions, and is described later.
The intervalve circuit is a bandpass filter, used to provide the necessary selectivity. Several methods of coupling were tried, and coupling by mutual inductance was adopted, because performance is quite satisfactory, and is simple to achieve. Wearite coils were again used, the coupling being obtained by adjustment of the spacing between coils. The filter consists of two PHF1 and two PHF2 coils for long and medit:m waves respectively ; unmodified PA2 coils are not suitable for this position because the large primary coil is self-resonant at the high-frequency end of the medium waveband causing a pronounced fall in $Q$ and receiver sensitivity at these frequencies. If PA2 coils must te used, this difficulty can be overcome by connecting a fixed capacitor of 200 pF (approximately) across the primary coil to shift the resonant point out of the medium-wave band.

Mutual-inductance coupling gives a pass band directly proportional to frequency; therefore for a

2 "Wavetraps," by S. W. Amos, Wireless World, January 1947

Fig. 1. Complete circuit diagram of the receiver. The primary windings $L_{7}, L_{9}, L_{12}$ and $L_{14}$ of the Wearite coupling coils ars left unconnected. All resistors are $\frac{1}{4}$-watt unless otherwise indicated.

given degree of coupling the required pass band can be achieved at one frequency only. Best results were obtained by spacing the coils to give optimum coupling (i.e., maximum gain) at $800 \mathrm{kc} / \mathrm{s}$ approximately in the medium waveband. Overcoupling is used on the longwave band, to preserve a reasonable bandwidth. The spacings necessary with PHF coils are indicated in Fig. 2.

An approximately constant pass band can be obtained by using a suitable combination of two forms of coupling, e.g. shunt capacitance and mutual inductance, and readers interested in using such mixed couplings can find design details in most standard textbooks ${ }^{3}$.

The anode-bend detector bias is provided by $\mathrm{R}_{7}$ and $\mathrm{R}_{8}$ in parallel, which carry the cathode current of V1 in addition to that of V2. This arrangement was adopted to enable a low value of cathode resistor to be used; this is necessary to preserve high d.c. gain. $\mathrm{R}_{8}$ is variable to enable the quiescent anode potential of V2 to be adjusted to equal the cathode potential of V1, i.e. to give zero quiescent suppressorcathode potential at V1. The screen of V2 is fed from the cathode of V1, so that in effect the screen voltage is stabilized. As mentioned in last month's article, this condition is also necessary for high d.c. gain. On receipt of a signal the average anode current of V2 increases and the anode potential falls, thereby applying negative bias to the suppressor grid of V1.
$C_{15}, R_{9}$ and $C_{16}$ form an r.f. filter, and $R_{10}$ is the volume control. It is permissible to control volume at this point because overloading of V 2 is prevented by the operation of the a.g.c. circuit. V3 is the output stage, and is of conventional design, but uses an SP61 for high gain. The anode load required is $20 \mathrm{k} \Omega$, and

[^2]

Fig. 2. Medium- and long-wove coil spacing in bandpass filter.
the maximum power output is approximately 1 watt.
The power pack is also of conventional design, resistance-capacitance smoothing being used as the total h.t. current consumption is relatively low ( 20 mA approx.).

If greater power output is required, an output valve of the 6 V 6 type may be used, but an output transformer of different ratio will be necessary to provide the output valve with the correct load. The smoothing resistor will need to be reduced or preferably replaced by a smoothing choke to provide the additional h.t. current whilst maintaining the h.t. voltage at the correct value of 230 volts.

The cathode of V1 is 100 volts positive (approximately) with respect to earth, and to reduce the heater-cathode potential to a reasonable figure, the centre-tap of the heater winding is returned to the junction of $R_{3}$ and $R_{4}$. The heaters are thus approximately 50 volts positive with respect to earth; this is advantageous because the resulting positive heatercathode bias reduces considerably the hum in the audio-frequency stages. Capacitor $\mathrm{C}_{5}$ is essential to prevent ripple voltages being fed to the cathode of V2. If the mains transformer has no heater centre tap, one side of the heater supply may be connected to the point $c$ in the cathode circuit of V1.
The layout of the receiver is illustrated in the photographs, and prospective constructors are advised not to depart radically from the arrangement of the r.f. section shown, as with such gain instability may occur.

In spite of the fact that the r.f. amplifier grid is under the chassis and the detector grid above the chassis, it was found essential to mount the aerial coils above the chassis, and the bandpass filter below. With the coil positions reversed, instability occurred due to coupling between the aerial and the bandpass filter.

It was found necessary to shield the aerial circuit switch wafer from the bandpass filter wafer, to avoid slight instability on long waves; only a small screen was required, actually a mounting bracket for a Yaxley-type switch.

A four-gang tuning capacitor was used, as these could be obtained relatively cheaply. The unused section separates the aerial section from the bandpass sections, and thus serves to reduce the chance of instability due to proximity coupling effects. A three-gang capacitor could, of course, be used, but there is a risk of instability due to proximity of aerial and bandpass sections.

The aerial circuit trimmers are mounted on top of their respective coils and the intervalve circuit trimmers are mounted alongside the respective coils with the adjusting screws projecting through the chassis. The wavetrap capacitor adjusting screw can be adjusted through a hole in the rear flange of the chassis. Thus all adjustments can be carried out with the receiver standing normally on the bench.

## Alignment

First, the suppressor of V1 should be strapped to the iunction of $L_{5}$ and $R_{2}$, to render the a.g.c. inoperative. This may give rise to some distortion due to detector overload during alignment, but such distortion should be ignored. Tune to a signal at the 550 -metre end of the medium band, and set the dial pointer on the capacitor shatt so that it indicates the wavelength correctily. Swing the tuning capacitors


Underside of chassis. Note screening bracket odjacent to aerial coil switch wafer.
" $S$ " meter, since its readings vary with received signal strength.

The third method does not require any meters. It will be found that the receiver is "dead" at one extreme setting of $\mathrm{R}_{8}$ and "lively" at the other extreme setting. With $\mathrm{R}_{8}$ set to the latter position, the receiver is tuned to a very weak signal, or noise. $R_{\text {, }}$ should then be rotated until it is at the point where the output of the receiver just begins in fall.

Once $\mathrm{R}_{8}$ has been correctly adjusted it should not require readjustment unless V1 or V2 is replaced. The receiver has been in continuous usc over a period of several weeks, including periods when the mains voltage was low, and there has been no need to readjust $\mathrm{R}_{8}$.
to the 200 -metre end of the band, and, using a relatively weak signal, adjust $C_{1}, C_{10}$ and $C_{12}$ for maximum output from the receiver, with the dial pointer indicating the correct wavelength. This adjustment may upset the calibration at the other end of the band, and it may be necessary to repeat the adjustments.

On long waves tune to a relatively weak signal near 1,000 metres and adjust $C_{2,}, C_{11}$ and $C_{13}$ for maximum receiver output, with the dial pointer indicating the correct wavelength.

It may be necessary to adjust $R_{8}$ initially to obtain signals, but in general this should not be so. After alignment has been completed the suppressor-cathode strap on V1 should be removed.

## Adjustment of A.G.C.

The quiescent anode potential of V2 must be adjusted to equal the cathode potential of V1, and the receiver should be switched on for at least ten minutes before this is done. The best method of making this adjustment is by the use of a highimpedance d.c. meter which is connected in turn to measure the anode-earth and cathode-earth potentials, whilst $R_{8}$ is adjusted to give equality of readings. The meter impedance must be high, preferably several megohms, because the anode potential of V2 is affected by the meter resistance.

Two alternative methods are available. A meter ( $0-10 \mathrm{~mA}$ ) may be connected in series with the screen feed of V 1, a $0.1-\mu \mathrm{F}$ capacitor being connected from earth to the screen side of the meter to avoid instability, and adjustment made in the absence of a signal. It will be found that at one extreme setting of $R_{8}$, the meter reading is a minimum of approximately 2.5 mA and at the opposite extreme a maximum of approximately 8 mA . $\mathrm{R}_{8}$ should be adjusted to the point at which the meter reading iust begins to incresse from its minimum value. Such a meter may be incorporated permanently in the receiver as an

The frequency to which the wavetrap, if required. should be tuned depends on local conditions. Details of the inductor used for rejection of the London Home Service are given in Fig. 3; the capacitor has a maximum capacitance of 450 pF . The number of turns required on the secondary winding $L_{6}$ depends on the rejection required and many be calculated as follows. The rejection of the wavetrap is given by

Number of decibels $=20 \log _{10}\left(1+g_{m} Z\right)$
where $g_{m}$ is the working mutual conductance of V1 and $Z$ is the impedance across $L_{6}$ at resonance. For 20 db rejection, which was considered adequate, $\log _{11}$ $\left(1+g_{m} Z\right)=1$, from which $1+g_{m} Z=10$, therefore

$$
Z=\frac{9}{g_{m}}
$$

With the screen-cathode voltage applied to V1, the working mutual conductance is approximately 4 mA volt. Therefore $Z=\frac{9}{0.004}=2,250$ ohms. The


Fig. 3. Details of the wavetrad inductor used to reject London Home Service.


Fig. 4. Comparative a.g.c. curves illustrating the performance of a superhet with iwo controlled valves and the t.r.f. receiver described in this article.
inductance of $L_{i}$ is approximately $160 \mu \mathrm{H}$ and the Q-value 150 . The dynamic impedance at $907 \mathrm{kc} / \mathrm{s}$ is thus given by

$$
\begin{aligned}
Z_{0} & =\mathrm{L} \omega \mathrm{Q}=160 \times 10^{-6} \times 6.284 \times 10^{3} \times 150 \\
& =137,000 \text { ohms }
\end{aligned}
$$

The impedance measured across $L_{5}$ is related to the dynamic impedance thus

$$
\frac{n_{1}{ }^{2}}{n_{2} 2^{2}}=\frac{\mathrm{Z}}{\mathrm{Z}_{0}}, \text { from which } n_{1}=n_{2} \sqrt{\frac{\mathrm{Z}}{\mathrm{Z}_{0}}}
$$

where $n_{1}$ is the number of turns on $\mathrm{L}_{5}$ and $n_{2}$ is the number on $\mathrm{L}_{\mathrm{f}}$.

$$
\text { Therefore } n_{1}=75 \times \sqrt{\frac{2,250}{137,000}}=9.6
$$

In fact 10 turns were used as shown in Fig. 3.
To reject signals at the high-frequency end of the medium waveband, it may be necessary to reduce the number of turns on both coils and/or the capacitance of the trimmer. To reject signals at the low-frequency end of the medium waveband, it may be necessary to increase the turns on both coils, but it should not be necessary to increase the capacitance.

The tuning of the wavetrap is best carried out after the receiver has been aligned, and before the suppressor cathode strap on V1 is removed.

## Valve;

An EF50 was used as r.f. amplifier, and cannot be replaced in this position by an SP61 because the SP61 has a long " tail" to its anode-current suppressor-bias characteristic, and gives poor a.g.c. performance for this reason. EF50's could be used throughout, without change of circuit values.

Constructors proposing to redesign the receiver using a valve other than an EF50 as r.f. amplifier, are advised to consult the valve characteristics, to ensure that the anode-current/suppressor-volts characteristic has reasonably early cut-off, not greater than 60-70 volts at the most.

## Performance

As mentioned before, the measured sensitivity is $20 \mu \mathrm{~V}$ on medium waves, and this does not vary appreciably over the whole band. On long waves the sensitivity is higher. The selectuvity is good, but
is masked by the a.g.c. action, which causes signals to " spread " over a relatively wide band. The a.g.c. is better than that of a superhet with two controlled valves, as shown by the curves in Fig. 4. The a.g.c. circuit arrangement used in this receiver is the subject of a patent application.

## LIMITS DF RADIO INTERFERENCE

## New British Standards Specification

ARECENTLY published revision of the British Standards Institution B.S. 800 defining new tolerable limits of radio interference, specifies the magnitude, duration and frequency of occurrence of radio interference which may be generated by various types of electrical appliances over the frequency band $200 \mathrm{kc} / \mathrm{s}$ to $1,605 \mathrm{kc} / \mathrm{s}$. The limits laid down are considered adequate for the protection from such interference of the majority of radio broadcast receivers operating within this band of frequencies.

The specification does not apply to the ignition systems of motor cars, nor to industrial, scientific and medical r.f. equipment, which are covered by other British Standards and Codes of Practice, nor to interference arising trom defective domestic apparatus.

The principal amendments in the new edition of B.S. 800 are :-
(a) Simplification of the technique of measurement of the noise voltage at the terminals of the interfering appliance.
(b) An increase in the permissible upper limit of the terminal noise voltage from 500 to 1,500 microvolts.
(c) Revision of the limits for the duration and frequency of occurrence of radio interference.
(d) Use of the "radio interference free mark," which was introduced in the 1939 edition of B.S. 800 but not brought into use owing to wartime conditions, is further postponed until the specification can be extended to cover television frequencies. This is necessary because electrical appliances which could satisfy the requirements in the $200-1,605-\mathrm{kc} / \mathrm{s}$ band might still cause intolerable interference in the television bands.

Copies of this new publication, B.S.800:1951 can be obtained from the British Standards Institution, Sales Department, 24, Victoria Strect, London, S.W.1, and the price is 3 s by post.

## RECORD PLAYER

## Design for the Home Constructor

IN response to requests for particulars of equipment suitable for use with " Goldring " gramophone pickups, the makers, Erwin Scharf, 49-51A, De Beauvoir Road, London, N.1, have issued a booklet (price 2 s ) which gives constructional details of a recommended amplifier and loudspeaker cabinet design.

An interesting feature of the loudspeaker is that the unit is placed horizontally and radiates into a corner of the room, with a spherical diffuser just above the diaphragm which is designed to give an apparent reduction in the size of the source of sound when reproducing speech.

The amplifier is of economical design and gives an output of 3 watts from a single tetrode, using 26 db of negative feedback A tone-compensated volume control is included and also a variable top-cut control.

## LETTERS TO THE EDITOR

The Editor does not necessarily endorse the opinions expressed by his correspondents.

## Reactivating Dry Batteries

RW. HALLOWS, who wrote in the October issue on this subject, may be interested to know that during the war years we supplied many hundreds of trickle chargers for reactivating l.t. batteries.

These were standard commercial 6 -volt chargers, and were connected to a 4.5 -volt battery for about 30 minutes The off-charge voltage then rose to about 6.0 and it was important that the battery was not used for a few hours after charging. With the increased supply of 1.t. batteries after the war very few chargers remained in use, despite the considerable saving in cost. It appeared that the consideration was the saving of batteries rather than the saving of expense.

The N.P.L. tests quoted revealed results comparable with our own findings, but the advantages of recharging are, of course, considerably less with present-day hearing aids, owing to the low l.t. and h.t. currents of about 30 mA and 1 mA respectively. A. EDWIN STEVENS.

Amplivox, Ltd.,
London, W.1.

RPECHARGING, restoring or reactivating dry cells is not new. The process has been used commercially in U.S.A. and a description of experimental and commercial equipment was given in Q.S.T. for June, 1944.

Suggested starting currents for charging were given as:-

| Size of cell | Current, mA |
| :---: | :---: |
| $1 \frac{1}{8} \mathrm{in} \times 3 \frac{1}{2}$ in | 10-15 |
| $1 \frac{1}{8}$ in $\times 1 \frac{1}{2}$ in | 7.5-10 |
| ${ }_{3}^{3} \mathrm{in} \times 1{ }_{8}^{1}$ in | 5-10 |
| $\frac{1}{2} \mathrm{in} \times 1 \frac{1}{2} \mathrm{ir}$ | 5-7.5 |

A fairly standard charging time of 22-24 hours seems to be satisfactory for discharged cells.

These notes may be useful for amateur experiment.
It is stated that with correct treatment $75-90$ per cent of all used cells can be restored to give from 10 to 25 times original service.

THOMAS G. WARD.
Bideford, N. Devon.

## Crystal Menace?

ADMITTEDLY the possibility of harmonic radiation, mentioned by C. Kidd in your October issuc, was not one of the factors considered when designing the Modern Crystal Set (Wireless World, September, 1951), but the two tuned circuits, one having unusually high capacitance, might be expected to make the effect very small. A test since made confirms this expectation.

The set was tuned to the London Home Service, the crystal current being 100 A , and a sensitive communications receiver on the same bench was connected to an acrial 20 feet away, led in through a screened lead. Completely independent earthing was not feasible, so the sets shared an earth lead from the first floor to ground level. Under these conditions weak harmonics were detected up to the seventh. The strength of the most powerful one, the third, was equivalent to a 2.5 -microvolt signal. When the $200-\mathrm{kc} / \mathrm{s}$ Light Programme was tuncd in with a crystal current of $4 \mu \mathrm{~A}$ no harmonics whatever could be detected.

On the indication of these results no further measurements or consideration of redesign seemed necessary. In reaching this opinion I took into account two other points. The first was that in regions of very high signal strength where incidentally there is nearly always already severe re-radiation from other non-linear elements listeners will tend to use a small acrial aperiodically coupled to the parallel-tune modification of the set. The other was that any modifications that occurred to me,
including the fairly obvious one of substituting bottom capacitance coupling for the present arrangement, have minor disadvantages which make their adoption a pity unless they are really essential.

If anyone in the London area has made tests which show that the matter ought not to be so lightily dismissed I shall be most interested to hear his results.

General Electric Company, B. R. BETTRIDGE.
London, W.C. 2.

## Diathermy Interference

I IKE R. Cussins (your Sept. issue), I too have observed 1 an objectionable interference pattern on several types of television receivers, both of t.r.f. and superhet designs. The pattern takes the form of a "herring bone" or "oak grain" band across the screen and occupies approximately one third of the height. Its position on the screen is usually fairly stable although pattern design may change slightly.

I have been informed from several unofficial sources that the cause of this interference is diathermy equipment. Having had some experience in the design of such apparatus several things puzzled me concerning the nature and existence of thie pattern.

One was that the pattern was not present when the Holme Moss transmissions were off the air, another was the evidence of modulation (a.f.) on the pattern, and a third was the considerable range attributed to the suspect diathermy equipment.

It was while studying a particularly pronounced specimen of this interference that I solved the first two puzzles. The pattern was obviously the result of a beat frequency caused by the harmonic or fundamental of some signal and that of Holme Moss transmission.

By injecting into the aerial sockets of a television receiver a pulse modulated frequency variable about 51$\mathrm{Mc} / \mathrm{s}$ and a fixed c.w. signal of $51 \mathrm{Mc} / \mathrm{s}$, I managed to reproduce the indentical interference pattern.

Further experiments pro:ed, as was expected, that the two signals had to have good stability to maintain the pattern constantly in its position on the screen.

Slight variation in stability caused the inside detail pattern to change without its position being altered.

Knowing the approximate power ratings of diathermy equipment, and also the degree of stability to be expected of its frequency adjustment (the patient forms part of the resonant circuit) I doubt if diathermy is the source of the interference.

Reports of this type of interference are being received from places twenty miles away from the nearest hospital.

It would appear that attention should be paid to other possible sources such as radar stations, aircraft beacons and navigation installations I would hasten to add, however, that before an onslaught be made upon the "authorities" demanding the elimination of such stations, a little further analysis of the pattern should be made.
H. W'ILLAN CRITCHLEY.

Scarborough, Yorks.

## Automatic Monitoring

R DANZIGER, writing in your August issue, scems to think that the general principles used in the B.B.C. automanc monitors, discussed in a recent I.E.E. paper, are those described by him in your June, 1948 issue.

He has evidently missed the main reasons for the successful application of Automatic Monitoring to the B.B.C. system.

First, it is not practicable 10 balance out programme signals which are derived from the two ends of even a relatively short (electrically) system. Phase distortion (or delay) on the connecting transmission line and its asso-
ciated apparatus, although it may be inaudible to the listener, prohibits this unless a very rough degree of balance is acceptable. We have used a rectified output arrangement to overcome this trouble and obtain balances which permit the detection of noise components $40-50 \mathrm{db}$ below programme peaks.

Secondly, we have provided the facility in the circuits, not only to give the proper relative aural sensitivity at both high and low levels, but to render the monitor properly proportioned to other forms of distortion such as frequency response, overload and transmission equivalent changes.

I would like to make it quite clear that any claim to success in our automatic monitors is not that we were the first to wish that programmes could be so monitored, but, as far as I know, we were the first to attain a reliable monitor that wouid on the average be at least as good as the man it replaced.

Actually, work on circuits basically similar to that suggested by Mr. Danziger was attempted in the B.B.C. considerably before 1948, but no claim was published as successful application of the design was regarded as the criterion of its value.

It is relevant to note that by early 1948 our final laboratory models had worked successfully and the first provisional patents were filed in June of the same year.
I.ondon, W.1.
F. A. PEACHEY.
B.B.C. Designs Department.

## Units in Indonesia

IN your August issue A. C. Kay suggests a new unit of capacitance.
In my personal opinion this is undesirable and even unnecessary if another metric value, the $n F$ (nano-farad) could be accepted for one-milliardth of a farad, in addition to the $\mu \mathrm{F}$ for one-millionth of a farad and the pF for onc-billionth of a farad, already adopted in most countries.

Thus $0.001 \mu \mathrm{~F}=1 \mathrm{nF}=1,000 \mathrm{pF}$.
Originally introduced-so far as I know-in Germany and also used in other Continental countries before the war, this nano abbreviation is now, in the Indonesian PTT, as normal as km for length of wire. Of course, it took a few months before everyone was used to this $n$ and there was some confusion with $n$, but now we just don't understand why anybody still writes $0.015 \mu \mathrm{~F}$ if he actually means 15 nF .

In circuit diagrams one can leave out $F, \Omega$ and $H$, since it is obvious that a resistor is $\Omega$ and not $F$ or $H$. For exampie:


Still one step further is the use of a code in which no dot appears; this is quite convenient since some countrics use commas instead of dots. In this system,
which is used by some manufacturers to indicate their parts, 1 ms means 0.0015 H and 2 n 2 means $0.0022 \mu \mathrm{~F}$ and M47 means 0.47 M 4 , etc.

Radio Division, PTT,
V. J. de GRIJS.

Bandung, Indonesia.

## "The Modulation Battle"

$\mathrm{M}^{\mathrm{R}}$R. BEAUMONT'S letter in your October issue fills me with amazement. Being already biased in favour of a.m., perhaps I got the wrong impression, but I thought the matter was solely one of economics and politics. The engineer may grant a small advantage to f.m., but his business is to provide the cheapest equipment to do a given job.

With regard to politics: the B.B.C. would prefer f.m.; it saves them money, even if relatively a small amount. The Government would also prefer f.m.; the higher cost of receivers means more purchase tax.

London, N.W.S.
W. M. DALTON.

## Recording Studios

READ with interest the excellent article by P. A. Shears on acoustic treatment of small recording studios ( $W$.W. September, 1951). Perhaps it will stımulate many home recordists to embark upon the oft-neglected art of studio treatment. The reverberation formula Mr. Shears gives as Eyring's is actually that due to Millington. Eyring's formula is

$$
T=0.05 \mathrm{~V} \text { S loge }(1-\mathrm{Xav})
$$

where Xav is the average value of absorption coefficient for the room. This formula gives less tedious calculations than Millington's.

Mr. Shears does not mention that preferred dimension ratios exist for room proportions. This is important in order to prevent several low-frequency eigentones occurring at nearly the same frequency. Height, width, length ratios of 1 : $1.26: 1.6$ are considered satisfactory for small studios.

The eigentone formula given is only exact for rectangular flat-walled rooms with completely rigid boundaries, but gives a useful approximation in many practical cases.

Panel absorbers of the type described have to be rather carefully designed and erected, as there is a risk that if their " $Q$ " is too high they will continue to emit sound after being acoustically excited and thus give reverberant sound "coloration" at their resonant frequency. Unless carefully mounted, panels may also produce buzzing or rattling noises when strongly excited. Similar enclosed resonant absorbers consisting of a volume covered with lino or roofing felt in place of a semi-rigid panel are now claimed to give similar absorption coefficients without the above disadvantages of panels.

A useful and low-priced book which might be added to the references is "Applied Architectural Acoustics" by M. Rettinger (Chemical Publishing Coy., Inc., Brooklyn, Ne: York)

London, S.E. 18.

## Redundant Word?

ON page 422 of the October issue of Wireless World appears a concocted word which I submit should not exist in a journal generally accepted to be of value in the education of technical people. This obnoxious word "wattage" is natural to the ignorant who do not appreciate that the watt is a unit of power, or rate of working.

It is unfortunate, I know, that the word "voltage" is perforce in common use since with alternating quantities the usual unidirectional terms tend to be meaningless, but this exception is no excuse for replacing a perfectly good word "power" by "wattage," any more than for the common mistake made by the uninitiated in referring to "amperage" (ugh!) when the correct lerm is "current."

London, N. 8 .

# Paris Television <br> Show 

Domestic Receivers for Two Standards

By A. V. J. MARTIN*

THE first specialized television exhibition in the world was held in Paris at the Musée des Travaux Publics from September 28th to October 10th, under the name Premier Salon de la Télévision. It met with great success and at the week-ends the crowds of visitors were such that the organizers had to limit the number of admissions. The possibility of prolonging the exhibition for a few days was considered, but other arrangements had been made and it proved impossible.

The organizers were the Télévision Française authorities and the Syndicat National de la Construction Radioélectrique. Excluding the Press, there were 23 exhibitors. Three of them were acrial makers, two were valve and c.r.t. manufacturers, and the remaining 18 were television set makers. The Télévision Française had made a big effort and put up a complete studio comprising a semi-circular stage, about 21 yards in diameter, surrounded by 800 seats for the public. Four dual-standard cameras (441/819

## * Editor. Télévision, Faris.

Model for 819 lines by Radio-Industrie. It has a 10 -in flatfaced tube and 22 valves. Below: Receiver with 12 -in tube by Ducretet-Thomson. Available for 441 lines with 16 valves or 819 lines with 19 valves.


The $\quad 185-\mathrm{Mc} / \mathrm{s}$ turnstile vision aerial on top of the Eiffel Tower.

lines) were in use and the scene was lit by projectors with a total power consumption of 300 kW . The " live" cameras were supplemented by films run from a film-scanner, which could be seen by the visitors through a glass panel. Programme material, either direct or from films, was available to the exhibitors continuously from opening till closing time.

The v.f. signals originating in the Salon were sent by coaxial cable to outside-broadcasting vans packed in the street and thence by $30-\mathrm{cm}$ microwave link to the studios of the Télévision Française. There they were demodulated, controlled and amplified, and sent to the Eiffel Tower transmitters through the usual coaxial cable. Depending on the standard in use, they went either to the old 441 -line transmitter at the foot of the Tower and by coaxial cable to the aerials on top ( $46 \mathrm{Mc} / \mathrm{s}$ vision), or to the new 819 -line transmitter on the fourth floor of the Tower and by a very short coaxial link to the 4-bay turnstile aerial ( $185.25 \mathrm{Mc} / \mathrm{s}$ vision). The accompanying sound was radiated on $42 \mathrm{Mc} / \mathrm{s}$ for the 414 lines and on $174.1 \mathrm{Mc} / \mathrm{s}$ for the 819 lines.

Thus in both cases the programmes were received at the Salon in the usual way through the standard transmitters, and the televisors were shown under actual working conditions. The three aerial makers exhibiting had supplied and installed on the roof of the building the necessary banks of aerials for both the standards, and the signal was distributed to the stands by ordinary coaxial feeders.

## On the Stands

Altogether 81 different receivers were shown. Most exhibitors had a standard chassis in different cabinets-some of these incorporated a broadcast receiver or a record changer, and others were for long-distance reception with one or two r.f. preamplifier valves. Seventy per cent of the sets were for the high-definition 819-line standard and included six dual-standard 441/819-line receivers. The number of valves varied between 15 and 22 for 441 lines and between 14 and 23 for 819 lines.

There were remarkably few projection receivers. Fifty per cent of the sets had 12 -in tubes, ten per cent had 14 -in tubes, and the other sizes, varying from 6 in to 24 in , were each under five per cent of the total. Table models were in a majority and were followed second and third by consoles and large-size combination models. Sensitivities ranged from 10 uV (longdistance) to 500 MV (local). There were frequently two versions of the same receiver, one for 441 lines $(46 \mathrm{Mc} / \mathrm{s})$, generally of the t.r.f. type, and one for 819
lines ( $185.25 \mathrm{Mc} / \mathrm{s}$ ), always a superhet. For the same sensitivity there was a difference of two to four valves between the two versions. The high-definition sets were up to twenty per cent dearer, though some makers were actually offering both versions at the same price.

The three acrial makers exhibited a wide range of products for both standards, from a smallsize "compressed" indoor aerial to an array of stacked fiveelement Yagis on a telescopic $59-\mathrm{ft}$ aluminium mast. One of the makers, Portenseigne, had a stand illuminated by ultra-violet light and the aerials were coated with fluorescent paints of different colours. The effect was striking, especially as the background was an enlargement of a photograph of the Paris rooftops where all the television aerials were also fluorescent. Belling \& Lee and Antiference were represented by their French distributors.

There were also two valve manufacturers. Mazda were showing the noval series and flat-faced c.r.ts and had a large-size luminous exhibit demonstrating ion-trap working. Visseaux had American-type tubes and flat-faced, metal-glass and all-glass rectangular tubes up to 20 in diagonal.

This exhibition was the first opportunity for the set makers to meet the public at large and take advantage of their remarks. Two general trends were evident: the set buyer wants a high-quality picture and he also wants a large-size picture. This last remark excludes, at least this year, the projection televisors, which are thought to lack brilliance and contrast. Regarding the first trend, high definition has, beyond the shadow of a doubt, been victorious in what we call "the cold war of the lines." Mr. Everybody has, at last, had a chance to see similar sets working side by side under similar conditions

Midget set with $6 \frac{1}{4}-\mathrm{in}$ tube by Sonora. The cabinet is an aluminium casting.



Dual-standard (441 and 819 lines) console by Ducastel, available with 12-in or 14 -in tube.
on both standards and does not hesitate a second-he wants the better picture provided by the 819 lines and reacts strongly against the lininess of the old 441 standard, especially on the large pictures he likes. What is more, he thinks that the difference in price is more than counterbalanced by the difference in quality and does not care a farthing about bandwidths and international agreements. As for the picture size, it is evidently linked with the fact that he is interested only in the 819 lines; the minimum size seems to be the 12 -in tube and interest is strongly directed towards flat-faced 16 -in and 20 -in tubes, preferably of the rectangular type which permits smaller cabinets.

Generally speaking the prices are high, mainly because televisors are not mass-produced in France at the moment. It is thought, however, that the exhibition will go a long way towards increasing the popular appeal of television, and a very substantial cut in prices, from 30 to 50 per cent according to the makers, is expected as soon as largescale production begins. For the moment, prices are such that television is within reach of only the richest part of the public, and this probably explains the trends towards quality and large size, even at higher cost. Nevertheless, top quality certainly and large pictures probably are good foundations upon which to start a television industry.

## Odds and Ends

The smallest and cheapest receiver in the show: the miniature Sonora, $16-\mathrm{cm}$ tube (over $6-\mathrm{in}$ ), 90 deg deflection angle, 14 rimlock valves, 441 lines, £54 10s (or 14 noval valves, 819 lines, $£ 69$ 10s). The biggest direct viewing tube: 24 in in an 819 -line receiver by Ducretet-Thomson. . . . The most expensive receiver: a beautiful piece of furniture in mahogany (outside) and sycamore (inside), including a flat 16 -in tube, 819 -line televisor, 12 -band broadcast receiver, and three-speed record-changer, by TéléAriane, price 5550 ... The biggest cabinet: by Philips, the Jumbo type for clubs, cafés, etc., with a 48-in diagonal picture (Schmidt projection system). ... The largest picture: 84 in diagonal on an outside screen, given by a Radiola projection receiver in two transportable cases. . . . The use of a 7-in electrostatic tube: by L.M.T. in a popular-priced receiver.
Dual-standard televisors: the Ducastel models for both 441 and 819 lines with switch selection.

## Imitation Nickel Plating

INN view of recent Government restrictions on the use of nickel for plating purposes, manufacturers will be interested in the imitation nickel-plate finish given by "Nicklit," a product of Metal Processes, Ltd., Kingsbury Road, Erdington, Birmingham, 24. This can be applied to brass and copper-and steel, too, if it is first coppered or brassed-by simple immersion in a warm chemical bath. There is no deposit-only a chemical change in the metal itself-so that the existing surface remains unaffected.

# Recording Television History * Amateur Show . International Brit.I.R.E. * F.M. for Amateurs * Transcontinental Television 

## Baird Plaque

"IN 1926 in this house John Logie Baird (1888-1946) first demonstrated television." This wording is on a plaque erected by the London County Council on 22, Frith Street, Soho, which was unveiled by Sir Robert Renwick, K.B.E., president of the Television Society, on October 24th.

It was on January 27th, 1926, that Baird gave a demonstration to some forty members of the Royal Institution and other visitors in an upper room in the house, using the apparatus that is now in the Science Museum, South Kensington. Although Baird and others had previously given demonstrations of televised silhouettes, this was his first demonstration of pictures with gradations of light and shade. When writing Baird's obituary-he died on June 14th, 1946, at the age of 58-we stated "His greatest contribution to television may be summed up in the words, "he was the first to make it work.'"

## B.B.C. Report

THE oblique references to the preference of the B.B.C. for f.m. for the proposed chain of v.h.f. stations are substantiated by the statement in the B.B.C. Report for 1950/51* that "a recommendation for the use of frequency modulation on v.h.f. was submitted to the Government, together with an outline proposal for a chain of stations through the country to give listeners the Home Service, the Light Programme, and the Third Programme on f.m."
The Report also states that, so far as colour television is concerned, it is hoped that the radio industry will design and manufacture equipment which can be thorougbly studied and tested before any decision about a future colour television system for public service is made.

## Amateur Radio Exhibition

THE fifth annual amateur radio exhibition, organized by the Radio Society of Great Britain, will be opened by Charles I. Orr-Ewing, O.B.E, at 12 noon on November 28th, in the Roval Hotel, Woburn Place, London W.C. 1 On each of the suzceediny three days it will open at 11 and w:L close daily at 9 p.m.
In addition to the stands of the fourteen exhibitors, there will be an exh.b.tion of home-built amateur

[^3]radio gear lent by R.S.G.B. members. The exhibitors include:-Air Ministry (R.A.F.), Admiralty (R.N.V.(W.)R.), Avo, Cosmocord, E.M.I., Eas.bind, English Electric. G.E.C., Panda Radio, Philpott's Metalworks, Salford Electrical Instruments, Short Wave Magazine, Television Society, Wireless World and Wireless Engineer, and Woden Transformer.

Demonstrations of equipment will be given during three one-hour periods each day. Admission is 6d.

## Brit.I.R.E.

A the recent annual general meeting of the Bratish Institution of Radio Engineers it was announced that H.R.H. the Duke of Edinburgh had accepted Honorary Membership of the Institution, of which his uncle, the Earl Mountbatten, is Vice-patron.

The topographical list of members of the Institution shows that, of the 56 countries in which membership is distributed, India has more than any other country overseas. The general secretary of the Institution (G D. Clifford) is therefore visiting India in the near future with a view to establishing Sections under an Indian Advisory Committee His itinerary includes Bombay, where there is already a Section, Delhi, Calcutta, Madras and Jubbulpore.

A convention will be held in Bombay in February with papers on the development and application of radio and electronic engineering in India.

At the annual meeting the following members were re-elected to office: Paul Adorian, president; W. E. Miller and L. H. Paddle, vicepresidents; and Sir Louis Sterling, J. L. Thumpson, Grp. Capt. S. Lugg and N. C. Cordingly, members of the Council. In addition, G. A. Marriott, Prof. Emrys Williams and G. Wooldridge were elected to the Council.

## Now Readv

T
HE Wireless World Diary for 1952 is now available from booksellers and stationers. This useful diary and reference book, now in its 34th year of publication, is a veritable mine of information of the sort that is so often wanted by radio men and yet not available in tabloid form.

As usual, the diary gives a week at an opening and the 80 -page reference section includes base connections for 670 valves, useful formulx, graphical design data and considerable general information. It is available in morocco leather at $6 \mathrm{~s} ~ \$ \frac{1}{2} \mathrm{~d}$, or rexine at $4 \mathrm{~s} 3 \frac{1}{2} \mathrm{~d}$ (including Purchase Tax).

## Radio and Rearmament

TT will be recalled that it was announced in the House a month or two ago that a committee was to be set up through which liaison between the Ministry of Supply and the radio industry could be maintained on matters affecting defence.
The radio industry representatives on the Radio Rearmament Advisory Committee, as it is called, which held its first meeting at the end of September, have now been announced. They are: A. G. Clarke (Plessey), L. T. Hinton (S.T.C.), M. M. McQueen (G.E.C.), F. S. Mockford (Marconi's), E. J. Power (Murphy), J W. Ridgeway (Ediswan), E. E. Rosen (Ultra), and C. O. Stanley (Pye).

## New Amateur Facilities

FREQUENCY modulation and pulse modulation are now permitted to be used by amateurs in the United Kingdom. Announcing this, the R.S G.B. states that, as a result of representations by the Society, both pulse amplitude and pulse width modulation are to be permitted within the $2,350-2,400,5,700-5,800$ and $10,050-10,450 \mathrm{Mc} / \mathrm{s}$ bands. A $50 \mathrm{Mc} / \mathrm{s}$ guard band is thereby provided at each end of the normal amateur bands. Power will be limited to 25 watts mean d.c. input and 2.5 kW peak r.f. power.

Frequency modulation will be permitted temporarily for one year on frequencies between 144.5 and $145.5 \mathrm{Mc} / \mathrm{s}$ provided that no interference is caused with Government services.

A further band has been allocated for television transmission - 425$455 \mathrm{Mc} / \mathrm{s}$ with a maximum d.c. input power of 25 watts. This decision has been made following test transmissions by R.S.G.B. members in collaboration with the Air Ministry and the Ministry of Civil Aviation.

## Coast-to-Coast Television

ALTHOUGH America's transcontinental television radio-relay link was used initially on September 4th for the transmission of scenes from the Japanese Peace Treaty Conference at San riancisco, it was not officially opened until September 28th. The overall length of the chain of 107 radio-relay stations is 2,992 miles, the distance between stations varying from 19 to 50 miles.

The system will ultimately employ six channels in each direction, operat-
ing on frequencies in the $3,700-$ $4,200 \mathrm{Mc} / \mathrm{s}$ band, although initially only one is in use. To avoid interference due to "skip transmissions" two frequencies separated by $40 \mathrm{Mc} / \mathrm{s}$ are used alternately on each channel along the route.

It is reported that 94 of the country's 107 television transmitters were linked to the "circuit" for the initial transmission.

## International Acoustics

THE first issue of Acustica, the international journal on acoustics, sponsored by the Acoustics Group of the Physical Society in this country and similar organizations in France and Germany, has now made its appearance.

The aim of the journal is "to cover the science of acoustics in all its aspects - theoretical and experimental, purely scientific and applied." Articles are in English, German or French with summaries in the alternative languages. Acustica will be issued six times a year, for which the subscription is 36 Swiss francs. The British representative on the Editorial Board is Dr. E. G. Richardson, of Kings College, Newcastle-on-Tyne, and the publisher, S. Hirzel, Claridenhof, Gotthardstrasse 6, Zurich, Switzerland.

## Fire Risks

FIRES caused by broadcast and television receivers during the years 1947-49 are analysed in the report of the Fire Research Board of the D.S.I.R. published by H.M.S.O. under the title "Fire Research, 1950." The table showing the rate of incidence of fires reveals that whereas the number of fires per 10,000 licensed broadcast receivers (including radiograms) has increased from 0.21 in 1947 to 0.34 in 1949, the figures for television sets have decreased from 6.4 to 3.7 during the same period.

The facts given in the report are more reassuring than those quoted in our Editorial in January this year, when the figures given by a responsible member of the Home Office indicated that the curve was rising very steeply.

## Athlone Fellowships

ToOnable Canadian engineering graduates to take post-graduate training in this country, thirty-eight Athlone Fellowships are to be awarded by the Government each year.

These Fellowships, of which 28 will be awarded annually to newly graduated candidates and ten to graduates from industry, will be tenable normally for two years.

Three of this year's holders of Fellowships are taking post-graduate courses in electronics at Imperial College, which, in one case, will be followed by a year's research at 'T.R.E.

## Speed of Light

THE apparatus used by the N.P.L. in the experiments which showed that the figure normaliy accepted as the speed of light was inaccurate by eleven miles a second, is now on show and will be demonstrated at the I.E.E., Savoy Place, London, W.C.2, until the end of November.

A cavity resonator is used in which a radio wave is reflected backwards and forwards between the two ends. When the time of travel between the ends equals the time interval between successice waves, they build up to an electrical resonance which can be detected with very high precision. The waves follow one another at a frequency of 10 thousand million per second ( $10 \mathrm{kMc} / \mathrm{s}$ ) and it is necessary to measure this frequency with an accuracy better than one part in a million.

## Radio and Power Cuts

WHILST on the one hand the B.B.C. is co-operating with the British Electricity Authority by broadcasting warnings of impending power cuts, criticism is levelled against it in the electrical press for its inconsistence in its approach to the problem of the power supply position at peak hours. Our associate journal, Electrical Review, criticizes the lengthening of the children's hour on television during a period in which the highest peak load occurs in winter. The Electrician gives figures of the increased power consumption during the recent broadcast on the Turpin-Robinson fight in New York. During the half an hour of the broadcast $100,000 \mathrm{kWh}$, requiring about 70 tons of coal, were consumed.

The warnings of impending electricity cuts are to be broadcast by the B.B.C. on 1,500 metres between $7.30 \mathrm{a} . \mathrm{m}$. and 12.30 p.m., and 3 p.m. and $6 \mathrm{p} . \mathrm{m}$. In addition, arrangements have been made with relay organizations to interject warnings in the transmitted programmes.

## l'ERSONALITIES

H.R.H. The Duke of Edinburgh. F.R.S., has accepted the office of President of the City and Guilds of London Institute for the Advancement of Technical Education. As already recorded His Royal Highness has also accepted Honorary Membership of the British Institution of Radio Engineers.
J. T. Marler, who joined the Marconi International Marine Communication Co.'s Dalston Works in 1907, has been appointed manager of the company's Operating Division in succession to $S$. Stansbridge, who recently retired. He will continue to represent the company on the Radio Officers' Panel of the National Maritime Board.
J. McG. Sowerby, B.A., M.I.E.E., who is a frequent contributor to Wireless World, has left CincmaTelevision, Ltd., where he has been
concerned with the design and development of electronic instruments since 1946, and joined English Electric, Ltd. From 1940 to 1946 he was with the Ministry of Supply and was responsible for the design and development of electronic instruments for Chemical Warfare Research.

## OBITUARI

The death occurred on September 7th of Commander F. G. Loring, O.B.E., R.N., M.I.E.E., at the age of 82. After his naval career, during which he specialized in wireless telegraphy, he was appointed, in 1908, the first Inspector of Wireless Telegraphy at the Post Office. On his retirement from the Post Office in 1930 he became a director of the International Marine Radio Co.
Dr. Anton Philips, who, with his brother, founded in 1891 the electric lamp factory which has grown into the world-wide Philips organization, died at Eindhoven, Holland, on October 7th at the age of 77.
C. H. G. Hobday, managing director of Hobday Bros., died on September 1st at the age of 52 .

## IN BRIEF

Receiving Licences.-Approximately $12,443,850$ broadcast receiving licences, including 933,050 for television, were current in the U.K. at the end of August, an increase of 8,950 during the month. The month's increase in television licences was 17,850 , the lowest since July last year.
Components Exhibition.-Next year's exhibition of components, organized by the Radio \& Electronic Component Manufacturers' Federation, will be held from April 7th to 9 th at Grosvenor House, Park Lane, London, W.I.
French Decca Chain.-The French Government has ordered from the Société Française Radio-Electrique, licensees of the Decca Navigator Co., a chain of Decca stations.
Dutch Television. - The Netherlands broadcasting authority (a corporate body on which is represented the four major broadcasting organizations) has brought into regular use-although at present only twice a week-its first television station. It is operating on the proposed C.C.I.R. standards- 625 lines, negative modulation, vestigial sideband transmission (upper sideband retained) and f.m. sound. The $5-\mathrm{kW}$ Philips vision transmitter operates on 62.25 $\mathrm{Mc} / \mathrm{s}$ and the sound transmitter on $67.75 \mathrm{Mc} / \mathrm{s}$. Transmissions are horizontally polarized.
S.W. Listeners are invited by the International Short Wave Club to participate in a competition designed to encourage the sending of better reports of short-wave reception. Postcards, giving details of the reception of an amateur or broadcasting s.w. station, should be sent to A. E. Bear, 100, Adams Gardens Estate, London, S.E.16, before January 1st.
"The Old N'Ions," as members of the Northampton Engineering College Past Students' Association are known, will be holding their twenty-fourth annual dinner and reunion on November 30th at the Connaught Rooms, London, W.C.2. Particulars are obtainable from R. W. C. Gilbert, 6, Ella Road, London, N. 8 .

New B.B.C. Stations. - Two more of the twelve proposed low-power stations to improve reception of the B.B.C. Home Service in certain areas came into operation on October 7th at Whitehaven (692 $\mathrm{kc} / \mathrm{s})$ and Barrow ( $1,484 \mathrm{kc} / \mathrm{s}$ ). Both transmitters will ultimately have a power of 2 kW , but initially are lower.

Servicing Exam.-The results of this year's Radio Servicing Certificate Examination, held jointly by the Radio Trades Examination Board and the City and Guilds of London Institute, show that of the 290 candidates for the examination held in May, 117 passed in both the written and practical tests. Forty-six candidates passed the writen examination but were referred in the practical test, and 19 candidates who were referred in the 1950 practical test completed the examination.

Wharfedale Wireless, the publishers of the book "Pianos, Pianists and Sonics," by G. A. Briggs, which was mentioned in our August issue, are organizing an essay competition on (a) Which in your opinion is the most interesting chapter in the book, and why? and (b) Which chapter do you find the least interesting, and why? Entry forms and details are available from Wharfedale Wireless Works, Idle, Bradford, Yorks.

Sets for Fijians.-In order to encourage the import of cheap broadcast receivers it is proposed to waive the duty on approved sets. An importer, R. O. Sharma, P.O. Box No. 8, Nadi, Fiji, who will be glad to receive information from interested manufacturers, advises us that the sets should cover the short-wave bands (with bandspread tuning) in addition to the m.w. band. As mains supply is not available in the majority of areas, the sets should be of the "all-dry" type.

Correction.-In the review, on page 403 of last issue, of the new book "Magnetic Recording," by S. J. Begun, a printer's error occlirred in the name of the company with which the author is associated. It is, of course, the Brush Development Company.
F.M. in Germany.-According to a correspondent, all but the cheapest broadcast receivers on the market in Germany now incorporate both a.m. and f.m. There are some twenty stations operating at present and about as many being built. The agreed i.f. is $10.7 \mathrm{Mc} / \mathrm{s}$.
U.S. Radio Chief.-President Truman has appointed Haraden Pratt, who has been secretary of the Institute of Radio Engineers since 1943, as his personal adviser on telecommunications.

World Radio.-According to figures published in the September issue of our New York contemporary, Tele-Tech, the western hemisphere, which has approximately 14 per cent of the world's population, has 75 per cent of the world's transmitter power. So far as the United States is concerned, it has, according to Tele-Tech, 65 per cent of the world's transmitter power, just over 50 per cent of the broadcast receivers of the world and 98 per cent of its television sets.
Canada's Department of Transport announces the appointment of F . G. Nixon as Assistant Controller of Telecommunications in the Department. Prior to joining the Radio Division of the Transport Department in 1937 he was doing research work with the National Research Council.
School Television. - Experimental transmissions of television for schools is planned by the School Broadcasting Council and the B.B.C. for next summer. During the experimental period selected schools will be equipped with marious types of receivers-directviewing and projection-and the industry is being asked to co-operate.

City and Guilds,-The new secretary of the City and Guilds of London Institute, in succession to G. C. Stephenson who has filled the post since 1924, is J. W. Voelcker, B.Sc., A.M.I.E.E., who, since returning to this country from the U.S.A. in 1925, has been with English Electric. He is honorary secretary in this country of the Massachusetts Institute of Technology and president of the M.I.T. Club of Great Britain.


RADAR MOSA!C of the Solent. Spithead and Southampion Water compased of twenty-one photographs of the p.p.i. presentation on a Decca Type 159 B marine radar set installed in the Company's motor yacht "Navigator.

Danish Television.-Regular onehourly transmissions on alternate weekdays began from the Danish television station on October 2nd. The experimental transmissions were stopped some months ago. The Copenhagen 625-line 100 -watt vision transmitter operates on $62.25 \mathrm{Mc} / \mathrm{s}$ with negative modulation. Double sideband transmission is cmployed. The f.m. sound transmitter operates on $67.75 \mathrm{Mc} / \mathrm{s}$ with a power of 50 watts. Transmissions are horizontally polarized.

Cable \& Wireless announce additions to both the Middle East and West Indian radio services. The CyprusUnited Kingdon radio-telephone service, which was opened last May, is now extended to the U.S.A., Canada, Cuba, Mexico and parts of Europe. In Lybia, the company's stations at Tripoli and Benghazi are being equipped for radio-telephone services, which will operate between both these points, and between them and Malta, with extensions to the United Kingdom. A radioteleprinter circuit is now operating between Bermuda and Montreal, and the Jamaica-Nassau radio-telegraph circuit has been replaced by a similar circuit between Bermuda and Nassau.
E.I.B.A.-The Electrical Industries Ball, organized in aid of the funds of the Electrical Industries Benevolent Association, will be held at Grosvenor House, Park Lane, London, W.I, on November 9th. In the report of the Association for 1950 donations from a number of radio concerns are acknowledged, including $£ 193$ collected at the London luncheons of the Radio Industries Club, £ 160 from the R.I. Club Ball, and £113 from the R.I. Club Glasgow.

Marconi College, claimed to be the first wireless college in the world, celebrated the fiftieth anniversary of its opening on October 12th. Originally established by Marconi's Wireless Telegraph Co. at Frinton-on-Sea, Essex, it has been at Chelmsford since 1904.
Electro-Acoustics.-A twenty-week course of lectures on electro-acoustical transducers is being held on Monday evenings at Southall 'lechnical College, Beaconsfield Road, Southall, Middx. The fee for the course, which began on October 8 th, is $£ 1$.

Four-year Course.-Applications for enrolment for the third four-year course in electronic engineering, which commences at E.M.I. Institures on January 15 th, should be received by November 30th. Details of the scholarship scheme, by which the $£ 400$ fee is halved, are available from the Institute 10, Pembridge Square, London, W.2.
" Mechanical Handling," our associate journal, is organizing the Third Mechanical Handling Exhibition and Convention, to be held at Olympia from Junc th to 14 th, 1952.
R.D.F. Reunion.-We have been asked by ex-Fit. Sgt. V. H. Wotton to announce that he is endeavouring to organize a reunion of 1941-43 members of No. 31 R.D.F. School, R.A.F., Clinton, Ontario. His address is 216 , Vicarage Farm Road, Heston, Middx.

The Guilds' Engineer."-The second number of the journal of the Engineering and Radio Societies of the City and Guilds College, South Kensington, which has this title, includes several articles of radio interest; among them a summary by H . Bishop. B.B.C. Chuef Engineer, of his presidentia
address to the College's Radio Society and two student papers; "Frequency Modulation Receivers," by P. M. S. Hedgeland, and "Trends in the Design of Small Power Transformers for use in Commúnication Equipment," by E. S. Parkes. The journal costs 5 s .

## INDUSTRIAL NEWS

Tannoy,-Three companies now constitute the Tannoy organization-Tannoy Products, Lid. (formerly Sound Rentals, Led.), Tannoy Rentals, Ltd. (handling the rental of equipment), and Tannoy, Ltd. (handling development work). With the reorganization, W. J. Haines, who has been with Tannoy eighteen years, is appointed general production manager of the main company, and A. E. Dunevein (prevously with Standard Telephones \& Cables), general commercial manager. Guy R. Fountain and his son Michael are directors.

Nagard, Ltd., designers and manufacturers of electronic research and industrial equipment, will be transferring their offices and factory from Brixton, London, S.W.9, to 18, Avenue Road, Belmont, Surrey (Tel.: Vigilant 0345), on November lst.
F. C. Robinson \& Partners, L.td., electronic instrument specialists, of Deansgate, Manchester, announce the appointment of Frank P. McKellen as sales manager. He was, until recently, senior signals officer at the British Military Headquarters in Berlin.

Loudspeaker Diaphragms will be manufactured at the rate of 30,000 per week by the new plant being installed at the works of Fibre Form, Lrd., Garratt Mills, 'I'rewint Street, Earlsfield, London, S.W.18. (Tel.: Wimbledon 6228.) It is expected that production will gradually be increased to 50,000 diaphragms a week.

Sales Department of Astor Boisselier \& Lawrence, Ltd., specialist technical wax manufacturers, is now at 9 . Savov Street, London, W.C.2. The telephone numbers remain unchanged- Temple Bar 5927 and 6942. The company's head office and works are at West Drayton, Middx.


## meetings

## Institution of Electrical Engineers

Ordinary Meeting.--"The LondonBirmingham Television-Cable System' by T. Kilvington, B.Sc. (Eng.), F. J. M. Laver, and H. Stanesby on November 8th.

Radio Section.-" The Life of Oxide, Cathodes in Modern Receiving Valves" by G. H. Metsön, M.C., Ph.D., M.Sc., S. Wagener, Dr. Phil., M. F. Holmes, B.Sc., and M. R. Child on November 14th.

Discussion on "Should Broadcasting be Superseded by Wire Distribution?" on November 26th. Opener, P. P. Eckersley.

The above meetings will be held at 5.30 at the I E.E., Savoy Place, London, W.C. 2 .

East Midland Centre.-"The Development and Application of the Vibrator as a Competitor of the Rotary Convertor" by J. H. Mitchell, Ph.D., B.Sc., at 6.30 on November 6th at Loughborough College.

Cambridge Radio Group.-Address by D. C. Espley, O.B.E., D.Eng., chairman of the Radio Section, at 6 on November 6th at the Cambridgeshire Technical College, Cambridge.

Mersey © North Wales Centre" The Life and Work of Oliver Heaviside" by Prof. G. H. Rawcliffe, M.A., D.Sc., at 6.30 on November 5th at the Liverpool Royal Institution, Colquitt Street, Liverpool.
North-Eastern Rudio Group. "Crystal Triodes" by T. R. Scott, B.Sc., on November 5th.
"An Electronic Process-Controller" by J. R. Boundy, B.Sc., and S. A. Bergen, M.B.E., on November 19th.

Both meetings will be held at 6.15 at King's College, Newcastle-on-Tyne.

North Midland Centre.-" The Nervous System as a Communication Network" by J. A. V. Bates, M.A., M.B., B.Chir., at 6.30 on November 13th at the Hotel Metropole, Leeds.

North-Western Radio Group.-"An Investigation into the Mechanism of Magnetic Recording" by P. E. Axon, O.B.E., M.Sc., at 6.30 on November 28th at the Engineers' Club, Albert Square, Manchester. South Midland Radio Group"The Life and Reliability, of a Radio Valve" by $H$. G. Metson, Ph.D., M.Sc., at 6 on November 26th at the James Watt Memorial Institute, Great Charles Street, Birmingham.

APID TESTING of deflection coils is facilitated at the Du Mont Laboratories, New lersey, by the use of a oneinch tube which bermits the yoke to be over the face of the tube, thereby obviating the need for disconnecting the tube.

North Staffordshire Sub-Centre."Television" by C. T. Lamping at 7 on November 5th at the P.O. Central Training School, Stone, Staffs.

Rugby Sub-Centre.-" Crystal Diodes" by R. W. Douglas, B.Sc., and E. G., James, Ph.D., and "Crystal Triodes" by T. R. Scott, B.Sc., at 6.30 on November 21st at the Rugby College of Technology and Arts, Rugby.

South-W'estern Sub-Centre.-"The Operation and Maintenance of Television Outside-Broadcast Equipment" by T. H. Bridgewater at 3 on November 28 th at the Rougemont Hotel, Exeter.

Ipswich District Meeting.-Lecture on "Television" at 6.30 on November 12th at the Grown and Anchor Hotel, Ipswich.

London Students' Section.-" The Use of Working Scale Models in the Development of Broadcasting Aerials" by T. R. Boys at 7 on November 27th at Savoy Place, London, W.C.2.

Students' District Meeting.-." Medical and Industrial Uses of Radio Frequency Energy" by H. Burton, B.Eng., at 7 on November 19th at the George Hotel, Reading.
British Institution of Radio Engineers
London Section.-" Developments in High-Erequency Transmitter Cables," by R. C. Mildner (Telcon), at 6.30 on November 21st at the London School of Hygiene \& Tropical Medicine, Keppel Street, London, W.C. 1.
North-Eastern Section._"Television Aerial Design," by G. L. Stephens (Belling \& Lee), at 6.0 on November 14th at Neville Hall, Newcastle-uponTyne.
Scottish Section.-"The Brain as a Piece of Communication Equipment," by H. W. Shipton, on November 6th at University College, Dundee; on November 7th at the University, Edinburgh; and on November 8th at the Institute of Engineers and Shipbuilders, Glasgow. These are joint meetings with the Institute of Physics and each begins at 7.0 .

## Institution of Electronics

Southern Branch.-"The Technique of Trustworthy Valves," by G. P. Thwaites, B.Sc., A.M.I.E.E., (S.T.C.), at 6.45 on November 14 th at University College, Southampton.

## Royal Institution

"Radio Astronomy," by Prof. J. A. Ratcliffe, O.B.E., M.A., F.R.S. (Cambridge University), at 9.0 on November 23 rd at the Royal Institution, 21, Albemarle Street, London, W.L.
British Sound Recording Association
"Electrical and Mechanical Problems of Record Reproduction," by K. R. McLachlan and R. Yorke, at 7.0 on November 16th at the Royal Society of Arts, John Adam Street, London, W.C. 2 .

Portsmouth Centre.-" Recording at the B.B.C.," by R. C. Patrick (B.B.C.), on November lst.
"Microgroove Recording and Reproduction," by E. D. Parchment (Decca), on November 14th.

Both meetings will be held at 7.0 at the Central Library, Guildhall, Portsmouth.

## Television Society

"The Murphy V'200 「elevision Receiver" by P. Kidd (Murphy Radio) on November 8th.
"Television Distribution by Wire" by K. J. Easton (Central Rediffusion Services) on November 23 rd .

Both meetings will be held at 7 at the Cinematograph Exhibitors' Association, 164, Shaftesbury Ave., London, W.C.2.

# Amateur Radio Developments 

A Review of Current Techniques

By J. P. HAWKER*

MORE than 7,000 amateur transmitting licences -double the peak pre-war figure-have been issued in the United Kingdom since the resumption of licensing in 1946. While it is perhaps true that the enthusiastic amateur to-day lacks the facilities necessary for highly original research and usually obtains his licence chiefly for the pleasure to be derived from radio operating as a hobby, he can, and does, play a not unimportant rôle in the practical application of new laboratory techniques to the general field of two-way communication. In this article it is proposed to review briefly a few of the trends noticeable in post-war amateur equipment in order to show a little of what the amateur experimenter is doing, and why.
One of the most serious problems facing the amateur transmitter since the war has been the mutual interference arising from the greatly increased activity. For example, if at any given moment 5 per cent of the licensed amateurs of the world wished to operate in the popular $14-\mathrm{Mc} / \mathrm{s}$ band then the $400 \mathrm{kc} / \mathrm{s}$ available would have to accommodate no less than 6,000 stations, of which possibly half would be using telephony. But it is not in the nature of the enthusiast to be unduly dismayed by such statistics, and indeed the problem has been tackled, with a fair degree of success, by:-(1) simplifying transmitter frequency changing; (2) increasing receiver selectivity, and (3) reducing the band-width of transmissions.
Transmitter Frequency Changing.-In 1939 probably some 90 per cent of British amateurs used crystalcontrolled transmitters and were limited to a few fixed frequencies. Those who anticipated that post-war operation would be along similar lines were soon proved wrong. From 1946 onwards variable frequency control rapidly grew in popularity as more and more amateurs found it essential to be able to pick a "clear" channel in the crowded bands. But in reverting once again to master oscillators, the amateur, perhaps more so than the designer of comparable commercial equipment, has been concerned with obtaining, from relatively simple and cheaply constructed apparatus, a good quality note as free as possible from frequency drift and keying chirp. In practice he has concentrated upon the use of a lowpower receiving - type valve as an oscillator, fed from a stabilized power supply and followed by an isolating stage which provides from 1 to 3 watts of r.f. output. By operating the oscillator

Fig. I Typical variable frequency oscillator using the modified Colpitts or " Clapp " circuit.
stage on 1.7 or $3.5 \mathrm{Mc} / \mathrm{s}$ with bandspread tuning, the v.f.o. (variable frequency oscillator) unit can be made stable enough for all practical purposes without the complications of temperature compensation and elaborate coil construction found in most commercial equipment of comparable stability. The amateur, incidentally, has done much towards popularizing the series-tuned modified Colpitts, or "Clapp," circuit shown in Fig. 1. The adoption of variable frequency control has led also to an important change in amateur operating technique; the practice of "netting," i.e., the use of the same frequency by two or more stations in communication, is now generally employed on all h.f. bands. While the system possesses many advantages for amateur working, the piling up of transmissions on the frequency of any unusual DX'station is at times a severe handicap.
As with the development of broadcast and communication receivers, there has been steady progress towards the simplification of transmitter tuning and band-changing. The amateur possesses a distinct advantage over the commercial designer in that his frequency bands are largely in harmonic relationship and represent only a comparatively small portion of the h.f. spectrum, complete frequency coverage is therefore not required. On the other hand, power efficiency of the final stage is of greater importance than for commercial applications owing to the strict limitation of input power. Much interest has been shown in recent months in the American development of a reasonably high-Q " all-band" power amplifier multiple-tuning system which can tune to any amateur band between 3.5 and $30 \mathrm{Mc} / \mathrm{s}$ without switching or coil changing. The basic arrangement of this tuner is shown in Fig. 2, where $L_{1}$ is a considerably smaller value inductance than $L_{2}$. On lower frequencies

[^4]$\mathrm{L}_{1}$ acts merely as a rather long lead to $\mathrm{C}_{1}$, which is thus effectively in parallel with $\mathrm{C}_{2}$, while on higher frequencies $\mathrm{L}_{2}$ behaves as an r.f. choke. Thus across the points X and Y the circuit tunes simultaneously to two widely different frequencies; by carcful selection of the inductances no two amateur bands nced appear at identical settings of the ganged tuning capacitors. The design of band-switched exciter units has also been facilitated by the use of wide-band interstage couplers and coil turret assemblies.

Receivers.-An interesting development in the search for improved receiver selectivity for telegraphy operation has been the use of a very low second i.f. (50-100 $\mathrm{kc} / \mathrm{s}$ ) in double-conversion superheterodyne circuits. A popular arrangement is to feed the output from a conventional $465-$ or $1,600-\mathrm{kc} / \mathrm{s}$ i.f. stage into an additional unit comprising a mixer and local oscillator, one or more stages of amplification at $85 \mathrm{kc} / \mathrm{s}$, followed by demodulation and audio amplification; such a unit usually being termed a "Q5er." Peaked audio filters and other audio-selection devices have also become more popular in recent years, though of course these aids to selectivity are not of recent origin. Crystal filter, "Q5-er " and audio filter is a combination whose selectivity, in practice, is usually limited chiefly by the stability of transmissions, the slightest drift of the incoming signals resulting in their sudden disappearance. Receivers for amateur communication with switched side-band selection have also been successfully demonstrated in this country and in the United States. But it should be reported that, compared with the 'thirties, relatively few amateurs now use entirely home-constructed receiving equipment except for v.h.f. working.

Efforts at reducing the band-width of telephony transmissions to permit the operation of more stations in any given band of frequencies, have been made by the more progressive amateurs; techniques used including speech-clipping with cut-off filters and "splatter" suppression. An attenuation at $4,000 \mathrm{c} / \mathrm{s}$ of 26 db with reference to the response at $1,000 \mathrm{c} / \mathrm{s}$ was recommended at the 25 th Anniversary Congress of the International Amateur Radio Union in 1950. Experimental single-sideband suppressed-carrier transmissions are regularly made by a number of stations throughout the world, but the added complications seem likely to restrict the use of this system.

Television Interference.-Increased amateur activity is not the only major problem which has influenced current techniques; television interference (TVI) is also radically affecting the design of amateur transmitters. Although such interference only amounts to a small percentage of the total number of television interference complaints investigated by the G.P.O. it does represent (to the individual amateur) one of the most difficult problems with which he has ever been confronted. Owing to the unfortunate choice (from an amateur viewpoint) of the television frequency in the London area, Alexandra Palace transmissions are most susceptible to interference from the third harmonic of $14-\mathrm{Mc} / \mathrm{s}$ amateur transmissions, particularly in areas where the television signals are weak. In addition, the intermediate and image frequencies of several makes of television receivers are such that, through no fault of the amateurs concerned, these
sets are liable to suffer interference from amateur transmitters in the immediate neighbourhood. The most successful answer to harmonic interference so far lies in screening and filtering the transmitter to a far greater extent than is normal amateur practice and in careful harmonic monitoring. In fringe areas complete screening of the transmitter is usually necessary, involving precautions to prevent the escape of r.f. power along mains supply leads, keying and power lines or even through meter apertures. The r.f. output is then fed to the aerial, or aerial matching unit, through a screened co-axial line via a multiple-section low-pass filter designed to attenuate the unwanted output above $30 \mathrm{Mc} / \mathrm{s}$. Outstanding work in connection with the cure of amatcur TVI has been carried out by a number of amateur investigators here and in the U.S.A., but the problem still remains a serious one in crowded districts where the distance between an amateur transmitting and the nearest television receiving acrial may be only a few feet.

Modulation Systems.-The desire to eliminate costly high-power modulation equipment is reflected in the development of narrow-band frequencymodulation using simple reactance modulation circuits. N.b.f.m. transmitters are designed to operate with a maximum deviation of the order of 2.5 to $3 \mathrm{kc} / \mathrm{s}$ and thus occupy no more ether-space than a conventional a.m. transmitter. Another advantage that the system possesses over normal f.m. systems, where the deviation is often of the order of $75 \mathrm{kc} / \mathrm{s}$, is that n.b.f.m. transmissions can be received satisfactorily on an a.m. receiver simply by tuning to one side of the carrier frequency. In the U.K. the terms of the amateur licence prohibit the use of n.b.f.m. on frequencies below $28 \mathrm{Mc} / \mathrm{s}$, but elsewhere the system, which is particularly suitable for mobile work, is proving effective on frequencies down to $3.5 \mathrm{Mc} / \mathrm{s}$. For similar reasons, interest has also been shown in "Taylor super modulation" a high-efficiency gridmodulation (a.m.) system in which a low-power audiofrequency amplifier is arranged to trigger a Class $C$ power amplifier and also a heavily biased "positive modulator" valve. With r.f. drive only applied, the p.m. valve remains in the cut-off condition, but on applying an audio signal this valve releases additional r.f. power into the common tank circuit during positive half-cycles; see Fig. 3.

While the average input power of the British amateur is now probably about 80 watts, considerable interest has been maintained in "flea-power" transmission. For example, during the 1949 R.S.G.B. low-power contest, Mr. T. F. Herdson (G6ZN), of Horbury, Yorkshire, made 116 contacts in 24 hours using a simple $3.5-\mathrm{Mc} / \mathrm{s}$ Hartley oscillator and one 90 V h.t. battery giving an input between $\frac{1}{4}$ and $\frac{1}{2}$ watt. Similarly, the 200 or more stations taking part each year in the R.S.G.B. national field day are limited to a power input of 5 watts, yet long-distance contacts are regularly achieved. Such results, however, probably depend more upon operating skill than upon the use of any new techniques. Most pronounced feature of medium-power transmitters has been the popularity of beam tetrode valves, particularly the type 807 and its equivalents, which are widely used as frequency doubler, buffer amplifier and single-ended or push-pull power amplifier.

Another feature of post-war amateur technique has been the development of rotary beam aerials for longdistance transmission and for v.h.f. applications; although even to-day such structures-for the h.f. bands at least-are less common in this country than overseas, owing partly to the cost of suitable materials and partly to the restrictions imposed under local by-laws and the Town and Country Planning Act. Two- or three-element beams for $28 \mathrm{Mc} / \mathrm{s}$, and more rarely for $14 \mathrm{Mc} / \mathrm{s}$, give reasonably sharp horizontal lobes and low vertical angle radiation. These beams generally use Yagi-type arrays and can be swung so as to radiate signals in any desired direction, often being controlled from the normal operating position by a mechanical or selsyn-type device to indicate the direction in which the beam is pointing at any given moment. Rotating aerials of this type have few equivalents in commercial practice.

Similarly, the influence of the amateur as an operator/technician can be seen in the electronic keyer, also primarily an amateur development. Unlike the better-known "bug" key, the electronic keyer automatically controls the length of the dashes as well as the dots and, in some models, the interva!
between each symbol. The main drawback to these ingenious devices is the amount of practice required in order to become proficient in their use, but the "tape-like" character formation which is eventually possible has encouraged their adoption by amateurs seeking to raise the standard of manual telegraphy operation.
V.h.f. Developments.-Perhaps no aspect of post-war amateur activity has attracted so much attention in non-amateur circles as the results achieved on v.h.f. To the professional communications engineer, accustomed to regarding propagation at these frequencies as being limited to little more than "line of sight," the transatlantic contacts on $50 \mathrm{Mc} / \mathrm{s}$ during the sun-spot peak of 1947-48, the 1,200 -mile contact in the United States and 520 -mile contact between a West Country station (G2BMZ) and Germany from fixed locations on $144 \mathrm{Mc} / \mathrm{s}$, and the 161 -mile contacts on $420 \mathrm{Mc} / \mathrm{s}$ all represent interesting examples of "freak" conditions. But the amateur has also demonstrated that low-power $144-\mathrm{Mc} / \mathrm{s}$ transmissions can be received over distances greater than 100 miles with a regularity far exceeding that which would have been thought possible only a few years ago. To what extent have such results been attained by the use of unorthodox or new techniques?

It should be emphasized that, generally speaking, the amateur is restricted to the use of standard commercial types of valve in the lower-price range and the by-no-means-new e.h.f. types available as "surplus," a factor of increasing importance as frequencies are raised. Similarly, the workshop facilities required for the construction of e.h.f. "plumbing" are possessed by few experimenters. Yet it is interesting to note that whereas on the h.f. bands the British amateur tends to look to his fellow enthusiasts in the United States for many of his new developments, this is far less true of the v.h.f. and e.h.f. bands on which results in this country compare most favourably with those achieved elsewhere.

The amateur v.h.f. receiver, unlike most commercial equivalents, is required to tune over at least part of any particular band without losing the degree of stability normally associated at these frequencies only with crystal-controlled local oscillators. Much attention has accordingly been paid to the development of stable os-cillator-tripler stages with the fundamental circuit on about $50 \mathrm{Mc} / \mathrm{s}$; and also to tunable intermediate-frequency stages for use in conjunction with c.c. (cry-stal-controlled) oscillators

The well-equipped amateur radio station at the Uxbridge Festival of Britain Industrial Exhibition. A QSL card of -appropriate design giving the station's call sign, G2FMF/A, is used to acknowledge the exchange of signals.
though it should be mentioned that the elimination of spurious responses has proved extremely difficult where a wide-coverage receiver is required. Another interesting development is the occasional use of panoramic reception, whereby the state of activity over all or part of a band is displayed on the screen of a cathode-ray tube by means of an f.m. oscillator.
The paramount importance of the first r.f. stage has encouraged the use of neutralized push-pull twin-triode valves such as the 6J6 or EC91 and also the currently popular Wallman cascode circuit (Fig. 4) which comprises a neutralized grounded-cathode triode followed by a grounded-grid triode, the usual combination for $144 \mathrm{Mc} / \mathrm{s}$ being a triode-connected 6AK 5 and a half-section of a 6J6, EC91 or 12AT7. A few amateurs, by using noise-generator techniques, have been able to make systematic measurements of the sensitivity of their v.h.f. receivers, though the practical application of the noise generator on $144 \mathrm{Mc} / \mathrm{s}$ and above has not proved easy. On $420 \mathrm{Mc} / \mathrm{s}$, crystal diode mixers, sometimes with crystal-controlled injection and "lighthouse" r.f. amplifying stages, have rapidly replaced the super-regenerative circuits favoured when the band was first released in 1948. The introduction of the 12AT7 and similar commercial valves is now permitting a less specialized approach to be made to this band.

For v.h.f. transmitting, commercial practice has been followed in the wide use of such valves as the 832, though at $420 \mathrm{Mc} / \mathrm{s}$ the output from this type is very limited and the "life" uncertain. Efficiency of power amplifiers in this band is being steadily improved as new valve types become available, and the South London U.H.F. Group have demonstrated an amplifier capable of an efficiency of about 60 per


Fig. 4. The Wallmon coscode r.f. amplifier, popular on the $144-\mathrm{Mc} / \mathrm{s}$ band.
cent at 25 watts input. On both 144 and $420 \mathrm{Mc} / \mathrm{s}$, multi-stage stabilized transmitters with a fundamental crystal frequency of about $8 \mathrm{Mc} / \mathrm{s}$ are now used by most amateurs working in these bands. Some interest is also being shown in the possible use of overtone crystal oscillator circuits with an ouput at about $72 \mathrm{Mc} / \mathrm{s}$ as a means of eliminating a number of frequency-doubling stages.

Yagi and stacked-array aerials are equally popular, though the wider horizontal coverage of the stackedarray is proving increasingly useful in bands where the limited amount of activity makes searching for pencil-beam signals as much a trial of patience as of equipment.

## SOUBCES OF INTEIRFERENCE

INEFFICIENT aerial-earth systems are, according to figures published in the Post Office Telecommunications fournal, by far the biggest individual cause of interference with sound broadcasting; but in the case of television the main individual cause is electric sewing machines. In both sound and television, however, faulty receivers hold second place.
In an endeavour, therefore, to reduce the evergrowing number of calls made on the Post Office Interference Investigation Service, a new pamphlet
has been issued giving simple tests which can be made by listeners and viewers to ascertain whether or not the trouble is in the installation. "Good Wireless and Television Reception," as it is called, includes a form for enlisting the services of Investigation Officers if the cause of interference appears to be outside the control of the set owner.

In the appended table the most frequent sources of interference are given as percentages of the cases investigated.

|  | SOUND <br> Complaints \% |  | TELEVISION Complaints \% |  | Radiation from radio receivers i.fs. <br> Misoperation of re- | SOUND <br> Complaints \% |  | TELEVISION Complaints \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Unknown; interference not observed by P.O. staff | 18,018 | 23.8 | 7,068 | 29.2 |  | 622 | 0.8 | 156 | 0.6 |
| Inefficient aerial/ |  |  |  |  | ceivers . . . | 539 | 0.7 | 204 | 0.8 |
| earth systems | 15,246 | 20.1 | 947 | 3.9 | Thermostats, misc. | 539 | 0.7 | 184 | 0.7 |
| Faulty receivers | 9,507 | 12.5 | 1,972 | 8.2 | Smoothing irons | 528 | 0.7 | - |  |
| Faulty wiring of buildings. | 5,029 | 6.6 | 234 | 0.9 | Vacuum cleaners | 527 | 0.7 | 257 | 0.9 |
| Refrigerators | 2,255 | 3.0 | 331 | 1.4 | Neon sign tubes . . | 503 | 0.7 | 192 | 0.8 |
| Fluorescent tubes . . | 1,787 | 2.4 | - | - | Underground mains | 492 | 0.6 | - |  |
| Radiation from re-  <br> ceiver time-base  <br> circuits . . | 1,725 | 2.3 |  | - | External cross modulation <br> Fans. | 414 391 | 0.5 0.5 | 521 | 2.1 |
| Radio transmitters. . | 1,469 | 2.0 | 1,007 | 4.2 | Calculating machines | 353 | 0.5 | 150 | 0.6 |
| Bedwarmers | 1,423 | 1.9 | - | - | Hairdryers.. | 292 | 0.4 | 697 | 2.9 |
| Motors, misc. | 1,334 | 1.8 | 315 | 1.3 | Motor car ignition . . | - | - | 1,096 | 4.5 |
| Sewing machines .. | 1,162 | 1.5 | 2,374 | 9.8 | Medical apparatus |  |  |  |  |
| Overhead power lines | 900 | 1.2 | 632 | 2.6 | (valve-operated).. | - | - | 306 | 1.2 |
| Drills | 791 | 1.0 | 221 | 0.8 | Filament-type lamps | - | - | 305 | 1.2 |

# Dimensions 

A Useful Check on Formulae and Calculations

IF you indulge occasionally in bouts of algebra, do you find, as I do, how distressingly easy it is to miss out a "squared" sign somewhere, or accidentally turn a " $x$ " into a " + ," or misplace a bracket? If one eventually spots the mistake, it may not be soon enough to avoid wasting a lot of time and effort ; and if one doesn't ....!

It may not be known to everyone who works about with formulæ how helpful it is to keep an eye on their "dimensions." You derive a formula for the impedance of a particular kind of circuit, shall we say, with the idea of finding out how it varies with frequency. If you have made a slip anywhere in the algebra the odds are considerably in favour of it affecting the dimensions of the equation; and (when you know how) it takes only a few moments to check that. Not every error can be detected by this test, but a worth-while proportion can. Quite apart from fault-finding, attention to dimensions is a more intelligent attitude to formule than mere blind substitution of figures.

The basic principle is that one can't add or subtract or equate things that are of different kinds or "dimensions," such as hours and miles, or square yards and gallons. But the quantities of them can be multiplied or divided, giving a quantity with different dimensions from either. A mile is a measure or unit of distance or length, and an hour a unit of time. Adding 100 miles to 4 hours is nonsense, but the number of miles can be divided by the number of hours, giving a quantity 25 of a unit of speed-the mile-per-hour. The dimensions of speed are length divided by time. Mere numbers, like the 25 in this case, can be ignored, because they have no dimensions in themselves and are there merely to fit in with the particular units chosen. The 25 would become some other number if one worked in $\mathrm{cms} / \mathrm{sec}$ instead of miles/hour.

So if the upshot of some mathematical manipulation were a formula such as

$$
v=\sqrt{25 d+\frac{1}{t^{2}}}
$$

where $v$ was the speed (or velocity) of something or other and $d$ and $t$ were a distance and a time respectively, you would know straight off that it was wrong. Velocity is neither the square root of distance nor the reciprocal of time.

So far as dimensions are concerned, width, breadth, distance, height, circumference, diameter, perimeter, etc., are all the same-length. If any two lengths are multiplied together the product is a quantity whose dimensions are length-squared, or area. And the product of three lengths is length-cubed or volume. So if you were to read that the volume of a sphere was $4 / 3 \pi r^{2}$ ( $r$ being the symbol for radius, which is a length) you would know for certain that it was wrong, and would probably suspect (quite rightly)
that the ${ }^{2}$ was a misprint for ${ }^{3}$. ( $\pi$, being the ratio of two lengths, is a mere dimensionless number.)

I have brought length in rather prominently at the start, because it is one of the recognized fundamental dimensions. It would be difficult to think of any more fundamental quantity in which to express length. One could, of coursc, say that it is velocity multiplied by time, but that would hardly be helpful seeing that velocity is itself derived from length and time. In fact almost all the multitudinous physical quantities, except electrical and magnetic, can be expressed in terms of three fundamental dimensions: length, time, and mass. That is why systems of units are named by three letters, such as c.g.s. (meaning the centimetre-gramme-second system) and m.k.s. (metre-kilogramme-second). We have already noted the simple example of velocity or speed, which is length/time.

To avoid confusion with other meanings of symbols, the dimensions of quantities are written in square brackets: [ $L]^{\star}$ for length; [T] for time ; $[M]$ for mass. The "dimensional equation" for velocity would therefore be

$$
[v]=\frac{[L]}{[\mathrm{T}]}
$$

but it is usually written

$$
[v]=\left[L \mathrm{~T}^{-1}\right]
$$

using the conventional alternative method of indicating division, by a negative "index." All mechanical quantities can be expressed by "powers" of length, time, and mass. $L$ is of course $L^{1}$, or the first power of $L$. And any quantity to the power 0 is 1 , which is unit quantity with no dimension-a mere numeral. And if we remember the rules about powers or indices-to multiply, add them ; to divide, subtract-then dimensional equations are simple. There should be no difficulty about this one :

$$
[A]=\left[L^{2}\right]
$$

where A stands for area. For volume we shall use another italic letter to distinguish from voltage :

$$
[V]=\left[L^{3}\right]
$$

If we come across a volume divided by an area we could therefore write

$$
\frac{\left[L^{3}\right]}{\left[L^{2}\right]} \text { or }\left[L^{3} L^{-2}\right]=[L]
$$

Acceleration is change of velocity per unit time, so its dimensions are $[v] /[\mathrm{T}]$ or $\left[L \mathrm{~T}^{-2}\right]$; force is equal to the acceleration imparted to unit mass, so dimensionally is $\left[L T^{-2} M\right.$ ] ; and so on. The dimensions of any mechanical quantity can be expressed by three numbers-the powers of $L, \mathrm{~T}$ and M ; in this case, $1,-2,1$.

But it is about time we got on to electrical quantities, before this subject begins to look more difficult than it really is. In most cases it is remarkably easy, because there is no need to analyse right down to

[^5]basic dimensions. A large proportion of the equations likely to be seen in Wireless World concern impedances. All impedances can be reckoned in ohms and therefore have the same dimensions. (That is, if one is concerned only with magnitude and not with the more subtle distinction of phase. It is possible, if necessary, to maintain the distinction between resistance and reactance by writing the dimensions of inductive reactance as $[j \mathrm{R}]$ and capacitive reactance as $[-j \mathrm{R}]$; but the examples to follow will take account of magnitudes only.)

There are some very commonly used formulx for finding the parallel reactance and resistance equivalent to a given series combination, and vice versa. In this example

$$
\mathrm{R}_{s}=\frac{\mathrm{R}_{p} \mathrm{X}}{\mathrm{R}_{p}^{2}+\mathrm{X}_{p}^{2}}
$$

where the symbols are too obvious to need a key, I either have or have not introduced a deliberate mistake. Perhaps you would like to say which, without looking it up in a book. By using the dimensions idea one can tell at a glance. Writing it out in full dimensional equations :

$$
[R]=\frac{\left[R^{2}\right]}{\left[R^{2}\right]}=\left[R^{0}\right]
$$

which is absurd. One might guess that a ${ }^{2}$ has dropped out of the numerator ; actually it should be $\mathrm{R}_{p}, \mathrm{X}_{1},{ }^{2}$.

Not:ce that in this simple example it was unnecessary to break down any of the quantities into more fundamental dimensions, because they were all the same at the beginning, so one had only to compare the indices on each side of the equation.

In calculating complicated circuits the algebra spreads over the paper in an alarming way, and it is very easy to make a slip when multiplying out the factors and adding similar terms. Suppose you had been dealing with Fig. 1 in this way and had arrived at the following :

$$
\begin{aligned}
\mathrm{Z}= & \frac{\mathrm{R}_{1} \mathrm{R}_{2}\left(\mathrm{R}_{1}+\mathrm{R}_{2}\right)+\mathrm{R}_{1} \mathrm{X}_{2}+\mathrm{R}_{2} \mathrm{X}_{1}}{\left(\mathrm{R}_{1}+\mathrm{R}_{2}\right)^{2}+\left(\mathrm{X}_{1}+\mathrm{X}_{2}\right)^{2}}+ \\
& j \frac{\mathrm{R}_{1}{ }^{2} \mathrm{X}_{2}+\mathrm{R}_{2}{ }^{2} \mathrm{X}_{1}+\mathrm{X}_{1} \mathrm{X}_{2}\left(\mathrm{X}_{1}+\mathrm{X}_{2}\right)}{\left(\mathrm{R}_{1}+\mathrm{R}_{2}\right)^{2}+\left(\mathrm{X}_{1}+\mathrm{X}_{2}\right)^{2}}
\end{aligned}
$$

A slip in such an effort would be excusable, so to go and use the formula straight away without looking it over would be inexcusable. Since all the denominator terms are resistance (or reactance) squared, the numerator terms must all be cubed. Most of them are, but two culprits immediately stand out- $\mathrm{R}_{1} \mathrm{X}_{2}$ and $\mathrm{R}_{2} \mathrm{X}_{1}$. Again, a ${ }^{2}$ must have dropped out from each. Assuming that in other respects the equation is correct, we can make a shrewd guess at whether it is the R or X that ought to be squared. For the circuit is quite symmetrical, and so are the resistance and reactance halves of the formula; the numerator terms in the resistance half are the same as those in the reactance ( $j$ ) half except that R and X are interchanged. So as it is the R's that are squared on the reactance side we would expect the X 's to be squared on the resistance side. And that, in fact, is correct ; the resistance numerator should be $\mathrm{R}_{1} \mathrm{R}_{2}\left(\mathrm{R}_{1}+\mathrm{R}_{2}\right)+\mathrm{R}_{1} \mathrm{X}_{2}{ }^{2}$ $+\mathrm{R}_{2} \mathrm{X}_{1}{ }^{2}$.

A very familiar equation is the one relating the resonant frequency ( $f_{r}$ ) of a tuned circuit with the inductance ( L ) and capacitance ( C ):

$$
f_{r}=\frac{1}{2 \pi \sqrt{\mathrm{LC}}}
$$

Here there is no difficulty about frequency; it is a

fig. 1. Although this circuit looks foirly simple, the formula for its impedance is quite impressive and deserves to be checked by " dimensions.'
number (of cycles) divided by a time (usually one second), so it is the reciprocal of time, and its dimensional equation is therefore

$$
[f]=\left[\mathrm{T}^{-1}\right]
$$

But we have at the moment no clue to the dimensions of $L$ and $C$, except that we know that when multiplied by frequency they are related to one another by their common relationship to reactance. But that fact doesn't get us any farther, because it is the one from which our equation was derived (by the act of making the inductive and capacitive reactances equal and defining $f_{r}$ as the frequency that makes them so).

We might try another approach by looking up the formulæ for capacitance and inductance. Here is a well-known one for the capacitance between parallel plates:

$$
\mathrm{C}=\frac{0.0885 \mathrm{AN}}{t} \quad \text { in } \mathrm{pF}
$$

where $A$ is the area of each plate in sq. cms., $N$ the number of spaces between plates, and $t$ the thickness of each spacing in cms. N being just a number it can be ignored dimensionally, and so presumably can 0.0885 ; [A] is $\left[L .{ }^{2}\right]$ and $[t]$ is $[L]$, so
$[C]=[L]$
Or so it seems. And here is one of the many inductance formulæ:

$$
\mathrm{L}=-\frac{0.00987}{l} \frac{d^{2} \mathrm{~N}^{2} \mathrm{~K}}{l} \quad \text { in } \mu \mathrm{H}
$$

where $d$ is the diameter of the coil in $\mathrm{cms}, \mathrm{N}$ the number of turns, $l$ the length of the coil, and K is "Nagaoka's constant." Inquiry shows that K is just a number, so all we are left with is $d^{2} / l$, which is a length, so we have

$$
[L]=[L]
$$

If you happen to know that at one time it was quite usual for both capacitance and inductance to be reckoned in centimetres, you may be satisfied with the above two results. But if you are so relentless as to go back to the frequency formula and incorporate these new findings, the outcome will not be quite so happy :

$$
\begin{aligned}
{[f]=\left[\mathrm{T}^{-1}\right] } & =\left[\mathrm{L}^{-\frac{1}{2}}\right]\left[\mathrm{C}^{-\frac{1}{2}}\right] \\
& =\left[L^{\left.-\frac{1}{2}\right]}\left[L^{-\frac{1}{2}}\right]\right. \\
& =\left[L^{-1}\right]
\end{aligned}
$$

Therefore $[\mathrm{T}]=[L]$
or time equals length. If that were true it would make things very much simpler-or would it? Anyway if it is, I'm a brass monkey and you are-anything you don't like-and it doesn't matter, because all science is nonsense. So on the whole it may perhaps be better to look over our capacitance and inductance formulæ and see if we've forgotten anything. If we had looked up the more painstaking kind of reference book we might have found them complicated by the
factor $\mu$ for inductance and $\kappa$ for capacitance-permeability and permittivity respectively. The only excuse for omitting them is that it was supposed to be understood that the formulæ concerned air-cored coils and air-dielectric condensers, and that with the particular units employed the values of $\mu$ and $\kappa$ are then both 1 so can be left out. But they must not be forgotten altogether-when considering dimensions, anyway. Presumably the absurdity about length being time would be put right if the dimensions of $\mu$ and $\kappa$ were included. What are their dimensions?

If I could give you the right answer to that I would at once become a sensation, because scientists have long wanted to know. The best that can be done is to work back from the frequency formula, putting $[\mathrm{C}]=[L \kappa]$ and $[\mathrm{L}]=[L \mu]$

$$
\begin{aligned}
{[f] } & =[\mathrm{T}-1]=[L \kappa]^{-\frac{1}{2}}[L \mu]^{-\frac{1}{2}} \\
\text { So }[\mathrm{T}]]^{2} & =[L][\kappa \mu]: \\
{[\kappa \mu]^{2} } & =\left[\mathrm{T} L^{-1}\right]
\end{aligned}
$$

Time divided by distance is a quantity that could perhaps be named "slowness of movement," but its reciprocal is more commonly used-speed or velocity. So turning both sides of the equation upside down we get

$$
[\kappa \mu]^{-\frac{1}{2}}=\left[L \mathrm{~T}^{-1}\right]=[v]
$$

Any healthily inquisitive person would now ask " What velocity ? " and this time the answer is available, and a very interesting one it is too-the velocity of electromagnetic waves through a medium having permittivity $\kappa$ and permeability $\mu$. But, you may say, there must be something wrong about this; $\kappa$ and $\mu$ for air are both 1 , and the speed of light through air is rather more than 1 cm . per sec! But this is forgetting the little matter of units. Our capacitance and inductance formulæ were for pF and $\mu \mathrm{H}$, not F and H ; and there were numerical constants beside. If you insist on $\kappa$ and $\mu$ being 1 without any constants being brought in, then you will have to accept 186,282 miles as the unit of length! Since you will probably find that more than a trifle inconvenient (imagine reckoning the flux density in a loudspeaker gap in lines per $34,701,000,000$ square miles!) you will probably be glad to accept the numerical constants in the formulæ already quoted, because when the convenient sub-units ( pF and $\mu \mathrm{H}$ ) are used these constants are not absurdly large or small. If, however, you are prepared to suffer some numerical incon-venience-within reason, of course-for the sake of principle, then you might go for the alternative, the m.k.s. system, in which the units are the metre, the farad and the henry ; and to make everything right the values of $\kappa$ and $\mu$ for empty space (which are denoted by $\kappa_{0}$ and $\mu_{0}$ ) must be very nearly $1 /\left(36 \pi \times 10^{9}\right)$ and $4 \pi / 10^{7}$ respectively. They could be given other values within this framework, so long as $1 / \sqrt{\kappa_{0} \mu_{0}}$ was equal to $299,790,000$ metres per sec. or whatever the true velocity of light may be. You see, nobody knows the actual separate values of $\kappa_{0}$ and $\mu_{0}$, or their dimensions; all we know is the value and dimensions of their product, $\kappa_{0} \mu_{0}$. It is as if we knew the voltage across a given resistor but had no means of finding either its resistance or the current through it. We would know IR without knowing either I or R.

All this about $\kappa_{0}$ and $\mu_{0}$ may seem rather academic and in the air (or perhaps, more appropriately, in space !), but it is an issue that cannot be dodged if one is to tackle electrical and magnetic dimensions, because every one of them involves $\kappa_{0}$; or $\mu_{0}$. One of the dangers, in fact, of "practical" formulæ is
that by making these factors equal to 1 they can be left out and are liable to be forgotten.

Since we don't know their dimensions separately we are stuck. The only way out is to conceal our ignorance by introducing a fourth fundamental dimension to supplement $L, \mathrm{~T}$ and M . This fourth dimension is still a matter of controversy. Officially it is $\mu$. But for some purposes it is more convenient to use electrical charge Q ; unit, the coulomb. Another alternative quartet that has been proposed is: $L, \mathrm{~T}$, I, V, leaving mass out. Each different selection of the fundamental four means a different list of dimensions for all the electric and magnetic quantities. If only we knew the dimensions of either $\kappa_{0}$ or $\mu_{0}$, all this uncertainty would be avoided. If, as might well be, $\kappa_{0}$ and $\mu_{0}$ are expressible in terms of $L, \mathrm{~T}$ and M , there would be no need at all for a fourth fundamental dimension.

But since in order to go any further it is necessary to make some sort of a choice, I will follow a number of authorities in taking $Q$ (quantity of electric charge, not tuned circuit " goodness" factor), and on this basis here are the dimensions of the main electromagnetic quantities.

| Quantity | Symbol | $L \quad$ T | M | Q |
| :---: | :---: | :---: | :---: | :---: |
| Capacitance | C | -2 2 | -- 1 | 2 |
| Current | I | $0-1$ | 0 | 1 |
| Electric Charge | Q | 0 | 0 | 1 |
| $\begin{array}{lr}\text { Electric } \\ \text { strength } & \text { field } \\ & .\end{array}$ | $\epsilon$ | $1-2$ | 1 | - 1 |
| Frequency .. | $t$ | $0-1$ | 0 | 0 |
| Inductance | L | 20 | 1 | - 2 |
| $\begin{array}{cr}\text { Magnetic } & \text { field } \\ \text { strength } & \ldots\end{array}$ | H | - $1-1$ | 0 | 1 |
| Magnetic flux .. | $\Phi$ | $2-1$ | 1 | - |
| $\begin{array}{rr}\text { Magnctic } & \text { Flux } \\ \text { density } & . .\end{array}$ | B | $0-1$ | 1 | - 1 |
| Magnetomotive force | F | $0-1$ | 0 | 1 |
| Permeability | $\mu$ | 10 | , | - 2 |
| Permittivity | $\kappa$ | -3 3 | $-1$ | 2 |
| Power .. | P | $2-3$ | 1 | 0 |
| Reluctance | S | $-20$ | $-1$ | 2 |
| Resistance reactance impedance) (also and | R | $2-1$ |  | -2 |
| Voltage or e.m.f. | V, E | $2-2$ | 1 | -1 |

Although this table is not exhaustive, it includes the quantities most commonly used in practiceenough to provide plenty of practice for a start. Here is a very simple example-the time constant of a resistance-capacitance combination, which as you probably know is RC. To get the dimensions of this product, you add the index numbers for R and C . Under $L, \mathrm{C}$ is -2 and R is +2 , so that goes out. $T$ is +2 and -1 , so that goes in, to the first power. $M$ and $Q$ both go out, so the result is $[\mathrm{RC}]=[\mathrm{T}]$, which is obviously correct for a time constant. Now suppose you know that an inductive circuit, consisting of $L$ and $R$, also has a time constant, but you don't know the formula. You could arrive at it by using the table. Try it.

Next consider another simple and well-known formula :

$$
\lambda=\frac{3 \times 10^{8}}{f}
$$

$\lambda$ being wavelength and $f$ frequency. [ $\lambda]$ is, of course, $=[L]$, and $[f]=\left[\mathrm{T}^{-1}\right]$. So it looks as if we are back
at our old absurdity $[L]=[T]$. But having been caught once in this sort of trap we are too wise to buy it again, especially as $3 \times 10^{8}$ is easily recognizable as the approximate velocity of light in space. Putting in its dimensions makes everything right. By now it ought to be clear that one must be on guard against concealed dimensions-hidden under some numerical " constant" which is really a dimensioned quantity with a particular value written in. And in this connection, the speed of light or radio waves in space is such an important constant scientifically that it is sometimes forgotten that in air it is slightly less and in paraffin wax or polythene or other solid or liquid dielectric it is a good deal less, because it depends on the value of $\kappa$. So the wavelength for a given frequency depends on where the waves are travelling.

Here is another example :

$$
Z_{0}=\sqrt{\frac{\bar{L}}{\mathrm{C}}} \sqrt{1-\frac{\omega^{2} \mathrm{LC}}{4}}
$$

If this is to be correct, then $\omega^{2}$ LC must be dimensionless, because it is to be added to 1 . And as the whole second factor under the root sign would then be dimensionless, $\sqrt{ }(L / C)$ must have the same dimensions as $Z_{0}$, which presumably is an impedance. (Actually it is the characteristic impedance of a simple low-pass $T$ filter section.) As to the first point, $\omega \mathrm{L}$ is a reactance, and so is $1 / \omega \mathrm{C}$, so $\omega^{2} \mathrm{LC}$ is a reactance divided by a reactance and is, therefore, dimensionless. The second point could be checked in a similar way, but let us use the table. We first subtract the C index numbers from the L numbers (because L is divided by C ) and then halve the result (to give effect to the square-root sign).

|  | $L$ | T | M | Q |
| :--- | ---: | ---: | ---: | ---: |
| L | 2 | 0 | 1 | -2 |
| C | -2 | 2 | -1 | 2 |
| $\mathrm{~L} / \mathrm{C}$ | 4 | -2 | 2 | -4 |
| $\sqrt{ }(\mathrm{~L} / \mathrm{C})$ | 2 | -1 | 1 | -2 |

As you see, the last line is the same as for resistance, impedance, etc. If you would like another example or two to check, here is the formula for the frequency at which a Wien-bridge type of oscillator oscillates:

$$
f_{0}=\frac{1}{2 \pi \sqrt{\mathrm{R}_{1} \mathrm{R}_{2} \mathrm{C}_{1} \mathrm{C}_{2}}}
$$

And if you want something to get your teeth into, here is one from p. 410 of the November, 1950, issue (No! Not guilty this time!):

$$
\frac{\frac{2 \omega \mathrm{CR}}{\omega^{2} \mathrm{C}^{2} \mathrm{R}^{2}-1}+\frac{2 \omega \mathrm{C}_{1} \mathrm{R}_{1}}{\omega^{2} \mathrm{C}_{1}^{2} \mathrm{R}_{1}^{2}-1}}{1-\left(\frac{2 \omega \mathrm{CR}}{\omega^{2} \mathrm{C}^{2} \mathrm{R}^{2}-1} \cdot \frac{2 \omega \mathrm{C}_{1} \mathrm{R}_{1}}{\omega^{2} \mathrm{C}_{1}^{2} \cdot \mathrm{R}_{1}^{2}-1}\right)}=0
$$

Actually it is nothing like so hard as it looks, and anybody who has had some practice with the kind I have just worked out should be able to O.K. it almost at a glance.

The next one will send you back to the table, and to make it a little more interesting I have introduced a deliberate mistake-a superfluous ${ }^{2}$. Can you work out which one it is?

$$
\mathrm{C}=\frac{\mathrm{L}^{2} \mathrm{I}^{2}}{\mathrm{~V}^{2}{ }_{\mathrm{HT}}}\left(\frac{\mathrm{~V}_{\mathrm{HT}} / \mathrm{V}_{\mathrm{M}}}{1+\mathrm{V}_{\mathrm{HT}} / \mathrm{V}_{\mathrm{M}}}\right)^{2}
$$

The correct version is on p. 314 of the September, 1950, issue, but to save you the trouble of looking it up I will give the answer at the end.

Lastly, here is a formula for the effective height (in metres) at $f \mathrm{kc} / \mathrm{s}$ of a rectangular frame aerial having N turns H metres high and W metres wide. The question is, does the 300,000 conceal any dimensions, and if so what?

$$
2 \mathrm{NH} \sin \left(\frac{\pi f \mathrm{~W}}{300,000}\right)
$$

In case the "sin" bothers you, I may explain that it must be the sine of an angle, and an angle is equal to the ratio of two lengths.

Apart from its value for checking, study of dimensions gives one a more intelligent interest in the formulæ one encounters, and often enables one, by grouping the symbols according to the dimensions, to extract a useful meaning from a new algebraical result.

And with that little summary of the matter, it only remains for me to say that the 300,000 in the last example must have the dimensions of a velocity, as you might have guessed from the number-though you might possibly have been put off by the absence of the other 000, which cancels out because $f$ is in kilocycles per second. And the intrusive ${ }^{2}$ in the previous example is the one attached to L .

## New Enit of Sensilivity?

THE great pioneers of electricity are immortalized in the names of the standard electrical units. Why should the equally great pioneers of radio be denied a similar honour? There are plenty of radio units now awkwardly expressed in electrical terms that deserve decent names of their own.

The thought is brought to mind by a recent leading article in our French contemporary Toute la Radio. It points out that the present expression for receiver sensitivity-so many microvolts to give standard out-put-is unfortunate and misleading because the greater the sensitivity the lower is the figure for expressing it. A way to improve matters, it says, would be to turn the figure into millivolts and give its reciprocal; thus a sensitivity of $20 \mu \mathrm{~V}$ would become 50 and a sensitivity of $50 \mu \mathrm{~V}$ (which is lower) would become 20 . For the name of the proposed unit, the article suggests the French pioneer General Gustave Ferrié. He was head of the French military wireless service, which he


General Gustave Ferrié 1868-1932 started in 1900, but is remembered chiefly as the designer of the famous Eiffel Tower station. He did a good deal of criginal research and was associated with Marconi in some of the early cross-Channel experiments. Britain honoured him with a doctorate of science of Oxford University and he was a vice-president of the old Wireless Society of London, now the R.S.G.B.

So which do you prefer, a sensitivity of 25 microvolts or 40 ferriés?

## CORRECTION

The Haynes e.h.t. unit illustrated on page 393 in the October issue is not oil-immersed as stated, but it is housed in a metal container.

# Holme Moss Television Station 

B.B.C's Third Transmitter Opens

THE new transmitter is situated some eight miles south of Huddersfield on the moor $1,750 \mathrm{ft}$ above sea level. The aerial, which is supported by a $750-\mathrm{ft}$ mast, comprises two tiers of four folded dipoles to give all-round coverage. The radiation pattern is restricted in the vertical plane and by this restriction a horizontal gain of 4 db is obtained.

The vision transmitter has a power output of 45 kW corresponding to peak white and is claimed to be the most powerful television transmitter in the world. The figure of 45 kW does not include the aerial gain; if this were added in accordance with Americar, practice, the station would be classed as one of 110 kW . The frequency is $51.75 \mathrm{Mc} / \mathrm{s}$ and the radiated sidebands lie below the carrier frequency.

The accompanying sound transmitter has a carrier power of 12 kW and operates on $48.25 \mathrm{Mc} / \mathrm{s}$. The outputs of the two are combined in the transmitter building and fed to the aerials via a 5 -in diameret coaxial cable having an impedance of $51.5 \Omega$. This is fitted with expansion joints every 150 ft and is blown to prevent condensation.

The combining unit is made of coaxial resonant sections arranged in the form of a balanced bridge so that substantially the whole of the output of each transmitter is fed to the aerial and very little indeed into the other transmitter. The loss in the resistance load on the bridge is only 300 W .

The vision transmitter starts off with a crystal-controlled drive unit operating at one-sixth carrier frequency. Following stages multiply the frequency and amplify it. The power stages comprise a push-pull class.C air-cooled triode stage which drives a push-pull cathode-follower stage. In its turn this drives the output stage, which is grid-modulated, and uses watercooled triodes in push-pull.

On the video side the incoming signal is amplified

and the picture-sync pulse ratio is adjusted to $7 / 3$. In the sub-modulator and modulator stages shunt-regulated amplifiers are used. The one in the modulator stage has an initial shunt-regulated amplifier with two ACM3 valves followed by a shunt-regulated cathode follower. This modulator has an output impedance of only 5!! and is capable of dealing with the varying grid current of the r.t. stage. This varies from zero to 3 A and has a shunt capacitance of 400 pF !

The shunt-regulated amplifier is one in which the valve concerned has another valve as its load, this load valve being driven also by a signal derived from the first. In the cathode-follower version, the second valve forms the cathode load of the first and its grid is driven from the voltage developed across a resistance in the anode of the first one. The principles involved have already been described ${ }^{1}$, and result in an extremely-low output impedance being obtained and a correspondingly great bandwidth.

The vision signal is taken to Holme Moss from London via Birmingham by standard coaxial cable of

[^6]

Above: A view of the $750-\mathrm{ft}$ mast of the Holme Mcss transmitter showing the station buildings and the stand-by mast. The detail of the television folded-dipole aerials and the v.h.f. slot aerial appears inset

Left : The $45-\mathrm{kW}$ visioin transmitter (left) and the $12-\mathrm{kW}$ sound transmitter (right)

(Left). The final stage of the vision modulator showing also the meter panel. (Right). The sound and vision signal combining unit. Here the signals from the two transmitters are mixed before being passed to the aerial
the type being laid throughout Europe for communication circuits. The cable actually contains six $\frac{3}{8}$-in coaxial tubes, 16 paper-insulated quads for control circuits and 172 quads for local telephone traffic. Two only of the coaxial tubes are available for television, the remainder being used for multi-channel telephone circuits. The signal is shifted in frequency and occupies the band $0.5-4.5 \mathrm{Mc} / \mathrm{s}$; special repeaters are used and, since harmonics of the carrier frequency lie within the pass-band, the repeaters are designed to keep second-harmonic production at least 75 db below the fundamental.
At the station the signal is frequency-changed in two steps back to the video form, the change in two steps being necessary to avoid the production of interfering freqnencies.
For the future station at Kirk O'Shotts, the signal is to be conveyed by a radio link from Manchester, so
that the present Manchester-Holme Moss cable will then form a spur off the main channel.

The cable, repeaters and terminal equipment have been installed and are operated and maintained by the Post Office. The transmitters, both sound and vision, have been supplied by Marconi's W.T. Conpany and are operated by the B.B.C.

On account of the exposed nature of the site, the building is of the cavity-wall type with double windows and is well heated. Since winter may at times isolate it, stocks of food and bedding are held in case the staff are unable to leave the station.
In addition to the main transmitters and aerial, a complete low-power transmitter ( 5 kW vision, 2 kW sound), and a second aerial system on a $150-\mathrm{ft}$ mast, have been installed for emergency use. The main transmitters can be used on the emergency aerial, but with power restricted to 20 kW .

## NEWS FROM THE CLUBS

Birmingham.-The annual general meeting of the Slade Radio Societv will be held on November 23rd. At the meeting on December 7th G. P. Thwaites, of Standard Telephones \& Cables, will talk on the manufacture of cathode-ray tubes. Meetings are held on alternate Fridays at 7.45 in the Parochial Hall, Broomfield Road, Erdington. Sec.: C. N. Smart, 110, Woolmore Road, Birmingham, 23.

Cleckheaton.-" The History of the R.S.G.B." is the subject of the talk by C. Sharp, G6KU, at the November 7th meeting of the Spen Valley Radio \& Television Society. Films provided by the Yorkshire Electricity Board will be shown at the meeting on November 21st. Meetings are held on alternate Wednesdays at 7.30 at the Temperance Hall, Cleckheaton. Sec.: N Pride, 100, Raikes Lane, Birstall, nr. Leeds.

Kingston.-An exhibition has been organized by the Kingston \& District Amateur Radio Society in aid of the United Appeal for the Blind. It will be held from 2 to 10 p.m.
on November 10th at the club's headquarters, Penrhyn House, Penrhyn Road, Kingston-on-Thames, and exhibits will include the radio-controlled model boat "Miss Eedee," which recently crossed the Channel. A transmitter will be in operation and home-constructed gear will be exhibited. Sec.: R. S. Babbs, 28, Grove Lane, Kingston-on-Thames, Surrey.

Leicester.-"Ele.trons" is the title of one of the films to be shown to members of the Leicester Radio Society on November 6th at the Club Room, Holly Bush Hotel, Belgrave Gate, Leicester. Sec.: L. Milnthorpe (G2FMO), 3, Winster Drive, Thurmaston, nr. Leicester.

Manchester.-Another club was added a few months ago to those already active in and around the city. The Waterloo Radio Society, as it is called, meets each week at St. Albans School, Barrow Hill Road, Waterloo Road, Cheetham. Sec: J. C. Henderson, 47, Maple Street, Cheetham, Manchester, 8, Lancs.

# Manufacturers' Products 

## New Equipment and Accessories for Radio and Electronics

## Tape Recorder Unit

$A^{\mathrm{N}}$ endless loop of tape is used in the magnetic recorder mechanism recently put on the market by Phidelity Magnetic Products, Ltd., of 65-66, Chancery Lane, London, W.C.2. This is 600 ft long and gives 30 minutes of reproduction at a speed of $3 \frac{3}{3}$ in per second. A higher running speed is also provided for, and this, with the aid of the footage counter. permits rapid selection of various parts of the loop. By means of contactor strips joined into the tape an automatic stop relay can be operated, so that if the loop is used for a number of short recordings it can be stopped at the end of each. For normal use a single contactor strip serves to identify the start and finish of the loop.

Suitable for building into a complete tape recorder, the unit is light in weight and has the unusually small dimensions of $10 \mathrm{in} \times 6 \mathrm{in}$. It can be supplied with record and erase heads of either low impedance or high impedance.

## Miniature Earphone

A NYONE who has experienced the discomfort of having his ears flattened against his head for several hours at a stretch will appreciate the advantages of the miniature hearingaid type of earphone. The ME3 model produced by Bonochord, of 48, Welbeck Street, London, W.1, is an example of what can be done in small size and light weight-it measures ${ }_{i \frac{3}{6} \text { in (diam) by } \frac{3}{8} \text { in (depth) and }}$ weighs $\frac{1}{3} \mathrm{oz}$. Inside is a radial Alcomax magnet with a Radiometal polepiece and a polystryrene bobbin wound with nylon-covered wire. For general use (not as a hearing-aid) the diaphragm is made of annealed steel and has an armature of silicon steel in the centre-by varying these the frequency response can be altered
within limits. The impedance is $80 \Omega$ at $800 \mathrm{c} / \mathrm{s}$ and the d.c. resistance of the coil is $42 \Omega$. Maximum power admissible is 25 milliwatts.

Electrical connection is made through spring contacts which retain the plug with a definite click-action.

## Amateur Beam Aerial

DESIGNED for use on the 2 metre amateur band, the Eddystone beam aerial in the illustration has a bandwidth of $144-146 \mathrm{Mc} / \mathrm{s}$ when properly adjusted to the mid-


Eddystone omoteur beam oerial.
band point. The radiator is a folded dipole formed of two brass tubular U-sections which fit into a centre section permanently fixed to the main boom; the other elements slide into support tubes welded on to the boom at the correct spacings. All elements can be adjusted in length and then locked. Overall gain is 9 db and the back-to-front ratio is 20 db .

The aerial is constructed of brass and copper and weatherproofed with durable black enamel. Measuring $43 \mathrm{in} \times 42 \mathrm{in}$ (maximum) and weighing ${ }^{3} \mathrm{Ib}$, the array has a low wind resistance and can be mounted on unstayed masts of up to 25 ft in height. It is available from the makers, Stratton \& Co., Ltd., Alvechurch Road, West Heath, Birmingham 31, at £4 16s 3d.



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# RANDOM RADIATIONS 

By "DIALLIST"

## Simple, My Dear Watson!

 A correspondent, who tells me that, although he has long been a landline telegraph operator, he knows nothing of wireless, is puzzled by the performances of a single-valve shortwave receiver which he has rigged up. He is not so much surprised by the fact that he can pick up morse transmissions from most parts of the world as by his ability to change from station to station without tuning. One night he ranged, without touching a thing, from Sweden to Panama, from Italy to Dutch Guiana, from Poland to Brazil, the United States, Holland, Honduras and many other countries. How, he asks, could this be possible? Simple, my dear Watson! Anyone who remembers using a home-made single-valve set in the early days of short-wave transmission and reception could give the answer at once. Just a case of hand capacitance, or body capacitance, to use the alternative name for the same thing. It occurs to me that many of the younger readers of $W . W$. may never have had experience of, or been exasperated by, this interesting effect. If you do your short-wave listening with a modern superhet, it isn't likely to be noticeable; but with a simple single-valve set it is usually very much in evidence.
## IIand Capacitance

The tuning of such a set is a very critical business, particularly on faint signals. If large unscreened coils are used (as they were in those days by most of us, and as I gather they are now by my correspondent), capacitance between the body of the operator and the coils-and, for that matter, other parts of the receiver-can have quite remarkable effects on the tuning. A common experience in the old days was to work up some faint signal to reasonable strength by long and patient hairbreadth tuning-and then to lose it (often for good and all!) by a small movement of hand or head. There were not so very many short-wave stations then, so that losing one did not often mean an automatic change to another, as it well might with that kind of set on to-day's crowded wavebands. Those who used early short-wave singlevalve receivers will recall the metal screens behind the front panels and
the enormously long extension tuning spindles that we fitted in the hope of eliminating the effects of this capacitance. There was an apocryphal tale of an expert who, on being asked by the twentieth beginner in one day "How can I avoid handcapacity?" (we called it capacity then), replied wearily "Try tuning with your toes, young man."

## Television in the States

On the day on which these notes were written I had a visit from a young friend who had just arrived back by air from a visit to Washington and New York; it was, in fact, less than 36 hours since he had left America. As he is a television enthusiast, we naturally soon found ourselves discussing the comparative merits and demerits of $50-\mathrm{c} / \mathrm{s}$, 405line, and $60-\mathrm{c} / \mathrm{s}, 525-$ line television. He had been greatly impressed by the size of c.r.t. screens in the U.S.A., by the number of programmes available at almost any reasonable hour and by the fact that it seemed to be the normal thing for hotels to be prepared to install a television set in any visitor's room in a matter of minutes, should he desire one and be willing to pay the charge made for the use of it. And, moreover, anyone can have the benefit of television, whether or not he owns a receiver or hires one in his hotel room; for television sets are part of the ordinary equipment of countless shops, bars, restaurants and so on. Television, in a word, is now firmly established as part of the everyday life in the big cities in the U.S.A.

## The Technical Aspect

My young friend formed the opinion that the general standard of television there is, from the technical point of view, nowhere near that set by the B.B.C. Note that I write "the general standard". the big transmitting stations, run by important manufacturing concerns, have high technical standards, which are rigidly maintained. But these stations are vastly outnumbered by others, often of very low power to our way of thinking, whose main puroose is to use television as the jam which mitigates the underlying dose of publicity. The quality of the
transmissions from these stations was generally speaking not too good; and often it was very poor. Defective linearity was the most frequent shortcoming, but other forms of distortion also occurred in many of the transmissions. His general impressions may be summed up like this: it was pleasant to have such a number of alternative programmes on tap for such a large part of the day, but not so good to find so few genuinely wattworthy. America is a little ahead of us in the matter of large-picture receivers and naturally a good deal ahead in long-distance relaying; but, taking it all round, our quality standards are higher and better maintained in both transmission and reception. Our 405 -line system gives at least as good a "direct" picture as their $525-$ line, and a much better picture from the majority of O.Bs and relays.

## Preferred Values

One day during a wartime radar course I was being put through a practical test by the chief instructor. "What's the value of that resistor?" he asked, pointing to one of the dozens that could be seen from the back of a stripped receiver. "Somewhere about 50,000 ohms," I replied.
"Come, come, I want a less vague answer than that. These radar sets are precision instruments." Being a student of rather senior rank I ventured to say: "Yes, I know; but the value of that particular resistor isn't all that critical. The book says 47,000 ohms, but I'm open to bet that if we take this one out and measure it, it will be some way off that figure." Well, we did take it out and it measured up at 49,250 ohms. It might equally well have shown any value between 42,300 and 51,700 ohms, for it was one of the $\pm 10$ per cent tolerance range. I don't know what happened in the other Services, but in the Army there was a tendency at one time to accept those preferred-value 47 s as fundamental truths-and it's quite possible that people were occasionally ploughed for giving "wrong" answers that were actually right. One sometimes finds the same sort of tendency in civil life. After all, 47 . . looks like an exact figure and is therefore apt to be misleading. The purpose underlying the adoption of these preferred values was to enable manufacturers to market colour-coded resistors of about $500,5,000,50,000$ and 500,000 ohms. With a $\pm 10$ per cent or $\pm 5$ per cent tolerance 47 . . . is a convenient middle figure-for manufacturing purposes. It isn't so
convenient for other purposes and I would like to see a return in circuit diagrams and so on to the fives and fifties. What do you think?

## The Bowl Fire

The problem I offered in the September issue was, briefly, this: with various domestic electrical appliances at work in the room, a wireless receiver produced loud interference noises from its loudspeaker. No electrical measuring instruments were available. How (a) could you most quickly determine which, if any, of the appliances at work was guilty? And (b) given that a bowl fire was responsible, what do you think was happening? I warned readers that it was something that I'd never come across before. The quickest way of tracking down the culprit is to switch off the appliances, one at a time. Cutting out the bowl fire brought instant peace. It was switched on again and the noises restarted almost at once. This bowl fire had a screwin heater element and a small intermittent arc was seen to be occurring at a point near the outer end of the socket between the male and female threads. I had the chance next day of examining the thing before it went off to be repaired. It was connected by a properly wired 3 -pin plug to a wall socket. The phase-lead connection was to the central "button" of the heater but the male thread of the heater and the female thread of the socket were coated with the dirt and oxidization of years of happy-go-lucky neglect. Moral: if you've a bowl fire, take out the heater element every so often and give both its thread and that of the socket a clean up with an old piece of fine emery cloth.

## Manufacturers' Literature

Message Repeater, a tape equipment for recording and repeating messages over a telephone network, described in a booklet from the Westinghouse Brake \& Signal Company, 82, York Way, King's Cross, London, N. 1.
Automatic Announcer tape equipment suitable for railway stations, described in another booklet from Westinghouse.
Osram Valve Manual Part 1, including receiving valves, c.r. tubes and electronic devices, available from The General Electric Co., Magnet House, Kingsway, London, W.C.2, at 5 s .
"High Definition" television receiver with a 15 -in tube, described in a leaflet from Sound Sales, Ltd., West Street, Farnham, Surrey.

Hearing Aid, a new Melotone model claimed to be economical to maintain, described in a leaflet from Cunningham Beattie, Ltd., 49, Wigmore Street, London, W.1.

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## Comfort While You Look

JUST lately Mrs. Free Grid has been away from home, having gone on a mountaineering expedition by helicopter with some other members of a " Women's Uplift Society" to which she belongs. This has rather left me to my own devices and I have been compelled, among other things, to patronize one of those establishments fitted with a dozen or more washing machines-laundrettes I believe they are called-which enable people to rend their own garments instead of leaving the job to somebody else.

I was washing out my smalls the other day and marvelling at the ingenuity of the slick business man who had first thought of the moneymaking possibilities of fitting up a large empty shop with rows of washing machines, when the idea came to me of trying to make an honest penny myself by fitting up a similar shop with lines of television sets where people might come and enjoy the tclevision programmes in comfort.

Now some of the less wellinformed among you may ask why I should expect people to patronize my proposed public television parlour when they can enjoy the programmes in greater privacy in the comfort of their own homes. But anybody who is in touch with housing conditions to-day knows that privacy is at a premium and our budding Benedicts are forced into the Rank atmosphere of the local amatorium where they are compelled to sit herded together in the darkness with a complete absence of home comforts.
There will be none of that sort of thing in my proposed establishment, which will have curtained cubicles and comfortably cushioned armchairs to reproduce, as far as possible, the conditions of home as it should be.

But anybody who expects to find what our American friends would probably call a " petting parlour," maybe a "necking niche," will have Mrs. Free Grid and her Watch Committee to reckon with, as the guiding principle will be comfort and not cuddles while you look.

## Which Came First?

ONE of the most interesting articles in the September issue of $W . W$. was that on radio telearchics. I must confess, however, that I feel very troubled about the misleading effect which the opening sentence may have on some of you. To save you the messy business of unwrapping your fish and chips, I will quote the exact words of the learned scribe: "Probably one of the carliest radio telearchic systems was that demonstrated at the Paris Exhibition of 1906 , when Professor Branly, using his famous coherer, showed how apparatus could be switched on and off at a distance."

Now I don't quarrel with the facts as stated, but I feel much less easy in my mind about the interpretation expressed in the opening words. I cannot help thinking that if I let this go unchallenged, some of you, who are too young to know anything of the early days of wireless, may think that radio telearchics was invented subsequently to wireless telegraphy, and I have more than a suspicion that the writer of the article, through a mental oversight, may even think that himself.

Actually, the reverse is true and radio telearchics was first in the field; indeed, it had to be as you will realize if you will give the matter a moment's thought. We will go no farther back than Marconi and his contemporaries of the 'nineties, all of whom sought a practical means of sending messages with-


Washing my Smalls. out the aid of wires over distances outside the range of optics and acoustics. Now in those days Mr. and Mrs. Piddington had not made telepathy the popular pastime it is to-day and so Marconi and other pioneers could not hope that their ether-borne messages would act directly on the brain cells of the intended recipients. It was obviously necessary, therefore, to devise means whereby the incoming wireless waves would switch on some sort of machinery which would automatically switch itself off


Earls Court, 1913.
when they ceased to arrive. The coherer and the morse inker (and later the headphone diaphragm) provided the answer to the problem, the decoherer and the back-spring of the inker-armature restoring the status quo when wavertains ceased to arrive. Whichever way you look at it, therefore, telearchics had of necessity to precede telegraphy; it had, in fact, to be invented as a necessary preliminary to communication.
Talking of telearchics, I should like to say how good I thought the demonstration was at Earls Court, but I don't think it was better than a telearchic display I saw, also at Earls Court, as long ago as 1913. In view of the limited technical resources available then, it certainly was marvelious but not quite so wonderful as W.W.'s over-enthusiastic Venerable Bede of those days would have us believe when he wrote in the September, 1913, issue that the model airships taking part in the demonstrations were "propelled by wireless."

## Modulation

THE divided opinions in technical circles about the respective merits and demerits of a.m., f.m. and p.m. are strongly reminiscent of the state of affairs which existed forty years or so ago when the burning question of the hour was c.w. or spark, or, in terms of personalities, Poulsen or Marconi. C.W. seemed, in broad theory, as though it ought to be the answer to the wireless maiden's prayer, but, in practice, it certainly was not. Long years afterwards, of course, c.w., with improved and, indeed, totally different methods of generation, turned the tables and pushed spark clean off the map, if I may mix my metaphors.

Casting our minds forty years on, it is highly probable that improved technique will have enabled one particular method of modulation to put all others out of court. I wonder which it will be?


An inexpensive yet precision instrument da inexped especially to meet the exacting needs of the modern service With six and laboratory technician. $50 \mathrm{Kc} / \mathrm{s}$. to frequency ranges covery is better than $80 \mathrm{Mc} / \mathrm{s}$., its acale reading. $15.5 .5 \mathrm{Mc} / \mathrm{s}$. \begin{tabular}{l|l}
$\pm 1 \%$ of the scale \& $1.5 \mathrm{Mc} / \mathrm{s} .5 .5 \mathrm{Mc} / \mathrm{s}$. <br>
$\pm 0 \mathrm{Kc} / \mathrm{s} .-150 \mathrm{Kc} / \mathrm{s}$. \& $5.5 \mathrm{Mc} / \mathrm{s} .-20 \mathrm{Mc} / \mathrm{s}$.

 

$150 \mathrm{Kc} / \mathrm{s} .-500 \mathrm{Kc} / \mathrm{s}$. \& $20 \mathrm{Mc} / \mathrm{s} .-80 \mathrm{Mc} / \mathrm{s}$. <br>
\hline
\end{tabular} $500 \mathrm{Kc} / \mathrm{s} .-1.5 \mathrm{Mcis}$. Scale sub-divisions for use in teleadequate discrimination Note the starred vision circuits. which combine to features below, mim signal of less than maintain a minimum and less than $3 \mu \mathrm{~V}$ $1 \mu \mathrm{~V}$ up to $20 \mathrm{Mc} / \mathrm{s}$. and $80 \mathrm{Mc} / \mathrm{s}$. between $20 \mathrm{Mc} / \mathrm{s}$ and 8

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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MF13-1 | 5" radar ube with metal-backed magnesium fluoride screen | Octal | 127.5 | 292 | 6.3 | 0.3 | 450 | 11 |
| MF31-22 | $12^{\prime \prime}$ radar tube with metal-backed magnesium fluoride screen | B12A | 308 | 471 | 6.3 | 0.3 | 400 | 11 |



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TYPE M5 $6 \frac{1^{\prime \prime}}{} \times 3 \frac{1^{\prime \prime}}{}{ }^{\prime \prime}$ R.F. loading 35 kVA .
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f28.17.8

## Model T845

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110/250.

## Model T675

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Vf If Va (Max) Wa
gm (Class B push pull)

* Taken at $\mathrm{Va}=1 \mathrm{kV} . \quad \mathrm{Vg}=-55 \mathrm{v}$.


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H\$63. Output $250-0-520 \mathrm{v}, 60 \mathrm{~m} / \mathrm{a}$., 6.3 v . at 3 amps., 5 v . at 2 amps.
HS 40. Windings as above. 4 v . at 4 amps ., 4 v . at 2 amps . Output
HS2. $250-0-250 \mathrm{r} .80 \mathrm{~m} / \mathrm{a}$
HS3. $350-0-350 \mathrm{v} .80 \mathrm{~m} / \mathrm{a}$. HS30. $300-0-300 \mathrm{v} .80 \mathrm{~m} / \mathrm{a}$ HS2X. $250-0-250 \mathrm{v} .100 \mathrm{~m} / \mathrm{a}$. HS75. $275-0.275 \mathrm{v} / \mathrm{a} .100 \mathrm{~m} / \mathrm{a}$. HS30X. $300-0-300 \mathrm{v}, 100 \mathrm{~m} / \mathrm{a}$. HS F Fux. $350-0-350 \mathrm{v}, 100 \mathrm{~m} / \mathrm{a}$
FSM63. (Midget). Output $250-0-250 \mathrm{v} .60 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v}$. at 3 amps., 5 v. at 2 mps .
FS2. $250-0-250 \mathrm{v} .80 \mathrm{~m} / \mathrm{a}$
FS30. $300-0-300$ v. $80 \mathrm{~m} / \mathrm{a}$. FS $3.350-0-350 \mathrm{v} .80 \mathrm{~m} / \mathrm{a}$
FS2X. $250-0-250 \mathrm{v} .100 \mathrm{~m} / \mathrm{a}$. FS75. 275-0-275 v. $100 \mathrm{~m} / \mathrm{a}$
FS 30 X. $300-0-300 \mathrm{v} .100 \mathrm{~m} / \mathrm{a}$. FS 3 X . $350-0-350 \mathrm{v} . ~ 100 \mathrm{~m} / \mathrm{a}$
All the above have 6.3-4-0 v. at 4 amps ., $5-4-0 \mathrm{v}$. at 2 amps .
Alt the above have $6.3-4-0$ v. at 4 amps ., $6.4-0$ v. at 2 amps .
F $\$ 43$. Output $425-0.425 \mathrm{v} .200 \mathrm{~m} / \mathrm{a}$., 6.3 v . 4 amps., C.T. 6.3 4 amps., C.T. 5 v .3 amps. Fully shrouded
FS50. Output $450-0.450 \mathrm{v}$. $250 \mathrm{~m} / \mathrm{a}$., 6.3 v .2 amps., C.T. 6.3 r FS50. Output $450-0-450 \mathrm{v}$. $250 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{e}$. 2
F30X. Ourput, $300-0-300$ v. $80 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v} .7 \mathrm{amps} ., 5 \mathrm{v}$.2 amps . Framed. Flying leads
F35X. Output, $350-0-350$ v. $250 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v} .6 \mathrm{amps} ., 4 \mathrm{v} .8 \mathrm{amps}$. . 4 v .3 amps., 0-2-6.3 v. 2 amps. Fully shrouded
FSI60X. Output, $350-0-350$ v. $160 \mathrm{~m} / \mathrm{3} ., 6.3 \mathrm{v} .6$ amps., 6.3 v .
3 amps., 5 v .3 amps. Fully shrouded
FS43X. Output, $425-0-425$ v. $250 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v} .6 \mathrm{amps} ., 6.3 \mathrm{v}$ 6 amps., 5 v. 3 amps. Fully shrouded
HS6. Output, $250-0-250$ v. $100 \mathrm{~m} / \mathrm{a}, 6.3 \mathrm{v} .6$ amps., C.T. s v.
3 amps. For receiver RI355. Half shrouded
HS150. Output, $350-0-350 \mathrm{v}$. $150 \mathrm{~m} / \mathrm{a}$., $6.3 \mathrm{v} .3 \mathrm{amps.}$, C.T. 5 v .
3 amps. Half shrouded
F36. Output, $250-0-250$ v. $100 \mathrm{~m} / \mathrm{a}$., 6.3 v .6 amps., C.T. 5 v
Famps. Half shrouded
FSI20. Outpur, $350-0-350$ v. $120 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v}, 2 \mathrm{amps} .$, C.T. 6.3 v .
2 amps., C.T. 5 y. 3 amps . Fully shrouded
FS256. Output, $250-0-250$ v. $80 \mathrm{~m} / \mathrm{a}, 6.3 \mathrm{v}$. at 6 amps., 5 v . at 3 amps. Fully shrouded
PRI/I. Output 230 v at $30 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v}$. at $1.5 / 2 \mathrm{amps} . .$.
FS150. $350-0.350 \mathrm{v} .150 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v} .4 \mathrm{amps}$, $5 \mathrm{v}, 3 \mathrm{amps}$
FSI $50 \times$. Output, $350-0-350 \mathrm{v}$. at $150 \mathrm{~m} / \mathrm{a}$., 8.3 v . at 2 amps
C.T., 6.3 v . at 2 amps ., C.T. 5 v . at 3 amps . Fully shrouded

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F4. Output, 4 v. 2 amps.. F6. Outpur, 6.3 v. 2 amps.
F12X. Output, 12 v . at $1 \mathrm{amp} .9 /$ - F 6 X . Outpur, 6.3 v .0 .3 amps .
F12. Output, 12.6 v . tapped 6.3 v . at 3 amps .
F24. Output, 24 v . tapped 12 v at 3 amps .
Fi2 and F24 framed with Flying Leads.
FU6. Output, 0-2-4-4-6.3 v. at 2 amps.
F29. Output, 0-2-4-5-6.3 v. at 4 amps .
FU6 and F29 clamped with Flying Leads.
F5. Output. 6.3 v . at 10 amps . or 5 v . at 10 amps . or 12.6 v . at
F6/4. Output, four at 6.3 v . tapped at 5 v . at 5 amps. per winding,
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20 v . at 5 amps ., 18 v . at 5 amps ., 15 v . at $5 \mathrm{amps} ., 12.6 \mathrm{v}$. at
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## ULTRA GEN

No. 3

## SOUND WITH VISION

It is a fact that realism in Television reception depends on both the quality of the picture and fidelity of the sound. A picture-however good-accompanied by poor sound quality, loses a great deal of effect and entertainment value.

The audio frequency range required for optimum tonal balance varies with the size and shape of the cabinet used. A large cabinet which inherently extends the "bass" response requires a corresponding increase in the higher audio-frequencies.

We recognise these facts and provide an audio channel of generous output power, with a bandwidth limited only by these acoustic considerations.

With Radio, however, the bandwidth and hence the audio response normally obtained (curve 4) is restricted by selectivity problems not present in Television reception. This restriction makes it difficult to obtain optimum tonal balance in a Radio receiver, particularly when using a large cabinet.

The design of a combined Television/Radio receiver therefore posed an anusual problem, since we decided that the radio sound reproduction must be comparable with the high quality provided on our Television sound channel.

At first sight, this seemed to require an expensive specially designed I.F. Amplifier for the Radio channel. The problem, however, was solved simply and economically by the use of our neutralized overcoupled Radio I.F. Amplifier stage (see W.W. July, 1951).

RESULT: Matched audio channels providing the same high quality sound for both Radio and Television (curves 2 and 3).
The electrical response curves below illustrate these points.
Curve (1) Response obtained on Television, but only suitable for use with a High-Fidelity reproducer (such as a Reflex cabinet system).
Curve (2) Television response necessary for good balance with a normal cabinet.
Curve (3) Radio response obtained using our neutralized over coupled I.F. amplifier-showing the close match with the Television response.
Curve (4) Radio response showing the attenuation of the "top" that occurs when the Radio I.F. amplifier is of the usual type with QK $<1$. If used on a combined Radio/Television receiver, the Radio tone would sound dull and lifeless in comparison.


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## Ihro of Ine latest <br> fROM THE RANGE OF B.S.R.GRAMOPHONE UNITS



MUS GRAMOPHONE MOTOR UNIT
MUJ. This De-luxe 78 RPM unit is fitted with an $8^{\prime \prime}$ diameter turntable, allowing it to be mounted in a neat compact case while still being able to play all sizes of records. It is the ideal gramophone unit for portable record players or gramophones and radiograms designed for space consideration. It is the manufacturers' choice where dependability 'coupled with low cost is essential. Models available for 78 RPM or $33 \frac{1}{3}$ RPM. Ideal for use with any type of pick-up.


TP1. SHADED POLE INDUCTION MOTOR been designed to give the maximum efficiency with the minimum physical dimensions. It is a motor with a thousand uses. SPECIFICATION:-
Voltage: 200/250, Frequency: 50 cycles. (Other voltages and frequencies to order.)

Starting Torque: $1.0-1.5$ inch ozs.
Full Load Torque: $1.2-2.0$ inch ozs. Mains Consumption: 10-15 watts.

Depending on temperature rating.
Speed (light): 2900 RPM
Shaft Diameter: . $1560^{\prime \prime} \pm .0000$
.0002

## Wiredess TJorld

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RADIO, TELEVISION
AND ELECTRONICS
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41st YEAR OF PUBLICATION

Managing Editor: HUGH S. POCOCK, M.I.E.E.
Editor:
H. F. SMITH
NOVEMBER 1951
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## VALVES...and their Applications

## R.F. VOLTAGE AMPLIFYING

INDIRECTLY-HEATED VALVES FOR BROADCAST RECEIVERS

The I.F. Stage

The I.F. stage requires a valve capable of providing a large gain with the desired bandwidth. It must give stable operation under all conditions, and its characteristics must be suitable for the application of A.V.C. A.V.C. must not, however, cause serious variations in the response curve of the stage, and the valve must be capable of handling input and ontput voltages over a wide range of signal levels without undue distortion. All these requirements are met by the Mullard EF41 and UF41 medium-slope, high impedance variable-mu pentodes.
The anode-to-control-grid capacilance of these valves is sufficiently small to ensure stable operation with normal I.F. transformers, provided that reasonalle care is taken with the wiring layout.
Using critically-coupled I.F. transformers having a single circuit impedence of $0.2 \mathrm{M} \Omega$, gains in the order of 200 are obtainable when the following stage is of high impedance. When, however, us is usual, a single I.F. stage is followed by the detector and A.V.C. diodes, the damping imposed by these diodes limits the gain from the grid of the I.F. valve to the detector input to about 100 , assuming a detector load of $0.5 \mathrm{M} \Omega$.
In normal 4-valve receivers where the detector is followed by an A.F. amplifier and high-sensitivity output pentode, the input required at the detector for full output can easily be obtained from the J.F. valve with moderate input signals. In order to reduce the risk of overloading on strong signals where the A.V.C. circuit is supplying a large hias voltage, the A.V.C. characteristics of the EF41 and UF41 are so matched to those of the corresponding frequency changers that, when the same A.V.C. voltage is applied to hoth stages, the gain of the I.F. valve with sliding screen voltage is reduced more slowly than that of the frequency changer.
The signal voltages on the I.F. valve are therefore not allowed to become excessive, and modulation distortion in this stage is small.
These valves may also be used as R.F. amplifiers before the frequency changer stage. For this application the screen voltage should be ohtained via a potentiometer


THE COMPLETE SERIES

|  | FREQUENCY <br> CHANGER | R.F. or I.F. <br> AMPLIFIER | DET., A.F.AMPLIFR. <br> \& A.V.C.DIODE | OUTPUT <br> PENTODES | RECTIFIERS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6.3 Heater | ECH42 | EF41 | EBC41 | EL41; EL42 | EZ40; EZ4I |
| 0.1 AHeater | UCH42 | UF41 | UBC41 | UL41 | UY41 |

Reprints oj̈ this article together with udditional dain may be obtained free of charge from the address below.

## EXTRA RUGGED . .

# production of <br>  




## to new high standards of accuracy

Demands from Industry and the Services for valves of a higher standard of accuracy and reliability have called for consideration of the machines employed in their manufacture. The result has been that our engineers have produced these two outstanding machines, both of which have been designed for the high speed production of valve components to a standard of accuracy and ruggedness which so far has not been equalled anywhere in the world.
These machines are already operating in Britain, U.S.A. and other parts of the world. In the Brimar Valve works at Footscray, Kent, England, they are engaged in the production of the high accuracy, extra-rugged Brimar TRUSTWORTHY Valves.
Please ask us for comprehensive details of these outstanding machines.

## NOTE THESE IMPORTANT FEATURES

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Designed to meet the need for a British stem machine. Capable of producing extra rugged miniature and noval stems with a high degree of accuracy, the Mitchell-Brimar stem machine offers these outstanding features :-

Processes actually carried out on the machine :
(a) Fine polishing of the glass disc.
(b) Bubble cushions raised in the glass around lower parts of pins
(c) Hydrogen cleaning of the upper and lower parts of the pins.
(d) The setting of the correct radial compression strain in the glass dise.

Simple change-over permits production of B7G or B9G stems at will.
Production rate 700 per hour approx. with a loss of 2 per cent. max.
One operator only.
Accessible adjustments
Easily and quickly dismantled. Extremely robust construction.
Easy maintenance.
Automatic pin feed
Automatic eiection of finished stem.

## The BRIMAR Grid Winding Lathe

The Brimar Grid winding lathe has been developed in order to produce a finished grid in one operation, thus reducing costs and improving the product.

1. Constant and variable-pitch grid production.
2. Increased accuracy of grid lengths.
3. Elimination of "spring back" when support wires are cut.
4. Maximum possible work can be done on grids on or at the machine. Thus it is possible to:
(a) Wind to the final profilc wherever the required profile permits
(b) Hot-stretch the strip
after winding, to
(c) raighten support wires

Burn out, during winding, the loose turns
(d) Autoen grids.
(d) Automatically stake
grids during winding.
(c) Cold-stretch, during the winding cycle, strips unsuitable for hot-stretching.
(f) Chop grids accurately to length.
5. Unusua. mechanical soundness.
6. Frecly interchangeable parts.

high fidelity MICROPHONES
FOR PUBLIC ADDRESS : RECORDING: AMATEUR RADIO


## TYPE MIC 22

This model incorporates the famous Acos "Filtercel " insert giving extreme sensitivity and high fidelity. Response is substantially flat from $40-6,000 \mathrm{cps}$. The microphone is vibration and shock proof and is not affected by low frequency wind nolses. Two alternative mountings are available for the MIC 22 head:
MIC 22-2 is supplied as a complete unit incorporating an attractive desk stand with cable side entry.
MIC 22.1 is for fitting to any British or American type standard floor stand and can also be used as a hand microphone.
PRICE 66 - 6. (Either Model)

TYPE MIC 16 Incorporates the Acos Floating Crystal Sound Cell giving a response substantially flat from $30-10,000 \mathrm{cps}$. Performance is unaffected by vibration or shock and low frequency wind noises. As in the case of the MIC 22, two alternative mountings for the MIC 16 head are available :
MIC 16-2 is a complete desk stand unit with side cable entry.
MIC 16-1 is ready for fixing to either British or American type floor stands by means of a knurled ring. PRICE 112 - 12. (Either Model)



## Providing technical information, service and advice in relation to our products and the suppression of electrical interference

What price snob appeal ?
There was a time when television aerials were erected with a view to making neighbours jealous. In those days, the more elaborate the aerial the greater the heart burning of the neighbours. It seems that shortage of materials is now controlling this ridiculous state of affairs. We have always deplored the "overselling " of television aerials, apart from the fact that to sell a more expensive aerial than is necessary is not good for dealer-customer relationship ; an unnecessary array of aerials is apt to cause some local authorities to act against their erection. There will always be places within a few miles of a transmitter where an ' $H$ ' will be found necessary because of interference or "ghosts," but we are delighted to record that there has been an enormous increase in the sale of dipoles, both indoor and outdoor.

## What is the average price of an

 aerial and what kind should I get?The latest designs bring down our average price of a TV aerial to something under four pounds inclusive of cable and we still sell all we can make of 'Multirod ' and 'Senjor H' for fringe area reception. Even so, this is not enough to meet the demand. We anticpiate that the sale of 'Doorods' at 26/6 (with feeder) and dipoles at $37 / 6$ (without feeder) will leap ahead still further. By the time this appears in print Holme Moss will be on the air. Reports of the test transmissions at this early date tend to indicate that the B.B.C. have been very conservative in their estimated coverage, but would we not all rather have a conservative figure than an exaggerated one?

Faced with the admitted shortages, we cannot see dealers erecting a senior 'H' aerial in a location where a dipole will do the job, or an outdoor dipole where a 'Doobrod' aerial is good enough. There will be lots of locations where the senior ' H ' will be essential and these aerials are hard to come by. In such locations an inferior grade of aerial will not do, and the sale of a receiver may be lost to a dealer who has the correct aerial. Normally it is silly


## Survey of Holme Moss Area

This is being written at the Radio Show, Earls Court. The number of visitors from the Holme Moss area is very surprising. All ask the question " I live at so-and-so, what aerial will I need "? That is very difficult to answer; all indications confirm that, in general, coverage will be much greater than was expected by anybody. This means that fewer ' H ' type aerials will be required "close in," and that those in the populated areas of the North East will have a greater chance to receive television.

Those who have been reading this page for over a year will recollect that when Sutton Coldfield opened we carried out an independent field strength survey on a radius of about 75 miles. We propose to do the same in Holme Moss area. The figures will be made known to readers as they become available. The last survey we carried out was greatly appreciated by Dealers, Press, Manufacturers and Technical Bodies. We will gladly add to our list names of those who would have use for such information. Members of the public are asked not to apply, as their interest can only be in respect of one location and the field strength figures will be publisbed in the "Wireless World" as they are produced.

It may interest some to learn that this new survev will be carried out on our new Mobile Research Unit This has been built on a two-ton chassis and is more robust in every way. The experience gained with the first vehicle has made it possible to design one much more suitable from practical as well as technical standpoints.

Feeding two receivers from one aerial.
With the ever increasing popularity of television, tenants of semidetached or terrace houses are suddenly faced with the fact that they have at least one thing in

common with their immediate neighbours-a chimney stack!
Consequently the question of feeding two receivers from one aerial is one that occurs frequently in our correspondence.
Where co-axial feeder is employed we usually suggest the arrangement shown in figure $\mathbf{I}$.


The three resistors should ali be of the same value, i.e. 27 ohms.

It should be noted that this system means that each set will receive a signal which is 6 d.b. down, compared to that being supplied by the aerial. It is therefore a matter for decision as to whether the signal strength allows for this degree of attenuation.
For twin feeder, a suggested arrangement is shown in figure 2.

## What is a good aerial ?

Every month many thousands of people take delivery of their new television receivers, and many more decide to invest in one. To those in the latter category, our advice is to buy the best television aerial you can for your own location.

The best is neither the one that is the more expensive nor the one that looks most impressive. Truth to tell, the mechanical "goodness" or the engineering of a television aerial is more important than its "electrics.". The electrical specification allows wide tolerances, but the aerial must stay up under adverse weather conditions; must withstand corrosion in the places that matter, and must have a reasonably long life.



# "SUPER FIFTY WATT" AMPLIFIER 

This amplifier has a response of $30 \mathrm{c} / \mathrm{s}$. to $25,000 \mathrm{c} / \mathrm{s}$, within $\frac{1}{4} \mathrm{db}$, under 2 per cent distortion at 40 watts and 1 per cent at 15 watts, including noise and distortion of pre-amplifier and microphone transformer. Electronic mixing for microphone and gramophone of either high or low impedance with top and bass controls. Output for 15/250 ohms with generous voice coil feedback to minimise speaker distortion. New style easy access steel case gives recessed controls, making transport safe and easy. Exceedingly well ventilated for long life. Amplifier complete in steel case, with built-in 15 ohm mu-metal shielded microphone transformer, tropical finish.


# FOUR-WAY ELECTRONIC MIXER 

This unit has 4 built-in, balanced and screened microphone transformers, normally of 15-30 ohms impedance. It has 5 valves and selenium rectifier supplied by its own built-in screened power pack consumption, 20 watts.
Suitable for recording and dubbing, or large P.A. installations since it will drive up to six of our 50 watt amplifiers, whose base dimensions it matches. The standard model has an output impedance of 20,000 ohms or less, and any impedance
 can be supplied to order.

# in almost the time.. 

(1) In almost the time it this advertisement (almost a minute), more than a mile of copper wire has been wound into Parmeko Transformers.
 This may only prove in passing that even skilled technicians will go to great lengths to please. What does impress a surprising number of Manufacturers of Electronic and Electrical Equipment is the light compactness of Parmeko Transformers in doing a man-size job so efficiently. -

# PARMEKO of LEICESTER 

Makers of Transformers for the Electronic and Electrical Industries



Best known of all instruments for the testing and servicing of radio and television equipment is undoubtedly the Weston Model E. 772 Analyser, a first-class portable instrument with a sensitivity of 20,000 ohms per volt on all D.C. ranges and 1,000 ohms per volt on all A.C. ranges. The additional features of wide range coverage, robust construction and simplicity in operation contribute toward making the E. 772 ideal also for laboratory and research work. Full details of this instrument. and also of the Model S. 75 - a Test Set covering 53 ranges - will gladly be supplied on request.

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Enjoy the luxury of radio when you want it, in every room in your home. For a small outlay you can have extra listening in the lounge, bedroom, kitchen or even the garage, and switch the radio on or off from any of these points - a feature that is exclusive
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* Ask your local radio dealer to demonstrate, or write to us for leaflets.


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## MODERN PRACTICAL RADIO AND TELEVISION

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It is impossible to detail even briefly in this small space the exhaustive ground covered by this comprehensive work, but the pamphlet we can send you will show you that these few remarks are no exaggeration.

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[^12]> "POINT ONE"' TL/12 12 WAT'i TRIPLE LOOP FEEDBACK AMPLIFIER PRICE : 27 GUINEAS

Craftsmanship is apparent on inspection. Performance is certified by the N.P.L.
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1 mfd .250 v
1 mfd. 450 v ..
2 mfd .350 v.
$2 \mathrm{mfd} 450 \mathrm{~V} ..$.
4 mid. 350 v .
4 mfd .450 v .
8 mid .150 v .
mid. 350
8 mfd .450 v
8 mfd. $500 \mathrm{v} \ldots \ldots \ldots \ldots . .$.
fixing.........................
8 mid. 600 v. centre-screw
fixing
16 mfd .350 v .
16 mid. $450 \vee$.
16 mfd. 500 v .
16 mfd. 700 v.
32 mfd .150 v
32 mfd .250 v .
32 mid. 350 v
$8 \mathrm{mfd} . \times 8 \mathrm{mfd} .350 \mathrm{v}$
$8 \mathrm{mfd} . \times 8 \mathrm{mfd} .450 \mathrm{v}$.
$8 \mathrm{mfd} . \times 8 \mathrm{mfd} .500 \mathrm{v}$.
8 mid. $\times 8 \mathrm{mfd} 500 V.$.
$8 \mathrm{mfd} . \times 16 \mathrm{mfd} .450 \mathrm{v}$
$8 \mathrm{mfd} . \times 16 \mathrm{mfd} .500 \mathrm{v}$.
$16 \mathrm{mfd} . \times 16 \mathrm{mfd} .450 \mathrm{v}$.
$16 \mathrm{mfd} . \times 16 \mathrm{mfd} .500 \mathrm{v}$
$20 \mathrm{mfd} \times 20 \mathrm{mfd} .200 \mathrm{v}$.
$24 \mathrm{mfd} . \times 24 \mathrm{mfd} .200 \mathrm{v} \ldots$.
25 mfd.
$\times 25 \mathrm{mfd}$.
200
$\mathrm{v} . .$.
$32 \mathrm{mfd} . \times 32 \mathrm{mfd} .150 \mathrm{v}$.
$32 \mathrm{mfd} \times 32 \mathrm{mfd} .450 \mathrm{v}$.
$100 \mathrm{mfd} . \times 100 \mathrm{mfd} .150 \mathrm{v} .$.
10 mfd .25 v.
12 mfd .50 v
20 mfd. 50 v .
25 mfd .2
25 mid .
50 mfd .50 v ...
250 mfd . 12 v .
250 mfd .25 v
250 mid. 25 v.......................
mfd. $\times 8 \mathrm{mfd} . \times 8 \mathrm{mfd}$.
3/9


Type 1, Bra
Type 1, for B7G button base. Type 2, for B9A noval base. Price 1/4 each, discounts for quantities.


## MICRO SWIT CHES

The three types illustrated are in stock. Leaf type, 3/6. Rubber plunger type, 3/3. Ball type, 3/-. Also Ultra small American type No. CR107/DC103, price 4/6. Other types may be available from time to time.


## GUESS WHAT FOR $£ 5$

The valve illustrated in our September "Guess What" Competition was an EF50 with the metal case removed. Prizes were sent to the readers whose solutions were the first three correct ones opened. The names of.the winners were posted in both our branches early in October.
This month's "Guess What" we think is a little harder, we invite you to tell us the name of the object illustrated. By way of a clue please note that we describe this item for sale somewhere in these four pages. Also please note the object is on show at our Fleet Street branch. We offer prizes of $£ 5$ to the first, $£ 3$ to the second, and $£ 2$ to the third correct answers opened.
There is no need to rush your answer to us, you can send it in when you next order from us. You have until first post on the 24th.

## ALL MAINS CHASSIS



This is the equivalent of a 4 -valve receiver for it uses three valves and a metal rectifier. It is all wired up ready to work of A.C. mains, complete with modern valves, ganged tuning, high precision dust-cored coil, first grade condensers and resistors, all on metal chassis. Tunes long and medium wavebands. Large clear dial. Receives home services; light programme Luxemburg etc. Chassis size approximately 9 in. $\times 4$ in. $\times 5$ in. Complete with valves, but less speaker, 69,6. Suitable speaker with matching transformer, 16/6nothing else needed. Postage and packing $2 / 6$ extra.

## 10,000, B.V.A. VALVES AT PRE-BUDGET PRICES


uon and have not been tested. Price is only $\mathrm{f6/19/6}$. If you cannot call to collect please include an additional $10 /-$ to cover cost of transit case and carriage. This is partly returnable to you if and when you return the transit case.


## MULTI-SPEED MOTORS

You can adjust this motor to almost any speed you want, it will work directly off A.C. mains, or if you require greater power or greater speed work it through a meta rectifier. This motor is fitted with a gear box enabling speeds down as low as 1 r.p.m. to be obtained. Prlce $14 / 6$, postage and packing $1 / 6$ extra.

## THIS MONTH'S SNIP

2 gin. Cathode Ray Tube, made by G.E.C. for the Government, No. CV964, ideal for scopes, miniature T.V., etc. This is an electrostatic tube, with standard base and green fluorescence. The sensitivity is X. 097 $\mathrm{m} . \mathrm{m} . \mathrm{v}$, and $\mathrm{Y} .13 \mathrm{~m} . \mathrm{m} . \mathrm{v}$. and filament voltage is 4 v . Wiring data supplied-limited quantity, 17/6 each.

BOOKS AND PUBLICATIONS

" DEMOBBED VALVES."Gives the commercial equivalents of many the commends of service valves, and conversely gives the service equivalent of many thousands of commercial type valves, an invaluable publication recently revised. Price 2/3. "AN ELECTRONIC TIMER." Shows how to build a device for controlling timed operations. The timer can be set to any timing up to 3 minutes. Price 2/3. THE ELECTRONIC SWITCH." Shows how to make a device for switching without mechanical contact. Price $2 / 3$. mechanical contact. Price $2 / 3$; Explains the working of an ingenious relay and gives several circuits including radio control. Price $1 / 9$ 3)-WATT ., CONVERTIBLE AMPLIFIER.". Shows how to construct a 3 -stage amplifier with an output of $3 \frac{1}{2}$ watts, a unique feature is that this amplifier fits into our "Occasional" cabinet. Price 1/6. "THE I.F. AMPLIFIER." Gives details of a $465 \mathrm{kc} / \mathrm{s}$. amplifier with A.V.C. detector and power output stage. Designed to fit into our "Occasional" cabinet, it is useful for aligning coil packs and for use as a signal tracer ardio servicing etc Price $1 / 6$ in radio ser THE, OCCASIONAL T.R.F. Shows how to build, a T.R.F. Receiver for medium and long wave reception, of looks and quality output comparable with sets priced between $£ 10$ and $£ 14$. This costs less than $£ 6$ to build including cabinet. Price ${ }^{1,6}$, "THE OCCASIONAL SUP. ERHET." "In areas where field strength is low and interference is high, a superhet receiver is essential. For less than $£ 8$ one can be buile into our "Occasional" cabinet. This publication gives all details. Price 1/6. "VAilve EQUIVALENTS." These are the best equivalents charts available today. Also the booklet can be used for keeping records of valve stocks. Price 2/6. "1.F. ALIGNMENT PEAKS." This book gives the I.F. frequencies of more than 4,700 receivers, British, more than 4,700 receivers, british, very popular British set is covered, very popular British set is covered,
and hints on finding the frequencies of unknown British sets are also given. Price 4/6. FOUR INTER ESTING LEAFLETS' (1) The Infra-Red Cell; (2) A millibar barometer from a sensitive altimeter; (3) A.V.F.O. from unit type TU5B; (4) The circuit for light-operated relay. These are free with all orders for publications this month.

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$150 \mathrm{~mA}, 350-0-350$ v. 6.3 v. at 4 amps, centre tapped, 5 v. at 3 amps, fully shrouded upright mounting. Price $32 / 6$.
$80 \mathrm{~mA}, 350-0-350 \mathrm{v} .6 .3 \mathrm{v}$. at 4 amps, 4 . at 3 amps, half shrouded drop through. Price 18/6.
$80 \mathrm{~mA}, 320-0-320 \mathrm{v} .6 .3 \mathrm{v}$. at 4 amps, 5 v . at 3 amps , half shrouded drop through. Price 19/6.

$70 \mathrm{~mA}^{2}$ 230-0-230 v. 6.3 v .at 3 amps , 5 v . at 2 amps , fully shrouded ing. Price 22/6.
$60 \mathrm{~mA} \quad 260-0-260$ v. 6.3 v. at 3 amps, 4 v. at 2 shrouded $d^{r}$ op through. Price 16/6.
$60 \mathrm{~mA}, 260-0-260 \mathrm{v}$. 4 v. at 4 amps 4 v at 2 amps Price 16/6. $40 \mathrm{~mA}, 250-0-250 \mathrm{v} .6 .3 \mathrm{v}$. at 4 amps Price 12/6.

## FILAMENT TRANSFORMERS

6.3 v . at 1.5 amps , standard type for receivers. Price 6/6.
2 v. at 2.5 amps , highly insulated for television. Price 7/6.

## STAND-BY BATTERY SET

Made originally for the Government for use in canteens, ctc., this 4 valve medium wave-band superhet uses 2 v . Mazda valves, and is het uses 2 v. Mazd. Palv. Speaker and usual controls. A good set and usual controls. that you can carry on listening to a programme despite a power cut. Unused but storage soiled, $\{4 / 5 /-$, carriage 5/- extra.

## COMPRESSED FIBRE BOARD

This fin. thick board is easier to work with than plywood, and is an ideal material for emergency cabinets or for permanent speaker baffles, trays, bases, backs and for sound and heat insulation.
5 ft . $11 \mathrm{in} . \times 2 \mathrm{ft} .11 \mathrm{in}$., callers only. Price 9/6.
$2 \mathrm{ft} . \times 2 \mathrm{ft} ., 3 / 6 ; 2 \mathrm{ft} . \times 1 \mathrm{ft} ., 2 /-$; ift. $\times$ ift., $1 / 3$.


## INDICATOR

 LAMPSComplete as illustrated. Price 1/6.

EXCELLENT CHRISTMAS PRESENT FOR MOTHER OR MARRIED SISTER.
The "Lectross" electric clothes drier/ convector room heater is a device which can be a heater all the week and a clothes drier on washing days. It will make life casier in any home but is an extra boon to those who live in flats or have to do their washing in the evening.
We have sold a lot of these and all purchasers have been delighted. In fact they find it difficult to believe we can sell such a good heater at such a low price. We could not, but for the fact that the "Lectross" manufacturer's we re forced into bankruptcy by the combination of a cancelled export order, and 100 per cent. Purchase Tax, which almost doubled the original price of 12 guineas, and so reduced home
sales to almost nil. We bought all the driers from the liquidators, and we are able to offer them to you at $£ 5 / 19 / 6$, which is less than one half of the original retail price, and only one quarter of what the price would be if they could be made to-day. We have not many more of these left, so be advised and order promptly. We also bought all the spare parts, so you need have no fears about repairs, in fact we guarantec always to be able to supply spares.
The size of the "Lectross" is 3 ft . wide, 3 ft , high $\times 5$ in. deep, it works off A.C. or D.C. mains consuming 750 watts, i.e., just less than one Unit.
The clothes which are hung over four chrome-plated rails are dried by the steady stream of hot air which comes from the bottom heater chamber.
If unable to collect please add $7 / 6$ for carriage and packing, and also state your mains voltage.

## GIVE A RADIO YOU HAVE

 MADE.You will find that the building of our all mains radio receivers is simplicity itself, and the more you make the less time each takes, everything down to the last nut and bolt is supplied and everything fits together in a professional manner.
finished the receiver looks and plays as well as those being offered in radio shops at anything between $£ 10$ and £14. So why not give one as a present to
someone dear to you this Christmas.


The one illustrated above we call our "Occasional T.R.F." in a choice of colours, Ivory, Walnut or Green, and costs just less than $\mathrm{f6}$ to make. The one below we call "The White Lady," this is an extra fine cabinet of pure white. The complete receiver costs about £6/5/- to build. Constructional data for either set is available at $1 / 6$ post free.


## ELECTRIC HEATERS

 Heavy cast framework totally encloses the elements, so these are 100 per cent. safe even in confined spaces, just right for your radio den garage, office, shop, etc.900 watt (heavy) model, $23 / 6$, plus $5 / 6$ carriage. Other models available are 750 watt, 500 watt, 250 watt, all these are $23 / 6$ each, plus $5 / 6$ each carriage. The 250 -wat model used as a foot-warmer keeps legs and body warm for less than a farthing per hour.


Orders by post are dealt with by our Ruislip depot. To avoid delay address to:- E.P.E. Ltd., Dept. 2, Windmill Hill, Ruislip, Mddx.


TERMINAL BLOCKS
Heavy duty type, 5 way 4 in. long $x$ lin. wide $x$ lgin. high. 30 gmp lin. wide $x$ ligin.
Heavy Duty type, 6 way porcelain 15 amp . rating. Price 1/6.
Heavy Duty type, 5 way porcelain 15 amp . rating. Price $1 / 3$.
Heavy Duty type, 3 way porcelain 15 amp. rating. Price 9 d .

SPECIAL COIL UNIT.
For use with American Receive: BC/AR/229, this coil unit C380 is in aluminium can, new and unused. 45/- each.

## PYE PLUG AND 6d. each SOCKET.

toin. ENERGISED SPEAKER. The resistance of field is 1100 ohms and the construction of the speaker is such that really good response must result. The ideal speaker for a quality amplifier or receiver. Limited quantity. Price $17 / 6$ each. postage and packing $2 / 6$ extra.


| 3tin. | 11 |
| :---: | :---: |
| 5 in. | 12 |
| $6 \frac{1}{2} \mathrm{in}$. | 12 |
| 8 in. | 14 |
| 10 in . | 25 |

as available.


Add $1 /-$ per speaker for packing and insurance.

## CATHODE RAY TUBES

Note-All these rubes have green Note-All
5 CP 1.5 in . electrostatic. American manufacture-medium persistence manufacture-medium persistence
suitable for T.V. or scope, in original cartons, 19/6 carriage and insurance $2 / 6$.
VCR517 6in. electrostatic, medium persistence, suitable for T.V. or 'scope work-unused, ex-new equipment, 22/6, carriage and insurance $\sqrt{5}$
VCR97. We have had a new delivery of this now famou: electrostatic 6in. T.V. tube, these are not the cut off type, they give a full picture, 42/6 carriage and insurance 5/-.
VCRS16 9in. magnetic tube, long persistence which makes it rather unsuitable for T.V. Price £2/10/postage and insurance $10 /$-. CV961. 7in. electrostatic, shor: persistence, suitable for T.V. persistence, suitable ror $2 / 6$.

## STOP PRESS. <br> CANCELLED EXPORT SHIPMENT.

We have acquired some ot consignment of the 5 -valve Superhet Receivers chassis, these use only first-class components and are all wired up ready to operate, complete with valves and 8 in . speaker.
They cover the long, medium and short wave bands and have gram input. Brand new and in perfect condition, limited quantity $\mathrm{Elo/10/}$, plus 5/carriage and packing.

Orders under $£ 2$ add $2 / 6$, under $£ 1$ add $1 / 9$. Postable items can be sent C.O.D., additional charge approx. 2/6. Lisr $6 d$. Early closing days: Wednesday, Ruislip; Saturday, City.

## ELPREQ

EX-GOVERNMENT UNITS


10 VALVE $1 \frac{1}{2}$-METRE SUPERHET.
Ideal for conversion into a Midlands or London region Televisor. lands or London region Televisor. These contain 6 valves type 2SP61,
and one each RL7, RL16, and EA50. and one each RL7, RLI6, and EA50.
Six I.F. Trans formers of $12 \mathrm{Mc} / \mathrm{s}$, $4 \mathrm{Mc} / \mathrm{s}$ band width, and hundreds of other useful components. Price 59/6, plus carriage and packing $5 /-$. These receivers are unused and in original wrappings.

## RECEIVER 3457

These cost over $£ 100$ each to build, they contain 15 valves type EF50 and one each of VR56, VR55, VR92, and 2 of types VR116 and VR54. These contain a host of vah:able pot' meters, motors, relays, gear box, and components of all descriptions, and in addition they contain the famous "Pye" $45 \mathrm{Mc} / \mathrm{s}$ television strip. Brand new in transit boxes. Price $\$ 5 / 19 / 6$.

## RECEIVER TYPE 21

Battery operated superhet covering 4.2 to $7.5 \mathrm{Mc} / \mathrm{s}$ and 19 to $31 \mathrm{Mc} / \mathrm{s}$., on 10 metre band, this operates as a double superhet. In brand new condition, complete with 9 valves and circuit diagram. Price $\$ 2 / 5 /-$ plus $7 / 6$ carriage. insurance and packing.

## POWER PACK TYPE 392.

This is an extremely useful unit which works off A.C. without modification giving an output of 700 v. D.C. adequately smoothed. Here is a list of the components contained in the power unit : Mains Transformer for 200-250 v. 50 cycle, with secondaries of $700-0$ 700 v , at $70 \mathrm{~mA}, 4 \mathrm{v}$. at 2.5 amps., 12.5 v . at 1 amp. (Note these are Admiralty ratings, the transformers will stand at least twice these figures). Also 2 rectifier valves, type CV54, 10-watt resistors, three 4 mfd .700 v . condensers, L.F. choke, 10 henry 100 mA ., 2 slydlok fuses. The power pack 2 slydiok fuses. The power pack is unused and is contained in a $\times 8 \frac{1}{2}$ in. Price $67 / 6$.
in. Price $67 / 6$
RECEIVER TYPE 78.
This covers the wave band 2.4 to $13 \mathrm{Mc} / \mathrm{s}$ and it is also fitted with a $1.000 \mathrm{kc} / \mathrm{s}$ crystal with an internal arrangement whercby its oscillator can be accurately checked with the crystal, the sets are complete with 5 valves, and they are brand new. and unused. Size is $6 t i n . x 88 i n$. $\times 10 \mathrm{in}$. approx. Price $84 / 10 / \mathrm{F}$, plus $7 / 6$ carriage, etc.

AMERICAN TYPE 6
INDICATOR.
This indicator known as A.S.B. uses the same circuit and the same equivalent parts as our famous Type 6. For instance, it uses tube type 5BPI which is the American equivalent of the VCR.97, it uses valves type 6AC7 which are the American equivalents of the the American equivalents of the full of very useful components. This unit can be made into an This unit can be made into an excellent scope and the "Wireless
World" data (avallable price 9 d .) will be an excellent gulde. Price for the indicator unit is $84 / 10 /=$, carriage 10/-extra.

## WHY PAY HIGH PRICES FOR COIL PACKS?



If you use our parts these literally fall together and our publication " Making Coil Packs" (Price 1/6) describes a simple method of alignment without using a signal generator and also gives circuits of typical receivers complete with gram arrangements.


PRICE LISTS OF PARTS
Set of 6 coils covering the three standard long, medium and short wavebands, $9 / 6$; Punched metal chassis, $1 / 9$; 6 Bank Trimmer assembly, $3 /-$; Midget wavechange switch, 4/-; Tag, panel condensers and other sundries to complete L.M.S. Coil Pack, 1/9.
When completed vour Elpreq coil pack will look like this

## VISUAL ALIGNMENT SIGNAL.

## GENERATOR.

An interesting article in the Octobe: Radio Constructor described an instrument which is a combination oscilloscope and signal generator. It is designed to generate a signal into a superhet then permit visual inspection of same signal after passing through the superhet. The article further shows how the instrument could be made for the very low price of $£ 5$.
This uses a small tube and is quite a compact instrument, so if its only use is that of checking the band pass on the I.F. transformers, in a high fidelity receiver, its construction is justified. It can, of course, be used for a variety of different jobs other than the alignment of I.F's, in fact, it is a good servicing 'scope.
We can supply a complete kit of parts for $\mathbf{E} 5$ containing valves, tube and all components except chassis and case. A re-print of the article from the Radio Constructor is available price 9 d .
The power pack not shown on the block diagram is, nevertheless, included in the kit.

## IF/AF AMPLIFIER AND SIGNAL TRACER.

During servicing, from time to time you come up against sets with intermittent and obscure faults. Faults which with standard instruments are most difficult to trace and which usually are real time wasters. The most successful method of tackling these faults is by substituting a receiver known to be good, replacing the old set stage by stage until the faulty seetion is located. Obscure faults are of ten multiple faults and with these substitution is the only reliable method.
Our IF/AF Amplifier will permit you to fault trace by this method and in addition you can use it to align and calibrate receivers and coil packs, which have just been built or repaired.
The Amplifier is extremely useful in the laboratory, for instance to check the performance of valves or other components by noting the check the performance of valves or other components by noting the output for a given input, and when experimenting with
Finally our IF/AF Amplifier and Signal Tracer can be used as a temporary power pack to provide H.T. and L.T. or can be quickly hooked up as an emergency receiver, gramophone amplifier, etc. Kits for three models are available, all are complete with valves. I.F. transformers, mains equipment, etc., they are in fact superhet receivers which only need an R.F. stage to complete them. And for the convenience of the user, room is left on the chassis and holes are drilled to accommodate the R.F. stage on other components under test.

## Three models are available:

## IF/AF DE LUXE.

This uses a standard type mains tranformer with full wave rectification and permits isolation from the mains. This is a complete kit with valves but less speaker. Price $\mathbf{£ 6 / 1 0 / -}$ with diagram, etc., carriage and packing 5/- extra.

## IF/AF UNIVERSAL.

This is on a smaller chassis and uses series working valves and is suitable for A.C. or D.C. mains. Price 86/5/- or with cabinet \&7, post and insurance 2/6 extra.

## IF/AF MODEL F.T.

This low price A.C. only model uses a filament transformer and half wave rectification. Price $£ 5 / 15 /-$ or with pakelite cabinet $£ 6 / 10 /-$, postage and insurance $2 / 6$ extra.

EX-GOVERNMENT UNTTS


Frequency Meters BC. 221
American manufacture. Accuracy .005 per cent. Frequency range $125 \mathrm{kc} / \mathrm{s}-20 \mathrm{Mc} / \mathrm{s}$.
Crystal controlled and temperature compensated. Makes an excellent V.F.O. without impairing its use as a frequency meter. Brand new and unused, complete with instruction book, $£ 35$, carriage paid. We have also a limited quantity of used BC. 221 Frequency Meters, carriage paid $£ 15$, and some without data charts, £10, spare crystals 35/- each.

## BATTERY CHARGER 21

This is an excellent unit fitted with heavy duty mains transformer and metal rectifiers. Its output is $160-200 \mathrm{v}$. at $t \mathrm{amp}$, so it is ideal for charging wet H.T. batteries. It can, of course, be used for charging L.T. batteries, in fact it will charge 70 cells simultaneously or any number up to this. In addition to charging cells, this unit can also be used to work D.C. appliances off A.C. mains, or if its output is fed into a resistance network then you can have a source of D.C. for experimenting. The charger works off standard $200-250$ charger works of standard 200-250
mains, and is contained in a neat mains, and is contained in a neat
perforated case, price $22 / 6$ plus perforated case, price 22/6 plus 3/6 carriage.

## D.C. TRANSFORMERS

Technicians will, of course, say that this is not a correct description, but it is a very useful way of describing a device which reduces D.C. mains to a voltage suitable for working toy trains, etc. These are really rotary transformers but when driven off the mains they give our 12 volts al 2 amp. Another good polly enclosed so that they can be kept away from tiny fingers. Also they can be used as motors Also they can be used as motors
for driving models or to given H.T. for driving models or to given H.T.
from car batteries. Price only from cat batteries. Pric
$5 / 6$ each plus $2 / 6$ postage.

## RECEIVER R. 1124.

This receiver contains a host of useful stuff, the most important of which is a coil pack which needs only the adjustment of its trimmers to receive AP. sound. It also contains Westectors, resistors switches and all the parts which make up a six valve superhet. The valves six vaive supernet. The valves one each of $8 \mathrm{D} 2,4 \mathrm{D} 1$ and 15 D 2 . We understand that these receivers We understand that these receivers
have never been used. Price only have never been used. P
$18 / 6$ each plus $2 / 6$ postage.

## RECEIVER 25/73

Add the Elpreq Coil Pack as described to this receiver and you have a really fine superhet, contains 6 valves, $465 \mathrm{ke} / \mathrm{s}$ I.F. 'transformer, etc. Price 24/6, data if required.

## HGH VOLTAGE

 RECTIFIERSBeing Ministry surplus these are available at really silly prices, This is your opportunity to experiment with that special plant you intended to make.
Type CV19, 63,000 v., max. 800 ma. čiso4 60 ..... $£ 4170$ Type CV1504, 60,000 v., max. 1,200 ma.,........ £5 $17 \underset{0}{0}$
ma.
Type
B51111,
14,000
v..
max
350 ma .
Type CV1120, 14,000 v. max.
Type $\mathrm{CV} 1508,8,000$ v., $\max ^{3}$.
Type $1,000 \mathrm{~m}$ a.............., $17{ }_{6}$
Type CV54, 7,000 v., max. 400
3 a .

## KI YSTRONS

Type No. 723AB, Type No. 714AB, Type No. CV129, $£ 3$ each. Other types may be available in smaller quantities. Send details of your special requirements
\&3OLOMETER 14 M.W. 10E 756 Used in connection with measurement of radio, infra red, etc., hermetically sealed in glass fube size 2 kin. long, Price $35 /-$ GAMMATRON
Triode transmitter type 54, 250 watts R.F. output, flaments 5 v at 5 amps. Price $£ 1 / 15,0$ each.

## INFORMATION WANTED Can any reader oblige us with information on Special Purpose Tube type CV271.

GERMANIUM DIODE Made by G.E.C. or B.T.H.. new and perfect. Price $4 / 6$ each.


TUNGAR VALVE RECTIFIERS Replacement for many home and industrial chargers :1 amp. type 68502. Price 9/6 $3 \frac{1}{2}$ amp. type 68507. Price 12.6.

## MERCURY VAPOUR

 RECTIFIERSCV2946-max. current 1.8 amps . max. $1,000 \mathrm{v}$. Price VU39-max. current 2.5 amps. BD10-2,00 V. Price... 25 BD10-max. current
max. 1,000 v. Price... $£ 6$ amps 10
A.C. MAINS OPERATED S-VALVE SUPERHET CHASSIS Completely wired, aligned and ready for immediate operation, covering threc wavebands, 13-37 metres, 57-100 metres and 200-500 metres. A realiy excellent receiver ideal for new installations or as a replacement chassis in existing radiograms, etc. The set employs a 5-valve line up either international octal valves 6 K 8 , $6 \mathrm{~K} 7.6 \mathrm{O} 7,6 \mathrm{~V} 6$ and 5 Y 3 or " E " types ECH 35 , EF36, EBC 33 EL33 and 5 Y3 or $5 \mathrm{Z4}$. The overall size is 81
 in. deep $x+11 \mathrm{im}$. Wide $\times$

Note these points:-
(1) Coil assembly can be removed as one unit.
(2) Wave-band indicator shows through glass scale.
(3) 4 watts output will work 10 in . or 12 in . speaker.
(4) Negative feedback and tone control.
(5) Flywheel tuning and large clear dial
(6) Dust cored coils and I.F. transformers.
(7) Sockets for pick-ups and extension speaker.

Only first-class parts have been used, e.g., mains transformer by "Parmeko," resistors by "Erie," "Welwyn" and "Morgan," fised condensers oy "Hunts" and "U.I.C.," trimmers and tuning condensers by "Wingrove Rogers," etc., etc.
Complete chassis less valves, $£ 9 / 10 / 0$.
Complete chassis with valves, $£ 11 / 10 / 0$
Complete chassis with valves and 10 in. speaker, $£ 12 / 10 / 6$.
If not collecting add 5/- carriage and insurance. Circuit diagram supplied free with chassis or separately price, $1 / 6$.

## VALVES

We believe that we carry larger stocks than any other firm in Middlesex; in consequence we can offer most types of Receiving valves at pre-budget prices, which means a considerable saving of purchase tax. Our stocks are much too assorted to list in these pages, and, as prices are controlled, we suggest you order your valve requirements by C.O.D. or send what you think will cover the order; we will refund any extras.
We have never specialised in Transmitting types, but naturally we stock a few of these, and in most cases, being war surplus, we can give you a considerable reduction on manufacturer's prices For instance, the one illustrated is a 250 -watt Transmitting tetrode, heater rating 12 v. 8 amps .; it measures $14 \frac{1}{2} \mathrm{in}$. long and $6 \frac{1}{2} \mathrm{in}$. across the bulb. It would cost anything up to $£ 20$ from the manufacturer, but we have a limited number to offer at $18 / 6$ each
Among other Transmitting types we can offer at low prices are :-
805 at 27/6, 807 at 12/6, PT15 at $27 / 6,1625$ at $12 / 6,813$ at $110 /=, 6 \mathrm{~J} 6$ at $13 / 6$, ML6 at $10 / 6$, 866 A at $18 / 6$, TZ40 at $47 / 6,860$ at $19 / 6,872$ at $47 / 6$.


## 10,000 B.V.A. VALVES AT PRE-BUDGET PRICES

## EXCELLENT XMAS PRESENTS



Novelty radio in coloured plastic cabinet only 6 in . high, ideal for a nursery or bedroom, complete with built-in moving coil speaker, 2 -gang tuning condenser, volume control and ON/OFF switch, all wired up ready to operate as soon as valves are fitted. Works off dry batteries. Valves required are three of type $1 T 4$ and one of $3 S 4$. Because of a frustrated export order, we are able to offer these sets brand new and perfect, complete except for valves, at the remarkable price of $49 / 6$ each, postage and insurance $2 / 6$ extra. Don't delay-send your order to-day.

Orders by post are dealt with by our Ruislip depot. To avoid delay address to:-E. P. E. Ltd., Dept. 2, Windmill Hill, Ruislip, Middx.

## SPECIAL PURPOSE TOGGLE

 SWITCHThis is a two " on "position switch. the first only stays on when helddown, the other stays on permanently. The two positions can be used independently, for instance to control one bright lamp and one dim lamp. American made. Price $2 / 6$ each.


EPICYCLIC DRIVES
Double drive with wheel for driving pointer, 8.1 ratio. Price 3:9. Single drive. Price $2 / 9$.

## FEED-THROUGFI INSULATOR

Ceramic with 2 B.A. rod and terminals. Price $1 / 9$ each.
1.F. TRANSFORMERS
$465 \mathrm{kc} / \mathrm{s}$ iron dust cores fitted in aluminium can size $1 \frac{1}{2} \mathrm{in}$. $x$ 1 tin. $\times 3$ din. Price $12 / 6$ pair.
$12 / 6$ pair.
Midget type, $465 \mathrm{kc} / \mathrm{s}$

${ }_{3}^{3} 1 \mathrm{in}$. (M400B). Price
$17 / 6$ pair. $465 \mathrm{kc} / \mathrm{s}$
ex-equipment in good condition fitted in standard size can, dust cored Price $7 / 6$ pair.

## $\xrightarrow{C-2}$ <br> METAL DIVIDERS

Really well made for Government workshops. Ideal for marking out workshops. deal for markin
on metal chassis. Price $3 / 6$.


## METER BARGANS

This is a $2 \frac{1}{2} \mathrm{in}$. moving coil meter. made up as a 1 -amp. R.F. meter, made up as a 1 -amp. R.F meter, thermo-coupled. With the thermocouple removed it will make excellent voltmeter or multi-range meter,
Sensitivity of the movement is Sensitivity of th
3 ma . Price $8 / 6$.
3 ma . Price 2 in . flush mounting,
$0-1 \mathrm{ma}$. moving coil. Price 15/-0-9 amp. A.C. or D.C. 2 tin flush mounting. Price $12 / 6$.
P.P INPUT TRANSFORMER Small size-pushpull, fully shrouded, $5 / 6$ each. Push - pull output transformers to match. 6/6 each.

## NEON LAMP

Earth leakage indicator, , etc. As used in "Viewmaster." Price 2/3.

Orders under $£ 2$ add $2 / 6$,under $£ 1$ add $1 / 9$. Postable items can be sent C.O.D., addit.onal charge approx. 2/6. List 6 d. Early closing days: Wednesday, Ruislip; Saturday, City.

152-153 FLEET STREET, E.C.4. Phone: CENTRAL 2833


# FIRST AGAIN! another greht scoop AN ALL WAVE RECEIVER AT HALF PRICE 

NOT A Kit, BUT A FACTORY BUILT JOB. FULLY ASSEMBLED, ALIGNED AND TESTED.

Made by a well-known manufacturer. 5 valve superhet, 3 wavebands, long, medium and short. For A.C. mains, 200-250 volts.

## HIGHEST QUALITY COMPONENTS USED THROUGHOUT.



Size of chassis: $-15 \frac{1}{2}^{\prime \prime}$ wide, $8^{\prime \prime}$ deep, $2 \frac{1}{4}^{\prime \prime}$ high.

## ABREND NEW FUEL SEZE REDIO

## LOOK AT THESE FEATURES

$\star 5$ New Brimar valves $\star 8^{\prime \prime}$ Elac closed field speaker $\star$ Yariable tone control $\star$ Large edgelit dial, $7 \frac{1}{2}$ " square $\star 2$-speed tuning with nylon drive $\star 4$ watts output $\star$ Sockets for p.u. and extension speaker $\star 465 \mathrm{Kc} / \mathrm{s}$ I.F. $\star$ A.V.C. $\star$ Circuit diagrams



$$
\begin{aligned}
& \text { SPECIAL REDUCED PRICE IF } 25 \text { /- } \\
& \text { PURCHASED WITH RECEIVER }
\end{aligned}
$$

Carriage, packing and insurance $10 /-$ extra.

If you need further details, please write. Circuit diagrams supplied for $1 / 6$.
Better still call and hear it yourself.

## LASKY'S RADID

## 37 TARIROW LBOAD, PADDINGTON, LONDDN, W. 9

## SAFETY FIRST

Fused test prods. Fully insulated pencil type with retractable point. Contact it only made when desired by pressing OD. Each prod contaius a cartridge type fuse and spring PRICE $4 / 11$ per pair (one red, one black). Poal

## VIBRATOR PACKS

For une with the P.C.R. Philips Communications Receiver 2-volt input. Supplied complete with vibritor and meta LASKY'S PRICE

$$
\begin{aligned}
& \text { LASKY's PRICE } \\
& \text { Carriage }{ }^{\text {E- }- \text { xtra. }}
\end{aligned}
$$

39/6

## CAR BATTERIES

By DELCO-REMY. Ex-American Army. Absolutely | perfect, brand new and unused, in maker soriginal packing |
| :--- |
| No. 1, 6 -volt 140 A.H. approx. Bize: Tin. deep, 131 n | ide, 9 hin. high. PRICE gence hard rubber case.

Cask's Price
£4/19/6
No. 2. 6-volt 90 A.H. Size: 9 in . LASKY'S PRICE

87/6
T.V. SCAN COILS FOR LINE AND FRAME
Brand new, manufacturer's surplus, For 9in, or 12in C. B. tuber. LASKY'S. PRICE $14 / 6$

PoM. TELEVISION FOCUS MAGNETS Suitable for any type of cathode ray tube. Tctrode and Triode. LASKY'S PRICE
Postage N/-extra.
16/11

## SELENIUM METAL RECTIFIERS

12 volts 6 amps., $27 / 6$, post 9d.extra
12 volts 1 amp., 79 , post 9 d d. extra.
12 volts $\frac{1}{3}$ amp, $3 / 11$, post 6 d . extra.


800 Voltwat $5 \mathrm{M} / \mathrm{a}$. and 1,200 voits on pulse circuits. ManuLASKY's PRICE 9/- each.

## COIL PACKS

By Weymouth. No. 1. Standard long, medlum and shor Wave coverage. Simple single hole fixing. For use with Postage $1 / 6$ extra. No. 2. As above, but of minlature dimensions, as follows: $3 \mathrm{iln} . \times 1 \mathrm{k} \mathrm{ln}, \times 2 \mathrm{ln}$. Price $44 /-$
By Osmor. Type Q Packs. Superhet tor $465 \mathrm{Kc} / \mathrm{s}$ I.F.'s. Medium short, short pred and tested in actunl receivers trawier band. Price $45 / 10$. Postage $1 / 6$ extru. All coil pgeks are supplied with tuil eircuit.
ALL OTHER TYPES AVAILABLE.

## ANTENNA ROD SECTIONS

Each sectlon is steel heavily copper plated, 12in. long and tin. In diameter. Any number of sections can be itted ting in diameter. LASE'S PRICE $2 / 8$ rer doz.; gi/- for 3 doz.; 11/-per half gross; 20/-per gross. Post free.

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 91n. 7/8: 91 n . fitted with armour phate glass $10 / 6$ new white 196 ; Wh $21 /$ - Special lor fiat face tubes, $22 /-15 \mathrm{in}$. solled white ; new, perfect, 87/6. Postage 1 -extra on all mask
## FILAMENT TRANSFORMERS

$$
\text { All prlmarles } 230 \text { volts } 50 \text { c.p.s. }
$$ FIL/2, 6.3 v. 1.5 m

FIL/3, $6.3 \mathrm{v}, 3 \mathrm{a}$
Price $7 / 6$
Price 12/6 Special Tranolormer, 30 volts ait 2 amps, with Price $5 /-$ tappings: $-3,4,6,6,8,9,10,12,15,18,20,24$ and 30 volty all is trans A, Price 19/6

## MAINS TRANSFORMERS

All $200-250$ volts 30 c.p.s. primary. Finest quality, fulls
 Alaments tapped at 4 voits. An ideal replacement trans MBA/5. $\quad 350-0.350 \mathrm{v} .125 \mathrm{M} / \mathrm{a} ., 6.3 \mathrm{v} .4 \mathrm{a} ., 5 \mathrm{v} .3 \mathrm{a}$. With maine tapping board MBA/6. $350-0 \cdot 350 \mathrm{v} .100 \mathrm{M} / \mathrm{a}, 6.3 \mathrm{v} .3 \mathrm{a} ., 5 \mathrm{y}$ v. 2 a . With makinh tapping board. Price 22/6

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8 mld 500 v.
8 mild. 450 . $\mathrm{m} . \mathrm{w}$
$5 \times 8$ mid. 500
12 mfd. 50 V. 16 mid. 450 .
16 mid. $500 \mathrm{v}, \mathrm{w}$.
$16 \times 16$ mid. 450
$24 \mathrm{mfd}, 450 \mathrm{v}, \mathrm{v}$
$20 \times 40 \mathrm{mid} .350$
32 mid. $450 \mathrm{~s} . \mathrm{w}$.
32 mid. 500 v.w.
50 mid. $12 \nabla . w$.
$50 \mathrm{mfd} .50 \mathrm{v}, \mathrm{w}$
$50 \mathrm{mfd} .950 \mathrm{r} . \mathrm{w}$
$53 \mathrm{mld}, 350$ v.w. A.O.

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For optimum acoustic performance with any good 121n apeaker. Labyrinth construction, walnut veneered and 14ty. masinace. Dimenstons: 27in. wide, 37 tla . high, 1415. maximum depth. Supplled with filted speaker fret gold Anigh. Litted R1I/11/:

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& \text { Carriage } 12 / 6 \text { extra }
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£7/10/0
EX-A.M. RECEIVER TYPE R.D.F. 1 Contains 14 vaives: 2 VR66; $15 Z 4 G ;$ i VR137; 6 VR65; condensers, evc. Frequency is it metres, but can be cone verted to 2 -metre working. The unit it contalned in a grey metal case, size $11 \mathrm{in} \times 1 \mathrm{in} . \times 8 \mathrm{in}$. Weight 35 lb

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## TYPE J/RA/1. 30 watts. HEAVY DUTY AMPLIFIER

Rack mounting, grey crackle Anished. Uses KTZ63 and L63, feeding 2 KT6is in push-puil. Rectifier type US2. Meter and switch for checking ath current readings. Panei $\times 12 \mathrm{inht}$, LASKY'S PRICE
J/RA/2. 10-12 WATT CHASSIS AMPLIFIER
Oresan Ls 3 feeding 2 KT01sin push-pull. Rectifer type U50. Bize: bin xilin or ehassis.

LASKY'S PRICE
Send 3d. stamp for further details of J/RA/2 and J/BA/2 Amplifiers.
TABLE MICROPHONE STAND
rwo sections, chrome plated. Crackle fanished base.

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Miniature Pentode ( 184,384 )
Midget Pentode, $40 \mathrm{M} / \mathrm{B}$
Push-Full, $80 \mathrm{M} / \mathrm{a}$. Ratios of $40: 1$ and $40: 1$ Push-Pull for PX4's
$80 \mathrm{M} /$ a heary duty, multi-ratio.
10 Watt multi-ratio
$0 \mathrm{M} / \mathrm{a}$. Yulti-rstio
Bulginin intervalve transformers. Ratio: 4 : 1
Postage extra.

## SMOOTHING CHOKES

$20 \mathrm{M} / \mathrm{a} .40 \mathrm{H}$.
$40 \mathrm{M} / a .8 \mathrm{H}$.
${ }_{5} \mathrm{M} / \mathrm{a} .150 \mathrm{H}$.
$80 \mathrm{M} / \mathrm{s} .10 .20 \mathrm{H}$.
$120 \mathrm{M}, \mathrm{a}, 10-20 \mathrm{H}$.
$150 \mathrm{M} / \mathrm{a} .10-20 \mathrm{H}$
$250 \mathrm{Ma.10-20}$
$150 \mathrm{M} / \mathrm{3} \mathbf{~ H}$.
$250 \mathrm{M} / \mathrm{a} .5 \mathrm{H}$.

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## EX-A.M. COM MUNICATIO RECEIVER

BRAND NEW IN WOOD TRANSIT CASE. Aerial. lested before despath. Sup. Cireult: B.F.O., A.V.C. R.F. Amp., two I'F. stages, magic eye, etc. 5 frequency
 $500-200 \mathrm{kc} / 1 . ; 200-75 \mathrm{kc} / \mathrm{l}$.

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The tele riblon set you can bulld at home from athudard Alexandra Palace. Sutton Coldfeld and Holme moss operation.
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Table or Console Model. Incorporates all the latest developments. the home Television for the home
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## TELEVISION CONSOLE CABINETS <br> DE LUXE MODEL Beautiful Walnut Veneer

For 9, 10 or 12 in . cathode ray tubes. Beautiful figured medium walnut finish, with high polish. Fitted with shelf for receiver, glass, speaker baffle and fret, and castors for easy movement. Undrilled. Suitable for use with the "Vicwmaster", "Practical Television," "Practical Wireless," and "Wireless World" televisors

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Carriage $12 / 6$ extra.
Outside dimensions of cab inet: 17in. $\times 16$ in. $\times$ 32in. high.
Why not convert your table recelver to a console?


## BUILD A PROFESSIONAL RADIO OR AMPLIFIER at Less than half TODAY'S PRICE

A MAINS OR BATTERY PORTABLE KIT


Midget 4-valve Superhet Portable Set covering medium and long wavebands.
Denfaned to operate on A.O. madng 200/240 volte, or by an "Alldry" battery. The set is so deslgned, that the mains section is supplied as a separite unit whicu may be added at any time. The Kit therefore can be supplied (n) as an "Alldry" Battery Buperhet Personal Set, which can then be accommodated In the Attache Case as illustrated above (size $9 \frac{\mathrm{dm} . \times 4}{} \times 4 \mathrm{in}, \times 7 \mathrm{in}$ ). This is (b) or as a Combined Mains Battery Superbet Portable Recelver, for which a polished Wood Cabinet is available to accommodate both Mains Unit snd Batteries together. Circuit incorporaten delayed A.V.C. Bud Pre-selective Audio Feedback. Kit is complete in every detail and includes ready hound frame aerias, fuly algned ybled chassis 8 in. $\times 41 \mathrm{n} . \times 2$ in.
We can supply the set elther as a complete Kit of Parts for £8/16/9 (incl. P.T.), (plus Cubinet and Mains Unit), or by supplying the components separately. The complete Assembly knetructlons, which include full price details (including prices of individual components), Circuit and Component Layout, etc., are available for $1 / 8$ incl. postage.

A T.R.F. BATTERY "PERSONAL" KIT


A complete Kit of Parts to build as Midget 4 -valve A Battery Portable Set, covering medfum wavebrad.
Consists of Regenerative T.R.F. circuit, employing Fl:
Tuned Frame Aerial with Denco Iron Dust Cored Coil. Valre line up, two I.T.4's (B.F. Ampl, and Det.), 185 and 384 output.
Kit is complete in every respect and includes drilled chasmis, and latest type Rols 3in. P.M. apeaker. Overall size of sssembled chassis ain. $x 2$ fin. $X 2 i n$.

还 The Complete Assembly Instructions, inciuding individual component prices, Circuit and Component Layout, etc. is available for $1 /-$ incl. post.

## A KIT OF PARTS

Complete in every detail, to build a 3 -valve Amplifer for A.O.jD.C. mains $200 \cdot 250$ volts.
Has an output of 3 watts, and Incorporates a Tone Control. Valve line up, 25A6,657, U31.
Our price of $\Sigma 4 / 12 / 6$ for complete kit, Includes a matched 6fin. P.M. speaker
to


A MIDGET 4-STATION "PRE-SET" RECEIVER
A complete Kit to build a 4 -suation " Pre-Set " Buperhet Recelver for A.C. mains operation.
The set is desigued to receive any three stations on medium waveband and one on long waves, each station being recelved by the turn of Totary Switch-No
$t$ is of midget size, b
has the performance of a far more expensive ready made set, but can be bullt for half the price.


Price of complete Kit of Parts (including aligned I.F. Transf. rnd drilled chassis. etc.), 28/2/6 (hacl. P.T.), (blns Cabinet $25 / 6$ ), or the components can be purchased separately. The complete Assembly Instructions including Individual Component Price List, Circuit and Com ponent Layout. etc.. Is available for $1 / 9$.

STEBNS "RADIO TUNER MANUAL" Price 2/6. (Plus 3d, Post), Contains complete and detailed asembly Instructions showing how to make - 1 Valve T.R.F. Tuning Duit, covering Long snd A 1 Valve T.R.F.
A 4 Station "Pre-Set" Superhet Tuning Onit, producing 3 Etations on Medium Wavehand and 1 on Long Waves. A 2 Valve Suptrbet Tuning Onit, covering Short, Medium Each Tuner is for ramsand Practical Component Iapour otion. Circuit Diawith complete component Price Listu.

THE WIRELESS WORLD MIDGET A.C. MAINS 2-VALVE REGEIVER

## We can supply sll the components to build thia set. Including Valves and Moving Coll Bpeaker for $\mathbf{\text { including Deslgner'scomplete bullding instructions }}$ (thes inciadigg Designer scomple bulling instructions (these <br> THE "SUMMER ALLDRY" BATTERY PORTABLE

As published in June issuc of "Practical Wireless." We can supply, from stock, all the componeats to build this Midget 3 -valve Portable for £2'19/6 (less valves). This also Inciudes dials. top panel and aly. sheet for chasactical Tagout and Price List is available for 9 din

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Commocord "a.P:20," for standard reconds, f3:11/5; Interchangeable (G.P.19) Head for L.P. records, $\mathrm{f}^{1 / 3 / 4}$ type, for L.P. and Marconi, Standard, IIghtweight Magnetic, \&1/15/10 Marconi Matching Transformer, 7/6.
Goldring, Standard, Ughtweight, Magnetic, 29/6.

## ALL KITS INCLUDE "EASYTOFOLLOW" POINT-TO-POINT WIRING DIAGRAMS

THE WIRELESS WORLD 3-VALVE SET


A Midget 3-valve T.R.P. Receiver for operation on A. 0 mains, covering long and medium wavebands
mains, coverigg long and medium wavebands. Ye are able to aupply ail of the components to build this
set, as designed, bind specined in the Feb. 1950 issue Including the drilled chassia, valves, and moving colz speaker, etc., at the following prices -
o construot comple te chassis, less dial and drive ansembly, £4/17/9. Ditto including dial and drive assembly 2512.9.
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reprint of the designer sarticle, giving Circuitand Assembly nitructions (thla is available separately for 9d.), toge ther of above assemblies.

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All Kits incorporate Metal Rectifiers, and are for use on A.C. mains $220-250$ volts. All Kits idelude th easily For charging 6 . battery at 11 amps., $£ 12 / 8$.
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Designed for the Pre-melection of THREE STATIONS to suit local conditions. each station being received by the furn of a rolary switch. We are able to supply all com ponents including drilled chassis to bulld this new type in October issue, for $36 / 3$ (plus cost of selected coll reprint of the deatrner's article (availahle weparate'y for $9 \mathrm{~d}_{\mathrm{s}}$ ), together with a practlical component layout make the assembly very easy
$\star$ Send 6d. P.O. for our STOCK LIST, it shows "hundreds" of.Wireles When ordering please includ
STERN RADIO LTD., 109
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AN A.C. MAINS "ALL-WAVE SUPERHET" CHASSIS


A completely assembled chassis for A.C. mains $200 \cdot 250$ volts, designed for good selective and quality reproduction, and serves as an Ideal replacement chassis for that "old
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in any position on cabinet. The set employs a modern J-valve line up, and covers three
wavehands, $16-50,190.550$ and $800-2,000$ metres. Flywavehands, $16-30,190.550$ an
Overall slune of ussembled chassis, 131 in . $\times 6 \mathrm{in}, \times 811 \mathrm{n}$. high. Dlal mize 9 in.
Frice of comple technsslg, wired and ready for use £1419/6.


A Kit of Parts to build a 6-8-watt Push-Pull Amplifier for operation on A.O. mains $\mathbf{2 0 0}-\mathbf{2 5 0}$ volts.
Incorporates a simple arrangement
magnetic, crystal, or light-welght pick-up to be used A 10 watt Output Transformer is designed to match from 2 to 15 ohm speakers. Tone control is incorporated, The overall size of the assembled chassis is 10 in . $\times 8$ in. $\times 7 \mathrm{in}$. high. Price of kit, complete in every detail, including drilled c
layoutis supplled

## chassis, supplied ready for use, £7/10

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 ELIMINATORA complete kit of parts to build a Midget" Alldry " Battery Eliminator, giring approx. 69 velte and 1.4 volts. may 4 -vaive superhet Recelver requiring H.T. and L.T. moltage the above, or upprox. to 69 volts.


The kitis quite easily and quiekly assembled and is housed in a light aluminium case, size 4 lin. $x ~$
Price of complete kit, with easy to follow assembly inPrice of complete kit, with easy to follow assembiy in
structiom, 426 . In andition we ean offer a similar COMPLETL KIT to provide approx. 90 Volts and 1,4 Volts.
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TWO NEW DENCO ULTRA MIDGET SUPERHET COIL TURRETS Both having a Rotary Turret Action
(a) The C.T.8. Turret consists of 4 STATION "PRESET " UNIT, from which any three Btations on Medium Waveband and one on Long
a turn of the Turret 8witch.
(b) The O.T. 10 Turret being a 3 Waveband Coil Pack. incorporating $i$ fourth switch position procidiag for completely sultching out Radio when using gram. The meftes: Medlum Wares 190 to 570 Metres and short Waves 15 to 50 Metres.


The outatanding advantages these units have over other similar units can be readily sern, the matn features being (a) Nent and Compact, the overall size being only 24 in . dia. (b) Fitting is simpolicity itself, each Turret ha
fixing and requilring oniy four connections.
(c) The Rotary Turret design switches the sctual Colls, (c) The Rotary Turret design swituse incorporate variableiron dust cores, on to positive contacts, thereby reducing stray capacities to the absolute minimum.
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arangement of $465 \mathrm{kc} / \mathrm{s}$, and due to their unique dealgn arrangement of $465 \mathrm{kc} / \mathrm{s}$, and due to their unique dealgn Turret 30/8 Price C.T.9. Turret $39 / 8$, C.T. 10 Turret 5 :/sill necessary data is included with each Turret. These can be supplied separately for $8 d$.
THE FAMOUS W.B. "STENTORIAN" RANGE OF R.M

 $31 \mathrm{n} .14 / 6$ : $\sin .146 ; 61 \mathrm{ln} .15 / 6 ; 8 \mathrm{in} .16 / 9 ;$
196 N New Type Rols, 3in. $21 /-; 4 \mathrm{in} .22 / 6$. Output Transi.maget $5 \cdot$ matt Multrato, 12 tappings between 24 - 1 and $114-1$ (some C.T.), 8 6. Wharfedale, 12 watt, pumh-pull, multiratio. 25 -. P/pull, 20 watt, multi-ratio, 37/6, and many
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Ext. Speaker Volume Control,
$2^{\prime} 6$.
New Electrolytic Condensers. Not Ex-Govt. All 450/500

 Cardbaard Tubular, 4 mfd. 500 v. $3 / 6$; $8 \mathrm{mfd} .500 \mathrm{v} .4 / \mathrm{F}=$ 16 mfd .500 v. 5/9. Can. Standard size ati 500 volta, 4 mid. $3 / 6,8$ mfd. $4 / 3 ; 8-8 \mathrm{mfd} .5^{\prime} 9 ; 16 \mathrm{mid} .5 / 6$ $16-16 \mathrm{mfd} .7 / 9$; $32 \mathrm{mfd} .6 / 9$.
Denco LF. Liver, for aceurately lining $465 \mathrm{~K} / \mathrm{c}$. and $1.6 \mathrm{~m} / \mathrm{c}$. I.F. channels, and associate circuits. Battery operated Potentiometers. New, not Ex-Govt. $2 \mathrm{~K}, 5 \mathrm{~K}, 10 \mathrm{~K}, 25 \mathrm{~K}$ $50 \mathrm{~K}, 100 \mathrm{~K}, 950 \mathrm{~K}$, 1,1 and 2 meg. Price, less switch,
$3 / 9$. Price with $\$ /$ Pole switch. $5 / 9$. Price with $\mathrm{D} / \mathrm{Pole}$ 3/9. Price
switch, 66 .
Surplus Potentiometers. All standard with extended spindles, $5 \mathrm{~K}, 10 \mathrm{~K}, 15 \mathrm{~K}, 20 \mathrm{~K}, 25 \mathrm{~K} .50 \mathrm{~K}, 100 \mathrm{~K}, \frac{\hbar, 1 \text { and }}{}$ 1 mag.. 2/-each.
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Colls, Denco "Maxl Q." midget size, Litz woand on Polyatyrene Formers, bith adjustable iron cores. Avail $3 / 9$, each. or with reactlon winding $4 / 9$. Denco Matched pair T.R.F. Colls for long and medlum waves, $6, \mathrm{E}_{\mathrm{f}}$ sir. long and mediumed pairs of coils, for T.R.F. covering long and medium waves, 10 \& pr., orfor Superhet ca vering
Lang, Medium and Bhort Waves, $11 / 8 \mathrm{pr}$. Ali types of Wang, med
Coil Pacte"
Coil Packs. Onmor Minget Coll Pack. gize 3 in $\times 2 \mathrm{Hn} . \times$ lin. covering B. M. and L. waves. Colls wound on Pficient performance with adjustable iron cores, ensure including full circults for Superhet $4 \mathrm{Bi}^{\prime} \mathbf{K} / \mathrm{c}$. Unit 52 ; (1ncl. P.T.). Thls Osmor Coll Pack ls also svailable for Midget Superhet HatTERY Portable seta including matched ready wound Frame Aerial. Price $54 / 2$ (incl P.T.). Weymouth Midget $31 \times 21 \times 1$ in. covering 8.M.L. $\mathrm{w} /$ barde, for $465 \mathrm{Kc} / \mathrm{s}$, er
Colls on each w/band, $51 / 6$.
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short-medinm-long waves. Both for 468 ke/s short-medinm-long waves. Both for $468 \mathrm{kc} / \mathrm{s}$. Incor-
porates gram. position, and employs mdjustable cored coils. $53 / 4$.
All of the sbbove Coil Packs include Switching, Padding and Trimmer Condenwer
20 hny. 250 . Midget 10 benry 250 ohms 40 mA ., $3 / 6$ 20 hny. 250 ohm $60 \mathrm{~mA}, 6 / 6 ; 20 \mathrm{hny} .300$ ohma. 100 mA .
$12 / 9$; 5 hny. $50 \mathrm{ohm} 250 \mathrm{~mA}, 28 / 6 ; 20 \mathrm{hny} .250 \mathrm{ohm}$. $120 \mathrm{~mA} .15 \mathrm{~F}: 9 \mathrm{hny} .250$ ohm , 120 mA . 8,$6 ; 18 \mathrm{hny}$ $200 \mathrm{ohm} ., 250 \mathrm{~mA}, 25^{\prime} 6$
1.F. Transformer, $465{ }^{2} \mathrm{E}$. New well-known manufactures's surplus in. $x$ in. $x$ lita. Iron Core, $8 /-$ earh. lenco Iron Core, 465 K e. or $1.6 \mathrm{~m} / \mathrm{c}, 1 \mathrm{j} \mathrm{ja} . \times 1 / \mathrm{im} . \times 3 / \mathrm{in}$. $16 / 6$ pair. Wearite Stand Cap, Tuned $465 \mathrm{~K} / \mathrm{c}, 201-\mathrm{pr}$.
 and 6.3 y .9 amp., 11/. (b) Inpot 230 volts, output E.E.T. Transformer. Prim. 230 volts 1 anp., $13 / 9$. 5 Kec . and 4 -volt tapped 2 volt, $58^{\prime} 6$. Do., but $4 \mathrm{~K}^{2} \mathrm{~V}$. $5 \mathrm{~S}^{2}$ -
Heater Auto Transformorn. (a) tapped 2 v. 4 v., 5 $\nabla$., and 6.3 volts $3 \mathrm{amp} ., 9 / 6$; (b) 4 v .3 amp . to k v .2 mmp . Reversible, 6 '6: (c) 4 v. 3 amp, to 6.3v, 2 amp. Rever Fible, $6 / 6$.
NEW SURPLUS ! 1 FOSTER TRANSFORMERS. Primary 230 volts. Becondary 12 volts 9 amps. $21 /$
Filament Translormer. Inputs 230 volte, outputs 6.3 . 1) amp., 8/3: 4 . 1 \& amp., $7 / 6$ : Input $200 / 250$ v output 4 v. (C.T.), 11 smpr, 4 v. 2 amp., 6.3 v. 2 amp.
$19 / 6$. Input 230 v . output 6.3 v. (C.T.) 4 amp., $17 / 6$. $4 \mathrm{in} . \times 2 \mathrm{in} .3,11,9 \times 5 \times 24 \mathrm{in} .5,3,10 \times 6 \times 24 \mathrm{in}, 6 /-$ $8,3,16 \times 8 \times 24$ in. $9 /-$
Mains Transformers. All Now gtock with Primaries tapped for 200-250 volts, Secondaries (a) $250-0-250$ volt, 80 mA ., 6.3 \%. (tapped 4 v.) 4 amp. and 5 . (tapped 4 v.) 2 amp., $18 / 6$ (asso stailable with $350-0-350$ voit at 18/6). Btern' $350-0-350$ volt, 150 mA .6 .3 r . (tapped 4 F.), 4 amp , and 5 v. (tapped 4 v.) 2 amp., $41 / 6$; (c) $350-0$ volt 200 . 250 mA ., $6.3 \mathrm{v} .6 \mathrm{amp} .79 / 6$, and many other ratines.
Westinghouse Reotifers. (a) H.T. 51. Rated 350-0-3.50 volts, $100 \mathrm{~mA} 35 / \mathrm{F}$ (b) ELT. 52 . Fated $350-0.350$. $200 \mathrm{~mA}, 37 / 6$; (c) K.T.53. Hated $500-0 \cdot 500$ $200 \mathrm{~mA} ., 50 /-$
Types. $14 \mathrm{D} 3611 / 3$; $16 \mathrm{HT} 28,12 / 6$; $16 \mathrm{FHFT} \overline{6}$, $17 / 9$ $36 \mathrm{EHT}^{25}, 13 / 10 ; 36 \mathrm{EHT} 25$ 18/2: $36 \mathrm{EHT40}, 2016$ $36 \mathrm{EHT} 45,22 / 6 ; 36 \mathrm{EHT} 50,24 / 10$ : $36 \mathrm{EET} 60,25 / 8:$ F/Wave Bridge Rectitiers.
For charging 2.4 or 6 volt at 11 amps.
For charging 6 or 12 volt at 11 smps.
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A Varisble Resistor for control of Charging Equipment (or Modela) up to 3 amps., 15/-
Sutable Selonium, Rectifiers. $10 / 6$.T., $5 / \mathbf{H}$, wave. 250 v. 50 mA ., $5 / 6$ Chso v. $100 \mathrm{~mA} ., 7 / 6$; 250 จ. $170 \mathrm{~mA} ., 13 / 9$.
Charger Transiormers. sultable for was with preceding Rectiflers. Each has ipput of 230 volts. Outputs (b) 24 volts tapped $15 \nabla, 9 \nabla$. and $4 v$, at 3 amps. $23 / 9$;
(b) 30 volts tapped 15 v. and $9{ }^{5}$. ist 3 amps., $25 / 9$ : (b) 30 volts tapped 15 volts tapped 8 at 3 ampus., $17 / 9$ (d) 12 volt if amps., 119; (e) 15 volts tapped 9 v . at 6 amps . $23 /-; 15$ volts tapped 9 v . at 11 amps., $14 / 3 ; 12$ voles 1 amp., 7/6.
A Battery Charger Whing Diagram is included with
purchase of Charger Tranaformer and Rectifier. purchase of Charger Transformer and Rectifter. Ad fustablo Mains Droppers. 14 in . dia. $\times 2$ in. (a). 15 amp.
1.500 ohms., $5 /=$ (b). 2 amp., 1.000 ohms, $43:$ (c) .3 1.500 ohms., 5/- \%

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To cut inin. dia. (B8a)
To cut 1tin. dia. (Octal)
To cut liln, dia. (English)
To cut lifn. dia, (EF50)
Adjustable Chassis Cutter for holes from jin . to $2 \boldsymbol{i} \mathrm{i}$ The "Handy-Utility" tin. Portable Electric Drill for use on A.C. or D.O. maids. A powerful and robust drill that will drill wood, metal, and almost anything. can also be used for grinding, bufing and wire brushing, otc.
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D.C. A vominor

ADVANCE
Audlo Generator Type HI
TAYLOR "WINDSOR"
70A Testmeter 1,000 ohms/volt
75A Testmeter 20,000 ohms $/$ volt
90 A Testmeter 1.000 ohms//volt. Isi Giraile
110B, O. and R. Brldge
65B Bignal Generator.
650 signal Generator
55A Wohbulator
30A Oacilloscope
180A Electronic Testmeter
290A Audio Genera
20 B Mignal Tracer
MISCELLANEOUS
Woe-Megger 250 v .
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BPL Foundation Meter 311 L . 1 MA BSD. calibrated ohros-volis

$\begin{array}{lllllll}£ 25 & 0 & 0 & 97 & 0 & 0 & 33 / 4 \\ £ 28 & 0 & 0 & 48 & 0 & 0 & 36 / 8\end{array}$ $\begin{array}{rrrrrrr}£ 12 & 10 & 0 & £ 4 & 10 & 0 & 17 /- \\ £ 15 & 0 & 0 & £ 5 & 0 & 0 & 20 /- \\ £ 17 & 10 & 0 & £ 5 & 10 & 0 & 23 / 6 \\ £ 15 & 15 & 0 & £ 4 & 15 & 0 & 22 /- \\ £ 11 & 0 & 0 & £ 2 & 10 & 0 & 176 \\ £ 15 & 10 & 0 & £ 4 & 10 & 0 & 88 /- \\ £ 17 & 15 & 0 & £ 5 & 15 & 0 & 83 / 6 \\ £ 14 & 14 & 0 & £ 4 & 14 & 0 & 20 /- \\ £ 29 & 10 & 0 & £ 9 & 10 & 0 & 3 / 6 \\ £ 27 & 10 & 0 & £ 9 & 10 & 0 & 34 /- \\ £ 22 & 10 & 0 & £ 7 & 10 & 0 & 29 /- \\ £ 29 & 0 & 0 & £ 9 & 0 & 0 & 37 / 6 \\ £ 15 & 15 & 0 & £ 4 & 15 & 0 & 22 /- \\ & & & & & & \\ £ 19 & 8 & 6 & £ 5 & 2 & 6 & 28 / 8 \\ £ 18 & 18 & 0 & £ 4 & 18 & 6 & 2610 \\ £ 12 & 12 & 0 & £ 3 & 12 & 0 & 18 / 4 \\ £ 5 & 0 & 0 & £ 1 & 10 & 0 & 9 / 2 \\ £ 83 & 0 & 0 & £ 25 & 0 & 0 & 111 / 2 \\ £ 25 & 0 & 0 & £ 8 & 0 & 0 & 34 / 9 \\ £ 25 & 0 & 0 & £ 7 & 0 & 0 & 33 / 4 \\ £ 3 & 10 & 0 & £ 1 & 0 & 0 & 7 / 6\end{array}$

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Dual spoed motor unlt
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Plek-up, two heade, and transformer
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Deces " turn-over "crystal 78 and L.P Acos GP20
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TRIXETTE
AC7s Auto 1 speed
P358 3 speed Don auto
A358 3 speed auto
R.P. $\quad 12 \mathrm{~m}^{\prime} \mathrm{t}^{\prime} \mathrm{y}$ $\begin{array}{rrr}\text { Cash } & \\ \mathbf{8 2} & 18 & 8 \\ £ 6 & 9 & 0 \\ \mathbf{2 3} & 11 & 8 \\ 15 & 0 \\ 14 & 8 \\ \mathbf{1 1 0} & 15 & 8 \\ \mathbf{8 3 3} & 14 & 8\end{array}$ $£ 2$
£15
£
14
7 $16 / 8$
422 $38 / 4$ $\begin{array}{crccccc}£ 3 & 18 & 4 & £ 1 & 9 & 4 & 7 / 6 \\ £ 3 & 11 & 5 & - & & = \\ £ 2 & 5 & 0 & - & & - \\ £ 2 & 9 & 0 & - & & - \\ £ 7 & 0 & 0 & £ 2 & 0 & 0 & 118 \\ £ 1 & 17 & 6 & - & & - \\ £ 2 & 13 & 0 & - & & - \\ £ 2 & 13 & 0 & - & & - \\ £ 3 & 12 & 6 & £ 1 & 2 & 6 & 7 / 6 \\ £ 6 & 2 & 0 & 22 & 2 & 6 & 10 /- \\ £ 3 & 8 & 2 & £ 1 & 0 & 0 & 7 / 3\end{array}$

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| MOTORS | Negliglble atray neid |  | Cash |  |  |  | $\begin{aligned} & 12 m^{\prime} t^{\prime} y \\ & D^{\prime} m m^{\prime} t a \text { ol } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B.S.R. Type PP.10. |  |  | \&1 18 | 0 |  |  |  |
| B.S.R. Typu SR. 1. |  |  | ¢1 12 | 0 | - |  | - |
| B.S.R. Trpe 8R. 2 |  |  | £15 | 0 | - |  |  |
| Collaro with fitted fan. | Clock or | anticlock | 82 | 0 | - |  |  |
| Collaro moters, match | ed pair |  | ¢ 4 | 0 |  | 40 | 8/4 |
| Set of three motors. 3, | , Collaro m | atchad, I, BSR-FPP10 | $26 \quad 2$ | 10 |  | 210 | 10\% |
| TAPES |  |  |  |  |  |  |  |
| E. M.1. low coercivity | 6001t. |  | 15 | 0 | - |  | - |
| E.M. I low coercivity | 1,200ft. |  | E1 5 | 0 | - |  | - |
| G.E.C. | 1,200ft. |  | \&1 10 | 0 | - |  | - |
| Durez | 1,200ft. |  | £115 | 0 | - |  |  |
| 8 prare spools, 1,200ft. |  |  | 4 | 6 | - |  | - |
| HEADS |  |  |  |  |  |  |  |
| Audigraph " TAMsA. | ". Record | Playback | ¢2 19 | 6 | $\square$ |  |  |
| Andigraph '" TAM8A', | ", Nrake |  | 2219 | 6 | - |  |  |
| Audigrajh " TAMSA' | ' Playbac | only .......... | £2 18 | 8 | - |  | - |

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## Ferrograph

MICROPHONES
Acos MIC-22-2

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Andigraph "T TAMAA" 10 highimpedance heads, with
circuit dlagram 106
TAPE DECK KITS (Motors 8 Heads)
3 motors: 2 GR1, 1 FP10. 2 heads: Erase. 1111 e
Record
3 motors:
motors: 2 Collaro matched, 1 FP1O, heads and
motors as in A. 3 heads. Rec./Phy/Erase and
Onolllator coil
3 motorsas in $B .3$ healsasin $\mathbb{C}$. Oscllater coll.
PKIt as A plus 1,200ft. E.M.1. tape and spare spol
As E. With (t.E.C. tape
As B. phas 1,200tt. E.M.1. and spare spool
As H. With G.E.C. tupe
As $\mathbf{A}$. With Durex tape . . . . . . . . . . . . . .
As C. Plus L,200tt. H.M.
As L. With G.E.C. tape
As D plus 1,2noft. E.M.I. tape and spare spool
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| $£ 11$ | 11 | 6 | $£ 3$ | 11 | 6 | 168 |
| ---: | ---: | ---: | :--- | ---: | :--- | :--- |
| $£ 12$ | 11 | 6 | $£ 4$ | 1 | 6 | $17 / 6$ |
| $£ 14$ | 11 | 0 | $£ 4$ | 11 | 0 | $20 /-$ |
| $£ 15$ | 11 | 0 | $£ 5$ | 1 | 0 | $20 / 10$ |
| $£ 13$ | 1 | 0 | $£ 4$ | 1 | 0 | $18 / 4$ |
| $£ 13$ | 6 | 0 | $£ 4$ | 1 | 0 | 189 |
| $£ 13$ | 11 | 0 | $£ 4$ | 1 | 0 | $19 / 2$ |
| $£ 14$ | 0 | $£ 4$ | 11 | 0 | $19 / 2$ |  |
| $£ 14$ | 6 | 0 | $£ 4$ | 11 | 0 | $19 / 7$ |
| $£ 14$ | 11 | 0 | $£ 4$ | 11 | 0 | $20 /=$ |
| $£ 16$ | 0 | 6 | $£ 5$ | 1 | 0 | $21 / 8$ |
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| $£ 16$ | 10 | 6 | $£ 5$ | 1 | 0 | $22 / 6$ |
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and erase heads in mumetal shields. Heavy and erase heads in mumetal shields. "Heayy balanced flywheel giving freedom from "wow and "flutter." Fast rewind. Heads are halftrack, giving one hour's playing time with $1,200-$ foot reet of tape. $£ 16 / 10 /$, plus carriage. etc. 10/.. Demonstrations at both Deptford and Lewisham branches.

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TINPLATE CHASSIS. Two sided, $10 \frac{1}{2} x$ $41 \times 2 \mathrm{in}$. undrilled, $2 / 9$ each.

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Sewing-Machine Motors, A.C.) D.C., complete with foot-controi pedal, pilot light, etc., brand new, in maker's carton, 4 only... Ex-W.D. Wave-Meter, complete and perfect AVO latest model Electronic Valve-Tester complere and as Valve-Tester, complete and as
new, with ali charts.............. $£ 40 \quad 0 \quad 0$ C.D.P. Wisc Recorder, less

BC.342, as new, with all valves ... $821 \quad 0 \quad 0$ Avo 1949 Capacity and Resistance Bridge, as new, prise ............ $88 \quad 0 \quad 0$
Cossor Impedance Bridge, Model 3389, as new, prise ............... \& 1910
Cossor Ganging Oscillator, Model 90
M.C.R.I., complete, with coils,
powerpack, phones, erc., asnew 8800
Eversheds, 500 v. wee megger, in leather case, as new, price
Garrard R.C.65, record changer, as new, price ........................
Taylor 120 A.C./D.C. Test meter,
as new, price

Owing to pressure of business we have been unable this month to list as many lines as in our previous advertisements but we have in stock Marconi Signal Generators, Record Changers, P.A. Equipment of all types, Communications Receivers, Test Meters, Quality Speakers, VOIGT Speakers in Cabinet as new, Transmitters, etc.

$\star$We have a large selection of 'British and U.S.A. Valve Testers, Test-Meters and Signal Generators, etc. Your enquiries are welcome. S.A.E. please.
THESE ITEMS ARE ONLY A SMALL SELECTION FROM OUR STOCK OF EQUIPMENT. YOUR ENQUIRIES FOR ANYTHING THAT YOU MAY NEED WILL BE WELCOME.

WE HAVE OTHER EQUIPMENT ARRIVING DAILY:
CASH OR CHEQUE WITH ORDERS.
ALL ITEMS LISTED ARE CARRIAGE EXTRA.

## 22 LISLE STREET, LEICESTER SQUARE, LONDON, W.C. 2

JUR BRANCH AT 39a (opposite) IS OPEN ALL DAY THURSDAY.
Phone: GERrard 4447, 8582 and 5507. Hours 9 to 6. Thursdays 9 to I.

#  

BRAND NEW RII55 RECEIVERS, in original cases, complete with 10 valves, $£ 12 j 10 /-$, $7 / 6$ packing and carriage.

BRAND NEW RI355 RECEIVERS, original cases, as specified for the "Inexpensive Televisor." complete with || valves, $\mathbf{E 2 / 1 5} /$-. $7 / 6$ packing and carriage.

BALANCED ARMATURE LOW RESIST. ANCE HEADPHONES: Type 1,5/II set Type 2, $7 / 11$ set.

HIGH RESISTANCE HEADPHONES, $12 / 6 \mathrm{sec}$.

MOVING REED HEADPHONES, Type 5 8/II ser.

LIGHTWEIGHT HIGH RESISTANCE HEADPHONES, $14 / 6$ set.
TANNOY HAND MICROPHONES, with switch in handle, 4/11.

ACCUMULATORS, by world-famous maker, 2 volt 10 a., 4/11.

## BURGOYNE SOLDER GUNS, 75/- <br> GRAMOPHONE AMPLIFIER KIT



Consists of complete Kir of Parts for a $2 \frac{1}{2}$-watt Mains-operated 2 -stage Amplifier for use with any cype of pick-up. Volume and cone controls are incorporated. Output impedance is 3 ohms. Cat. No: AMPI47. Price complete, 59/6. For $200-250 \mathrm{v}$. mains with valves and diagrams.

## GRAMOPHONE UNITS

Connoisseur 2-speed Gram Unit, less pick-up

620193 Pick-up and 2 heads for above ....... Conrad Rim Drive Gram Unit, Iess pick-up, 78 r.p.m. ............................ Conrad Rim Drive Gram Units, 33 r.p.m.
Decca 3-speed Rim Drive Gram Unit, less pick-up ...........................
Decca single-speed Rim Drive, less Decca si 1964 All the above................................... $\mathrm{E}_{3} 14$ andy.

## VCR97 C.R. TUBES

These tubes are new but have slight cut-off, 19/6, plus 5/-packing, carriage and insurance.

## THREE-PIECE AERIAL

Ex-U.S.A. copper-plated steel, highly flexible with non-stick screw joints, tapering 考in. to tin. Brand new in container, 6/9, packing and carriage 1/6.
insulated Base, 2/6.
MAINS NOISE ELIMINATOR KIT. Two specially designed chokes with three smoothing condensers with circuit diagram. Cuts out all mains noise. Can be assembled inside existing receiver, 6/- complete.


BUILD A PROFESSIONAL LOOKING RADIO AT LESS THAN HALF TO-DAY'S PRICE
We can supply all the parts to help you. Bakelite Cabinet (Brown or Ivory)... Packing and insurance
Punched chassis, 3-valve plus rectifier T.R.F.

Engraved Glass Dials, J80-550 and 800-2,200 m.
With station names, new wavebands T.R.F. Coils, 180-550, 800-2,200
metres, pair
Drum (2 $\frac{3}{4}$ in, diam.)
Driving head
Double pointer
Spring
Nylon cord (yard
Dial Front Plate..
SEND $1 / 6$ FOR EASY TO FOLLOW POINT TO POINT DIAGRAMS. THE CIRCUIT DIAGRAM AND PRICED PARTS LIST, which shows you how YOU can build the Receiver illustrated above at a total cost of
£5/19/6
The Radio is a TRF 3-valve and metal rectifier Receiver for operation on $200 / 250$ volt A.C mains. Waveband coverage is $180 / 550$ metres on medium wave, and $800 / 2,000$ merres on long wave. The Dial is illuminated. The artractive bakelite cabinet to house the Receiver, size 12 in . long, 5 in . wide, 6 in . high, can be supplied in either walnut or ivory colour.


The famous Dulci Midger Receiver for use on either A.C. or D.C. mains, $200 / 250$ volt. This is a 2 -waveband 4 v . Superhet Receiver covering the short waveband from 13.6 metres to 50 metres, and the medium waveband from 200-550 metres. Can be supplied in either ivory or brown bakelite cabinet.
Size $7 \frac{3}{4} i n$. length.
6in. height.
$5 \frac{1}{6}$ in. depth.
This receiver is fully covered by the manufacturer's guarantee.
Price $£ 8 / 15 / 0$, carriage paid
THIS OFFER CANNOT BE REPEATED
H.T. ELIMINATOR AND TRICKLE CHARGER KIT
All parts to construct an eliminator to give an output of 120 volts at 20 mA , and 2 volts to charge an accumulator. Uses metal rectifier, $£ 2$.

SUPERHET COILS
16-50, 180-550, 800-2,000 metres, set, including circuit, 10/6.

SUPER QUALITY TELEVISION MAGNI. FYING LENS. To suit 5 in ., 6 in . or 7 in . Tubes. Increase picture size considerably, 25/-each.

## METAL RECTIFIERS

Bridge type
2 v. 5 amps, ... $2 /-\quad 6$ v. 1 amp.
 Output 650 v. $1 \mathrm{~mA} .4 / 7$ each.
f,000 v. $1 \mathrm{~mA} ., 6 /=$ each.
Outputs given are half wave. Two of either Rectifiers can be used in voltage doubling.

## BATTERY CHARGER KITS

All incorporate metal rectifiers. Transfórmers are suitable for $200 / 250$ v. A.C. 50 cycle MAINS. Cat. No.
2002 Charges 6 volt accumulator at
I amp. Resistance supplied to charge 2 v . accumulazor .. at I amp.
\&1 76

## BRAND NEW CAR BATTERIES



Delco-Remy, in original cases 6 v. $100 \mathrm{a} ., 44 / 17 / 6$, plus $7 / 6$ carriage and packing. 6 v .140 a ., $£ 5 / 10 / \mathrm{m}$, plus $7 / 6$ carriage and packing. 12 v. 85 a:, British made, $£ 5 / 10 /=$, plus $7 / 6$ carriage and packing.
6 v . 170 mA ., in reak case, $85 / 10 / 0$, plus $7 / 6$ carriage and packing.
T.V. WHITERUBBER MASKS (CORRECT ASPECT). We can supply a speciallydesigned White Rubber Mask for 6 in . C.R. qubes at 8/6 each.
9in. White Masks, 9/6.
12in. White Masks, 16/1 I. Round or flat faced.
SORBO RUBEER MASKS, GREY FELT FINISH (NEW ASPECT RATIO).
9in., 5/-: $12 \mathrm{in} ., 9 / 6$.
P.M. MOVING COIL LOUDSPEAKERS ( 3 ohm voice coils)
$2 \frac{1}{2} \mathrm{in}$. Goodmans ......................................... 15/-
3in. Plessey .................................................. 15/-
5in. Plessey .............................................. 12/6

6in. Truevox ........................................... 12/6
8in. Plessey ......................................... 14/6
IOin. P.R.C................................................. $27 / 6$
I2in. Truevox ....................................... 70/-
Please add $1 / 6$ for post orders under 40/: 1/2 under 20/-. Cash with order or C.O.D.

Open every day until 6 p.m., includin: Saturdays.
Closed I p.m. Thursdays.
PADdington 3271
PADdington 3272

## MAINS <br> TRANSFORMERS

These transformers are all famous radio manufacturers' surplus and are fully Interleaved, impregnated and guaranteed.
Primary $200-250$ v. P. \& P. on each 1/6 extra.
$300-0.300,100 \mathrm{~mA}, 6$ vole 3 amp, 5 vole $2 \mathrm{amp}, 17 / 6$.
$320-0-320,100 \mathrm{~mA}, 6$ vole 3 amp . 5 vole 2 amp, $17 / 6$.
320-0-320, $120 \mathrm{~mA}, 6$ vols 4 amp, 5 volt $2 \mathrm{amp}, 25 /-$.
Heater Transformer, 4 vols 3 amp, 4 volt $3 \mathrm{amp}, 2$ volt 3 amp, 2 volt 3 amp , $7 / 6$. $250-0-250,100 \mathrm{~mA}, 6 \mathrm{v} .3 \mathrm{amp}$, $4 \mathrm{v} 3 \mathrm{amp},. 4 \mathrm{v}, 3 \mathrm{amp}, \mathrm{i} / 6$. $4 \mathrm{v} .3 \mathrm{amp}, 4 \mathrm{v}, 3 \mathrm{amp}, 17 / 6$.
$250-0 \mathrm{mp}$ (to be used on common heater chain with $6 \times 5$ rectifier), $13 / 6$. $280-0-280,80 \mathrm{~mA}, 6 \mathrm{v} .3 \mathrm{amp}$, ${ }^{4} \mathrm{v} .2 \mathrm{amp}$, drop-through, 14/-. Drop thra, 350-0-350 v. 70 mA . $6 \mathrm{v} .2 .5 \mathrm{amp} .5 \mathrm{v} 2 \mathrm{amp},. 14 / 6$. Semi-shrouded, drop-thro' or upright mouncing 280-0-280 80 $\mathrm{mA}_{12 / 6} 4 \mathrm{v} .6 \mathrm{amp}, 4 \mathrm{v} .2 \mathrm{mp}$, 12/6.
Auto-wound H.T 280 voles at $360 \mathrm{~mA}, 4$ v. $3 \mathrm{amp}, 2$ v. 3 amp . or 6 v .3 amp . Separate 4 v .3 amp rectifier winding (uprighe or drop-through), $10 / 6$.
$350-0-350 \mathrm{v}, 120 \mathrm{~mA}, 4 \mathrm{v} .6 \mathrm{amp}$. 4 v. 3 amp , drop-chrough, $21 /$. Auto-transformer, yarious combinations of voltages including 110 v .70 watt, and $3 / 4$ volts windings ar $1 \mathrm{amp}, 2$ vole 1 amp . drop-through or uprighe mouncing, $10 / 6$.
Heater Transformer Pri. 200250 v., 6 v. |f amp, 6/q. P. \& P. each 9 d .

## ELECTROLYTIC CONDENSERS

$16+16 \mathrm{mid} .450 \mathrm{v}$. wkg., $5 / 6$. 50 mid. 50 wkg., $1 / 9$.
100 mfd . 12 v . $\mathbf{w k g} .1 / 3$.
$50 \mathrm{mfd} .12 \mathrm{v} . \mathrm{wkg} .1 /$.
$25 \mathrm{mfd} .25 \mathrm{v} . \mathrm{wkg}_{\mathrm{g}}, 1 / 2$.
$16 \times 8 \mathrm{mfd}$., $450 \mathrm{wkg} ., 4 / \mathrm{m}$
$8 \mathrm{mid} .450 \mathrm{v} . w \mathrm{~kg} ., 2 / \mathrm{s}$.
$250 \mathrm{mid} .12 \mathrm{v} . \mathrm{wkg} ., 1 / 3$.
$15 \mathrm{mfd} .500 \mathrm{v} ., 4 / \mathrm{m}$
$8 \mathrm{mfd} .500 \mathrm{v} ., 3 / \mathrm{m}$.
$8 \times 8 \mathrm{mfd} .450 \mathrm{wkg}, 3 / 6$.
32 mfd .350 wkg., $2 / 6$
$32+32 \mathrm{mfd}$. small tube tag ends
$200 \mathrm{v} . \mathrm{wkg} ., 2 /$.
$16+8$ mid. 350 wkg ., miniature tag end, 3/-
P.M. SPEAKERS
with less

|  | trans. trans |
| :---: | :---: |
| $3 \frac{1}{2} \mathrm{in}$. | 11/6 |
| 5 in . | 15/-12/6 |
| $6 \frac{1}{2} \mathrm{in}$. | 14/6 11/6 |
| 8 in. | 17/-14/6 |

IOin. M.E. Speaker Field Coil 1,100 ohms, speech coil 2.3 ohms, 17/6.
P. \& 'P. on' each of the above 1/-extra.
Constructor's Parcel. Comprising chassis $10 \pm \times 5 \frac{1}{2} \times 2 \mathrm{in}$. with speaker nd valve holder cut-ours, Sin. P.M. speaker with eransformer, twin gang with trimmers, pair T.R.F. coils long and medium iron cored, four and medium holders 20 K volume control and wave-change switch. Post-paid, 21/-.

# D. COHEN <br> RADIO \& TELEVISION COMPONENTS 



Walnut Bakelite Cabinet, $14 \frac{2}{2} \mathrm{in} . \times 10 \frac{1}{2} \mathrm{in} . \times 8 \mathrm{in}$., complete with 5 -valve superhet chassis, with 5 -vaive superhet chassis, plate, drum, 2-speed spindle, plate, drum, 2 -speed spindle, four pulley wheels, two springs, four brown kno
$25 /$, post paid.

Pensolda 6 volt Light Weight Soldering Iron, weight $3 t$ ounces complete with $1 \frac{1}{2}$ yards circular flex. 8/6. Post \& pack. 1/-. Complete with suitable heater transformer Primary 230/250 volts, $10 / 6$. Post \& pack. $1 / 9$. Transformer not sold separately.


LINE AND FRAME COILS, low line, high frame complete with mounting bracket (removed from chassis), guaranteed, 6/6.
LINE AND E.H.T. TRANSFORMER. 5 Kv . (removed from chassis). guaranteed, $9 / 6$.
HEATER TRANSFORMER. Primary $230 / 250$ secondary 2 volt $2 \frac{1}{\frac{1}{2}}$ amp., $5 /-$. FRAME BLOCKING OSCILLATOR TRANSFORMER, 4/6.
SMOOTHING CHOKE. 2 hen. $200 \mathrm{~mA}, 3 / 6$.
SMOOTHING CHOKE. 5 hen. $250 \mathrm{~mA}, 5 / 6$.
T.V.CHASSIS. Size $9 \frac{1}{4} \times 9 \frac{1}{4} \times 34,3 \%$
P.M. FOCUS UNIT. For any 9 in. or 12 in . Ube, except Mazda 12 in ., state tube, $12 / 6$.
P.M. FOC US UNIT. For Mazda $12 \mathrm{in} ., 15 /$.

MAINS or BATTERY SUPERHET'PORTABLE COILS. Comprising medium wave frame aerial and long wave loading coil, used as aerial coils. Midget iron cored screened L/M osc. coils, complete with circuir I.F. frequency Midgetiron co
$465 \mathrm{Kc} ., 9 / 6$.
6 IRON CORED LONG, MEDIUM and SHORT SUPERHET COILS coupling winding on all bands, $13.5-50,180-550,1,000-2,000$ metres, complete with circuit, $8 / 6$.
METAL RECTIFIERS, 250 v. 60 mA , latest midget Selenium type, $6 / 6$ post pd. OUTPUT TRANSFORMERS. Standard type 5,000 ohms imp.. 2 ohms speech coil, $4 / 9$; Push-Pull 6 v. 6 matching 10 watt 2 ohms speech coil, $6 / 9$. Miniature type to suit $155,5 /$-.
SET OF 3 BROWN KNOBS marked " wave change," "tuning," and "volume," $1 / 6$.
SMOOTHING CHOKES. 30 mA 300 ohm .
45 mA 300 ohm .
60 mA 6.8 hen.
80 mA 10 hen.
6-pin 6 volt synchronous vibrator
6 volt standard 4 -pin vibrator
Vibrator transformer $250-0-25080 \mathrm{~mA} .6$ vole. Pri

TELEVISION MASKS
White Rubber. 9in. with glass, 10/6. White Rubber. 12 in . with glass, $15 /$. 15 in . white rubber mask, soiled, 12/6, plus 1/.P. \& P. Midget Components. Twin gang zin. diameter, tin. long. (The dimensions of this gang are slightly yeeper than a standard volume control.) Pair Medium and Lang iron cored T.R.F. Coils $\frac{3}{4}$ in. long $x$ tin. wide complete with a 4 -valve all-dry circuit, tuning seale and pointer knob. All the items $10 / \mathrm{r}$ post paid.
All-Dry A.C. Mains Supply Unit, size $3 \frac{1}{2}$ in. long $\times 2 \frac{1}{4} i n$. wide $\times 1$ tin. deep. We can supply a complete all-dry circuit, using the above Midget Components to incorporate the above Power-Unit, 19/6, pose paid with circuit.
Midget Bakelite Cabinet. 7in.
$5 \frac{1}{3} \mathrm{in}$. $\times 5 \mathrm{in}, \mathrm{c} / \mathrm{w} 5$-valve $\mathrm{S} / \mathrm{h}$. chassis med.flong wave scale and back (cakes std, swin gang condenser and $3 \frac{1}{2}$-in. speaker). 15/-. P. \& P. I/6.
Line and Frame Coil Assembly. Frame coils wound but not fitted (full instructions supplied). High impedance frame ; plied). High impedance frame ; 5-1, 8/6.
Wave Change Switches. 6pole 3-way, 2/-; 3-pole 2-way 1/2; 4-pole 3 -way, $1 / 9$; 5 -pole 2-way midget, $1 / 9$. P. \& P. 3d. each.
Pre-Aligned Midget 465 Kc . Q. $120,9 /$ per pair, post 6 d . Miniature 465 Kc.l.F.s. Q.120, per pair $10 / \because$.
465 Kc* Midget I.F.s. Q. 120, size $\frac{1}{2} \mathrm{in}$. long, lin. wide, $\begin{aligned} & \text { in. }\end{aligned}$ deep, by very famous manufacdeep, by very. Pre-aligned adjustable turer. Pust cores, per pair, $12 / 6$. Iron Cored 465 Kc . Whistle Filter, screened, each 2/6.
Valve Holders. Paxolin International octal, 4d. each. Moulded international octal, 7d. each. EF50 ceramic, 7d. each. Moulded B7G slightly soiled, 6d. each.
Line Cord. 3-way 0.3 amp . 180 ohms per yard, $1 / 3$ per yard. Ceramic P.F.S. 3 each of the following : 330, 220, 180 and 82. 2/6.
 -450 pi., 10d.
Twin Gang $\mathbf{C o n d e n s e r}$. 0005 Tuning Condenser, 54 -. With trimmers, 7/6. Post and packing 6d.
Twin Gang Midget .00037 with perspex dust cover and with perspex
trimmers, $8 / 6$. Post and packing trim.
6d.

Mains. Droppers. 0.3 amp. 460 ohms, tapped 280 and 410 , $1 / 6 ; 0.2 \mathrm{amp}$. 717 ohms, tapped at 100 ohms, vitreous, $1 / 6$; 0.3 amp .950 ohms, tapped 700 and $825,2 / 6 ; 0.2 \mathrm{amp} .1,000$ ohm, vitreous, tapped, $2 / 6$. P. \& ${ }^{\prime}$ P. on each, 3 d .

Volume Controls by famous manufacturer. Long spindle and switch $t$, $\frac{1}{2}$, 1 and 2 meg., 4/each ; 20,25 and 50 k ., $3 / 6$ each. Post and packing 3d. each.
Volume Controls, by famous manufacturer. Long spindle less switch, 5 k., 50 k., 500 k., 1 meg 2/6 each. P. \& P. 3d. each.

Terms of business: Cash with order. Dispatch of goods within 3 days from receipt of order. Where post and packing charge is not stated please add I/- up to El and $1 / 6$ up to $£ 2$.

# 23, HIGH STREET (Opposite Granada Cinema), ACTON, W. 3 

## CLYDESDALE

## Bargains in Ex-Service Radio and Electronic Equipment

## FIELD TELEPHONE

The "Tele" F battery powered unit, completely self-
contalned, table type bakelite moulded case. Ringing generator, Used but reconditioned and tasted prior to desputch. Uses "s" or "T" sell batterles (not supplied). overall dimensions: of $\times 6 \frac{1}{2} \times 5 \|$ in.
CLYDESDALE'S
PRICE ONLE
POST
PAID

PUMP DESICCATOR ADM. PATT. 12128 FOR TELESCOPES AND BINOCULARS Hand operated complete with spare gel cell and conn. tubes. Stroke cap 480 ces. fitted humidity gauge, reads
$10 / 100 \%$ vacuum gauge $0 / 30 \mathrm{ln}$. In wood transit case $191 \times 121 \times 9$ in.
CLYDESDALE'S
85.10 .0 OARRIAGE

COOLANT PUMP BY PACKARD U.S.A. A turbine type pump, directly driven from semi-ball point, mpline wocket (by trotor not supplied), clockwise rotation with satety valve, sludge vent. etc.
Dia. of turbine 6in., dla. of purmp chamber 81 in ., depth 2 in . Inlet and outlet dia. 1ifn. Overall dim.: $111 \times 7 \frac{1}{2} \times 13 \mathrm{in}$ $\begin{array}{ll}\text { CLYDESDALE'S } \\ \text { PRICE ONLY }\end{array} 49 / 6$ CARRIAGE

## FEATHERING PUMP 5U/402

Driven by a 24 v. D.C. motor type C28ul, through 2.1 reductlon gear, fluid moved by two 12 -tooth wheels. Safety valve fitted. Overall dimensions $121 \times 6 \times 6 \mathrm{in}$. Pumping rate: lubricating oil, 2 gals. per min. approx. Air pressure: 40 tbs. per sq. In. Oil pressure: over luo lbe. per sq. in. Inlet, 3 in . Outlet, 3 in.
CLYDESDALE'S
PRICE ONLY
$2.10 .0 \quad$ OARRIAGE
PAID

## ELECTRONIC IGNITION TESTER <br> Type V.E.D. Patt. 563562, made by English Electric

A Cathode Ray Teater employing an entirely new technique in ignition testing of internal combuation engines. Enables the electrical performance of the
entire Ignition aystem to be ohserved on the gcreen of entire Ignition aystem to be ohserved on the screen of the Cathode Ray Tube, while the engine ti running-
Will operate from 6,12 and 24 volta D.C. or 230 v. A.C. Built into a blick crackie case with hinged front and carrying handle. Dim.: $151 \times 81 \times 11$ in.
$\left.\begin{array}{ll}\text { CLYDESDALE'S } \\ \text { PRICE ONLY }\end{array}\right\}$

## CRYSTAL OYEN

Brand new, extremely mensitive with adjustable thermootatle control and thermometer. Built into a cork-lined metal box $12 \times 6 t \times 6 \mathrm{fin}$. Wgt. 51 l ibs.
CRYDESDALE'
\&3.19.6

PAST

INDICATOR UNIT TYPE 217a
Containing 100 microamp iod. $2\{\mathrm{ln}$. flush mitg. meter, din calibrated $\ln$ yards: vol. controls, toggle ew., etc., in metal case $6 \times 41 \times 21 \mathrm{n}$.
$\begin{array}{ll}\text { CLYDESDALE'S } & 25 / \mathrm{POST} \\ \text { PRICE ONLY PAID }\end{array}$

## FLUXMETER WY. 0023



Deaigned to calibrate the Held of Magnets within the range of 500 to 4,000 garss and to determine their polarity. Complete with probe anit and contained in a hardwood case with hinged lid and handle. Instructions on lid. Dim.: $12 \neq 9 \times 6 \mathrm{~m}$.
CLYDESDALE'S
${ }_{6} 5$
CARRIAGE

COMMAND RECEIVER CCT/CBY 46129 U.S.N. version of the BC-453 for that sharp channel 12 K 8 . 12 ser range $550-190 \mathrm{Kc}$, with 6 valves, $3 \times 128 \mathrm{~K} 7$, Dim. : Il $\times$ ©i $\times 51 \mathrm{~s}$. Finish black, tess dynamotor.
CLYDESDALE'S
PRICE ONLY
O/
$\underset{\text { PAID }}{\text { POST }}$
Clrcuits of BC-453 available at $1 / 3$.

## NEW LIST NO. $B$

Giving details and illustrations of exservices ftems and cancelling all previous lists and supplements.

Ready November-Price 1/6.
Price credited on first purchame of $10 /$ - or over.
R3547 CHASSIS LESS VALVES
Probably the greatest breakdown value of any of the Rular Recelvers. Contalna n removable 45 mes. I.F. Atrip, 24 . reversible motor, nith $700: 1$ geariug, relay, pote, Charsis enclosed in metal case. Dim. : $18 \times 13 \times 7 \mathrm{in}$. $\begin{array}{lll}\text { CLYDDESDALE'S } \\ \text { PRICE ONLY }\end{array} \quad 39 / 6 \quad$ CARRIAGE

## THE R3601 RECEIVER UNIT

A 14-valve dual chaseis radar receiver, with 85 mes. and 45 mes. I.F. stripp. R.F. section, high cycle power atation.
 suppled complete with valves. Housed in metal case $18 \times 9 \times 8 \mathrm{in}$., finish light blue.
$\underset{\text { PRICE ONLY }}{\text { CIYDESDALE's }} \$ 4.12 .6$ CARRIAGE

AMPLIFIER A127I IOU/549


A one-valve (VRăf = EF36) Amplifier Chaseis, with 400 ohm 4M 2 B relay, 2 transformers, vol. control, cond. and resistors, mounted on rubber in a black fimished metal case $56 \times 412$
clypesdale's
10/6
POST

## MULTICORE CABLE

8 Core, metal braided and PVCcovered, $1 / 9$ per yard, post 3 d . 6 Core, metnil braided and PVCcovered, $1 / 9$ per yard, post 3 d . 2 Core, metal braided, 8d. per yard, post 3 d .
Metal Brafled Sleeviug, 3 mra. 1 yd. long, 3 for $1 /=$, pont 3 d .

## 日7G VALVEHOLDERS

These are of Paxolin construction, 9 d , each. Post 3 d .

> Ex-services items, totalling \&5 or over in value, can now be obtained on Easy Terms at any of our branches. Just choose your fitem or thems, pay a deposit of ti. in the g aud we will do the rest avallable to Personal Shoppers only.

## MAINS DROPPER

Vitreous enamel construction 717 ohma, tapped at 110 ohms Capable of baddling 30 watta. Dimensions: $3 \%$ in. $\times$ ifin djam.
CLYDESDALE'
2/6
POST
3.

JEFFERSON TRAVIS UF-2 TRANSCEIVER CHASSIS


Partly stripped by the M.O.S., leme vaiven, tunlng inductance, owe. connectionk, but otherwise fairly intact. A fine basis lor a transportable type two-way radio. Original ire-
quencies $60-75$ mes. Valve types $2 / 6 \mathrm{Y} 7$. 12J3. The unit comprises two chassis, with controls and speaker mounted on chrome plate etched steel panels, housed in cabinet finiaher black crackle. Dim.; $153 \times 18 y^{\times 88} \mathbf{i n}$. CLYDESDALE'S
£2
CARRIAGE
PAID

JEFFERSON TRAVIS UF-I POWER SUPPIY
Complete meli-contained vibrapack. Ingut 12 volts. Outputs $120 / 150$ v. D.C. $30 / 50 \mathrm{~mA}$. Choke capaclty amoothes and 2 L .T. Laps. Unused but vibrator contacts stuek due to long etorage. Complete with synchronous vibrator, amoothing cond, etc., in metal case. Dim.: $7 \times 3 \times 4 \mathrm{in}$.
CLYDESDALE'S CARRIAGE PRICE ONLY
$25 /=$
PAID
S.440-B V.H.F. TRANSMITTER CHASSIS

Partly atrlpped by the M.O.S., lesp valves, tuning colls and cryetal, but otherwise fairly intact.
A fine basis for V.H.F. TX. or 144 tnes, rig Orginal irequencies $85-98$ mes., valve types $3 / \mathrm{BR} 34$, 2/6A7, BV6. Housed in louvred case, finizhed grey crackle. MYDESDALE'S MYICE ONLY

27/6
POST

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WIRELESS SET NO. 38 Mk. 2 BRAND NEW
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100 watts $110-200-230-250$ v...............
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