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DECEMBER 1957

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Wireless World

ELECTRONICS
Radio · Television



FORTY-SEVENTH YEAR OF PUBLICATION

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Wireless World

ELECTRONICS, RADIO, TELEVISION

Managing Editor : HUGH S. POCOCK, M.I.E.E.

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DECEMBER 1957

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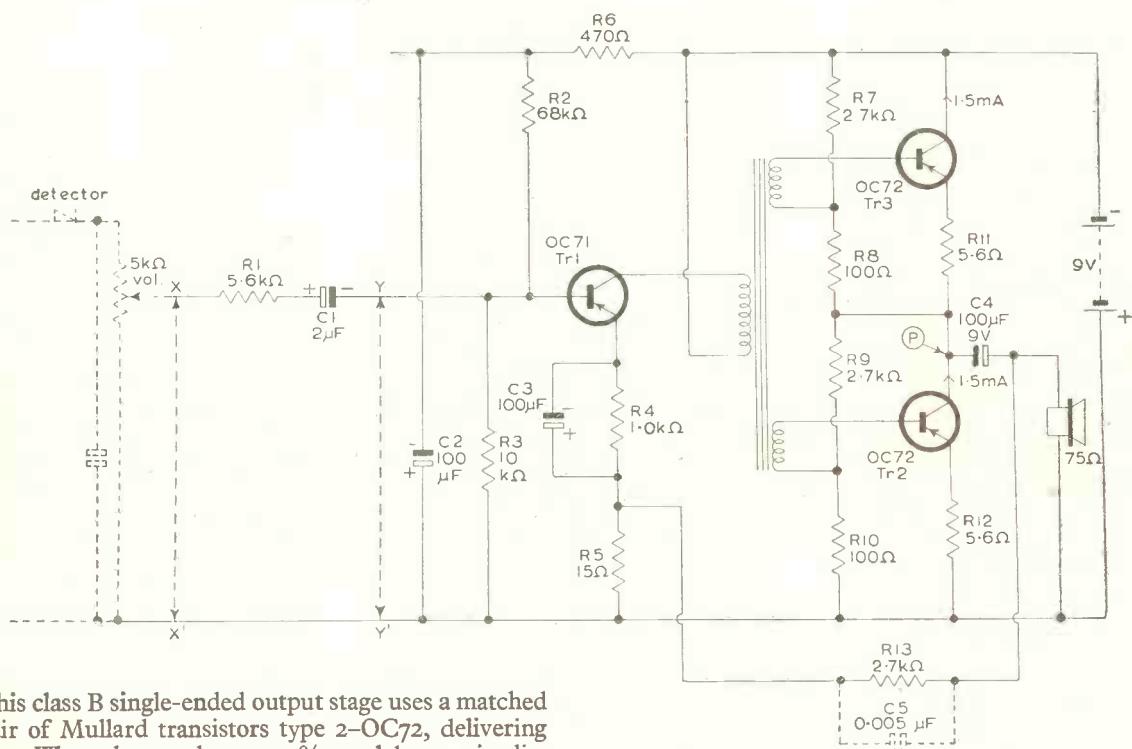
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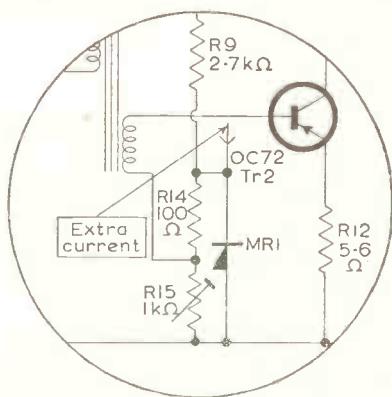
Transistor**Output Stage for Personal Receivers**

This class B single-ended output stage uses a matched pair of Mullard transistors type 2-OC72, delivering 100mW to the speaker at 10% total harmonic distortion. The OC72s, which are used without cooling fins, each have a maximum dissipation of 25mW. The circuit will operate safely and satisfactorily up to an ambient temperature of 45°C. Capacitive coupling to the speaker does away with the need for a centre-tapped supply. The point 'P' is automatically held to half the supply voltage.

A Mullard OC71 is used in the driver stage, with d.c. stabilisation provided by R2-R3-R4. The coupling transformer has a turns ratio of $7:1 + 1$, with primary resistance $<750\Omega$ and secondary resistances $<100\Omega$. The primary inductance is 5H with 1.5mA d.c. flowing.

The input impedance at YY' is about $3.5k\Omega$, which is partly due to feedback from the speaker via R13. R1 further increases the input impedance at XX' to 8 or $9k\Omega$. A drive of 180mV r.m.s. across XX' is necessary to provide 100mW output when transistors at the minimum sensitivity limit are used. Undesired feedback from the output stage to earlier stages in the receiver is prevented by R6-C2. The battery drain is about 10mA on speech and music, and 4mA with zero signal. The circuit is therefore suitable for incorporation in pocket-size personal receivers.

A further battery economy is provided by the modification shown in the inset, which allows operation to much lower voltages without excessive crossover distortion by stabilising the base bias voltage. The point at which the battery must be discarded is therefore postponed. With this arrangement a small extra current, taken from some other point in the receiver, is required by MRI.



Twenty-one Years

IN offering belated felicitations to the B.B.C. on the 21st anniversary of the establishment of the world's first high-definition television service, *Wireless World* has in mind in particular the work of the Engineering Division under the successive direction of Sir Noel Ashbridge and Sir Harold Bishop. Although we allow ourselves to be distracted occasionally by the efforts of the programme departments, it is with the millivolts per metre and the quality of the modulation that we are primarily concerned.

Already, the network of high-, medium- and low-power transmitters covers 98 per cent of the population; but the remaining 2 per cent, approximately a million souls, are not to be forgotten, for we learn that very low-power transmitters which will operate unattended are being developed to illuminate the remaining dark corners. Although local complaints are inevitable there can be no doubt that the country as a whole has been well served by the planning departments of the B.B.C.

Against the background of the early 30-line experiments by Baird which were broadcast by the B.B.C. on medium waves from 1930, the 405-line standard adopted in 1936 well merited the description "high-definition." It still does for the majority of viewers in this country, who own receivers of modest size and cost and who look at programmes in which the greater part of the "information" conveyed to the brain is essentially of a dynamic rather than a static nature. The need for a higher standard becomes apparent only when the programme people turn their cameras on still subjects containing detail finer than the resolution of the system (which includes the performance of the receiver) or when too large a screen is viewed at too short a distance. Few will dispute that the picture quality broadcast by the B.B.C. is still better than that of the majority of commercial receivers, which have to be produced at a price which the public will pay.

What of the future? It is not improbable that new techniques will eventually be evolved for the production, at prices we can afford to pay, of receivers with larger screens, higher definition

and/or colour. When that day comes the B.B.C. will be ready to play its part, for it has already started an exploration of the potentialities in this country of Band V as a medium for the propagation of pictures of normal and higher definition; it is also broadcasting colour signals on Band I for the use of receiver manufacturers.

Pioneer Experiment

OUR congratulations and best thanks to the Russians for having placed a 1-watt transmitter in an orbit which traverses most of the civilized world, and on frequencies which were well chosen for revealing the effects of the ionosphere. Congratulations, also, to the radio receiving and radar tracking resources of this country for the speed and accuracy with which they were brought into action, and the ingenuity already displayed in extracting the maximum possible information from quickly improvised experiments.

Radio has given invaluable service to the physicists and astronomers in determining the motion of the satellites. It has also collected for itself a mass of data which is already yielding fresh knowledge of the constitution of the upper atmosphere and of the way in which radio waves are propagated. But because the life of the batteries has been relatively short, the transmitted frequencies restricted, and the trajectories have been at this time of year for the most part outside the ionosphere, much more remains to be done before the exploration of the fine structure of the ionosphere by extra-terrestrial waves reaches the same level as that attained by the ground ionospheric sounding stations of the world.

In many ways these first exciting days are reminiscent of the early experiments of Rutherford on atomic structure when far-reaching results were deduced from the patient observation of and subsequent cerebration on the scintillation of alpha particles on a zinc sulphide screen. Once again, it is the "scintillation" of the received signal strength and Doppler frequency shift which holds many of the secrets now being unravelled.

Band V Tests

U.H.F. TELEVISION BROADCASTS BY THE B.B.C.

AT the request of the Television Advisory Committee the B.B.C. has started a further and more ambitious series of u.h.f. television experiments. Initially these tests, which began on November 9th, will employ the 405-line standard with vision on 654.25 Mc/s and sound on 650.75 Mc/s, but from about next April, after the transmitter has been modified, they will be on 625 lines with negative modulation and sound changed to 659.75 Mc/s, ± 50 kc/s, f.m.

The B.B.C. has installed at the Crystal Palace a 10-kW (peak) u.h.f. vision transmitter and a 2.5-kW carrier power sound transmitter manufactured by E.M.I. The equipment is low-power modulated on both sound and vision channels and employs klystrons in both audio and video final stages. These klystrons use three external cavity resonators and operate as linear amplifiers with a power gain of approximately 100. They are driven by a modulated amplifier stage operating with a cathode modulated circuit. The output of the transmitters is combined in a circuit of the filter bridge type constructed in rectangular section waveguide. The combined output is then conveyed to the aerial by an elliptical (12in by 6in) waveguide. The elliptical waveguide is made of 99.5% aluminium in 12-ft lengths. At the top of the television mast the waveguide is transformed into a 5-in concentric feeder to take power to the four driving points of the helical aerial, the pole supporting the aerial forming the outer of the concentric feeder.

The helical aerial of $\frac{1}{2}$ in diameter copper rod comprises four bays, mounted one above the other on the same vertical axis, each having a linear height of five wavelengths. Each bay is fed at the centre, the helix being wound from the centre point of the bay in opposing directions to cancel the vertical component of radiation. The aerial has a power gain of 20 and after allowing for losses in the feeder and waveguide system, the effective radiated power of the vision signal is of the order of 125 kW (peak) in the horizontal plane.

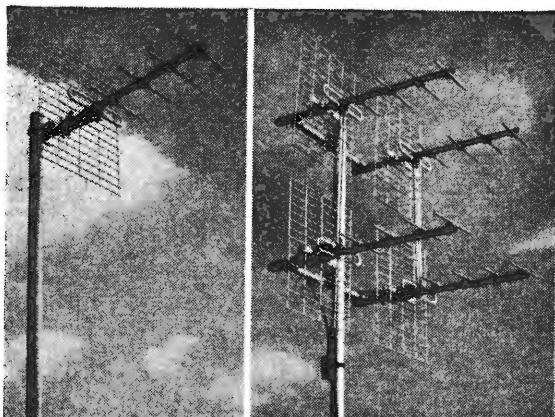
Surmounting the Crystal Palace mast the Band V helical aerial is about 700 feet above ground. There are 48 turns in all, each being approximately 2λ long

The transmitter is in use for several hours a day radiating the same programme as that being broadcast by the Band I transmitter in the same building. Later on, the pictures on 625 lines will be produced at Lime Grove from flying spot film-scanning equipment (supplied by Cinema - Television) and sent by a coaxial cable to the Crystal Palace.

Various types of receiver, representative both of designs that might become available at economic prices to the public and also of types at present unsuitable for domestic use, will be employed by the B.B.C., radio industry, Post Office, D.S.I.R., and I.T.A. to study the received pictures. The B.B.C. hopes that the information gained from these tests will throw light on the problems which would be encountered were it decided to provide television services in the u.h.f. bands and also the effects of a change of television standards for those bands.

It will be recalled that the B.B.C. started investigations into u.h.f. propagation some two years ago. These were concerned not only with service area tests but for the purpose of obtaining data on co-channel interference. For this purpose they employed Mullard transmitters, modulated by square-waves. They were installed at various television stations, and regular field-strength measurements were made over long periods at various locations, some as far away as the Shetland Islands.

The long-distance tests were followed in 1956 by a series to determine propagation conditions within a typical service area using a transmitter at the Crystal Palace, working into a Yagi aerial and radiating a peak power of 1 kW over a fairly narrow beam when modulated with square waves; pulse modulation was also used for some of the tests. The bearing of the aerial, which was at a height of 440ft, was changed from time to time so that field-strengths could be measured over the whole circle from Crystal Palace.



Receiving aerials for u.h.f. television (Belling & Lee)

WORLD OF WIRELESS

"Scatter" Frequencies

SIX 400-kc/s bands have been allocated by the American Federal Communications Commission for ionospheric scatter transmissions. The lower frequency in each of these bands is 32.6, 34.6, 36.6, 46.6, 49.6 and 54 Mc/s, respectively. To avoid interference with American television stations, those frequencies which lie within the U.S. television channels will be used by scatter stations remote from the United States and its territories.

Some of these frequencies, of course, come within our TV channels and reference is made in the B.B.C.'s annual report to the interference (mainly in S.E. England) being caused by forward-scatter transmissions. Interference in the neighbourhood of the U.S. Air Force station at Kingston Blount, Oxford, was at one time very severe.

The possibility of more widespread use of forward scatter is viewed with some concern by the B.B.C., which stresses in its report that television broadcasting bands should be protected from any such threatened interference.

Intermodulation Testing

AT an informal meeting of representatives of the leading British recording companies and pickup manufacturers, convened on the initiative of M. Minton, chief development engineer of Cosmocord, Ltd., the question of standards for expressing intermodulation distortion in pickups was discussed. At present no universally accepted method of testing has been established and comparison of published figures is often meaningless. After a general survey of the present position a working party was elected to investigate the problem in detail.

It has now been agreed that any further discussions of the working party shall be on a formal basis within the framework of R.E.C.M.F. Panel "N" (gramophone equipment).

Research Awards

THE Paul Instrument Fund Committee, set up by the Royal Society, Physical Society, Institute of Physics and I.E.E. "to receive applications . . . for grants for the design, construction and maintenance of novel, unusual or much improved types of physical instruments and apparatus for investigations in pure or applied physical science," have announced three awards.

Dr. D. Gabor, Mullard reader in electronics, Imperial College, receives £100, making £1,900 in all, for work on a new type of Wilson cloud chamber in the form of a resonant microwave cavity. Professor G. F. J. Garlick, professor of physics in the University of Hull, receives £2,700 to enable him to carry out studies of phosphors and photoconductors with a view to the development of solid-state light image amplifiers or converters. The third award, of £2,000, goes to Dr. H. H. Hopkins, senior lecturer in physics (technical optics), Imperial College, for the construction of a static scanning fibrescope.

B.B.C. Colour Tests

A SECOND series of test transmissions of colour television are being undertaken by the B.B.C. This new series of experimental transmissions, which began in October and will continue for about six months, are being radiated from the B.B.C.'s Crystal Palace station (Channel 1) outside the normal programme times.

The purpose of the tests, which are being conducted with a modified version of the American N.T.S.C. system, is:

- (1) To provide a source of high-grade colour picture signals so as to permit colour receiver development work to continue,
- (2) To enable further experience to be gained in the operation of the colour studio and colour transmitting equipment, and
- (3) To obtain further knowledge of the compatibility provided by the particular system of colour transmission being tested.

Details of the somewhat involved cycle of transmission times are obtainable from the B.B.C.

Faraday Medallist

FOR his "outstanding contributions in the field of international communications and particularly in the development of long-distance, deep-sea telephone cables and their repeaters," Sir Gordon Radley, K.C.B., has been awarded the Faraday medal of the Institution of Electrical Engineers, of which he is the immediate past-president. Sir Gordon, who is the first engineer to be director general of the Post Office, has been in the G.P.O. since 1920 when he joined as a temporary inspector in the research branch. In 1944 he became the first holder of the office of controller of research and was successively deputy engineer-in-chief, e.-in-c., and deputy director general until he assumed his present position in 1955.

On his appointment in 1954 as deputy director general he retained, at his own request, technical responsibility for the British contribution to the transatlantic telephone cable with which he had been so closely associated.

Computer Standardization

ONE of the aims of the recently formed Data Processing Section of the Radio Communication and Electronic Engineering Association is the formulation of standards for computers, and to this end a number of working parties have been set up. One is concerned with nomenclature, another with tape standards for both analogue and digital computers, while yet another is studying information storage cores. The section, of which C. Metcalfe (E.M.I. Electronics) is chairman, includes 16 member-firms of the Association plus four other companies.

A growing number of associations and groups are being formed in this country to discuss data processing equipment and the R.C.E.E.A. Data Processing Section is investigating the possibility of forming

a joint organization, through which information could be pooled.

As already announced, the R.C.E.E.A. is collaborating with the Office Appliance and Business Equipment Trades Association in organizing the first British Electronic Computer Exhibition and Convention, to be held at Olympia, London, from November 28th to December 4th next year.

The R.C.E.E.A. has also become one of the sponsoring organizations for the next Instruments, Electronics and Automation Exhibition to be held at Olympia from April 16th to 25th next year.

T.E.M.A.—The first awards in a competition introduced by the Telecommunication Engineering and Manufacturing Association for the best final-year apprentice of member-firms, were made at the Association's annual dinner on November 13th attended by some 270 members and guests. The recipients of the £25 awards in each of the three categories were:—D. V. Moreton (graduate in training) of A.T. & E.; R. L. Reid (student apprentice) of Ericsson; and B. A. Edwards (technician apprentice) of S.T.C. The T.E.M.A. dinner coincided with the publication of the Government white paper on changes in the telephone service including the introduction of electronic group routing and charging equipment (GRACE).

R.T.E.B.—A record number of candidates sat for this year's examinations for the servicing certificates issued by the Radio Trades Examination Board. Of the 1,117 taking the sound radio exam, 466 (42%) passed and 336 have to retake the practical test. Entrants for the television exam. totalled 237. Of these 106 (45%) passed and 48 have to retake the practical test. An analysis of the entrants shows that some 50% of the candidates were under 19 years of age, which may account for the examiners' view that approximately half the candidates lacked practical experience.

An Appointments Service for servicemen has been introduced by the R.T.E.B. It is available free to employers and the 2,500 holders of the Board's servicing certificates. Particulars are available from the Board at 9, Bedford Square, London, W.C.1.

Two research scholarships, valued at £435 per annum, have been awarded by the B.B.C. to graduates in electrical engineering giving them the opportunity to work for a higher degree. The subjects for research must be in those fields of telecommunications or physics which have an application to sound or television broadcasting. The recipients are J. B. Izatt, graduate of Aberdeen University, who will conduct his researches in the electrical engineering laboratories of Robert Gordon's Technical College, and W. A. G. Voss, who graduated at Queen Mary College (University of London), where he will continue his research work.

Medical Colour TV.—The American pharmaceutical firm, Smith Kline and French Laboratories, who have an establishment in this country and earlier this year demonstrated American closed-circuit colour television at St. Bartholomew's Hospital, London, have now ordered a mobile colour television unit from Marconi's. It will employ the anglicized 405-line N.T.S.C. system and will be placed at the free disposal of medical authorities for use at professional meetings. Both 21-inch direct-viewing colour monitors and medium-screen projectors will be used with the unit, which will also incorporate a monochrome channel.

Visit to Germany.—The Brit.I.R.E. proposes to arrange a party to visit factories, research laboratories and other radio establishments in Western Germany in the early summer of next year. The tour is planned to extend over about 10 days and in general the mornings would be devoted to technical visits and the afternoons to sight-seeing.

General Radio.—We are asked to point out that General Radio Co., of 9-10, Noel Street, London, W.1, whose advertisement appeared on page 92 of the November 1957 issue of *Wireless World* is not associated with the General Radio Co., of Cambridge, Massachusetts, U.S.A. Nor are they associated with Claude Lyons, Ltd., of Liverpool and Hoddesdon, Herts, who are the exclusive agents in the U.K. for the General Radio Company, of Cambridge, Mass., U.S.A.

Technical Hitch.—The opening of the I.T.A. transmitter at St. Hilary, Glam., originally planned for December 17th, has been postponed. An advanced design of aerial had been planned, but unforeseen technical difficulties have arisen necessitating further development work. Marconi's are therefore replacing it by a more conventional type giving similar coverage.

Test transmissions from the v.h.f. sound transmitter installed at the television station at Kirk o' Shotts, Central Scotland, began on November 15th. The station, which is due to come into regular service before the end of the year, will radiate horizontally-polarized transmissions on 89.9, 92.1 and 94.3 Mc/s with an e.r.p. of 120 kW.

Transatlantic trials of "Dectra," the long-range version of the Decca Navigator, are again under way. The tracking pattern is being produced from two of the stations in the East Newfoundland Decca chain and the ranging pattern by synchronized transmissions from stations in Newfoundland and Scotland. Tests on routine civil and military flights are being undertaken during these trials. Canada's fourth Decca Navigator chain, centred on Quebec, was brought into service on November 5th.

Brit.I.R.E.—In the Institution's report for the year ended March 31st the total membership is given as 5,568—an increase of 176 during the year, and of over 800 during the past three years.

Transatlantic Television.—A standard Pye 17-inch television receiver, fed from a rhombic aerial, was used in New York for the reception of B.B.C. television transmissions direct from London on November 1st. The set was lent to Press Wireless, Inc., and was used at their receiving station at Baldwin, Long Island.

TV on Tape.—For his achievements in the development of a practical video tape recorder, Charles P. Ginsburg, manager of advanced videotape development in the Ampex Corporation, California, has been awarded the David Sarnoff Gold Medal by the American Society of Motion Picture & Television Engineers.

Soviet Colour Television.—Three systems of colour television are now being tested in Moscow and Leningrad, according to *Soviet News*, to determine which one to adopt in the Union. At present there are approximately two million monochrome receivers in use in the U.S.S.R.

Transistor Circuit Techniques.—A course of ten evening lectures on transistor circuit techniques is to be held on successive Tuesdays from January 21st at the Medway College of Technology, Maidstone Road, Chatham, Kent.

"**Electronics in Industry**" is the title of a five-day course organized by the factory department of the Ministry of Labour, to be held at Burton in Wirral, Cheshire, from January 20th to 24th. The fee is £6, including tuition and residence, for people from adjoining areas, but £7 for others. Applications should be sent to J. B. Newton, the warden, Burton Manor Residential College for Adult Education, Burton in Wirral, Cheshire.

Radio transmissions of particular interest to yachtsmen, and lists of coast radio stations and radio beacons, are given in the 52-page reference section of the *Yachting World Diary* for 1958, which includes all the day-to-day information the yachtsman requires. The Diary costs 10s in leather binding or 6s 6d in waterproof Rexine.

"Induction" Licence.—The period covered by the £2 licence for "inductive" paging systems recently introduced by the Post Office is five years, not one year as stated on page 518 of our last issue. The number of sending and receiving "stations" covered by the licence is unlimited.

Receiving Licences.—An increase during September of 66,978 in the number of combined television and sound licences in the United Kingdom brought the total to 7,398,185. This figure, together with the 6,945,178 licences for domestic sound receivers and 324,078 for car radio, brings the overall total at the end of September to 14,667,441—a decrease of nearly 18,000 during the month.

A two-day conference on band theory of metals and the structure of the Fermi surface has been organized by the Physical Society. It will be held at Imperial College, London, on December 19th and 20th. The conference fee for non-members is one guinea. Applications for programmes and registration forms should be addressed to Miss Miles at the Society's headquarters, 1, Lowther Gardens, Prince Consort Road, London, S.W.7.

Personalities

Rear-Admiral Sir Philip Clarke, R.N. (retd.), K.B.E., C.B., D.S.O., immediate past-president of the British Institution of Radio Engineers, was recently presented with a silver cigarette box bearing the Institution's coat-of-arms in commemoration of his presidency from 1954 to 1956. Sir Philip was director of the Naval Electrical Department at the Admiralty from 1951 to 1955.

Sir Harold Bishop, C.B.E., director of engineering in the B.B.C., has accepted the invitation from the Television Society to become a vice-president. Sir Harold has been with the B.B.C. since 1923, and was chief engineer for nine years before he succeeded Sir Noel Ashbridge in 1952.

Sir Ivone Kirkpatrick, G.C.B., G.C.M.G., has succeeded **Sir Kenneth Clark, K.C.B.**, as chairman of the Independent Television Authority. Sir Ivone, whose appointment by the P.M.G. is for five years, retired from the Foreign Office last February. He is 60. At the beginning of the war he was director of the foreign division of the Ministry of Information, and in 1941 became controller of the B.B.C.'s European Service.

Sir Harry Railing, D.Eng., Hon.M.I.E.E., has relinquished the position of chairman and joint managing director of the General Electric Company, which he joined in 1905 to take charge of the test department and laboratories at Witton Engineering Works. Sir Harry, who received a knighthood in the New Year's honours of 1944, was trained as an electrical engineer on the continent, where he received his degree, and then spent some time in the U.S.A. before joining the G.E.C. He is succeeded by **Leslie Gamage, M.C., M.A.**, who joined the company as assistant secretary in 1919.

R. N. Fitton, who 28 years ago founded the original company manufacturing Ambassador receivers, has relinquished the managing directorship of Ambassador Radio & Television, Ltd., and is succeeded by **Denis Robinson**, who is also managing director of E-V, Ltd. Both companies are in the Camp Bird Group.

Eric E. Pratt has been appointed commercial manager in the electronics and equipment group of the Plessey Company. He was at one time in the equipment division of Mullard and more recently was sales manager of Airtech, Ltd.

Next Year's National Radio Show has been fixed for August 27th to September 6th with a preview on the 26th. This will be the 25th national show and will again be held at Earls Court, London.

WHAT THEY SAY

Visionary.—"I sometimes think that one or two dealers must really believe the old saying, 'without vision the people perish,' because they don't seem to stock much in the way of non-vision receivers!"—*Arthur Glover, Murphy Distribution Manager.*

"What's in a Name?"—"Radio communications, in the broad sense that includes broadcasting and aids to navigation, is the technology for which the I.R.E. was founded. But today only a minority of the members of I.R.E. would claim that 'radio engineer' best describes their calling. In fact, the word 'radio' does not appear once among the names of the I.R.E. Professional Groups, and only one-half of the Group organizations have any direct interest in radio frequency techniques as such."—*Donald G. Fink, Editor, "Proceedings of the Institute of Radio Engineers."*

James Reekie, B.Sc., Ph.D., A.M.I.E.E., F.R.S.E., appointed chief engineer of Semiconductors, Ltd., the recently formed Plessey - Philco company, has been in Canada for the past 12 years. Dr. Reekie was for some time professor of physics at the University of Toronto and later head of the department of physics at the Royal Military College of Canada, but immediately prior to returning to this country he was research director in semiconductors and solid state physics for the Northern Electric Company, Montreal.



Alan Lee, M.A., M.I.E.E., is appointed to the newly created chair of electrical engineering (radar and telecommunications) at the Royal Military College of Science, Shrivenham, Wilts., where he has been head of the radar and telecommunications branch since 1941. Professor Lee, who is 50, joined the college in 1935, having previously spent a short time in research in industry and teaching at the R.A.F. electrical wireless school at Cranwell.

Arthur Charlesby, D.Sc., Ph.D., A.R.C.S., F.Inst.P., is appointed to the new chair of physics at the Royal Military College of Science. After a period in the scientific research department at the Ministry of Aircraft Production he served with the R.A.F. until 1945 and from 1949 to 1954 was a principal scientific officer at A.E.R.E., Harwell. For the past two years Professor Charlesby, who is 41, has been head of the radiation department of Tube Investments Research Laboratories.

Robin W. Addie, M.A., who was for some years technical commercial manager of Philips and for the past 18 months has been assistant commercial manager, has left the firm and joined E.M.I. Electronics as export manager. He graduated from Cambridge in 1939 with a degree in engineering and joined Philips in 1946. He is the chairman of the Radio Industry Council's exhibition technical committee and has for the past few years been largely responsible for the sound and television relay installations at the National Radio Show.

K. S. Brown, the new president of the Institution of Radio Engineers (Australia), spent five years in England after graduating Bachelor of Electrical Engineering at Melbourne University. During his stay in this country he spent two years with the G.E.C. at Coventry and three years with S.T.C., where he was engaged on radio and line transmission equipment. He returned to Australia in 1939 to establish a valve division in the S.T.C. factory at Sydney and he is now manager of the electronics division which absorbed the valve division.

Major C. Collaro, O.B.E., has resigned his position as chairman and managing director of Collaro, Ltd., owing to ill-health, but will continue to be available to the company on technical matters. **Henry Roughton** succeeds him as managing director and **E. B. Urietti**, previously works manager, has joined the board.

F. R. W. Strafford, M.I.E.E., has been exclusively retained as technical consultant for aerial and aerial components by Kimber-Allen, Ltd., of Myron Works, London, S.E.13. Mr. Strafford will continue his technical practice in other radio and electronics spheres.

W. Woolfenden, engineer-in-charge of the Croydon I.T.A. station since its opening in 1955, has been appointed e.-in-c. of the Authority's St. Hilary transmitter. He was with the B.B.C. for eight years before joining the I.T.A. and was an R.A.F. radar officer during the war. He is succeeded at Croydon by **G. E. Tagholm**, B.Sc.(Eng.), who was on the B.B.C.'s Alexandra Palace staff before joining the Authority.

A. J. Solomon, executive engineer at the Post Office receiving station at Ongar, Essex, since 1955, succeeds **G. K. Fagg**, who retired on August 30th, as manager/engineer of the Post Office radio station at Bodmin, Cornwall. Mr. Fagg joined Marconi's as a radio operator in 1912 and in 1921 went to the company's research department. He subsequently joined Cable & Wireless, transferring to the Post Office in 1950 when C. & W.'s services in the U.K. were integrated with those of the G.P.O. Mr. Solomon is also an ex-Marconi man. He was for some time in the commercial receiver development section at Chelmsford.

A. T. Black, C.B.E., has left the Ministry of Supply, where he was director of electronics production (munitions), and has joined Pena Copper Mines, Ltd., where he will direct the group's electronics division. It will be recalled that Pena recently acquired Peto Scott Electrical Instruments and Cosmocord.

H. W. Shipton, A.M.Brit.I.R.E., who for some years has been electronics development engineer at the Burden Neurological Institute, Bristol, has accepted the position as research associate in medical electronics in the State University of Iowa, U.S.A. He is probably best known for his work on toposcopic display systems for electro-encephalography. His duties at Bristol will in future be shared by Dr. R. Cooper and W. J. Warren.

M. W. S. Barlow, M.A., A.M.Brit.I.R.E. (G3CVO), who was a founder member and secretary of the British Amateur Television Club and has contributed to *Wireless World* on amateur television topics, has left Marconi's at Chelmsford, where he has been a development engineer for the past four or five years, to take up an appointment with the Canadian Marconi Company.

Baron C. de Beer, who has been associated with the Rediffusion group of companies for some years, being until recently assistant chief engineer of the Jamaica Broadcasting Company (a member of the group), has joined the Rocke International Corporation, of New York, as chief engineer (broadcast and communications). For ten years prior to joining Rediffusion he was a signals officer in the R.A.F.

N. P. White, recently appointed manager of the components division of A. C. Cossor, Ltd., joined the company in 1939 and has successively held the positions of manager of the methods department and chief production engineer.

OUR AUTHORS

R. J. Hitchcock, M.A., A.M.I.E.E., author of the article on page 599, joined Cable & Wireless in 1948, where he was initially engaged on radio-frequency allocation work and represented the company at international conferences including the Extraordinary Administrative Radio Conference in Geneva in 1951. He is now in charge of a section of the engineer-in-chief's department responsible for the design of aerials, radio propagation and radio circuit performance studies, prediction of optimum usable frequencies and other radio frequency matters such as interference, etc. He is a member of the U.K. study groups of the C.C.I.R. dealing with ionospheric, tropospheric and ground-wave propagation.

Francis Oakes, A.M.I.E.E., A.M.Brit.I.R.E., M.Inst.E., and **E. W. Lawson**, A.M.I.E.E., who contribute the article in this issue on a transistorized galvanometer, have previously collaborated to write for *Wireless World*. They are both with the Ferguson Radio Corporation, where Mr. Oakes (a frequent contributor to *Wireless World*) is in charge of transistor applications research and Mr. Lawson is in charge of the standard laboratory at Enfield. Mr. Oakes, who came to this country from Austria, was for some time assistant chief of the electronics laboratory of the Morgan Crucible Company before joining Ferguson. Mr. Lawson, following service with the Ministry of Aircraft Production during the war, was in charge of quality control at Plessey until joining Ferguson.

G. J. Phillips, M.A., Ph.D., B.Sc., A.M.I.E.E., who writes in this issue on discriminator bandwidth in f.m. broadcast receivers, joined the B.B.C. engineering division in 1951 after post-graduate work on ionospheric measurements at the Cavendish Laboratory, Cambridge. Dr. Phillips has been engaged on B.B.C. transmitting aerial design and is now in charge of receiver and measurement work in the B.B.C. research department at Kingswood Warren, Surrey.

Sqn. Ldr. G. de Visme, B.Sc., Grad.I.E.E., contributor of the article on a phase indicator, took his degree at London University in 1942 and then spent four years in R.E.M.E. After demobilization he worked for two and a half years in the G.E.C. research laboratories, and then in 1950 joined the education branch of the R.A.F. He is now instructor in electronics at the R.A.F. Technical College. Since joining the air force he has obtained a diploma in electronics from Southampton University.

OBITUARY

James P. McKenzie, M.C., A.M.I.E.E., chairman and managing director of Sifam Electrical Instrument Co., Ltd., died on October 9th at the age of 68. After the first world war he was for a short time with Elwell Radio before joining Standard Telephones & Cables. He later became sole British agent for the French company Société Industrielle pour la Fabrication D'Appareils de Mesure and when in 1927 tariffs made the import of instruments prohibitive he formed the present Sifam company using the name by agreement with the French company.

James G. Yates, who since 1946 has been a lecturer in the Department of Engineering at Cambridge University, where he did "outstanding work in building up the teaching of electronics," died on November 1st, aged 42. A graduate of Trinity College, Dublin, he joined the Radar Research and Development Establishment at Christchurch in 1940, where he worked throughout the war.

Lionel W. Sansum, secretary and director of A. F. Bulgin & Co. for over 30 years, died on October 15th,

F.M. Discriminator Bandwidth

By G. J. PHILLIPS, M.A., Ph.D.
B.Sc., A.M.I.E.E.*

ITS SIGNIFICANCE IN
HIGH-QUALITY BROADCAST RECEPTION

FROM time to time in the technical literature the advantages have been discussed of a f.m. discriminator which remains linear over a bandwidth very much in excess of the deviation range of the signal being received¹. Some of these articles give the impression that wide-band discriminators offer a clear advantage in all f.m. applications, and can give a useful reduction of many types of interference. It is the purpose of this article not only to discuss those aspects in which better performance can be achieved by this means, but to review all aspects of the performance in relation to the requirements of a broadcasting service. Interest in wide-band discriminators was at one time aroused by the possible use of f.m. for long distance short-wave communication², but it is more convenient for discussion to consider

* B.B.C. Engineering Research Department.

¹ See for example "F.M. Receiver Design," by Lawrence W. Johnson, *Wireless World*, October 1956, p. 497.

² Argumbau, L.B., and Granlund, J., "Sky-Wave F-M Receiver," *Electronics*, December 1949, p. 101.

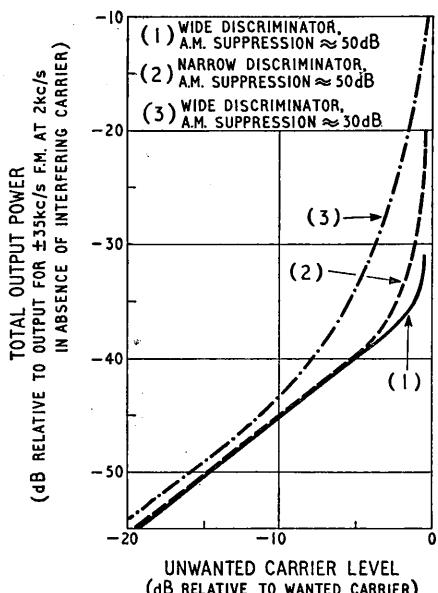


Fig. 1. Power output due to co-channel interference as a function of carrier ratio. In taking these curves the wanted carrier was unmodulated, and the interfering carrier was modulated with ± 35 kc/s deviation at 2 kc/s. An aural weighting network was used in front of the power meter. The narrow discriminator with approximately 30 dB a.m. suppression ratio gave a curve practically identical with curve (3).

first the interference that can arise between two separate f.m. transmitters operating on the same channel—i.e., co-channel interference.

Co-channel Interference.—We shall suppose, in discussing the interference heard when listening to the stronger of two co-channel transmissions, that two different programmes are being radiated. On any given receiver, assuming the signal strength is adequate, the interference will depend on the level of the interfering carrier relative to the wanted carrier. Before going any further we should have some idea of the kind of noises that will mar the wanted programme. There are two distinct forms of interference. First, the unwanted modulation may be recognizable in the background and secondly, there may be a characteristic "swishing" noise.

The so-called capture effect is concerned with the first type of interference only. If the unwanted carrier is equal in strength to the wanted carrier the two programmes will be equally audible, but as the unwanted carrier is reduced the unwanted modulation rapidly becomes fainter. The ratio of carrier levels at which it just becomes inaudible is termed the capture ratio. Now it is sometimes assumed that interference troubles are over at this stage, but this, alas, is not so. There remains a noise which (except when there happens to be a pause in both programmes) might be described as a "swishing" or "fizzing" noise. This second type of interference unfortunately remains audible for a much smaller unwanted carrier level than that existing at the "capture" stage, and arises from a beat effect between the two f.m. signals. Both amplitude and phase modulation of the wanted carrier result from the addition of a weaker carrier of a slightly different frequency, but interference is normally reproduced in a f.m. receiver by virtue of the phase modulation component. In the absence of modulation on either carrier a steady beat note corresponding to the transmitter frequency difference is expected—though in practice some warbling of the note will occur. But if either or both of the carriers are deviated the swishing noise is produced as the frequency difference passes rapidly through the audible range.

The dependence of the total interference power on the carrier ratio is shown by the experimental curves in Fig. 1. They all refer to measurements made with a special receiver in which the bandwidth before the limiter was kept at ± 100 kc/s. Limiting was achieved in two stages, giving a very good degree of a.m. suppression. A Foster-Seeley discriminator was used which was linear over a bandwidth of at least ± 1 Mc/s, but, in order to obtain precise discriminator bandwidths, either a wide (± 1 Mc/s) or a narrow (± 120 kc/s) band-pass filter could be inter-

posed between the limiter and the Foster-Seeley circuit. Two signal generators were used, the outputs of both being fed to the receiver; an unmodulated carrier was used to represent the wanted transmission and a carrier with ± 35 kc/s f.m. at 2 kc/s was varied in level to represent a modulated interfering signal. Under these conditions the receiver output power represents the interference and has been plotted against the level of the unwanted carrier. The two alternative discriminator bandwidths were used with the full limiting maintained, curves (1) and (2). In addition, the wide-band condition was measured with the limiting efficiency reduced to that of a fairly good domestic receiver for f.m. reception, curve (3).

It is seen that in all cases there is at first a straight-line region where the interference is proportional to the unwanted carrier level; this occurs where the latter is relatively small and only the "swishing" noise is present. Curve (1) shows that, given good limiting and a discriminator of ± 1 Mc/s bandwidth, the interference remains proportional to the unwanted carrier level until a carrier ratio of about 2 dB is reached. At this point breakthrough of the unwanted modulation begins to reinforce the other interference and the curve begins to rise more steeply; this is the "capture" threshold. If the discriminator is narrowed to ± 120 kc/s this threshold occurs at a lower level of the unwanted carrier as shown by the earlier rise of curve (2). The effect of reduced limiting efficiency, as shown by curve (3) for the wider discriminator, is two-fold: (a) earlier onset of the breakthrough of unwanted modulation and (b) increased interference at all carrier ratios. The curve for the narrow-band discriminator with reduced limiting is not shown here—it was found to coincide within 1 dB with that for the wider discriminator; no significant difference between the discriminators was apparent, due presumably to the restriction in performance now imposed by the limiter. In all cases the graphs continue as straight lines at 45° for unwanted carrier levels lower than those plotted in Fig. 1, until receiver noise in the output becomes comparable with the power being measured.

In a communication system we wish to make the best of the situation even when the carriers are nearly equal. It is then worth while paying considerable attention to limiting efficiency. Then, but only then, a wider discriminator can be used to gain some further advantage. On the other hand, for a broadcasting service a 20 dB carrier ratio is not sufficient to give reasonably interference-free reception. This may seem an incredible statement when Fig. 1 shows that a signal-to-interference ratio of some 55 dB occurs for a 20 dB carrier ratio. But that is the startling thing revealed by experiments on co-channel interference—the small amount of it, in terms of audio power, that can spoil reproduction, particularly of music; this is true whether or not the modulation on the unwanted carrier corresponds to the same programme. Now Fig. 1 shows that for an unwanted carrier at or below the -20 dB level the various arrangements differ in performance by no more than 1 dB. This includes a narrow-band discriminator with an a.m. suppression ratio³

³ The a.m. suppression ratio used here is defined as the ratio of the output due to the f.m. to that due to the a.m. when a signal having 40% a.m. at 2,000 c/s simultaneously with ± 30 kc/s (40% of 75 kc/s) f.m. at 100 c/s is fed to the receiver. Its measurement has been discussed by G. G. Johnstone in the August 1957 issue of *Wireless World*, p. 378.

of about 30 dB, since it performs substantially as shown by curve (3).

Should the a.m. suppression ratio be less than 30 dB the story is rather different. Extra interference is produced for all carrier ratios. This is because, when an audio-frequency beat is produced, it is not only the phase modulation of the resultant of the two carriers that matters; amplitude modulation also can contribute appreciably to the interference at the receiver output.

Multi-path Distortion.—Another phenomenon closely related to co-channel interference is distortion arising from multi-path propagation. With a very large path difference, in fact, the physical conditions are virtually the same as for co-channel interference when there are two stations some distance apart broadcasting the same programme. Fortunately, this has been anticipated in f.m. station planning since (without allowing for any further advantage possible by a directional aerial) it is intended to secure a carrier ratio of at least 20 dB between co-channel stations for 99% of the time when in the appropriate service area. It is not surprising, therefore, to find that a delayed signal some 20 dB below the direct signal causes distortion when the path difference is greater than about 5 miles. This distortion is particularly noticeable on piano music. It changes somewhat in character as the path difference changes from, say, 20 miles (when it takes the form of a fizzy noise like co-channel interference) down to 5 miles (when it becomes almost indistinguishable from the effect of something loose in the loudspeaker). It should be added that the shorter the path difference (below about 20 miles) the larger the delayed signal that can be tolerated, so that reflections with only 1 mile or less path-difference must exceed a half of the direct signal in amplitude to give appreciable distortion. This is because the frequency of difference between the direct and delayed signals arriving at the receiver can no longer be very great, and so a frequency high compared with that of the modulation cannot be produced. This subject has been discussed more fully by M. G. Scroggie in a previous issue⁴.

Regarding co-channel interference and multi-path distortion, experience has shown an a.m. suppression ratio of 35 dB to be a good target to aim at in receiver design; given this, receivers with discriminators of ordinary bandwidth will not under conditions applicable to broadcasting show appreciably greater interference than a more elaborate receiver. Any interference will be predominantly that corresponding to the audio component of the phase modulation of the resultant signal. Further improvements in difficult situations must rely on suitable orientation of a directional receiving aerial.

Impulsive Interference.—Turning now to impulsive interference, Fig. 2 gives the result of measurements using the experimental receiver with full limiting. Short impulses of controllable amplitude were applied to the input of the receiver at a constant rate, a fairly high rate (2,500 per second) being used to facilitate measurement of the interference when using impulses of small amplitude. They were applied in the presence of a f.m. carrier to which the receiver was tuned. The output power due to the

⁴ See "F.M. Multi-Path Distortion," *Wireless World*, December 1956, p. 578.

impulsive interference has been plotted against the amplitude of the impulses.

The difference in performance of the two discriminators is small, being no more than a few decibels at all levels of interference. Moreover, for repetition rates met in practice, the amount of interference heard when the impulse amplitude is less than the peak carrier amplitude is not serious. The region of importance is therefore when the impulses are greater than the threshold value marked in Fig. 2, and there the wide-band discriminator gives slightly more interference than the discriminator of conventional bandwidth. The effect of reducing the a.m. suppression ratio is not shown here; a moderate reduction merely gives a more gradual step at the threshold. Generalizations in the case of impulsive interference are difficult to make since factors other than discriminator bandwidth and a.m. suppression

put of the ideal limiter, being purely f.m., has sideband amplitudes which are symmetrical about the carrier frequency (principally two equal components at ± 200 kc/s relative to the carrier in the case being considered). With an ordinary Foster-Seeley discriminator one diode is mainly sensitive to the component 200 kc/s higher than the wanted carrier in frequency, and the other to the component 200 kc/s lower. The contributions of the diode circuits to the final output are of opposite polarity. With no modulation on the wanted carrier the extra outputs of the diodes due to interference should, by symmetry, be equal in magnitude and therefore cancel. This will apply even when the interfering carrier varies in frequency or amplitude due to modulation. With deviation of the *wanted* carrier frequency the situation is not so straightforward, and cancellation will not generally be complete.

In practice we may say that besides i.f. selectivity, various departures from the ideal both in limiter performance and in symmetry of the discriminator play a part in adjacent channel protection. More experimental work is needed to be able to decide how important these are. There is as yet no evidence that the use of a wide-band discriminator will help with this form of interference; in fact its greater sensitivity to ± 200 kc/s components may result in more interference for a given degree of symmetry. There would seem to be a good case, however, for a limiter which is efficient in suppressing amplitude fluctuations up to a few hundred kilocycles per second. This will make the best of available selectivity though, as stated above, an improvement in the i.f. selectivity curve is always capable of giving less interference. A *slope* of the amplitude response curve of the i.f. stages at 200 kc/s from the carrier frequency can play a part by causing the effective strength of the interfering carrier to vary as it is deviated by modulation; the *shape* of the response curve as well as the attenuation at the adjacent channel frequency must therefore be considered.

Conclusions.—A wide-band discriminator reduces co-channel interference only when the unwanted carrier is comparable in strength with the wanted carrier. This means that in conditions where the improvement due to the wide-band discriminator is becoming important the background interference is then too high for a satisfactory broadcasting service. Expressed in another way, a significant improvement using a wide-band discriminator is achieved only when the wanted-to-unwanted carrier ratio is less than about 6 dB. But it is not until an interfering transmission or a long-delayed echo is more than 20 dB below the wanted signal that reproduction becomes sufficiently free from background noise or distortion to be acceptable for a broadcasting service; in certain critical cases a carrier ratio greater than 30 dB is needed to avoid noticeable effects. Moreover the limited improvement mentioned above can be achieved only at the expense of considerable complication in the receiver; for optimum performance of a wide-band discriminator the a.m. suppression ratio must be at least 50 dB.

On the other hand if conditions are restricted to those encountered in broadcast reception a narrow-band discriminator and an a.m. suppression ratio of 35 dB are generally satisfactory, and no significant improvement is to be obtained from a wide-band discriminator and increased a.m. suppression. A practical point worth noting here is that a.m. sup-

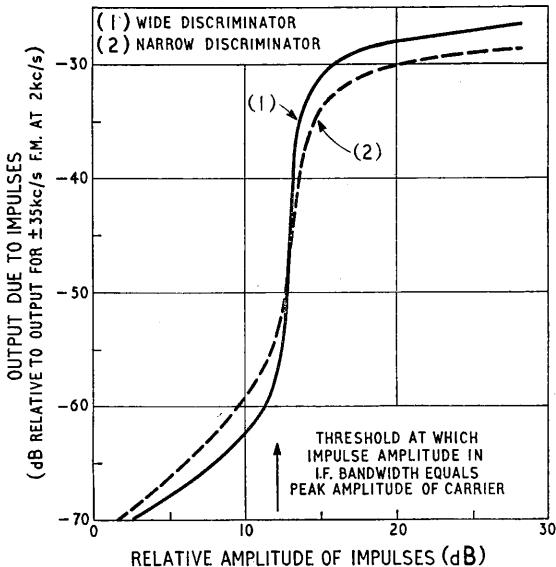


Fig. 2. Input/output characteristics for impulsive interference. The measurement was made in the presence of a carrier with ± 30 kc/s f.m. at 50 c/s, the 50 c/s output being eliminated by a high-pass filter. The impulse repetition frequency was 2.5 kc/s.

ratio are involved. For example, some receivers employing a ratio detector have been found less susceptible to impulsive interference than a receiver with a limiter and a Foster-Seeley discriminator, although the measured a.m. suppression ratio was inferior in the ratio detector receivers. A limiter before a ratio detector does not necessarily lose this advantage under impulsive interference conditions, and can improve the performance with other forms of interference.

Adjacent-channel Interference.—Adjacent-channel interference (due to a transmission with a carrier frequency differing by 200 kc/s from the frequency of the wanted carrier in the case of broadcasting) can of course always be reduced by improvements in the i.f. selectivity. The selectivity should be sufficient to ensure that the interfering carrier is fairly small compared with the wanted carrier at the stage where limiting takes place. Then a good limiter and a symmetrical two-diode discriminator can in theory provide good protection. This is because the out-

pression may vary considerably with small changes in tuning in the case of some receivers. A receiver should therefore be designed to ensure that the suggested a.m. suppression ratio is reached or exceeded when tuned under normal conditions, since it is seldom practicable to tune for best results in the presence of co-channel interference or multi-path distortion.

Regarding other forms of interference, several aspects of receiver design are usually involved and

the importance of some of these are still being studied. But there does not appear to be any clear advantage in using a wide-band discriminator and in one case at least (impulsive interference) its performance appears, if anything, to be poorer than that of more conventional arrangements.

I am grateful to various colleagues for their helpful discussion, in particular Mr. J. G. Spencer who also made available the experimental results which form the basis of the curves of Figs. 1 and 2.

ИСКУССТВЕННЫЕ СПУТНИКИ ЗЕМЛИ

ARTIFICIAL SATELLITES OF THE EARTH

Observations by Radio on the First Transmitters Beyond the Ionosphere

T

HERE was great excitement in the world of radio on October 5 when it was learnt that the Russians had launched their first satellite. In spite of much previous discussion on the reception of satellite signals*, the actual event took everyone by surprise. Observing stations were hastily improvised from existing equipment by amateurs and professionals alike. The B.B.C. used their listening station at Tatsfield, the D.S.I.R. their radio research establishment at Slough, and the G.P.O. their measuring stations at Baldock and Banbury. At the same time the radio astronomers at Cambridge and Jodrell Bank worked furiously to rig up equipment for precise position-finding measurements on the actual track of the satellite, while similar measurements were started immediately by the Royal Aircraft Establishment, Farnborough, and at Malvern by the Royal Radar Establishment. Between these official organizations and the many amateurs who made observations were bodies like the British Astronomical Association, whose Radio Section took recordings of the signals at their small station at Clacton.

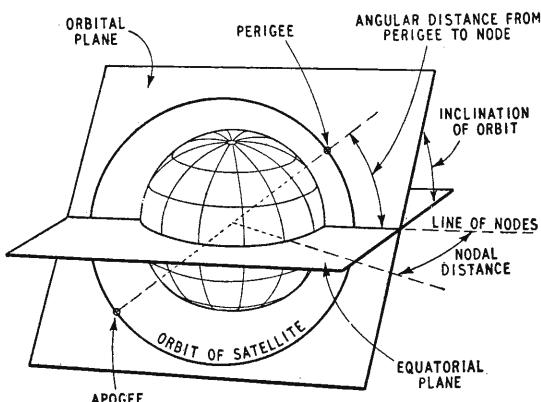
Nobody in this country was prepared for the use of 20Mc/s and 40Mc/s as the transmission frequencies because it was expected that the American satellite, using 108Mc/s, would be the first to be launched. This state of unpreparedness should never have existed, however, for the frequencies were published in the June, 1957, issue of the Russian journal *Radio*, which is available in this country, and were officially notified to the Royal Society in the following August. The June issue of *Radio* contained two articles (from the first of which our title is reproduced) mainly giving advice to amateurs for observing the satellite. The first begins:—

"During the course of the International Geophysical Year it is intended in the U.S.S.R. to launch

a number of artificial satellites of the earth, equipped with radio-transmitting apparatus. Radio observers of the signals from these satellites will make it possible to obtain fresh data regarding the structure of the ionosphere and to determine with accuracy the size, shape and position of the orbits of the satellites, and also to draw conclusions regarding the processes and occurrences taking place in the satellite during the course of its flight."

The second article mentions the use of two radio transmitters "having frequencies of approximately 20Mc/s and 40Mc/s, and the power of the transmissions will be approx. 1W. These transmitters will operate continuous over a long period (this period being limited by the sources of electrical power contained in the satellite). Consequently, the special radio reception points as well as radio amateurs throughout the whole of the territory of the Soviet Union as well as countries abroad will be able to receive time and time again the radio signals

Fig. 1. Elements of the orbit of an artificial satellite.
(Reproduced, with acknowledgments, from *Radio*.)



* Going back as far as 1945 in this journal. See, for example, "Extra-Terrestrial Relays," by Arthur C. Clarke, October, 1945, issue.

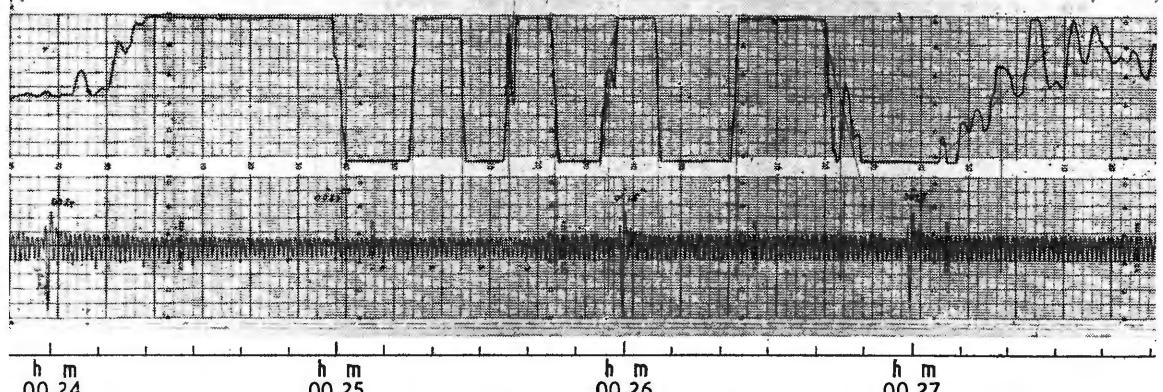


Fig. 2. Record of interferometer output taken from Sputnik I's 40-Mc/s transmission at Cambridge on October 6. The lower waveform is a timing reference, and the 1-minute and 10-second intervals are shown on the scale below the chart.

transmitted by the equipment mounted in the satellites.

"The signals given out by the transmitters in the satellites will be similar to telegraphic strokes having a length of from 0.05 to 0.7 seconds. The transmission will be arranged to proceed in such a manner that one transmitter will be heard during the interval in the transmission of the other."

Of course, we know now that the actual pulse duration was approximately 0.3 second, on both frequencies in the first satellite and on 20Mc/s in the second satellite. Moreover the frequencies proved to be 20.005Mc/s and 40.002Mc/s—the increments of 0.005 and 0.002 being made probably in order to generate audio beat frequencies of 5kc/s and 2kc/s with local oscillations of 20Mc/s and 40Mc/s at the ground receiving stations. We know also that the 23-inch aluminium-alloy sphere of the first satellite carried four projecting rod aerials of 2.4-2.9 metres in length, which were folded back against its body during the flight in the rocket but afterwards swung out on swivels to their correct positions. The 184-lb weight of Sputnik I was said to have been largely made up by the weight of the batteries, which have been estimated as supplying a power of 10-30 watts.

The second satellite is reported by the Russians to contain a great deal more telemetering equipment—for measuring temperature and pressure, cosmic rays, electromagnetic radiation from the sun in the short-wave, ultra-violet and Röntgen regions, and also various physiological parameters from the passenger dog. Very little is known at present on the precise method of modulating all this information on to the radio frequencies, but it is likely that some time-sharing system is used, even though two carriers are available.

Pulse Recurrence Frequency

In Sputnik I, it was stated by the Russians that the mark/space ratio of the pulses was modulated and also "the frequency of the telegraphic messages". Whether this meant the radio frequency or the pulse recurrence frequency was not clear. The B.B.C. at Tatsfield noted a gradual increase in p.r.f. from 108 pulses per minute to 150 per minute before the keying on 20Mc/s stopped altogether on October 7. In the second satellite the keying on

20Mc/s stopped on November 3, leaving both transmissions in continuous operation.

Most people are by now familiar with the general nature of the orbits of the two satellites, but before passing on to the radio astronomy measurements it may be as well to look briefly at the basic astronomical parameters involved. For this purpose we quote from the June issue of *Radio* mentioned earlier.

Elements of the Orbit

"In consequence of the ellipticity of the orbit, the height of the satellite from the earth will vary during one revolution; the point at which the height of flight is maximum is called the *apogee*, whereas the point of minimum height is called the *perigee*. In order to be able to determine completely the shape, size and position of the orbit of such a satellite, it is sufficient to have a knowledge of five different magnitudes (Fig. 1): the height of the perigee, the height of the apogee, the inclination of the orbit (i.e. the angle which the plane of the orbit makes with the plane of the equator), the distance between the nodes (i.e., the angle which the line crossing the orbital plane and the equator makes with a given celestial line also lying in the plane of the equator—the line fixed by the vernal equinox) and, finally, the angular distance between the perigee and the node.

"These magnitudes are called the elements of the orbit; they provide the fundamental data required for determining the number of revolutions within a 24-hour period. They will have to be determined as many times as possible in order to ascertain the variations which will occur in the satellite's orbit† before it reaches the point at which it begins to fall rapidly and finally disintegrates.

"... The orbital plane of the satellite does not share in the rotation of the earth, whereas the observers, who are located on the surface of the earth, naturally follow the rotation of the earth from west to east. ... During the time of one rotation of the artificial satellite (which will probably be approximately 1.5 hours) an observer located on the equator would be moved 2500 km towards the east,

† "As a result of the resistance of the atmosphere and also as a result of deviations of the pull of gravity from a central direction, the elements of the orbit will be gradually altered."

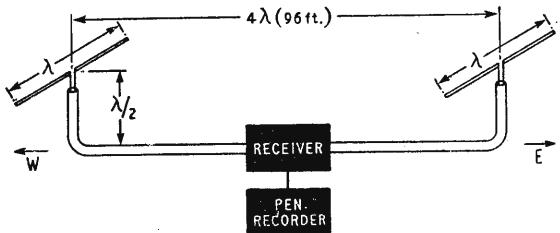


Fig. 3. Schematic of the 40-Mc/s interferometric aerial system at Cambridge. It was actually modified from a 38-Mc/s radio telescope used on radio stars.

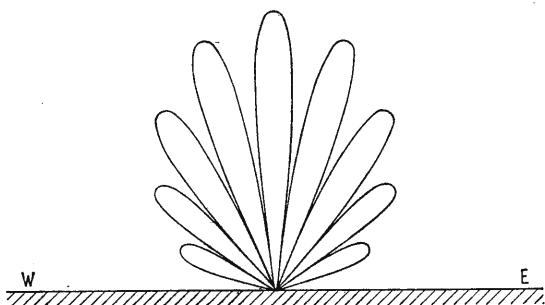


Fig. 4. General form of the interference-pattern type of polar diagram produced by the spaced aerial system in Fig. 3.

whereas an observer situated at a latitude of 45° would be moved 1760 km and an observer situated at a latitude of 60° would be moved 1000 km. The northern and southern limits of observation are determined by the inclination of the orbit of the satellite, which defines how far the satellite will move either to the north or to the south. During every period of twenty-four hours the artificial satellite will make 16 revolutions round the earth and in so doing will make, as it were, a regular pattern or 'network' over the earth's surface. The satellite to be launched in the U.S.S.R. will travel in such a manner that it will pass over practically every inhabited region of the earth.

"The time during which it will be possible at any given point on the earth's surface to pick up radio signals from the artificial satellite will be determined by the speed of the satellite (8 km per second) and the greatest distance at which it is possible to receive the signals transmitted. The time for receiving signals will probably last for several minutes."

The "several minutes" in the last paragraph is illustrated in practical terms in Fig. 2, which is one of the first recordings of Sputnik I's signals taken at the Mullard radio astronomy observatory at Cambridge. It was obtained at night in the first hour of October 6, and occupies a total time scale of nearly 5 minutes. This record is actually the output of a receiver fed from interferometric type of aerial system of the kind already described in *Wireless World*.^f Two spaced dipoles are used, as shown in Fig. 3, giving an interference pattern consisting of multiple lobes as in the polar diagram Fig. 4. A source of signals like a satellite passing through this pattern therefore produces an output from the receiver which goes through maxima and minima of the kind shown on the record.

^f "Radio Astronomy," July, 1951.

At any particular height above ground a plan view of the minima between lobes in Fig. 4 takes the form of a hyperbolic pattern, as shown in Fig. 5. The actual positions of these lines are established of course, from a knowledge of the geometry and geographical positioning of the aerial system (which is arranged on an accurately surveyed east-west line). Similar hyperbolic patterns can be drawn for all heights above ground. Thus, from the time intervals between minima on the Fig. 2 record and the roughly known velocity of the satellite (derived from the period of rotation), it is possible to calculate a series of points with particular spacings on a straight line that will fit on to one of the hyperbolic patterns. In this way the track of the satellite relative to the aerial system can be found, as shown in Fig. 5, while the hyperbolic pattern in use will give the height.

Measurements of this kind were made not only at Cambridge (on the 40Mc/s transmission) but also by the Royal Aircraft Establishment and the Royal Radar Establishment, both of whom used crossed interferometric aerial systems. All three establishments in addition took measurements of the changes in frequency produced by the Doppler effect. The results were used for calculating the velocity of the satellites and also for obtaining ranges from which the tracks could be obtained for correlation with the interferometric methods. To explain how the Doppler method is used to obtain this velocity and range information we again give a direct quotation from the *Radio* articles.

"The Doppler effect is concerned with the variations in frequency which are produced when the transmitter and receiver approach one another or move further apart from one another. The known principle is that when the source of the waves and the receiving station approach one another the frequency observed is higher than the emitted frequency. Conversely, if the transmitter and the receiver are receding from one another, the frequency as received will be lower than that emitted.

"The speed of approach or recession of the satellite will vary according to a special pattern on account of the elliptical shape of the satellite's orbit. It will readily be seen that it is not merely a ques-

(Continued on page 577)

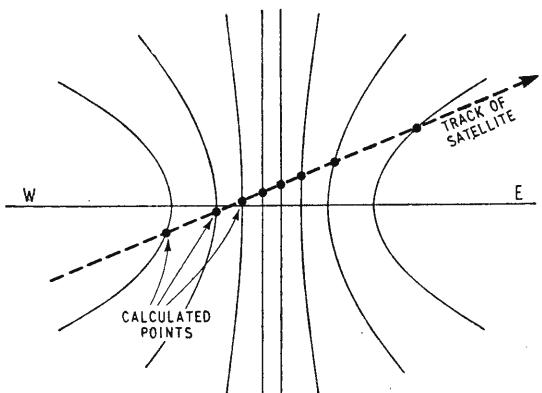


Fig. 5. Plan view of a horizontal plane cutting through the interference pattern in Fig. 4 at a particular height. The hyperbolae represent the minima between lobes. The calculated points are fitted to these hyperbolae to give the track of the satellite.

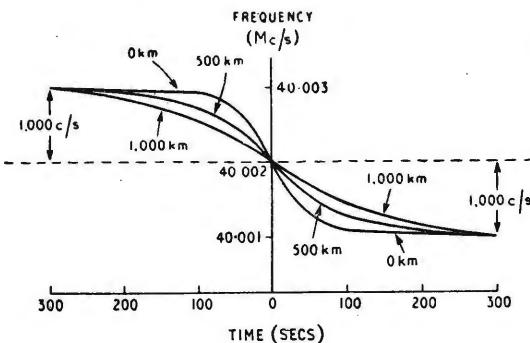


Fig. 6. Curves showing change of received frequency with time produced by the Doppler effect as a satellite approaches and recedes from the receiving station. The three curves represent transits at different ranges. The transmitted frequency is 40.002 Mc/s. (Reproduced from Radio.)

tion of approaching in a straight line at constant velocity and then passing the observer station and receding at the same constant velocity. The speed in relation to the receiving station will vary according to the angle of the particular section of the orbit in relation to the point of observation. When the angle between the direction of movement of the satellite and the direction of the waves received by the receiving station is greater than 90° , the satellite commences to recede from the receiver; the velocity of this motion of recession gradually increases and reaches its maximum before the signals cease altogether. At first the signal will be found to have its maximum frequency, and then when the satellite gets near to the reception point the frequency will decrease somewhat, and finally, when the satellite is moving away from the observer, the frequency will decrease down to the minimum. This is shown in diagrammatical form in Fig. 6.

"The period during which the frequency change due to the Doppler effect will be noted will last for two to three minutes and consequently it is essential to be ready for measuring any differences before the satellite comes into range."

At Cambridge the frequency changes were measured by heterodyning the incoming satellite frequency of 40.002 Mc/s with a local 40-Mc/s oscillator and comparing the resultant audio beat note with an equivalent signal from a calibrated variable a.f. oscillator. The comparison of audio frequencies was done by ear and by keeping a Lissajous figure stationary on a c.r. tube display. Readings were taken at 3-second intervals, to obtain graphs of the kind shown in the Russian diagram Fig. 6. As indicated, the total frequency change on 40.002 Mc/s was about 2 kc/s, taking place over periods of about 2 to 10 minutes or more, depending on the range. It will be noticed that the frequency transition occurs rapidly at short ranges and slowly at long ranges.

From the Doppler law relating the rate-of-change of the curve to the distance of the observer it is possible to calculate the actual range of the satellite on a particular transit. Measurements on two successive transits will then give the track and height by triangulation. At Cambridge the results of these Doppler observations were combined with those of the interferometric methods, and, as is well

known, figures for the various parameters illustrated in Fig. 1 were obtained with extreme accuracy.** The inclination of the orbit was found to within ± 10 minutes of arc, for example, the period of rotation to within ± 0.3 seconds and the heights at the apogee and perigee to within ± 10 kilometres. This was a remarkable achievement.

When the signals from Sputnik I ceased, greater attention was naturally focused on the radar observations. These were made at the Jodrell Bank radio astronomy establishment, using the giant 250-ft diameter radio telescope, and at the Royal Radar Establishment, Malvern, with a new 45-ft radio telescope.

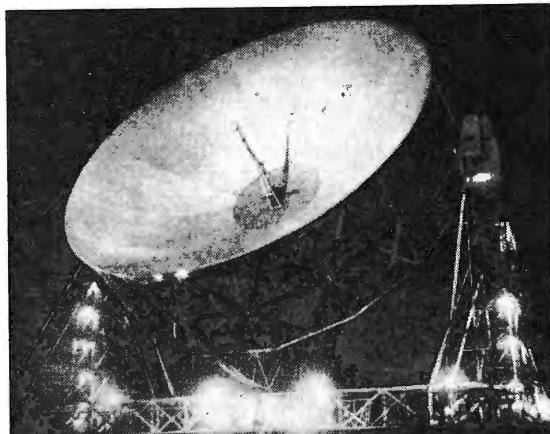
Ranges by Radar

Jodrell Bank operated with two radar transmitters. The first, on 36 Mc/s, had a peak power of 10 kW, a pulse duration of 150μ sec and a p.r.f. of 75 per second. The second, working on 120 Mc/s, also had a peak power of 10 kW, with a pulse duration of 2 msec and a p.r.f. of 10 or 20 per second. When observations were made on the orbiting rocket belonging to Sputnik I, the range of detection on 120 Mc/s was limited only by earth curvature, and adequate signal/noise ratios were obtained at ranges of over 900 miles. The pencil beam of the 250-ft paraboloid has a calculated angular width of about $2^\circ - 3^\circ$ at 120 Mc/s and about 8° at 36 Mc/s, while the calculated power gains at these frequencies are respectively 6,500 and 600. A much finer pencil beam was used at Malvern—only 0.5° in angular width—obtained with a frequency of 3,000 Mc/s. Here, ranges of over 800 miles were reported on the rocket.

At the D.S.I.R. station at Slough and the B.B.C. station at Tatsfield, some interesting observations were made on the maximum ranges at which the satellite signals could be heard. With Sputnik I the signals were received for about 30-35 minutes on each satellite transit, which suggested that they were coming from far beyond the optical horizon (about 2,000 miles range) where one would not normally expect to hear them. In fact the range was about 4,000 miles. The probable explanation for this

** See for example "Radio Observations of the Russian Earth Satellite," *Nature*, November 2, 1957.

The 250ft steerable radio telescope used at Jodrell Bank Experimental Station for observing the satellites by radar techniques.



is, of course, that the waves from the satellite transmitter were refracted by the ionosphere (through which they would pass from outside) in such a way as to bend them round the curvature of the earth. The ionosphere was also no doubt responsible for the curious short burst of 20Mc/s which usually occurred before the main signal was received. At Slough most of the measurements were, in fact, done on 20Mc/s because of the greater effect of the ionosphere on that frequency. At Cambridge, on the other hand, they used mostly 40Mc/s in order to avoid the inaccuracies introduced by the ionosphere in the position-finding measurements.

Signal Strengths

Many different aerials were pressed into service by the B.B.C. at Tatsfield—open-wire types, horizontal rhombics, double rhombics, vertical "V"s, short-wave stacks—while receivers were standard communication types with beat frequency oscillators. Both signal-strength and frequency measurements (for Doppler calculations) were made. With the first satellite the signal strength was occasionally as high as $35\mu\text{V/m}$ during the first few days, but most of the time was only just above noise level. The signal from the Sputnik II was much weaker, as might be expected from the greater range, and was generally less reliable.

The variations recorded in the signal strength were, in fact, one of the most complex aspects of the satellite transmissions. There were several different periodicities in these fluctuations and a number of possible reasons for them. The report from Cambridge in *Nature*** mentions three likely effects: (a) rotation of the radiation patterns of the satellite's aerials by the spinning of the satellite; (b) changes of polarization in any plane-polarized component of the transmitted signal also produced by the spinning of the satellite; (c) changes of polarization caused by Faraday rotation†† in the ionosphere resulting from the earth's magnetic field. The June issue of the Russian journal *Radio*, incidentally, comments on the expected variations as follows:—

"... At some points in its movement the aerials of the satellite will be located in such a way that the wireless waves reaching the aerial of the receiving station will have a circular polarization. At other times the aerials fitted to the satellite will be pointing straight in the direction of the receiving aerials of the observer station, so that the waves reaching the receiving station have a linear polarization."

To distinguish between these possible effects the Cambridge observers fitted up receiving aerials with mutually perpendicular planes of polarization. It was then found that the fading patterns on the two aerials differed in phase by $\pi/2$, showing that the rotation of the plane of polarization was the most important cause of the signal fluctuations. To distinguish between the rotation due to spinning and that due to the Faraday effect, they made observations of the fading periodicities on both 20Mc/s and 40Mc/s. The significance here is that the Faraday rotation is proportional to the square of the wavelength, and, therefore, produces more rapid fading on 20Mc/s than on 40Mc/s. The fading due to the spinning of the satellite, however, is independent of frequency.

Curves have been plotted of several of the period-

icities of fading against G.M.T. for both the 20-Mc/s and the 40-Mc/s signals. The two curves for a particular satellite transit coincide more or less exactly if the periodicity scale on 20Mc/s is arranged to represent values four times as big as those on the 40-Mc/s periodicity scale. In other words, at twice the wavelength the fading periodicity is quadrupled—which shows that the periodicity is proportional to the square of the wavelength and supports the hypothesis that some of the fading is, in fact, due to Faraday rotation.

The Cambridge observers also say in *Nature* that their fading periodicity measurements indicate that Sputnik I was spinning at seven revolutions per minute. It has been noticed that this spin fading is accompanied by a marked irregularity in the Doppler curves. The effect, they say, may be caused by the periodic reversal of the sense of the circularly polarized component of the transmission as the satellite spins.

The Faraday rotation measurements, among others, are likely to be of great value in the studies of the ionosphere which form part of the International Geophysical Year programme. As an example, the electron density of the ionosphere is of great interest. The angle of rotation of the plane of polarization of the transmitted wave is determined by the total number of electrons along the "line-of-sight" path to the receiving aerial. Consequently, as the satellite moves along its track the length of the path through the ionosphere changes and also the number of electrons. This in turn produces a change in the angle of rotation of the polarization, giving an alteration of signal strength at the ground receiving station. Knowing the track of the satellite and the inclination of the earth's magnetic field to the "line-of-sight" path, it is possible to find the rate of change of electron content along this path.

Ionospheric Refraction

The existence of radio transmitters above the ionosphere at varying heights and at varying angles of elevation make possible other types of investigations. To quote again from *Radio*: "It must also be borne in mind that the signals received from the artificial satellite will have had to pass right through the ionosphere and in so doing will doubtless be subjected to refraction, both on entering and on leaving the ionosphere. . . . In turn, the amount of this refraction will depend upon the wavelength, so that the data received from all sources regarding the reception conditions of both signals on their different wavelengths will, when properly collated, supply further information regarding the structure of the higher strata of the earth's atmosphere."

As an example of this, the Cambridge workers mention in *Nature* measurements which allow the angle of refraction of the waves to be found at different angles of elevation. The angles of arrival of the 20-Mc/s and 40-Mc/s signals are measured by comparing the apparent times at which the source crosses the minima lines of similar interferometers working on these respective frequencies.

Preliminary measurements of this kind have already been done at Cambridge. They mark the beginning of a new era of scientific study, which has only been made possible by the tremendous technical achievement of placing these radio stations in space beyond the ionosphere.

†† A brief explanation of Faraday rotation was given in the December, 1956, issue, p. 595.

Satellite Observations for Amateurs

By O. J. RUSSELL,* B.Sc. (Hons.), A.Inst.P.

THE use of frequencies of 20 to 40 Mc/s in the Russian satellites opened up the possibility of large-scale amateur observations with gear already to hand in most amateur stations. It is hoped that some American satellites will also employ such frequencies in view of the larger numbers of amateurs who may participate. The original announcement that the American satellite project would use minimum power transmitters, requiring specialized aerial systems and very low noise-factor 108-Mc/s receivers, and would use equatorial orbits that would prevent any reasonable possibility of reception in these latitudes, had discouraged British satellite observing programmes. The Russian launchings have altered this situation drastically, and lead to the hope that American satellite projects will also enable observers to participate with easily obtainable equipment.

Receiving equipment for 20 Mc/s may be almost any type of conventional communication receiver. If well warmed up, such receivers will be stable enough for the Doppler shift measurements of velocity. A better solution is the use of a crystal-controlled converter (see Fig. 1), enabling the communication receiver to be used on a low frequency band—say 3 Mc/s, where stability will be enhanced, thus facilitating Doppler measurements. For 40 Mc/s a similar converter is ideal, and had information on frequencies been generally known, many such equipments would have been in use. However, most amateurs were able to utilize the 20-Mc/s channel straight away. For possible 108-Mc/s observations, a low noise crystal-controlled converter of the type used for 2-metre reception would be suitable. Such converters may be adapted from existing 2-metre converters.

Aerial systems may have any degree of complexity. A simple vertical aerial is ideal for Doppler and general long-range observation of the satellite signals. The all-round low-angle polar diagram of a vertical aerial is very suited to this work. The vertical may consist of a 12-ft vertical rod or wire, coaxially fed, and may be elaborated into ground-plane and similar aerial types. Tracking the satellites by the use of a rotating beam array is unlikely to be very accurate or satisfactory by "peaking" for maximum signal strength. However, by tracking on the minimum signal in an "end on" null, even a simple rotary dipole may be satisfactory. With conventional 21-Mc/s beams, it will often be found that the beam "works backwards," owing to the reflector becoming in effect a director on the lower frequency.

A simple minimum radio interferometer is shown in Fig. 2. For a vertical transit of the satellite, this will give three null positions, and ideally these are sufficient, if the velocity is known from Doppler measurements, to fix uniquely the height and track of a satellite. For other than a vertical overhead transit, the central null will lie on a straight line

but the other nulls will lie on hyperbolæ, as already shown in the previous article. If space is available greater separation of the dipoles of the interferometer may be used, so that more nulls may be obtained and the track fixed more certainly.

For the practical arrangement, triply folded wire

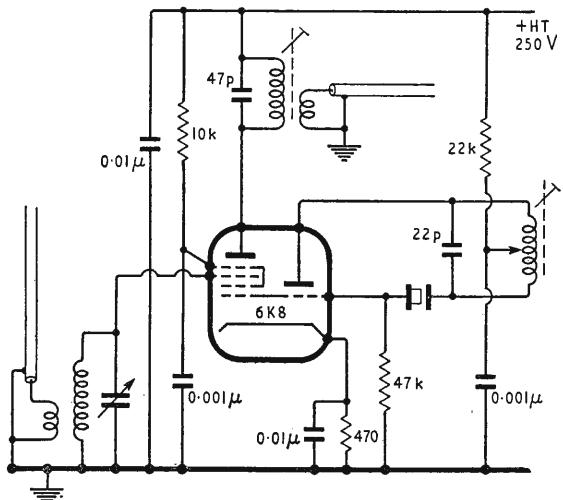


Fig. 1. A simple crystal-controlled mixer stage may be used as a frequency converter. A Squier type of overtone oscillator using the third harmonic will function with ordinary production crystals. For a 4-Mc/s i.f. a crystal with a 5.333-Mc/s fundamental will serve for 20-Mc/s reception, and a 12-Mc/s crystal will serve for 40 Mc/s. For optimum results an r.f. stage should be used in front of the mixer stage.

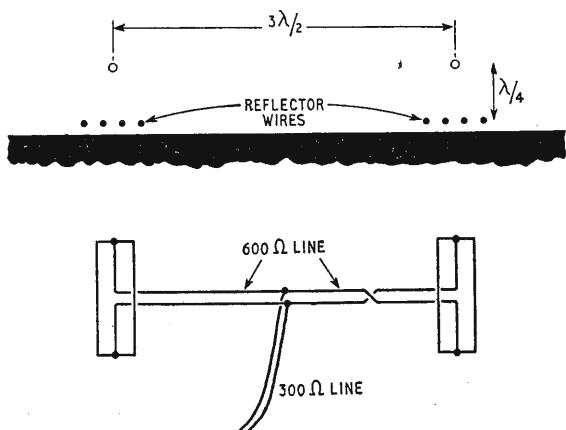


Fig. 2. Schematic of a simple interferometer aerial system giving three null points. At the altitude of the satellites the two outside nulls lie on hyperbolæ as shown in Fig. 5 of the previous article on page 576.

*Amateur station G3BHJ.

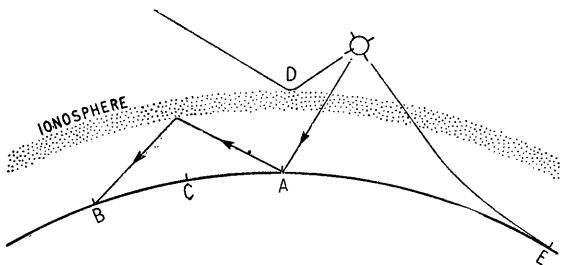


Fig. 3. Some possibilities in reception of satellite signals. At A the direct wave is received. B receives a ground and ionospherically reflected signal, while C is in a skip zone receiving no signals, as the direct ray is reflected into space at D by the ionosphere. At E atmospheric refraction extends the ground wave.

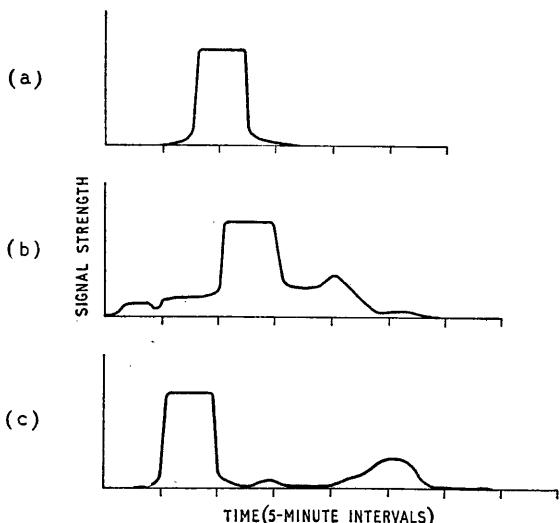


Fig. 4. Signals as received under varying ionospheric conditions. At (a) the signal is as heard with negligible ionospheric effects. At (b) some ionospheric reflection prolongs audibility. At (c) the satellite traverses a skip zone, and again peaks into good audibility after the true transit.

dipoles will match nicely into $600\text{-}\Omega$ spaced feeder line. The feeder line should be air-spaced, using light-weight spreaders. Wax impregnated dowel rods are light and quite suitable, being somewhat more convenient than heavy ceramic spacers. The physical centre between the two dipoles is used as the point to attach a $300\text{-}\Omega$ line to the receiver. By using the $1\frac{1}{2}\lambda$ spacing and transposing one $600\text{-}\Omega$ feed line as shown, the simplest possible interferometer giving a central null and two other nulls, one each side of it, is achieved in a reasonably small space. Two amateurs, both using such systems in directions at right angles to each other, will be able to obtain valuable data for track estimation, on the principles already described in the previous article.

For the 20-Mc/s frequency one wavelength may be taken as 49ft. The folded dipoles should be cut to a length 5% less than this, but being inherently broad-band a round length of 47ft will be satisfactory. They should be supported a quarter wavelength above four reflector wires which are half a

wavelength long and separated by 2ft from each other. The reflector wires need only be a few inches above ground level. For 40 Mc/s these dimensions may be halved. On this higher frequency the erection of interferometers of greater spacing will be facilitated, so that more nulls may be achieved and more "zero signal" observations made to obtain more useful data.

Signal observations may be made with any degree of elaborateness, ranging from simple "listening to the signal" upwards—depending on what equipment is available. At a close transit the optical-path condition for the first satellite was some 1,500-2,000 miles in either direction, so that the transmitters were audible in direct line-of-sight for a path length of about 3,000-4,000 miles. For less close approaches optical path conditions will be shorter. Under these conditions, representing little or no ionospheric transmission and the inaudibility of the WWV transmission, the signal suddenly leaps into audibility, peaks to a very strong value, maintained almost rock steady, and then rapidly declines to a weak signal. Having thus heard the signal appear on a dead band after hours spent listening to receiver noise was an eerie and exciting experience. Generally, once the signal has appeared, a weak signal is audible for some three or four minutes after it is beyond the optical horizon, under conditions of little or no ionospheric propagation. Under "good DX" conditions, with a high level of ionospheric ionization, the signal may undergo a number of vicissitudes, as shown in Fig. 3. Under such conditions the satellite signals may be heard well in advance of transit time, and long after. Some amateurs have followed the signals for upwards of an hour. Moreover the writer has heard the signal disappear, traverse a skip zone and again peak into audibility. Cross-observations on the strengths of the 20- and 40-Mc/s transmissions may thus yield valuable information about ionospheric conditions, as mentioned in the previous article.

For Doppler shift measurements a close transit is not necessary, for at 1,500 miles range the approach is practically head-on initially, and corrections that are quite small may be made if necessary. Moreover, in these latitudes even the correction for the rotational velocity of the earth is small, and will never exceed some 500 miles per hour. Aural estimates made by setting the receiver b.f.o. to zero beat and measuring the change in b.f.o. setting over a transit are unlikely to be better than within some 30-50 c/s. Moreover the sweep of the conventional b.f.o. is too wide to enable accurate calibration to be made. A very small variable capacitor of one or two picofarads connected from the b.f.o. valve grid to earth will give a vernier control which may be calibrated in cycles to enable accurate measurements to be made. A cathode ray tube comparison system using Lissajous figures, as mentioned in the previous article, will enable measurements to be made to less than a cycle. The "conversion factor" is almost precisely 1.5 cycles per megacycle of received frequency per thousand miles per hour. A more accurate figure is 1.491 cycles. Thus, on 20 Mc/s for a satellite velocity of 18,000 miles per hour, we should observe the frequency 540 c/s high when approaching end on, and 540 c/s low when receding end on.

Finally, the unexpected must always be expected in such observations. Undue reliance need not be placed upon newspaper reports. The transmissions from WWV on 20 Mc/s precisely provide exact

timing signals—and they also provide tone plus pulse transmissions which have deluded official and other observers unacquainted with such matters that they were hearing the "beeps" of the first satellite. The 1-Mc/s harmonic marker frequencies from a Class D wavemeter are also useful for locating the frequency, particularly as disturbed conditions have prevented WWV signals from being heard on many occasions.

Estimates of "tone" quality should also be made, as variations in this may well be due to frequency modulation telemetering. This, of course, is standard procedure, which has appeared in the popular newspapers as "mystery code signals baffle observers". The only mystery, however, has been the calibration scale and what particular variable was being measured.

Simple Measurement of Phase Difference

By Squadron Leader
G. de Visme, B.Sc.

DIRECT INDICATION OF $\sin \theta$ BY VALVE VOLTMETER

AMONG the number of methods which exist for measuring the phase difference between two sinusoids of the same frequency are the following:—

(1) Lissajous ellipses derived from the sinusoids are displayed on a cathode ray oscilloscope, and in terms of the ratio of vertical to horizontal extent thereof, the phase difference can be calculated. The amplitudes of the sinusoids have first to be equalized. The determination of which is the leading sinusoid presents a further problem.

(2) The phase of one sinusoid is advanced or retarded as necessary to bring it into phase, or anti-phase, with the other; the control for doing this may be calibrated directly in degrees.

(3) The sinusoids are separately squared, the resulting square waves added, and the final waveform rectified. The d.c. level of the rectified sum depends on the phase difference of the sinusoids, being zero for 180 degrees phase difference and a maximum for zero phase difference. The square wave amplitudes have to be equal to start with. Again, ambiguity exists as to which wave leads which.

(4) A modification of (3) exists whereby the square waves are differentiated, the resulting pulse trains being used respectively to switch each valve of an Eccles-Jordan relay. The mean

anode current of one or other of the valves is proportional to the angle of phase difference. Once again there is ambiguity as to which sinusoid leads which.

(5) One sinusoid is fed into a phase splitter, the two outputs of which (whose amplitudes must be equalized) are fed one to each of the anodes of two diodes connected as a balanced modulator. The other sinusoid is fed equally to each anode. The net output across the two diode loads in series is a (rather complex) function of the phase difference.

The above methods all suffer from one or more defects—either they are complicated, or frequency-sensitive, or the output bears a complex relation to the phase difference, or there is ambiguity as to which is the leading wave.

Basic Theory

The method to be outlined has the advantage of extreme simplicity and is, in theory at least, almost independent of frequency. The ambiguity as regards lead or lag still occurs, but a comparatively simple addition is suggested which avoids this. Using a phase-shifting device consisting of accurately measured components so as to give an

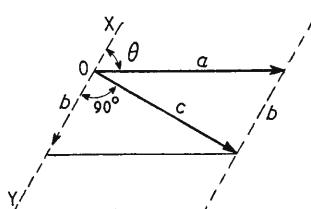
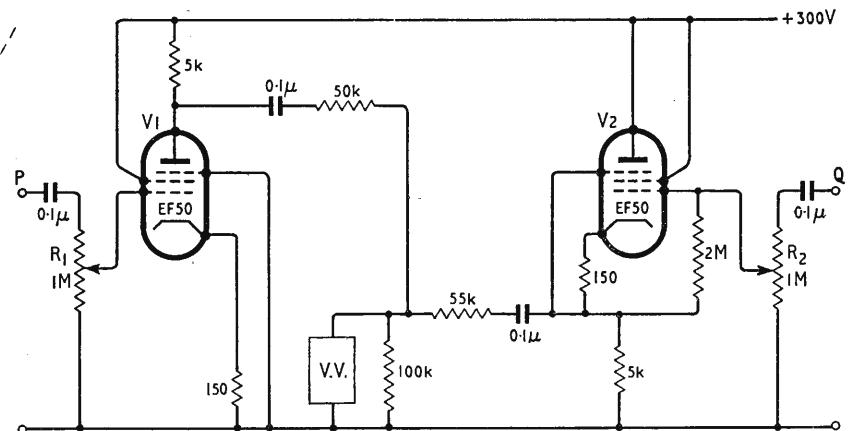


Fig. 1. Vector diagram of measurement procedure.



Right: Fig. 2. Circuit for the measurement of phase-difference.

accurately known phase shift, the measured phase difference tallied with the calculated value to within less than 1% in the range 100 to 2,000 c/s.

Suppose the two sinusoids differ in phase by less than 90 degrees; then, if one is reversed in phase and added to the other, its amplitude may be adjusted to make the amplitude of the resultant a minimum. If the un-reversed signal is initially adjusted to yield a deflection of 1 on a valve voltmeter, the minimum resultant will give a deflection of $\sin \theta$, where θ is the phase difference.

Thus, in Fig. 1, let a be the generating vector of one of the sinusoids, and let OX be the direction of the generating vector of the other, so that OX makes an angle θ with a . The vector along OX will, after phase reversal, lie along OY. Its length has to be adjusted so that its vector sum with a has least length; let it be b when so adjusted. For the resultant c to be of minimum length it must lie at right angles to XY, this giving the shortest path between the two parallel lines shown dotted in Fig. 1. Thus in the right-angled triangle so formed $c/a = \sin \theta$. Evidently, had the direction OX lagged a by θ , exactly the same condition would have obtained—hence the ambiguity.

A Practical Circuit

The required circuit is shown in Fig. 2. It is seen that the addition takes place in the common resistance ($100\text{k}\Omega$). V1 is the phase reversing valve, while V2 is a cathode follower, with a very large input and a very small output impedance. Two points have to be observed in connection with the circuit. In the first place, the phase shifts introduced by the respective input networks, whilst necessarily not zero, must at least be equal. Secondly, for accurate addition, the total impedances of the series arms of the adding network must be equal in both magnitude and phase—hence the resistance values.

The operation is as follows:—

- Connect the sinusoid sources respectively to points P and Q.
- Turn the potentiometer R_1 to zero and adjust potentiometer R_2 so that the reading on the valve-voltmeter is 1, or if possible 10, volts.
- Adjust R_1 till the reading on the valve-voltmeter is at a minimum. This reading is $\sin \theta$

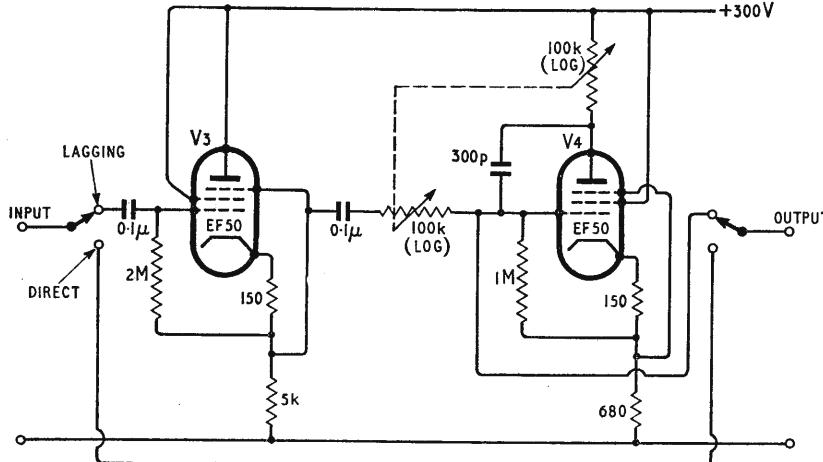


Fig. 3. Additional circuit to secure a small known phase lag.

or $10\sin \theta$, according to the original reading on the meter.

To decide whether θ is a lead or a lag, a small phase lag is introduced into the input to P by the circuit shown in Fig. 3, and the control R_1 is adjusted to give a new minimum. If the new minimum exceeds the original, the input to P lags the input to Q, and vice versa.

If θ is large, say 85° , it is possible that no new minimum will be attainable after introducing the lag—even with R_1 set at zero. This implies that the input to P lags that to Q by 85° . Had the reverse been the case, introducing the lag would have caused a drop in the minimum.

For θ very small, say 2° , it is very hard to decide for certain whether it is a lead or a lag by comparing the minima before and after the added phase lag, since the minimum is so small anyway. The phase-lagging device can be set to give only a very small lag indeed—comparable with 2° in fact—and its effect on the value of the minimum is then just detectable.

In Fig. 3, V3 is a cathode follower, while V4 is a Miller valve presenting an input capacity equal to $(1+A)$ times the anode-grid capacity, i.e. $(1+A) \times (300 \text{ pF})$. The series potentiometer ($100\text{k}\Omega$) and the $100\text{k}\Omega$ potentiometer in the anode circuit of the Miller valve are ganged, and are both logarithmic. The RC circuit producing the phase lag therefore has its R and C simultaneously variable. The resistance of either potentiometer can be accurately controlled from about $1\text{k}\Omega$ to $100\text{k}\Omega$, and so a given phase lag, say 10° , can be derived at any frequency from 10 c/s , say, to $10^4 \times 10 \text{ c/s} = 100 \text{ kc/s}$, with one sweep of the dial. This dial is accordingly calibrated logarithmically in frequency from 10 c/s to 100 kc/s , so that at a given setting, say 1 kc/s , the device produces a phase lag of 10° at 1 kc/s . If a smaller phase lag is required, it is only necessary to turn the dial to a higher frequency setting, and vice versa. The $680\text{-}\Omega$ resistance in the Miller valve cathode enables this valve to handle the greatest possible input without distortion, consistent with admitting a 100 to 1 gain change.

It can be seen from the vector diagram of Fig. 1 that for phase differences of more than 90° this method does not give a true minimum, and the smallest obtainable vector sum corresponds to $\sin \theta = 1$ and no input from R_1 . In this case neither sinusoid should be reversed in phase. By simply adding to the circuit of Fig. 2 a potentiometer connected between the anode and un-bypassed cathode of V1, and deriving the signal from the sliding contact, we can obtain this sinusoid reversed or unreversed, as necessary.

RETURN LOSS

By THOMAS RODDAM

2.—Return Loss and the Television Picture

LAST month I discussed the convenience of the return loss concept in carrying out calculations on mismatched lines. At each junction, you will remember, we can determine this quantity—we shall come to details of methods later—and then, by imagining a very short impulse sent down the line, we can work out the sort of pulse train which will arrive at the point of observation. We have seen in a practical case, too, how such delayed echoes can distort the signal. In place of the standing wave ratio, which tells us how the signal is distorted in space, the return loss offers a direct approach to the problem of determining how the signal is distorted in time. Since we are rarely in several places at once, but often in one place for some time (especially when time is measured in the milli- and microseconds of the radio engineer), the return-loss method appears to be the most suitable one to use.

The purpose of all this is, of course, to find out whether the circuit is a satisfactory one, whether it needs changes to improve the matching somewhere, or perhaps even if we could relax our tolerances on some parts of the system and save a little money. We must, therefore, be prepared to set some sort of limits to the distortion which a practical signal can be allowed to suffer in transmission.

Return Loss and Response Curves

Usually in setting limits for a transmission system we make use of the steady state characteristics, i.e. the amplitude and phase responses plotted as functions of frequency. Sometimes you will find references to wavy amplitude responses as standing wave responses, because if a system has a wavy response in space at one frequency it will usually, but not always, have a wavy response in frequency at one point; but this sort of muddled thinking can lead to serious difficulties. Since we want to be able to find the frequency response, and since we also want to work with return loss, it is worthwhile tying the two together by a small amount of mathematics.

The easiest way of tackling the problem seems to be to consider a steady single-frequency signal which can be represented as $\exp j\omega t$. Exp x is another way of writing e^x with the advantages that it is all on one line, allows larger print to be used for x , and that it takes one's mind away from the "raising to the power" angle, and reminds one of the functional nature of exp. We have, of course, the basic equation $\exp jx = \cos x + j \sin x$, so that we can always get back to cosines by taking the real part and throwing away the rest.

Travelling down the line then, we have a unit signal $\exp j\omega t$; we need not write A $\exp j\omega t$ because A can be unity if we choose. We choose. We also have a reflected wave travelling back from the mismatch at the termination. There may be several reflected waves sent back from various junctions, but let us stick to one for the moment. This reflected

wave has an amplitude m ; and is delayed by a time τ , since it has travelled down the line and back again. It can, therefore be written $m \exp j\omega(t-\tau)$. The total signal is then the sum of those two, that is $\exp j\omega t + m \exp j\omega(t-\tau)$. But we know that $\exp(a-b) = \exp a \cdot \exp(-b)$, so that the total signal equals $\exp j\omega t [1 + m \exp(-j\omega\tau)]$.

This means that the original $\exp j\omega t$ has been modulated by an amount $m \exp(-j\omega\tau)$. For small values of m this reduces to an amplitude modulation term $(1 + m \cos j\omega\tau)$, and a phase modulation of arc tan $(m \sin \omega\tau / [1 + m \cos \omega\tau]) \approx m \sin \omega\tau$.

There are some rather important relations to be derived here. The maximum and minimum amplitudes are, of course, $(1+m)$ and $(1-m)$. Now we know that m (a number) is directly related to the return loss (a decibel quantity), and that

$$m = \frac{Z_0 - Z_1}{Z_0 + Z_1}$$

provided that we measure the return loss at the point under consideration to get the apparent Z_1 . Consequently,

$$(1 - m^2) = \frac{4Z_0Z_1}{(Z_0 + Z_1)^2}$$

But $10 \log (Z_0 + Z_1)^2 / 4Z_0Z_1$ is the reflection loss, which is therefore also equal to $-10 \log (1 - m^2)$. A quick look in the textbooks (Hardy, "A Course on Pure Mathematics", 10th edn., p. 400, Cambridge University Press) shows us that

$$10m^2 < -10 \log (1 - m^2) \leq 10m^2/(1 - m^2) \text{ for } 0 < m^2 < 1.$$

This enables us to get a pretty good idea of the reflection loss in terms of the size of the ripples in the amplitude response. For example, if the response showed 1 dB ripples we should have $m \approx 0.1$ so that the reflection loss $-10 \log (1 - m^2)$ would be very close to $10m^2$ or 0.1 dB. The ripples in the phase characteristic have an amplitude of m radians, in this case about 6° .

Echoes and Response Curves

I am not going to do any more mathematics here, although the case of two echoes is both interesting and important. You can find it mentioned in the appendix to a paper by Mertz (*J. Soc. M.P.T.E.* Vol. 60 p. 572, 1953). Especially interesting is the possibility of a pre-echo, if we may call it that, which enables us to get a flat phase characteristic but ripples in the amplitude characteristic or, to a first approximation, a flat amplitude with ripples in the phase characteristic.

Before going any further there is one important simplification to be made. Most systems we consider are of finite size, so that the signal takes a finite time to get from input to output. This delay time corresponds to a phase characteristic which is a straight line when plotted against frequency, the slope

$d\phi/d\omega$ being equal to the delay. We shall not cause any error in our studies if we put our clocks back and make this delay time zero. The phase shift should then also be zero, and we can concentrate on the deviations from the horizontal straight line, the zero phase axis. The results of our mathematics have been summarized by Mertz (loc. cit.) who refers us back to Wheeler (*Proc. I.R.E.* Vol. 27, p. 359, 1939). Mertz says:

1. A single echo appears as an array of ripples or sinusoidal scallops in both the amplitude response and phase characteristics.

2. The delay of the echo from the main signal influences the coarseness or fineness of structure of the scallops. The echo delay is inversely proportional to the wavelengths of the scallops measured along the frequency scale in the plotted characteristics.

3. The amplitude of the echo, relative to that of the main signal, influences the amplitude of excursion of the scallops. The relative echo amplitude (if small enough) is equal to the peak-to-zero excursion in the amplitude response characteristic, measured in nepers. It is equal similarly to the phase shift peak-to-zero excursion, measured in radians.

4. There is a phase shift of 90° between the array of ripples in the amplitude response characteristic and that in the phase characteristic. That is, the former are cosinusoidal, and the latter sinusoidal, ripples.

In Fig. 1 you can see how the echo spacing is related to the amplitude and phase responses. The particular features to be noted are the relationship between echo spacing and ripple frequency (the closer the echo the fewer the ripples in amplitude and phase response in a given band-width); and the sideways shift of the phase ripples with respect to the amplitude ripples.

Very often in the literature you will find references made, not to the phase characteristic, but to the delay characteristic. There are actually two different delay characteristics, and it is not too difficult to get confused between them. I wouldn't be at all surprised if "Cathode Ray" has already dealt with this question: if not, he probably will. But until that happy day let us take a quick look at Fig. 2, which represents a quite arbitrary phase characteristic. A nice smooth curve, drawn the way it is just to remind you of a triode anode-current/anode-voltage characteristic.

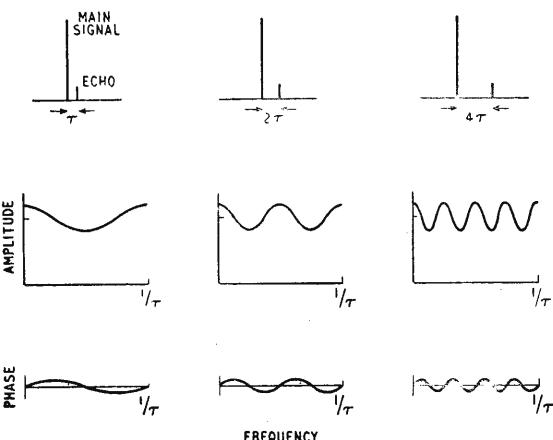


Fig. 1. Amplitude and phase response characteristics associated with various single-echo spacings.

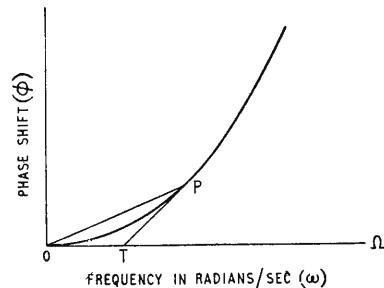


Fig. 2. Triode-like phase characteristic.

At the point P, the phase shift is ϕ and the frequency (the radians/second) ω . The slope of the line OP is $\tan^{-1}PO\Omega$ and is, of course, ϕ/ω . The slope of the actual phase characteristics at P is the slope of the tangent line PT, and is $\tan^{-1}PT\Omega$. This, of course, is $d\phi/d\omega$. The first of these, ϕ/ω , is called the phase delay, while the second, $d\phi/d\omega$, is called the envelope delay. It may seem odd to you, if you haven't met this before, that there should be two kinds of delay. That is why I drew a triode-like sort of curve. We are all quite happy to say "This valve takes 5 mA at 200 volts; and has an impedance of 10,000 ohms." Applying Ohm's Law, however, the impedance would seem to be $200/(5 \times 10^{-3})$, or 40,000 ohms. Most of us never consciously consider that the valve has two equivalent impedances, one for the steady h.t. supply (40,000 ohms), and one for small signals (10,000 ohms), the 10,000 ohms being, as you well know, the incremental impedance.

Envelope delay gets its name from the analytic process of considering what happens when two steady signals at frequencies ω and $\omega + d\omega$ are applied to a circuit. These beat together, and the delay experienced by the quasi-signal, the beat peak, is found to be $d\phi/d\omega$. If $d\phi/d\omega$ is constant over the band needed to transmit a pulse, $d\phi/d\omega$ is the actual pulse delay: if $d\phi/d\omega$ is not constant, there is some dispersion and the pulse loses its shape. You cannot measure exactly the velocity of a pig through a sausage factory.

We are, at the moment, considering a single clear echo. How big can it be before we object to it? The clearest collection of data is that given by Mertz (loc. cit.) whose Fig. 7 is reproduced as Fig. 3. Mertz gives some notes on these curves, which are best quoted in full:

(a) Mertz. A suggestion, based largely on experience with picture transmission, on the course to be expected of the tolerance as a function of echo delay.

(b) Doba (1949, unpublished memorandum). Relative values of tolerance indicated, adjusted toward crosstalk limit at long delays. Picture consisted of small solid rectangles on a flat field.

(c) Mertz, Fowler and Christopher. Data on only two delays, summarized for two pictures. Figures are for echo "just perceptible" to median observers, and "impairment to picture, but not objectionable," or worse, to most critical 10% of observers.

(d) Christopher (1950, unpublished memorandum). Data covering pictures and engraved geometrical figures. Form of summary curve, taken as reasonably representative, smoothed from data.

(e) Fowler and Christopher. Echo "just perceptible" to median observer. Single sensitive picture. (Continued on page 585)

(f) International Radio Consultative Committee. Limits recommended for overshoot and echoes. These are really for a 405-line 3-Mc/s video band system.

In considering these curves we should not, I think, lay too much stress on (a), which represents figures put up just after the war as "probable good practice." This curve is really a guide to the experiments which led to the setting up of the standards of curve (f). Now C.C.I. standards tend to be better than domestic standards. Norman Douglas, I think it was, said somewhere that you should never give a man a dinner more than 10% better than he would get at home. The C.C.I. view seems to be to replace never by always: even engineers want to know that they are keeping up with the Jones'. The smooth curve (d), given by Christopher, looks like a reasonable target for the designer, with about 6 dB to spare before anyone is likely to be at all worried.

The echo delay in Fig. 3 is given in microseconds. For transmission along cables the velocity of the signal will be about 2×10^{10} cm/sec., or 200 metres/microsecond. This means that, if the signal travels 100 metres to a mismatch and then travels back to the observer, the echo pulse will have gone 200 metres and will be delayed by 1 microsecond. We could therefore add to the bottom of Fig. 3 a second scale saying "distance to reflector in hundreds of metres," with the same number positions. This then gives us all the information we need for studying a television transmission network—which could just be the aerial you share with your neighbour.

Distortion Due to Echoes

It is, to my mind, much easier to understand the way in which the picture is distorted due to each picture element having a small echo, than to try to make an estimate of the subjective effect of a non-uniform phase characteristic. There used to be some gramophone records, made I think by the German Siemens Company, of speech which had been transmitted over a very long telephone line without phase equalization. You could hear quite distinctly the difference in time of arrival between the high-pitched "sh" sound and the deep "uh." In the same way you can proceed from the idea of an echo to the phase curves of Fig. 1. You can then in terms of Fig. 3 find the corresponding criteria for either the shape of the phase curve, or the shape of one of the delay curves. It is then quite reasonable to say that any device which has such and such sort of phase or delay curve will produce a given echo. We have already seen, indeed, that the size of the echo is equal to the amplitude of the phase shift wave (half the peak-to-peak) measured in radians. We have also seen that if the "modulation frequency" of the phase characteristic is $1/\tau$, then the echo delay is just τ . This theme can be expanded in detail, and it offers a very simple method of turning an amplifier phase characteristic into picture distortion. Inside the black box which is our amplifier we have something which behaves to some extent like an echo chamber.

More important at this stage is the effect of distorting the echo. If the echo is differentiated, two small pulses, one of which is inverted, are produced from the original pulse, and, according to experimental evidence, differentiated echoes may be about 10-15 dB larger than the full echo. Here again we can construct the appropriate phase, phase delay, and

envelope delay curves and apply tolerances to them. From the various ways of plotting the phase curve corresponding to a differentiated echo you can again work back to interpret a black box phase response as a differentiated echo, if this is appropriate, and thus treat a wider range of black box responses in terms of their echo form. To do this in any detail would need an article to itself.

A point of very great importance is the fact that when the echo delay time is zero the echo amplitude is not important, except, of course, that the reflection loss must be considered. This means that a device which produces, as some people will put it, standing waves does not itself suffer. It is only when the echo gets back along the line that it can do any real harm.

The reader will, I hope, already have realized that the right-hand part of Fig. 3 applies to the ordinary ghost of television reception. It is one

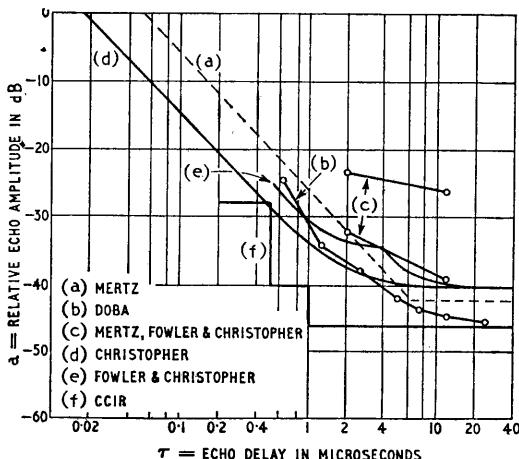


Fig. 3. Reported tolerances on echo amplitude as a function of echo delay.

of the advantages of this pulse and echo method of analysing the behaviour of circuits that it ties together as a single story a whole set of phenomena which would otherwise be treated piecemeal. What is more, the single story is one which is directly related to the final subjective effect. This idea of asking what happens to a pulse is one which has wide applications. It can be used, for example, in estimating the transient response of a feedback amplifier, where the first signal to arrive at the output has been amplified by the full gain of the amplifier in many cases. This initial spike is followed by the main body of the pulse in which the signal has had time to travel round the feedback loop and through the amplifier a second time.

Audio frequency applications of return loss are not so important to readers of *Wireless World*. The echo treatment shows that you must have plenty of room for the echo to get separated from the main signal. In television a microsecond is quite a long time, but in ordinary audio work we don't have to worry about much less than 100 microseconds, and that means that we need 10,000 metres to get our pulse and echo separated enough. This is not, however, very far for a trunk telephone network, so that the telephone transmission man is always aware of return loss. It is just within the range of interest for the wire broadcasting

people. At power frequencies, where a pulse of about 10 microseconds would be the one to consider, the line length would need to be about 600 miles. This is a practical length of course for long trunk lines, and at points where the echo and the signal (the supply) reinforce each other (i.e. when τ is an integral multiple of 1/50 sec) the voltage on the line can go well above its normal value if the load comes off. I cannot remember if anyone has gone above 400 kV yet, but you will see that a 25% echo, adding another 100 kV, would be a pretty alarming thing to happen to anybody's power line.

Return Loss Measurement

It still remains to discuss the way in which we can measure the return loss which our apparatus gives when we use it at the end of a line. Measurement consists of the comparison of an unknown quantity, the quantity to be measured, with a known standard. This is, of course, a truism, though if you look at the "Philosophy of Physical Science" by Sir Arthur Eddington (Cambridge University Press, 1939), you will find that two thirds of the text are devoted to paving the way for general statements

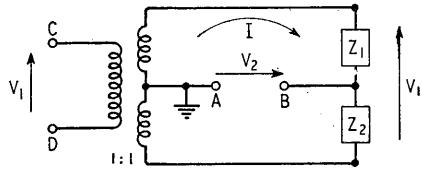


Fig. 4. Basic bridge circuit used in return loss measurement.

on measurement and observation. Usually, of course, the standard with which we make the comparison is, directly or indirectly, a fundamental standard. We could, I have no doubt, trace the sub-standard pint back to the standard kilogram. Return loss is not defined to be measured in this way against the background of the basic units. The question we ask when measuring return loss is not really "How many units of such and such?", but rather, "How nearly does this resemble that?"

Immediately after writing the last phrase it became apparent that it must be qualified. We may, in measuring return loss, ask either of two questions. "How far does this deviate from that?" is the first question, to which we may add "and in what manner?" as the second. In general, we find that we are only interested in the first question when we are concerned with what are so elegantly termed "user aspects." For buying or selling, or installing a piece of equipment, we may wish to know that the return loss against the nominal or actual line impedance is greater than x dB, and our interest will end there. When we are designing or adjusting a piece of apparatus, on the other hand, we wish to know how the impedance deviates from the ideal in order that we may attempt to correct it. We have distinguished between these two reasons for measurement because rather different experimental methods are used.

Let us consider the circuit shown in Fig. 4. This form of bridge circuit, using a centre-tapped transformer, is well known.

The current I which flows round the loop, is given by

$$I = V_1 / (Z_1 + Z_2) \quad \dots \quad \dots \quad \dots \quad (1)$$

and the detector open-circuit voltage, V_2 , is given by

$$V_2 = \frac{V_1}{2} - IZ_1 = \frac{V_1}{2} - \frac{V_1 Z_1}{Z_1 + Z_2} = \frac{V_1 (Z_2 - Z_1)}{2 (Z_2 + Z_1)} \quad (2)$$

$$\text{or } V_2 = IZ_2 - \frac{V_1}{2} = \text{the same} \quad \dots \quad \dots \quad \dots \quad (3)$$

$$\text{Thus } V_1/V_2 = 2 (Z_2 + Z_1) / (Z_2 - Z_1) \quad \dots \quad \dots \quad \dots \quad (3)$$

Apart from the factor 2, this is just what we require for the determination of the return loss of Z_1 against Z_2 , or Z_2 against Z_1 . We can write

$$20 \log \left| \frac{V_1}{V_2} \right| = 20 \log \left| \frac{Z_2 + Z_1}{Z_2 - Z_1} \right| + 6 \text{ dB} \\ = (\text{R.L.} + 6) \text{ dB} \quad \dots \quad \dots \quad \dots \quad \dots \quad (4)$$

Before going on to discuss the direct use of this bridge circuit we may, I feel, dispose of another mathematical question. Suppose that we write the return loss as $20 \log r$. Then

$$r = |(Z_2 + Z_1) / (Z_2 - Z_1)| \\ = \left| \left(\frac{Z_2}{Z_1} + 1 \right) / \left(\frac{Z_2}{Z_1} - 1 \right) \right| \quad \dots \quad \dots \quad \dots \quad (5)$$

Now either or both Z_1 and Z_2 may be complex, and we can write $Z_2/Z_1 = x + jy$. Thus

$$r = |(x + 1 + jy)/(x - 1 + jy)|$$

which gives us $r^2 = [(x + 1)^2 + y^2] / [(x - 1)^2 + y^2]$

or $r^2(x^2 - 2x + 1) + r^2y^2 = x^2 + 2x + 1 + y^2$

i.e. $(r^2 - 1)x^2 - 2(r^2 + 1)x + (r^2 - 1)y^2 = 1 - r^2$

$$\text{or } \left(x - \frac{r^2 + 1}{r^2 - 1} \right)^2 + y^2 = \left(\frac{r^2 + 1}{r^2 - 1} \right)^2 - 1 \\ = \left(\frac{2r}{r^2 - 1} \right)^2 \quad \dots \quad \dots \quad \dots \quad \dots \quad (6)$$

This is just the equation of a circle with radius

$$2r/(r^2 - 1) \text{ and centre at} \dots \quad \dots \quad \dots \quad (7)$$

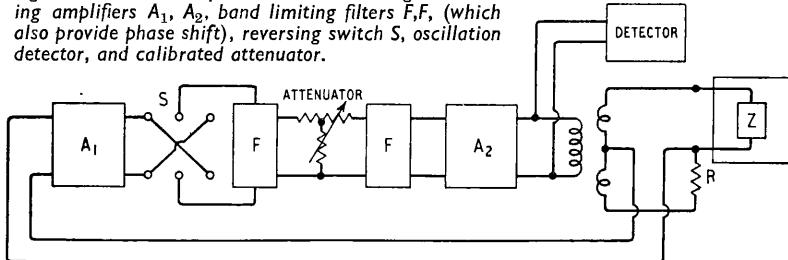
$$x = (r^2 + 1)/(r^2 - 1), y = 0 \quad \dots \quad \dots \quad \dots \quad (8)$$

Remembering that x and y in equation (6) above are just the real and imaginary parts of the impedance ratio Z_2/Z_1 , we see that if we measure the return loss, which means that we determine r , we know only that the relationship between x and y is such that equation (6) is satisfied. The resistive component may be the wrong amount, or it may be correct, but with some unwanted reactance. These various possibilities affect the phase of the reflected signal, while we are concerned only with its size.

Having dealt with this bit of algebra, which we shall make more use of later, let us consider the problem of measuring the return loss just as a number. Look back now to Fig. 4 and equation (4). Suppose that across AB we connect the input of an amplifier, assumed to have a very high input impedance, and that the output, assumed to have a very low impedance, is connected across CD. If the gain of the amplifier is adjusted to be a very small amount greater than $(\text{R.L.} + 6)$ dB we have satisfied one of the two conditions required for oscillations to build up from the ordinary circuit noise. If the gain is just less than $(\text{R.L.} + 6)$ dB such oscillations will not build up.

This gain condition is, of course, not sufficient to

Fig. 5. Basic circuit of return loss measuring set showing amplifiers A_1 , A_2 , band limiting filters F , F , (which also provide phase shift), reversing switch S , oscillation detector, and calibrated attenuator.



ensure oscillation: it is necessary also that the signal should suffer the correct phase shift in its passage through the system. Under steady oscillation conditions the signal must, in fact, go through exactly $2n\pi$ radians phase shift in a complete traversal of the circuit. This involves us in some special design problems which we shall now discuss.

The designer of an amplifier for this kind of test will naturally wish to use negative feedback to stabilize the gain of the amplifier and thus avoid the need for its frequent recalibration. A consequence of the use of negative feedback is that the phase shift through the amplifier will be very nearly the same at all frequencies away from the edges of the pass-band. This puts a very severe restriction on our chances of finding the correct phase for oscillation in the particular region in our frequency band where the return loss is lowest (i.e. worst), which is where we are most interested in measuring it. It is only reasonable, however, to use filters to define our frequency band. These filters are our salvation from the point of view of phase, because each half-section we use gives us a phase shift across the band of 90° . Thus a not unreasonable combination of two sections of low-pass and two sections of high-pass filter will assure us of two test frequencies at any given phase, while a reversing switch anywhere in the loop will give us two more. Whether this is sufficient or not depends on the sort of impedance we are going to test. If it varies rapidly we may need more test points, though the phase shift in the bridge itself will help us; if it is a pure resistance it does not matter much at what frequency the test is made.

In some commercial designs of return loss tester additional phase shift is provided as a side product of the need to introduce these filters, and to adjust the gain. The amplifier is split into two portions, each provided with negative feedback. The feedback does not embrace the output transformer of the first amplifier or the input transformer of the second. The purpose of these transformers is to establish a convenient impedance level for the filters which are connected between the amplifiers; and they offer a very useful contribution to the phase characteristic of the whole system.

The block diagram of a return loss tester of this kind is shown in Fig. 5. The oscillation detector may be one of a variety of devices. A simple diode and meter, a pair of headphones if the system is for audio frequency use, or a tuning indicator valve, are three possibilities which spring to mind. An instrument of this kind can easily provide a discrimination of one decibel. Moreover the calibration is very easily checked using standard resistors, and these can be readily built in. Such an instrument is, indeed, just what it should be; straightforward, easily checked, and generally suitable for providing the yes-no

discrimination needed in routine testing.

For the designer, as we have already seen, this information is not sufficient. He needs to know the actual value of the return loss in order to correct his design. One available method, which I have never seen used or described, is to apply to the bridge network of Fig. 4 a band-limited noise input as V_1 , connect

an r.m.s. reading instrument to measure V_2 , and then fiddle about with resistance and capacitance boxes across Z_1 or Z_2 as required to get the lowest value of V_2 . This technique, described rather slightly here, would be a possible test room approach to a situation where closer return loss tolerances than normal production permits are needed, subject to an over-riding limitation on the complexity of the correcting network. The most likely example I can bring out of the hat where this technique would be of use, is an audio-frequency amplifier with an input transformer using a high permeability alloy core which for economic reasons has been pushed slightly beyond the reasonable design limit. I do not doubt that there are other examples of just-over-the-edge adjustments.

Normally, however, the designer must measure the return loss at a number of points in the working band. Equation (5) and the results which follow from it lead us to the conclusion that the normal technique will probably be to use an impedance bridge. We may, however, find it convenient to measure admittances, especially at high frequencies. If so, we have:

$$r = \left| \left(\frac{Z_2}{Z_1} + 1 \right) / \left(\frac{Z_2}{Z_1} - 1 \right) \right| \quad (9)$$

$$= \left| \left(\frac{Y_1}{Y_2} + 1 \right) / \left(\frac{Y_1}{Y_2} - 1 \right) \right| \quad (10)$$

$$= \left| \left(\frac{Y_2}{Y_1} + 1 \right) / \left(\frac{Y_2}{Y_1} - 1 \right) \right| \quad (11)$$

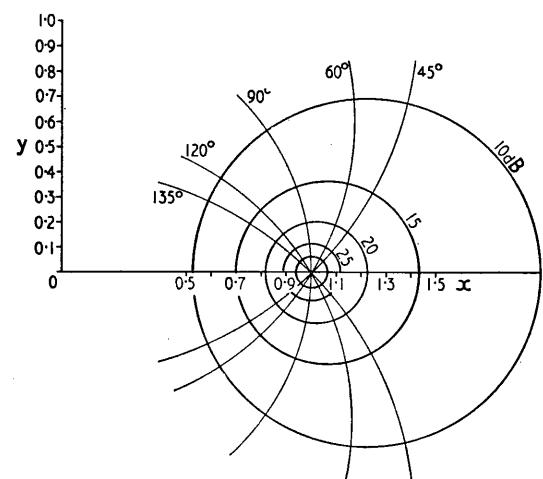


Fig. 6. Return loss contours and orthogonal phase circles for normalized impedance or admittance. (For a fuller construction use Table 13, p. 60 of Mole, "Filter Design Data" (Spon, 1952), or equations 7 and 8).

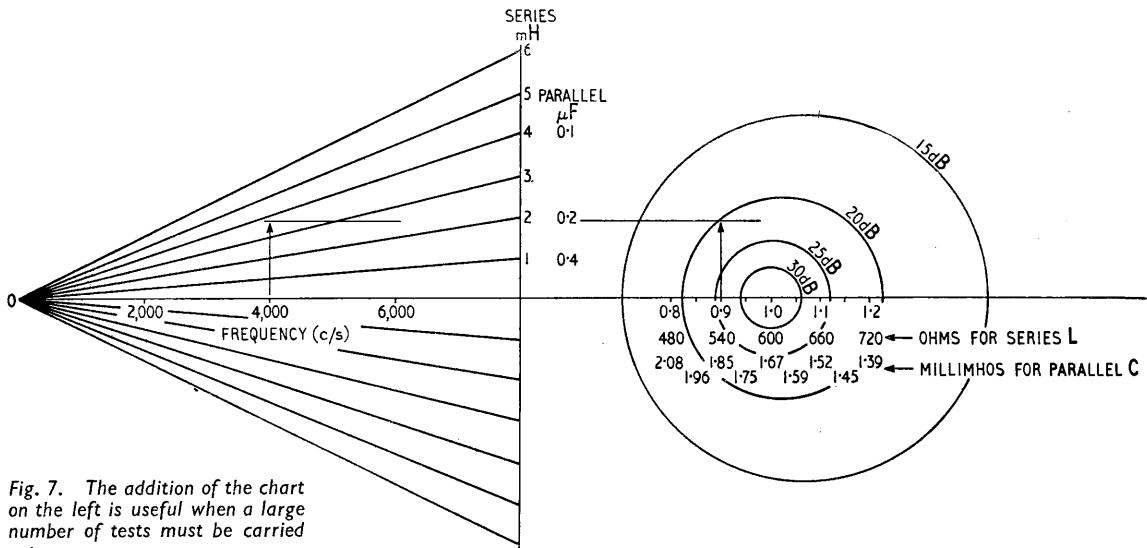


Fig. 7. The addition of the chart on the left is useful when a large number of tests must be carried out.

the only point being that in going from (10) to (11) we have concealed a phase shift of 180° .

The results which were obtained above as equations (7) and (8) are incorporated in Fig. 6. On this diagram, on the rectangular co-ordinate system we plot a trace of the normalized impedance or admittance. We can then read off the return loss from the system of circles, and we can also see where our impedance is going wrong, either through its reactive behaviour, or through a basically wrong value of resistance level. What is more, we can see where it goes wrong most, so that it can be corrected stage by stage. With some experience it is easy to interpret traces on Fig. 6 and to devise suitable correcting networks.

Where a large number of tests are to be carried out within a prescribed frequency range and at a fixed impedance level, it may be worth while to construct the special form of combined impedance and return loss chart shown in Fig. 7. This particular one is suitable for the classic 600-ohm audio frequency case. The example marked in shows that an impedance consisting of 540 ohms in series with about 3.8 mH will give a return loss of 20 dB at 4,000 c/s. As we have seen, these charts may be used for admittances or impedances, so that we can consider $R + j\omega L$ or $G + j\omega C$ equally conveniently. C may, of course, be negative: I cannot think offhand of a bridge which gives negative values of L .

There remains one measuring technique for return loss which is of value in some special video frequency problems. If we wish to transmit $1\mu\text{sec}$ pulses say along a line which must be well-matched, we can check the matching by means of the pulses themselves. All we need to do, and this does not mean there are no experimental difficulties, is use a length of cable equivalent to about $1\ \mu\text{sec}$ of travel (giving us $2\ \mu\text{sec}$ go and return), and examine the signal for echoes. This method is used for looking at impedance irregularities in cables, and suitable pulse generators and oscilloscopes can be obtained for it. It is rather a "made-to-measure" approach, because the cable itself probably will not have exactly its nominal impedance, so that, for example, you may be matching to 80 ohms instead of 75 ohms.

Not much more can be said about return loss in a

general survey. As might be expected the return loss chart of Fig. 6 has come to look very like the Smith chart. Which approach is the more useful in any particular problem is a matter to be decided by experience, but a rough guide is probably that return loss is more appropriate whenever the system is big enough for echoes to be separated out: if I sing in the bath, that's standing waves; if I shout at a distant cliff, return loss.

CLUB NEWS

Birmingham.—An air traffic control officer from Elmdon airport will talk on air traffic control at the meeting of the Slade Radio Society on December 6th. The club meets at 7.45 at the Church House, High Street, Erdington. Sec.: C. N. Smart, 110, Woolmore Road, Erdington, Birmingham, 23.

Brighton and District Radio Club, which operates station G3EVE, continues to meet at the Eagle Inn, Gloucester Road, on Tuesdays at 8.0, where visitors and prospective members are welcome. Sec.: R. Purdy, 37, Bond Street, Brighton, 1.

Northern Mobile Rally.—Plans are being made for a mobile rally centred on the West Riding for April 27th. Offers of support should be sent to N. Pride, secretary of the Spen Valley & District Radio & Television Society, 100, Raikes Lane, Birstall, W. Leeds, Yorks.

Nottingham.—The Amateur Radio Club of Nottingham, G3EKW, meets every Tuesday and Thursday at 7.15 at Woodthorpe House, Mansfield Road. The programme includes constructional work, morse training, lectures and discussions. Sec.: F. V. Farnsworth, 32, Harrow Road, West Bridgford, Nottingham.

Pontefract.—Meetings of the Pontefract Area Transmitting Group are now held at the Queen's Hotel, Pontefract, on the first, third and fifth Thursday of each month. The club transmitter, G3FYQ, has been installed at the hotel. Sec.: W. Farrar, G3ESP, 6, Hemsworth Road, Ackworth, Pontefract, Yorks.

Wellingborough.—Members of the Wellingborough and District Radio and Television Society will debate the statement "That the days of radio are numbered" at their meeting on December 12th at 7.30 at the Silver Street Club Room. Sec.: P. E. B. Butler, 84, Wellingborough Road, Rushden, Northants.

Choke or Capacitor Input?

Significance of the Two Systems in Power Supplies

By "CATHODE RAY"

AMONG requests received from readers is one for an explanation of the why and wherefore of swinging chokes. Resisting the temptation to invent an analogy between them and swinging cats (or even pirates) I will go straight into a comparison between the two diagrams presented as Fig. 1. A period of 15 seconds is allowed for reaching the conclusion that they both represent full-wave rectifier circuits, and that (b) is exactly the same as (a) except that C_R is missing. Those who are not well up in the design of such circuits might suppose that the only real difference was that the d.c. output from (b) was less well smoothed; a deficiency which could probably be made up by increasing the capacitance of C , and certainly by adding another choke-and-capacitor filter stage. Actually, however, the two circuits work on entirely different principles and have different characteristics. In particular, the choke L in (b) has to be of a special kind, commonly known as a swinging choke, quite different from the one in (a).

Circuit (a) is the arrangement commonly used for supplying h.t. current to small power amplifiers, etc., from an a.c. supply. C_R acts as a reservoir. If no current is being drawn off it charges up during the first few cycles to the peak voltage of each half of the transformer secondary coil. This state is illustrated in Fig. 2(a), which covers one complete a.c. cycle. Current cannot be shown on this diagram because there is none going either in or out.

When current is drawn by a load it starts to discharge C_R , as indicated by the downward slope from A to B in Fig. 2(b). C_R can only recharge when the transformer voltage rises above its own voltage, thereby providing a small balance to drive current

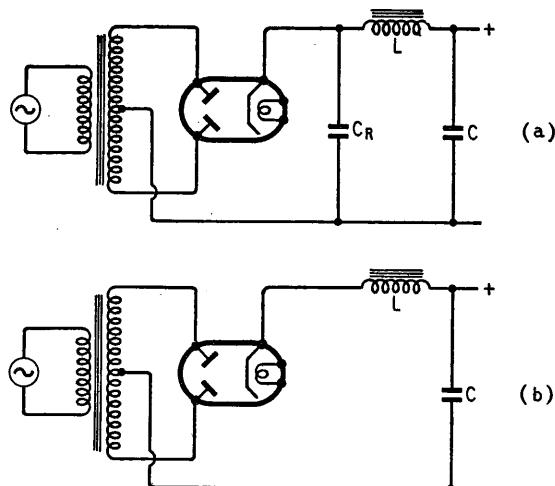


Fig. 1. Two alternative types of full-wave rectifier circuit:
(a) capacitor input, and (b) choke input.

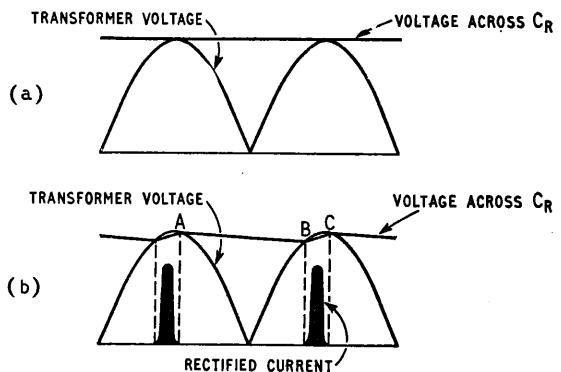


Fig. 2. Diagrams showing the working conditions of a capacitor-input circuit, when (a) there is no current, and (b) load current is being taken.

through whichever half of the rectifier is receiving it. During this phase, marked B to C, C_R has to receive enough current to keep the load supplied continuously throughout half a cycle.

This is where the designer is faced with a dilemma. If he makes C_R small it will lose voltage rapidly between a.c. peaks, the result being a much lower average output voltage at full load than at no load. In technical language, it has bad regulation. It follows too that there is a very large ripple on the output voltage, necessitating much smoothing. If on the other hand he makes C_R large enough to hold the output voltage well up, B comes nearly to the voltage peak, so the period represented by BC is only a small fraction of the half-cycle (AC) and the peak current through the rectifier is therefore many times greater than the steady load current. This is bad for the rectifier, unless an abnormally large sized one is used. It is also bad for the transformer, unless a large and expensive model is used, because a pulse waveform has a much greater r.m.s. value—which is what counts in heating the windings—than the mean value, which is the useful output.

One puts up with these inconveniences when the amount of power to be supplied is so small that the extra cost of the components is not worth seriously bothering about, and especially when the load current is fairly constant, as it is for example when it consists of a Class A amplifier. The current peak can if necessary be kept within reasonable bounds by means of a resistor in series with the rectifier. And the system does have the advantage that the output voltage can be a fairly high percentage of the peak input voltage.

But for large power amplifiers, say 50 watts or more, the extra cost of the rectifiers and transformer on account of the highly peaked current waveform is serious. What is perhaps more serious

is that high-power amplifiers often work in Class B (or C), so the current drawn is liable to fluctuate between wide limits. The steep fall-off in output voltage when the current drawn increases—in short, the bad regulation—is then a most undesirable feature of this capacitance-input power supply system.

Compare the choke-input system, Fig. 1(b). Let us suppose that the inductance, L , of the choke is large enough to keep the current through it practically constant. Then the output voltage across the smoothing capacitor C must be practically constant and can be represented by a horizontal straight line. On the rectifier side of the choke the voltage (neglecting the loss of volts in the rectifier when it is conducting) consists of the half-cycles seen in Fig. 2. So the voltage across the choke must be the difference between these semi-sine-waves and the constant voltage. The question is, how high up in Fig. 3 must we draw the horizontal line to represent the constant output voltage?

If we neglect the resistance of the choke and assume it is purely inductive, the voltage across it must be entirely alternating, with no d.c. component. This means that its average each side of its zero line is equal. The horizontal output-voltage line can be regarded as the zero line for the choke voltage, which is then represented by the half-cycle waveform above and below it. To be purely alternating, the shaded areas below the line must be equal to those above. This is the same thing as saying that the height of the horizontal line must be equal to the average height of the half-cycle waveform. The books show us that this height is $2/\pi$ or 0.64 times the peak height, which we call V_{max} :

Since we know that the voltage across an inductance L is equal to L times the rate at which the current through it is changing, we can find the current waveform. Its slope at any point must be proportional to the shaded voltage, so is something like Fig. 4.

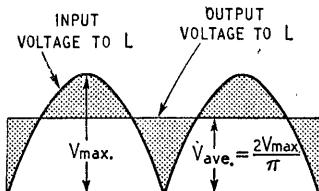


Fig. 3. Approximate voltage relationships in a choke-input circuit with very large choke inductance, when some current is flowing.

At this stage you may object that we were supposed to assume a constant output current and here I am showing it varying. I would point out however that we assumed it was *practically* constant, which means that any variation is small. So Fig. 4 represents a small ripple on a relatively large constant current. There *must* be some ripple, to generate the shaded voltage across L .

With our simplifying assumptions the output voltage is as shown in Fig. 3, regardless of the amount of d.c. drawn by the load. So the choke voltage, and therefore the current ripple needed to induce it, is the same at all load currents. In practice an increase in load current does drop the output voltage slightly, because it has to pass through the neglected resistances of choke, rectifier and transformer. Provided these are kept low, the output voltage remains steady at nearly 0.64 times the peak value over a wide range of output current, instead of varying steeply as in the capacitor-input system.

In practice, L cannot be so enormous that the



Fig. 4. Waveform of ripple current corresponding to the voltage waveform in Fig. 3.

ripple current is negligible. It may be fairly small compared with full load current, but if the load current is reduced sufficiently a point will be reached where it is not as big as the ripple, so current will cease altogether at the troughs of the ripple. During these periods of interrupted current (twice per a.c. cycle) L obviously cannot give rise to any voltage whatsoever and our theory breaks down. In the limit, when there is no load current at all, L might as well not be there, and C tends to take the place of C_R in Fig. 1(a), so that voltage across it builds up to the peak level.

The relationships between output voltage and load current therefore work out as in Fig. 5, where (a) is the capacitor-input curve and (b) the choke input. The "critical load" for (b) is the load current which is only just enough to be continuous in spite of the ripple. At smaller load currents the output voltage soars up towards peak value, and at larger currents it falls gradually owing to the resistance of the rectifier, etc. The steeper fall of (a) is because of the effect explained in connection with Fig. 2.

One of the objectionable features of (a) is that if current is not being drawn—for example, while valves are warming up—the voltage rises about 40% above its full-load level, so all the components concerned have to be rated accordingly. The choke-input system can be freed from this disadvantage if its load current is never allowed to fall below the critical point. This can be ensured by a suitable resistor connected in parallel with C and known rather unpleasantly as a bleeder. Such a device would be wasteful if the current taken by it—at least equal to the critical load current—was not small compared with the full load current; say at most a tenth and preferably less than that. So the requirement for L is that it must be large enough for the critical load current to be of this order.

An approximate calculation—given at the end, in case anyone is interested—shows that the critical inductance, which is the minimum inductance needed to ensure continuity of current, and which we will call L_c , is equal to the critical load resistance (R_c) divided by $6\pi f$, where f is the supply frequency to the full-wave rectifier. At $f = 50$ this reduces to $L_c = R_c/940$. To take an example, suppose the output voltage (at the critical load) is 500, and one doesn't want the critical load to be more than 10mA. Then $R_c = 500/10 = 50k\Omega$. Assuming $f = 50$ c/s, $L_c = 50,000/940 = 53$ henries. If the full load current is something like 150 or 200mA, that is a formidable inductance to provide, especially if (in order to realize the benefits of the system) its resistance has to be kept low.

Fortunately, however, there is no need for its inductance to be anything like 53H at full load. 5H would be more than enough to ensure continuity of current. In the capacitor-input system, the important thing is to ensure adequate smoothing inductance at full load current, and to avoid saturation of the choke core a gap must be left in it, which necessitates more turns to keep up the inductance and therefore more resistance or higher cost. But

the choke in the choke-input system can be allowed to saturate quite a lot at full load provided it gives a high inductance at critical load. I am not certain of the origin of the description "swinging"** for this kind of choke, which was used at least as far back as 1929, but apparently it refers to the variation of inductance when the d.c. through it is varied.

That is not the only difference between it and the ordinary smoothing choke. Fig. 3 shows that the peak voltage across it at all working load currents is about equal to the full output voltage. So the insulation of the windings must be adequate.

One way in which the critical current can be reduced (or alternatively the critical inductance reduced) is to tune the choke to the fundamental ripple frequency, which is twice the supply frequency. This is done by connecting a suitable capacitor across L. Admittedly it bypasses the higher ripple frequencies, but they can easily be dealt with by the subsequent smoothing filter. Suppose in the previous example we cut down the 10mA inductance of the choke to 20H. This alone would not provide enough impedance at 100 c/s to keep the fundamental ripple current below 10 mA peak, but it could be made to do so by means of about 0.127 μ F in parallel with it.

The rectifier used in conjunction with choke-input is usually a gas-filled type, because that has negligible slope resistance and so promotes the constancy of output voltage. The absence of current peaks much greater than the full load current means that quite a small rectifier can handle considerable power. Unless some historian can prove the contrary, it may be taken that choke-input was introduced specifically to enable the best use to be made of the then new gas-filled rectifier.

Summarizing

The capacitor-input system gives bad regulation and requires higher rated transformer, rectifier and smoothing capacitors than choke-input. In low-power apparatus, especially for more or less constant load current, these disadvantages, being small, may be outweighed by the advantage of higher output voltage. The greater the power to be supplied the more likely the choke-input system is to show an overall economy, and for Class B and similar requirements it is far the better. The choke must have a low resistance and a high inductance at low

* The earliest reference I know is in an article by F. S. Dellenbauch and R. S. Quimby in Q.S.T., March, 1932.

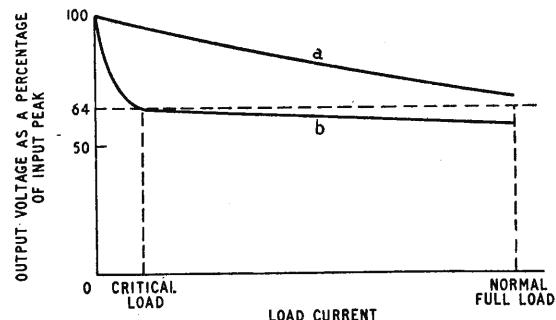


Fig. 5. Comparison of output voltage/current curves for (a) capacitor input and (b) choke input systems.

current, and be capable of standing peak voltages of the same order as the maximum output voltage. It is helpful to tune it by parallel capacitance to minimize the critical load current, below which the output voltage rises very steeply.

Lastly, here is the derivation of the $L_c = R_c/6\pi f$ formula. In Fig. 6, I_d is the d.c. or load current and I_a is the peak ripple current at its fundamental frequency, which is $2f$. At the critical value of I_d it is equal to I_a . Denote the peak alternating voltage by V_{max} ; assuming sine waveform, its average value is $2V_{max}/\pi$. The load current I_d is equal to this divided by the total d.c. resistance, of load plus choke, rectifier and transformer. At the critical I_d these additions are normally small enough to neglect

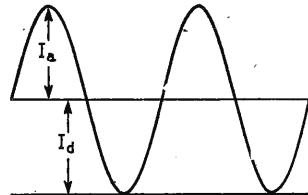


Fig. 6. Fundamental ripple and load currents at the critical point.

compared with the critical load resistance R_c , so critical $I_d \approx 2V_{max}/\pi R_c$.

Now the peak alternating component of the full-wave rectified "input voltage to L" in Fig. 3, at its lowest frequency (which is $2f$, the fundamental ripple frequency) is $4V_{max}/3\pi$. Again neglecting the rectifier etc. resistance, and also the impedance of C at that frequency, we have $I_a \approx 4V_{max}/3\pi X_L$, where X_L is the reactance of the choke at frequency $2f$, so is $4\pi fL$.

Putting $I_d = I_a$, which is the critical condition:

$$\frac{4V_{max}}{3\pi \times 4\pi f L_c} = \frac{2V_{max}}{\pi R_c}$$

which simplifies to

$$L_c = \frac{R_c}{6\pi f}$$

British Standard Specification for Ebonite

THIS is a revised version of the war-time emergency standard specification BS234 of 1942 and it covers three groupings of ebonite.

The specification covers ebonite in the form of sheets, rods, tubes and mouldings suitable for electrical and certain electronic applications. It also covers the loaded type of ebonite specified in the Wireless Telegraphy Board specification No. K109.

It lays down standards and tolerances for thickness and size of sheets; thickness, length and diameter of tubes, and length and diameter of rods.

Section 3 defines the nature of electrical tests that shall be applied, these cover permittivity and power factor.

Appendix C is concerned with tests at audio frequencies and Appendix D permittivity and power factor at radio frequencies. In the latter case tests are made at approximately 1 Mc/s. A circuit diagram of an approved test bridge is included.

The revised specification, which is known as BS234: 1957, covers 24 pages and costs 6s (6s 9d by post). Copies are obtainable from British Standard Institution, 2, Park Street, London, W.1.

LETTERS TO THE EDITOR

The Editor does not necessarily endorse the opinions expressed by his correspondents

Loudspeakers in Parallel

REFERRING to the interesting article "Loudspeakers in Parallel" by J. Moir (October, 1957), I assume the author is dealing with directional speakers when he says that no increase of apparent source size is achieved by using two or more in parallel; if this assumption is correct, I agree with Mr. Moir's findings.

But if we use omni-direction speakers the results are quite different, especially in concert halls. We have found that spacing four omni-directional speakers wide apart on the platform not only broadens the apparent source size, but also subdues hall resonance. (Carnegie Hall, New York—in spite of its reputation—possesses the biggest bass "honk" in the world, and the effect of spacing loudspeakers on the platform is quite magical.)

Mr. Moir speaks with authority on cinema installations, in which horn loading gives an impression of efficiency, due mainly to strong directional effects; but if we watch and listen to an orchestra we must be impressed by the largely omni-directional quality of the sound from the various instruments. I am convinced that the only way to recapture this effect in reproduction is to use omni-directional speakers, and any success we have had in this field has been due mainly to a realization of this simple truth.

As regards 1.f. improvement obtained by using parallel speakers close together, how right Mr. Moir is! Two speakers on a baffle give astonishing bass; the 1.f. output is double, and the risk of distortion from overloading is halved: in fact we get something for nothing in the audio region where it is usually wanted the most.

G. A. BRIGGS,
Idle, Yorks. Wharfedale Wireless Works, Ltd.

MR. MOIR'S enthusiasm for so-called stereophonic reproduction leads him in your October issue to a piece of special pleading which does not fully present what can be achieved by effective sound distribution from a single-channel source under domestic conditions. Mr. Moir's observations are confined to twin loudspeakers spaced 8-10ft apart with the listener moving laterally at an unspecified distance from the source.

I submit that his conclusion that an increase in the apparent size of the source cannot be achieved without "stereophony" is insupportable without full consideration of all the following factors:—

(a) Multiple loudspeaker placement not necessarily confined either laterally to the position considered most advantageous to stereophony; nor vertically to floor level whereby the apparent height of the source becomes fixed unsuitably; nor to two in number since even enthusiasts for "stereophony" advocate at least a third speaker so placed as to fill the central "hole"; nor to the specified position on the vertical axis—since rotation causes marked alteration of the results achieved.

(b) Control of the frequency range of individual speakers up to (with two only) complete elimination

of the bass range on the one side with or without elimination of the treble range on the other.

(c) The location of the observer along the axis, including a position *between* two speakers.

(d) The type of reproduced sound, particularly speech—when the greatly enlarged source (!) renders the method unsuitable. The superiority of multiple closely spaced small cones in the bass range and the diminution of eigentone excitation by strategically placed ancillary speakers (the latter not mentioned by Mr. Moir) are of course not relevant to the present discussion, which is concerned solely with the possibility of effective sound distribution in the domestic listening area without resort to multiple channels.

A. H. BARZILAY.

Stellerbosch, S. Africa.

Projection Television

I WILL admit I am staggered by A. G. Tucker's claim (October issue) that he can view a forward projection picture from a modified Philips 1800 chassis, with 450 watts lighting in the room.

The black level of the picture can only be that of the light reflected from his aluminiumized screen, so his picture contrast range must be from white to a shade of grey, even if the 450 watts is indirect lighting. I am certain that satisfactory daylight viewing is impossible, and I speak from experience.

I have sold and installed several forward projection models, always against my advice to the customer, and have had several dissatisfied customers in consequence. Apart from the insufficiently lit picture, there is all the trouble of setting up the projection console in the centre of the room, with trailing mains lead and aerial lead, while the illusion of reality is killed by the sound coming from the console instead of the screen.

The back projection model is quite another matter, and, as typified by the Ferranti 20K series, is, in my opinion, the best of all television pictures, and far less tiring to the eyes than direct tube viewing. If viewed against the light from the window, even on a bright sunny day, the picture is quite acceptable, and at night, a correctly optically focused 24in screen picture compares more than favourably with any direct vision receiver, with the added advantage that the line structure is practically unnoticeable. Overall focus is far superior to any 21in tube receiver I have handled, and the picture has a beautiful photographic quality.

Before the advent of the 17in screen, we sold large numbers of back projection models, but nowadays there is not sufficient public demand, and manufacture has apparently ceased. Perhaps we shall see a renaissance of the projection television receiver when colour transmissions begin?

O. V. WADDEN,
Hounslow. Wadden & Hill, Ltd.

MR. O. V. WADDEN, in his September letter, is evidently unaware of the "Daylight" type of viewing screen recently developed, which does

in fact permit of daylight viewing of film and projection television pictures without need to darken the room. Developed precisely to meet the difficulty in situations where black-out may be undesirable or impracticable, this screen requires no shielding or other special precaution in ordinary daylight conditions, and will under those conditions provide a picture comparable in contrast and brilliance with the same picture shown in darkness.

"Free Grid's" projected and future receiver (July issue), therefore, makes no kind of nonsense except that, the "Daylight" screen being a translucent or rear-projection one, the picture will appear in the adjoining room! A simple mirror arrangement, however, suffices to get it back again, and "Free Grid" is in fact predicting a development which I can assure your correspondent has already taken place and is actually in use in many schools and other specialized applications to-day. A more practical technique, however, is to fit the projector with a short-focus lens and house it in one cabinet or wall-cupboard with the mirror and screen itself, and I have in fact been using this arrangement for some time.

I have two of these screens, which are black or nearly so, apparently unbreakable, and can be used for either TV or film projection with projectors of quite moderate power and, being colour-corrected for incident light over most of the visual spectrum (actually 4,500-6,500 Å), for monochrome and colour projection also. And how near the mark "Free Grid" actually came (albeit retrospectively!) is suggested by tests recently carried out by the B.B.C. at Lime Grove, in which a spotlight powered by a high-intensity arc of $2\frac{1}{2}$ kW at ten yards failed to quench the colour picture on one of them with 750 watts in a projector using single-frame 35mm Kodachrome film—an apparently miraculous result possibly accounted for by the name "Black Magic" or the clue "regenerative" accompanying it, since the stilb¹ value of the "quenching" beam exceeded that of the projector by a factor of the order of 4, and its intensity in terms of foot-candles by considerably more.

Whatever the reason, which is in fact the novel one that the screens exhibit *gamma-plus* characteristics, i.e., maintain their contrast values under conditions hitherto thought to be impossible, they are effectively "blind" to ambient light of any intensity likely to be found in the average classroom or living room and remain unshaken by conditions intolerable to any front-projection or ordinary back-projection screen, and it is almost startling to show a picture in the dark and suddenly switch on several hundred watts of light without apparent effect whatever.

But the makers exclude direct sunlight on the not unreasonable ground that whereas the intensity of the best tungsten projector lamp at full loading is under 20 stilb, that of the sun is of the order 200 stilb (that at Lime Grove was *circa* 60 stilb). This suggests the conclusion, confirmed in practice, that for optimum results the screen should be as small as possible consistent with acceptable magnification, because the output of even the best high-intensity c.r. tube in terms of lumens falls considerably short of that of a 1,000-watt projector lamp, and my own experience indicates 4 sq. ft. as the present upper

limit of advisable screen area under average room conditions in daylight, e.g., a mean ambient light level of 12-20-foot candles. And I say *present* because, a true "Daylight" or anti-dilution screen having been developed, the limiting factor has now become the light available at the projector which is by no means likely to remain a static quantity.²

To summarize briefly: (a) Mr. Gould is in order; (b) Mr. Elliott is in order; (c) "Free Grid" is in order, but conservative and a few degrees out of phase; (d) Mr. Wadden is a little "off-beam" but now I hope in daylight.

For which scandalous generalization I apologise.
"ANGSTROM UNIT."

Hadlow Down,
Sussex.

Line Scan Ringing

K. G. BEAUCHAMP in his article in the September issue makes a statement that the ratio of the ringing frequency to the flyback frequency is 2.7:1 and not 3:1, due to the booster diode conducting for more than one half cycle of the fundamental resonance. I disagree with this statement for the following reasons.

For a typical design one half cycle of the fundamental resonance is about 14 μ sec. For $1\frac{1}{2}$ cycles of oscillation the difference in time between the ratios of 3:1 and 2.7:1 is 1.55 μ sec, so if Mr. Beauchamp's statement is correct this will be the time the booster diode conducts in excess of one half cycle of the fundamental frequency. For a typical timebase the difference in potential of the booster diode cathode at the commencement and finish of the flyback is about 25 volts, due of course to the impedance of the valve. Since during the flyback period the peak potential to which the valve cathode rises is some 4,000 V, it is possible to calculate how long the diode conducts in addition to one half cycle of oscillation.

The instantaneous diode cathode voltage $e=4,000 \sin \omega t$

$$\therefore 25 = 4,000 \sin \omega t \\ \sin \omega t = 0.0065 = 0.37^\circ$$

$$0.37 \\ \text{Expressed in time} = \frac{1}{180} \times 14 \mu\text{sec} = 0.029 \mu\text{sec.}$$

This then is obviously not the reason for the ratio of the frequencies being 2.7:1.

If Mr. Beauchamp carefully examines the ringing frequency during the flyback period he will find the first and last quarter cycles are of shorter duration than the centre cycle. This is due to the capacities of the circuit being charged and discharged by the main flyback pulse. For minimum ringing during the scanning stroke exactly $1\frac{1}{2}$ cycles of the oscillation must occur during the flyback period and this is made up of one cycle of the ringing frequency at 2.7 times the fundamental, plus the charge and discharge times of the capacities. This is clearly shown on page 91 of *Mullard Technical Communications*, No. 14, August, 1955.

Mr. Beauchamp also states that with 5th harmonic tuning, better e.h.t. regulation can be expected. This is only true if the e.h.t. is lower for the 5th harmonic condition. For the same value of e.h.t. the regulation with 3rd and 5th harmonic tuning is similar. With 5th harmonic it is necessary to increase the overwind turns and this increases the leakage induc-

¹ Stilb = candelas/sq cm; a unit of intrinsic brilliance in a light-source or illuminant.

² And is not necessarily limited to that obtainable from the incidence of electrons on the phosphor in a c.r. tube.

tance, which results in a worsening of the regulation.

Mr. Beauchamp gives the credit for this method of tuning the leakage inductance of the line transformer to C. E. Torsch, but the original work was carried out by P. J. H. Janssen of the Philips Company in Holland and is described in Patent Specification 723, 510 the date of the application being December 19th, 1951.

K. E. MARTIN,

Mullard Research Laboratories.

Salfords, Surrey.

X-radiation from TV Sets

I NOTICE that on page 468 of your October issue, it is implied that a television receiver with a 24-inch tube employing 17 kV on its final anode may result in significant X-ray radiation.

My Association has been giving considerable attention to the problem of possible X-ray radiation from television receivers. While investigations are not yet complete, it can be stated that the viewing public has nothing to fear from this source when the set is operated inside its cabinet. Tests made with an e.h.t. voltage of 27 kV and a beam current of 500 μ A showed a barely detectable radiation at the front of the safety screen; at voltages below this there was no detectable radiation in a forward direction. At 20 kV and with a beam current of 800 μ A, there was no detectable radiation at any point on the outside of the cabinet, even when the safety glass implosion screen was removed.

The indications are that the critical voltage at which X-ray radiation commences to be significant is in the region of 25 kV, although this must be qualified by a number of other factors.

S. E. ALLCHURCH,
Secretary, The British Radio Equipment
Manufacturers' Association.

London, W.C.1.

"Do It Yourself" Interference

IN a recent series of weekly programmes in the B.B.C.'s Television Children's Hour Gilbert Davey has shown his youthful audience how to make a simple radio receiver.

The circuit is that of a one-valve regenerative detector—a dangerous source of heterodyne interference at any time and particularly when in the hands of a child whose knowledge of positive feedback is, understandably, limited. The tuning and reaction condensers are of the solid dielectric type so it would not be easy to adjust the set to the threshold of oscillation without contributing even more interference to the already chaotic state of the medium-wave band.

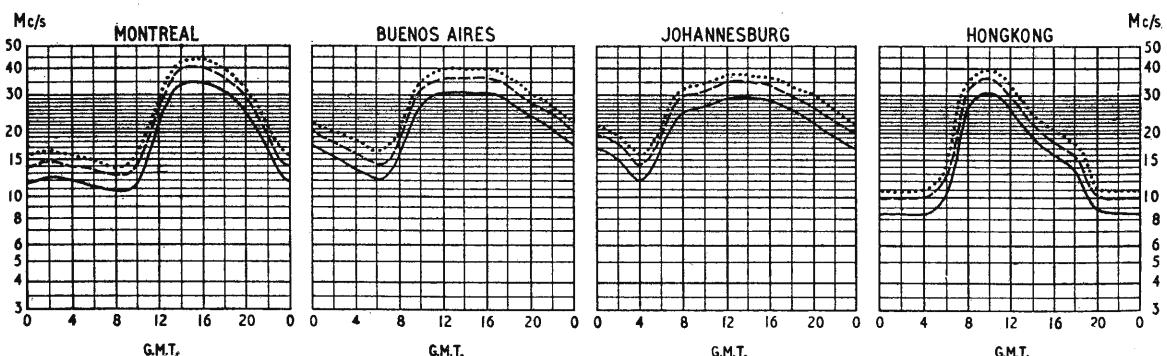
So we have the strange paradox of the B.B.C. Sound Broadcasting Service doing its best to improve reception for its dwindling listening audience and, at the same time, the B.B.C. Television Service giving to hordes of eager youngsters minute details for making an instrument which, basically, is a transmitter capable of ruining reception for thousands of listeners.

It is understood that the response to the Corporation's offer of printed instructions for making the set has been very large which would suggest that the Post Office radio interference sleuths can look forward to a busy season as thousands of one-valve transmitters, with youth at the helm, merrily join in the free-for-all "jam session" on the medium waves.

It is doubtful whether any appeal to the new set owners NOT to oscillate will have any greater effect than Capt. P. P. Eckersley's famous entreaty "PLEASE don't do it" from Two Emma Toc in the early nineteen twenties.

DOUGLAS WALTERS.
Godalming.

SHORT-WAVE CONDITIONS Prediction for December



THE full curves given here indicate the highest frequencies likely to be usable at any time of the day or night for reliable communications over four long-distance paths from this country during December.

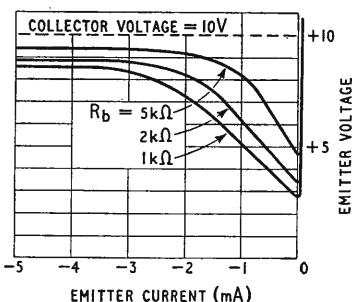
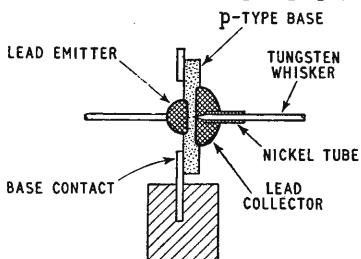
Broken-line curves give the highest frequencies that will sustain a partial service throughout the same period.

..... FREQUENCY BELOW WHICH COMMUNICATION SHOULD BE POSSIBLE FOR 25% OF THE TOTAL TIME

- - - PREDICTED AVERAGE MAXIMUM USABLE FREQUENCY

— FREQUENCY BELOW WHICH COMMUNICATION SHOULD BE POSSIBLE ON ALL UNDISTURBED DAYS

New Switching Transistor developed by the German Post Office was described by W. von Münch at the recent International Components Symposium at Malvern. It is constructed rather like an n-p-n alloy junction transistor, with lead-antimony emitter and collector electrodes alloyed on to a high-resistance p-type base. During the alloying process a tungsten whisker encased in a nickel tube is embedded in the collector so that it just penetrates the collector junction. When a resistance is connected in the base circuit the device has a negative-resistance characteristic rather like a point transistor (see emitter input graph).



This gives a regenerative action which produces a rapid switch-over, when the emitter is suitably triggered, from a high resistance condition (right) to a low-resistance condition (left). The electric field set up in the base region by the tungsten whisker accelerates the current carriers and thereby gives a switching time of only 0.1-0.2 μ sec. It is notable that this high-speed response is obtained with a transistor whose base region is as thick as that of an ordinary a.f. transistor. Pulse repetition rates of up to 2Mc/s can be handled by the device.

8½ r.p.m. Record development was described by Dr. P. Goldmark of the Columbia Broadcasting System Laboratories at the ninth annual convention of the Audio Engineering Society held recently in New York. These records were developed under the sponsorship of the American Foundation for the Blind, and are designed for speech reproduction. This allows the groove amplitude to be the same as that on the 16½ r.p.m. records using a $\frac{1}{4}$ -mil radius stylus tip also developed by the C.B.S.

Technical Notebook

Laboratories for the Chrysler car record player (described in *Audio Engineering* for December, 1955). The upper frequency limit is, however, halved, but for speech this limitation is not serious. A 7-in diameter record provides four hours of speech, and a 12in record 10 hours. The same tone arm as in the car record player is used. A viscous fluid in the vertical bearing damps out any tendency for the pickup to move relative to the record when the whole player is moved horizontally, while still providing a bearing free enough to allow the extra fine record grooves to be tracked with a stylus force of only two grams. The pickup cartridge in the arm is balanced about a horizontal axis, and the arm itself is rigid in a vertical plane, so that vertical movement of the player as a whole also does not displace the stylus from the groove. Moreover, if the pickup is accidentally moved by hand across the playing surface only the stylus force acts on this surface, and this force is so low that any scratches produced are not audible. This is an important advantage for blind users and is also, of course, valuable in the original car record player application.

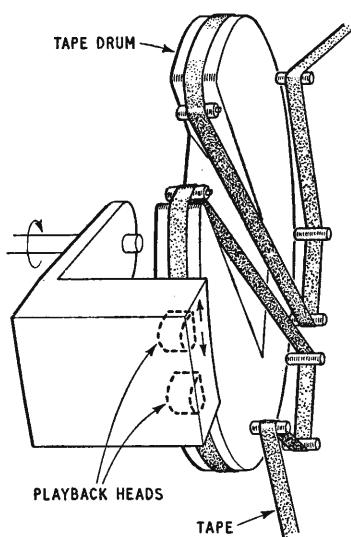
Half-Century Time Constant is claimed for three 1- μ F capacitors, shunted by their own insulation resistance of 1.5×10^9 ohms, which have been on test so far for six years at the Telegraph Condenser Company. At the beginning of the six-year period they were charged to 500 volts and are now still well above 400 volts. The high insulation resistance has been achieved by the use of plastic film dielectrics, which are now tending to replace paper for low leakage applications. Very thin films are desirable to reduce the size of capacitors, and development is proceeding on polystyrene films of only 0.0001-0.00025 inch in thickness. It is expected that capacitors of up to 1 μ F for operation at a maximum of 50 volts d.c. will be possible using metallized films of this type. These, of course, will be very suitable for transistor circuits.

Analogue Divider produced from a combination of rectangular-hysteresis-loop magnetic materials and transistors used as switches is described by D. H. Schaefer in un-

published report PB111969. The device gives an average output voltage which is the quotient, with correct sign and accurate to $\pm 2.5\%$, of two input voltages. An extension of the principle to a much more general computing element is discussed, and this gives an output proportional to various functions containing quotients.

Frequency Shift Modulation, a quantized system loosely comparable with frequency shift keying, is suggested as a means of obtaining high quality sound radio transmission through a dispersive medium, such as the ionosphere, in unpublished report PB118806 by L. B. Argumbau, J. Granlund, E. E. Manna and C. A. Strutt. This follows an account of experiments investigating the possibility of using frequency modulation techniques to establish a transatlantic radio link of local broadcast quality over an ionospheric path. It is concluded that ordinary frequency modulation would not be successful because of the complexity of the ionospheric path.

High-Speed Correlation Computer. —The sketch shows in simplified form the mechanical system of the Ramo-Wooldridge device mentioned in September. A 28-inch length of magnetic tape from the storage reel

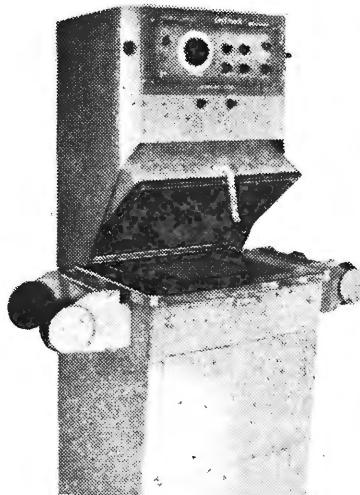


is held stationary on the fixed drum, while an arm carrying the two playback heads rotates about it. For each revolution the heads are automatically displaced one step by a cam mechanism, the range of travel being from zero displacement to 2.5 inches. A head amplifier is mounted on the rotating arm and its output is fed out by means of slip rings and brushes.

Oxide Film Resistors, using mixtures of tin and antimony oxides, should soon be in commercial production in this country. They are notable for good thermal stability and should be capable of high temperature operation. The films have a high resistance to abrasion which makes them particularly suitable for potentiometer elements, although there is also a high contact resistance between the element and wiper which may prove a disadvantage. In manufacture, the oxide films are prepared by spraying chloride solutions of the tin and antimony on to heated glass or ceramic bases. The process is said to be relatively simple and reproducible, permitting good control over the chemical properties of the film. Examples were shown at the recent International Components Symposium at Malvern and described by G. V. Planer, of Planer Laboratories.

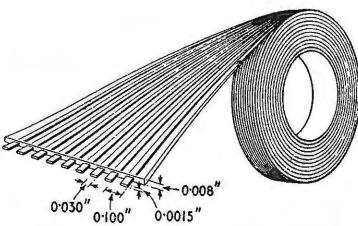
Stone-like Qualities are said to be possessed by an inorganic plastic called Rosite which is now being manufactured in this country by a subsidiary of Plessey. Chemically it is a calcium aluminosilicate with a microscopic grain structure, integrally reinforced with asbestos fibre. It has inherent heat resistance, arc resistance and dimensional stability at high temperatures, and is therefore suitable for many electrical applications.

Electronic Photo Printer.—Below is illustrated the American LogElectronics equipment described in our November issue.



ber 1957 issue (p. 547) which is now being handled and further developed in this country by E.M.I. Electronics.

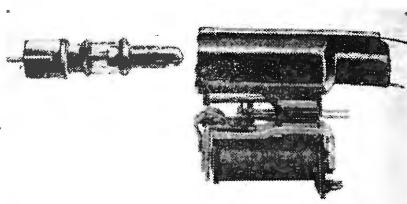
Flat Tape Cable, a new type of multi-conductor cable made by the Tape Cable Corporation of New York, is notable for its small cross-sectional area and low capacitance between conductors compared with equivalent conventional cables. Described in the September, 1957, issue of *Electronic Industries*, the cable is a ribbon-like flexible film of transparent polyester insulation with flat copper conductors only 0.0015 inch thick embedded in it. A 100-ft. roll of 50-conductor tape cable weighs only 2½ lb, which is said to represent a saving of 85% in copper over conventional types. The capacitance



between conductors is claimed to be less than 5pF per foot, while earthing alternate conductors reduces this to less than 1pF per foot in free space. The cable is particularly suitable for making flexible connections between chassis or sub-assemblies, such as printed circuit boards, and has been used successfully in applications requiring a continuous flexing on a radius of $\frac{1}{4}$ inch.

Zinc Capacitor Electrodes are said to be far superior to aluminium for metallized paper capacitors in an unpublished report (PB111715) from the Sprague Electric Company of America. A solid hydrocarbon is considered to be the most suitable impregnant. The temperature characteristics of metallized capacitors are shown to be equivalent to those of foil capacitors, and samples have been found to be satisfactory after 1,000 hours at 85°C and at 1-5 times the rated voltage.

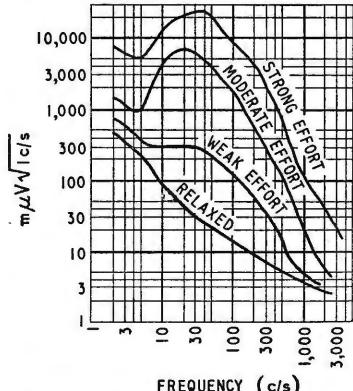
Relay Vacuum Switch recently introduced by Engel and Gibbs is a small evacuated glass tube containing contacts which can be operated by the armature of a miniature relay. Voltages up to 2000V, a.c. or d.c., can be switched in the space occupied by a miniaturized Post Office type relay, with a maximum switching capacity of 2kW. There is no arcing, of course, as the make and break occur in a vacuum. The switch is operated mechanically from the outside through a metal diaphragm, requiring a force of approximately 85 grammes. It is silent in operation and can be used in any position. A switching frequency of 20 operations



per second is possible with non-inductive loads and 3 per second with inductive loads. The actual tube is contained in a plastic case which provides protection and insulation and also positions the device accurately on the relay.

Electrolytic Oxygen Generator has been developed by the U.S. Naval Research Laboratory from a standard commercial nickel-cadmium battery by replacing the nickel oxide plates with sheet nickel ones. Since the cadmium plates do not gas during most of a charge or discharge and the inert plates gas continuously, a single gas is produced in a cell at any time. The battery type of construction is said to be advantageous in both weight and size. Details are given in unpublished report PB121245.

Muscle-Potential Spectra shown below were obtained from the thigh muscle of a man by means of a Muirhead-Pametrada wave analyser when weak, moderate or strong efforts were made to contract the muscle and also when it was relaxed. This experiment was done at Guy's



Hospital Medical School in order to establish the frequency band required in the design of an electromyograph amplifier. The most important components associated with the contraction lie between about 10c/s and 600c/s (the values on the vertical axis being proportional to the square root of the power in a bandwidth of 1c/s). There is a discussion on the method of using the analyser on these random waveforms (including frequency analysis of amplifier noise) by A. Nightingale in the October, 1957, issue of the Muirhead journal *Technique*.



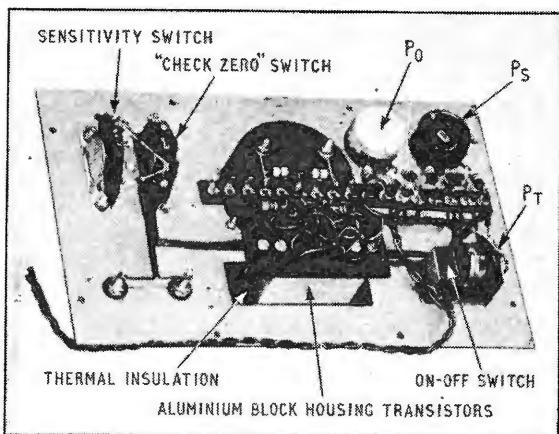
General view of null detector.

Sensitive D.C. Null Detector

A Transistorized Galvanometer Giving a Full-Scale Deflection for $50\mu A$

By FRANCIS OAKES,* A.M.I.E.E., A.M.Brit.I.R.E.,

M.Inst.E., and E. W. LAWSON,* A.M.I.E.E.



Underside view of panel

THE accuracy of measurement obtainable by bridge or potentiometer methods is frequently determined not so much by the accuracy of the standard resistors or voltage sources as by the sensitivity of the null detector available. This is particularly true in the case of routine measurements in production departments, inspection departments and routine laboratories where equipment has to be simple and robust because of its use by semi-skilled operators.

The availability of junction transistors capable of operating at extremely low current levels has made possible a substantial improvement in the design of null detectors in terms of sensitivity as well as mechanical and electrical ruggedness. In addition, the cost of an instrument of the type to be described is less than that of a conventional galvanometer of equal sensitivity, slower response and substantially greater mechanical and electrical vulnerability.

Basic Principles.—Junction transistors are capable of operation as d.c. amplifiers subject to limitations imposed primarily by their saturation currents and base-to-emitter potentials. These parameters are of the order of a few microamps and of about 100mV, respectively, at room temperature. Furthermore, they are subject to substantial changes due to temperature variation, difference in parameter values from unit to unit even of identical type being a further complication. In spite of these limitations, simple transistorized d.c. amplifiers can be constructed which are superior in performance to conventional amplifiers of comparable cost, provided advantage is taken of circuit techniques suitable for minimizing zero drift arising as a consequence of circuit parameter changes. Such techniques are primarily based on the use of balanced long-tail pairs and of stabilization of the operating point of transistors at low voltage and low current levels.

An amplifier embodying these techniques was

described in *Wireless World*, November, 1956.† Since then, new high-frequency transistors with smaller junction areas and smaller leakage currents have become available, and advantage was taken of this, by substituting such transistors in place of the low-frequency types originally recommended. With an input impedance of approximately $20k\Omega$ and a current gain of the order of 1,000, feeding into a $50\text{-}0\text{-}50\mu A$ moving-coil instrument, a suitable basic unit is provided round which to build the instrument.

Circuit Arrangement.—The main issue in deciding on circuit arrangements for this type of instrument is to make a suitable choice for the placement of sensitivity controls. In principle, two alternatives are available: (a) attenuation in front of the amplifier, (b) attenuation further along the amplifier chain or at the meter terminals.

Method (a) was chosen for the following reasons: Attenuation in front of the amplifier affords maximum protection from damage by overloading. The amplifier will stand an overload of approximately 1,000 times full-scale deflection. Thus, if the sensitivity is cut to 1/10 and 1/100 to provide alternatives to the most sensitive range, the instru-

* Ferguson Radio Corporation Ltd.

† D. M. Neale and F. Oakes: "Transistor D.C. Amplifier."

ment can accept 1 volt, 10 volts and 100 volts at the input terminals without sustaining damage, whilst a null can still be detected with a discrimination of $20\mu\text{V}$, $200\mu\text{V}$ and 2mV respectively.

Method (b), on the other hand, would offer the advantage of greater zero stability on the attenuated ranges. For use of the instrument as a null detector, this is of minor importance, however, as the final check is always made on the most sensitive range. A complete circuit diagram of the instrument is shown in Fig. 1. The schematic circuits in Fig. 2 indicate the actual input connections at the three sensitivity control settings.

Construction.—The instrument is housed in a small box containing the $50-0-50\mu\text{A}$ moving coil meter, which is very robust in comparison with a galvanometer of a sensitivity approaching that of this instrument, i.e., $0.05\mu\text{A}$ full scale.

The sensitivity can be varied by means of a spring-loaded range switch arranged to return to the minimum sensitivity position. The medium and maximum positions can be locked in, if desired, by means of catches on this switch.

For setting up, two zero controls are required, to adjust for open-circuit input and short-circuit input respectively. These adjustments are facilitated by a second switch, spring-loaded to return to normal working position. Moved up, it removes the input signal and short circuits the amplifier input, moved

down it opens the input terminals. By this means, zero adjustment can be checked rapidly and without removing the signal source from the input terminals.

In order to minimize zero drifts, the transistors are mounted in holes drilled into an aluminium or brass block and by insulating this block against ambient temperature variations. Each transistor is wrapped with copper foil until a tight fit in the hole.

Before setting up, a few minutes must be allowed for the collector temperatures to settle, after which the zero adjustments can be made and the instrument is ready for use. In case of frequent or continuous use, it may be preferable to keep the instrument permanently switched on; with a total current drain of the order of only 2mA , battery replacement is not a serious problem, and the additional stability and immediate availability for use may well justify the extra cost.

Performance Data:

Sensitivity: $0.05\mu\text{A}$ full-scale deflection.

1mV full-scale deflection.

Resolution: 10^{-9} amperes.

2×10^{-5} volts.

2×10^{-14} watts.

Zero drift: Short term. Not more than 5% of full-scale deflection for 10 minutes at constant ambient temperature.

Long Term. Depends on ambient temperature changes.

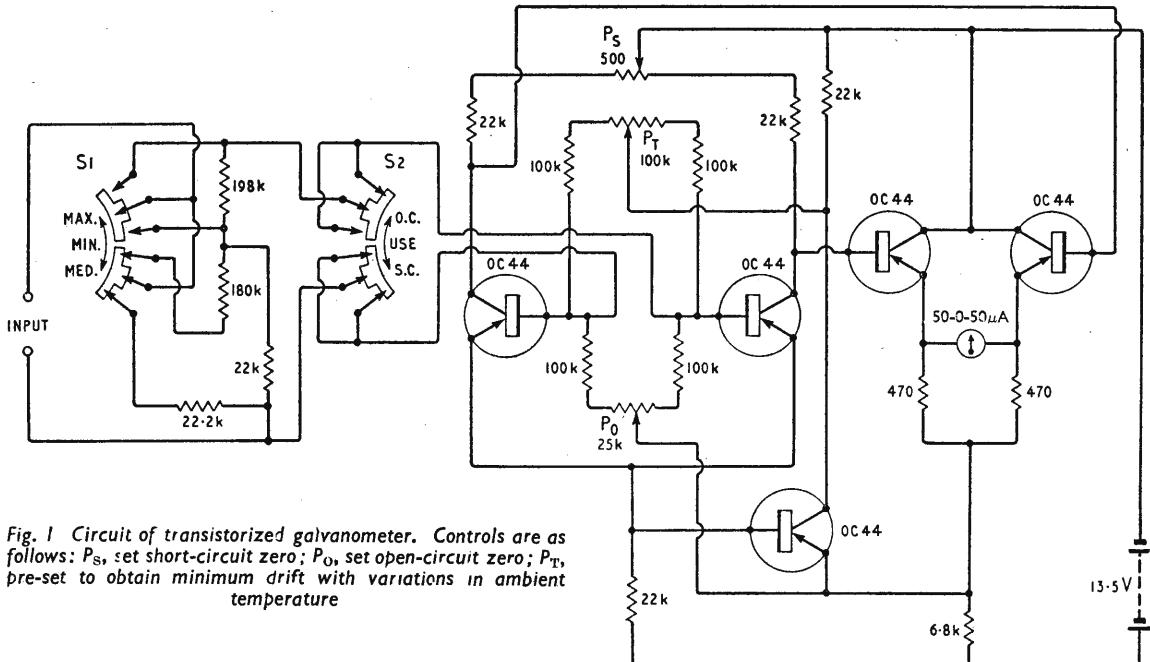
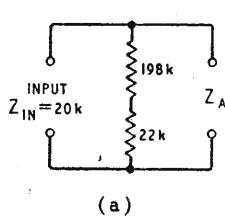
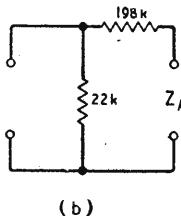


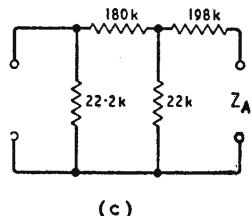
Fig. 1 Circuit of transistorized galvanometer. Controls are as follows: P_S , set short-circuit zero; P_0 , set open-circuit zero; P_T , pre-set to obtain minimum drift with variations in ambient temperature



(a)



(b)



(c)

Fig. 2 Attenuator circuit arrangements. (a) Maximum sensitivity, gain 1,000. (b) Medium sensitivity, gain 100. (c) Minimum sensitivity, gain 10. The input impedance of the amplifier Z_A is $22\text{k}\Omega$, nominal

Aerial/Propagation Mismatch

By R. J. HITCHCOCK,* M.A., A.M.I.E.E.

THE success of the first transatlantic submerged repeater cable and the planning of a second emphasises the resurgence of the cable as a serious competitor to radio circuits for long distance point-to-point traffic. This seems an apposite moment therefore to see whether the h.f. point-to-point services as a whole are exploiting their propagation medium, the ionosphere, to the greatest possible extent.

By using the most modest form of equipment and aerial, costing no more than a few pounds, it is possible to communicate at some time of the day with the most distant parts of the earth. While this phenomenon may be exciting and useful to radio amateurs it has had an unfortunate effect on those financially responsible for the development of point-to-point systems. It has resulted in economies in sites and aerials and in attempts to obtain more out of radio services than the often limited engineering facilities warrant. In this respect the cable engineer has been more fortunate, in that his communication link must be completely engineered before one word of traffic can be passed.

The advent of leased channel and automatic circuit operation have resulted in the demand for higher circuit performances over the radio path. Whilst constant improvements in equipment are partly meeting this demand, much could be achieved by applying our steadily increasing knowledge of propagation to the design of aerial systems.

Early Lack of Propagation Data.—Serious h.f. point-to-point communication within the Commonwealth can be said to have started about 1927 with the completion of the last of the four Franklin beam array services linking the United Kingdom with the Dominions of Australia, Canada, India and South Africa. It is interesting to reflect that at the time these aerial arrays were planned and erected our knowledge of the ionosphere was still in its infancy and in fact the means of scientifically exploring the ionized layers postulated by Heaviside had not yet been established. That the characteristics of these arrays very closely match the mechanics of propagation now known to exist makes the design of the Franklin beam aerial all the more remarkable, and it was indeed unfortunate that owing to their high cost and inflexibility few such aerials were erected.

It was another thirteen years before Appleton and Beynon¹ published their solution to the problem of a ray propagating through a curved layer with a parabolic ionic-density/height relationship. During all this time the number of h.f. communications systems had steadily increased and more often than not the new services were opened on relatively small

wide-band aerials at restricted sites. Of necessity these aerials had to be sited and constructed with insufficient scientific knowledge of the propagation characteristics likely to be met with along the route. Thus throughout the formative years of their development, only a very limited amount of ionospheric data was available on which to base the planning of h.f. services.

Modes of Propagation.—Information on modes of propagation, i.e., the exact path whereby h.f. radio signals travel between two points on the earth's surface using the ionosphere as the medium of propagation, is still very limited.

In the past it has been usual for communications engineers to make simple mode models depicting a series of equidistant hops between the ground and a thin mirror-like reflecting layer at some finite height, usually representative of the F₂ layer. Because such simple mode models consider neither the relative influences of the several

layers nor take account of the distance a ray may travel within the F layer during refraction, results based on simple mode methods have been very misleading.

After the second world war there was a tendency to assume that our knowledge of h.f. propagation was complete or at least adequate and to move on to the new problems of v.h.f. During the sunspot minimum period 1953-54, however, it became apparent to many users of point-to-point h.f. that predictions of optimum frequency based on simple modes of propagation often failed. In order both to improve these predictions and to achieve a sounder basis for the design of aerial systems it became evident that far more information on modes of propagation was needed.

During the last three years considerable work has been done on this subject at the Radio Research Station of the Department of Scientific and Industrial Research. In addition to pulse tests on fixed frequency stations as far apart as Osaka (Japan) and Ascension Island, a transportable equipment capable of variable frequency operation is now in use². It is not the purpose of this paper to discuss the methods whereby the active modes of propagation along any great-circle path can be deduced from observations of pulse transmissions except to note that the main measurements consist of (a) observing the angle of elevation of the down-coming rays as described by Wilkins and Minnis³, and (b) observing the break-up and relative arrival times of the various components of the original pulse. In addition further valuable information on modes of propagation is being

* Cable and Wireless Ltd.

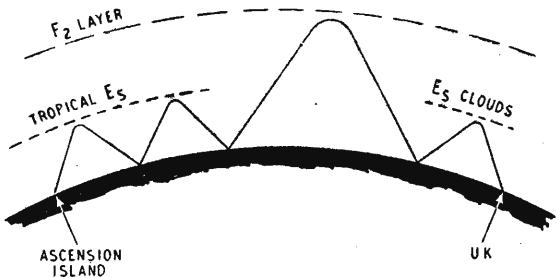


Fig. 1. Typical propagation mode between Ascension Island and the United Kingdom. The diagram is not to scale and the arrival angle is actually 6° to the ground.

obtained from the back-scatter observations described by Shearman.⁴ Although only a small part of the Radio Research Station's observations and conclusions have yet been published⁵, the complexity of aligning possible propagation modes to the observed results is an exceedingly difficult task. On the Ascension Island/U.K. path where nearly 5000 observations have so far been made it is apparent that during daylight the first two or three hops from Ascension are between the earth and the tropical sporadic E layer, the remaining hop or hops being via the F₂ or temperate E_s clouds⁵ (Fig. 1). The most interesting feature of these tests is the confirmation that the predominant modes arrive at very low angles of elevation, in fact the arrival of two main modes below 7° was a normal occurrence.

Advantages of Using Low-angle Modes.—The correct exploitation of these low-angle modes results in two very definite advantages to the user of h.f. In the first place the least attenuated mode is the one arriving at the lowest angle, that is to say the mode suffering the fewest number of ground and ionosphere reflections.

Calculations of the attenuation suffered by different modes is naturally complex and will vary with circuit, frequency, time, season, type of ground at earth reflection point, etc. On a medium distance north-south multi-hop circuit of the order of 7000 km, for example, where the ground reflection points are over land and only propagation via the F₂ layer is considered, the total attenuation of the lowest ray during the daytime is likely to be some 6–8 dB less than that for the next highest ray. During the night this gain will probably be reduced to the order of 4–6 dB. To this may be added the relative gains due to focusing caused by layer curvature (usually called convergence gains). This focusing effect is greatest for near tangential rays and therefore the highest gains occur on the lowest angle modes. Taking into account theoretical values⁶ of convergence gains for the same sort of circuit, and assuming that the gains of both transmitting and receiving aerials are constant throughout the vertical plane, then the field strength of the mode with the lowest angle of arrival might be expected to be some 9–11 dB above that for the second highest arrival angle.

The second great advantage to be gained from exploiting the lowest angle mode is that this mode will be present for the longest possible time; in fact near the fade-in and fade-out periods it will be the only mode to propagate. Kift⁵ has shown that the operating time gained can be very considerable. On the Ascension Island/U.K. circuit in April 1956, for

example, the lowest mode (4°) at 20 Mc/s would be present from about 0700 to 2000 G.M.T. whereas a higher angle mode at 12° would only be present from about 0930 to 1900 G.M.T.

It has been shown that the lowest angle mode has both the greatest potential field strength and the longest operating time. That full advantage of this has seldom been taken in the past is probably due to two reasons which may well be interconnected. In the first place there has unfortunately existed a belief that angles of arrival were considerably higher by night than by day, this seems to have been coupled with the generalization that low frequencies necessarily meant high angles, day or night. Of course in certain circumstances low frequencies are necessarily associated with high angles but as a generalization there is no validity for the belief. Appleton and Beynon¹ have shown that for a thick parabolic layer at a given height and thickness, provided the angle of incidence of the ray with the layer remains constant, the distance the ray penetrates through the ionosphere depends on the ratio f/f_0 where f is the transmitted frequency and f_0 the critical frequency at the area of refraction. In practice, over much of the route, the ratio f/f_0 is often higher by night than by day resulting in greater hop lengths by night. Quite often, therefore, on multi-hop circuits the main angle of arrival will be lower by night than by day. (Of course hop lengths will in any case be slightly different by night as layer heights either increase or decrease, depending on geographical location.)

The second reason why low-angle modes have seldom been exploited is to be seen in the inherent nature of aerials themselves. For example, if on a certain circuit, where the day frequency is 19 Mc/s and the night frequency 8 Mc/s, low-angle modes arrive at about 7° both night and day; then for simple horizontal dipoles to have their major lobes at this angle, the one for 19 Mc/s would need to be 120ft above ground and that for 8 Mc/s 280ft above ground. Masts for such aerials are not often available. This discrimination by horizontally polarized aerials against low-angle modes at low radio frequencies (Fig. 2) may well have significantly contributed to the belief that at night only high-angle radiation existed.

"Avoidable Aerial/Propagation Matching Loss"—If it is assumed that the angles of arrival and departure are equal then it is obvious that on an h.f. circuit optimum performance on any given frequency is achieved when the major lobes in the vertical plane of any given transmitting and receiving aerials both coincide with the lowest active mode of propagation. If we define this state of affairs as entailing no "avoidable aerial/propagation matching loss" then it is interesting to see the magnitude of the loss suffered by typical point-to-point systems in use to-day.

Consider a middle-distance route of the order of say 7000 km where both the transmitting and receiving aerials are medium-sized rhombics limited in size to about 350ft side length and in height to about 100ft. (This can be considered typical of many of the better international and inter-Commonwealth stations.) The frequencies used on such a route will probably vary from 7 to 20 Mc/s and for the purposes of this example predominant modes of the orders of 4° and 12° have been taken as representa-

tive of those met with in practice. If both aerials are at the top of their respective masts then the following approximate " avoidable aerial/propagation matching losses " can be expected to occur on these high and low angle modes as the various frequencies are used:

Main Mode	Order of Frequency.			
Arrival Angles	20 Mc/s	15 Mc/s	10 Mc/s	7 Mc/s
4°	-2 dB	-4 dB	-12 dB	-17 dB
12°	-15 dB	-11 dB	-10 dB	-11 dB

If the aerial height was limited to 70ft, a limitation still met with in practice, then for the same angle of elevation, path lengths, etc., the approximate " avoidable aerial/propagation matching losses " might be expected to be:

Main Mode	Order of Frequency.			
Arrival Angles	20 Mc/s	15 Mc/s	10 Mc/s	7 Mc/s
4°	-4 dB	-5 dB	-14 dB	-20 dB
12°	-12 dB	-11 dB	-12 dB	-15 dB

The above figures are computed from the relative gains of the theoretical polar diagrams of both transmitting and receiving aerials at the required angle of elevation and operating frequency as well as average values of different mode attenuation and convergence gains. When it is also considered that the lowest mode is always present and will normally exist for considerably more of the time than the higher modes, particularly near the fade-in and fade-out times, then the degree to which many of the present h.f. systems fail to make use of their propagation medium is evident.

Reducing the Losses.—If the 15-, 10- and 7-Mc/s transmissions in the above example were made from transmitting and receiving aerials of the same size but at 150ft above ground then the approximate " avoidable aerial/propagation matching losses " might be expected to reduce to the order of:

Main Mode	Order of Frequency.			
Arrival Angles	15 Mc/s	10 Mc/s	7 Mc/s	
4°	-2 dB	-3 dB	-4 dB	
12°	-14 dB	-10 dB	-9 dB	

Thus without enlarging the aerials it should be possible, by increasing the height from 100ft to 150ft, to increase both the operating time and circuit gain. It will be seen that this latter figure theoretically varies from about 2 dB at 15 Mc/s to 7 dB at 10 Mc/s, with the gain at 10 Mc/s increasing to 9 dB during periods when only the lowest mode is propagating. Further overall circuit gains could be achieved by increasing the size of the rhombics, but unfortunately site limitations often make this impossible in practice. (It is estimated that if the transmitting and receiving aerials in the foregoing example were increased to 550ft side length, against the 350ft side length considered, a further circuit gain of the order of 5 to 6 dB could be achieved at 10 Mc/s.)

Characteristics of large and high rhombic aerials at the new Rugby " B " station of the British Post Office have been discussed by Booth and MacLarty⁷ and Cook and Hall⁸. It must remain questionable, however, whether it is a wise concept to consider non-resonant aerials such as the rhombic capable of producing suitable radiation characteristics over a wide range of frequencies, say of the order of one octave. The angle of elevation of the main lobe

will vary considerably over this range and consequently discriminate against the low angle modes for much of the time. To reduce these losses to a minimum it is considered that an aerial should only be used over a relatively narrow band of frequencies and that the average 24-hour radio circuit requires four designs of aerial to cover the sunspot maximum and sunspot minimum day and night frequency ranges. It has been found that by this means it is usually possible to restrict the design of any one aerial to the approximate frequency range 1 to 1.4. Of course, only two of the four designs need be erected at one time.

Conclusions.—Many point-to-point h.f. circuits in operation to-day are unnecessarily inefficient because aerial designs are not matched to the predominant modes of propagation. Although our knowledge of modes is still very limited it is steadily growing and in the near future methods are likely to be evolved whereby mode prediction will be practicable. In the meantime current research indicates that on medium and long distance circuits the low angles of arrival predominate over all other angles both by day and night and the exploitation of these low angle modes, by increasing aerial heights, would result both in increased operating hours and increased circuit gains. In addition many

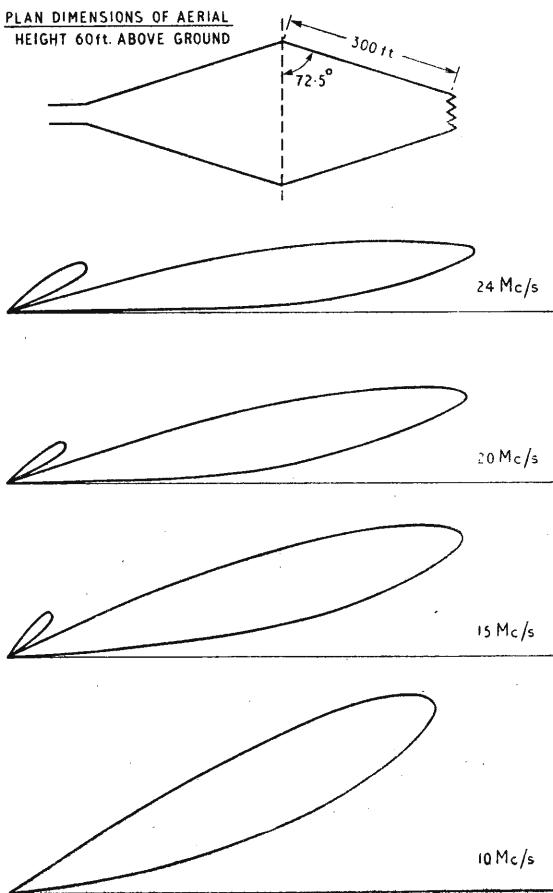


Fig. 2. Variations in angle of elevation of major lobe of a typical rhombic aerial with changes in frequency.

h.f. services are trying to operate from inadequate sites where space is insufficient to allow the construction of larger, higher-gain aerials.

The overall gains to be achieved from improvements to aerials and sites are considerable. It is estimated that on many existing point-to-point services gains of from 10 to 15 dB are possible on the lower frequencies. This could be of considerable importance during sunspot minimum years when operating frequencies are of necessity low and circuit performance often poor.

Further, in order that the "avoidable aerial/ propagation matching loss" should be kept to a minimum it is considered that non-resonant aerials such as the rhombic, which are generally considered to have a wide frequency range of the order of 2 : 1, should normally be confined to much narrower frequency limits.

ACKNOWLEDGEMENT.—The author would like to acknowledge most helpful discussions with Mr. F. Kift.

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Radio Teleprinter Equipment

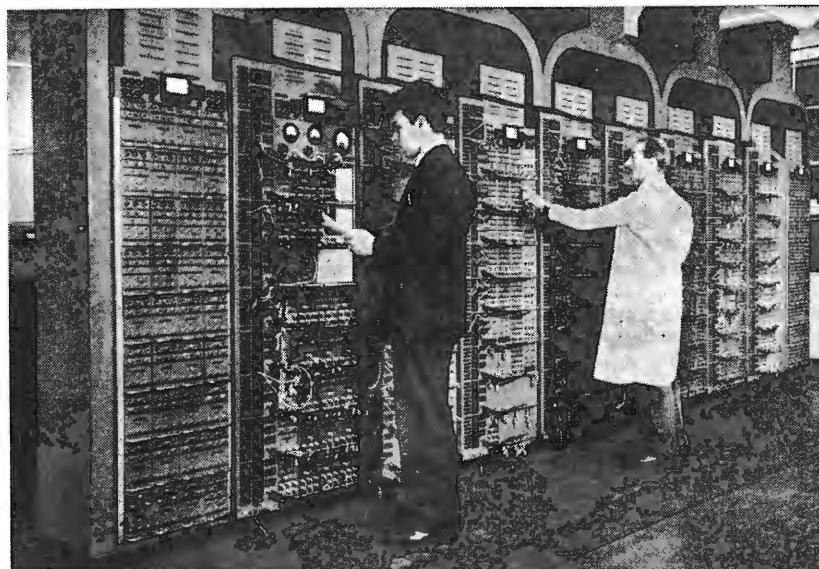
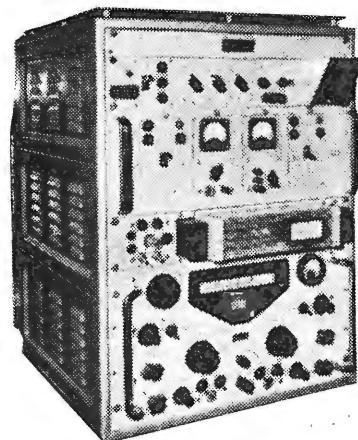
THE unconventional Type RA17 communications receiver, described in the August 1957 *Wireless World*, forms the heart of a new frequency shift keying (FSK) radio teleprinter receiving equipment introduced by Racal Engineering. Known as Type RA62 this FSK receiving terminal, as it is called, comprises, in addition to the RA17, the Frequency Shift Converter Type FSW1, Cathode Ray Monitor Type CRM1 and, as an optional unit, Regenerative Repeater Type TRR2. All four are shown in the illustration housed in a cabinet measuring 30in high, 21in wide and 30in deep, and weighing 213 lb. Provision is made for operation on a.c. supplies of 50 to 60 c/s at 100 to 125 or 200 to 250 volts.

The audio output from the receiver, which is on 600 c/s or 2,550 c/s according to the deviation used, is amplified and shaped in the FSW1 unit and emerges as d.c. mark and space pulses of suitable amplitude for direct operation of a teleprinter, or tape perforator.

The CRM1 unit is a compact oscilloscope designed specifically for monitoring the audio output of the receiver, and it serves also as an aid to tuning.

The function of the TRR2 regenerative repeater is to generate distortionless telegraph signals from input signals which may carry heavy and variable distortion and, which, without correction, are likely to impair the satisfactory working of a teleprinter. It is also particularly useful in relay circuits where the received signals are re-transmitted.

The makers are Racal Engineering, Ltd., Western Road, Bracknell, Berks.



CONTROL SYSTEM SIMULATOR using purely electronic techniques has been designed and built by E.M.I. Electronics. Known as GATAC, it is actually an analogue computer and is intended primarily for studying the complex non-linear three-dimensional control problems associated with guided weapons. It is said to be capable of simulating the control, guidance and propulsion systems and the aerodynamic performance of any existing British guided weapon. Recent work has been on the Naval guided weapon SEA SLUG. The computer also has general application to the study of industrial control systems such as in chemical and nuclear engineering.

"Grid-Diode" Saw-Tooth Generator

By T. A. MENDES, M.B.E.

THE saw-tooth generator to be described was developed by the writer in the course of building a general-purpose oscilloscope, and has been in use for some time now, giving excellent results. To the best of his knowledge and belief it is new. Using common types of valves, it is almost ridiculously simple to set up, and provides a constant-voltage output that is independent of frequency, together with voltage and current pulses suitable for flyback black-out application. Its frequency range extends certainly to 250 kc/s and probably higher; it synchronizes readily; the valve heaters may be run from an existing earthy supply.

The output voltage is too low for direct application to the deflector plates of a c.r.t., a fact that some may consider a major disadvantage. But is it? A circuit that develops a voltage high enough for such direct application has disadvantages of its own: at least one extra valve, and sometimes two, are required to achieve reasonable linearity; the voltage applied to the c.r.t. is asymmetric, leading to trapezium distortion and deflection defocusing; the amplitude control varies the sweep frequency as well as the width of the trace. There is gnashing of teeth when the time base is not in use (as for phase-shift tests, etc.), and no X-amplifier is forthcoming.

In the low-voltage circuit there is no difficulty about linearity if the charging source is high enough, and the valves saved from "linearity duty" can be applied as an amplifier (preferably push-pull), thus clearing up all the difficulties listed above. The circuit to be described is therefore of considerable practical as well as academic interest.

As is usual, the saw-tooth voltage is produced by charging a capacitor slowly through a high resistance, then discharging it rapidly through a low resistance. As, however, part of the discharge path is the diode formed by the grid and cathode of a triode, it may be as well, before proceeding to the actual circuit,

A SIMPLE TIME-BASE CIRCUIT WITH A WIDE FREQUENCY RANGE

to recapitulate some of the peculiarities of triodes in the positive-grid region.

Consider, then, Fig. 1, which is the anode-volts/anode-current curves of a typical small triode—one section of a 6J6. Any triode will be represented by a similarly shaped and grouped "family," only the scales varying from type to type. It will be seen that in the positive-grid area all the curves run together into one curve, which may be termed the asymptote. (This statement is not mathematically true, but is amply true for all practical purposes.)

"Freezing" the Working Point

The line AB in Fig. 1 is a 150 k Ω load-line drawn from an h.t. supply voltage of 350 V, and will be seen to cut the asymptote at the point where the " $E_g = 1.6$ V" curve (shown dashed) just enters it. If, therefore, the valve represented by the curves were connected in series with 150 k Ω across a 350 V supply, and the grid voltage gradually changed from some negative value into the positive area, the working point would move along the line AB towards the left—but only as far as the asymptote. Any increase in positive grid voltage beyond +1.6 V would merely leave the working point "frozen" on the asymptote. The anode voltage and current would remain unchanged for all values of E_g greater than +1.6 V. The grid voltage at which this "freezing" takes place will be referred to in what follows as the "freezing bias" and be denoted by E_f .

A further point of importance is that when the grid is positive it draws current from the bias source, and thus appears as a finite resistance. The value of this "diode" resistance—which we shall denote by r_d —may be obtained either from the valve curves if available or by experiment. It is not constant, but may be considered so for what follows. In general it is of the order of 200 or 300 ohms, a figure that in the writer's experience is suitable as a first approximation for any small triode.

We may now turn to the actual circuit, which is shown in Fig. 2. Here V1 is a small medium- or high-mu triode ($\frac{1}{2}$ 6J6) with the characteristics sketched in Fig. 1. V2 is a small beam tetrode (6AQ5). R_c biases V2 to the required anode current. R_g is of course merely a grid leak. The remaining components will be discussed later.

A brief outline of the operation of the circuit, shorn of all details, would run as follows: With capacitor C uncharged or only slightly charged, the cathode current I_k of V2 sets up across R_k a voltage E_k more than sufficient to cut off V1. C, however, charges slowly through R and a point is reached when the grid of V1 is carried sufficiently positive to approach the cathode voltage and allow

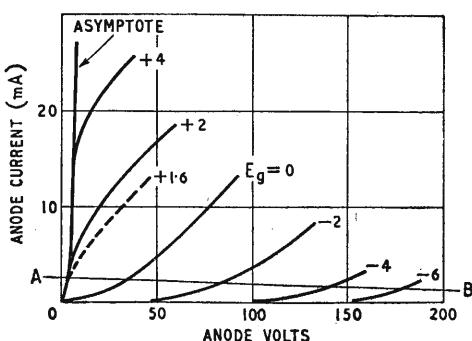


Fig. 1 Anode-volts anode-current curves of typical small triode ($\frac{1}{2}$ 6J6) showing positive-grid characteristics, with 150 k Ω load-line drawn from 350 V.

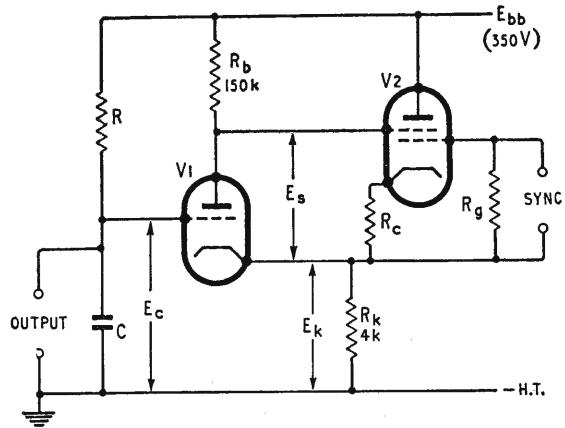


Fig. 2 Basic circuit of the "grid-diode" saw-tooth generator.

V1 to conduct. The plate current of V1 reduces E_s , which in turn reduces I_k and consequently also E_k , carrying the cathode of V1 negative and further increasing its anode current. The action is cumulative, and E_s abruptly drops to so low a value that V2 is effectively cut off, while the grid of V1 is suddenly left positive to its cathode by a voltage greater than the "freezing bias." C now discharges through R_k via the diode formed by the grid and cathode of V1, and the grid voltage drops. E_s does not at first change, as the working point is frozen on the asymptote. Eventually, however, the grid-cathode voltage drops to the value of the "freezing bias" and tends below, so that E_s can begin to rise, thereby triggering off the reverse cumulative action, abruptly restoring the original voltage across R_k . V1 is once more cut off; C recharges slowly through R, and the cycle repeats.

Due to the d.c. coupling between the two valves the cumulative actions described are extremely fast, and may, to a very close approximation, be considered instantaneous.

With the foregoing brief outline in mind we can now make a more detailed examination of the processes involved, and develop design formulae.

If E_k and E_s are considered to represent the numerical values of these voltages at a time at which V1 is cut off, and if we write E_o for the cut-off bias of V1 at an anode voltage of E_s , then clearly V1 will start conducting only when C has charged to a voltage:

$$E_o = E_k - E_s \quad \dots \quad \dots \quad \dots \quad (i)$$

at which point V2 is suddenly cut off. With V2 cut off, the current in R_k is the sum of the grid current (I_g) of V1 which is supplied by the capacitor C, and the anode current (I_b) of V1 which is supplied by the h.t. line.

The voltage across R_k is now given by $R_k I_g + R_k I_b$, and since I_b is the "freezing bias" anode current of V1, and is thus known and constant, we may put $R_k I_b = E_x$ and it is clear that the source of I_g sees the common cathode resistor as a resistance R_k in series with a resistance-less generator developing a voltage E_x so polarized as to oppose it. Also in series is of course the diode resistance r_d of the grid-cathode path. Thus an effective voltage of $E_o - E_x$ is driving a current I_g through a load of $r_d + R_k$.

The grid-to-cathode voltage is that across r_d and is given by:

$$E_g = (E_c - E_x) \frac{r_d}{r_d + R_k} \quad \dots \quad \dots \quad (ii)$$

and for the circuit to work it is necessary for the value of E_g found from equation (ii) to be greater than the "freezing bias" E_f found from the curves for V1.

Now C discharges and E_c drops (while E_x remains constant) until the point at which the value of E_g given by equation (ii) equals that of E_f . The voltage across the capacitor at this stage we shall denote by E'_c and is found by substituting E_f for E_g in equation (ii) and solving for E_c . This works out to:

$$E'_c = nE_f + E_x \quad \dots \quad \dots \quad \dots \quad (iii)$$

where $n = (r_d + R_k)/r_d$, and at this point V1 is once more cut off and the cycle repeats. Apart from the initial long charge from zero to E_c then, the saw-tooth voltage across C consists of a slow rise from E'_c to E_c followed by a rapid drop back to E'_c . Thus the peak-to-peak sweep voltage developed is given by:

$$\Delta E_c = E_c - E'_c = E_k - (E_o + nE_x + E_x) \quad \dots \quad (iv)$$

The ratio of scan time (t_s) to flyback time (t_o) is of course a function of the ratio R to $R_k + r_d$, and obviously R_k is best held as low as possible. In practice R will generally be in two parts—one variable and one mixed. By proper choice of the value of the fixed resistor the time ratio can be held to a predetermined minimum—say 10:1. For those who may be interested, the time-ratio is given by:

$$\frac{t_s}{t_o} = \frac{R}{R_k + r_d} \cdot \frac{\log A}{\log B} \quad \dots \quad \dots \quad (v)$$

where:

$$A = \frac{E_{bb} - E'_c - \Delta E_c}{E_{bb} - E'_c}$$

and

$$B = \frac{E'_c - E_x}{E_c - E_x}$$

As a numerical example consider the circuit of

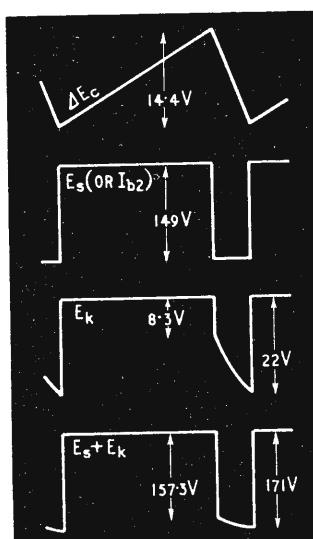


Fig. 3 Waveforms in the circuit. Voltages are for the numerical example discussed in the text. The flyback is shown disproportionately wide for clarity. Although "idealized", the curves drawn differ only very slightly from corresponding oscilloscope traces at frequencies at which stray capacitance is not troublesome.

Fig. 2 with R_c so chosen that the cathode current of V2 with V1 cut off runs to 16mA. This produces a voltage E_k of 64V. Let also $E_s = 150V$ when V1 is cut off. Reference to Fig. 1 shows that at an anode voltage of 150V V1 cuts off at -6V. This gives us $E_o = 6V$. Also from Fig. 1 we find $E_f = 1.6V$, and at this grid voltage E_s will be about 1V (quite low enough to cut off V2) while the anode current I_b is around 2.25mA. We may call this 2.5mA to account for the very small cathode current in V2, and this gives us $E_x = R_b I_b = 10V$. Since we have already found that r_d is approximately 200 ohms, our value for n works out to 21. These values inserted in equation (iv) yield a sweep voltage $\Delta E_e = 14.4V$, which should be sufficient to drive any amplifier.

Note here that to find E_f the load-line must be drawn from the full h.t. supply voltage E_{bb} , and not from E_s , since by the time the asymptote is reached V2 is cut off and may as well not exist.

Circuit Waveforms

At this point we may give some thought to the other waveforms in the circuit, and a moment's consideration will show that E_s and E_k as well as the anode current I_{b2} of V2 are in the form of negative-going pulses, the shapes of which are sketched in Fig. 3 along with the saw-tooth to indicate time-relationships. The curve at the trough of E_k is caused by the discharge current of C. The most easily available pulse is that between the anode of V1 and earth, and is the sum of E_s and E_k it is of a value and polarity ideal for flyback black-out (return-trace blanking).

Actually the circuit could be used purely as a pulse generator, producing either current or voltage pulses, the current pulses existing in the anode circuit of V2. The current pulse may with advantage be used to obtain a voltage pulse by inserting a low resistance in the anode circuit of V2. Since such a resistance would in general be very much smaller than R_b for an equivalent voltage, stray capacitance would be so much less troublesome at high frequencies.

Synchronization is straightforward, the mechanism being obvious from Fig. 2. However, input across R_g will not ordinarily be convenient, and the more normal method will be the application of the sync signal between the grid of V2 and earth. Unfortunately V2 then becomes a cathode-follower, and it would appear that a relatively large signal might be necessary.

However, while no quantitative investigation has been made, the circuit has been found to be quite sensitive to sync signals of the order of one volt or so, even with the input between grid and earth. The actual circuit used by the writer is shown in Fig. 4 and is extremely sensitive to synchronization. The d.c. coupling of the sync valve (V3) does away with the need for R_g and R_a of Fig. 2. The operating anode voltage of V3 must of course be less than E_k , but is quite sufficient if E_k is of the order of 40V or more.

What may be annoying in certain applications, is the transfer of the pulses across R_k into the source of sync signal via the grid-cathode capacitance of V2 (and the anode-grid capacitance of V3); but this can be rendered negligible by operating

V3 as a pentode, taking advantage of its very small C_{ga} .

Linearity is excellent, since C need never charge to more than 5% or so of the applied voltage, which in this case is $(E_{bb} - E_e)$. Since linearity is acceptable up to 15% charge, a lower source voltage could be used to enable smaller values of C to be employed for the same frequencies, or lower frequencies to be obtained with the same value capacitors. If such a low voltage source is obtained by dropping the h.t. supply, however, a voltage regulator valve is likely to be necessary. In any case,

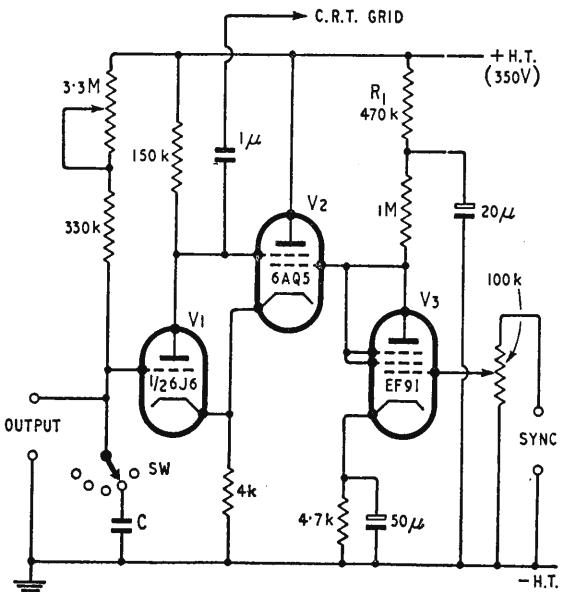


Fig. 4 Complete circuit as used by the writer, showing the (optional) sync amplifier valve, V3. The switch SW selects different capacitors for "coarse" frequency control, while "fine" control is provided by the 3-MΩ potentiometer.

purists may apply any trick "linear" circuits they desire (pentodes, cathode-followers, etc.).

As to amplitude, a glance at equation (iv) will show that ΔE_e is entirely independent of R and C, and hence of the repetition frequency. This is quite true in practice: the trace on the oscilloscope screen is constant whatever the setting of the "coarse" (C) or "fine" (R) frequency controls. While for long-term accuracy of calibration this may be not any too reliable, because of valve deterioration—especially since grid current flows—for short-term approximate work the constancy of output is a definite advantage.

No amplitude control has been provided in the circuit itself, since it is intended to work into an amplifier with a gain control. Any control that varies ΔE_e will necessarily vary the frequency as well—an annoying effect inherent in any amplitude control that directly varies the generated voltage. However, if an amplitude control is particularly desired, equation (iv) provides the clue: vary E_k . This is easily done by making R_c of Fig. 2 or R_i of Fig. 4 variable, and indeed such an arrangement could be quite handy if fitted as a pre-set control

for initial adjustment and occasional correction of calibration as valves age.

So much for the two-valve version actually used by the writer; it will be appreciated that the circuit is easily adaptable to use with the triode-pentode valves now so popular as mixers in v.h.f. sets. Such valves were not available to the author when this article was written but he did try—with tongue in cheek—the circuit of Fig. 5. Somewhat to his surprise, it worked extremely well, producing a

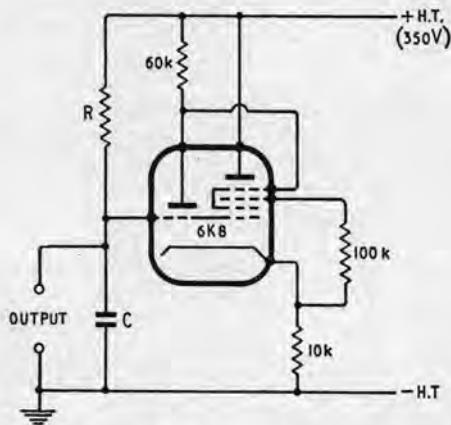


Fig. 5 This experimental version, using the once-popular American triode-hexode converter valve 6K8, produced an excellent saw-tooth of about 8V. Triode-pentodes such as 6X8, 6U8, etc., would probably be better.

saw-tooth every bit as good as that of the two-valve version, though E_s and E_k curves were humped and rounded, and unsuitable for flyback black-out use. This was probably due to the extension of the grid of "V1" into the cathode-to-anode stream of "V2," an effect that would be absent in the new triode-pentodes.

Many popular makes of oscilloscope still appear to be using the thyratron (gas-discharge) sweep generator followed by an X-amplifier, obtaining flyback black-out by differentiating the signal from the positive-going X-plate through a low time-constant coupling to the "grid" of the c.r.t. The circuit of Fig. 5 (or its triode-pentode version) is very strongly recommended as a replacement when the thyratron finally "goes," as its wider frequency range, its constant amplitude, and its cheapness make it well worth the small trouble of modifying.

Those who are interested, but have qualms about the complications of designing an amplifier, may rest assured. A single EF91 or Z77 operated from a 300-V supply with 250V on the screen and 1.5V bias will provide a practically distortionless output of 200V peak-to-peak across a 10,000-ohm anode load resistor for an input of 1.06V r.m.s. (3V pk-pk). This is ample for an average 5in c.r.t. as an X-amplifier. Assuming a total stray capacitance of 50pF the frequency response will be 3dB down at 320kc/s (1dB down at 160kc/s). A shunt-peaking 2.5mH choke in series with the anode resistor will improve this to 1dB down at 430kc/s (3 dB down at 580kc/s)—ample for a general-purpose oscilloscope. A pair of EF91s under the same conditions in cathode-coupled push-pull would provide the same gain

and a balanced output of 400V peak-to-peak. The amplifier is simple enough.

Finally, a few design considerations. The starting point will generally be the output voltage requirement, based on the input demands of the amplifier. It is as well to develop a voltage considerably in excess of the maximum input to the amplifier, if only to enable the trace to be "spread out." (The amplifier will distort, of course, but the distorted part of the trace will be off the screen.) Also it is desirable to keep the saw-tooth between 5% and 10% of the charging voltage in order to keep the value of C within bounds at low sweep frequencies.

Since it is desirable to keep R_k as low as possible, a low value of E_k is indicated, and hence low values for all terms within brackets in equation (iv). Thus a short-base, high-slope valve should be selected for V1 to keep E_s down, and the valve chosen should also have its asymptote as close to the zero volts ordinate as possible in order to ensure a low value for E_s during discharge. E_s and E_k depend on the value of R_b , which should be as high as possible, and here enters V2.

For V2 a valve with low screen current requirements is indicated, so that R_k can be kept high without too far reducing screen voltage. Beam tetrodes seem preferable to pentodes in this respect. Since a low value for R_k is in any case being aimed at, this takes care of n .

With the value of R_k tentatively decided, that of E_k is found, and the anode current of V2 derived. A little juggling with R_k and I_{b2} may be necessary to complete the job.

An alternative design method is that of throwing together a few reasonably assorted components and poking about till the desired output is attained; the circuit is a sufficiently persistent—not to say insistent—oscillator to permit of this approach. Had it not been the chances are that the writer, at any rate, would never have discovered it.

R.I.C. Specifications for Radio Materials

CARE is necessary when choosing metallic finishes for metal parts used in radio and other electronic equipment, as some combinations of plating and base metals can greatly accelerate corrosion under tropical conditions.

Contact potential must also be considered and a guide to the combinations found satisfactory in practice is given in the revised specification (Issue No. 2) of RIC/1000/B now being issued by the Radio Industry Council. The subject is choice of finishes in common use for metals; also for wood and insulating materials, including conducting coatings on glass and ceramic.

Concurrently available is RIC/1000/A giving guidance on the choice of materials for use in radio and other electronic equipment. Classes of materials dealt with include metals, plastics, insulating materials, wood, lubricants, wires, adhesives and soldering fluxes and elastomers. Grouped under the last-mentioned heading are natural and synthetic rubber, polythene, PVC and similar materials. Electrical and mechanical tests are described.

These specifications are not mandatory, but a British Standard based on them is at present under consideration by the British Standards Institution.

Copies of these two specifications can be obtained from the Radio Industry Council, 59, Russell Square, London, W.C.1; RIC/1000/A costs 10s and RIC/1000/B 8s, including postage.

The "Quad" Aerial

Its Advantages for Indoor Use on Bands I and II

By F. B. SINGLETON (GW3CGM)

SOME ten years ago, when ten-metre amateur activity was at a peak occasioned by the solar cycle, the "quad" aerial was widely used. The reason for this account is that the writer feels it ought to be more widely known, particularly as it has advantages when used as an indoor aerial.

The "quad" is believed to have originated at Station HCJB, Ecuador, and, when it first appeared on the ten-metre scene, usually consisted of a two-turn square loop, with a quarter-wavelength side, and backed by a similarly constructed reflector, the planes of the two loops being parallel. The loops were mounted so that the sides were all at 45 degrees to the horizontal, and, for horizontal polarization, were open at the bottom corner for connection of a 300-ohm feed line to the driven loop and a phasing stub to the reflector. An investigation at the time¹ showed that folding the driven loop did not result in a very close match to the line impedance and pointed out that folding the reflector was no more necessary than with any other type of aerial. It also showed that when the diagonals of the loop were all at 45 degrees to the horizontal the gain was slightly higher, as expected on theoretical grounds.

With the fading of sun-spot activity the "quad" was lost to view for a time, but about two years ago it made a reappearance as a twenty-metre aerial and it was stated that the impedance of a single-turn loop with reflector spaced 0.2 wavelength was approximately 75 ohms and the gain claimed for the two-element combination was 10 dB, although 8 dB seemed a more reasonable figure².

Modern houses have roofs which are less steeply pitched than formerly, with insufficient height for a full-size Band I aerial and insufficient spread, except when parallel, or nearly so, to the ridge,

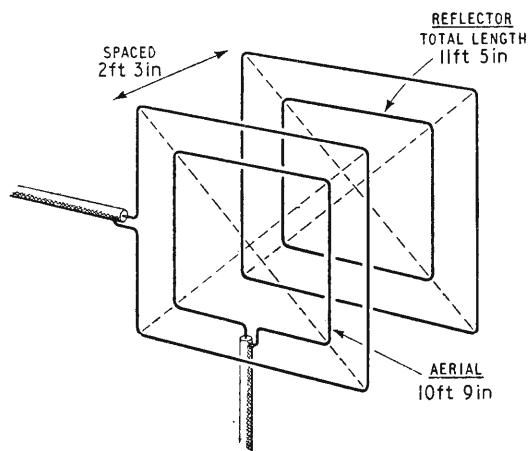


Fig. 2. Addition of an inner loop for Band II sound transmissions.

for a slot aerial. The "quad," which is both shorter than a dipole and narrower than a slot, would appear to be the answer to the inside aerial problem for the inhabitants of such houses, especially in view of the gain claimed for it. It is now two years since the writer brought one into use on Channel 4 (Sutton Coldfield), with satisfactory results. Fig. 1 gives a sketch of the one then in use. It will be seen that there is no phasing stub connected to the reflector, the necessary reactance being introduced by the more usual method of making the reflector about 5% longer than the driven element.

With the coming of Band II sound broadcasting the need for a more effective aerial than a piece of wire strung along a picture-rail was felt, and in the meantime further descriptions had appeared^{3, 4}, which showed that it was possible to combine "quads" for different bands. As a result, the system shown in Fig. 2 was set up and is working satisfactorily.

It will be seen that the Band I loop is opened in the centre of a vertical side (for vertical polarization), which side being a matter of convenience, and the Band II loop is opened in the centre of a horizontal side for the connection of the feeders. The spacing is a compromise for the two frequencies, since reducing it has the effect of lowering both gain and impedance. As originally described, the total length of one loop was based on the formula $468/f$ for a half-wavelength, where f is the frequency, but this formula is intended to allow for end-effects on a half-wave dipole. As the "quad" has no ends the writer thought it would be better to use $492/f$ for calculating the wire length,* and

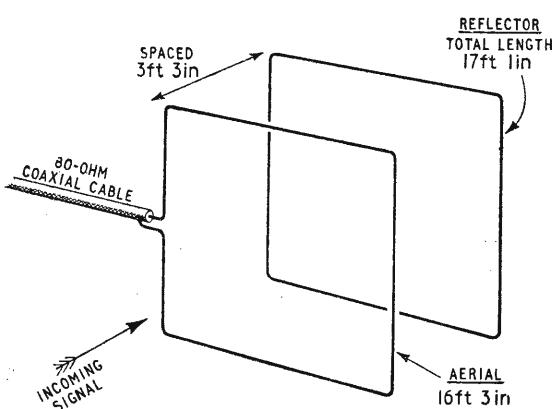


Fig. 1. Dimensions of "quad" aerial for Channel 4 (60 Mc/s).

* Note, actual length of wire = $2 \times 492/f$ —Ed.

although no measurements have been possible it does appear to give results which are certainly no worse than those obtained with shorter elements.

There would appear to be no great compromise involved in combining "quads" for Channels 3, 4, or 5, of either vertical or horizontal polarization, with a Band II system, but the combination with Channels 1 or 2, particularly the former, gives a gross mis-match on one or other band. The writer is not in a position to investigate this, but suggests that the spacing be set for the Band I signal and the results obtained on Band II be accepted. It appears that adequate signal on Band II is obtained in most locations where a usable Band I signal, from the same transmitting site, is present, and when the Band II aerial is a simple dipole. That being the case, it seems that a single Band II loop, with an impedance of the order of 110 ohms and a gain over the dipole of about 1 dB, should be more than adequate. In the event of the transmitters not being co-sited the problem is merely that of siting two systems in the roof rather than one.

The dimensions given are for a frequency of 60 Mc/s, for the Channel 4 "quad" and for 90 Mc/s

for the Band II system. For other frequencies the dimensions should be scaled accordingly.

Construction is quite simple using plastic-covered stranded wire carried on frames made of two garden canes forming the diagonals of the square. Pieces of string passed through holes in the canes outside the corner of the squares support the wire and make adjustment of the positions of the corners easy. Metallic supports of any description might well result in shorter loops being necessary because of the increased capacitance effects.

It only remains to say that the writer's "quad" is slightly more than 60 miles from the transmitting aerial at Sutton Coldfield.

REFERENCES

- ¹ "Technical Topics—The 'Quad' Antenna," *QST*, Nov., 1948
- ² S. B. Leslie, Jr., "A Cubical Quad for 20 Metres," *QST*, Jan., 1955.
- ³ Albert M. Magagna, "A Dual Quad for 15 and 10," *QST*, May, 1956.
- ⁴ John C. Pomeroy, "A Tri-Band Quad," *QST*, Sep., 1956.

Books Received

Dry-Battery Receivers with Miniature Valves by E. Rodenhuis. Volume in the Philips Technical Library series discusses data on and uses of various types of miniature valves and includes detailed description and circuits of six complete a.m. and two a.m./f.m. receivers. Pp. 242; Figs. 248. Price 32s 6d. Cleaver-Hume Press, Ltd., 31, Wright's Lane, London, W.8.

Department of Scientific and Industrial Research Report for the year 1955-56, includes a summary of work carried out by the various research establishments of the department, and co-operative industrial research organizations. Pp. 314; Price 9s 6d. H.M.S.O., London.

Transistor Circuits by Rufus P. Turner, covers d.c., a.f., r.f. and i.f. amplifiers, oscillators, use in power supplies, triggers and switches, control devices and also complete radio receivers and test instruments including Geiger counters. Pp. 160; Figs. 147. Price 2.75 dollars. Gernsback Library Inc., New York, 11. Available in this country from Modern Book Co., 19-23, Praed Street, London, W.2. Price 22s.

Simplified Electronics by Rufus P. Turner. General introductory book covers most aspects of the subject including semi-conductors and microwaves. Pp. 126, many illustrations and figures, price 75 cents. Trend Books, 5959, Hollywood Blvd., Los Angeles 28, California. Available in this country from Arthur F. Bird, 66, Chandos Place, London, W.C.2, Price 7s.

A Stable Decade Amplifier for the Frequency Range 10 c/s to 1 Mc/s by D. C. G. Smith, B.Sc., A.Inst.P. Describes design and performance of such an amplifier with a gain stabilized to 10 ± 0.1 . Pp. 10; Figs. 7.

Radio Interference from High Voltage Distribution Systems by S. F. Pearce describes measurements on existing 33 and 132 kV lines. Pp. 7; Figs. 11. The above two reports are available from the Electrical Research Association, Thorncroft Manor, Dorking Road, Leatherhead, Surrey; price 10s 6d each.

High Fidelity Loudspeaker Enclosures by B. B. Babani gives twenty designs (mainly American) including folded horns, reflex cabinets of small size or with

horn-loaded ports and the Karlson tapered slot enclosure, and also general construction and design hints. Pp. 46; Figs. 25; Price 5s. Bernards (Publishers), Ltd., The Grampians, Western Gate, London, W.6.

Definitions and Formulae for Students: Radio and Television Engineering by A. T. Starr. Fourth edition includes typical circuits. Pp. 65; Figs. 47. Price 2s. Sir Isaac Pitman and Sons, Ltd., Parker Street, London, W.C.2.

Brimar Radio Valve and Teletube Manual No. 7, includes information on new valve types previously supplied as separate data sheets. Pp. 336, Price 6s. Standard Telephones and Cables, Ltd., 63, Aldwych, London, W.C.2.

High Fidelity: A Practical Guide, by Charles Fowler. Basic acoustic theory leads to discussion of all types of units (including radio tuners) for high-quality sound reproduction, with emphasis on criteria for judgment and comparison. Pp. 310; Figs. 113. Price 37s or 4 dollars 95 cents. McGraw-Hill Book Co. Inc., 95, Farringdon Street, London, E.C.4, or 330, West 42nd Street, New York 36.

EDITORIAL ASSISTANT WANTED

Wireless World invites applications for a post as editorial assistant. The duties are as varied as the contents of the journal and call for wide technical interests, a well-developed critical faculty and a talent for lucid exposition. A good grounding in physics and some experience in radio and electronics are essential; evidence of writing ability would be an advantage.

Applications should be addressed to the Editor, Wireless World, Dorset House, Stamford Street, London, S.E.1.

News from the Industry

Elliott-Automation, Ltd., is the name of the holding company which now links the recently merged interests of Elliott Brothers (London), Ltd., and Associated Automation, Ltd. The Elliott-Automation group includes among others the following subsidiaries: Electroflo Meters, Hall Telephone Accessories, Micanite & Insulators, and British Industrial Plastics. In addition there are the various divisions of Elliott covering computing, guided missiles, microwave instruments, aviation instruments, Swartwout electronic control gear and nucleonics.

Computer consultancy service is now offered to industry by the analytical department of Short Brothers & Harland at 208a, Regent Street, London, W.1. The department is equipped with four Short general purpose analogue computers and a recently installed English Electric DEUCE digital computer.

I.T.A.'s North-Eastern transmitter, at Burnhope, five miles south-east of Consett, Durham, will be equipped by Marconi's with vision and sound transmitters, combining units, and programme input equipment. They will also supply the twin 8-stack horizontally-polarized directional aerials to be mounted on a 750-ft mast.

Ferranti's 75 years of progress is traced in a special issue of *The Ferranti Journal*. Most of the space is naturally devoted to the company's interests in power engineering but there are two articles dealing with its more recent entry into the fields of computers and semiconductor devices.

Ambassador-Baird.—Changes are announced by Camp Bird Industries for the marketing of both Ambassador and Baird receivers which are now manufactured at the Ambassador works, at Brighouse, Yorks. The distribution of Baird receivers and tape recorders (through a limited number of wholesalers) will be centred at Camp Bird House, Dover Street, London, W.1. Ambassador will continue to be distributed direct to dealers from Brighouse. Eric Gamble, sales director of Camp Bird Industries, has joined the board of Ambassador Radio and Television, Ltd.

Hartley Baird Group, which includes Ambassador, Duratube & Wire, Hartley Electromotives and P.C.D. (Printed Circuit Development), incurred a loss of £75,000 during the sixteen months ended last April. This is reported in the review of John Dalgleish, chairman of Camp Bird, Ltd., who have a 64% holding in the group.

Standard Telephones & Cables and their associates Bell Telephone Manufacturing Co., Antwerp, have been awarded the contract to supply the coaxial cable, three submerged repeaters and terminal equipment for the Anglo-Belgian submarine cable telephone scheme, planned for introduction in time for the opening of the Brussels International Exhibition next April. The scheme provides for 120 two-way telephone channels using a frequency band of 60 to 552 kc/s in one direction and 672 to 1164 kc/s in the other. The repeaters, 9ft long and 10in diameter, are similar to those supplied by S.T.C. for the Newfoundland-Nova Scotia section of the trans-Atlantic telephone cable.

S.T.C. and their Paris associates Le Matériel Téléphonique, have been awarded the contracts for the supply and installation of the s.h.f. transmission equipment and aerials for the recently announced cross-channel radio relay system for multi-circuit telephony and television. The terminal stations will be near Folkestone and Lille with intermediate repeaters in France. The service, which is scheduled for introduction early in 1959, will provide two channels each capable of carrying 600 telephone circuits and two channels each suitable for two-way 819-line television.

Marine Radar.—Since Decca entered the marine radar field in 1950 they have received orders for fitting over 7,000 vessels. The estimated number of radar-fitted ships throughout the world is between 15,000 and 16,000.

British Communications Corporation is supplying the 15-watt base station and ten 5-watt mobile transmitter-receivers for the ambulance service of the Halifax Borough Council. B.C.C. has recently cooperated with the manufacturers of the Vespa motor scooter, and H. Miller, Ltd., generator manufacturers, to equip scooters with radio for police use. The reference in last month's issue to the use of B.C.C. radio-telephone equipment for the Newport railway marshalling yard should have been in the past tense.

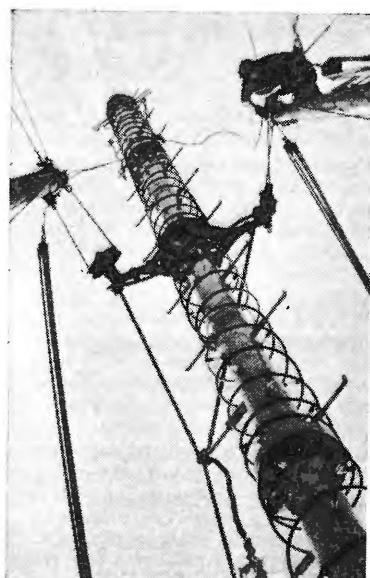
Aveley Electric, Ltd., of Aveley Industrial Estate, South Ockendon, Essex, have been appointed agents in the United Kingdom for the Narda Corporation, of New York, and the W. German companies Gossen, of Erlangen, and Electronic G.m.b.H., of Munich. Narda specializes in microwave components, Gossen in pointer instruments and Electronic G.m.b.H. in carbon film resistors.

Westinghouse Brake and Signal Company announce a new arrangement with Westinghouse Electric International of New York for the exchange of research information on semi-conductors. A new branch of the works at Chippenham has been built, with elaborate air conditioning, for the production of silicon and germanium power rectifier elements.

Rosite, Ltd., has been formed as a subsidiary of the Plessey Co. for the production of the cold moulded plastic Rosite (see Technical Notebook, p. 596) under an agreement recently made with the Rostone Corporation, of Lafayette, Indiana, U.S.A. The company is operating from Kembrey Street, Swindon.

Livingston Laboratories, of Retcar Street, London, N.19, have been appointed exclusive representatives in the U.K. and Eire by the tube division of Varian Associates, of Palo Alto, Cal. The agreement with the previous representatives, Rocke International, was terminated in June.

Winston Electronics, Ltd., Shepperton, Middlesex, have been appointed sole United Kingdom agents for a number of industrial electronic control instruments manufactured by Beckman Instruments, G.m.b.H., of Munich, Germany, and Beckman Instruments, Inc., of Fullerton, California, U.S.A.



B.I. Callender's riggers dismantling the helical Band V aerial at the E.M.I. works at Hayes, Middlesex, for re-erection on the Alexandra Palace mast for the u.h.f. television tests recently started by the B.B.C.

Marconi closed-circuit television is being used at a branch of the Royal Marsden Hospital, London, to assist in the deep therapy radiation treatment of patients. The equipment is used in conjunction with a radioactive caesium source and permits the treatment to be carried out by remote observation to safeguard doctors and radiographers against harmful long-term excess radiation.

Hivac, Ltd., are marketing an augmented range of directly-heated sub-miniature valves many of which are exact equivalents of American types. The range (with U.S. equivalent in parenthesis) includes XFY14, output pentode (5672); XFR1, r.f. amplifier pentode (1AD4); XFR3 r.f. oscillator triode (5676) and XR4 r.f. power amplifier (6397).

S.T.C. have installed sound reinforcement equipment in the conference hall of the Trades Union Congress Memorial Building, Great Russell Street, London, W.C.2. Speeches from the dais are radiated by two "slot diffuser" loudspeakers behind the panelling above the speaker, but for speeches from the "floor" loudspeakers at the rear of the hall are brought into circuit and the others muted.

P.A.M., Ltd., of Merrow Siding, Guildford, installed a Pye industrial camera in the Grocers' Hall, London, which was linked by G.P.O. cable to the Mansion House where they had set up three large-screen (4 ft by 3 ft) Nera forward-projection receivers to enable delegates to watch as well as hear speakers at the recent Coal Utilization Council's convention luncheon.

Decca windfinding radar, manufactured under licence by the Société d'Optique, de Mécanique, d'Électricité et de Radio, is to be supplied for 14 meteorological stations in France and its colonies.

Hudson Electronic Devices, Ltd., are supplying 100 walkie-talkie receivers to the G.P.O. They will be used during investigations to locate equipment causing radio interference.

Videotape Patents.—The Radio Corporation of America and Ampex Corporation have signed an agreement for the exchange of patent licences covering vision-on-tape recording and reproducing systems for both monochrome and colour.

Oryx Electrical Laboratories, Ltd., of 98 Dominion Road, Worthing, Sussex, manufacturers of Oryx soldering instruments, are setting up their own home sales organization and orders should now be addressed as above.

Morganite Resistors, Ltd., who just under 10 years ago moved to the Bede Trading Estate, Jarrow, have transferred to a new factory of some 25,000 square feet alongside the original one.

Solartron's first production model of their electronic reading automaton (ERA) has been bought by Boots the chemists. It will be installed at their head office in Nottingham to "read" the sales recorded on the cash register rolls from the firm's 1,300 branches.

Miles Electronics, Ltd., has been formed by F. G. Miles, Ltd., the aircraft manufacturers, of Shoreham, in association with the Lombard Development Corporation. The new company has grown from the Miles electronics division and is at present mainly concerned with the design and construction of flight simulators and analogue computers.

RCA Great Britain have supplied sound reproducing equipment, including pre-amplifier, power amplifier, and f.m. tuner, for No. 10 Downing Street. The equipment was originally installed for the Conference of Prime Ministers, but is now used for the play-back of recordings made at cabinet meetings.

Ross, Courtney & Co., Ltd., manufacturers of components, wire, terminals and accessories, who are this year celebrating their diamond jubilee, have opened an extension to their Ashbrook Road Works, Holloway, London, N.19. This is the second extension in four years. The company is a subsidiary of the Southern Areas Electrical Corporation group, of which P.A.M., Ltd., is also a member.

OVERSEAS TRADE

C.R. Tubes.—£10,000 worth of 21-inch rectangular c.r. tubes are being supplied by Siemens Edison Swan, Ltd., to the Campagna Commercial de Cinematografia, of Milan. They will be used in television chassis made by E. K. Cole, Ltd., which are being housed in cabinets of Italian manufacture.

Duplicated radar equipment for approach control and general surveillance at the Luxembourg airport is being supplied by Cossor Radar & Electronics, Ltd. The order also calls for triplicate display units, two of which will be remotely controlled.

Sound reproducing equipment for the simultaneous translation system in the new headquarters of the United Nations Educational, Scientific and Cultural Organization in Paris is being installed by Pamphonics Reproducers. The installation, which provides for a five-language translation system, includes amplifiers, control consoles, 500 microphones and 2,000 headphones.

Communications equipment, including three 3.5-kW h.f. transmitters (with their associated drive, keying and monitoring equipments), a 30-kW linear amplifier and receivers, has been ordered from Marconi's for the Khartoum Communications Centre in the Sudan.

A complete television station for operation in Band III has been purchased from Marconi's by Radio Valencia of Venezuela. It comprises a 2-kW vision transmitter, a 1-kW sound transmitter, aerial array, studio equipment, film scanner, vision and sound links and 3-camera o.b. unit. Marconi's have also recently supplied a 2-kW medium-frequency sound broadcasting transmitter for unattended operation in Venezuela.

British Physical Laboratories, who exhibited at the recent Canadian I.R.E. Convention, have appointed R.O.R. Associates, of Toronto, as their sole distributors in Canada. The United Mineral & Chemical Co., of New York, have been appointed distributors for the United States east coast and mid-west. Dr. V. A. Sheridan, managing director of B.P.L., has been touring North America and attended the Toronto Convention.

South Africa.—The Board of Trade is considering erecting a pavilion for the annual South African Rand Easter Show. A sixth of the available space would be occupied each year by a prestige display (among the subjects suggested is electronics) and the remaining 8,000 square feet would be available to manufacturers and industrial organizations. Those interested in the project, which would be introduced in 1959, should communicate without delay with the Export Publicity and Fairs Branch, Lacon House, Theobalds Road, London, W.C.1.

NEW ADDRESSES

Siemens Edison Swan have opened a cathode-ray tube service depot at Fourth Avenue, Team Valley Trading Estate, Gateshead, Durham (Tel.: Low Fell 75463). It will deal with c.r. tubes only; valves must be returned to the service depot at Brimsdown, Middlesex. The company has also opened offices, showroom, warehouse and maintenance workshop, at 76-80, Sherlock Street, Birmingham.

E.A.P. (Tape Recorders), Ltd., recently moved from 9 Field Place, London, E.C.1, to a new factory at Bridge Close, Old Church Road, Romford, Essex (Tel.: Romford 62366).

Direct TV Replacements have moved from 134 to 138, Lewisham Way, New Cross, London, S.E.14 (Tel.: Tideway 6666). They have installed an Ipsophone recorder for taking orders when the office is closed, for which the telephone number is Tideway 6668.

Alma Components, Ltd., have moved their works and offices from 165 Ossulston Street, London, N.W.1, to 551 Holloway Road, London, N.19 (Tel.: Archway 0014).

DECEMBER

LONDON

3rd. I.E.E.—“Some aspects of half-wave magnetic amplifiers” by G. M. Ettinger; “Some transistor input stages for high-gain d.c. amplifiers” and “A transistor high-gain chopper-type d.c. amplifier” by Dr. G. B. B. Chaplin and A. R. Owens; and “Dekatrons and electro-mechanical registers operated by transistors” by Dr. G. B. B. Chaplin and R. Williamson at 5.30 at Savoy Place, W.C.2.

10th. Institute of Physics.—“Infra-red and microwave modulators using free carriers in germanium” by Dr. A. F. Gibson (R.R.E.) at 5.30 at 47 Belgrave Square, S.W.1.

11th. Physical Society.—Reports on “The Paris meeting on colour television, 1957” by L. C. Jesty; “The meeting of the C.I.E. Working Party on calorimetry, Teddington, 1957” by Professor W. D. Wright; and “The symposium on visual problems of colour, Teddington, 1957” by Dr. W. S. Stiles at 3.30 at Imperial College, S.W.7.

11th. I.E.E.—“A flying-spot film scanner for colour television” by H. E. Holman, G. C. Newton and S. F. Quinn at 5.30 at Savoy Place, W.C.2.

11th. Institute of Physics.—“Irregularities and movements in the ionosphere” by Dr. B. H. Briggs (Cavendish Laboratory) at 6.0 at 47 Belgrave Square, S.W.1.

13th. Television Society.—“Dressing television: cabinet design” by L. J. Griffen (Kolster Brandes) at 7.0 at 164 Shaftesbury Avenue, W.C.2.

16th. I.E.E.—“Electronics and automation—electronics in the textile industry” by K. J. Butler at 5.30 at Savoy Place, W.C.2.

16th. British Computer Society.—“Parallel programming: a study of a new technique in digital computer programming” by Dr. S. Gill (Ferranti) at 6.15 at Northampton College of Advanced Technology, St. John Street, E.C.1.

17th. I.E.E.—“Recent uses of ultrasonics in investigating the characteristics of materials” by Dr. J. Lamb at 5.30 at Savoy Place, W.C.2.

18th. Brit.I.R.E.—“Recent developments in electronic instrument design” by E. Garthwaite and A. G. Wray at 6.30 at the London School of Hygiene, Keppel Street, W.C.1.

20th. B.S.R.A.—“Lightweight pickup design” by Stanley Kelly at 7.15 at the Royal Society of Arts, John Adam Street, Adelphi, W.C.2.

BIRMINGHAM

2nd. I.E.E.—“Electronic control of machine tools” by D. T. N. Williamson at 6.0 at the James Watt Memorial Institute, Great Charles Street.

13th. Society of Instrument Technology.—“Electronic instrumentation trends and implications” by R. J. Redding (Evershed & Vignoles) at 7.0 at Regent House, St. Phillips Place, Colmore Row.

CAMBRIDGE

3rd. I.E.E.—“The Mullard radio astronomy observatory” by M. Ryle at 8.0 at the Cavendish Laboratory.

CARDIFF

4th. Brit.I.R.E.—“Demonstrations on aerial circuits” by H. V. Sims at 6.30 at the Cardiff College of Technology and Commerce, Cathays Park.

6th. Institute of Physics.—“Microwave triodes” by Professor M. R. Gavin (University College of North Wales) at

MEETINGS

5.15 in the Physics Department, University College of South Wales.

CHATHAM

12th. Institution of Production Engineers.—“The practical uses of electronics in industry” by K. A. Zandstra, at 7.30 in the Assembly Room, Sun Hotel.

CHELMSFORD

10th. I.E.E. (Graduate and Student Section).—“Television film recording” by E. J. Stocks at 7.0 at the Public Library.

EDINBURGH

3rd. I.E.E.—“Infra-red radiation” Kelvin lecture by Dr. G. B. B. M. Sutherland at 7.0 at the Carlton Hotel, North Bridge.

13th. Brit.I.R.E.—“High-quality sound reproduction” by R. E. Cooke at 7.0 in the Department of Natural Philosophy, University of Edinburgh.

GLASGOW

12th. Brit.I.R.E.—“High-quality sound reproduction” by R. E. Cooke at 7.0 at the Institution of Engineers and Shipbuilders, 39 Elmbank Crescent.

LEEDS

3rd. I.E.E.—“The use of transistors in radio and television” by Dr. A. J. Biggs and E. Wolfendale at 6.30 at 1 Whitehall Road.

MANCHESTER

11th. I.E.E.—“Ferrites” by Dr. D. H. Pringle at 6.45 at the Engineers’ Club, 17 Albert Square.

12th. Brit.I.R.E.—“Process heating” by M. O’C. Horgan at 6.30 at the Reynolds Hall, College of Technology, Sackville Street.

NEWCASTLE

2nd. I.E.E.—“Recent uses of ultrasonics in investigating the characteristics of materials” by Dr. J. Lamb at 6.15 at King’s College.

11th. Brit.I.R.E.—“Stereophonic sound and tape recorders” by D. H. McBean at 6.0 at the Institution of Mining and Mechanical Engineers, Neville Hall, Westgate Road.

PLYMOUTH

5th. I.E.E.—“The B.B.C. sound broadcasting service on very-high frequencies” by E. W. Hayes and H. Page at 3.0 at the Electricity Showrooms, New George Street.

LATE-NOVEMBER MEETINGS

27th. Institute of Physics.—Symposium on “The design of physics research laboratories”; speakers will include B. S. Fleming-Williams (Sylvania-Thorn Colour Television Laboratories) and J. G. Cornwell (G.E.C. Research Laboratory), at 2.30 in the Lecture Theatre, Royal Institution, 21 Albemarle Street, London, W.1.

28th. Institution of Electronics.—“The high fidelity reproduction of sound” by C. Brown (Philips) at 6.30 in the Assembly Hall, University of London Institute of Education, Malet Street, London, W.C.1.

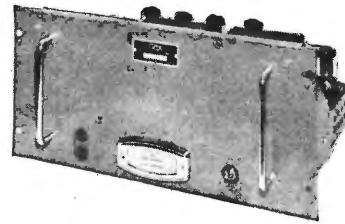
29th. Brit.I.R.E.—“Automatic programming” by Dr. P. M. Woodward at 7.0 at the North Gloucestershire Technical College, Cheltenham.

new



60 watt AMPLIFIER

The power amplifier T664, illustrated below, has been developed to meet the need for a unit of relatively high output to be used in larger Sound installations. The T664 is primarily designed for mounting in our Rack-Equipment assemblies and to this end has duplicated plug-and-socket facilities on all points for inter-connecting a multiplicity of amplifiers. It can also be made available as a self-contained unit, if required, with ventilated cover. The necessary mixers and pre-amplifiers can be chosen from our range according to requirements.



Brief specification :—

Input: Sensitivity .85v.; Resistance 470KΩ

Output stage: Four EL34 valves in parallel push-pull.

Output impedance: 165Ω, 100 v. line.

Distortion: Less than 1% at 60 watts output.

Feedback: 16 db.

Frequency response: 50-20,000 c/s ± 1 db.

Hum and Noise: Better than —65 db.

HT/LT supply: 2 amps, 6.3 v.; 30 mA., 300 v.

Please write for full details of our complete range of Sound Reproducing Equipment.

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P934

RANDOM RADIATIONS

By "DIALLIST"

The Live Chassis

IN a recent issue of the New York *Radio Electronics* the editor, Fred Shunaman, had a strongly worded article calling attention to the dangers of the live chassis in domestic mains receiving equipment. I'm completely with him, for I've always regarded the transformerless set run from a.c. mains as an electrical horror. If Mr. Shunaman calls them lethal when the standard a.c. mains supply in his country is 110-117 volts, how much more so are they here with mains voltages ranging from 200 to 250 volts? Probably well over half of the millions of sound and television sets in use here to-day get their a.c. mains supplies via 2-pin plugs and sockets, or even lamp socket adaptors. It's therefore a fifty-fifty chance that the chassis is connected to the live wire. Heaps of folk make a practice of switching off their sets at the mains. If—and in older houses it's rather a big if—the switch breaks the live lead, the chassis then automatically becomes dead. But if it's the neutral that is broken, the chassis and one wire of the often considerable length of flex between it and the socket are live. Those who will fiddle about inside their sets without knowing the faintest thing about them run no small risk and there's always the possibility that a fault may develop when the set is out of use and cause a fire. Things are safe enough if only people will follow the makers' instructions and switch off at the set, for that switch breaks both leads.

What Do You Think?

The double-wound mains transformer has two such big advantages that one wonders why more manufacturers don't use it, in their more expensive models at any rate. Its core is connected to the chassis and if this is well and truly earthed there's no chance of the chassis becoming live. Again, a mains transformer makes it possible to do away with those horrible chains of valve heaters. If one heater in a series chain burns out, all cease to light up and the serviceman's task of locating the culprit isn't exactly made easy. When a valve's cathode is returned to chassis the p.d. between it and the heater may

be undesirably large. I wonder if any manufacturer has toyed with (or even tried out) the idea of building in a constant-voltage transformer? In many parts of the country there are considerable drops in the mains voltage at times. They can be large enough to effect the working of television sets seriously either by giving rise to picture shrinkage or by upsetting the sync.

Band V Possibilities

BY the time you read this experimental television transmissions in Band V should be under way. The idea behind this joint effort initiated by the Television Advisory Committee and carried out by the B.B.C. is first to discover whether such ultrahigh frequencies can be used for TV broadcasting in this country. Both 405-line and 625-line definitions are to be used so that the results can be compared. To me it seems that with Band V we've a heaven-sent opportunity of developing a really high-definition system. Naturally that can't be done in Bands I or III; but in Band V such a service could be developed with the same relation to the present B.B.C. and I.T.A. services as in sound broadcasting the v.h.f./f.m. transmissions bear to those on the medium-wave and long-wave bands. There's no need for a man to exchange his a.m. receiver

for an f.m. set unless he chooses to; but if he wants the improved service, it's there waiting for him. In the same way, the potentially higher definition would be there for anyone who cared to go in for a Band V television receiver. Though (and probably because) we led the world by getting the first TV service going, to my mind it's a sad fact that our 405-line standard is the lowest to be found anywhere. In Band V we could develop something even better than the admirable 819-line French system. Let's hope we have a shot at it!

The Shape of Things That Came

AWAY back in 1936, in the December 11th issue of the then weekly *Wireless World*, I was rash enough to forecast what the future was likely to have in store for sound and television in a dozen years from then. The paragraph in "Random Radiations" ended: "If you want a fine chance of hurling the epistolary brick at me, file this number of *W.W.* and write to tell me how wrong my predictions proved to be!" One reader did the filing and he has now been kind enough to send me the cutting—without the brick. My dates were thrown out by the war, which closed down television and prevented progress from being made in domestic sound receivers. Otherwise I seem to



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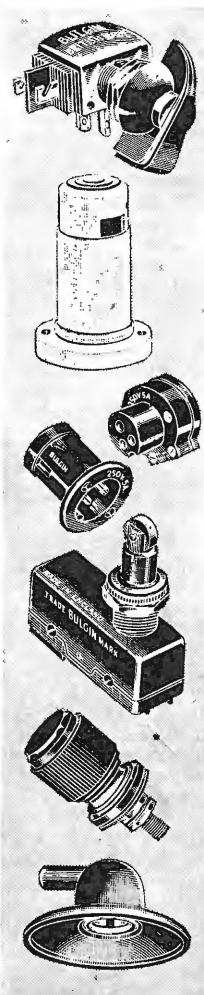
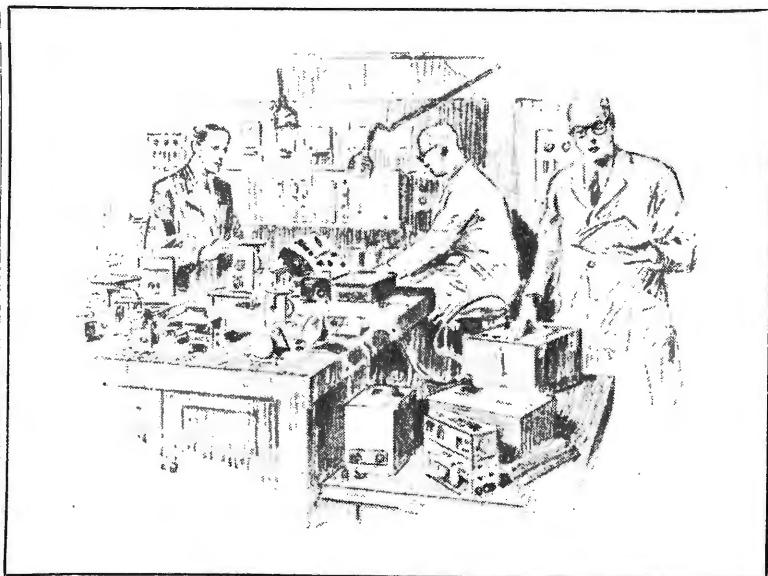
have been a fairly reliable prophet. I wrote that I expected that the bulk of local listening would be on v.h.f. and that the quality would really approach perfection owing to the much wider range of modulation frequencies that it would be possible to use. Some sets would be for v.h.f. only. I was over-optimistic in believing that the standard domestic set would by then be a combined television and v.h.f. set, though things now seem to be tending that way. My only big bloomer was the statement that I didn't believe that the television set of the near future would contain a cathode-ray tube. Even now I'm still not convinced that line-by-line scanning on the screen of a modified form of oscilloscope (which is what the TV set is) is the final answer to television transmission and reception. It's admittedly a pretty good answer, but I firmly believe that a better one will be found, though I'm not going to risk this time forecasting a date.

A New Pastime?

DX WORK on v.h.f. sound broadcasting stations seems likely to become almost as popular a hobby as it once was in other broadcasting bands. Readers living in many different places write to tell me of some quite remarkable experiences. One of them lives at Aylesbury, Bucks, which doesn't lie very high and there's a good deal of hilly ground in some directions. My correspondent uses a dipole-cum-reflector indoor aerial directed on Wrotham. His record shows occasional good reception from Wenveoe, particularly in the morning and evening. Others recorded are Norwich, Holme Moss and Sutton Coldfield among the B.B.C. stations. Between June 14th and 22nd he logged German, Dutch and Italian stations. Conditions became unfavourable from then until early September, since when he has been receiving three French stations.

Hearing Electrically

A NUMBER of readers concerned professionally with hearing and auditory perception have asked for further information on the experiments on direct electrical stimulation of hearing, to which I referred in the September issue. The work was undertaken by two French doctors, Charles Eyrès and André Djourno, who recently communicated their findings to the Academy of Medicine, Paris. Their work was brought to my notice by a note in the *Sunday Times* of July 14th.



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"Ears Have They, and Hear Not"

AT one time it used to be the custom among the semi-literate to clinch an argument by saying "I've seen it in print." The "print" in question was usually to be found in one of the more sensational newspapers. If it appeared in a newspaper it *must* be true; so the upholders of this argument-clinching cliché used to think. A newspaper to them meant as much as the "Guid Book" to a kirk-going Caledonian.

Those times have passed however, for the authoritarian position of the newspapers has long ago been undermined by the B.B.C. Nowadays the criterion of truth is "the wireless," and the educational status of those who believe what they hear on "the wireless" is considerably higher than semi-literate. The word of the B.B.C. is so powerful in its effect on certain minds that it is almost frightening.

A month or two ago as Mrs. Free Grid and I sat in front of our modern infra-red fire, she suddenly gave a snort of disgust as she looked up from the October issue of *W.W.* which had just come to hand. This was the issue in which "Cathode Ray" discussed certain scientific theories, past and present, including the old and popular one of an all-pervading ether through which wireless waves were supposed to travel. "Surely," said Mrs. Free Grid, "even he must be aware that wireless waves are airborne and always have been, as the B.B.C., who surely must know, wouldn't constantly use the expression 'on the air'?"

Naturally I made a spirited defence of "Cathode Ray" but only succeeded in losing scientific caste myself, and now he has let me down badly by making a statement in which even I cannot support him. He states in the November issue that sound "is a physical disturbance that would exist even if there were no living creatures to hear it." In my view it is only necessary to sub-

stitute the word pain for sound and feel for hear in order to show that "Cathode Ray's" statement won't hold water.

I'm not trying to dabble in philosophy with its theory of pan-subjectivism when I say that pain and sound would cease to exist if there were no living creatures to feel and hear them. In the absence of *living* creatures the physical disturbances which cause the mental phenomena of pain and sound would, of course, still exist.

'Phoning While You Speed

THE modern generation finds it hard to believe that there was ever a time when there was no such thing as sound broadcasting and television. In the same way, I think, the generation of a decade or so hence will find it hard to believe that our cars were not connected by radio to the national telephone system.

It would be, technically speaking, quite possible for our cars to be "on the phone" today if only the G.P.O. would do something about it. As it is, I pay 5s, register myself as a business with my H.Q. at home, and I can then apply for a mobile radio licence to cover radio-telephony between my home and car, but my ambition is to be able to call any telephone subscriber from my car.

This could be so easily arranged if the P.M.G. would erect a suitable transmitting and receiving station on the roof of every telephone exchange. Then by calling this exchange-roof station I could be plugged into the line of any subscriber just as though I were ringing from home. Not only could I call any subscriber but I could communicate with any other car, provided that it happened to be within wireless range of a telephone exchange.

I think that a start could be made by the A.A. and R.A.C. who could rig up a radio link on the roofs of their phone boxes for night use so that stranded motorists would be saved the necessity of trudging a mile

to the nearest box as I had to do recently after midnight in order to put in a call for help. Unlike my proposed G.P.O. exchange arrangement, this roadside radio link between stranded car and breakdown service would have to be unmanned and so completely automatic; but what of that?

The only snag in my whole idea of cars-on-the-phone is that women drivers would certainly try to drive and carry on an interminable telephone

conversation simultaneously. This would mean that during the telephone talk the car would be virtually unmanned—or should I say un-womaned—and this would constitute another road hazard.

For some years the G.P.O. has provided a radio-telephone link so that small craft in the Thames estuary could be connected to the national telephone system. Why can they not extend the idea for cars in the manner I have suggested?

The Old W.W. Tie

WHEN visiting the National Radio Show and other quasi-radio gatherings like the Audio Fair I often feel that those of us who have some general interest in and knowledge of the scientific side of radio ought to have some distinguishing emblem whereby we could recognise our fellow savants and be picked out by the stand attendants from the milling crowd who are only interested in the programmes.

I can think of nothing better than to follow the example of our public schools and other famous institutions by sporting a specially designed "Old Wireless World Tie," for it need hardly be said that anybody having any wireless engineering qualifications at all is a regular reader of this journal. Indeed, I recollect a former Editor of *W.W.* saying in pre-war days that to be a regular reader of *W.W.* was a qualification in itself. I would suggest that anybody who could produce proof that he was a reader of ten years standing should be entitled to wear the tie which would, of course, be sold only to those who could produce a certificate signed by the Editor.

Those of us of more than ten years standing would be entitled to wear on it a bar for every extra period of five years. Those who could produce proof that they had been readers since the first number (April 1911) without missing an issue would be entitled to receive a complementary copy each month for the rest of their lives; maybe they would deserve it.

First it is necessary to settle the question of a suitable design and here is where I need the assistance of some of you with heraldic experience, as things like "bends sinister" and "gules argent" are just Greek to me. As you will gather I want something completely out of the ordinary in neckties; something like a coat of arms complete with Latin motto such as Audio, Video, Olfaciam, for I am convinced that the radio transmission of smell will one day be achieved.

If enough of you write to the Editor about the suggestion something is bound to happen, as Editors are as much susceptible to public opinion as politicians are at election time.*

* Observation noted : no comment—ED.



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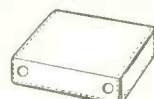
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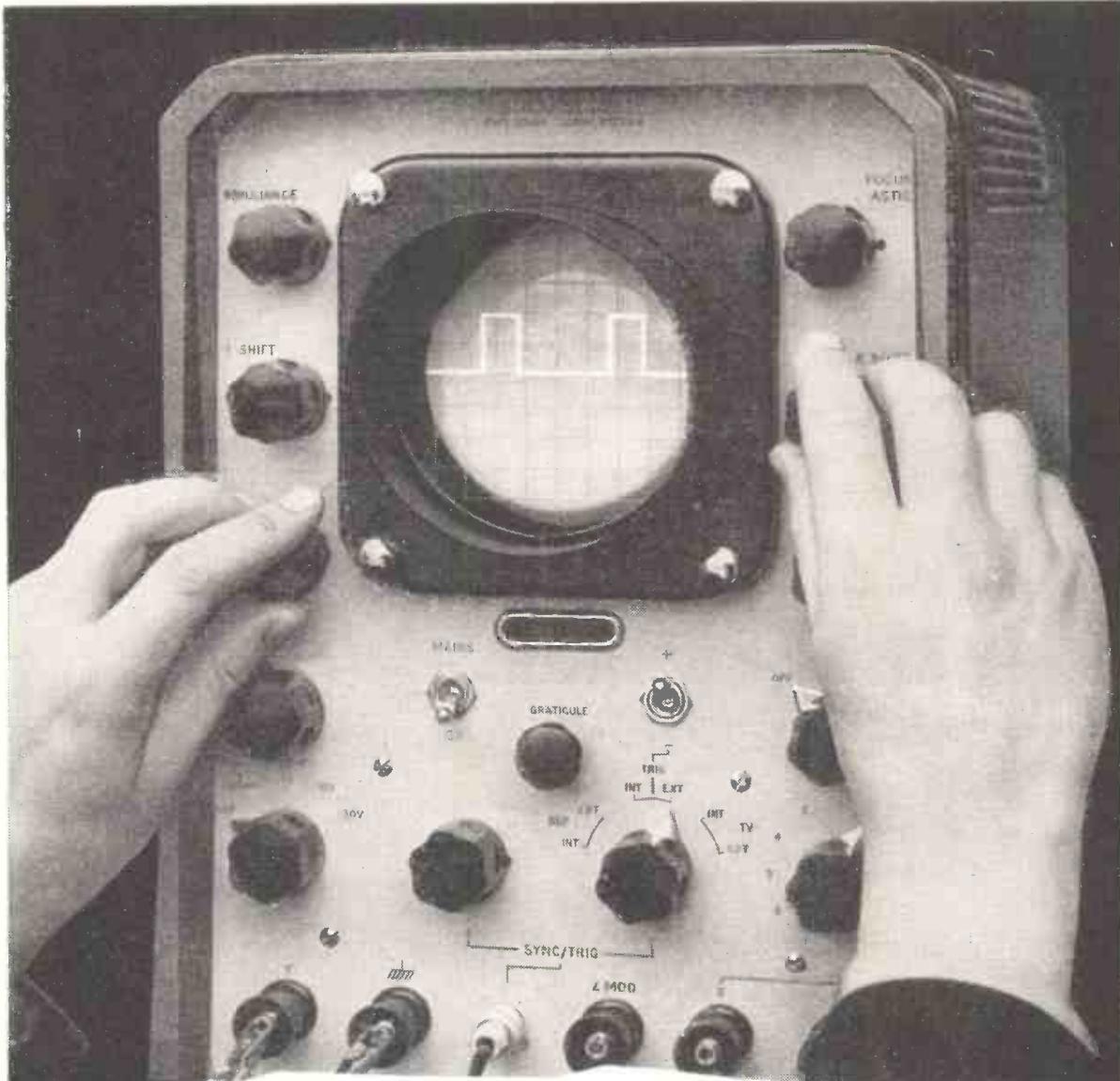
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" " (at 100mA) (V)	0.5	0.44
Reverse leakage current (at -20V) (uA)	1.5	10
Hole storage recovery time* (μ sec.)	0.35	0.35
Capacitance (at -10V) (pF)	4.0	4.0

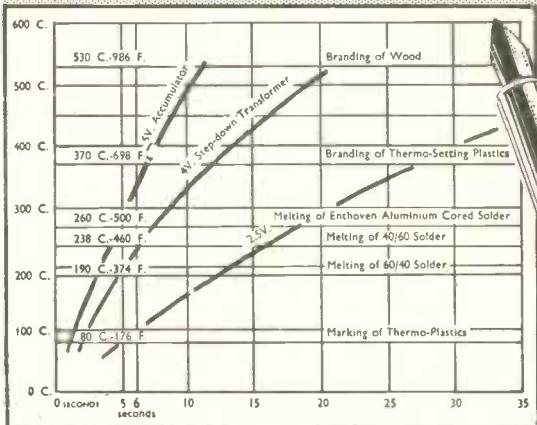
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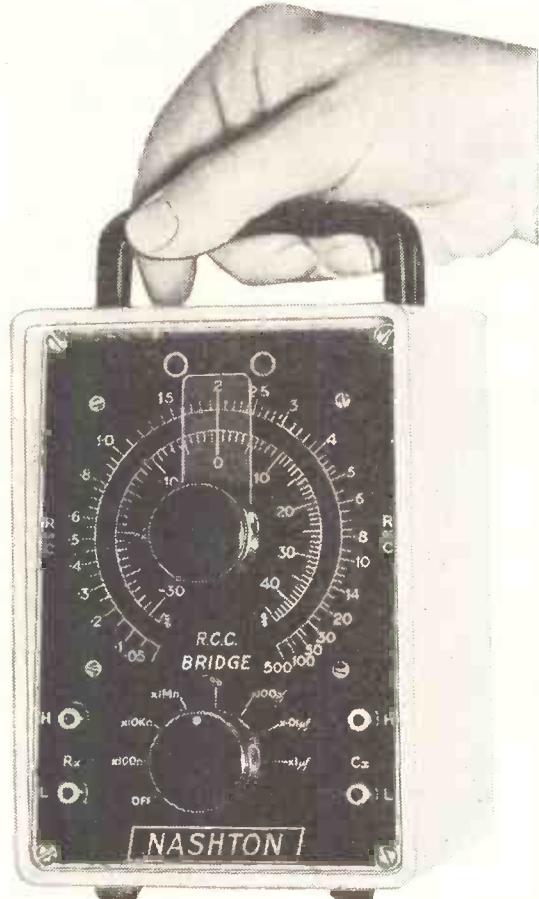
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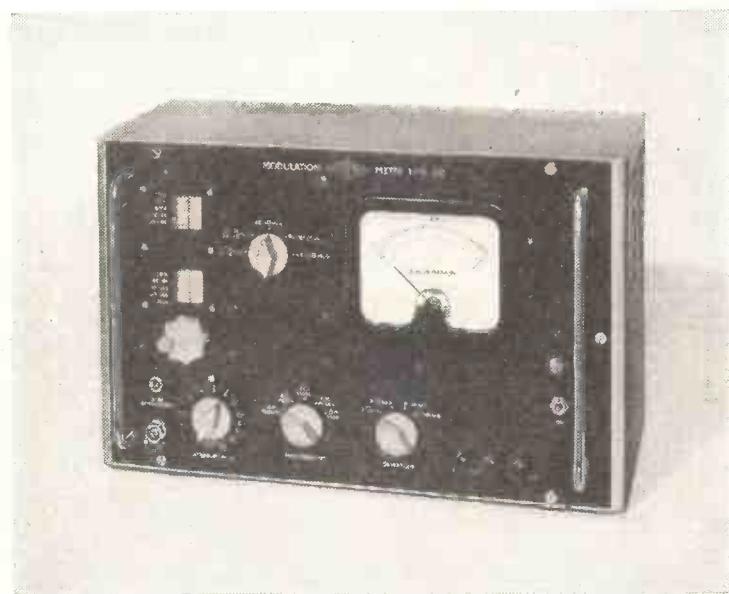
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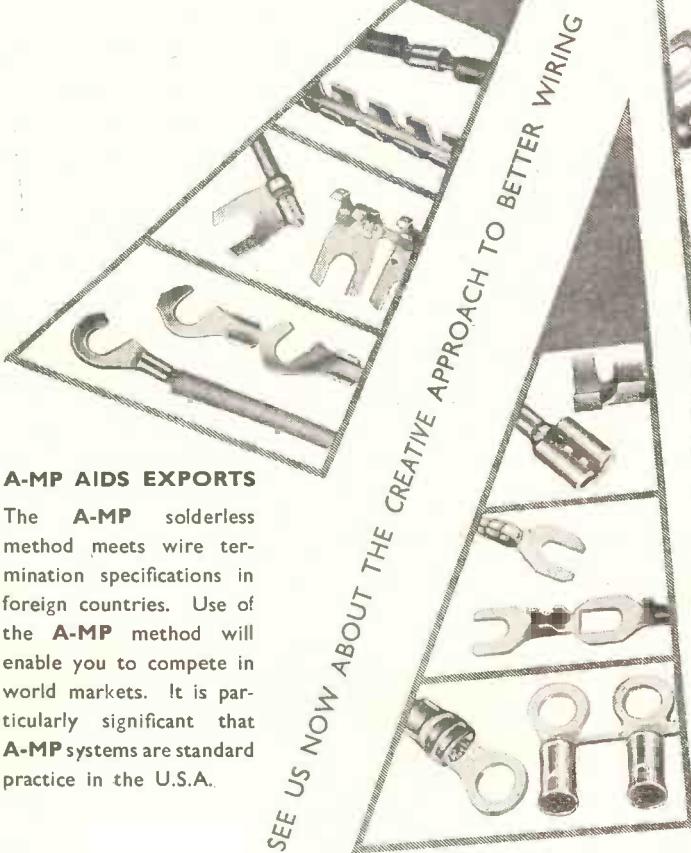


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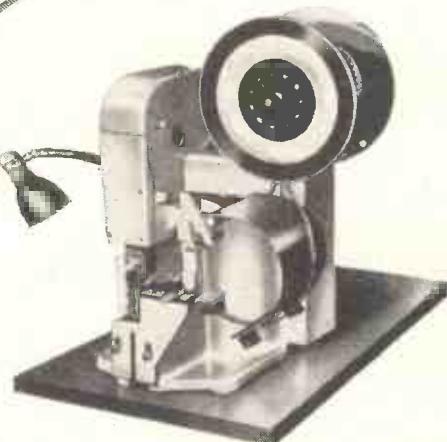
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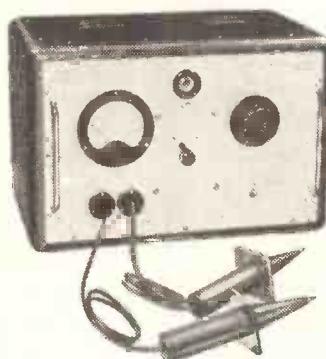
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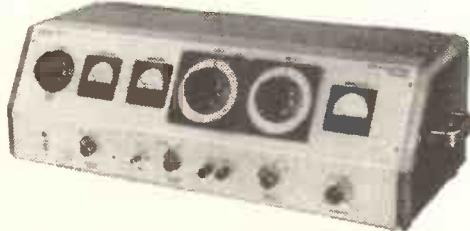
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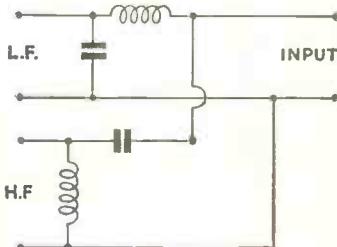
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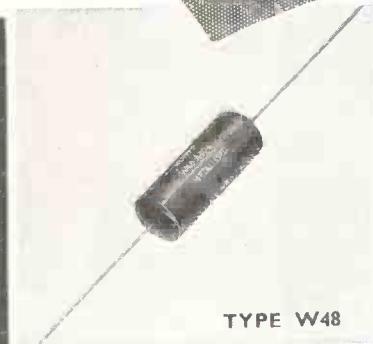
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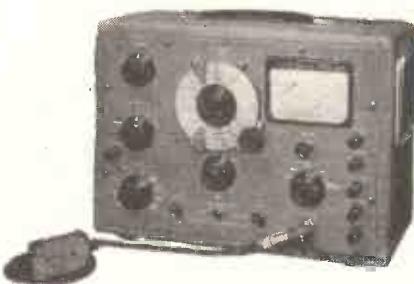
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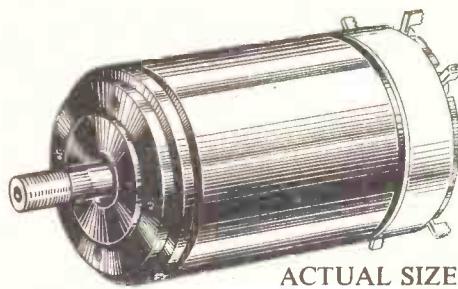
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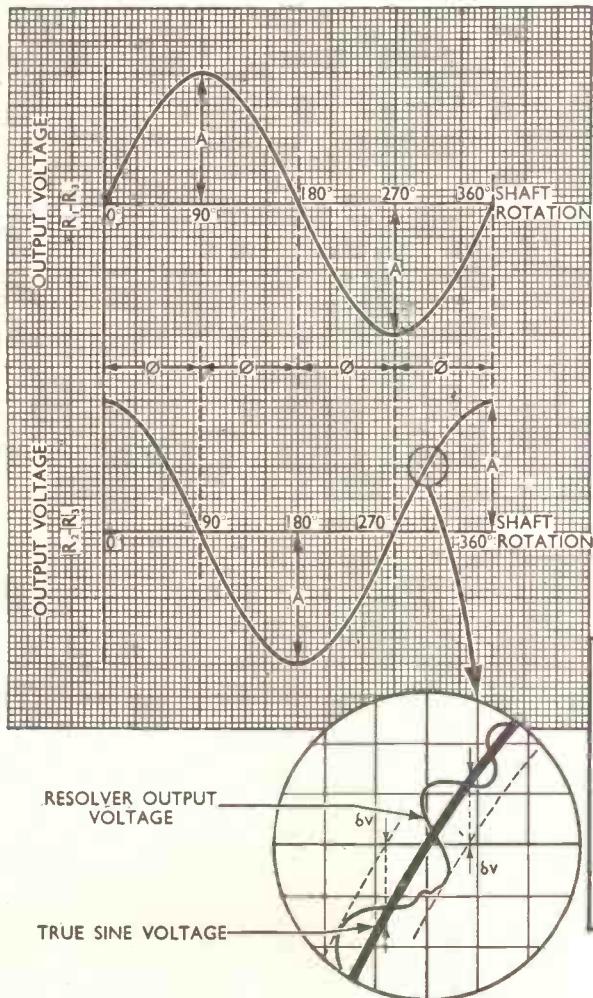
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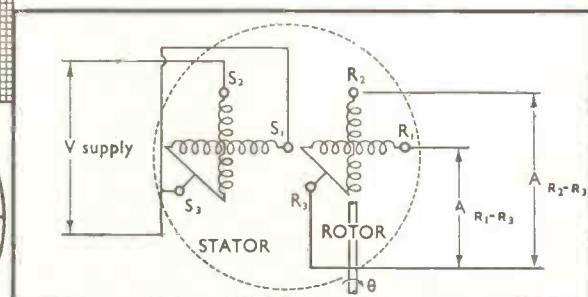
ACTUAL SIZE



A Synchro Resolver consists of a rotor carrying two windings at right angles which rotates in a stator also having two mutually perpendicular windings. If the synchro is connected as shown below, the voltages A_{R1-R3} and A_{R2-R3} vary sinusoidally as shown in the accompanying graphs. How closely the voltages of a Sperry size 11 Resolver follow this sine relationship can be judged from these performance figures:

- (a) Angular separation of Nulls = $\theta = 90^\circ \pm 4'$
- (b) Transformation Ratio $A = KV$
where $K = 1 \pm 1\%$ from model to model
Variations in $K = \pm 0.2\%$ in any one model
- (c) Voltage departure from true sine
Model A = $6V = \pm 0.2\% A$
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Accuracy better than $\pm 0.005\%$.

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10 c/s, 100 c/s, 1 kc/s, and 10 kc/s.

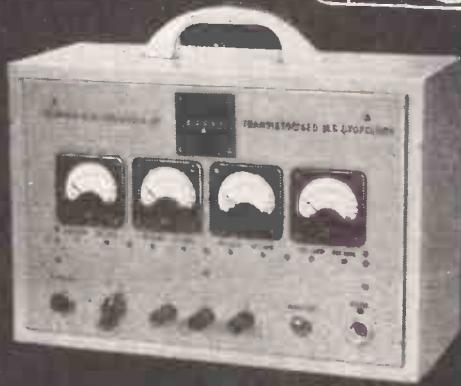
Portable - weighs only $27\frac{1}{2}$ lbs. and measures
 $14\frac{1}{2}'' \times 7\frac{3}{4}'' \times 11\frac{1}{2}''$.

Low power consumption - only 2W at 12V.

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Both types of equipment are constructed from Venner
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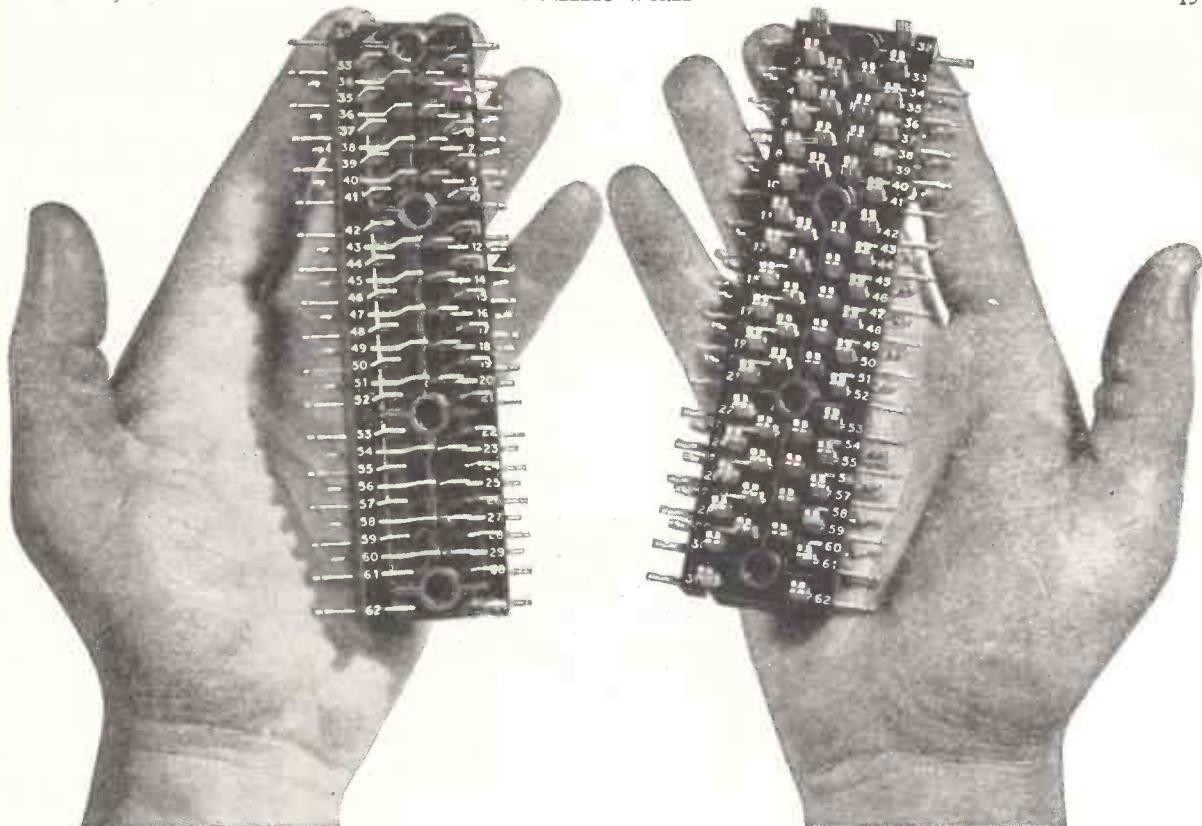
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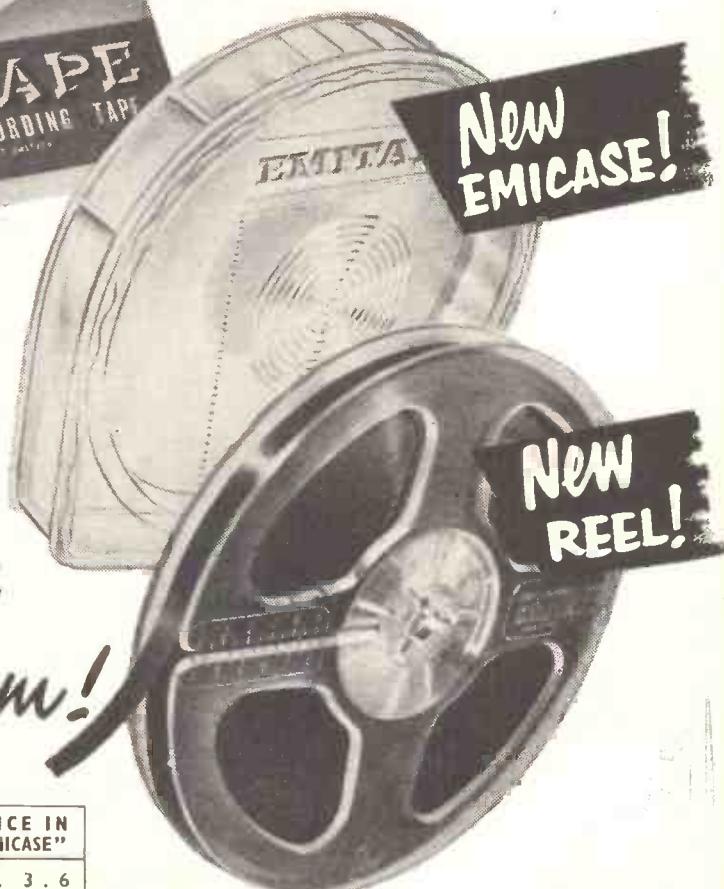
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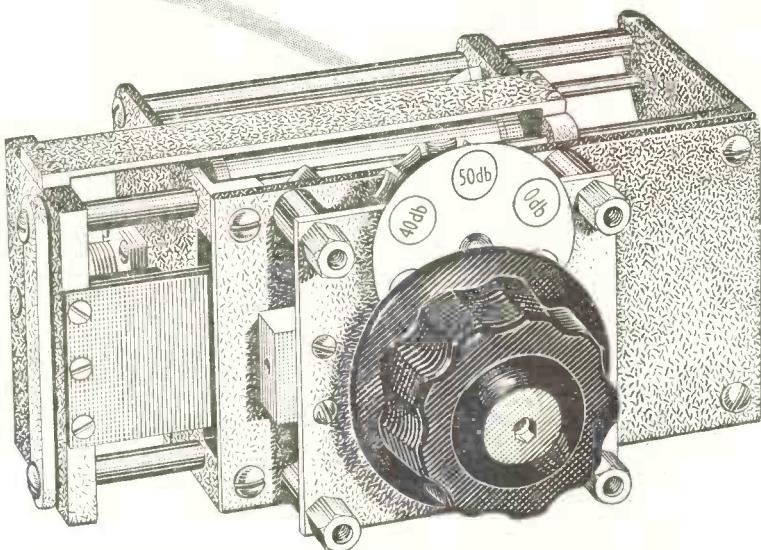
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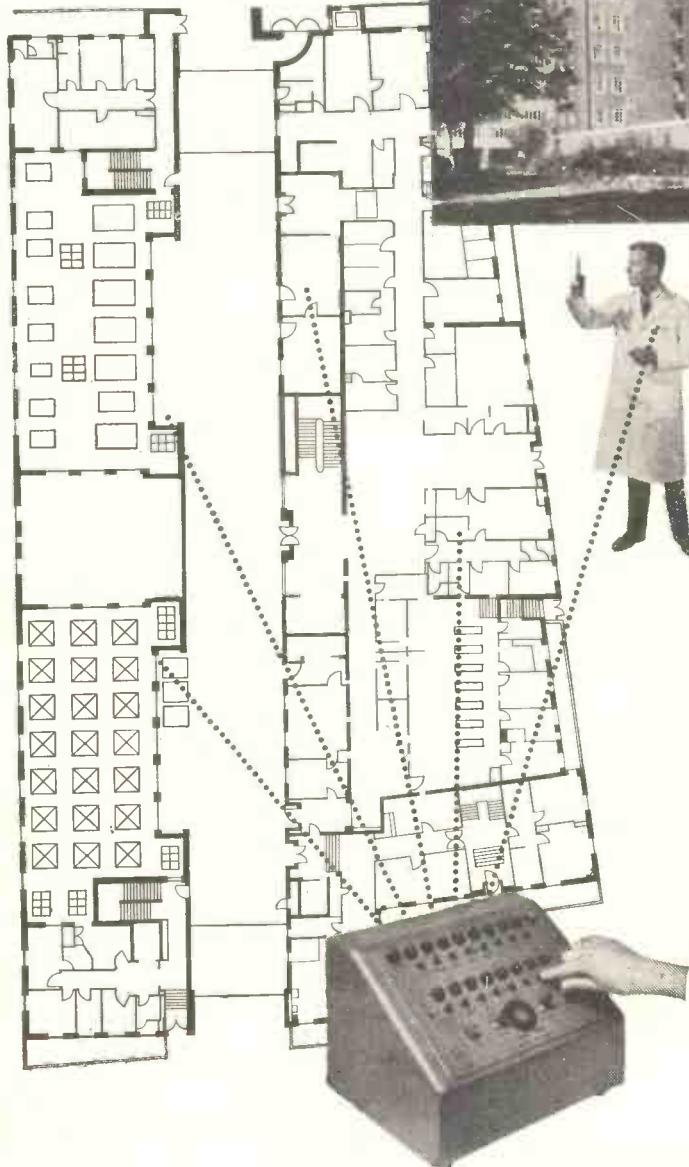
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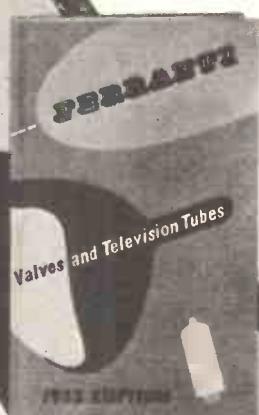
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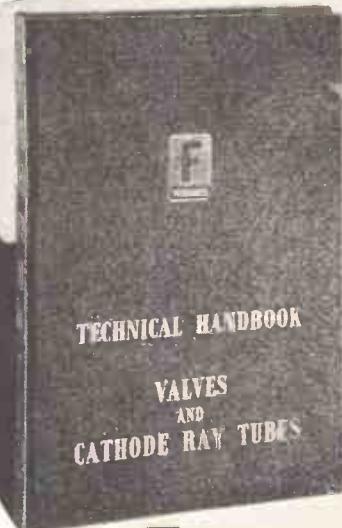


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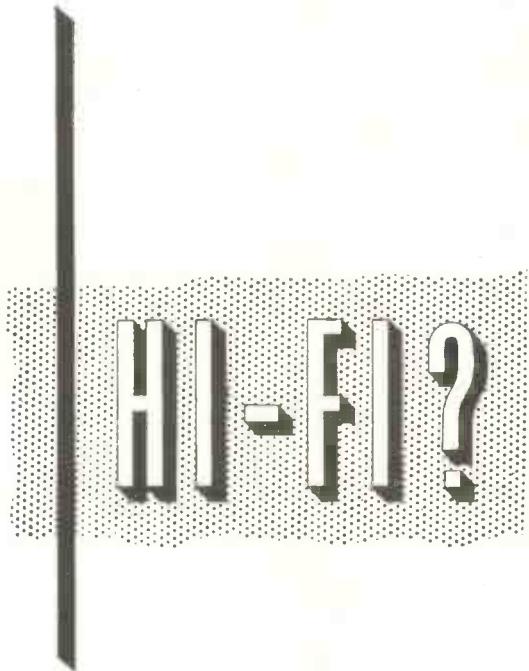
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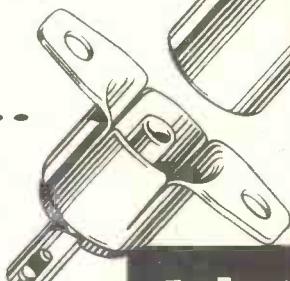
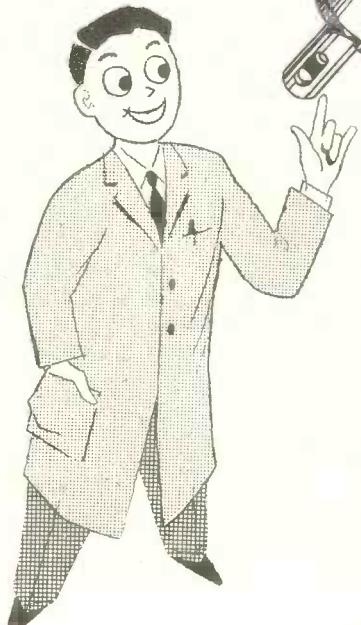
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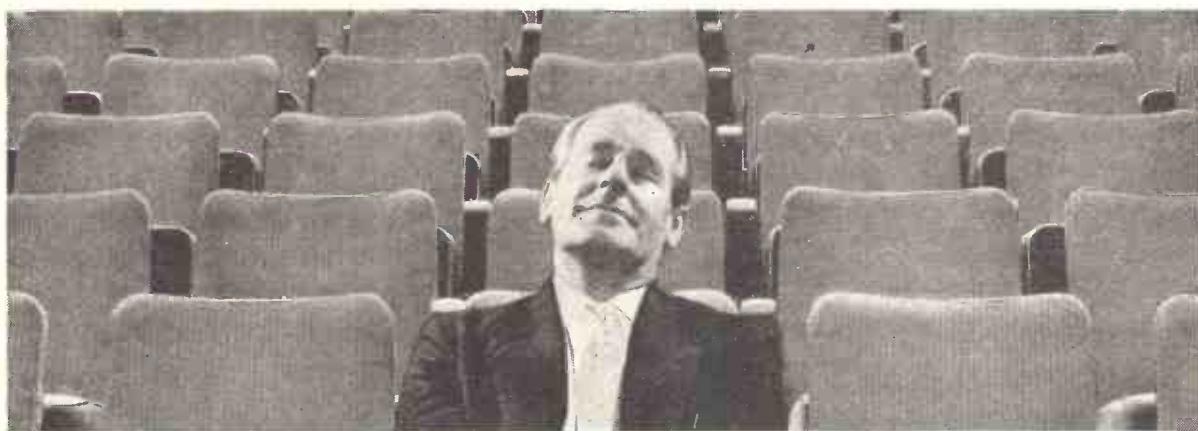
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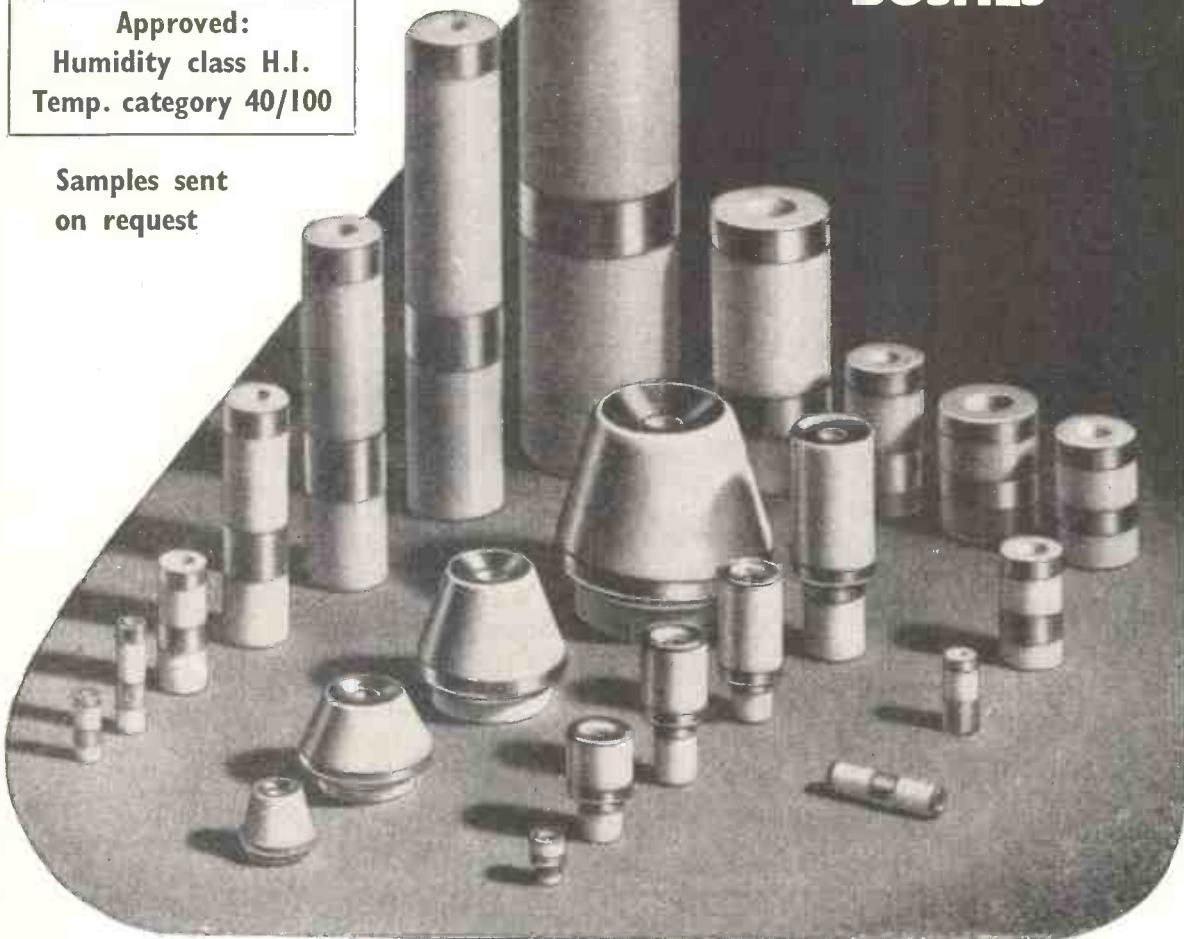
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- Capable of external modulation, both pulse and fm.
- Equipped with integral electronically-regulated power supplies.
- Frequency calibration accomplished by a $\pm 0.1\%$ direct-reading wavemeter.

SIGNAL GENERATORS Basic Unit Model HU-2

Plug-in Tuning Unit Model No.	Power Output Calibrated	FREQUENCY RANGE
G1822		18,000—22,000 mc/s
G2225		22,000—25,000 mc/s
G2427		24,700—27,500 mc/s
G2730	—10 to —90 dbm	27,270—30,000 mc/s
G3033		29,700—33,520 mc/s
G3336		33,520—36,250 mc/s
G3540		35,100—39,700 mc/s
		37,100—42,600 mc/s
		41,700—50,000 mc/s

Model SG-1218, Signal Generator and Model SS-1218 Signal Source are available to cover the frequency range 12,400 to 17,500 mc.

SIGNAL SOURCES Basic Unit Model HU-1

Plug-In Tuning Unit Model No.	Power Output Average
S1822	10 mw
S2225	10 mw
S2427	10 mw
S2730	10 mw
S3033	10 mw
S3336	9 mw
S3540	5 mw
S3742	Approx. 3 mw
S4150	Approx. 3 mw

MODULATION :

Internal modulating:

Frequency 1000 cps square wave.
Requirements for external pulse modulation:

Pulse repetition frequency ... 100 to 10,000 pps.
Pulse width rate 0.5 to 10 microseconds.
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Waveform Sawtooth or sine wave.
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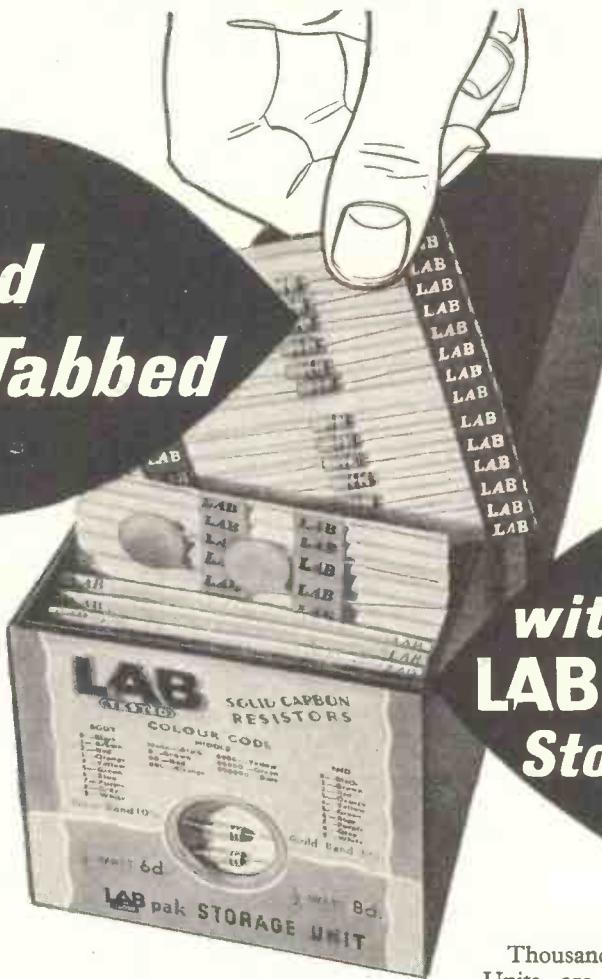
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LM	5 & 10	—	5 to 100K	72	300
LP	5 & 10	—	5 to 100K	72	300
CERAMICAPS					
CER	Tubular	500	3 to 470pf	141	500
HK	Tubular	500	470 to 5000pf	141	500
HKD	Disc	500	470 to 5000pf	141	500
Tolerances available ±2% 10%					

The LAB Continuous Storage Units are available from your normal source of supply, but more detailed information and literature can be obtained from

THE RADIO RESISTOR COMPANY LIMITED

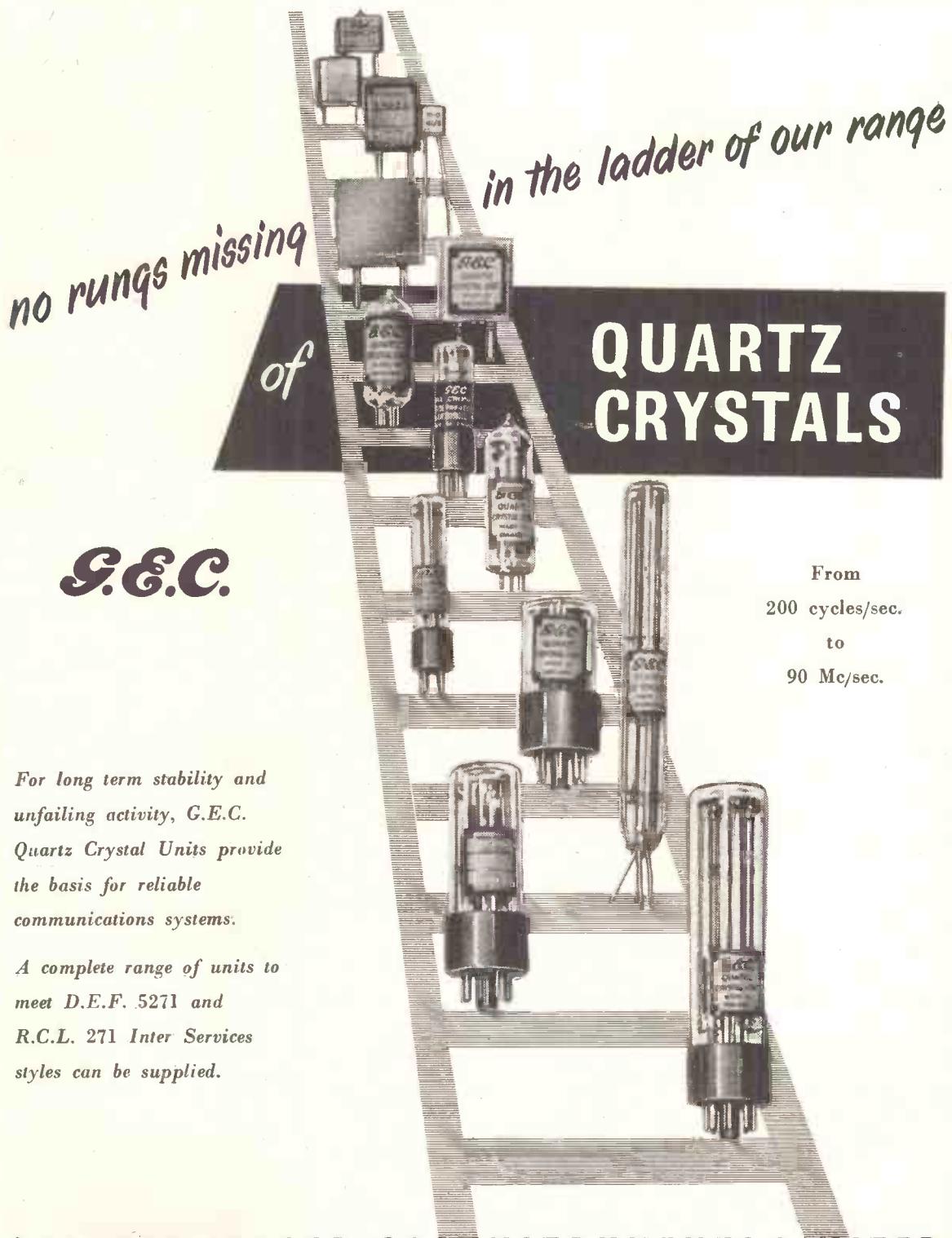
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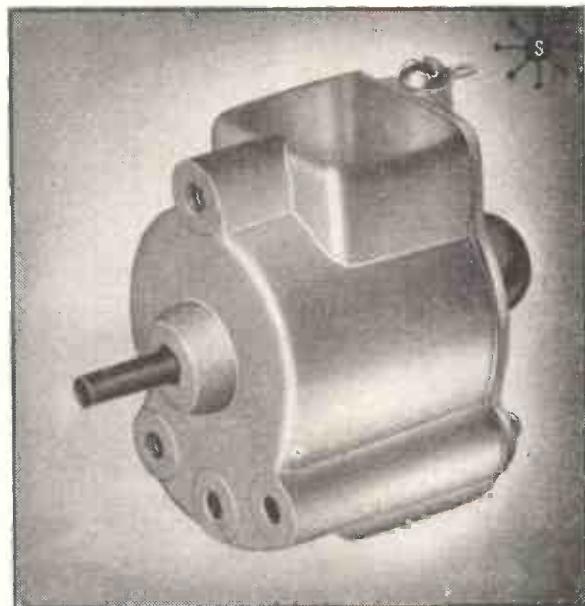
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Staar-Kinder

Manufacturers are invited to write or telephone for full information on this governor controlled constant speed motor. Only slightly larger than a match-box, the Staar-Kinder Motor presents a noiseless power unit of extremely low current consumption.

The standard unit is for 6v. operation, but the motor can be supplied for usage at other voltages up to 12v.

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... battery operated player
for single 45 r.p.m. records

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★ Powered by Staar-Kinder motor. Operating voltage 6v., current consumption as low as 27 mA while playing.

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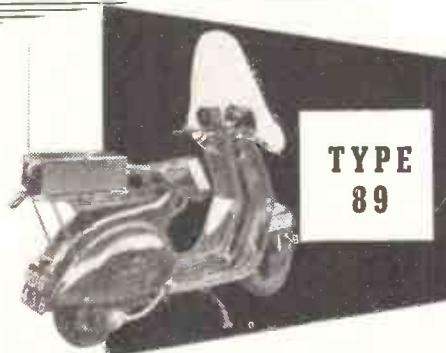


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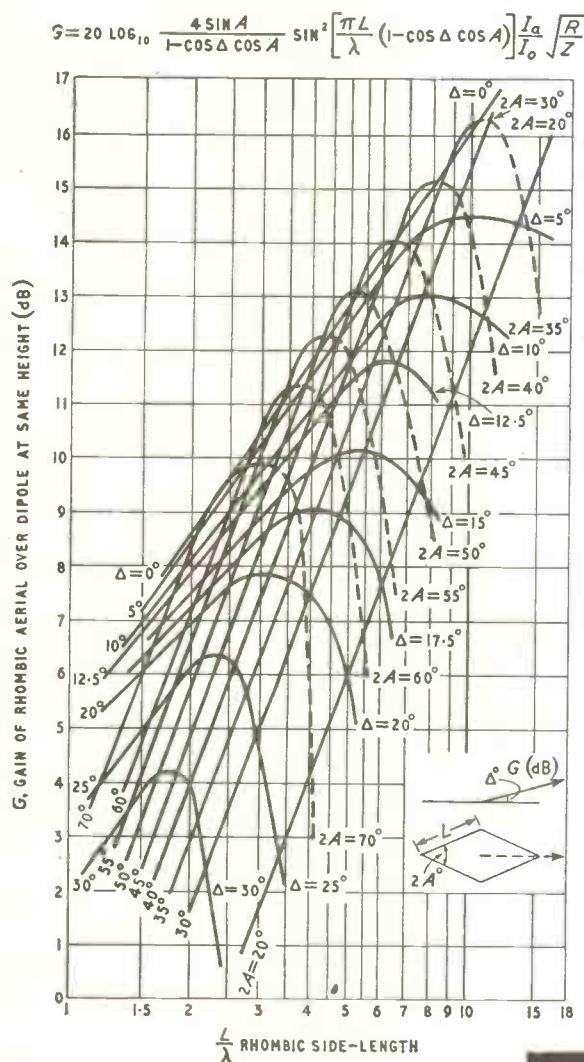
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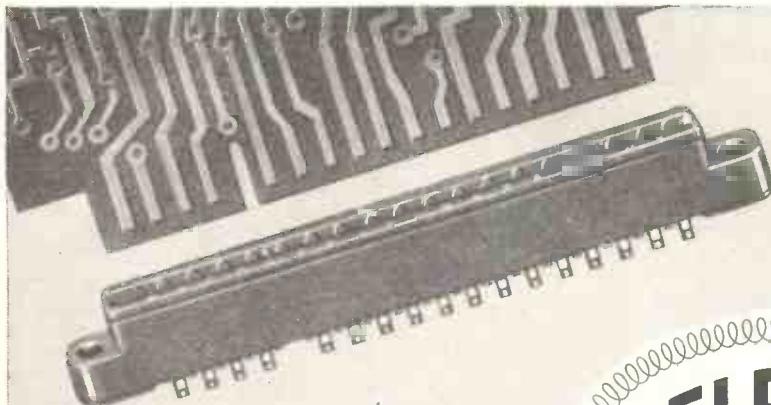
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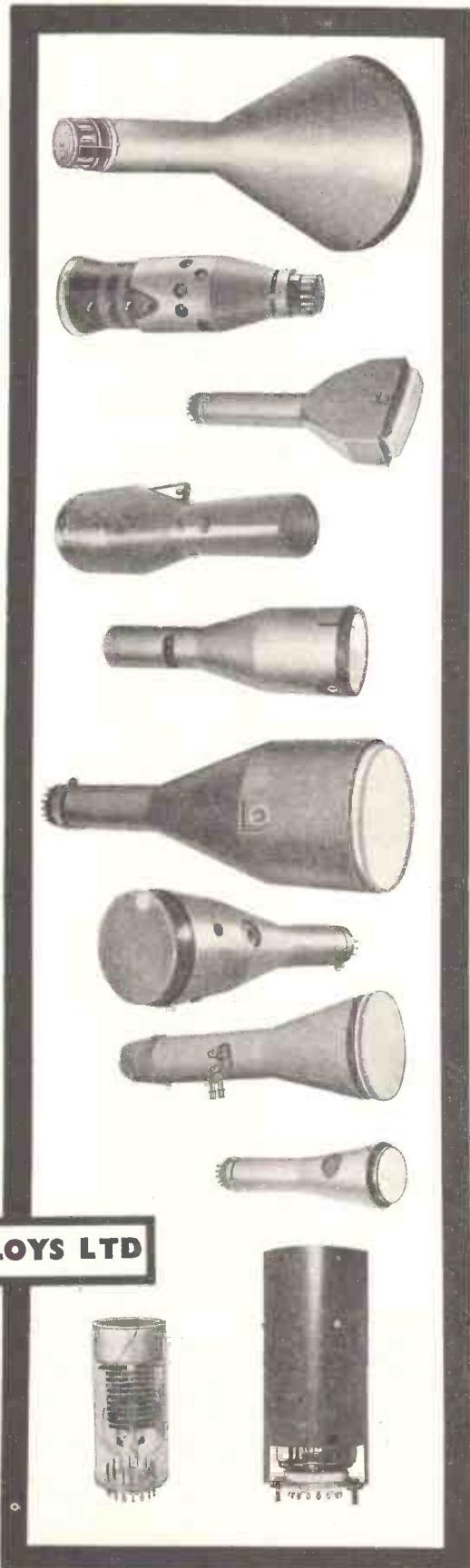
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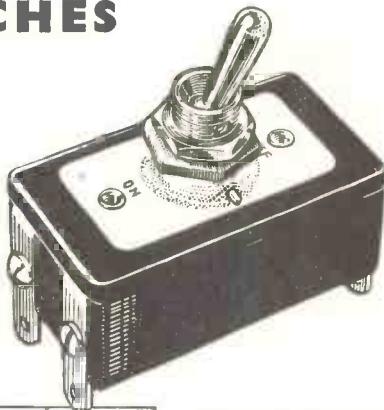
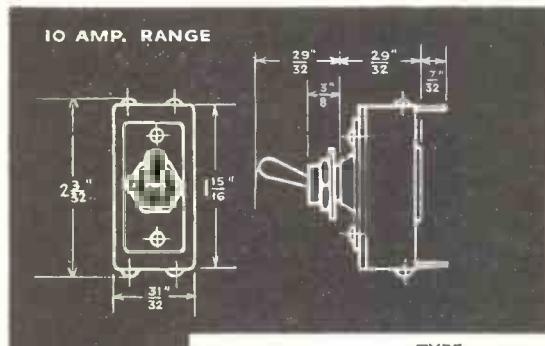
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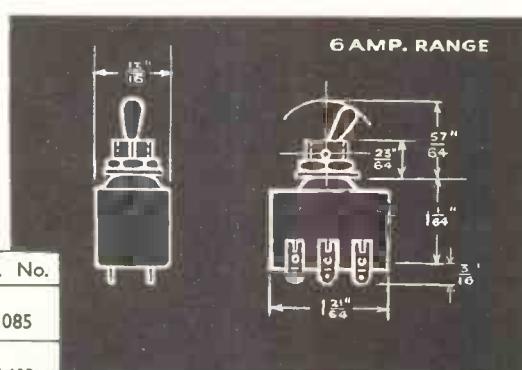
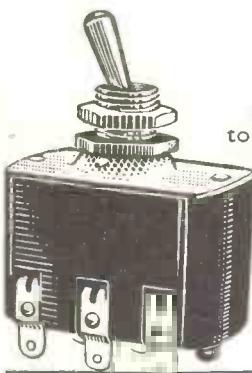
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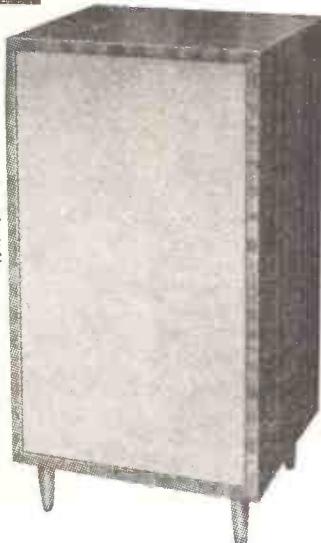
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Concert Grand Cabinet showing layout of deck



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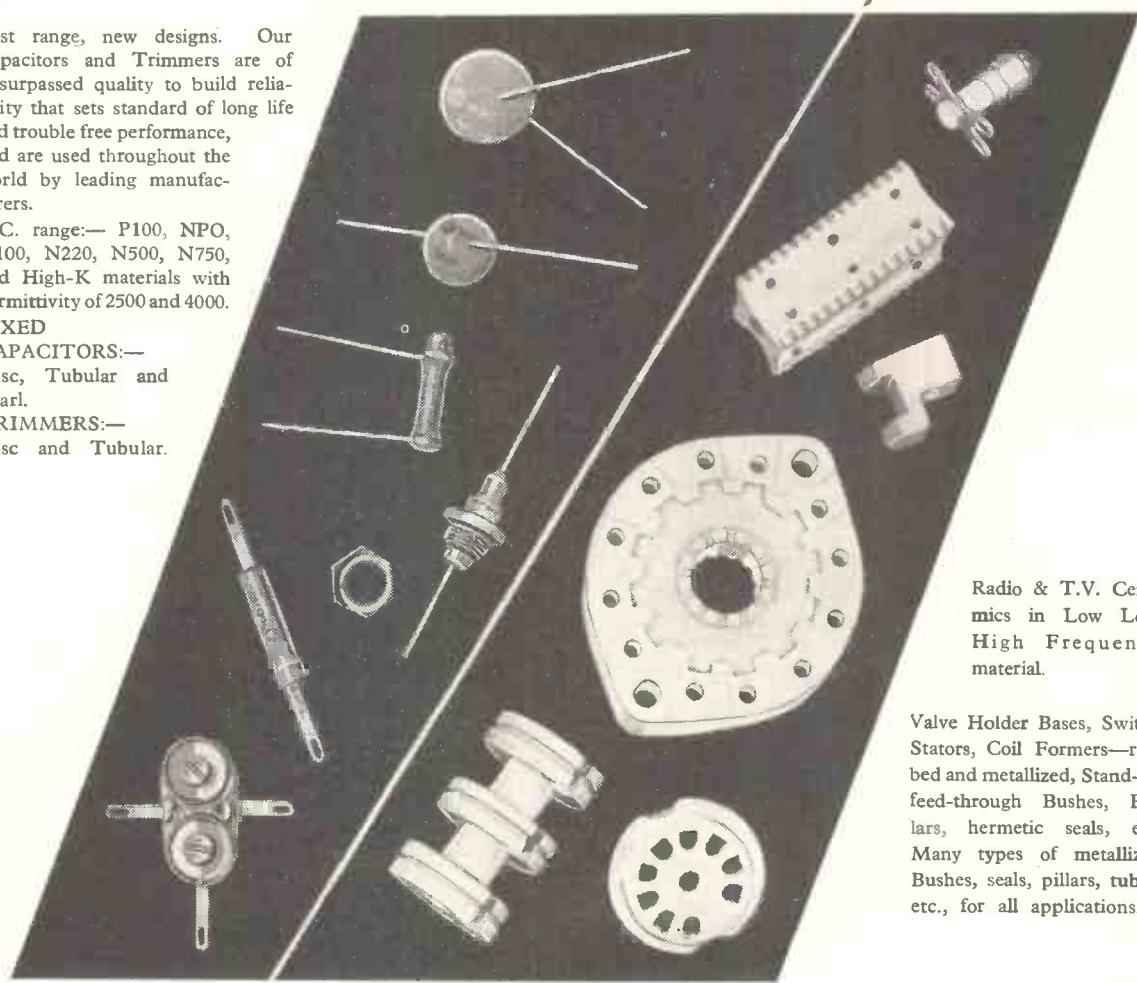
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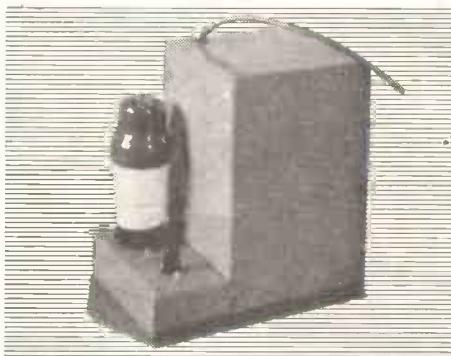
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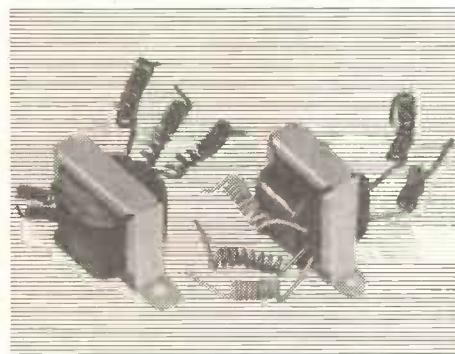
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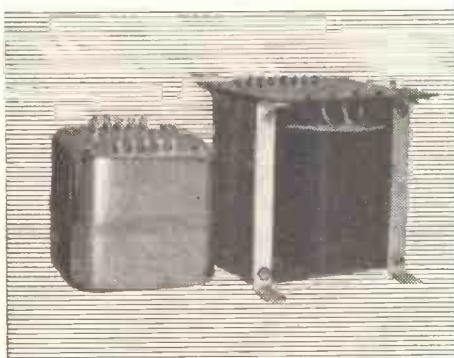
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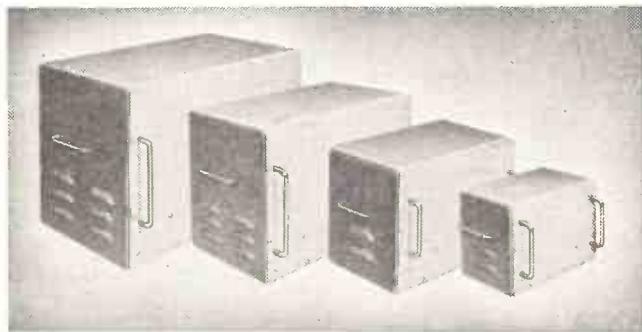
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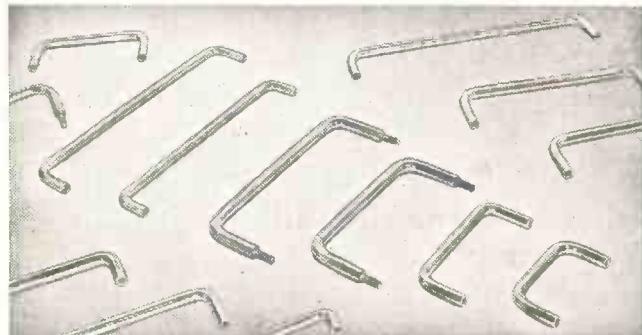
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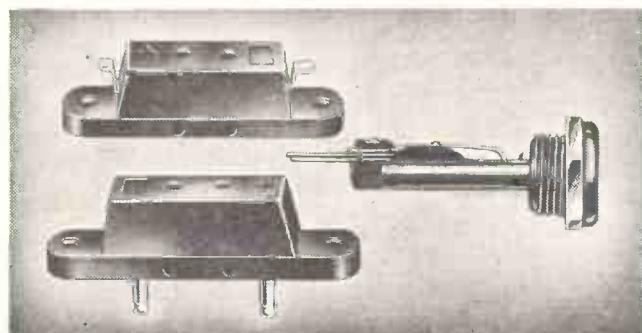
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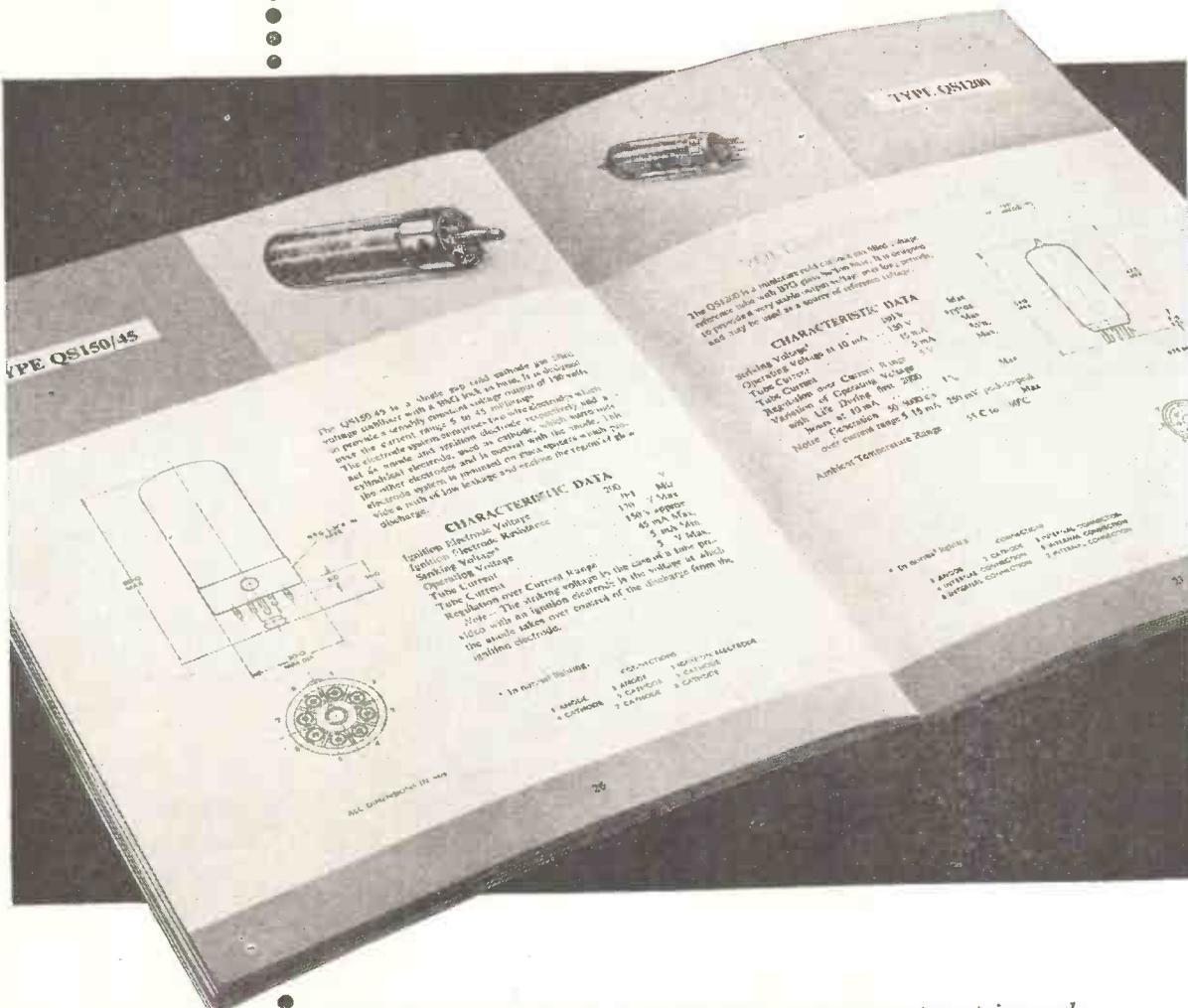
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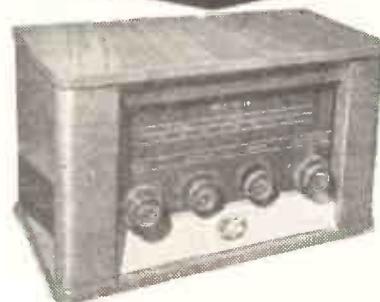
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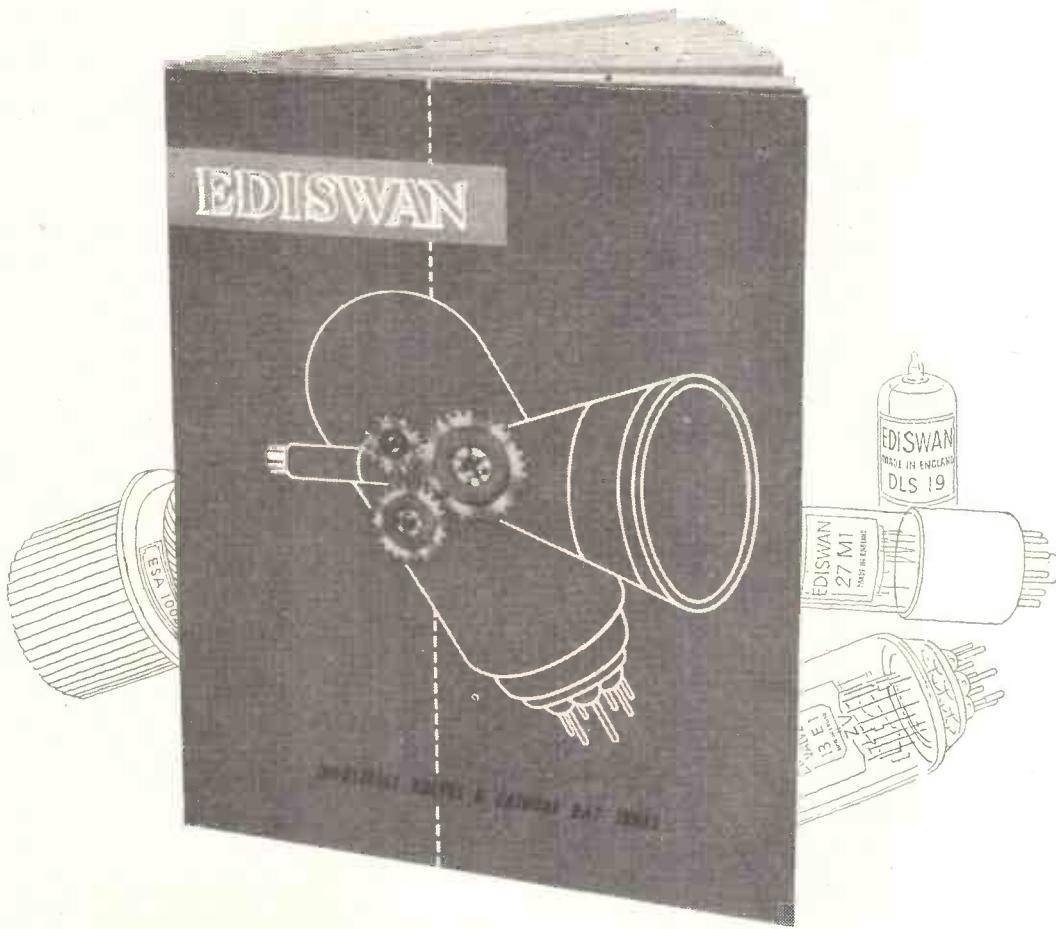
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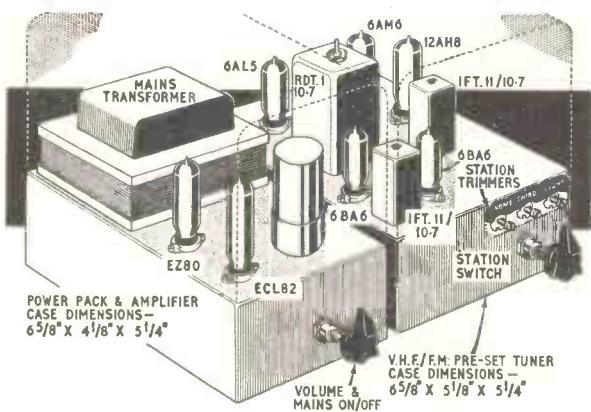
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Write for full data to the address below.

ABRIDGED DATA

The 3AFP1 is suitable for symmetrical or asymmetrical operation.

Heater

$V_h = 6.3V$ $I_h = 0.55A$

Typical Operation

$V_{a1} + a_3$	1000V
V_{a2}	210 to 320V
V_g	-28 to -65V
S_x	20V/cm
S_y	11.5V/cm

ETEL

Cathode Ray
Tubes



FLEXIBLE REMOTE CONTROL OUTFITS

offering facilities for making prototype flexible remote controls as required, without flexible casing. The Remote Control Flexible Shafts in these Outfits cover the range of torque loadings required for volume controls, wave change switches and condensers used in electronic, radio and television equipment.

No. I30 (.130 in. dia.) for controls up to 4 inches long
No. I50 (.150 in. dia.) for controls up to 6 inches long

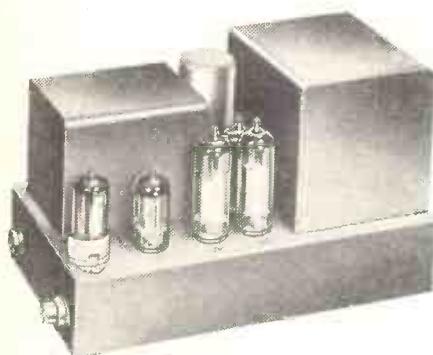
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Detailed Parts and Price List available upon request to Dept. W.

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10 WATT PUSH-PULL
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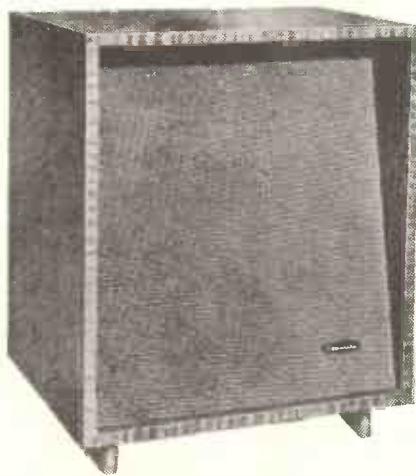
"These are Rare Virtues"

was the concluding comment by Mr. P. Wilson, The Technical Editor of "The Gramophone", reporting on the performance of GOODMAN'S '315' in the August 1957 issue of "THE GRAMOPHONE".

"This '315' Reproducer is the integrated version of the GOODMAN'S three-unit system which aroused my (and my wife's) enthusiasm in the report which was published last December.

What I said then can't be repeated on this renewed experience—and during the past month or so I must have listened to the Reproducer for some 250 hours, which is quite a long time when one comes to think of it. During the whole of that time it has never given us one moment's uneasiness, whether at low volume or at very high. It is sweet and clean and clear even on the slightest whisper; and it takes the crescendos to climaxes of tremendous power without a falter and with equal clarity. There is one difference from the earlier combination that I tested; the provision of the attenuators for the middle and treble units. I have no doubt whatever that these will enable a better balance to be obtained with the bass output. For the conditions I am using at the moment, I find the best setting of these controls to be about minus 6db., i.e., three steps down from maximum. In some other room I might want to modify these settings; there is plenty of range. One thing, however, I should insist upon: once a suitable setting has been decided, the controls should be left at that. What more is there for me to say? . . . I have never heard a better combination at any price and certainly this is the best middle register response I have yet come across. The two things that in my view stand out (and my wife concurs) are first, that the low part of the scale never seems to be obtrusive, though special listening indicates that all parts from the lowest bass to the highest treble are there; and the second, that the Reproducer sounds good, whether at high or at low volume or in passage from one to the other. These are rare virtues."

*EXTRACT from "THE GRAMOPHONE", August 1957
issue, reprinted by kind permission of the Editor*



This same quality in performance and standard of workmanship is found in the

◀ "SHERWOOD ENCLOSURE" which can be supplied fully equipped and tested as a single or twin unit system, or, if preferred without Loudspeakers.

The SHERWOOD is of unique design artistically and acoustically, and is intended to house the AXIOM 150 Mk. II (12", 15 watts) or the AXIOM 22 Mk. II (12" 20 watts) with provision for a TREBAX High Frequency unit and variable attenuator. It is finished in mahogany or walnut.

Dimensions: Height: 27½", Width: 23½", Depth: 20½".

GOODMANS 'High Fidelity Loudspeaker Manual (1957)' contains full details of the entire range of their High Fidelity products. A copy will be sent free on request.

'315' REPRODUCER SPECIFICATION

TYPE :

Multiple unit wide range loudspeaker system.

UNITS :

Bass : 12" Direct Radiator (Audiom 60 Bass).

Mid-Range : Horn Loaded Pressure Driven (MIDAX).

Treble : Horn Loaded Pressure Driven (TREBAX).

FREQUENCY RANGE :

30 c/s. to 16,000 c/s. (-8 db. at 20,000 c/s.)

CROSSOVER FREQUENCIES :

750 c/s. and 5,000 c/s. (Network XO/750/5000).

MAXIMUM POWER HANDLING CAPACITY :

15 watts (British Rating)

30 watts (American Rating)

IMPEDANCE :

15 ohms at 400 c/s.

ANGULAR DISTRIBUTION :

90° (Minimum at any frequency).

BASS LOADING :

Acoustical Resistance Unit (ARU.172).

CONTROLS :

Separate controls for mid-range and treble units, in the form of two constant impedance 8-step attenuators calibrated in 2 db steps.

CABINET :

Rigid construction with full acoustic lagging. Distinctive sapele veneers, finished in medium rosewood colour. Continental styling.

DIMENSIONS :

Height 37", width 23½", depth 21½".

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Australian Agents: British Merchandising (Pty.) Ltd.,

183 Pitt Street, Sydney, N.S.W.

Apply to: P.O. Box 3456, Sydney, for H.F. Loudspeaker Manual, 1957.

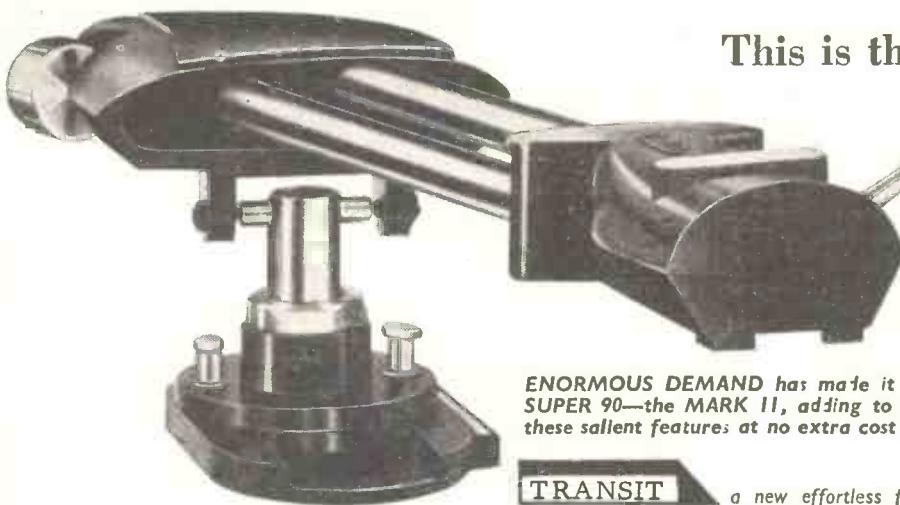
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even lower vertical force can now be achieved.

RIGIDITY

this is implicit in the design of the new 'T' type pillar.

SIMPLICITY

height adjustment ring makes mounting on a turntable of any height simplicity itself.

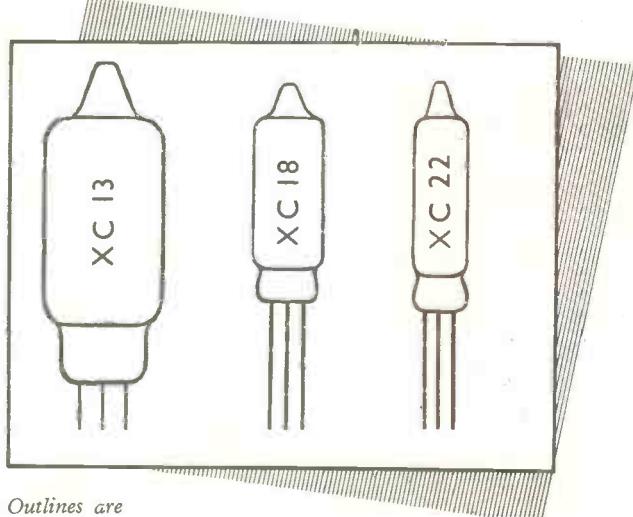
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RATINGS (nominal)	XC13	XC18	XC22
Anode strike volts (min)	200	210	210
Anode maintain volts	70	73	70
Trigger strike volts	75	68	69
Trigger maintain volts	55	55	55
Continuous cathode mA	7.5	1.0	0.25

C12.



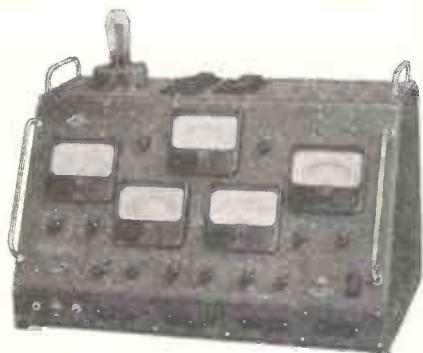
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TECHNICAL CHARACTERISTICS: Filament volts: 19 values from 1.1 to 117 v. Anode volts: variable from 0 to 300 v max, current 100 mA. Auxiliary Grid volts: Two identical sources. Variable from 0 to 300 v. max, current 15 mA. Control Grid volts: Variable from 0 to 50 v. Power supply stabilisation: less than \pm 1% variation of all sources for \pm 10% power supply variation. Power supply: 110-130-220-250 v. 50-60 c/s. Tubes used: 3 x 5Y3 GB, 2 x 6V6, 2 x 6L6, 3 x 6AU6, 2 x OB2. Dimensions: 24 x 13 $\frac{1}{2}$ x 15 $\frac{1}{2}$ in. (610 x 340 x 400 mm.). Weight: 66lb. (30 kg.).

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TECHNICAL CHARACTERISTICS:

Sensitivity: 10,000 ohms per volt A.C. and D.C.
A.C. and D.C. volts: 3 (666 Ω/V)—7.5—30—75—150—300—750
A.C. and D.C. currents: 150 μ A—1.5—15—75—150—1,500 mA.
Accuracy: 1.5% on D.C. ranges and 2.5% on A.C. ranges.
Resistances: 0—2 M Ω .
Dimensions: 5 $\frac{1}{2}$ x 4 x 1 $\frac{1}{2}$ in. (140 x 100 x 40mm.).
Weight: 1lb. 8oz. (680 gr.).

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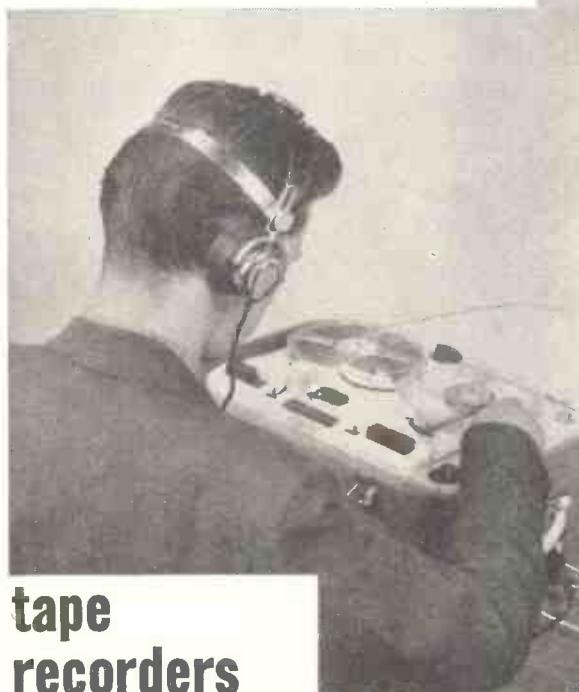
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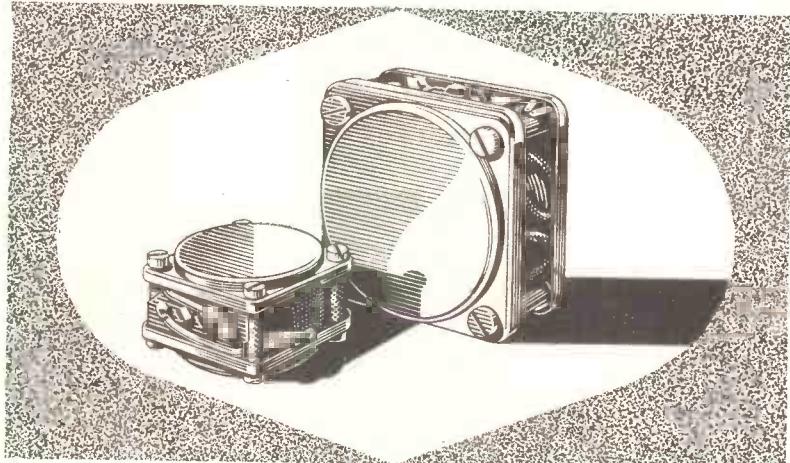
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are now even easier to install



Designers of communications equipment, will welcome the new mounting and terminating arrangements of the Mullard 25mm and 36mm pot cores.

Unique design features that make installation easier than ever, include positions for tag boards on three sides and a new system of fixing, which eliminates the need for additional mounting plates.

Combining constructional advantages with sound technical performance, these 25mm and 36mm pot cores take full advantage of the low loss of Ferroxcube to produce inductances of up to 30 henries, together with high Q values over a wide frequency range. As an additional service these pot cores can be supplied wound to individual specifications, if required.

Write now for full details of the comprehensive range of Mullard pot cores currently available.

Outstanding features

- * Controllable air gap, facilitating inductance adjustment
- * Self screening
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Mullard



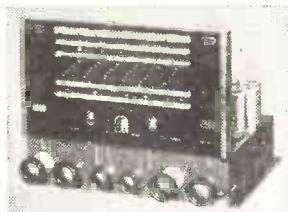
**'Ticonal' permanent magnets
Magnadur ceramic magnets
Ferroxcube magnetic cores**

Mullard Ltd., Component Division, Mullard House, Torrington Place, W.C.I

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Armstrong AF 105 CHASSIS

CUSTOM BUILT INTO A COMPLETE RADIOPHONIC



For those who want high quality reproduction without the "do-it-yourself" work that is normally involved, we offer the audio perfection of the AF 105 Amplifier (with AM and FM radio) in an acoustically designed non-resonant cabinet with a choice of good quality speaker and gramophone units as shown below.

In each case the results represent a very close approach to genuine high fidelity performance and of a much higher standard of listening than is possible from ordinary commercial radiograms. Hear them for yourself at our Holloway Demonstration Rooms (open Weekdays and Saturdays until 6 p.m.) or, if you are unable to visit us, take advantage of our 7 day free home trial arrangements.



THE STANDARD AF 105 RADIOPHONIC

The basic equipment comprises the AF 105 in the STANDARD cabinet, with adjustable reflex chamber. Alternative gramophone units (GOLDRING GL 56 Transcription Unit, or COLLARO RC 457 Autochanger) and 10in. speakers (WHARFEDALE Golden, or GOODMAN T47) can be fitted to choice as follows:

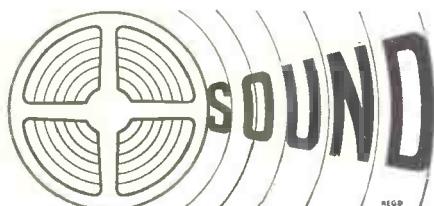
PRICE SCHEDULE

1 with RC 457 and T47	£88	4	6
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AF 105 £37 Cabinet available separately.			

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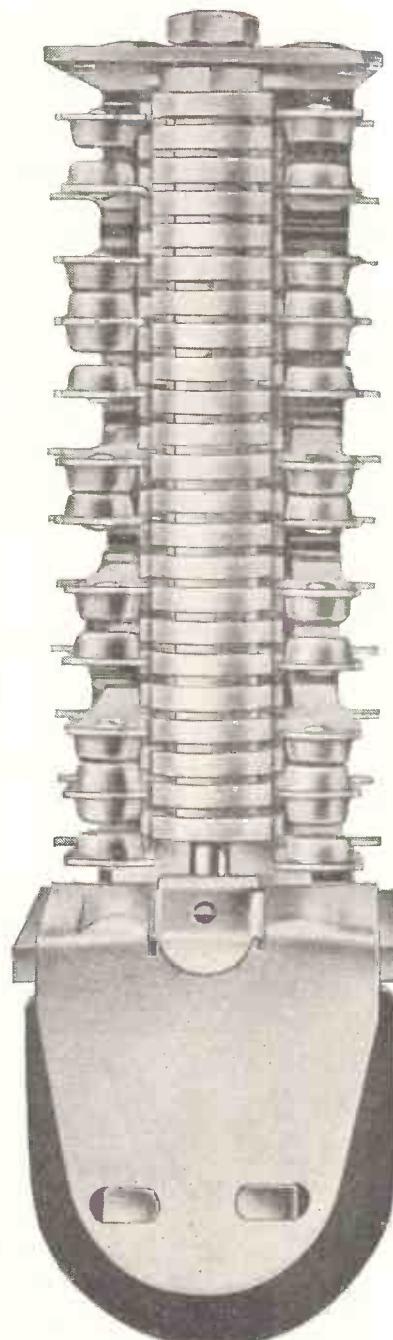
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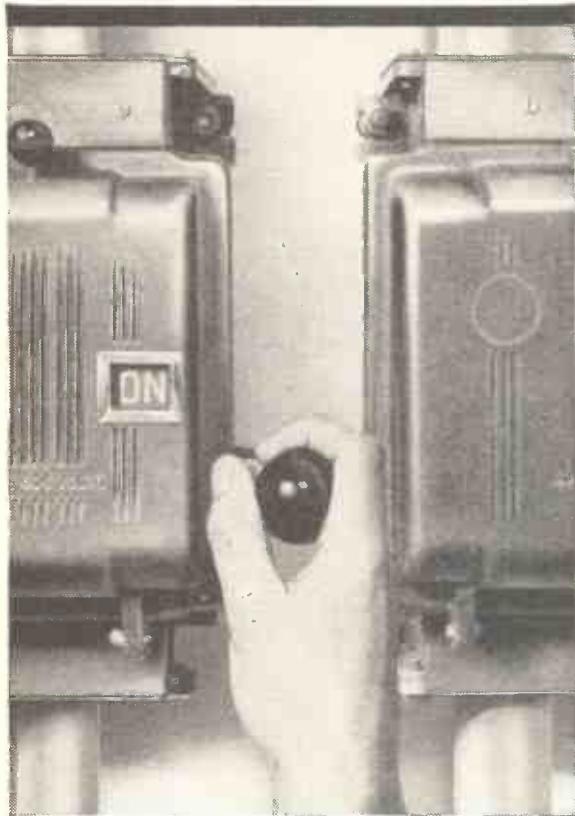


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Insulating and sheathing materials are Vulcanised Rubber, Polythene, and PVC. For really tough assignments Mervin (PVC) and 'Merthane' (Polythene and PVC) cables particularly resist acids, oils, alkalis and solvents, oxidising agents and direct sunlight.

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LIVERPOOL 20



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We cannot do the Indian Rope Trick but with

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We can operate any element requiring rotation or push-pull movement, or both, no matter if the controlled element is close to or at a distance from the control point.

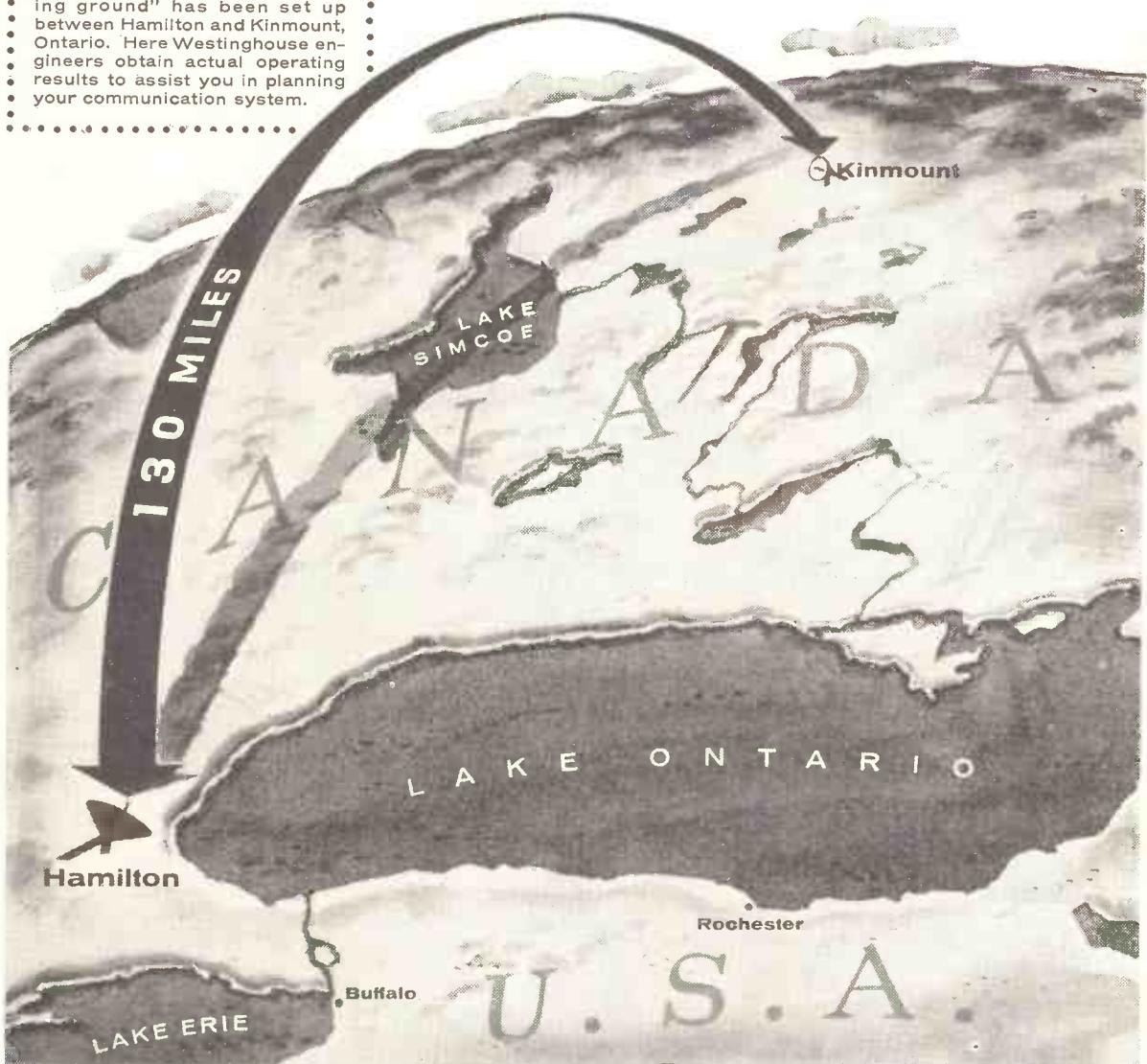
We can operate from an accessible point, switches, valves and other electrical and mechanical devices located in inaccessible places.

We can, in fact, solve your problems.

Flexible Shaft Handbook available to technicians on request to Dept. W.



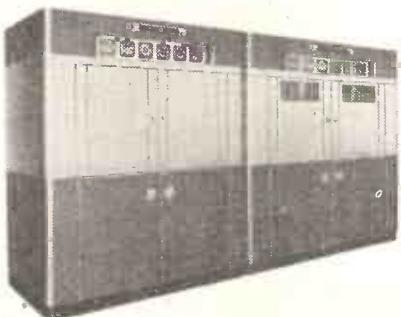
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Transmitting and Receiving Equipment
is compactly and durably designed for
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- Now for the first time in the communications field, scatter equipment for super-high frequency transmission for fixed or transportable operation has been introduced by Canadian Westinghouse.

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Contact your local Westinghouse Sales Office for Descriptive Bulletin H83-100 or write Canadian Westinghouse Company Limited, Electronics Division, Hamilton, Canada.

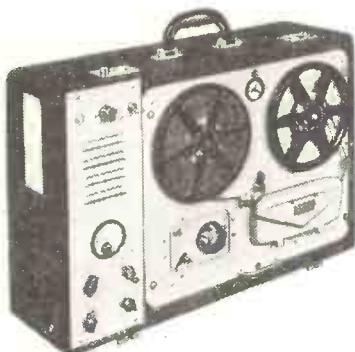
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Try our post service for your spools, splicers, tapes, etc. All leading makes in stock, and sent to you by return post.



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Super-sensitive FM Tuner £24.3.0 plus £9.8.4 P.T.



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PLUG-IN-AND-PLAY Record Reproducers

Above is the RCA "PRESIDENT" High Fidelity phonograph, ready-to-play, automatic changing, console record reproducer of outstanding quality. Panoramic multiple speaker system; new triple control with balanced loudness feature; 20 watt peak push-pull power from extended range amplifier; elegantly styled in superb cabinets in walnut, light oak, or dark oak finishes.



68 GNS.

(tax paid)

The RCA "VICE PRESIDENT" High Fidelity phonograph (illustrated right) is a beautifully styled record reproducer with a quality of reproduction never before associated with instruments of its size. Panoramic triple speaker system; 10 watts peak power from push-pull amplifier with frequency range 40-20,000 cycles; triple control system; 4-speed changer.

43 GNS. (plus £1.15.0 optional legs)
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RCA GREAT BRITAIN LIMITED, Lincoln Way, Sunbury-on-Thames, Middx.
(An Associate Company of Radio Corporation of America) Telephone: Sunbury-on-Thames 3101.

THE WAYNE KERR VIDEO OSCILLATOR TYPE O.22B



Specification

Frequency Range:
10 kc/s—10 Mc/s in 6 ranges
and 50 c/s square wave.
Frequency Stability: better
than 1 in 10^3 in 1 hour.
Frequency Accuracy: 1%.
Output Range: + 10 db
to - 50 db on IV p-p.
Output Level: Constant to
 ± 0.5 db at any frequency
setting. Output
Impedance: 75 ohms.
Total Harmonic Content:
less than 1%.

OUTPUT LEVEL STABILISED TO $\pm \frac{1}{2}$ DB
Over full frequency range 10 kc/s—10 Mc/s

An outstanding feature of the Wayne Kerr Video Oscillator Type 0.22B is a thermistor bridge circuit stabilising the amplitude. Once set the output level will remain constant within 0.5db while the oscillator frequency is varied over its full range of 10 kc/s to 10 Mc/s.

Other advantages are the facility for indicating the modulus of the load impedance to which the instrument is connected and a 50 c/s square wave output for examination of the low frequency characteristics of video networks.

In transportable case, or for standard 19" Rack mounting £175



WAYNE KERR

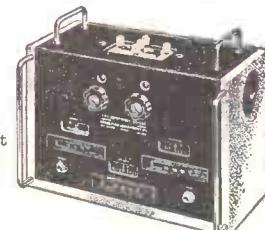


**Radio Frequency Bridge
Type B601**

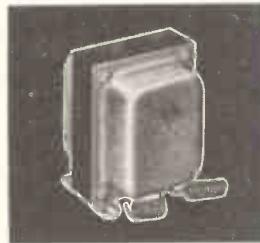
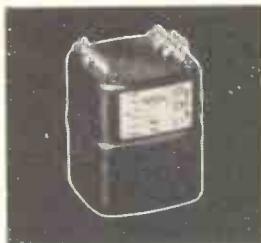
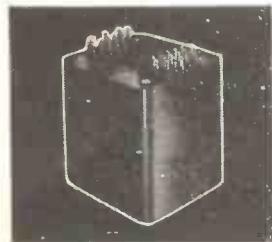
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Type B.801**

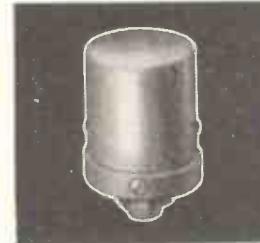
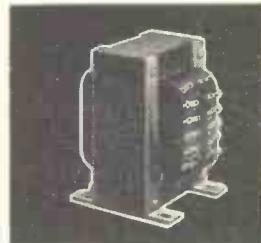
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TRANSFORMER CO. LTD



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especially to suit your home!



The latest improvements are incorporated and these extra features, that make for flexibility in use.

- ★ Separate Control Panel and/or
- ★ Combined pre-amplifier and control unit
- ★ Extra Power for F.M. Tuner Units

The separate control unit or the combined pre-amplifier and control unit can be fitted in the top or front of the cabinet, and the main amplifier, connected to the control unit by the special leads supplied, may be placed wherever it is convenient.

There is no doubt whatever that music lovers will find this amplifier provides them with a means of obtaining the perfect quality reproduction they so much desire.

With separate control panel £21 10 0

With combined control panel and pre-amplifier ... £27 0 0

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NEW LOW-COST RADIO RELAY EQUIPMENT FOR DEPENDABLE, ECONOMICAL MULTICHANNEL COMMUNICATIONS

*RCA MM-2 provides
multiplex telephone and
telegraph circuits in 152 to 174 mc band*



RCA MM-2 radio relay equipment is ideally suited for private, commercial or governmental application where from 1 to 6 channels are needed for opening new radio communications. The modulation bandwidth, from 300 cps to 28 kcs, can provide up to five 3 kc carrier derived telephone-channels plus one voice frequency channel. Each channel may be further multiplexed for high speed voice frequency carrier telegraphed circuits, teleprinter or manual telegraph, tele-metering and control circuits.

Compact, Easy Access Design. The entire MM-2 equipment, including multiplex equipment such as the RCA MV-124, can be mounted in one standard 19" width rack. All tubes, components and adjustment controls are readily accessible for maintenance and service purposes. The simplicity and dependability of the equipment reduce maintenance to a minimum.

The Transmitter unit, with built-in power supply, features crystal con-

trol and phase modulation, and provides a power output of 60 Watts. When used in conjunction with a directional type antenna, the effective radiated power may be increased.

The Receiver makes use of two crystal controlled local oscillators in a double conversion superheterodyne circuit. A Receiver Power Supply is also furnished as part of the basic equipment.

Low Cost MM-2 Packages are available to meet the needs of every user. RCA Communication specialists will study the system requirements, terrain, and other factors, to recommend the correct equipment package. Adoptions will be made to meet local power supply, or a power supply will be included in the equipment package.

For further information on this low-cost radio communications equipment see your local RCA Engineering Products Distributor or write to Dept. RR49L, RCA International Division, 30 Rockefeller Plaza, N. Y. 20, N. Y.

TYPICAL MM-2
TERMINAL rack shown here
with transmitter, receiver, and
power supply on upper half
with multiplex equipment
mounted below.



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RADIO CORPORATION of AMERICA

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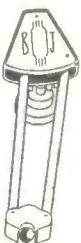
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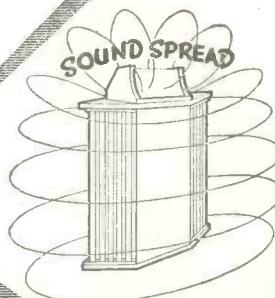
See also our advertisement on page 48.

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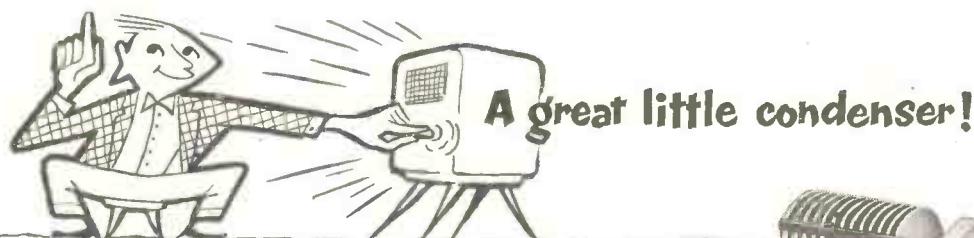
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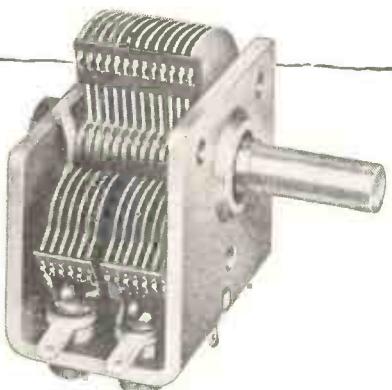
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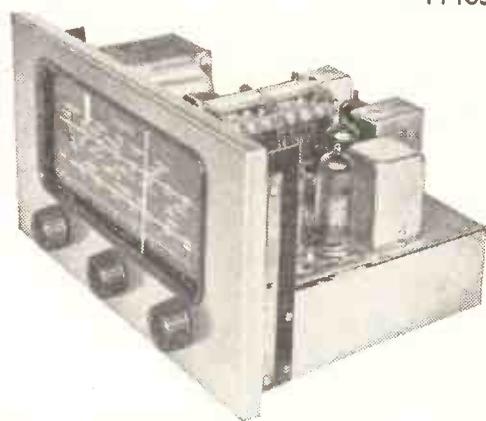
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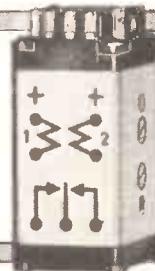


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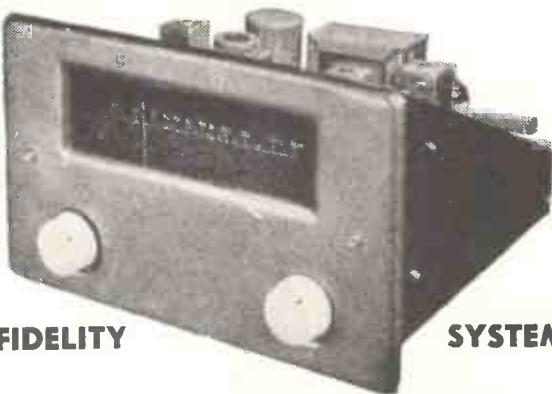
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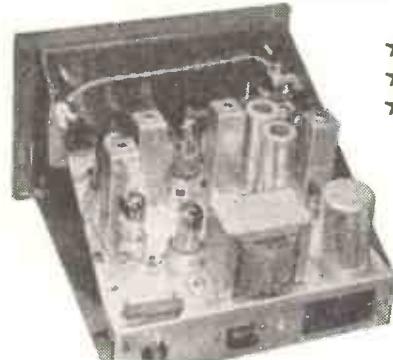
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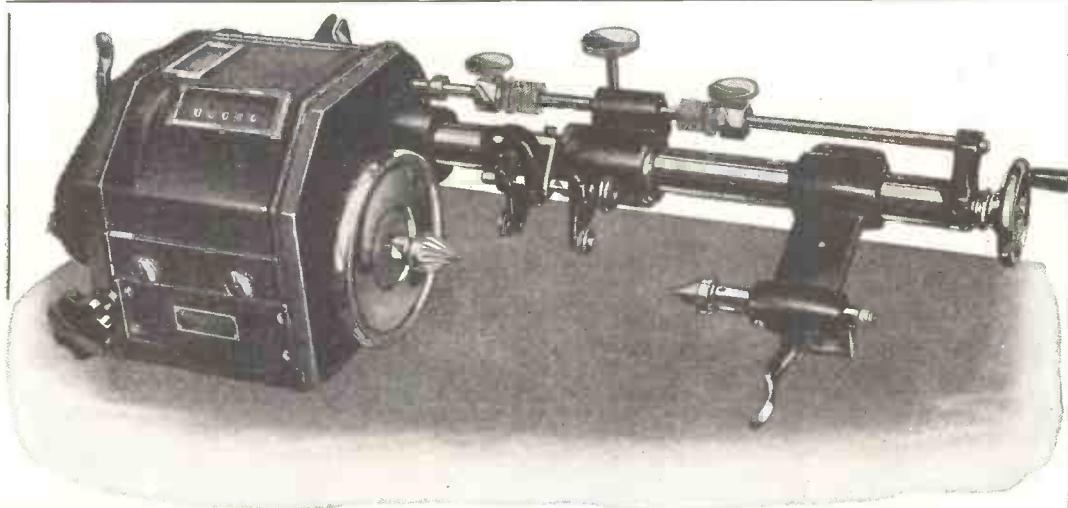
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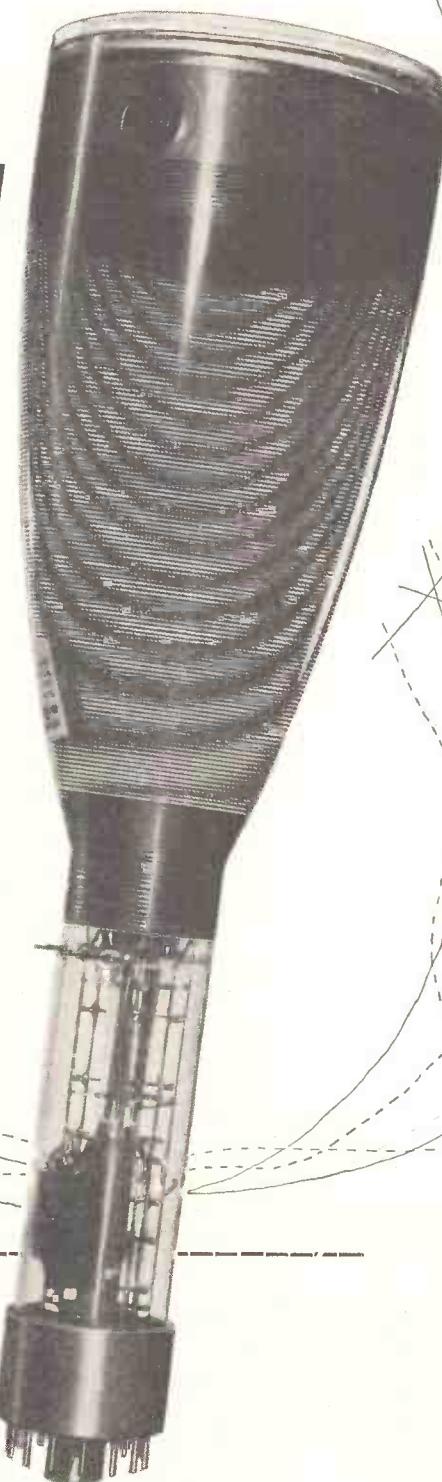


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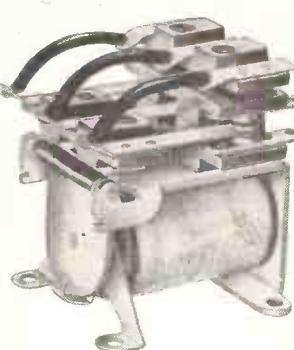
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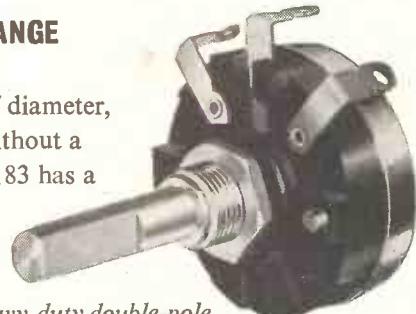
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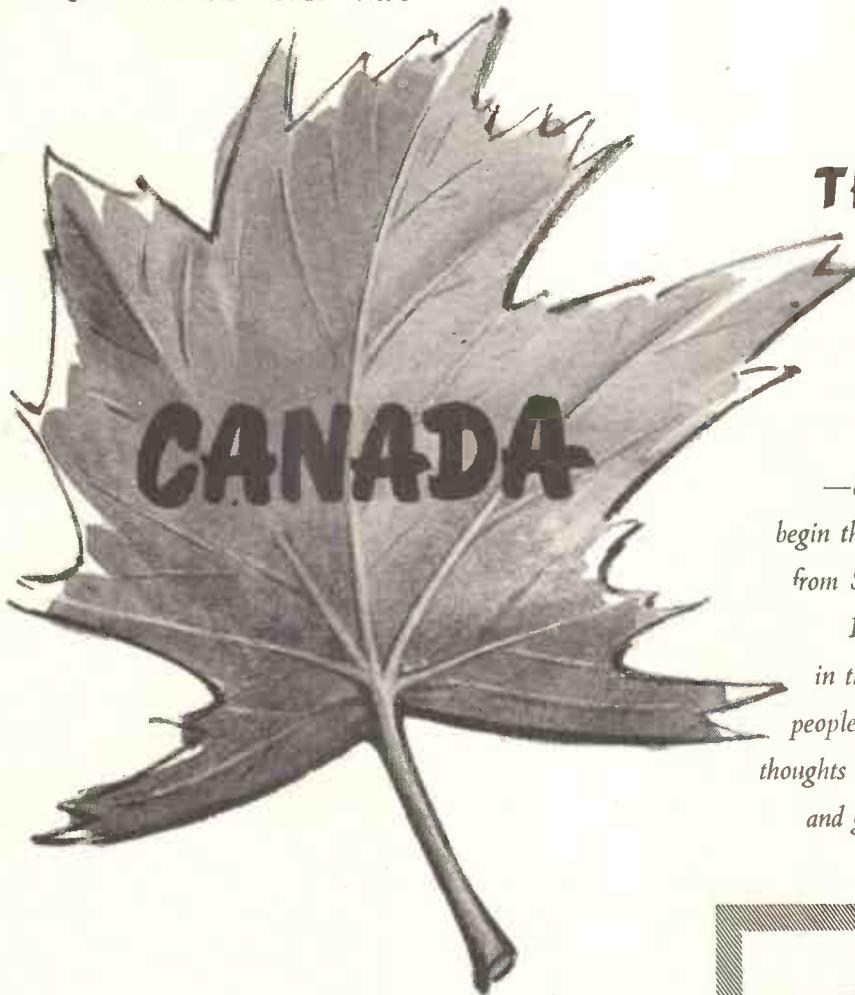
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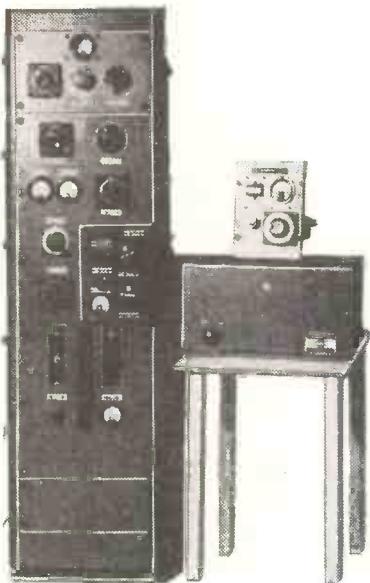


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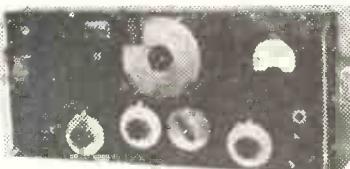
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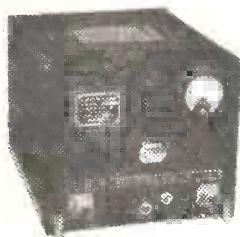
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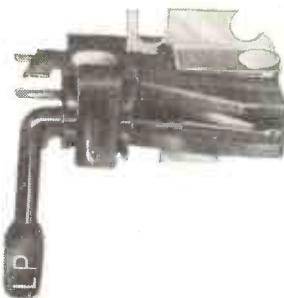
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AMERICAN HANDY TALKIE. Type B.C.611 including two operating crystals (5-6 Mc. band),

£19/10/-. Postage and packing 10/-.

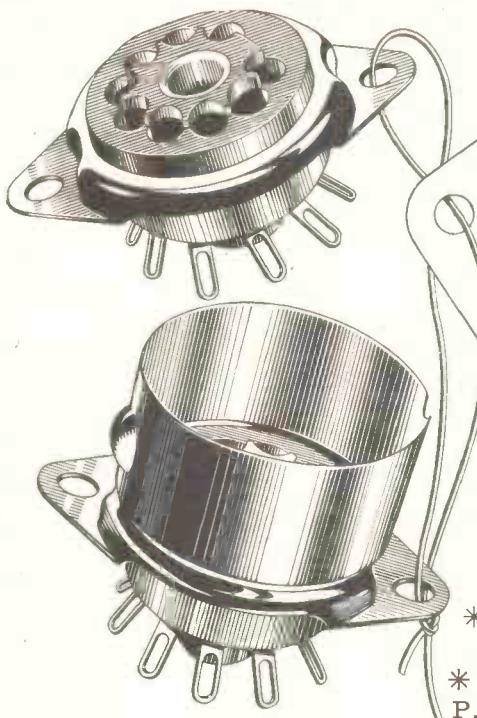
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Telephone Towcester 312



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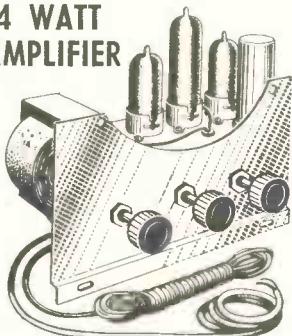
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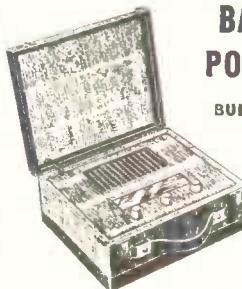
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**THREE VALVE TYPE (ECC83, EL84,
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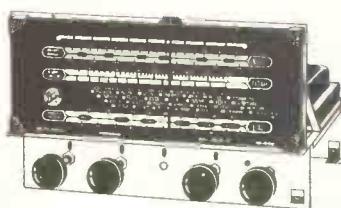
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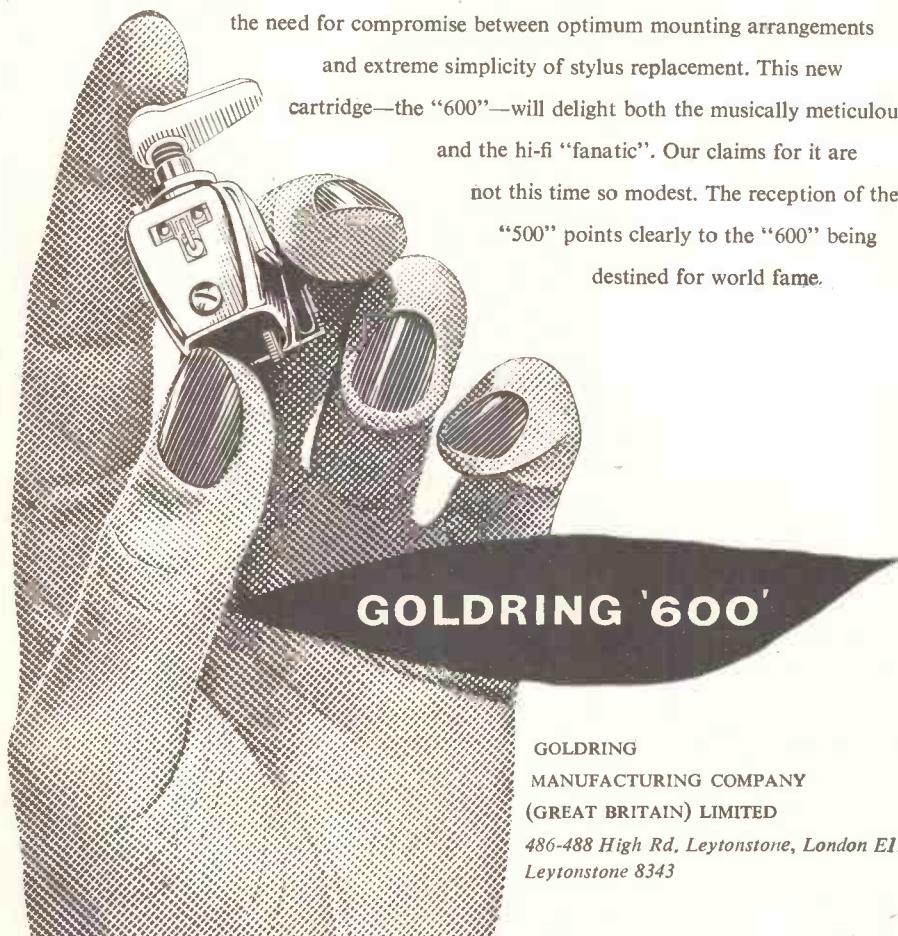
The "600" is similar in shape and size to the latest version of the "500". Replaceable styli—diamond for L.P. and sapphire for 78 r.p.m.

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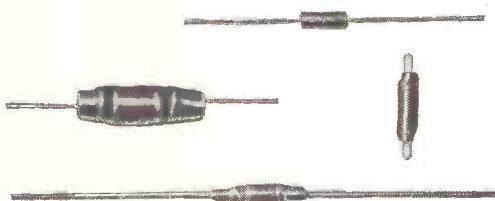
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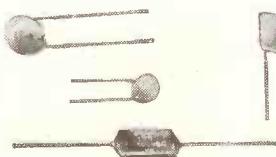
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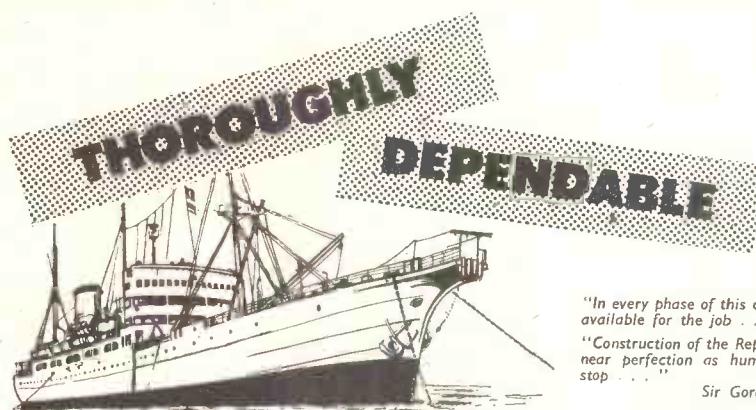
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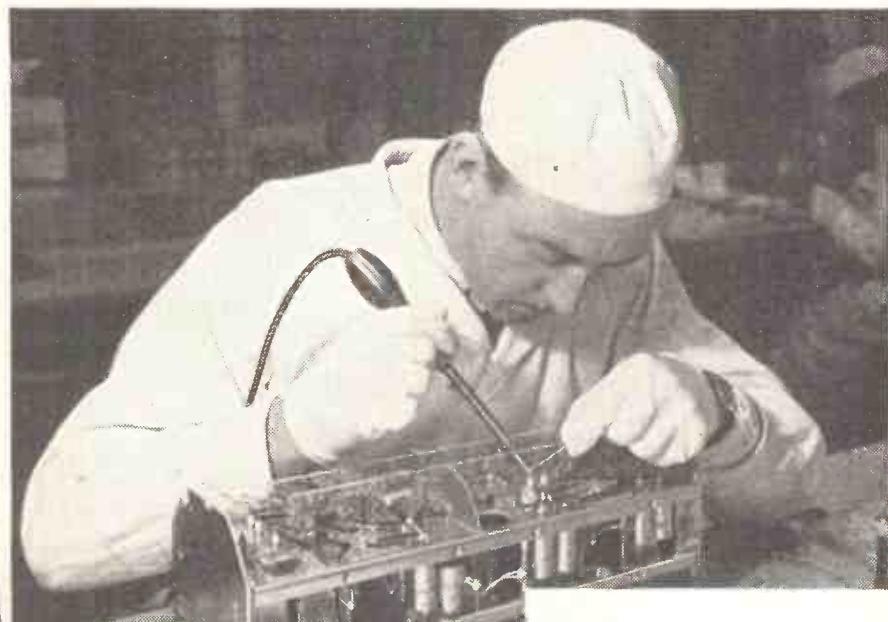


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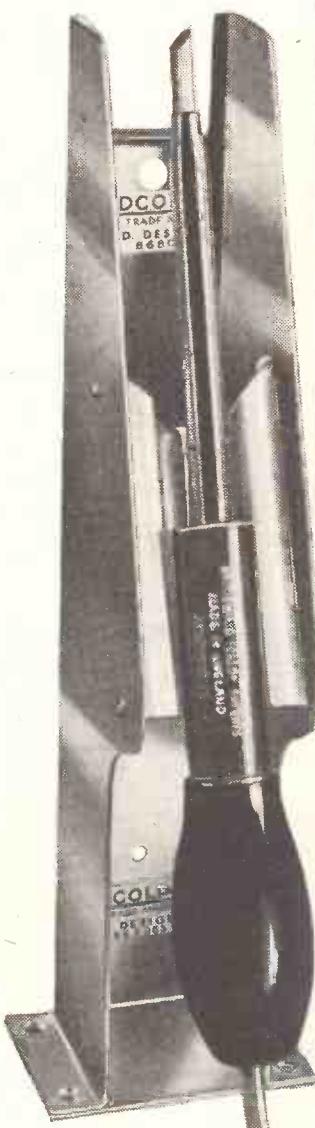
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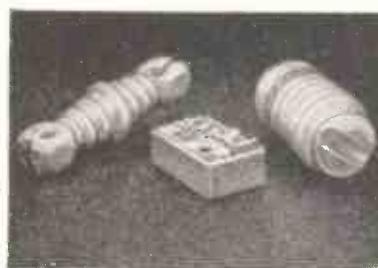
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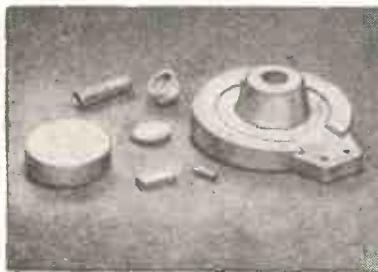
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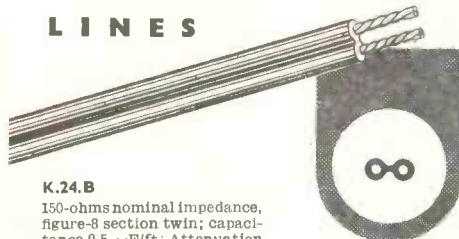
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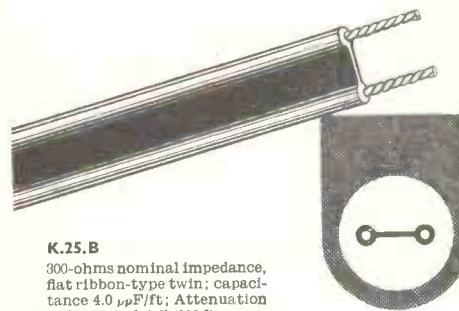
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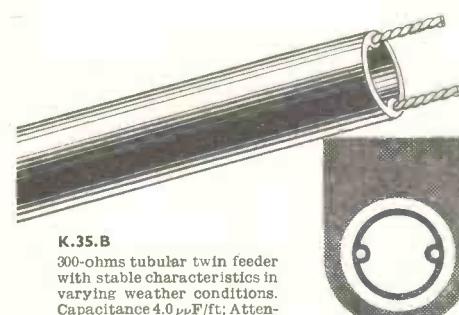
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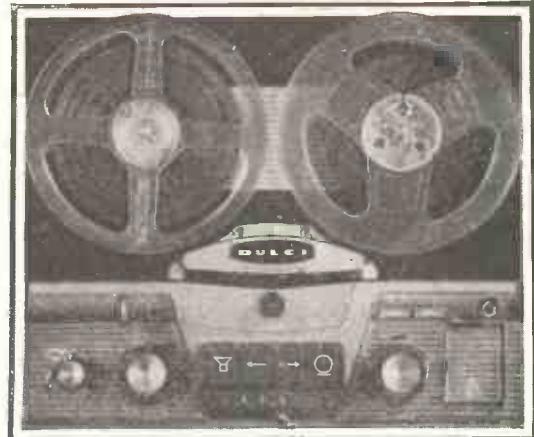
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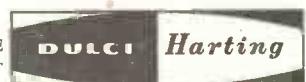
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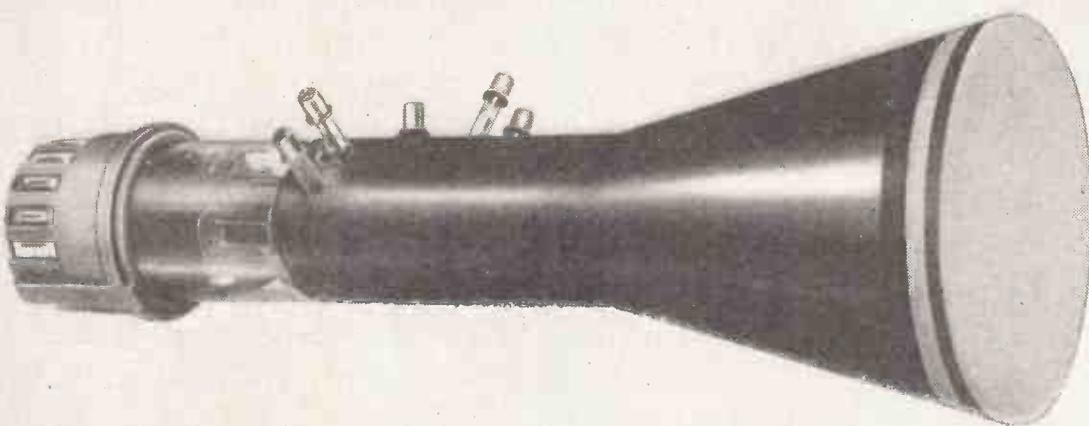
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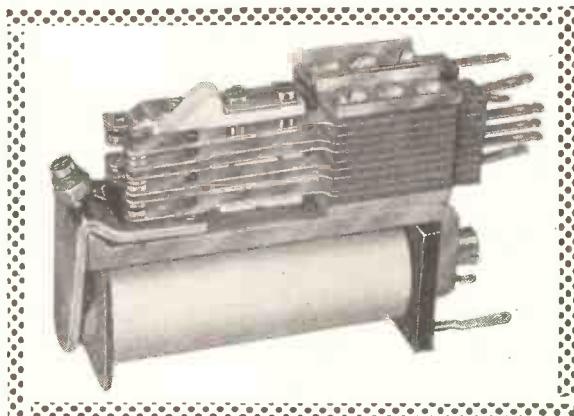
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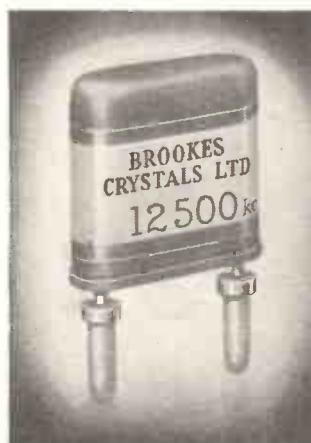
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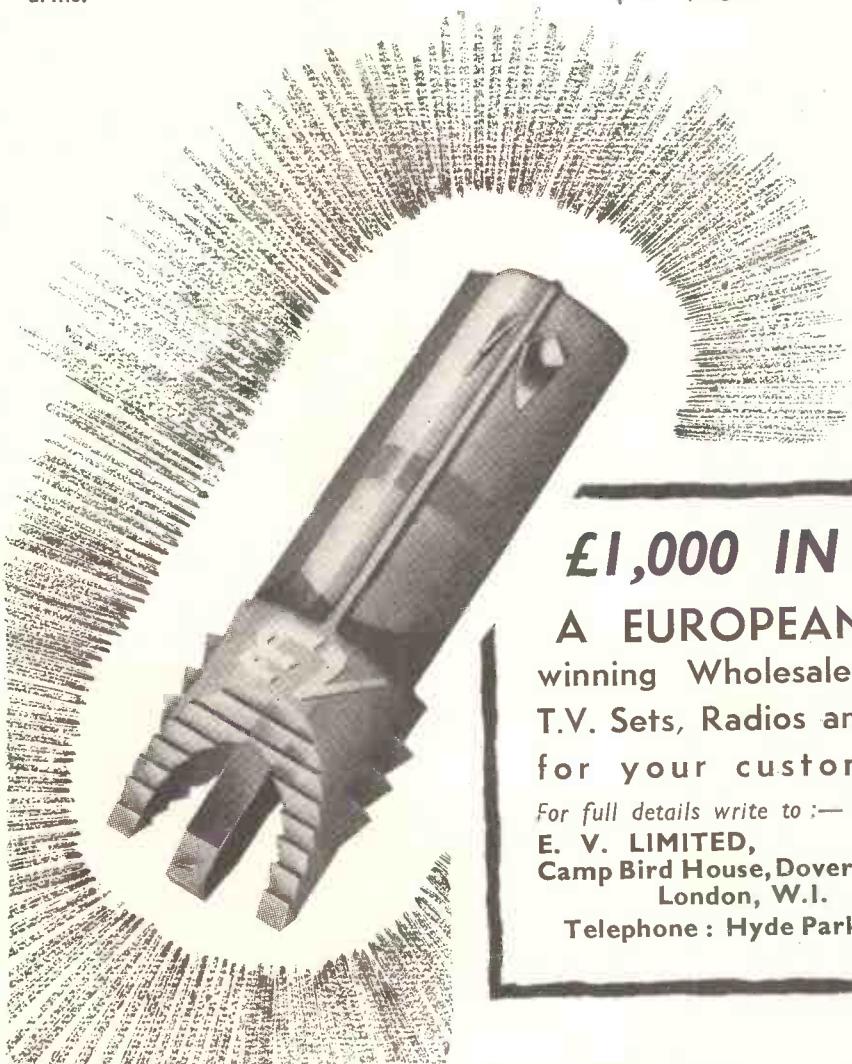
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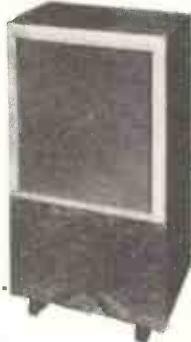


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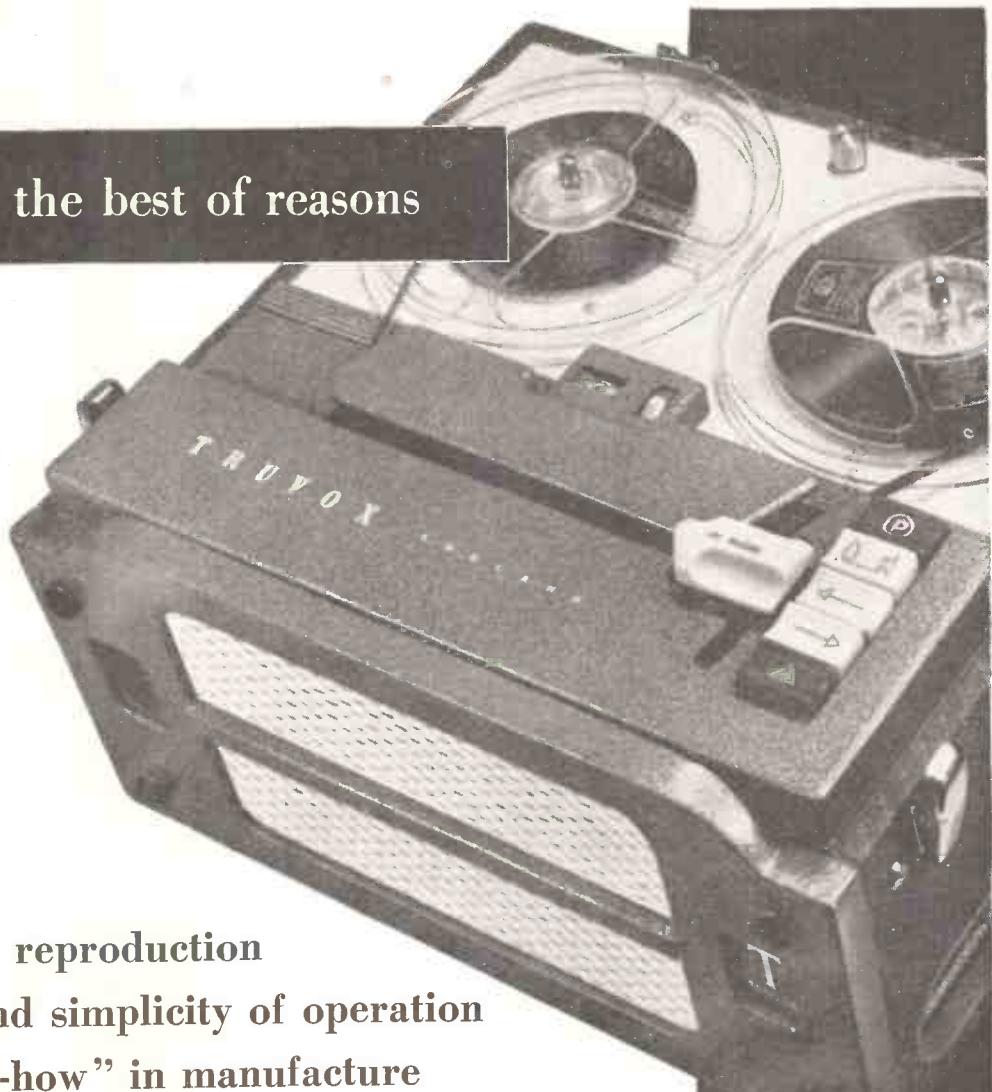
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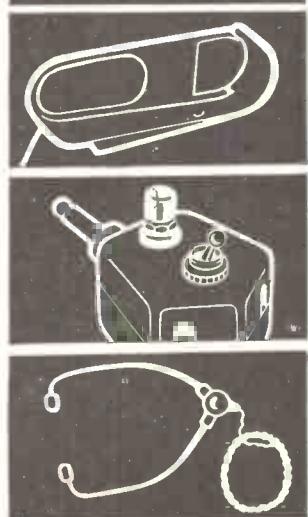
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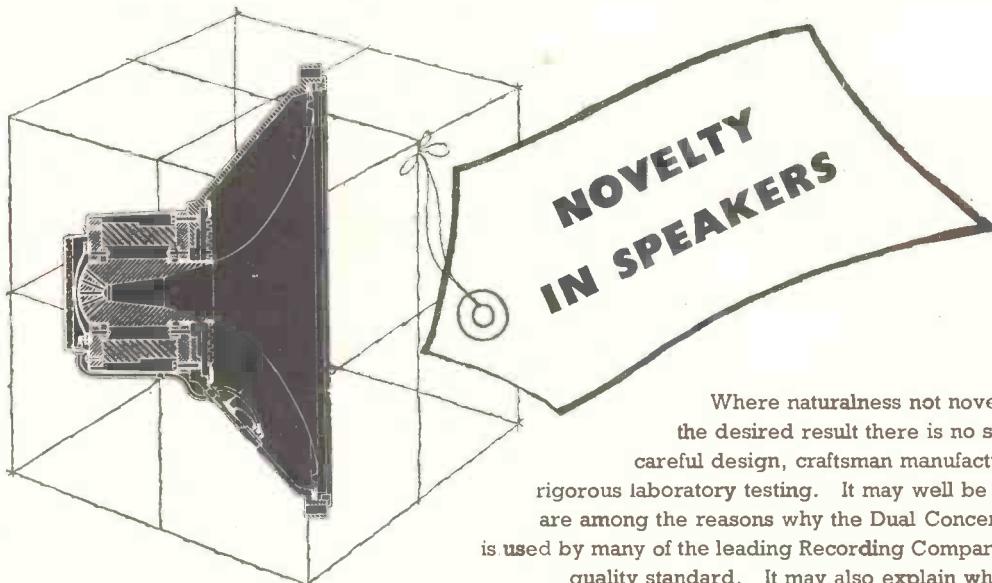
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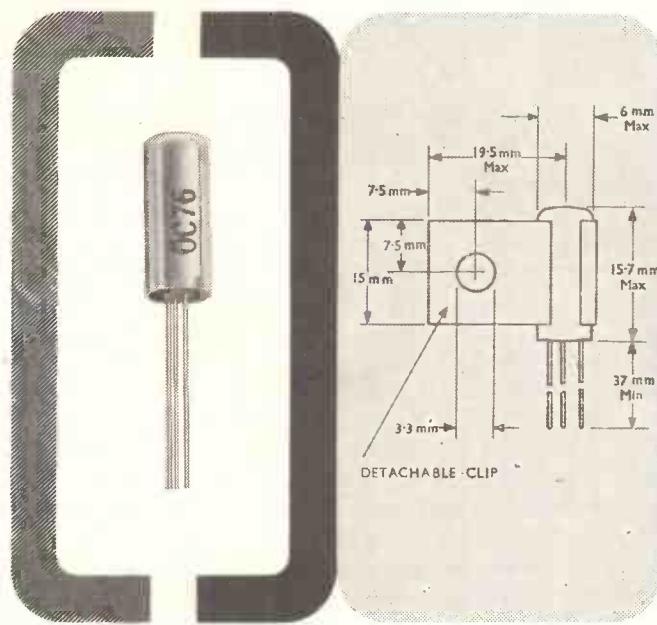
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The pentode type knee of the OC76 characteristic is carefully controlled to give a low and uniform "bottoming" voltage. Its collector will withstand 30 volts d.c. in grounded base. In grounded emitter 30 volts d.c. may also be applied when the total base-to-ground impedance is less than $1\text{k}\Omega$ or the collector current is cut off by a reverse base bias.

Limiting values (absolute ratings)

Max. collector voltage	32V peak	32V d.c.
Max. collector current...	250mA peak	125mA d.c.
Max. junction temp.	75°C continuous operation. 90°C intermittent operation (total duration 200 hours max.)	

Abridged Characteristics

Max. collector leakage current at $V_c = -10\text{V}$	10 μA
Current amplification cut-off frequency	350kc/s
Collector knee voltage at $I_c = 125\text{mA}$	-0.4V
Power dissipation (without heat sink) at 25°C	125mW
Power dissipation (bolted to heat sink) at 45°C	100mW

This transistor is particularly suited for d.c. converters. For example, two OC76's in push-pull can be used to convert low input voltages to high output voltages with a d.c. to d.c. efficiency greater than 75% at power levels up to 700 milliwatts.

As a power oscillator, efficiencies of over 90% are possible with the OC76, while the high peak current of $\frac{1}{2}$ amp can be used to close large relays and operate small motors.

The OC76 is available in quantity. Full data is available from the address below.



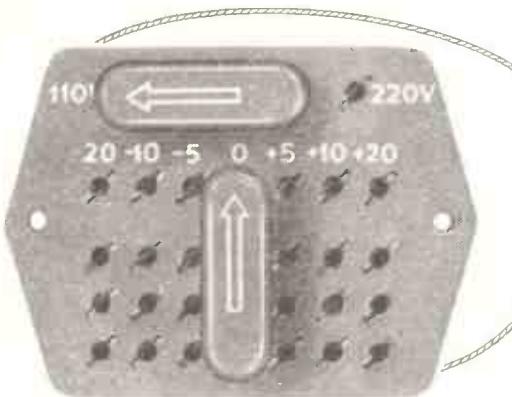
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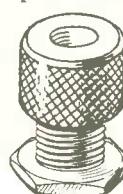
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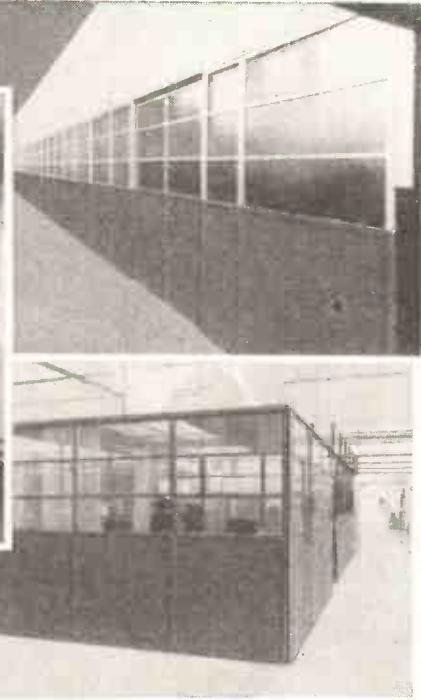
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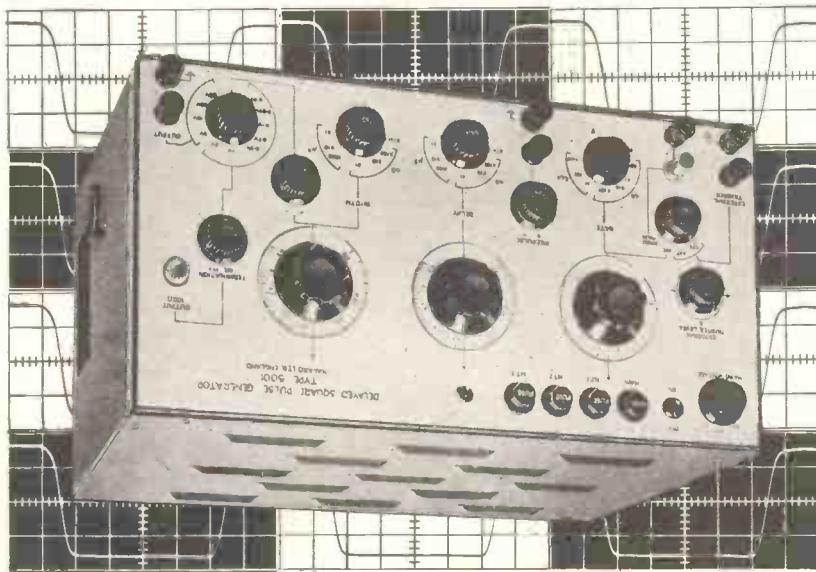
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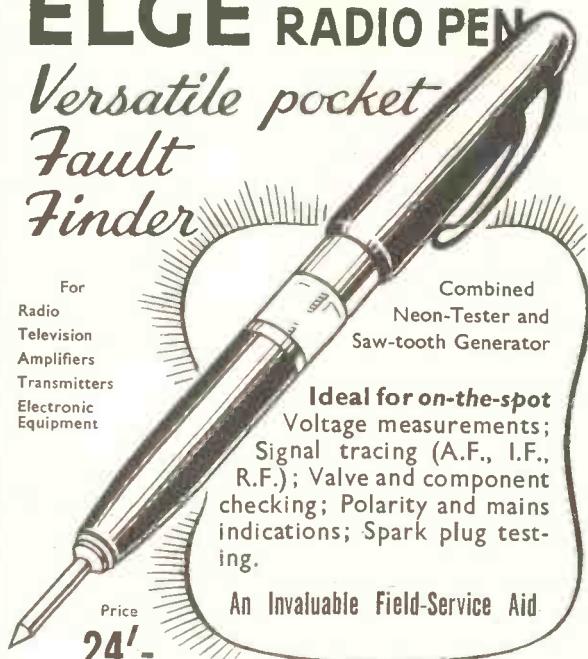
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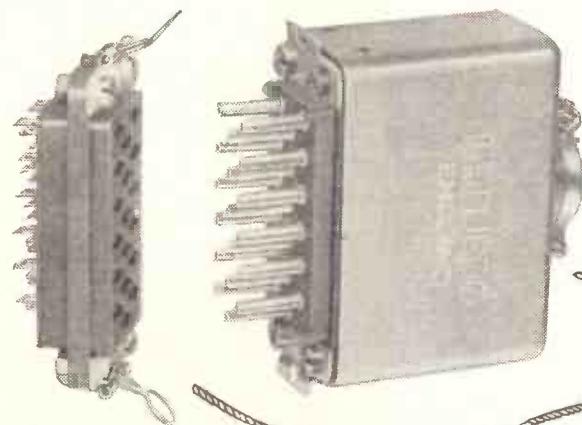


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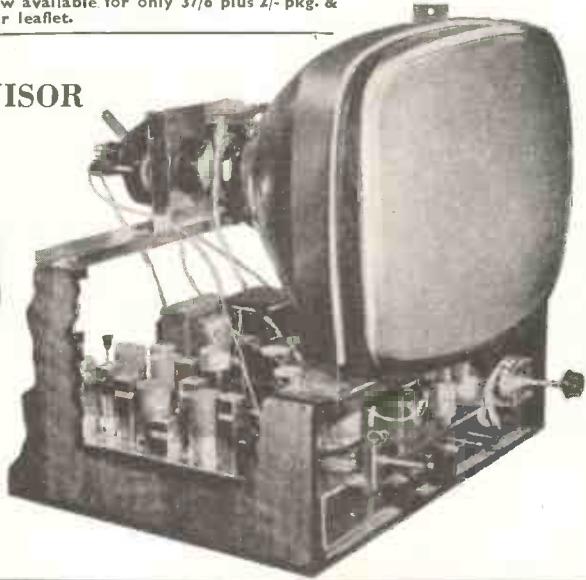
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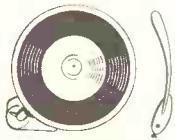
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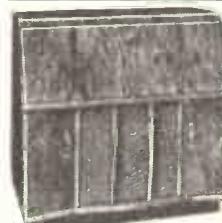
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Dark Piano finished with gold and black styling, overall size 39in. long, 32½in. high, 16in. deep. Two sliding doors, concealing on the left a black panel 18½in. x 20½in. finished in medium mahogany, and on the right a detachable board 12½in. x 18½in. and a shelf which may be used for record storage. Cash Price 18 gns., plus 25/- pkg. and carr. Credit Terms: Deposit £2/18/- and 8 monthly payments £2 6/-.

The new Spencer West Band Three converter is now available at £6/5/- plus pkg. and post 3/-.

Spencer West Pattern Unit 25/- plus 1/- pkg. and post. For elimination of B.B.C. interference or I.T.A.



PREMIER BUREAU DE LUXE

A superb cabinet in finely figured walnut veneer. Interior light sycamore with rexine matching lining. Overall dimensions: 33in. high, 34in. long, 17½in. deep. Uncut control panel on right-hand side approximately 16in. x 10½in., uncut baseboard on left-hand side 15in. long, 13½in. deep. Two full size felt-lined storage cupboards in the lower part of the cabinet. Cash price 16½ gns.

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We carry a comprehensive stock of components by all leading manufacturers.

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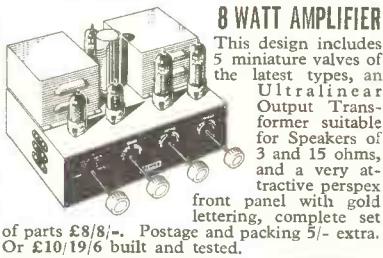


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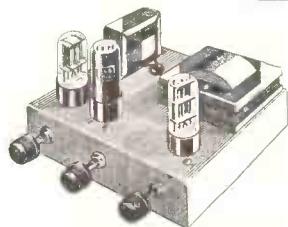
NOW SUPPLIED WITH ULTRALINEAR OUTPUT TRANSFORMER.

All the components for model 510, PLUS pre-amplifier, on one chassis (total six valves), chassis gold hammer finished. May be purchased for £12/12/- plus pkg. and post 7/6. This version complete and tested £15/15/- Or pre-amplifier and tone control in a separate unit £14/14/- plus pkg. and post 7/6.



8 WATT AMPLIFIER

This design includes 5 miniature valves of the latest types, an Ultralinear Output Transformer suitable for Speakers of 3 and 15 ohms, and a very attractive perspex front panel with gold lettering, complete set of parts £8/8/-. Postage and packing 5/- extra. Or £10/19/6 built and tested.



4 WATT AMPLIFIER

MAY BE BUILT FOR £4.10.0 Plus 2/8 Pkg. & Postage

Instruction Book 1/- post free. A steel case is now available, complete with engraved panel, for 15/6 extra. The amplifier may be supplied complete for £5/5/- plus pkg. and post 3/6, or fitted in case at £6 plus pkg. and post 3/6. Engraved panel 3/6. Post free.

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Complete ready to connect to any type of Pick-up and Speaker (9 ohms) A.G. Mains 900/250 v. Volume and tone control fitted with knobs. Overall size 7½in. long x 3½in. wide x 2½in. high.
£2 : 19 : 6

Suitable speaker 7 x 4in. Plus packing and postage 2/10.

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THE LATEST TYPE 17in. RECTANGULAR TUBE AT £17 (INCL. TAX), POST AND PACKING 21/- EXTRA. ALSO 14in. RECTANGULAR TUBE TYPE 14LPA £13/19/6 (INCL. TAX) PACKING AND CARRIAGE 15/- EXTRA.

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plus pkg. & post 3/-

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MAY BE BUILT FOR £7.19.6 Plus 3/- Pkg. & Postage

These two receivers use the latest type circuitry and are fitted into attractive cabinets 12in. x 6½in. x 5½in. in either walnut or ivory bakelite or wood. Individual instruction books 1/- each, post free.

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ALL components to build the complete Receiver, including output stage, may be purchased for £15/5/-, or all components less output stage but including Power Supply, for £13/19/6, plus packing and postage 3/6 on each.

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DECEMBER 1957

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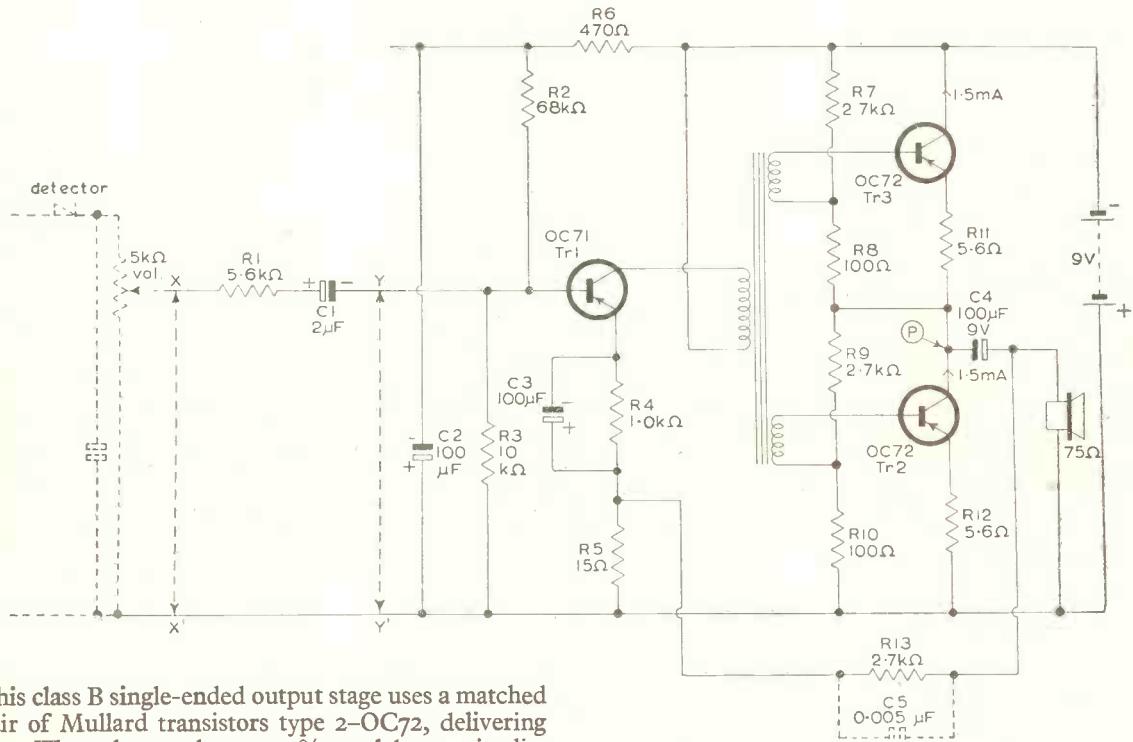
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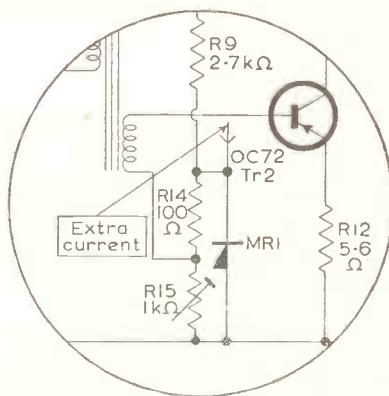
Transistor**Output Stage for Personal Receivers**

This class B single-ended output stage uses a matched pair of Mullard transistors type 2-OC72, delivering 100mW to the speaker at 10% total harmonic distortion. The OC72s, which are used without cooling fins, each have a maximum dissipation of 25mW. The circuit will operate safely and satisfactorily up to an ambient temperature of 45°C. Capacitive coupling to the speaker does away with the need for a centre-tapped supply. The point 'P' is automatically held to half the supply voltage.

A Mullard OC71 is used in the driver stage, with d.c. stabilisation provided by R2-R3-R4. The coupling transformer has a turns ratio of 7 : 1 + 1, with primary resistance <750Ω and secondary resistances <100Ω. The primary inductance is 5H with 1.5mA d.c. flowing.

The input impedance at YY' is about 3.5kΩ, which is partly due to feedback from the speaker via R13. R1 further increases the input impedance at XX' to 8 or 9kΩ. A drive of 180mV r.m.s. across XX' is necessary to provide 100mW output when transistors at the minimum sensitivity limit are used. Undesired feedback from the output stage to earlier stages in the receiver is prevented by R6-C2. The battery drain is about 10mA on speech and music, and 4mA with zero signal. The circuit is therefore suitable for incorporation in pocket-size personal receivers.

A further battery economy is provided by the modification shown in the inset, which allows operation to much lower voltages without excessive crossover distortion by stabilising the base bias voltage. The point at which the battery must be discarded is therefore postponed. With this arrangement a small extra current, taken from some other point in the receiver, is required by MRI.



"Bleep, bleep"

for

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The immense developments of this present age are something to stir the imagination. The satellite of our picture is not so far ahead and more momentous things will follow in its train.

Wherever research and practical experiment are called for, Brimar valves are in the forefront—maintaining their high reputation for performance and reliability.

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FOOTSCRAY, SIDCUP KENT. Footscray 3333



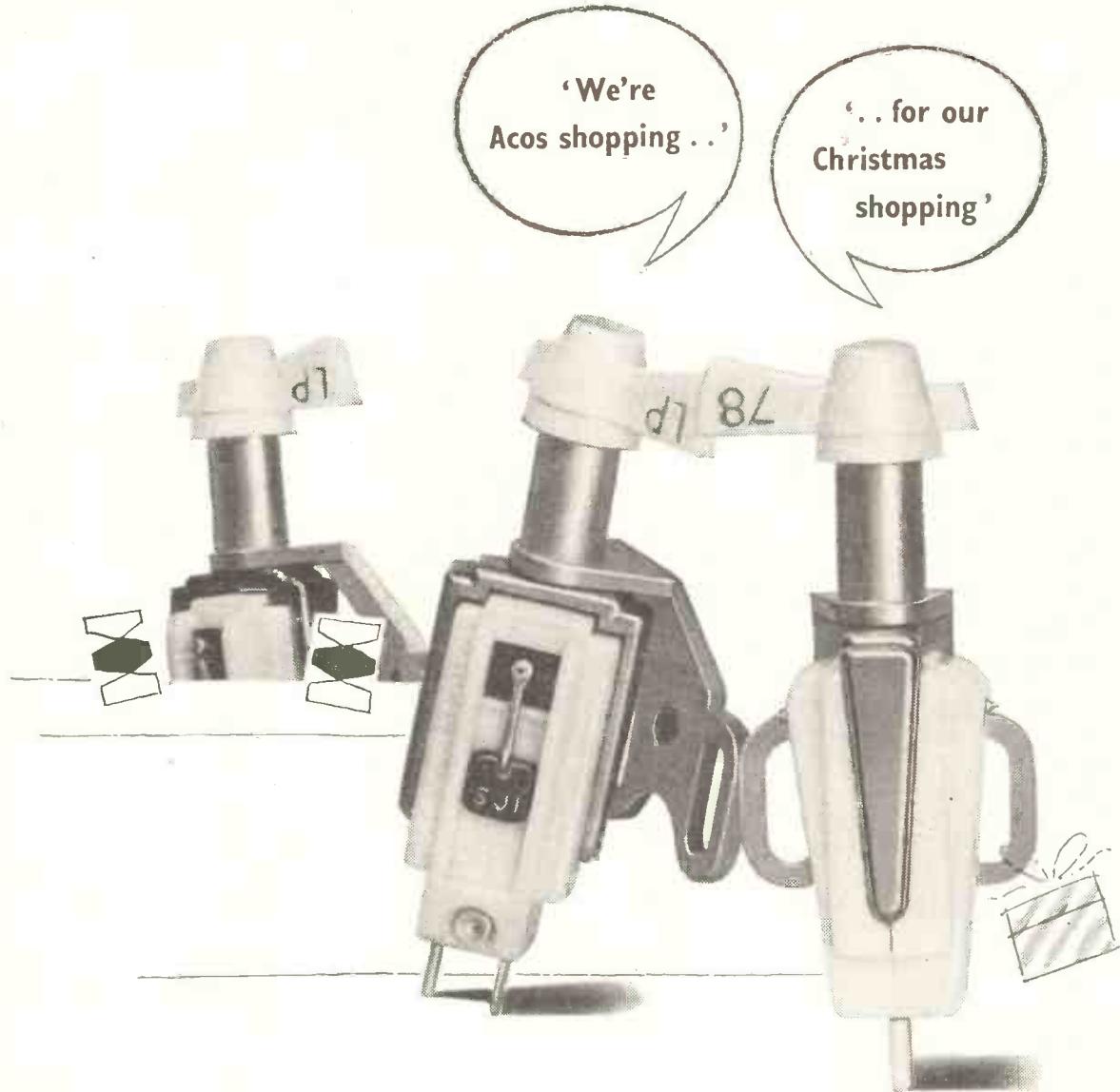
**who, as always
got there
first!**

Reproduction of
an advertisement
by BRIMAR in
December, 1955



Standard Telephones and Cables Limited

Regd. Office : Connaught House, Aldwych, London, W.C.2)
FOOTSCRAY, KENT FOotscray 3333



You, too, will want to select Christmas presents for friends and relations or even **YOURSELF**.

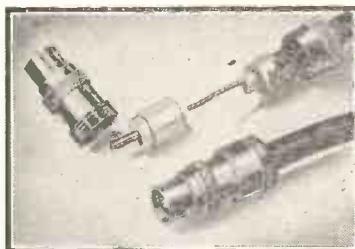
Your choice must be Acos.

Records grow festive and long-living on Acos x500 styli; you can't do a better turn to a turntable than, say, the magnificent new Black Shadow pick-up, or the appropriate GP65 series cartridge; tape recorders luxuriate on Acos microphones. Pleasing, handsome gifts, at a reasonable price, for a hi-hilarity Christmas.

acos

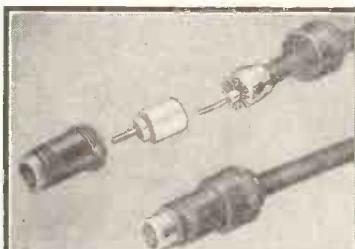
FOR CHRISTMAS GIFTS IN STYLI

"BELLING-LEE" CO-AXIAL PLUGS AND SOCKETS

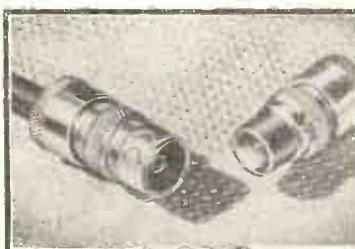
**L.734/P/A1. FREE PLUG**

Coaxial and semi-air-spaced feeders can be accommodated by these plugs. Their complementary sockets are L.734/S and L.604/S (fixed), and L.734/J/AL (free). Cable loading: Coaxial feeders: solid to $\frac{1}{8}$ in. diaelectric. Semi-air-spaced: outside diameter $\frac{1}{8}$ in.

Finish: Nickel-plated or polished aluminium.

**L.781/P2. INSULATED FREE PLUG**

The insulation of the body and the cap is nylon and therefore very robust. Cable loading: Coaxial, up to $\frac{1}{8}$ in. dia. Colour range: Black.

**L.734/J/A1. FREE SOCKET**

This component is extremely useful for extending coaxial cable runs in workshops and demonstration rooms, etc. Any number of cable lengths may be used. Finish: polished aluminium.

"BELLING-LEE" NOTES

ISLE OF WIGHT I.T.V.

We wonder if the majority of those in the area to be served by Chillerton Down realise how fortunate they are compared to those who live in the area served by St. Hilary. The base of the 700 foot mast stands about 550 feet a.s.l. giving an aerial height of 1,250 feet, looking straight across the Solent and Southampton water. The land slopes from over 730 feet south of Swindon to the sea. We have heard that some people are erecting I.T.V. aerials now, and orientating on the B.B.C. signal. In most cases this will be satisfactory owing to the favourable nature of the ground. In difficult locations we would not recommend the erection of band III aerials unless a band III signal of some kind is available, but under fairly open conditions such as prevail over most parts of the area to be served by Chillerton Down, we would prefer to orientate an aerial on a compass bearing.

We know there will be lots of locations tucked away below the brow of the downs, and on the banks of the Wey river and the Avon for example, where band III reception may be very difficult, but in general a very large number of people will get first class viewing from the new I.T.A. transmitter on the Isle of Wight. We anticipate that many people in coastal towns living in hotels or flats

will make very good use of the "Golden V," the indoor aerial with outstanding style. This is a broadband aerial but it is more efficient on band III than on band I.

Normally we would not recommend an indoor aerial of any kind in, shall we say Bournemouth, 25 miles from the transmitter, but when most of this distance is across water, it is well worth while trying, and we feel sure a lot of well designed indoor aerials will be sold and used.

ADDING ON AERIALS

When we recommend that a certain band III or F.M. aerial may be attached to an existing band I array, we know that there is sufficient strength in the band I aerial to take the added weight and windage. Do not thoughtlessly add on where there is danger of the band I aerial breaking under the additional strain. Some makes of aerials are not as strong as others. A one inch mast may be steel, or light alloy, and you may not know the gauge of material, i.e. the thickness of its walls. We have seen some ridiculous erections that bring nothing but discredit to our industry, and regulations from council authorities. Before adding a band III or F.M. array, check up on lashings and brackets and if they are in bad condition, change them.

STORM AND TEMPEST

While the winter months are generally considered the most trying for outside fittings such as television aerials, summer can bring unexpected gales of short duration. One such period occurred this year during July, where, in one district of South East England, thousands of television aerials were rendered useless overnight. In hundreds of cases secondary damage by way of broken tiles, etc., cost much more than the aerial which had to be replaced. On this occasion, as in every other similar one, the percentage of "Belling-Lee" aerials affected was negligible. Every time that sort of thing happens more dealers realise that it does pay to fit "Belling-Lee" in the first instance. We mean it when we say that "Belling-Lee" aerials go straight up and stay up straight.



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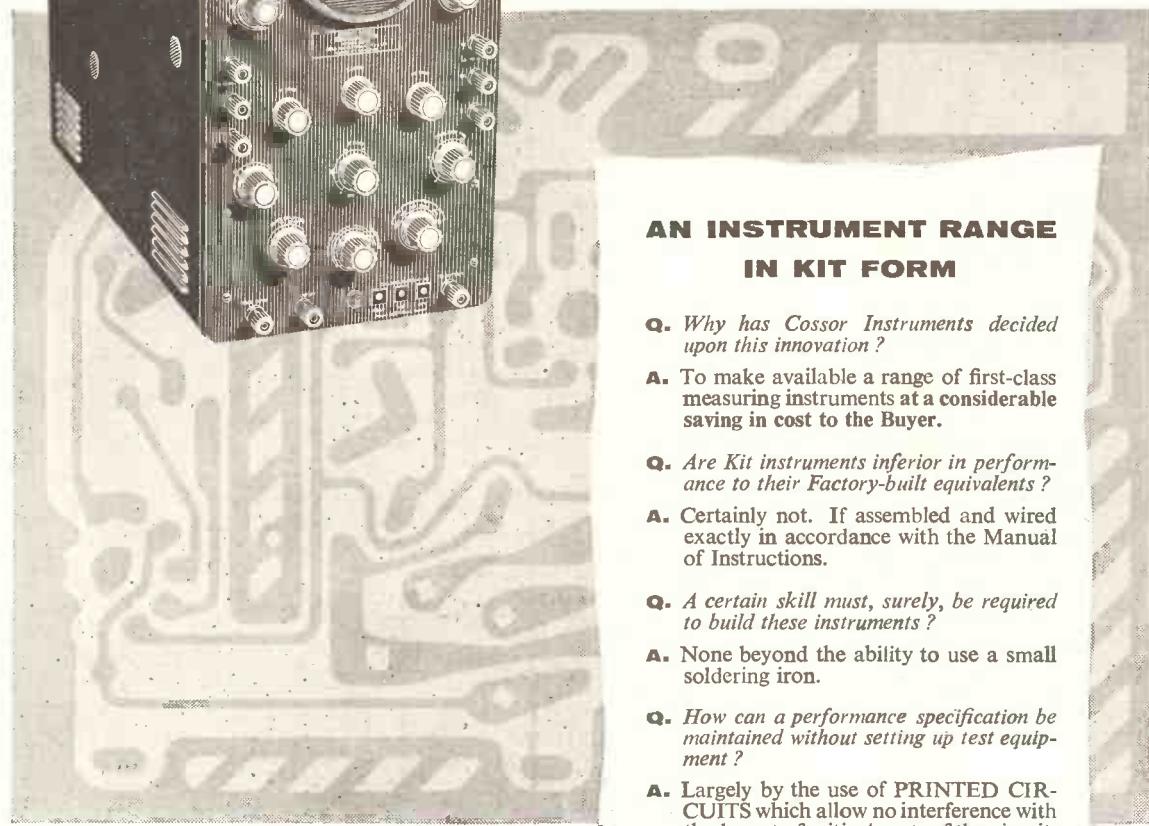
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- Q.** *Could I have more information on these interesting instruments?*
- A.** With the greatest of pleasure. Just write to:

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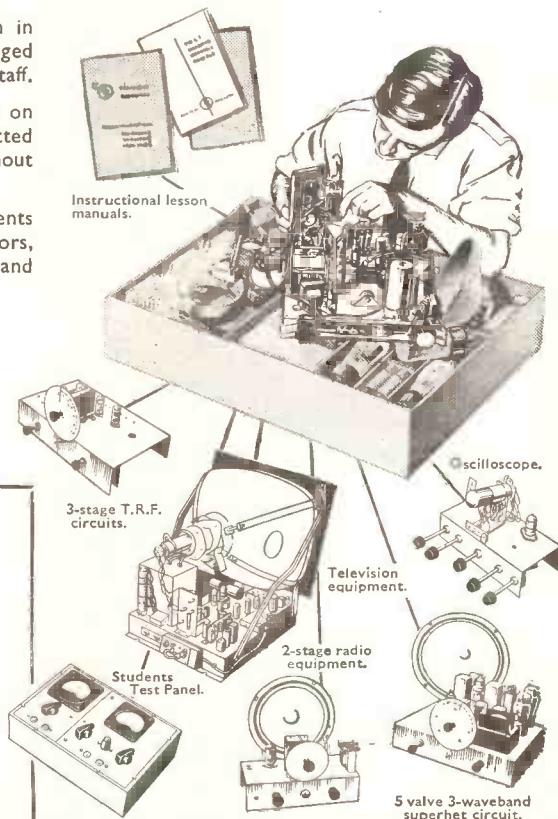
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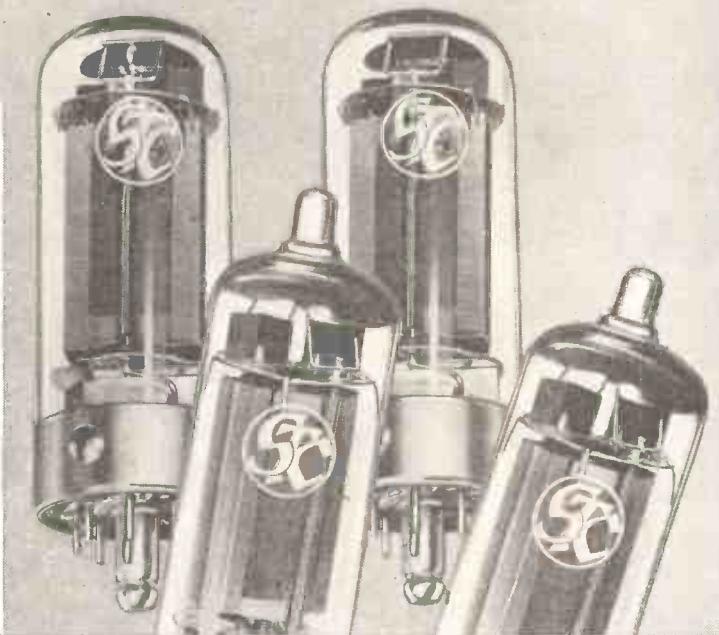
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IC107

Electrical equivalents

FOR THE

807



plus these EXTRA advantages



SMALL SIZE

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The range of four valves offers
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These new STC valves are loctal-based, indirectly-heated, beam-power amplifiers electrically similar to the U.S.A. type 807 but with extra advantages. Little more than half the size of the 807 the electrode assemblies are more compact... stronger and more rigid... and the glass bulbs less vulnerable. Shorter grid and anode leads, and glass base with miniature-type pins reduce inter-electrode capacitance and improve performance at the higher frequencies. Thus, both mechanically and electrically, they offer a new high standard of reliability, which, together with their small size, makes them particularly suitable for use in mobile equipment.

5B/254M double-ended	5B/255M single-ended	5B/257M single-ended	5B/258M double-ended
6.3V	6.3V	12V	19V
0.9A	0.9A	0.47A	0.33A

Where the overall seated height must be kept as low as possible, the single-ended type 5B/255M may be used under conditions other than those of high altitude or anode modulation. The 5B/254M is available under the code 5B/254G, as a flying lead version.



Standard Telephones and Cables Limited

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63 ALDWYCH

LONDON W.C.2

MARCONI TELEVISION RECORDING EQUIPMENT

TYPE BD679 RECORDING CHANNEL

16mm Film presents a most economical and flexible means of recording Television pictures since film costs are low, developing and printing techniques are advanced and a wide range of fine grain film stocks are readily available. Projection, editing, viewing, dubbing and handling are all easily carried out with standard equipment. The Fast Pull-down technique presents great advantages over other systems of recording on film but the mechanical difficulties of moving the film in the short period of frame blanking have hitherto prevented the employment of the technique. These problems have now been successfully overcome by Marconi's.



Features

Exceptionally high picture quality.

Specially developed gearbox enables Fast Pull-down technique to be employed. F.P.D. Mechanism has given over 3,000 hours trouble-free operation.

Pull-down time adjustable, normally set at 2 milliseconds permitting recording of fully interlaced picture. Simple single-lens optical system avoids loss of contrast.

Sound can be recorded on optical track,

magnetic stripe or separate synchronous magnetic track.

Conveniently placed input selector switches, monitor and level controls. Sound/Vision cueing device incorporated.

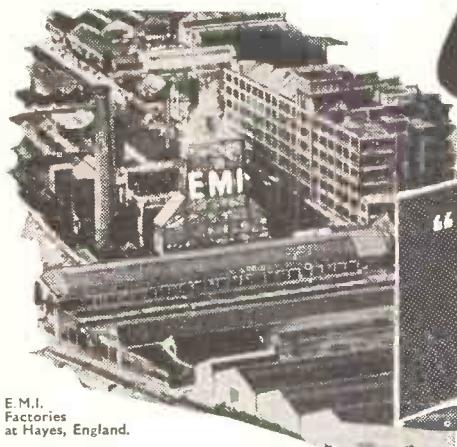
Recording can be made on positive or negative stock of a wide variety, either direct positive, direct negative or reversal. Magazines hold 2,400 ft. (2,000 ft. magnetic stripe) or film may be fed directly into a rapid processor.

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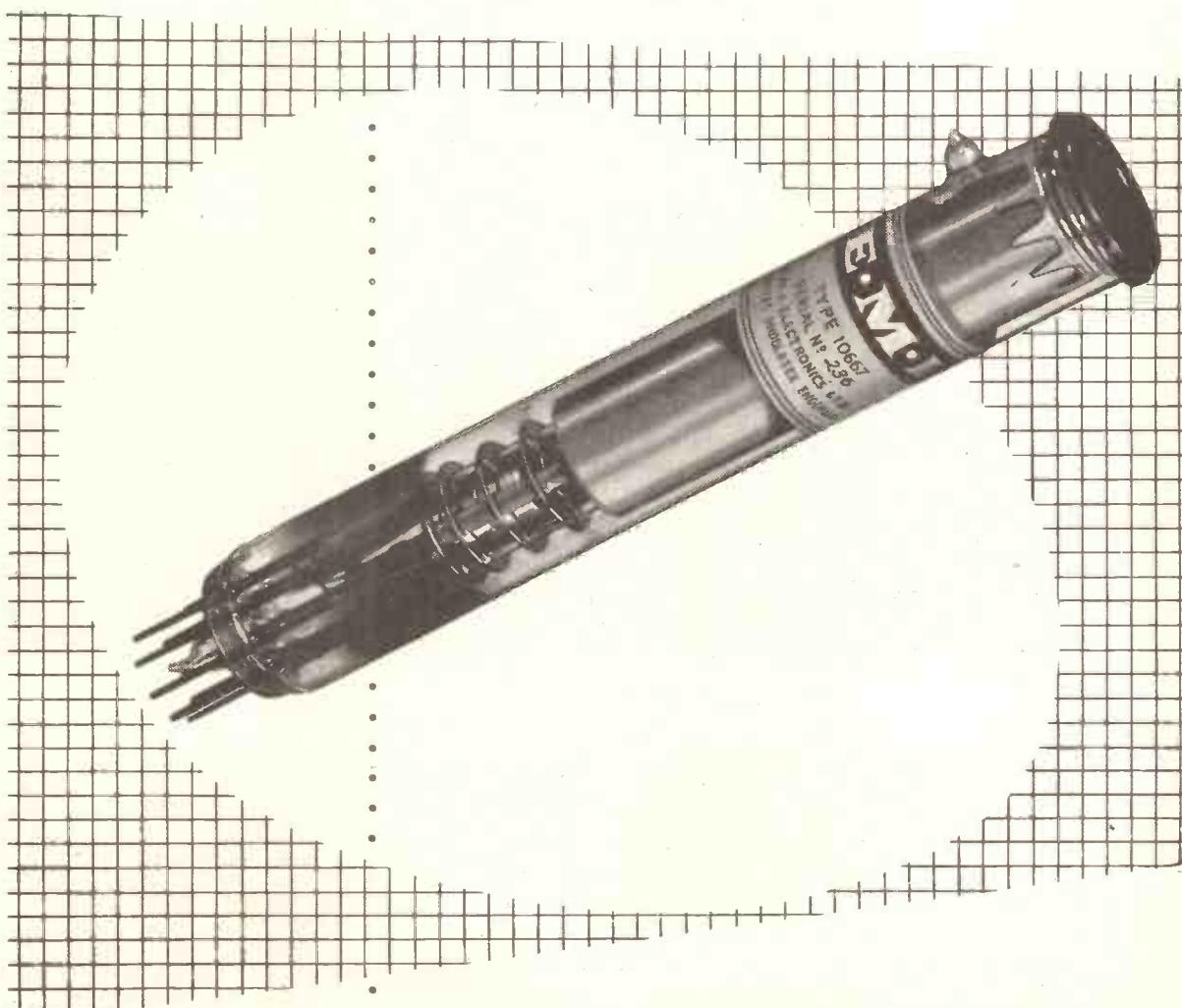
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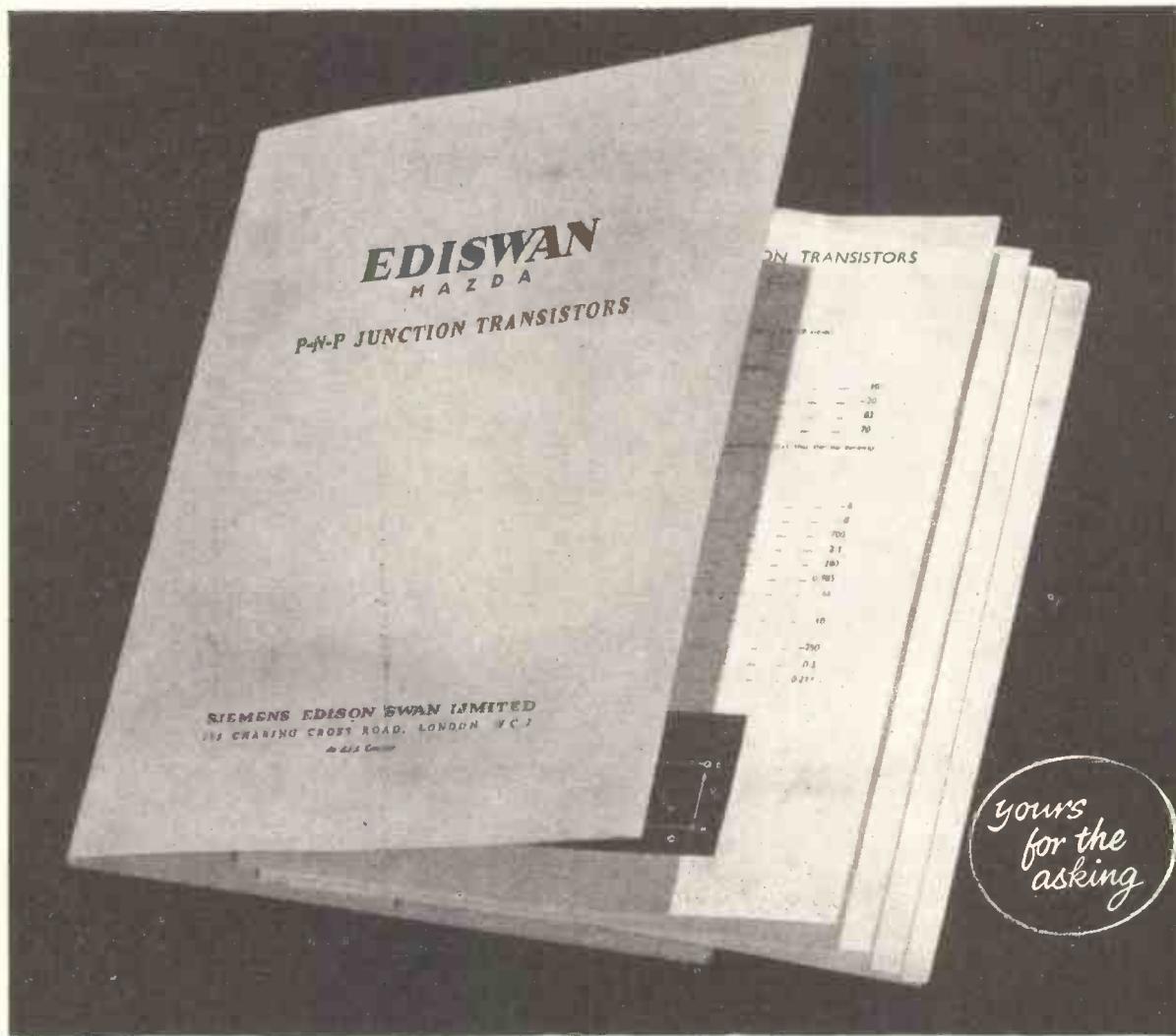
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If you are manufacturing or designing electronic equipment you will find this folio of data sheets helpful as a source of reference. It gives you comprehensive information and characteristic curves covering the whole range of EDISWAN Mazda transistors.

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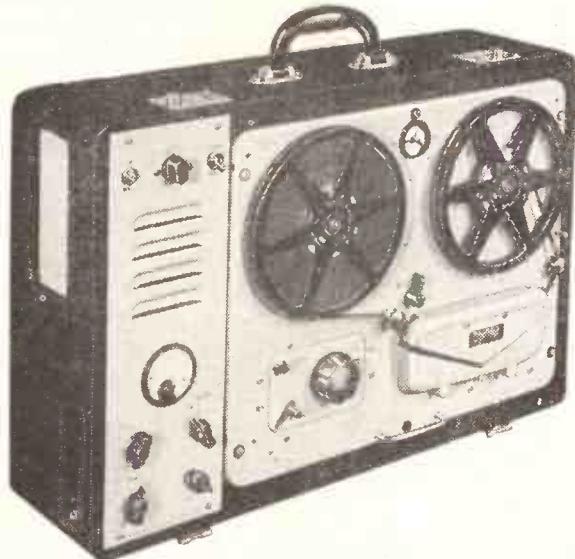
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TELEPHONE: GERRARD 8660. AN A.E.I. COMPANY

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CRC 15/4

Vortexion



The above recorder uses a synchronous capstan motor and for use on 12 volt car battery a 50 c/s \pm 1 cycle 230 v., 120 w. power supply unit is available as detailed below.

T.R.G.10 MINIATURE AMPLIFIER AND VERSATILE

PRE-AMPLIFIER. A modern miniature amplifier, measuring only $4\frac{1}{2} \times 5$ in. over front panel and projecting $10\frac{1}{2}$ in. to the rear. Uses C core transformer material to obtain low external magnetic field and has less than 0.1% harmonic distortion at 10 watts output. The amplifier response is level 15 c/s. to 50,000 c/s. within 0.2 db. The 3-valve pre-amplifier will operate direct from recorder heads with correction networks for different tape speeds and switched inputs are provided for radio, microphone and gram. with correction for all recording characteristics.

"SUPER FIFTY WATT" AMPLIFIER. This heavy duty amplifier is available for long life under arduous conditions. The normal life being 5,000 hours without valve change.

POWER SUPPLY UNIT for operation with Tape Recorder or similar equipment on 12V. car battery.

This D.C. to A.C. supply unit has been specially manufactured to provide 1% accurate 50 cycle A.C. power for 50 c/s synchronous motors and amplifiers sensitive to mains noise. The output from the 50 cycle is well filtered to reduce harmonics and give approximately the same degree of quietness as normal 50 cycle mains. The efficiency is over 80% at wattages over 50. Terminals for a remote control switch are fitted to prevent carrying the heavy low voltage L.T. cables any distance from the battery. The unit can then be fitted at the point closest to the battery to prevent voltage drop on leads and the A.C. satisfactorily extended to any required position.

The unit is fitted in an 18 gauge steel case to give screening, but it should not be placed close to tape heads in case the field causes slight hum.

The case measures 9in. x 6in. x 9in.

Full details and prices of the above on request

VORTEXION LIMITED, 257-263, The Broadway, Wimbledon, London, S.W.19

Telephones: LIBerty 2814 and 6242-3

TAPE RECORDERS and AMPLIFIERS

★ The total hum and noise at $7\frac{1}{2}$ inches per second 50-12,000 c.p.s. unweighted is better than 50 db.

★ The meter fitted for reading signal level will also read bias voltage to enable a level response to be obtained under all circumstances. A control is provided for bias adjustment to compensate low mains or ageing valves.

★ A lower bias lifts the treble response and increases distortion. A high bias attenuates the treble and reduces distortion. The normal setting is inscribed for each instrument.

★ The distortion of the recording amplifier under recording conditions is too low to be accurately measured and is negligible.

★ A heavy mu-metal shielded microphone transformer, is built in for 15-30 ohms balanced and screened line, and requires only 7 micro-volts approximately to fully load. This is equivalent to 20ft. from a ribbon microphone and the cable may be extended 440 yds. without appreciable loss.

★ The 0.5 megohm input is fully loaded by 18 millivolts and is suitable for crystal P.U.s, microphone or radio inputs.

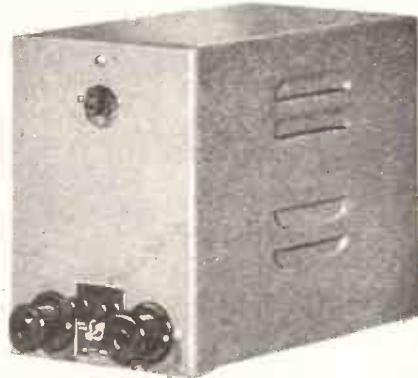
★ A power plug is provided for a radio feeder unit, etc. Variable bass and treble controls are fitted for control of the play back signal.

★ The power output is 4 watts heavily damped by negative feedback and an oval internal speaker is built in for monitoring purposes.

★ The play back amplifier may be used as a microphone or gramophone amplifier separately or whilst recording is being made.

★ The unit may be left running on record or play back, even with 1,750ft. reels, with the lid closed.

CP20A AMPLIFIER. This standard amplifier for extreme tropical use will operate from 230 v. A.C. mains or 12 v. car battery and give 15 w. output for a consumption of 5.5a. Inputs for 30Ω balanced microphones, M.I. P.U. and Cr. P.U.



Telegrams: "Vortexion, Wimble, London."

Choose 

Ful-Fi



the turnover crystal cartridge with ALL the features!

When you buy components to put into your product there is only one sound rule to apply—buy the best. Otherwise you risk the reputation of your firm.

Already the Ful-Fi has established itself throughout the world as a reliable and efficient cartridge with an excellent performance.

Of the two models available the TC8M is a high fidelity version with a response which is flat within ± 3 db. up to 12,000 c.p.s. and yet has an output at 1,000 c.p.s. at 1.2 cm/sec. at .3 volts. The TC8H type gives most pleasant listening with low gain amplifiers. It has a flat output up to 7,000 c.p.s. and gives an output at 1,000 c.p.s. at 1.2 cm/sec. of .9 volts. Both cartridges are very easily fitted and depending upon the tone-arm construction the stylus pressure may be adjusted between 6 and 12 grams.

A powerful advantage of the Ful-Fi is the ease with which it may be removed from the pick-up arm for examination or cleaning.



Whether you are contemplating a "one-off job" or the laying down of a track for commercial production you are well advised to find out about the Ful-Fi. Send for full technical literature and the report of an unbiased test conducted in Australia (if you have not received a copy).

★ **The Ful-Fi cartridge is fitted to the Monarch—the world's finest autochanger.**



BIRMINGHAM SOUND REPRODUCERS LTD., OLD HILL, STAFFS.

Britain's best Hi-Fi Equipment

We have devoted over 22 years entirely to the design and manufacture of audio equipment and we are proud of our position as leaders in this field. We were the first firm in the world to design and market Amplifiers having a total distortion content as low as 0.1%; a claim which was received with incredulity in 1945, but which was subsequently confirmed by the National Physical Laboratory and has become an accepted world-wide standard.

High engineering ideals have guided our efforts, and Leak Amplifiers have been the choice of the B.B.C., Commonwealth and foreign broadcasting authorities and Recording Studios. This acceptance by professional audio engineers has led to a demand for Leak equipment from music lovers throughout the world.

On the important question of prices it is appropriate to mention one of the basic principles of Leak design. From long experience and by extreme attention to design details during development work on the pre-production models, we enable our craftsmen to achieve a high output per man-hour. The labour costs thus saved offset the increased cost incurred for high-grade materials, components and finishes, and this, together with quantity production (made possible only by a world-wide market), explains how quality products may be sold at reasonable prices.

An important Test Report . . .

Independent laboratory tests of the Garrard 301 transcription turntable were recently carried out by Audio Instrument Company Inc., New York, U.S.A., under the direction of Mr. C. J. Lebel (Chairman of one of the groups which prepared the NARTB Standards). It was necessary that the pick-up and amplifier system should conform in response to the RIAA-New AES-new NARTB response curve within ± 1 db, and in the tests of this excellent transcription unit the components selected for use as complying with this requirement were a Leak tone arm fitted with Leak cartridge and a complete Leak pre-amplifier and power amplifier Model TL/10.

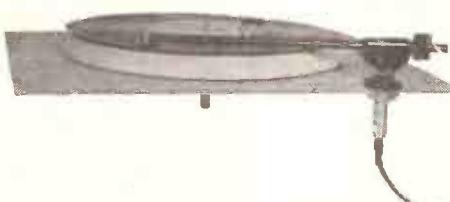
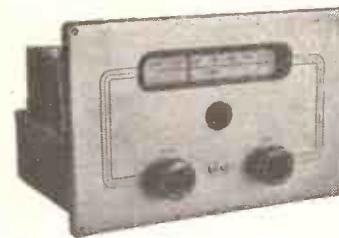
The full test report appeared in the February, 1957 issue of "Wireless World," pages 22 and 23.

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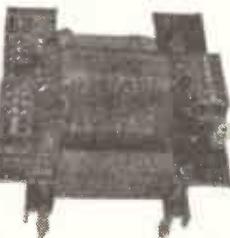
MAINS ISOLATION TRANSFORMER



Makes servicing safe, also makes

the adjustment for differences in mains voltages very simple. Input tapped 200-250v., output tapped 200-250v. Continuously rated at 500 watts, intermittent rating 2000 watts. Cable entry by terminal blocks, two separate screens for suppressing mains interference. Size approximately 14" x 6" x 6", weight approximately 40lbs. Price £5/12/6. Carriage and insurance 7/8 (up to 250 miles).

500 WATT STEP DOWN TRANSFORMER



With output tapped from 110v.-155v. in 3 volt steps, massive transformer which will withstand considerable overloading. Price 45/- plus 5/- carriage (up to 250 miles).

DON'T BE CAUGHT LIKE THIS



CAR STARTER CHARGER KIT

All parts to build 6- and 12-volt charger which can be connected to a "flat" battery and will enable the car to be started instantly. Kit comprising the following.

Mains transformer	22/6.
6-amp. rectifier	17/6.
Regulator Stud Switch	3/6.
Resistance Wire	2/-
Resistance Former	2/6.
Main on/off Switch	2/6.
0-5 amp. Moving Coil Meter	12/6.
Construction Data	1/6.
plus if bought all together price is	52/6
plus 3/6 post and packing.	

MAKING A SOLDER GUN

A 7-second solder gun of the type costing £2/6 was described in Pract. Mech. Only two essential parts are required—(a) transformer and (b) push switch. These we can supply at 13/6, plus 2/- post. The rest of the parts you will have in your own "junk" box. Copy of the article concerned given free with the kit.

VACUUM PUMP



Rotary vane type. Spine drive shaft—threaded inlet and outlet, also makes good compressor. Price 22/6, plus 2/6 post and packing.



MULLARD AMPLIFIER

A Quality Amplifier designed by Mullard. Power output exceeds 10 watts. Frequency response almost flat from 10 to 20,000 C.P.S. For use with the Acos "Hi G" and other good pick-ups. Made up and ready to work is £12/10/- or £1/10/- down and 8 payments of £1/10/- plus 10/- carriage and insurance.

MULLARD PRE-AMP. We are pleased to offer as a ready-made unit. It uses the low hum/noise high gain pentode type EF86. It takes its power supply from the amplifier and incorporates 2 switches to provide immediate compensation, for radio microphone, L.P. and 78 records. The price of this unit is £4 post and insurance 3/6 extra.

Or 10/- down and 9 payments of 10/- if purchased with above, combined price is £18 or 30/- down and 8 payment of £2.



LAST FEW

HIGH FIDELITY AMPLIFIER



3 valve 4 watt with frequency response better than 40-15,000 C.P.S. Control panel size 8in. x 2½in. comes fixed to chassis but is intended for independent mounting. Separate bass and treble controls giving fullest variation of cut and lift. Separate switch, absolutely no mains hum. Remarkable value at £4/19/6.

CABINETS FOR ALL

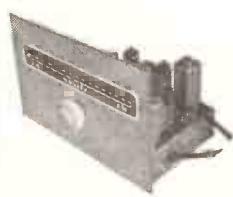


The CONTINA

Another addition to our range of cabinets. This is of new revolutionary design, styled after the best of Continental radios. Externally, it is finished in highly polished dark walnut veneer, with paneling picked out in gold. Interior is of some very high standard, its veneer being light mahogany which contrasts nicely with the dark walnut and generally gives a very pleasing appearance. The doors slide on metal runners and are fitted with gold inset finger plates. A really excellent cabinet for any home-size 9ft. 1½in. long, 1ft. 3in. deep, 2ft. 1½in. high, including legs which are 10in. from floor. Motor board 19¾in. x 17in., equipment aperture 17½ x 9½in., gives ample space for 8in. speaker. Ample storage space for recordings. Price £19/19/- carriage and insurance, 20/-.

F.M. TUNER

This is a high fidelity unit which although moderately priced has a performance equal to the highest priced. Its stability is very good and extremely good results have been received with the simplest of aerials as far away as Eastbourne. The unit is made up ready to work and has its own power supply for A.C. mains. Demonstration at all our branches. Price 12/- p.m.s. or £1/12/- down and 8 payments of £2. Post plus insurance 5/-



THE "CRISPAN" BATTERY PORTABLE

A 4-valve truly portable battery set with very many good features as follows:—

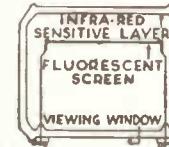
- Ferrite Rod Aerial.
- Low consumption valves (DK96 range).
- Sparket circuit with A.V.C.
- Ready built and aligned chassis if required.
- Beautiful two-tone cabinet.
- Guaranteed results on long and medium waves anywhere.

All parts, including speaker and cabinet, are available separately or if all ordered together the price is £7/15/- complete, £1/15/- deposit and seven monthly payments of £1. Post and insurance 3/6. Ready built chassis 30/- extra. Instruction booklet free with parts or available separately 1/6.



THERMAL DELAY VACUUM RELAY

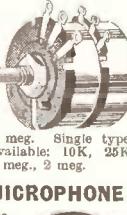
This can be the basis of a process timer—plastic sealer controller. Sequence switching—infra red indicator—overload protection. Our booklet free with the relay or separately 1/6, gives suggested circuits. Hermetically sealed with 4-pin base, heater resistance approx. 1,500 ohms. This can be used for overload protection. Approximately 17 milliamperes through the heater coil will cause the contacts to close. Limited quantity—8/6 each, post and insurance 1/6.



"Cats eye" used for seeing in the dark. Will work burglar alarms, counting circuits, smoke detectors and the hundred and one other devices as will the simpler type of photo cell. Price 5/- each. Post and ins. 1/-. Data will be supplied with cells if required.

MORGANITE POTENTIOMETERS

Single and 2 gang types available, standard size with good length spindle, and new and boxed. Gang type 3/4 each—values available: 5K, 5K, 10K, 10K, 1 meg. + 1 meg. Single types 5K, 10K, 25K, 50K, 100K, 250K 1 meg., 2 meg.



CRYSTAL MICROPHONE

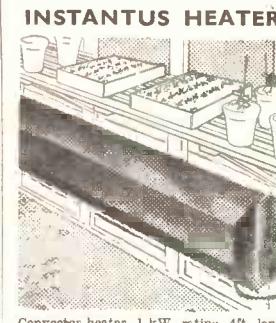
Miniature crystal type has high gain and is suitable for all purposes—tape recorders—amplifiers. Price 4/9 post and ins. 9d.



TRANSISTORS

A good range of transistor parts, miniature transformers, electrolytics, etc., available at all branches.

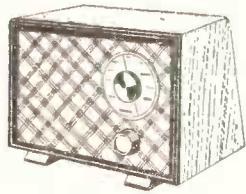
Red Spot and audio .. 10/- Blue Spot 1.6 Mc.s. .. 15/- White Spot 2.5 Mc.s. .. 20/-



Convector heater, 1 k.w. rating, 4 ft. long, made from heavy gauge sheet steel (galvanised). Can be used for greenhouse, workshop, aviary, etc., etc. Price £2/10/- or with thermostat, £2/5/- carriage 5/- GUARANTEED 5 YEARS.

2 KW MODEL. Free standing, thermostatically controlled, £5/17/6.

OUR 19/6 COLUMN



THE SKYSEARCHER

This is a 2-valve plus-metal receiver set useful as an educational set for beginners, also makes a fine second set for the bedroom, workshop etc. All parts, less cabinet, chassis and speaker, 19/6. Post and ins. 2/6. Data free with parts or available separately 1/6. 3-valve battery version also available at the same price.

ALL-MAINS AMPLIFIER



Powerful three-valve. Mains amplifier ideal for dances, parties, etc. Complete less chassis, cabinet and speaker (available if required)—data 1/6 (free with parts). Price 19/6, plus 2/6 post and insurance.

CHIME LITE 19/6

It is a hall light, as well as a double chime and you can make it in a couple of evenings for the total cost of only 19/6 including instructions, post 2/-—data available separately price 2/-.

Simplex Transistor Kit

Makes ideal bedroom radio, uses one transistor and one crystal diode. Complete less case 19/6, case 5/- extra, post and ins. 1/6.

A.C./D.C. Multimeter Kit

Measures A.C./D.C. volts and ohms. All the essential parts including metal case, 2in. moving coil meter, selected resistors, probe for shunts, range selector, switches, calibrated scale and full instructions, price 19/6 plus 1/6 post and insurance.

BAND III CONVERTER

Suitable London, Midlands, North, Scotland etc. All the parts including 2 valves, coils, fine tuner, contrast control, condensers and resistors. (Metal case available as an extra.) Price 19/6 plus 2/6 post and insurance. Data free with parts or available separately 1/6.

Build this in ONE evening



Undoubtedly the most up-to-date television for the home constructor. You can build it in an evening and the set when finished will be equal to a factory made equivalent. What other constructor T.V. has all these features?

- No technical knowledge required
- All miniature valves
- Metal rectifier
- Turret tuner
- 12-channel circuitry
- Multivibrator time bases
- Ferrite cube, E.H.T. and scan coils
- 34/38 mc/s. I.F.
- Suitable for any modern 12, 14 or 17in. tube

The building cost (less tube) is only £29/10/- plus 10/- carriage and insurance. All parts guaranteed twelve months. Full information and data free with parts or available separately, price 3/6.

THIS MONTH'S SNIP

TAPE DECK—Made by the famous Truvox Company. This contains exactly the same essentials as the current model. Only the styling is different. It also takes the stereophonic head.

SPECIFICATION: 3 B.T.H. shaded pole motors with silent friction drive eliminate noise and vibration. Push button controls—electrically and mechanically interlocked. Patented electric type push-button control and brake. Tape loading, on the drop-in principle, accommodation for reels of 7" diameter. Tracking sense to British and American standards. Playing timer, up to 3 hours with L.P. Tape or 2 hours with Standard Tapes. Two tracks side by side with safety gap. Positive Azimuth adjustment of Record/Player head. High Impedance Heads. Overall size 14" x 12" x 5" approx. £20 only of these fine decks offered at non-repeatable price of £17/10/- or £23/10/- down and eight monthly payments of £2. Non-callers add 10/- carriage and insurance.

DON'T STUMBLE IN THE DARK



Install 2-way switches. Our outfit comprises 30 yards. Multi-core cable, two 2-way switches, two wood blocks. Full instructions. 19/6 each (post and insured 2/6).

12in. T.V. CABINET — 15/-

We are offering these at not much more than the cost of the plywood they contain. If not wanted for TV, many useful items can be made—record storage cabinet, H.F. loudspeaker case, bookcase, etc., etc. Price 15/- Carriage 3/6.



Clock numerals to suit these cases etched on metal, 2/6.
Post 9d. if ordered separately.

CLOCK CASE

Also suitable for barometer or other instrument. Nicely polished. Price 4/6, post and packing 1/6.



Wrap our heated cable around the pipes in your loft to prevent a freeze-up. 21 yards £1/1/- post free

THIS MONTH'S SPECIAL BARGAINS

E.S. HOLDER, panel mounting, bakelite, insulated, 2/-.



FILAMENT TRANSFORMER 200-240 v. tapped mains input: 6.3, 3 amp. output. Ex. equipment but unused, 6/6 each.

THERMAL DELAY UNIT 6.3 v. operated, switches on or off, 3/6.

YAXLEY SWITCH, 1 position, 6 pole, 3 bank, 2/6.

500 K.C. CRYSTAL (10X E/500) Plug-in type 6/6. 5-0-5 CENTRE zero milliammeter 2½in., 12/6.

BALANCE METER 10D/13762, will function as highly sensitive relay, 45/- each.

12in. HIGH FLUX (12,000 lines) SPEAKER, 3 ohm speech coil, 37/6, plus 3/6 post and insurance.

FLUORESCENT LIGHTS



These are complete fluorescent lighting fittings. Built-in ballast and starters—stove enamelled white and ready to work. Ideal for the kitchen, over the workbench and in similar locations.

Single 40. 4ft. 8in. long, uses a 40 watt tube.

Twins 20. Uses two 20-watt standard tubes. Price 39/6 each, with tubes.

Carriage and ins. up to 150 miles 5/6, up to 250 miles 7/6.



MINI-RADIO

Uses high-efficiency coils—covers long and medium wavebands and fits into the neat white or brown Bakelite cabinet—limited quantity only. All the parts, including cabinet, valves, in fact, everything, £1/10/- plus 3/6 post. Constructional data free with the parts, or available separately 1/6.

THERMOSTATS



2½in. x 1in. x 1½in. high.

Useful for the control of appliances such as convector, glazed vulcanites hot plates, etc. Adjustable to operate over temperature range 50-550 deg. F., with heavy silver contacts.

1½ amp. 3/6; 5 amp. 5/6; 2 amp. Q.M.B. 5/6; 15 amp. Q.M.B. 15/6; 15 amp. wall mounting type 19/6.

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All enquiries to Eastbourne address and please enclose S.A.E., terms are cash with order.

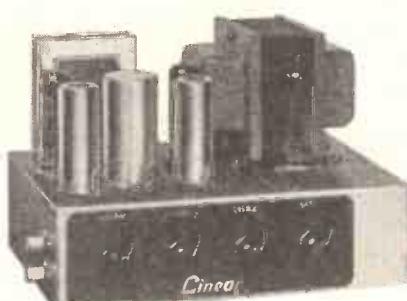
THE LINEAR 'DIATONIC'

A HIGH FIDELITY ULTRA LINEAR AMPLIFIER WITH INTEGRAL PRE-AMP

A special feature is the compactness of the unit. Full advantage has been taken of latest component miniaturisation developments to produce a 10-watt Hi-Fi push-pull amplifier incorporating tone control preamplifier stages within the measurements of $9 \times 7 \times 6\frac{1}{2}$ in.

In addition two high impedance input sockets are provided for microphone and gram, etc. Each input has its associated vol. control, five B.V.A. valves are employed ECC83, ECC83, EL84, EL84, EZ81.

H.T. and L.T. power supply point is included for a radio tuner.



L45 MINIATURE 4/5 WATT QUALITY AMPLIFIER

Size only $6 \times 5 \times 5\frac{1}{2}$ in. high. 3 d.b. Negative Feedback. Sensitivity 30 m.v. for full output. 3 Mullard valves. ECC83 Triode, EL84 Power Output, EZ80 Rectifier. Separate Bass and Treble Controls. For 200—250v. 50 c.p.s. A.C. Mains. An ideal unit for use with Gram. or 'Mike'. Output matching for 2—3 ohm speakers. Retail Price £5/19/6.

LT/45 TAPEDECK AMPLIFIER

A complete unit ready for connection to 200—250v. 50 c.p.s. A.C. Mains, 2—3 ohm speaker and practically any make of Deck. Negative feedback, equalisation adjustment by multi-position switch for $\frac{3}{4}$, $\frac{7}{8}$, 15in. per sec. Retail Price 12 Gns.

LG3 2/3 WATT GRAM AMPLIFIER

Overall size $6\frac{1}{2} \times 4 \times 2\frac{1}{2}$ in. For 200—250v. 50 c.p.s. A.C. Mains. Controls: Tone/Mains 'On-Off,' and Volume. Output for 2—3 ohm speaker. 49/9.

**12 RETAIL PRICE.
GNS.**

SIZE ONLY 9—7—6 $\frac{1}{2}$ ins.

Weight: 12 $\frac{1}{2}$ lb. Power consumption 90 watts For 200-230-250v. 50 c.p.s. A.C. mains. Outputs for 3 and 15 ohm speakers.

Chassis stoved Grey—Blue hammered finish.

Attractive Cover with Chromium carrying handles now available at 17/6.

From your local stockist or, if in difficulty, direct from us.

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for the Connoisseur**

THE LATEST

"TL/12 PLUS" POWER AMPLIFIER
and the

"VARISLOPE III" PRE-AMPLIFIER

are designed to give the highest possible fidelity from records, radio and tape.

OTHER LEAK PRODUCTS "Trough-Line" F.M. Tuner Point One Pre-amplifier Dynamic Pickup

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LOUDSPEAKERS: Goodmans · Tannoy · Wharfedale

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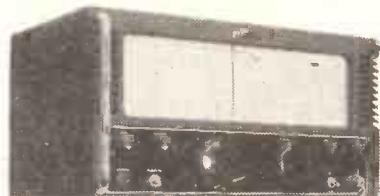
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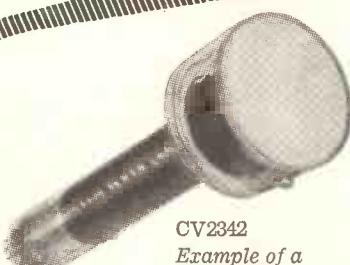
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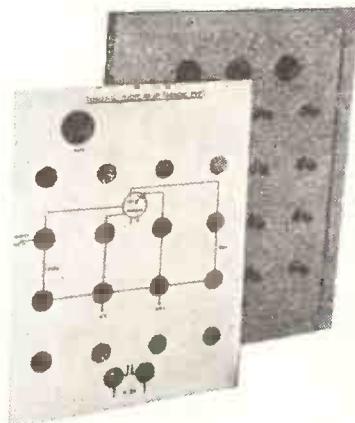
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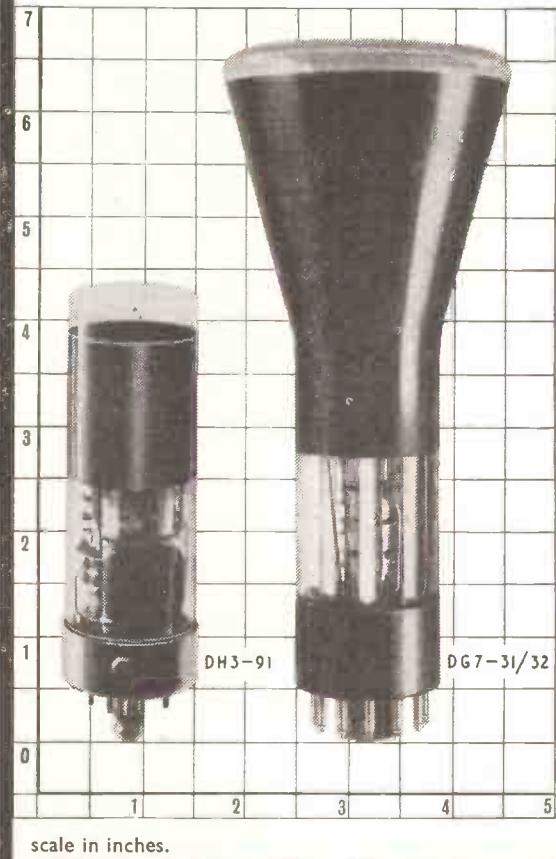
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Heater 6.3 volts, 0.55 amp.

Typical Operation

V _{a1+a3}	500V
V _g	-8 to -27V
S _x	0.19 mm/V.
S _y	0.22 mm/V.

Low Voltage Cathode Ray Tubes



scale in inches.

DG7-31/32

DG7-31 (*Asymmetrical Deflection*)
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Heater 6.3 volts, 0.3 amp.

Typical Operation

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V _{a2}	0 to 120V
V _g	-50 to -100V
I _{a2}	-15 to + 10 μ A
S _y	0.39 mm/V
S _x	0.25 mm/V
Line width (measured on a circle of 50 mm diameter with V _{a1+a3} = 500V and I _t = 0.5 μ A)	0.5 mm



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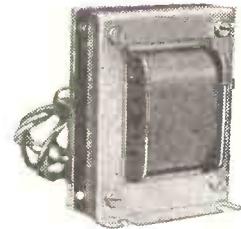
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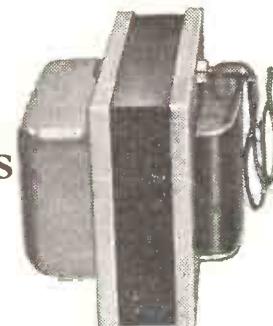


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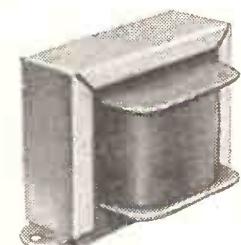
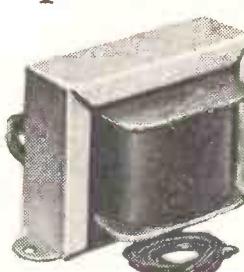


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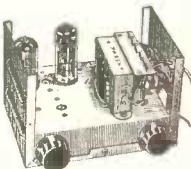
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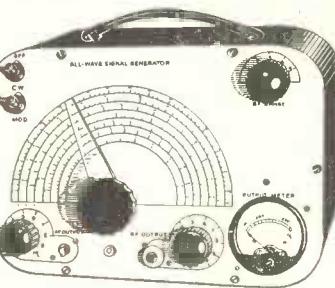


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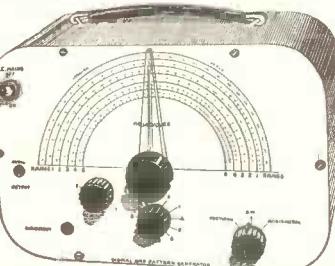
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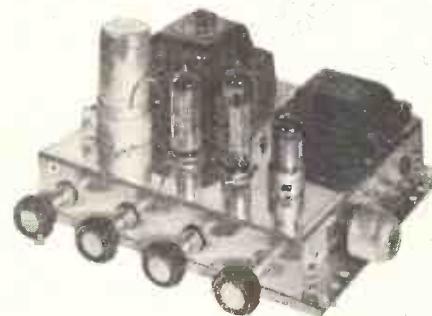


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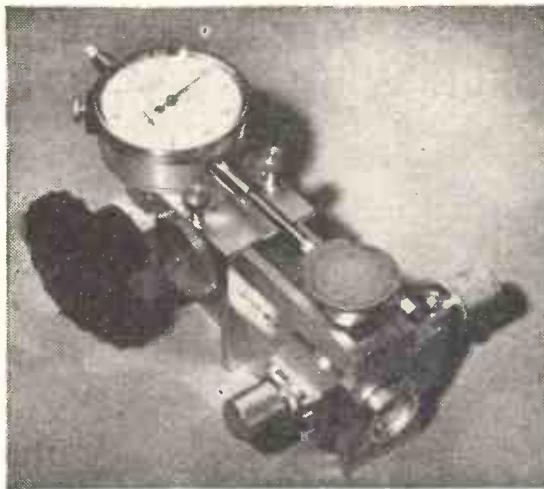
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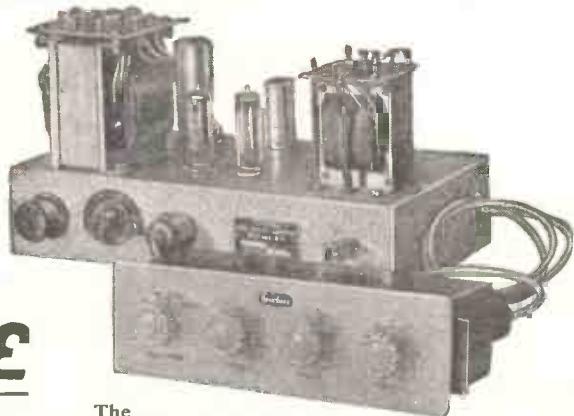
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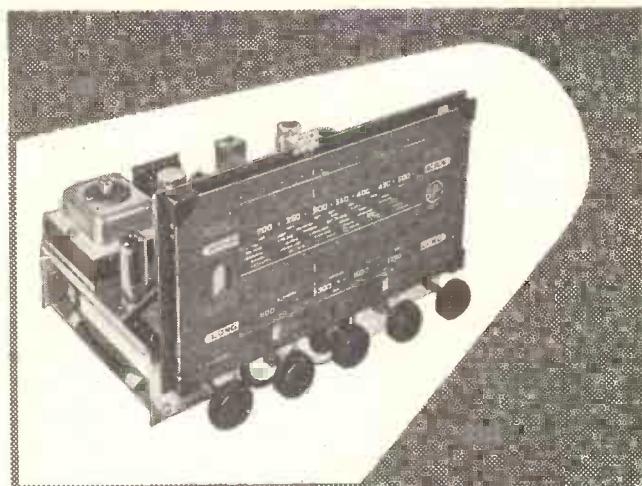
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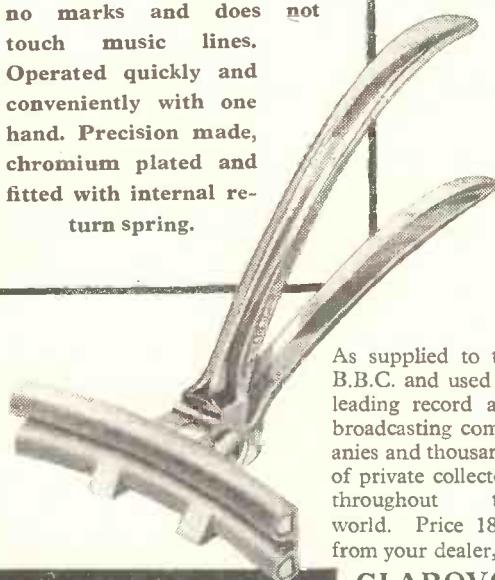
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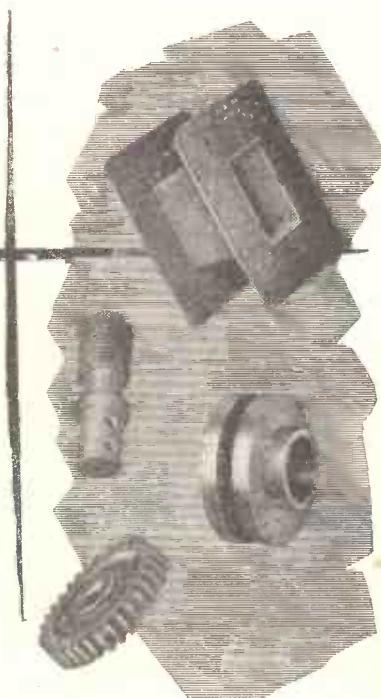
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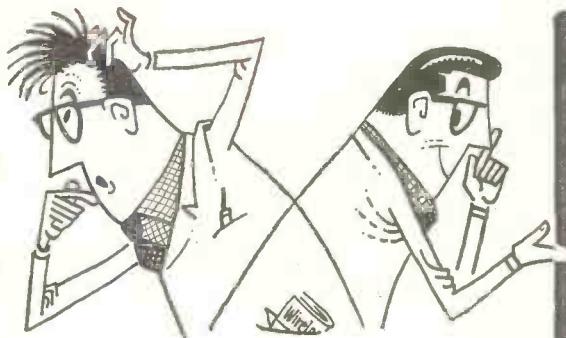


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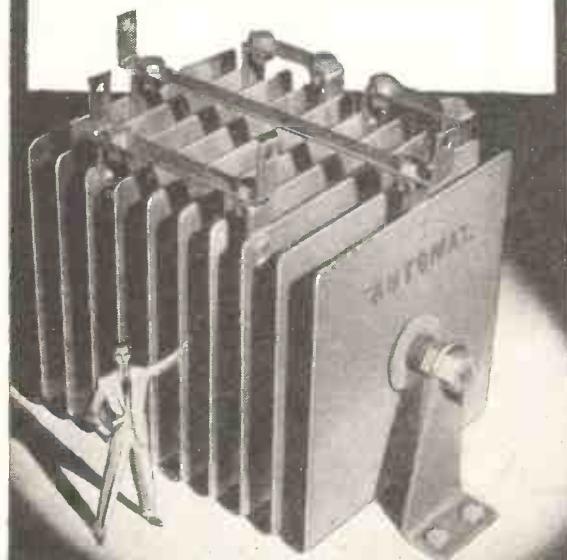
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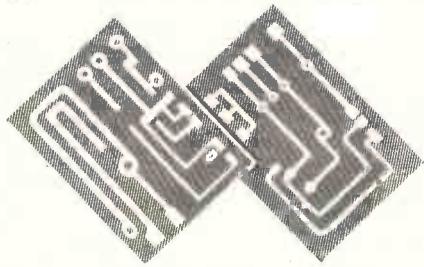
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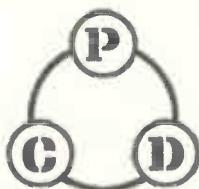
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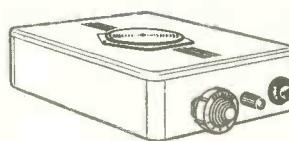
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Moving Coil Headphones with earpads and 6ft. lead 12/6. U.S. make ELECTROLYTICS: 8 x 8 350 v. 20 mfd. 150 v. working, 1/6 each. Discount for quantity. Top prices paid for tape recorders, etc.

RADIO EXCHANGE CO.

27 HARPER STREET, BEDFORD.
TRADE AND MAIL ORDER ONLY.

*a NEW simple-to-operate
means of
checking transistors*

the BONOCHORD TRANSISTOR TEST SET TYPE 40

This new BONOCHORD instrument has been designed for simplicity of operation when measuring the basic grounded emitter parameters. It can be used for routine testing during production, in the service department, and the laboratory, in fact wherever there is a need for facilities for quick checking of transistors. The BONOCHORD Transistor Test Set Type 40 will test any p.n.p. transistor, with the exception of very high-power types. Here are some of its features.

- Measures I_{CO} the collector current with zero base current.
- Measures α the current gain in grounded emitter by small signal A.C. measurement.
- Junction voltage variable to 9 volts in standard arrangement but alternative range can be supplied.
- Collector current variable to 10mA.
- Compares transistor noise quantitatively.
- Operates from 110, 200-250 volts A.C. mains.
- Housed in attractive cabinet finished in grey slove enamel.
- Dimensions approx. 14½" wide by 18" high by 8½" deep.

Bonochord

Full details from Bonochord Ltd., 48 Welbeck Street, London W.1
Telephone: WELbeck 8245

We offer a complete Tape Recorder Service

These are some of the other well-known models we stock:

Vortexion 2A	88 gns.
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Brenell Mk. 4	53 gns.
Brenell Deck with pre-amplifier unit	38½ gns.
Elon	62 gns.
Grundig TK5	53 gns. inc. mic.
" TK8	72 gns. ex. mic.
" TK20	98 gns. do.
Ferrograph 3A/N	79 gns.
Elizabethan	65 gns.
Truvox	66 gns.

★ ★ ★

Tapes
L.P. and Standard

E.M.I.

Scotch Boy

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We stock all the leading makes of amplifiers, control units, transcription units, pickups, loudspeakers and FM Tuner units.

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Three-directional reproduction, full frequency range fidelity, microphone storage facilities, and the finest styling ever. Twin track with automatic switching and push button operation. Magic Eye recording level indicator.

Price 100 gns. (ex. microphone)

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We engineered the best—then improved it

We just weren't satisfied with the best when we engineered the Tannoy Variluctance Pickup Cartridge.

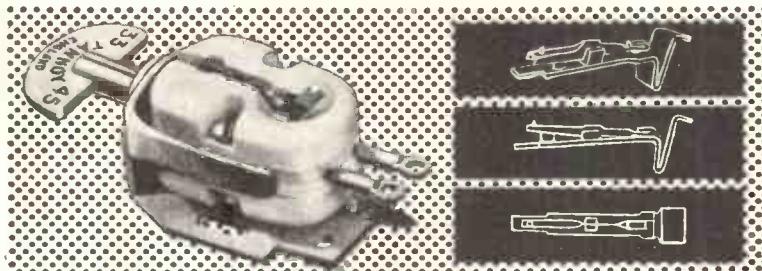
Our design engineers went to work right away and perfected the "Complidex," a brand new stylus assembly that utilizes with even greater efficiency both the cantilever and variable reluctance principles. Using a combination of two distinct metals our design engineers overcame the inevitable compromise between magnetic and mechanical requirements entailed by a conventional homogeneous material. Result—the new

"Complidex" Stylus has increased magnetic efficiency within the gap plus improved mechanical efficiency of the cantilever. Further development gives correctly graded damping without disturbing the optimum vertical-lateral ratio of compliance.

Like their predecessors, the new "Complidex" Styli—with either sapphires or diamonds—allow instantaneous replacement without tools. **The new "Complidex" Styli can be used to convert the original (Mark 1) cartridge to Mark II specification.**

SPECIFICATION

Each cartridge hand-made and laboratory tested
Frequency response within 2dB to 16,000 Kcs.
No resonant peaks
No undamped resonances in sub-supersonic range
Simple turn-over mechanism
Stylus assemblies completely independent
Instantaneous replacement of stylus without
use of tools
Optimum lateral-to-vertical compliance ratio
Very low effective dynamic mass
Output: 20 mV at 12 cm per second
Termination load: 50,000 ohms.
Tracking weight: 6 grams for all discs
Available with either diamond or sapphire stylus



TANNOY Mark II 'VARILUCTANCE' PICKUP CARTRIDGE

Tannoy Products Ltd. (Practitioners in Sound),
West Norwood, London SE27. Telephone: Gipsy Hill 1131

TANNOY

NP 60



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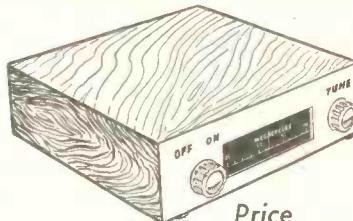


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Guaranteed 12 months.
Complete with its own power supply. Easily fitted. Cash with order. We pay the postage.

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Complete with its own power pack and polished wooden cabinet. Nothing else to buy. Will work with any amplifier, record changer, radio or radiogram. Full, clear instructions with each tuner. Fully guaranteed.



CR50 BRIDGE measures 10 pfd to 100 mfd and 1 ohm to 10 Megohms in fourteen ranges, with a total scale length of over 120 inches. This instrument was specially designed for bench use, having a sloping front panel and extra heavy gauge steel case, finished in black crackle. The controls are arranged so that quick and accurate readings may be taken. Balance indication is by a magic eye fed from a high gain amplifier. A leakage test is incorporated for condensers. Internal standard are 1% accuracy. Complete with all valves and instructions, ready for use from 200/250 volt A.C. mains, £7/18/-, plus 4/6 carr./pack.

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Further details will be sent by return of post on receipt of self addressed and stamped envelope.

Send your order to:—

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40,000 MICRO SWITCHES

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MK. 4 BR
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**78/- PER
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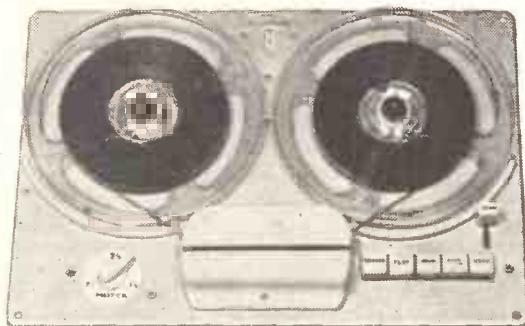
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Special quotations to manufacturers for large quantities.

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INTRODUCING THE NEW MOTEK K9 TAPE DECK!

Outstanding features include:

- ★ 3 speeds at turn of knob ($7\frac{1}{2}$ in. per sec., $3\frac{3}{4}$ in. per sec. and $1\frac{7}{8}$ in. per sec.).
- ★ Built-in rev. counter for precise tape location.
- ★ Pause control.
- ★ Fully automatic push-button operation with spare contacts on Record and Play wafers to allow for possible amplifier wiring (8 two-way changeover switches).
- ★ High impedance, record and erase heads. (Simple azimuth adjustment).
- ★ Three-motor drive.
- ★ Fast, forward and rewind functions without handling tape.
- ★ Low wow level.



List Price 21 gns.

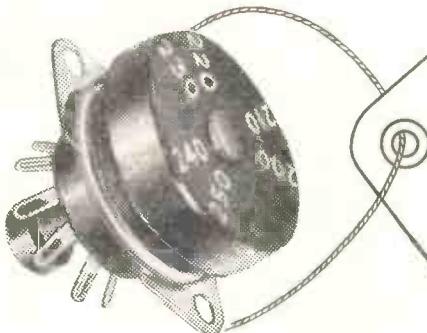
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miniature mains
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McMURDO
*Miniature
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**STANDARD B9A (NOVAL) VALVEHOLDER WITH 2-PIN
CAPTIVE PLUG.
UP TO 6 TAPPING POSITIONS.
MARKING TO CUSTOMERS' REQUIREMENTS.**

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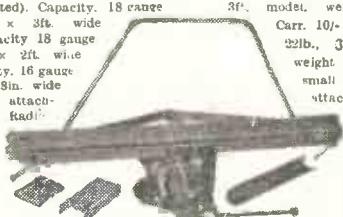
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MVS 11

PARKER'S SHEET METAL FOLDING MACHINES. HEAVY VICE MODELS

No. 1 (illustrated). Capacity 18 gauge mild steel x 3ft. wide. No. 2. Capacity 18 gauge mild steel x 2ft. wide. No. 3. Capacity 16 gauge mild steel x 18in. wide. End vise attachments or radii chases, Trav. Box making, are supplied if required.



3ft. model, weight 56lb., £6/5/- Carr. 10/- 2ft. model, weight 22lb., £5/-. 18in. model, weight 18lb., £5/-. Carr. on small models 4/- £1 with attachments 5/6.

Attachment angle for 3ft. 3/8 per ft. Small models 2/- per foot.

Machines guaranteed send for details

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and FLEXIBLES
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Stern's "fidelity"

TAPE RECORDER

"IT REALLY DOES SOUND BETTER THAN ANY OTHER"

TESTED AND APPROVED AT THE TRUVOX LABORATORIES

IT INCORPORATES: The NEW TRUVOX Mk. IV TAPE DECK together with the "fidelity" MODEL HF/TR2 TAPE AMPLIFIER (both fully described on this page), and a Rola 10 x 6in. P.M. speaker.

- BEFORE CHOOSING YOUR TAPE RECORDER YOU SHOULD HEAR THIS MODEL—TRULY "Hi-Fi" RECORDINGS ARE OBTAINABLE and it is comparable to much higher-priced Recorders.

Alternatively send S.A.E. for ILLUSTRATED LEAFLET.

CREDIT SALE: Deposit £12/8/- and 9 monthly payments of £4/10/8.

HIRE PURCHASE: Deposit £24/15/- and 12 monthly payments of £2/5/11.

PRICE ... Including CRYSTAL MIKE and 1,200ft. reel of PLASTIC TAPE.

£49.10.0. (OR £3 EXTRA WITH REV. COUNTER.)

(Plus £1/10/- carriage and insurance, of which £1 is refunded on return of Packing Case.)

A COMPLETE KIT OF PARTS TO BUILD
The "fidelity" TAPE AMPLIFIER Model HF/TR2
including POWER SUPPLY UNIT
FOR ONLY £12.0.0 (Plus 6/- Carr. and Ins.)



This amplifier has been expressly designed to meet the requirements of the enthusiasts for High Fidelity reproduction. It is based on the very successful design, completed by the Mullard Technicians and only really high-grade components are incorporated; truly HIGH FIDELITY Recordings are obtainable whilst "Hi-Fi" reproduction is assured by use of a high-quality Output Transformer by Gilson. It incorporates a "variable" Recording Level indicator, a two-position equaliser for 31/2 and 71/2 speeds, and an effective Tone Control arrangement. Monitoring facilities, speaker Socket are incorporated and in addition a position is provided to enable it to be used as an independent Amplifier for Gramophone Records or Radio Tuning Unit. Overall size: 11in. x 6in. x 6in. high. Suitable for nearly all makes of Tape Decks. When ordering, please advise make of deck in use.

THE ASSEMBLY MANUAL PRACTICAL DIAGRAMS, etc. are available for 2/8 or send S.A.E. brief details.
WE ALSO SUPPLY THE HF/TR2 ASSEMBLED AND READY FOR USE FOR £16.0.0. (Plus 6/- Carr. & Ins.). H.P. TERMS. Deposit £5 and 9 monthly payments of £1. CREDIT TERMS: Deposit £4 and 9 monthly payments of £1/8/4.

The Mk. IV DECK CAN ALSO BE SUPPLIED INCORPORATING PRECISION REV COUNTER for £20/9/- H.P. TERMS: Deposit £15/4/6 and 12 months of £1/8/3. CREDIT SALE: Deposit £7/12/3 and 9 months of £2/15/10.

Home Constructors!
BUILD YOUR OWN "Hi-Fi" TAPE RECORDER
WE OFFER YOU

(a) The model HF/TR2 AMPLIFIER and POWER UNIT, both fully assembled, together with the TRUVOX MK IV TAPE DECK for ... ALTERNATIVELY as above but the HF/TR2 Amplifier and P/Unit as a COMPLETE KIT OF PARTS	£38 10 0
(b) The model HF/TR2 AMPLIFIER and POWER UNIT both fully assembled, together with the TRUVOX TAPE DECK incorporating PRECISION REV COUNTER	£35 0 0
ALTERNATIVELY as above but the HF/TR2 Amplifier and P/Unit as a COMPLETE KIT OF PARTS	£41 10 0
(c) The model HF/TR2 AMPLIFIER and POWER UNIT, both fully assembled, together with the COLLARO TRANSCRIPTOR	£33 0 0
ALTERNATIVELY as above but the HF/TR2 Amplifier and P/Unit as a COMPLETE KIT OF PARTS	£35 0 0
plus 12/6 Carr. and Insurance.	£31 10 0

TO COMPLETE THE RECORDER ... WE OFFER

The Portable Carrying Case... Also Crystal Mike ... A Rola 10 x 6in. P.M. SPEAKER ... 1,200 ft. Plastic Tape

ALL FOR £8.10.0. (plus 7/6 Carr. & Ins.)

STERN'S TAPE PRE-AMPLIFIER and ERASE UNIT

Provides the "Link" between the HIGH-QUALITY AMPLIFIER and TAPE DECK.

STERN'S MODEL HF/TRIP ... A completely assembled Pre-Amplifier with own Power Supply. Can be supplied correctly matched for use with Truvox, Brenell or Collaro Decks, and incorporates Recording Level Indicator and Monitoring facilities. Please send S.A.E. with any inquiry.

PRICE £11.10.0 (plus 5/- Carr. and insurance)



THE NEW TRUVOX Mk IV TAPE DECK

UNDoubtedly ONE OF THE BEST TAPE DECKS ON THE MARKET.

PRICE £27.6.0 (Plus 10/- Carr. and Ins.)

CREDIT TERMS: Deposit £6/17/- and 9 monthly payments of £2/10/-

H.P. TERMS: Deposit £13/13/- and 12 monthly payments of £1/5/4.

SPECIFICATION: ● 3 B.T.H. shaded pole motors with silent friction drive eliminating wow and flutter. ● Push-button controls, electrically and mechanically interlocked (patented). ● Patented electric-type push-button controlled brake. ● Inching to assist editing; tape loading on the drop-in principle accommodation for reels of 7in. diameter. ● Tracking sense. To British and American standards. ● Playing times: Up to 3 hours with L.P. Tape or 2 hours with Standard Tapes. ● Two tracks side by side, with safety gap. ● Playing time indication by precision revolution counter or large visual type indicator plate, according to choice. Positive Azimuth adjustment of Record/Player Head. ● High Impedance Heads. ● The metal work is Gold Hammered finish. ● Overall size 14in x 12½in, from top of face of panel, overall depth 5in.

The Mk. IV DECK CAN ALSO BE SUPPLIED INCORPORATING PRECISION REV COUNTER for £20/9/- H.P. TERMS: Deposit £15/4/6 and 12 months of £1/8/3. CREDIT SALE: Deposit £7/12/3 and 9 months of £2/15/10.



WE MAKE SPECIALLY REDUCED PRICES FOR COMBINED ORDERS

OR ADD TAPE TO YOUR EXISTING AMPLIFIER . . . WE OFFER YOU

- (d) The Model HF/TRIP TAPE PRE-AMPLIFIER together with the TRUVOX MK IV TAPE DECK £235 0 0
- (e) ALTERNATIVELY as in (d) above but Truvox Deck incorporating PRECISION REV. COUNTER £38 0 0
- (f) The model HF/TRIP TAPE PRE-AMPLIFIER together with the COLLARO TRANSCRIPTOR Tape Deck £31 10 0

PLEASE INCLUDE 12/6 to cover cost of Carriage and Insurance.

HIRE PURCHASE and CREDIT SALE TERMS are available on all equipment (excluding Kits of Parts). Send S.A.E. for details.

NOTE . . . The Collaro Transcriber is in short supply and there may be a delay in delivery. We will however book an order.

The Deck switches of the Transcriber have to be "wired-up". We will complete this wiring, for use with either the HF/TR2 or the HF/TRIP, for an extra charge of £1.00.

WHY NOT HAVE A COMBINED TAPE-RECORDER-RADIOGRAM

We will quote for a "Hi-Fi" Amplifier, Radio, Tape Unit, the Tape Deck and Pre-amplifier and a Gram Unit . . . Prices range from £72.00 (plus Cabinet and Speaker.) Send S.A.E. with enquiry.

Open Monday to Friday 9 a.m.—5 p.m. Saturday 9 a.m.—1 p.m.

STERN RADIO LTD.

(DEPT 109/W)

109 & 115, FLEET ST., LONDON, E.C.4

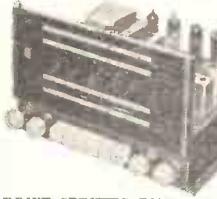
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IT'S MUCH
BETTER

THE NEW ARMSTRONG P.B.409
AM/FM RADIOPHONIC CHASSIS
PRICE

£29.8.0

(Plus 7/6 carr. and ins.).



BRIEF SPECIFICATION:—
A 9 valve line up employing the latest MULLARD preferred-type valves. Provides complete coverage of the VHF/FM Transmissions, plus the SHORT, MEDIUM and LONG waves. Has Push-Pull output with negative feedback, for 6 watts Peak output. Quick action "Piano Key" Selectors and separate Bass and Treble Controls. Has "Magic Eye" Tuning Indicator. Dimensions 13in. x 9½in. x 8in. high. Dial size 11½in. x 5½in.

HOME CONSTRUCTORS !!
BUILD YOUR OWN "Hi-Fi"
LOUDSPEAKER SYSTEM

WITH W-E'S WELL KNOWN RANGE OF READY-TO-ASSEMBLE CABINETS, ALL ARE BEAUTIFULLY MADE AND FINISHED AND VERY EASILY ASSEMBLED. ONLY A SCREWDRIVER IS REQUIRED. THE ABE PACKAGE PLAT IN CARTONS AND COMPLETE WITH SCREWS. WE SHOW A FEW HERE BUT OTHERS ARE AVAILABLE. SEND S.A.E. FOR LEAFLET.

CALL IN AND LISTEN TO THEM

THE JUNIOR
BASS REFLEX
CORNER CONSOLE

A new contemporary-style cabinet, specially designed to give maximum reproduction quality from Stentorion 8in. or 10in. units, with provision for Tweeter Unit, if required. Measures 33in. x 22½in. x 18in. Price £9/9/- or with the 8in. Stentorion Speaker £13/12/6 or with 10in. Stentorion Speaker £14/8/6.



The "PRELUDE" Hi-Fi
CONSOLE CABINET
Takes any make of tape-deck or record player amplifier, pre-amplifier control unit, and radio tuner. Size 33in. x 19in. x 19½in. Height above baseboard is 6½in. Price £13/13/-.



THE "PRELUDE"
BASS REFLEX
CORNER CONSOLE

This most attractive cabinet has been specially designed to utilise the natural acoustic properties of the walls, and is also obviously suitable for use where space-saving is a consideration. It is sturdy constructed to take every advantage of Stentorion 8in. or 10in. units, with provision for Tweeter Unit. Size 33in. x 21in. x 17in. Price £10/10/0 or with the 8in. Stentorion Speaker £14/13/6 or with the 10in. Stentorion £15/9/6.

The "PRELUDE" Hi-Fi
TABLE CABINET

Designed to take any make of Tape Deck, Single Record Player (not Auto-changer), Pre-amplifier Control Unit, and Radio Tuner. Price £9/19/6. Size 19in. x 19in. x 19½in.

HIRE PURCHASE and CREDIT SALE TERMS
ARE AVAILABLE. SEND S.A.E. for details.
WE ALSO HAVE THE GOODMAN SHERWOOD
ENCLOSED IN STOCK.

MODERNISE YOUR OLD RADIOPHONIC

THE ARMSTRONG MODEL A.F. 105
AM/FM RADIOPHONIC CHASSIS

A Genuinely Hand Made Chassis

- Developed to meet the needs of those who require really high quality radio and record reproduction and who, for reasons of expense or lack of room in existing or proposed cabinets, cannot consider the normal high-fidelity system. The A.F.105 is as good as, or better than, many of the high quality amplifiers, and associated units. Independent and continuously variable Bass and Treble controls give a wide range of control. SEND S.A.E. FOR DETAILS.

PRICE £37 (Plus 7/6 carr. and ins.).

CREDIT SALE TERMS: Deposit £9/5/- and 9 monthly payments of £3/7/10.

HIRE PURCHASE TERMS: Deposit £18/10/- and 12 monthly payments of £1/14/4.

THE MODEL A.F.O.—3 Waveband A.M. only
RADIOPHONIC CHASSIS

PRICE £11.16.4

(plus 7/6 carr. and ins.).

H.P. TERMS: Deposit £5/18/4 & 8 monthly

payments of £1/7/8.

This is a standard 5-valve A.C. Mains Superhet Receiver Chassis covering Long

Medium Short

Wavebands having Gram and Extension Speaker Sockets.

Reproduction from both Radio and Gram is really good and makes an ideal chassis for a simple domestic installation. Overall size is 12in. x 7in. x 7½in. high.

Really Modern Demonstration Rooms are now available for the convenience of callers.

Stern's "fidelity" F.M. TUNING
UNIT

A 5-Valve Tuner incorporating

the latest Mullard Permeability Tuned

Unit. Price assembled less Power

Supply:

£14.10.0

(Plus 7/6 carr. and ins.).

TERMS: (a) H.P. Deposit

£7/5/- and 9 monthly payments of 18/4;

(b) Credit Deposit £3/12/6 and 9 monthly payments of £1/6/7.

Provides "Hi-Fi" reproduction with any make of Amplifier and many Radio Receivers. It incorporates: • The latest Valve Line-up—ECC85, 2 type EF85, EF91 and EM80. • A "Magic Eye" Indicator. • Power consumption is 1.7 amps at 6.3 volts and 25 mva. at 250 volts.

STERN'S "fidelity" COMBINED A.M. and F.M.
TUNING UNIT

This is IDENTICAL to the Stern's F.M. Tuner illustrated above, but in addition incorporates the MEDIUM WAVE-BAND and thereby also provides a selection of foreign stations. PRICE £18.18.0 (Plus 7/6 carr. and ins.).

TERMS: (a) H.P. Deposit £9/9/- and 10 monthly payments of £1/1/-; (b) Credit Deposit £4/15/- and 9 monthly payments of £1/14/7. Send S.A.E. If further data required.

HOME CONSTRUCTORS... You can build

(a) The "fidelity" F.M. TUNING UNIT FOR £10.0.0

(b) The "fidelity" AM/FM TUNING UNIT for £13.0.0

THE COMPLETE ASSEMBLY DIAGRAMS AND INSTRUCTIONS CAN BE OBTAINED FOR 1/6 each.

STERN'S POWER SUPPLY UNITS

Fully smoothed with all output connections terminated to connecting blocks, thereby enabling ease of connecting to a Radio Tuner Unit or Amplifier, etc. (the Compact 5 Amplifiers are immediately connected in this way). Overall size of Units is 9in. x 3½in. x 4½in. high. TWO MODELS ARE AVAILABLE. Type "A" Unit provides 250-300 volts at up to 70 mA, and 6.3 volts at 3½ amps.

PRICE £2.17.6 (Plus 2/- Carr. and ins.).

Type "B" Unit provides 250-300 volts at up to 100 mA and 6.3 volts at 3½ amps.

PRICE £3.3.0 (Plus 2/- Carr. and ins.).

WE ALSO SUPPLY THESE UNITS AS COMPLETE KITS
OF PARTS

A detailed wiring-up leaflet is supplied (this is available separately for 9d.), and they are very quickly and easily assembled.

Type "A" Unit Complete Kit. PRICE £2/9/6.

Type "B" Unit Complete Kit. PRICE £2/15/-.

(Carriage and insurance is 2/- extra.)

IT'S MUCH
CHEAPER

THE DULCI MODEL H.4

COMBINED
AM/FM
RADIOPHONIC
CHASSIS

A 4 Waveband Receiver designed for first rate reproduction of Radio and Gram.

PRICE £24.6.6

(Plus 7/6 Carr. and ins.).

CREDIT TERMS: Deposit £6/2/- and 9 monthly payments of £2/4/7. H.P. TERMS: Deposit £12/3/3 and 12 monthly payments of £1/2/7.

BRIEF SPECIFICATION:—

- Covers Short, Medium and Long and F.M. Wavebands.
- Employs full A.V.C.
- The Latest 7-valve line-up.
- For 3 or 15 ohm P.M. Speakers.
- "Magic Eye" Tuning Indicator.
- Excellent Tone range up to 4 watts output.
- Internal aerial for local stations.
- Overall size 12in. x 8in. x 7in. high.

A Good Quality Chassis and Well Recommended.

THE DULCI MODEL H.4.T.

Combined AM/FM Tuning Unit
incorporating own Power Supply.

MODEL H.4.T. This model is the "TUNER UNIT VERSION" of the H.4 Radiogram Chassis illustrated and described above. It has the same coverage of A.M. and F.M. Wavebands (4 altogether) and precisely the same in size and appearance, except that it has three Controls only, being TUNING, WAVECHANGE and Volume On/Off, mounted centrally on the chassis. A self-contained Tuner incorporating own Power Supply.

PRICE £20.17.0

(Plus 7/6 Carr. and ins.).

CREDIT TERMS: Deposit £5/4/3 and 9 monthly payments of £1/18/4. H.P. TERMS: Deposit £10/8/6 and 12 monthly payments of 19/4.

THE DULCI
MODEL H.3.
COMBINED
AM/FM
RADIOPHONIC
CHASSIS

This model is very similar to the model H.4 described above but covers 3 WAVEBANDS instead of 4 (omitting the Short Band) and is for 3 ohm Speakers only. Overall size is as for the H.4.

PRICE £20.17.0 (Plus 7/6 Carr. and ins.).

CREDIT TERMS: Deposit £5/4/3 and 9 monthly payments of £1/18/4. H.P. TERMS: Deposit £10/8/6 and 12 monthly payments of 19/4.

RECORD PLAYERS
THE VERY LATEST MODELS
ARE IN STOCK

MANY AT REDUCED PRICES !!!
TRANSCRIPTION UNITS—AUTOCHEANGERS
SINGLE RECORD PLAYERS
Send S.A.E. for ILLUSTRATED STOCK LIST

CASH ONLY OFFER !!!

This latest Brand New B.S.R. MONARCH 4-SPEED AUTOCHANGER
£8.7.6 (Plus 5/- Carr. and ins.).

• Minimum baseboard size required 14in. x 12½in., with height above 5½in., & height below baseboard 2½in.



WE ALSO HAVE A FEW ONLY
COLLARO MODEL 456 4-Speed "Mixer" Autochangers.
The Units are BRAND NEW and incorporate the STUDIO
"O" Pick-up. PRICE £8.19.6 (Plus 5/- Carr. and ins.).

Open Monday to Friday 9 a.m.—6 p.m.

Saturday 9 a.m.—1 p.m.

**STERN
RADIO LTD.**

AMPLIFIERS
PRE-AMPLIFIERS

HIGH FIDELITY FOR THE HOME CONSTRUCTOR

COMPLETE KITS OF PARTS FOR THE "Hi-Fi" ENTHUSIAST

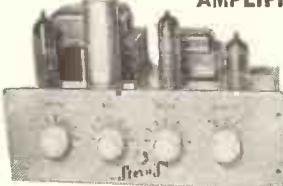
QUALITY OF THIS NATURE HAS NEVER BEFORE BEEN OFFERED AT SUCH LOW COST

STERNS REMOTE CONTROL UNIT

Designed in particular for use with the MULLARD 5-10 Main Amplifier.

Ideally suited for simple domestic installation as an alternative to the more elaborate Pre Amplifiers. Complete and described opposite. Tone Control facilities are really excellent and in conjunction with the "5-10" Main Amplifier reproduction is of very high quality. Perfectly suitable for use with all the popular Record Players (B.S.B., Collaro, Garrard) and the modern Radio Tuner Units. Front Panel contains: (a) Coloured Indicator; (b) Separate BASS and TREBLE CONTROLS; (c) 3 position Selector Switch; (d) Volume Control. Inputs on back for Radio and Gram. and Gram. equalising is incorporated. FULL DATA is contained in the 5-10 MAIN AMPLIFIER MANUAL at 1/6.

THE MULLARD "3-3" QUALITY AMPLIFIER



A small Compact Amplifier capable of VERY HIGH QUALITY REPRODUCTION on both RADIO and GRAM.

PRICE for Complete KIT OF PARTS..... £6.19.6

(plus 5/- Carr. & Ins.)

Alternatively supplied ASSEMBLED and READY for USE..... £8.12.6

(plus 5/- Carr. & Ins.)

The complete SPECIFICATION and ASSEMBLY DIAGRAMS are available for 1/6.

Developed from the very popular 3 valve 3 watt Amplifier designed in the Mullard Laboratories. We strictly adhere to their specification but in addition we have added switched equalising for L.P. and 78 records and a position for Radio Inputs, plus additional power to feed a Radio Tuning Unit. Extremely simple to assemble and ideally suitable to incorporate with an F.M. Tuner and Record Player in a small installation.

BRITAIN'S FINEST "H.F.I" AMPLIFIER

The GENUINE WILLIAMSON "Still sets the standard for all amplifiers." Many versions of the Williamson have been offered to the public at various low prices but the only Williamson is the Amplifier the designer's specification and employing the very highest grade Components that he specifies, i.e. PART-RIDGE TRANSFORMERS, CHOKEs, etc. It is only in doing this that the exceptionally high standard that has been attained. WE HAVE DONE THIS!!... and we offer these KITS OF PARTS, including Partridge and other high-grade Components, as follows:-

(a) To build the MAIN AMPLIFIER ONLY £14.10.0
(illustrated above)
(b) To build the TWIN POWER SUPPLY UNIT ONLY..... £13.10.0
(Insufficient space to illustrate this)
(c) COMPLETE KIT to build both above £27.0.0

We will also supply COMPLETELY ASSEMBLED and will be pleased to quote. Credit and H.P. Terms are available. The complete SPECIFICATION and general ASSEMBLY INSTRUCTIONS are available for 3/6.

Our "fidelity" PRE-AMPLIFIER, illustrated and described above, or alternatively the RCA Pre-Amplifier at £16/5/-, is recommended for use with the Williamson.

DEPT. 109/W

**109-115 FLEET ST.
LONDON. E.C.4**

Phone: FLEet Street 5812-3-4.

The MULLARD "5-10" MAIN AMPLIFIER



Probably the most popular and successful Amplifier yet designed and

certainly needs no recommendation from us. Our kit is complete to MULLARD'S specification including the latest ULTRA LINEAR OUTPUT TRANSFORMER and the recommended Mullard Valve line-up. All specified Components are supplied and Power Supply is available to drive a Radio Tuner Unit.

PRICE OF COMPLETE KIT OF PARTS £9.10.0
(Plus 5/- Carr. & Ins.)

or alternatively we supply—

FULLY ASSEMBLED AND TESTED for £11.10.0
(Plus 5/- Carr. & Ins.)

WE ALSO OFFER THE "5-10" INCORPORATING THE LATEST PARTRIDGE ULTRA LINEAR OUTPUT TRANSFORMER FOR AN EXTRA £1.6.0.

The ASSEMBLY MANUAL containing FULL SPECIFICATION is available for 1/6. It also includes full data on the REMOTE CONTROL UNIT.

(a) The COMPLETE KIT OF PARTS to build both the MULLARD 5-10 and the REMOTE CONTROL UNIT for.....

(b) The COMPLETE KIT OF PARTS to build both the MULLARD 5-10 and the "fidelity" PRE-AMPLIFIER-TONE CONTROL UNIT for.....

ALTERNATIVELY WE WILL SUPPLY ASSEMBLED and FULLY TESTED, as follows:-

(a) The MULLARD 5-10 and the REMOTE CONTROL UNIT for..... CREDIT SALE TERMS: £3/10/- Deposit and 9 monthly payments of £2/5/3. H.P. TERMS: 27 Deposit and 9 monthly payments of 17/9.

(b) The MULLARD 5-10 and the "fidelity" PRE-AMPLIFIER-TONE CONTROL UNIT for..... CREDIT SALE TERMS: £4/15/- Deposit and 9 monthly payments of £2/14/7. H.P. TERMS: £29/9/- Deposit and 12 monthly payments of 17/6.

THE ABOVE PRICES ARE SUBJECT TO £1.6.0 EXTRA IF PARTRIDGE TRANSFORMER IS PREFERRED.

WHEN ORDERING PLEASE INCLUDE 7/6 to cover cost of Carriage and Insurance

TUNING UNITS
RADIO RECEIVERS

TUNING UNITS RADIO RECEIVERS

STERN'S "fidelity" PRE-AMPLIFIER-TONE CONTROL UNIT

"A design for the Music Lover"



This unit can be used with any Main Amplifier. Briefly it has inputs for all types of MICROPHONES, HIGH and LOW GAIN PICK-UPS and a RADIO TUNING UNIT. It incorporates (a) GRAM EQUALISING CONTROL, (b) STEPPUT FILTER, (c) Continuously variable BASS and TREBLE CONTROLS, a variable OUTPUT CONTROL which enables its use with any type of Microphone. Jack Sockets are incorporated for TAPE RECORD and TAPE REWIND BACK.

Used with the "5-10" the production is comparable to that normally associated only with the very expensive commercially made High Fidelity Amplifiers.

PRICE OF COMPLETE KIT OF PARTS £6.6.0

WE ALSO OFFER IT ASSEMBLED READY FOR USE £8 (plus 5/- Carr. & Ins.).

The ASSEMBLY MANUAL contains full specification and is available for 1/6.

SPECIAL PRICE

REDUCTIONS—WE OFFER

£11.11.0

£15.15.0

£14.0.0

£18.18.0

A COMPLETE KIT OF PARTS, STERN'S "HIGH QUALITY" 8-10 WATT AMPLIFIER



Has power supply available for Radio Tuning Unit.
Price of COMPLETE KIT OF PARTS £7.10.0
(plus 5/- Carr. & Ins.)

WE ALSO OFFER IT ASSEMBLED and READY FOR USE for £9.10.0
(plus 5/- Carr. & Ins.)

This amplifier has proved one of the most popular models yet offered to the HOME CONSTRUCTOR. It provides really excellent reproduction up to 8 watts, employing 6V6s in push-pull and incorporating negative feedback. Suitable for the use of both 3 and 15 ohm Speakers. The complete SPECIFICATION and BUILDING INSTRUCTIONS are available for 1/6.

"Wire-to-Wire" Diagrams are included and all Components are available separately.

SPECIAL CASH ONLY OFFER !!

This very attractive PORTABLE AMPLIFIER CASE together with a good quality GRAM AMPLIFIER and a matched 6in. P.M. SPEAKER, ALL FOR £8.7.6 ONLY
(plus 7/6 Carr. & Ins.)

The Amplifier consists of a 2 Stage design incorporating the modern B.V.A. valves types ECC83, EL34 plus EZ80 Rectifier and has separate BASS and TREBLE CONTROLS. The Portable Case will also accommodate almost any make of Autotransformer and is attractively finished in Maroon and Grey colour Rexine —WE ALSO SUPPLY SEPARATELY.

(a) The 2-stage (plus Rectifier) AMPLIFIER, £4/2/6.

THE FOLLOWING HIGH FIDELITY AMPLIFIERS ARE IN STOCK

STERN'S COMPACT "5-2" ... A 2-stage high sensitivity Amplifier having separate BASS AND TREBLE Controls and GRAM EQUALISING. Developed for high quality reproduction, includes separate Power Supply Unit with spare power available to drive Radio Tuner.

£8.16.0

THE DULCI MODEL D.P.A.10. A 10 watt, "Ultra Linear" High Fidelity Amplifier with £19.19.0

THE DULCI MODEL H11 ... A self powered AM/FM Tuning Unit combined with a "Hi Fi" Preamplifier Control Unit—all on one £29.3.10

THE ARMSTRONG MODEL A.10 Mk. II. With associate PREAMP-TONE CONTROL UNIT, this model is perfectly consistent with Armstrong's £32.0.0

very high reputation.

THE NEW LEAK "VARISLOPE" PREAMPLIFIER together with the TL12 plus AMPLI. £34.13.0

THE "VARISLOPE" is available separately for £15.15.0

THE ROGERS "JUNIOR". With associate PREAMP-TONE CONTROL UNIT. £26.0.0

THE RCA "ORTHOPHONIC". 12-20 watt, high fidelity Amplifier and associate PRE-AMPLIFIER TONE CONTROL UNIT. £41.0.0

HIRE PURCHASE and CREDIT TERMS are available on all models.

Illustrated and Descriptive leaflets are available. Send S.A.E.

F.M. TUNING UNITS BY MOST OF THE LEADING MANUFACTURERS.

(b) The PORTABLE CARRYING CASE..... £3/17/6
(c) 6in. P.M. SPEAKER..... 16/9

Carriage and insurance 4/- extra

We also have a smaller PORTABLE CASE ideal for Record Players. PRICE ONLY £3/3/- (plus 5/- Carr. & Ins.)

Attractively finished in high-grade Rexine and robustly constructed with initial measurements at 13½" x 15½" in. high

it will therefore accommodate all makes of Record Players including Autotransformers. An uncut baseboard is also supplied.



PIRANI HIGH VACUUM TEST EQUIPMENT

Manufactured by "W. G. PYE LTD." for
M.O.S. ATOMIC RESEARCH STATION

5, HARROW ROAD,
PADDINGTON, W.2.

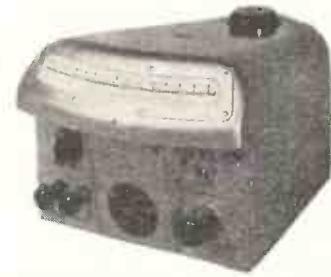
PADDINGTON 1008/9 and 0401
CABLES: HENELEC, LONDON



PIRANI BRIDGE UNIT



PIRANI CONTROL UNIT



PYE SCALAMP GALVANOMETER

(SOLD SEPARATELY £12-10-0)

THIS COMPLETE VACUUM TESTING EQUIPMENT (5 ITEMS AS SHOWN)
OFFERED BRAND NEW IN ORIGINAL CARTONS. WITH INSTRUCTION BOOK.

£33-10-0

CARR. PAID

(SPARE PIRANI GAUGE HEADS, EDWARDS TYPE M6, LESS CALIBRATOR, 15/- EACH)



PIRANI GAUGE
HEAD WITH
CALIBRATOR

QUARTZ CRYSTALS

FT243—FUNDAMENTALS

80 Types 5706.667 Kc/s to 8340 Kc/s. (in steps of 33.333 Kc/s).
120 Types 5675 Kc/s to 8.650 Kc/s. (in steps of 25 Kc/s).
(Excluding Types 7,000/7,300 and 8,000/8,300.)

5/- EACH

7,000 Kc/s to 7,300 Kc/s. in steps of 25 Kc/s. **7/6 EACH**
8,000 Kc/s to 8,300 Kc/s. in steps of 25 Kc/s.

Complete Sets of 80 Crystals £6. Complete Sets of 120 Crystals
£7/10/-.

FT2 41A—54th HARMONIC

80 Types 20 Mc/s to 27.9 Mc/s. (in steps of 100 Kc/s.). **5/-**

Excluding 24-25.9 Mc/s.
These Types 7/6 each.

Complete Set of 80 Crystals £6

100 Kc/s., Gold Plated D.T. Cut.....	15/-
100 Kc/s., Standard 10X.....	15/-
150 Kc/s., Two Pin Round.....	12/6
160 Kc/s., Two Pin 10X.....	12/6
200 Kc/s., FT241A.....	10/-
500 Kc/s., FT241A.....	10/-
500 Kc/s., Brook's Special Holder.....	15/-
2,500 Kc/s., Octal.....	10/-
5,000 Kc/s., Piezo 2-Pin Holder.....	12/6

P.O. Type 4B Ceramic

100 Kc/s., 819.6 Kc/s.....
163.9 Kc/s., 1,000 Kc/s..... **15/- EACH**

CERAMIC 2-PIN BANANA PLUG

15,010 Kc/s., 11,135 Kc/s., 16,455 Kc/s., 19,025 Kc/s.
15,110 Kc/s., 16,335 Kc/s., 16,700 Kc/s., 18,125 Kc/s. **7/6 Each**

TCS COLLINS TYPE 3-PIN. FT249

1,665.5 Kc/s., 1,700 Kc/s., 2,073.5 Kc/s., 1,962.5 Kc/s.,
2,072.5 Kc/s., 2,410 Kc/s. **7/6 Each**

MARCONI S.T.C. 10X, TYPE 2-PIN IN KILOCYCLES

10,166	10,534	10,878	11,851	1572.5	1727	1875	2090
10,189	10,545	11,437	11,876	1579	1740	1930	2118.25
10,233	10,557	11,463	12,685	1588.68	1761	1981	2196
10,245	10,567	11,501	12,600	1613.25	1764.5	2012	2261
10,300	10,622	11,526	1506.75	1650	1775	2055	2295
10,433	10,755	11,587	1554.5	1674.9	1780	2065.75	2312
10,445	10,767	11,751	1561.1	1680	1815	2067.5	2315
10,501	10,823	11,788	1566.5	1680.5	1835	2037.5	2430
10,511	10,856	11,814	1566.75	1700	1875	2089	

TEST EQUIPMENT

FERRANTI TESTVAC

High Speed Vacuum Tester 290/250 a.c. ... £10 10 0
BRAND NEW WITH DATA.

U.S.A. R.F. WATTMETER TS-87/AP

3 position 0-10/15/30 watts
Complete with photo-cell, 2 spare lamps and leads,
with transit case. BRAND NEW.

£10'10'0 P.P. 7/6

BC 906D

FREQUENCY METER Range 150-235 Mc/s
65'- P.P. 7/6

WAVE-GUIDE WATTMETER

Type VV8921 10 cm.

Complete in transit case

BRAND NEW **£5'10'0** P.P. 7/6

TEST SET 229

ADMIRALTY TYPE 600 Mc/s

Complete in transit case

BRAND NEW **£5'10'0** P.P. 7/6

FLUXMETER WY0023

RANGE 500/4,000 GAUSS.

This Instrument comprises 4½ in. Weston Meter and
Probe Unit for calibrating the field of Magnets. Brand
new in polished wooden case.

59'6 P.P. 3/6

Extra Probe Unit with 3 spare Measuring Gaps **7/6.**

CATHODE RAY TUBES

VCR139A	£1 15 0
VCR139A Mu-metal Screen	5 8
VCR897. Full T.V. picture (carz. 2/-)	22 0 0
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MU-METAL SCREENS for VCR97 or 817	10 0 0
VCR97. Slight-cut-off. Carr. 2/-	15 0 0
SPBL. Brand new	£1 10 0

AC/DC RADIO-GRAM CHASSIS**3-WAVEBAND SUPERHET**

(with internal aerial)

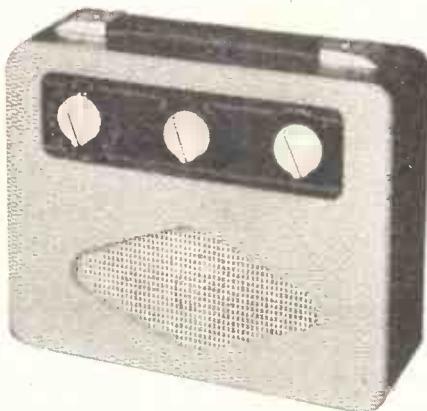
Medium wave, 187-575 m. Short. 16-50 m. Long. 900-2,000 m. With gram switching. Complete with five Marconi valves Type X109, W107, DH107, N108 and U107 and 7 x 4 Elliptical speaker. Ideal for portable radiogram. Chassis size 10 x 4 x 4 in.

£7 / 19 / 6 P.P. 5/-.

Also available with same line-up as above. 2 short wave. 11.27-31.9 m. 31.2-91 m. and medium wave 187-575 m. and Gram Switching.

£7 / 19 / 6 P.P. 5/-.

Over 300 different types B.V.A. and American valves in stock. Send for Lists.

**WALKIE-TALKIE**

Type "38" Trans/Receiver

Brand new complete with 2 pr. 'Phones, 2 Mikes, Junction Box, Canvas Bag, and 4 Section Aerial, and spare Valves.

65/- P.P. 5/-.**TRANSMITTER/RECEIVER**

ARMY TYPE 17 MK. II

Complete with Valves, High Resistance Headphones, Hand-mike and Instruction Book and Circuit.

Frequency Range: 44.0 to 61 Mc/s.

Range approximately: 3 to 8 miles.

Power requirements: Standard 120 v. H.T. and 2 v. L.T.

Ideal for Civil Defence and communications.

BRAND NEW 59'6

Calibrated Wavemeter for same 10/- extra

TRANSMITTER/RECEIVER SCR 522

Comprising the well known BC625 and BC624A Units. The complete unit is in very good condition having very useful parts including Relays, Transformers, Condensers, etc.

Less valves 45/-, carr. 6/-.

TRANSISTOR PUSH-PULL AUDIO AMPLIFIER

(200 MILLIWATTS OUTPUT)

Build this Push-Pull Amplifier which is ideal for Crystal or Magnetic Pick-up Amplification. Baby Alarm, Microphone Amplifier, etc.

Powered by 6-volt Dry Battery lasting for months.

Complete Kit of Parts including 4 Transistors and all Components with Circuit (less Speaker) and plastic case. £4/10/-.

TRANSISTORS**JUNCTION TYPE P-N-P**

(British Manufacture)

RED-SPOT 800 kc/s Audio Frequency.....	10/-
BLUE-SPOT 1.6 Mc/s Mixer and Frequency Changer	15/-
WHITE-SPOT 2.5 Mc/s R.F. and I.F. Amp.....	20/-

All Transistors are Tested and Guaranteed
N.B. The Red-Spot is similar to Mullard OC71

"EAVESDROPPER"**THREE-TRANSISTOR POCKET RADIO**

(No Aerial or Earth required)
Variable tuning, medium waves. Total cost, as specified, including Transistors, Transformers, Coils, Condensers and Battery, etc., with circuit and plastic case.
All items sold separately.

77'6 POST FREE

With single 'phone 82/6. With 'Acos Mike 90/-. With Min. Hearing Aid 90/-.

The New**"TRANSISTOR-8"**

Push-Pull Portable Superhet

Can be built for £11/10/-

This Portable 8 Transistor Superhet is tunable for both Medium and Long Waves and is comparable in performance to any equivalent Commercial Transistor Set
Simplified construction enables this set to be built easily and quickly into an attractive lightweight cabinet supplied.

TEN STAR FEATURES

- ★ 8 Specially selected Transistors
- ★ 250 Milliwatts Output Push-Pull
- ★ Medium and Long Waves
- ★ Internal Ferrite Rod Aerial
- ★ 7 x 4 Elliptical High Resistance Speaker
- ★ Drilled Plastic Chassis 8½ x 2½ in.
- ★ Point to Point wiring and practical layout
- ★ Economical. Powered by 7½ v. battery
- ★ Highly sensitive
- ★ Attractive lightweight contemporary case

We can supply all these items including Cabinet for £11/10/-
All parts sold separately

Send for circuit diagrams, assembly data, illustrations and instructions, and full shopping list 1/6.

N.B. Pair of XC101's supplied at additional cost of 40/-
Call and hear demonstration model
Further details in the August issue of "Radio Construction"

MINI-TWO**TWO-TRANSISTOR MINIATURE POCKET RADIO**

The smallest Transistor set offered on the market. Variable Tuning, Drilled Chassis, Plastic Case size 3in. x 2in. x ¾ in. Miniature Hearing Aid. 2 Transistors and all components including 1½ volt Battery, Circuits and full practical layout diagrams.

Total Cost **49'6 Complete.****TRANSISTOR SIGNAL TRACER**

Complete Kit with 2 Transistors Components, Phones and Circuit and plastic case.

42/6

COLLARO RC456

4-speed auto-changer. Latest type with crystal turnover pick-up. £3/19/6. P.P. 3/6.

TRANSISTOR SQUARE WAVE GENERATOR

Complete Kit with 2 Transistors. Components. Circuit and plastic case.

25/-

"HOMELIGHT"**2-TRANSISTOR PERSONAL PORTABLE**

Variable Tuning

We can supply all components including 2 Transistors, Diode, Resistors, Condensers and Miniature Hearing Aid and Plastic Case size 4½ x 2½ x 1½ and 1½ v. Battery FOR 52/6.

All items sold separately

DIODES

B.T.H. GERMANIUM	1/6
MULLARD OA74	2/6
IN21	3/6
IN22, IN23, IN21A	5/-

MODEL-MAKERS' MOTORS

Two types available 12 or 24 v. with ½" spindle 10/- each

RP24 10/- RP 25 12/6 RP 26 25/-

Brand new with valves, carr. 2/6.

6 v. VIBRATOR PACKS

Output 120 v. 30 mA, 12/6. Brand new.

RP24 10/- RP 25 12/6 RP 26 25/-

Brand new in original carton.

COLLARO RC/3/554

3-speed single player with crystal turnover pick-up type "T". £6/19/6. Carr. 3/6.

"YOU CAN RELY ON US"

Stockists of all Radio and Electronic components for manufacturers, laboratories, Educational authorities, and the amateur.



THE NEW AVO MULTIMINOR

This first-quality pocket instrument available from stock.

DC. $2\mu\text{A}$ to 1 A in 5 ranges, 0-1,000v in 7 ranges.
AC. 0-1,000v in 5 ranges. Resist. 0-2meg in 2 ranges.
10,000 Ohms per volt.

Price £9.10.0 Leather Case 32/6
or 9 payments of 23/3
or Deposit 63/4 and 6 payments of 22/2

ALL OTHER AVO INSTRUMENTS IN STOCK

RADIO SERVICING COMPANY

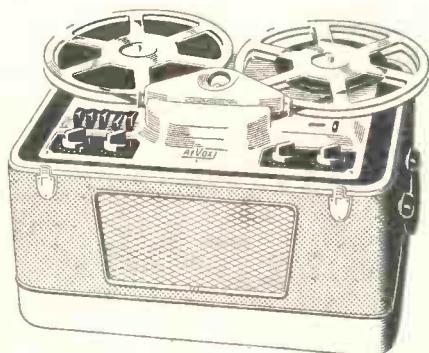
82, SOUTH EALING ROAD, LONDON, W.5

Next to South Ealing Tube (TURN LEFT) 9 to 6 p.m., Wednesday 1 o'clock.

Telephone : EAL. 5737

Come and Hear It

Last month we announced the coming of the superb new Revox Tape Recorder illustrated here. It is a precision made Swiss machine with a professional performance and specification. The price is 110gns. and brief details are given below. This machine is now available for demonstration at our showroom and we would urge you to come and hear this really superlative recorder.



Twin tracks. Frequency range 40-15,000 cps \pm 2db at $7\frac{1}{2}$ /sec. 3 inputs. 3 motors. Record and replay heads with separate amplifiers. Two channel mixing. Will take spools up to $10\frac{1}{2}$ in. diameter.

Quality Mart

8 DARTMOUTH PARK AVENUE,
LONDON, N.W.5
GULLIVER 1131

POLYTHENE

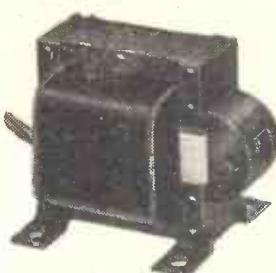
PROTECTIVE CAPS & PLUGS
FOR
STANDARD INTERNAL & EXTERNAL
THREADS
OR
SPECIAL MOULDINGS

AMPLEX APPLIANCES (KENT) LTD.

19 DARTMOUTH ROAD, HAYES, BROMLEY, KENT
(RAVENSBOROUGH 5531)

All export enquiries to
ANGLO NETHERLAND TECHNICAL EXCHANGE LTD.
3. TOWER HILL, LONDON, E.C.3.

A. C. SOLENOID type SAM/T.



Increased Performance
Continuous 14 ozs. at $\frac{3}{4}$ "
Instantaneous to $5\frac{1}{2}$ lbs.
Same dimensions as Type SA.

Larger and smaller sizes available. Greatly increased discounts for quantities. Also Transformers to 7kVA 3 Phase

R. A. WEBBER LTD.

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Phone: 74065

RADIO · TELEVISION · HI-FI · ELECTRONICS · RECORDERS

AUTO-CHANGERS

See us for your requirements or send for our latest list.

COLLARO
4-SPEED
MIXER AUTO-CHANGER

Latest model RC.456 incorporating auto and manual control enabling records to be played singly or automatically. Complete with Studio crystal pick-up and sapphire stylus. List £13.17.0. LASKY'S PRICE £8.19.6 Post 5/-.

COLLARO "JUNIOR"
4-SPEED MOTOR AND
PICK-UP

Collaro "Junior" 4-spd. motor and pick-up with HGP59 cartridge. Post 3/6.

£4.12.6

B.S.R.TU9, 4-speed motor and latest B.S.R. "full-fit" pick-up. Post 3/6. Motor only, 59/6, post 2/6. Pick-up only, 37/6, post 2/6.



Collaro 4/564 4-speed Single Player with Studio T.p.u. crystal cartridge and stylus. Automatic stop. LASKY'S PRICE £7.70 Carr. 3/6.

TRANSCRIPTION
TURNTABLES

COLLARO 4-speed Transcription Turntable, 4T200/PX, £19.10.0. Less pick-up £14.18/- Carr. 7/8

The New AVO MULTIMINOR. 19 ranges A.C. & D.C. 10,000 ohms per volt D.C. 1,000 ohms per volt A.C. Pocket size: 5 1/2 x 3 1/2 x 1 1/2 in. Complete with leads and clip £9.10.0. Post 3/6.

TRANSISTORS AT A
REASONABLE PRICE

R.F. P.N.P. Junction type, suitable for medium and low frequency oscillators, frequency changers and I.F. amplifiers 1.5 to 8 Mc/s (double spot—yellow & red) **21/-**

AUDIO P.N.P. Junction type, suitable for high gain and low frequency amplifiers, and for output stages up to 250 milliwatts, (double spot—yellow and green). **10/-** Post Free.

★ TESTED AND GUARANTEED EFFICIENT

★ HERMETICALLY SEALED and unaffected by temperature variations.

Full operating data and circuit diagrams for a simple receiver superhet, T.R.F., multi-vibrator, relaxation oscillator, audio amplifier, oscillators, signal tracers, etc., supplied with each Transistor.

MULLARD TRANSISTORS

OC70 or OC71 OC 72 OC16

21/- 30/- 60/-

BRIMAR TRANSISTORS

TS1 12/6. TS2 12/6. TS3 15/-

TS4 27/6. TP1 or TP2 40/-

TJ1 7/6. TJ2 7/6. TJ3 13/6.

LASKY'S TRANSISTOR SUPERHET
TUNER FOR HOME CONSTRUCTION
ON PRINTED CIRCUIT

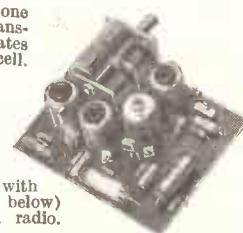
Uses three R.F. Transistors and one Germanium Diode, three I.F. transformers. Ferrite rod aerial. Operates on one 6 v. battery and one 1.5 v. cell. Printed Circuit, 3 1/2 in. x 3 1/2 in.

CAN BE BUILT **£5.12.9**

FOR. Post 3/6. Full details and illustrations post free on request.

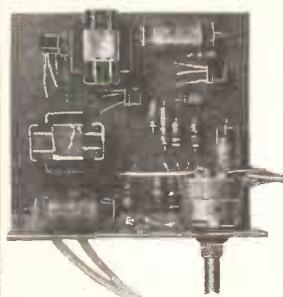
Demonstrations at both addresses.

NOTE.—This Tuner in conjunction with our Transistor Amplifier (see below) makes an excellent Transistorised radio. Cabinets available.



LASKY'S TRANSISTOR AMPLIFIER KIT

(200 milliwatts) For construction on a Printed Circuit



All components available separately.

SUB-MIN. TRANSISTOR TRANSFORMERS **4/6** Post 1/- 45-1 ratio each.

ALL TRANSISTOR COMPONENTS. Trans., midget, min. and sub-min. Coils, Ferrite Rods, sub-min. Condensers, etc.

PICK-UP BARGAIN
"RONETTE" Lightweight Crystal Pick-up with 2 cartridges. LASKY'S PRICE **45/-** Post 2/6.

ACOS HGP37 p.u. Cartridges, l.p. and standard, complete with stylus. List 41/7. LASKY'S PRICE **18/-** Post 1/-.

Size: 3 1/2 x 3 1/2 in. Height can be under 1 in. Uses our new hermetically sealed Transistors and operates from 6-volt battery. Output impedance 3 ohms.

FULL DETAILS, CIRCUIT
DIAGRAM AND SHOPPING
LIST 1/- post free.

COMPLETE KIT including 4 Transistors, all brand new components, latest T.C.C. miniature condensers, printed circuit and full instructions. **79/6** Post 3/6.

DEMONSTRATIONS AT
EITHER OF OUR ADDRESSES



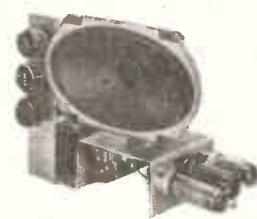
Teletron "Companion"

3-T TRANSISTOR POCKET RADIO. T.R.F. circuit covering medium and long waves, with balanced armature output. Ferrite aerial. Note small size: 4 1/2 x 3 x 1 in. You can build this novel transistorised pocket receiver for only 89/6 Post 2/6. Full instructions and price list. All components available separately.

LASKY'S
RADIO

STOP PRESS BARGAIN

12in. TRUVOX SPEAKERS, 15 ohms, 10 watts. LASKY'S PRICE **45/-** Post 3/6.

LASKY'S 4-WATT
PORTABLE GRAM
AMPLIFIER

Will suit any type of crystal or magnetic pick-up. Uses 3-valves: EL84 output, LE3 and EZ80 rect. Speaker and controls are completely separate and can be mounted as shown or on anywhere in cabinet where most suitable.

COMPLETE with 3 valves and knobs, less Speaker. **79/6** Carr. 5/-.

7 x 4 in. Elliptical Speaker, if required, 19/6 extra.

Details and circuit diagram post free on request.

LASKY'S PORTABLE
GRAM AMPLIFIER KIT

2 watts. Note small dimensions approx. 6 1/2 x 3 1/2 in. max. height 5 in. Uses EL84 output and 6X4 rectifier, double-wound transformer, tone control, output transformer, etc. Built on a T.C.C. PRINTED CIRCUIT which greatly simplifies construction and eliminates wiring errors.

COMPLETE KIT, including valves, printed circuit, full instructions, less Speaker Carr. 2/6. **58/-**

7 x 4 in. Elliptical Speaker, if required, 19/6 extra.

★ H.P. TERMS and CREDIT SALES available on certain items.

MORE MONEY-SAVING LASKY BARGAINS ON NEXT PAGE

EVERYTHING FOR HOME CONSTRUCTOR & SERVICEMAN

TRUVOX 'SENIOR' SPEAKER DRIVING UNIT (pressure type)
Power handling cap. 15 watts peak.
With 12ft. cinema horn reproduces down to 17 cps.

List £7/15/- Lasky's Price 59/6
Carr. 5/-

MOVING COIL P.M. SPEAKERS

2½in. 17/6.	3in. and 3½in. 19/6
5in. 19/6.	6½in. 17/6. 8in. 21/-
10in. 29/6.	12in. 29/6.
6½in. with transformer.....	21/-
7×4in. Elliptical.....	19/6
10×7in. Elliptical.....	32/6

SPECIAL OFFER DUAL CONCENTRIC SPEAKERS (15 in.)

High Fidelity. 25 watts, 15 ohms imp., full freq. range 20 c.p.s. to 17,000 c.p.s., resonance 20 c.p.s. Complete with crossover unit. List £27/4/6.

LASKY'S PRICE £16.19.6

Carr. 7/6 plus 30/- for wood packing case (returnable).

6-VALVE RADIOPHONIC CHASSIS COMPLETE WITH VALVES

Famous Manufacturer's Surplus. 6-valve 3-wave Superhet. 13-50 m. short. 200-550 m. medium. 1,000-2,000 m. long. Brand new Mullard valves ECH42, EF41, L63, EB41, 6V6, g.e., EZ40 and finest quality components. Gram., switch, 465 Kc/s I.F. tone control, three-colour dial. Overall size 13½ x 6in. height 12in. Aperature required for dial and controls 11 x 3½in. **COMPLETE WITH VALVES**, output units, knobs, etc.

LASKY'S PRICE £10/19/6

Carriage and packing 7/6 extra

5-VALVE RADIOPHONIC CHASSIS COMPLETE WITH VALVES

3-wave superhet. 16-50 m. 200-550 m. 1,000-2,000 m. Brand new Mullard and Mazda valves—6C9, 6F15, GLD20, N108, U107. Overall dim. 13in. long, 6in. deep, 7in. high approx. for A.C. mains 200/250 v. **LASKY'S PRICE** 7 GNS.

complete with all valves.

Carr. and Pkg. 7/6 extra

Price without valves £5/4/-

HI-FI ELECTROSTATIC SPEAKERS ("TWEETERS")

Easy to fit to any radio, TV receiver or amplifier. Full data and circuit diagram supplied. LSH75. For outputs up to 6 watts, 8/-. LSH518. For outputs of 10-12 watts, 12/6. LSH100. For outputs up to 20 watts, 14/-. Post free

LPH65. MOVING COIL TWEETER.
Imp. 5.5 ohms, freq. range 2,000-2,200 50 c/s. For outputs up to 8 watts. 2½in. diameter. All post free. 39/6.

SPEAKER COVERINGS. Large stocks of Tygan and "Someweave" Speaker Coverings. Any size piece cut. Send for samples and prices.

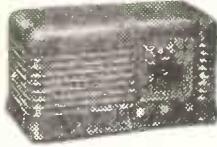
MAKERS' SURPLUS TV COMPONENT BARGAINS

WIDE ANGLE 38 mm.	
Line E.H.T. trans., ferro-cube core, 9-16kV.	25/-
Scanning Coils, low Imp. line and frame	25/-
Ferro-cube cored Scanning Coils and Line Output Trans., 10-15 kV., EY51 winding. Line Trans. Complete with circuit diagram, the pair	50/-
Frame Output Transformer.....	6/6
Scanning Coils, low Imp. line and frame	17/6
Frame or line blocking osc. transformer	4/6
Focus Magnets Ferrox-dure.....	19/6
P.M. Focus Magnets Iron Cored.....	12/6
Duomag Focalisers.....	22/6
300 mfd. Smoothing Chokes	15/-
Electromagnetic focus coil with combined scan coils	25/-

STANDARD 38 mm.	
Line Output Transformer 6.9 kV. E.H.T. and 6.3 v. winding Ferro-cube	19/6
Scanning coils. Low Imp. line and frame	12/6
Diode by Igranic	14/6
Frame or line blocking oscillator transformer	4/6
Frame output transformer	7/6
Focus Magnets	
Without Vernier	12/6
With Vernier	17/6
Focus Coils, Electro-magnetic.....	12/6
200 mfd. Smoothing Chokes	10/6

INEXPENSIVE EASILY BUILT RADIO SETS

Lasky's Radio Constructors' Parcels contain everything to build up-to-date and very efficient sets at low cost.



PARCEL No. 1

Contains everything to build a 4-valve 3-wave superhet for 200/250 A.C. mains. Uses 6K8, 6K7, 6Q7, 6V6 valves. Attractive wood cabinet, walnut veneer, or plastic cabinet as illustrated. Size 12×6½×5½in. deep. **CAN BE BUILT FOR** £7/19/6 Carr. and packing 2/6

PARCEL No. 2

Contains everything to build a T.R.F. 3-valve set for 200/250 A.C. mains, medium and long waves. Uses 6K7G, 6J7, 6V6 and metal rectifiers. Neat plastic cabinet, walnut or ivory finish, or wood cabinet. Size 12×6½×5½in. deep.

CAN BE BUILT FOR £5/10/0

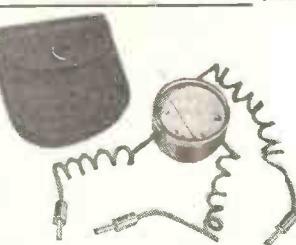
Carriage and packing 2/6.

INSTRUCTION BOOK for either above sets 1/- post free.

CABINETS ONLY, plastic or wood, 17/6.

Post 2/6

All components available separately



LASKY'S (HARROW ROAD) LTD.

42 TOTTENHAM COURT
ROAD, W.1.

Nearest Station Goodge Street
MUSEUM 2605.

ALL MAIL ORDERS TO HARROW ROAD PLEASE

BAND III. Very large selection Band III Converters, Aerials, Turret Tuners, Co-ax. Cable.

CO-AX. CABLE, 80 ohms semi-airspaced, finest quality, stranded. Per yd. 9d. Doz. yd. 7/6. Any length supplied.

16" METAL CONE C.R.T.

Type T901. Not "seconds" but brand new and perfect in original cartons. Gives large 11×14½in. picture. Guaranteed by us for 3 months. Listed at £23/0/-

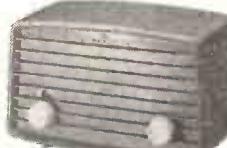
LASKY'S PRICE £8/9/6

Carr. and Insur. 22/6 extra
Masks, Anti-Corona, Bases and Ion Traps available.

17in. C.R. TUBES

Rectangular, aluminised or ion trap 0.3 heater. Brand **£12/19/6** new and unused. Carr. and Insur. 22/6

LASKY'S NEW MIDGET T.R.F. CONSTRUCTOR PARCEL



CAN BE BUILT FOR ONLY 99/6

Post & Pkg. 5/-

Handsome contemporary design case, overall size 8in. wide, 4in. deep, 5in. high. 2 latest double-purpose valves EBF0 and ECL80, contact cooled rectifier. For A.C. mains 200-250 v. Med. and long wave, 5in. P.M. speaker. Plastic cabinet in cream, pastel green, pink, blue. FULL DATA, instructions, circuit diagram and shopping list, 1/6 post free.

All components available separately.

CABINET only, as illus., 12/6 plus 4/6 post and pkg.

POCKET VOLT TEST METERS

Two ranges, D.C. 0-250 v. and 0-25 v. Complete with leads in canvas case.

Lasky's Price 12/6

Plus 2/6 post and packing. In leather case 1/6 extra.

LASKY'S RADIO

ALL-DRY POWER UNITS

By Decca. Suitable for any battery radio using 1R5, 1T4, etc., 67½ volts H.T., 1½ volts L.T. For full details see our November advertisement

LASKY'S PRICE 29/6
Post 3/6

FERRITE RODS

Large selection of Ferrite Rods, all lengths, in stock. Price, per rod, 2/6 to 3/6.

MAINS TRANSFORMERS

All 200-250 v. 50 c.p.s. primary finest quality, fully guaranteed.

MBA/3. 350-0-350 v 80 mA. 6.3 v. 4 a. 5 v. 2 a. Both filaments tapped at 4 volts.

MBA/7. 250-0-250 v. 80 mA. 6.3 v. 3 a. 5 v. 2 a. Both filaments tapped at 4 volts.

AT13. Auto trans. 0-10-120. 200-230-240 v. 100 watts.

MT.341. Tapped input 250-0-250, 120 mA. 6.3 v. 5 amps, fully shrouded.

27/6

FILAMENT TRANSFORMERS

All 200-250 v. 50 c.p.s. primary, finest quality, fully guaranteed. 6.3 v. 1.5 amp..... 5/11

6.3 v. 3 amp..... 9/6

0-30 v. 2 amp. tapped voltages 19/6

GERMANIUM CRYSTAL DIODES

GEX.00 1/6. GEX.34 3/6. WG5 3/6. GEX.54 and OA74 5/-. GD3 3/6. GD4 3/6. CG12E 5/-

20,000 VALVES IN STOCK

Here are a few examples of brand new surplus and imported valves:

EB91 7/6 EV41 10/6 EY80 14/6

EB41 7/6 EF80 10/6 EZ40 8/6

EABC80 10/- EF85 10/6 EZ80 8/6

EAF42 10/- EF86 12/6 PCF82 12/6

EBC41 10/- EF88 10/- PCC80 12/6

ECC85 10/- 6K8 10/6 PL81 13/6

ECC88 15/- 6V6 8/6 PL82 10/6

ECC83 9/- 6K7 5/6 PVS3 11/6

ECC82 9/- 6Q7 10/- PVS4 10/6

ECC81 9/- 6L7 8/6 PVS1 10/6

ECC87 8/6 5Z4 9/6 PVS2 10/6

12A.U7 8/6 DAF86 10/- PY83 10/6

12A.X7 8/6 DL96 10/- GAT6 7/6

EB89 10/6 DK96 10/- GAT7 7/6

ECP82 11/6 DM70 9/- 384 9/-

ECH81 11/6 EV51 12/6 IT4 9/-

ECL80 10/6 EC84 11/6 IR5 7/6

Also full stocks of B.V.A. Valves and C.R. Tubes at the new lower list prices.

WRITE FOR COMPLETE LIST

SPECIAL RECTIFIER OFFERS

RM.0, 125 v. 30 m/a ... 4/11

RM.1, 125 v. 60 m/a... 5/11

RM.2, 125 v. 100 m/a... 6/6

RM.3, 125 v. 120 m/a... 7/6

RM.4, 250 v. 125 m/a... 16/-

RM.5, 250 v. 150 m/a... 21/-

Post extra

All makes and types in stock.

Send to us for your requirements.

Open all day
Saturday. Early closing Thursday
(both addresses)

**SELENIUM
RECTIFIERS**

L.T. Types

2/6 v.	1/2 a.h.w.	1/9	
6/12 v.	1/2 a.h.w.	2/9	
F.W. Bridge			
6/12 v. 1 a.	4/11	6/12 v. 1 a.	19/9
6/12 v. 2 a.	8/9	6 v. 2 a.	27/9
6/12 v. 3 a.	11/9	6/12 v. 2 a.	29/9
6/12 v. 4 a.	14/9	6/12 v. 4 a.	38/9
6/12 v. 6 a.	19/9	6/12 v. 4 a.	56/9
6/12 v. 10 a.	25/9	Above ready for use with mains and output leads. Cases well ventilated and finished in stoved blue hammer. Carr. and pack- ing 3/6.	
H.T. Type H.W.			
120 v. 40 mA.	3/9		
250 v. 50 mA.	5/9		
250 v. 80 mA.	7/9		
250 v. 150 mA.	9/9		
300 v. 250 mA.	12/11		

**ASSEMBLED
CHARGERS**

6 v. 1 a.	19/9
6/12 v. 1 a.	27/9
6/12 v. 2 a.	29/9
6/12 v. 3 a.	38/9
6/12 v. 4 a.	56/9
6/12 v. 6 a.	56/9
6/12 v. 10 a.	25/9
Above ready for use with mains and output leads. Cases well ventilated and finished in stoved blue hammer. Carr. and pack- ing 3/6.	
H.T. Type H.W.	
120 v. 40 mA.	3/9
250 v. 50 mA.	5/9
250 v. 80 mA.	7/9
250 v. 150 mA.	9/9
300 v. 250 mA.	12/11

BATTERY CHARGER KITS

Consisting of Mains Transformer F.W. Bridge, Metal Rectifier, well ventilated steel case. Fuses, Fuse-holders, Grommets, panels and circuit. Carr. 2/6 extra.

6 v. or 12 v. 1 amp.	22/9
6 v. 2 amps.	25/9
6 v. or 12 v. 2 amps.	31/6
6 v. or 12 v. 4 amps.	53/9

BATTERY CHARGER KIT

Consisting of F.W. Bridge Rectifier 6/12 v. 5 a. Mains Trans., 0-9-15 v. 6 a. output, and ammeter. Only 49/9. Post 3/-.

All for A.C. Mains 200-250v., 50 c/s.
Guaranteed 12 months

Assembled 6v. or 12v. 4 amps.

Fitted Ammeter and selector plug for 6 v. or 12 v. Louvred metal case, finished attractive hammer blue. Ready for use with mains and output leads. Double Fused. Only 47/9 Carr. 3/6. 75/- Ready for use with mains and output leads. Carr. 3/9. Or Deposit 13/9 and five monthly payments 13/9.

MANUFACTURERS: SURPLUS TRANSFORMERS. Primary 200-240-250 v. Drop through type 250-0-250 v. 70 mA. 6.3 v. 3 a. 11/9. Postage 2/9.

EX GOVT. SMOOTHING CHOKES

300 mA., 20 H. 150 ohms	19/6
250 mA., 5 H. 50 ohms	12/9
150 mA., 10 H., 50 ohms	10/11
100 mA., 10 H., 100 ohms	6/9
100 mA., 5 H., 100 ohms, tropicalised	3/11
80 mA., 10 H., 350 ohms, tropicalised	3/11
50 mA., 50 H., 1,000 ohms	6/9

EX GOVT. CASES. Well ventilated, black crackle finished, undrilled cover. Size 14 x 10 x 8½in. high. IDEAL FOR BATTERY CHARGER OR INSTRUMENT CASE. COVER COULD BE USED FOR AMPLIFIER. Only 9/9, plus 2/9 post. Size 13½in. x 8in. x 6½in. with undrilled perforated cover finished in stoved grey enamel, 7/9, plus 2/9 post.

SPECIAL OFFERS. Small 2 gangs .0005 mfd., 4/9. Electrolytics 32-32-32 mfd. 250 v., 2/9 each or in lots of six, 2/3 each.

RE-ENTRANT SPEAKERS, 8 watt, suitable for above, 25/- each.**5 CORE FLEX.** Henleys circular rubber 14/36. Each lead colour coded. 1/6 yard.**EX GOVT. MAINS TRANSFORMERS**

All 200-250 v. 50 c/s input.	
120-0-120 v. 40 mA.	5/9
250-0-250 v. 60 mA., 6.3 v. 3 a., 6.3 v. 1 a. Potted 4/1-3½-3in.	11/9
Pr. 0-110-200-230-250 v. 275-0-275 v. 100 mA., 6.3 v. 7 a., 5 v. 3 a.	18/9
230-0-230 v. 80 mA., 12.6 v. 1.5 a. 5 v. 2 a.	11/9
400-0-400 v. 250 mA. 5 v. 2 a., 5 v. 2 a. 12.5 v. 3 a., 5 v. 3 a.	18/9
	12/9

R.S.C. BATTERY TO MAINS CONVERSION UNITS

Type BM1. An all dry battery eliminator. Size 5½ x 4½ x 2in approx. Completely replaces batteries supplying 1.4 v. and 90 v. where A.C. mains 200-250 v. 50 c/s. is available. Suitable for all battery portable receivers requiring 1.4 v. and 90 v. This includes latest low consumption types. Complete kit with diagram. 39/9 or ready for use 46/9.

JUNCTION TRANSISTORS for Audio stages. Only 7/6. For R.F. 17/6.

MINIATURE MOTORS. 24/28 v. D.C. or A.C. Size only 2½ x 1½in. Spindle 1½in. long, ¼in. diam. Made by Hoover Ltd., Canada. Price only 9/9.

M.E. SPEAKERS. 2-3 ohms R.A. 8in. Field 600 ohms, 11/9.

Type BM2. Size 8 x 5½ x 2½in. Supplies 120 v., 90 v., and 60 v., 40 mA. and 2 v. 0.4 a. to 1 amp. fully smoothed THEREBY COMPLETELY REPLACING BOTH H.T. BATTERIES AND L.T. 2V. ACCUMULATORS when connected to A.C. mains supply 200-250 v. 50 c/s. SUITABLE FOR ALL BATTERY RECEIVERS normally using 2 v. accumulator. Complete kit with diagrams and instructions, 49/9, or ready for use, 59/6.

**R.S.C. TRANSFORMERS****FULLY GUARANTEED.****MAINS TRANSFORMERS**

Primaries 200-230-250 v. 50 c/s.

FULLY SHROUDED UPRIGHT MOUNTING

250-0-250 v. 60 mA., 6.3 v. 2 a., 5 v. 2 a.

350-0-350 v. 70 mA., 6.3 v. 2 a., 5 v. 2 a.

250-0-250 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.

250-0-250 v. 100 mA., 6.3 v. 6 a., 5 v. 3 a.,

for R1355 conversion

200-0-300 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.

300-0-300 v. 130 mA., 6.3 v. 4 a., 5 v. 3 a.,

1 a., suitable for Mullard 510 Amplifier

375-0-375 v. 150 mA., 6.3 v. 4 a., 5 v. 2 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 2 a., 6.3 v.

2 a., 5 v. 3 a.

425-0-425 v. 200 mA., 6.3 v. 4 a., c.t.,

6.3 v. 4 a., c.t., 5 v. 3 a., suitable

Williamson Amplifier, etc. 49/9

TOP SHROUDED DROP-THROUGH TYPE

260-0-260 v. 70 mA., 6.3 v. 2 a., 5 v. 2 a.

350-0-350 v. 80 mA., 6.3 v. 2 a., 5 v. 2 a.

250-0-250 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.

300-0-300 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

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350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.

350-0-350 v. 150 mA

R.S.C. A10 ULTRA LINEAR 30 WATT AMPLIFIER

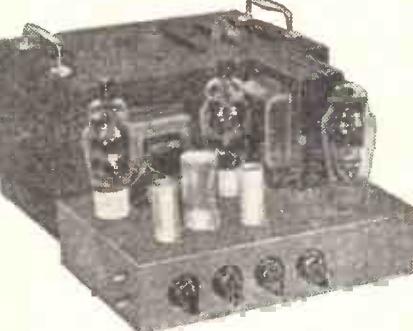
NEW 1957 DESIGN, HIGH FIDELITY PUSH-PULL UNIT EMPLOYING SIX VALVES. EF86, EF86, ECC83, 807, 807, GZ34. Tone Control Pre-amp stages are incorporated. Sensitivity is extremely high. Only 12 millivolts minimum input is required for full output. **THIS ENSURES THE SUITABILITY OF ANY TYPE OR MAKE OF MICROPHONE OR PICK-UP.** Separate Bass and Treble controls give both "lift" and "cut" with ample tone correction for long playing records. An extra input with associated vol. control is provided so that two separate inputs such as "mike" and gram., etc., etc., can be simultaneously applied for mixing purposes. **AN OUTPUT SOCKET WITH PLUG IS INCLUDED FOR SUPPLY OF 300 v. 20 mA. AND 6.3 v. 1.5 a. FOR A RADIO FEEDER UNIT.** Price in kit form with easy-to-follow wiring diagrams.

Cover as illustrated

Only 10 G.N.S.

car. 10/-.

Or Factory built with 12 months' guarantee £12/19/6. TERMS ON ASSEMBLED UNITS. DEPOSIT 35/9 and 9 monthly payments



EXPORT ENQUIRIES INVITED

Type 807 output valves are used with High Quality Sectionally wound output transformer specially designed for Ultra Linear operation. Negative feedback of 20 D.B. in main loop. **CERTIFIED PERFORMANCE FIGURES ARE EQUAL TO MOST EXPENSIVE UNITS AVAILABLE.** Frequency response ± 3 D.B., 30-20,000 c/s., Tone Controls, ± 12 D.B. at 50 c/s., ± 12 D.B. to ± 6 D.B. at 12,000 c/s., Hum and noise 70 D.B. down. Good quality reliable components used. Chassis finish blue hammer. Overall size 12 x 9 x 9in. approx. Power consumption 150 watts. For A.C. mains 200-230-250 v. 50 c/s. Outputs for 3 and 15 ohm speakers. **EQUALLY SUITABLE FOR THE CONNOISSEUR OR FOR LARGE HALLS, CLUBS, OR OUTSIDE FUNCTIONS. IDEAL FOR USE WITH MUSICAL INSTRUMENTS SUCH AS STRING BASS, ELECTRONIC ORGAN, GUITAR, etc. FOR DANCE BANDS, GARRISON THEATRES, etc.**

Microphones, Speakers, 12 v. Rotary Converters, etc., at keen cash prices or on terms with amplifiers.

18/9 extra.

Only 10 G.N.S.

car. 10/-.

Or Factory built with 12 months' guarantee £12/19/6. TERMS ON ASSEMBLED UNITS. DEPOSIT 35/9 and 9 monthly payments

EXPORT ENQUIRIES INVITED

LT/45 HIGH QUALITY TAPE DECK AMPLIFIER

COMPLETE WITH POWER PACK and OSC. STAGE. Suitable for Collaro, Lane, Truvox, Aspin, Brennel, etc., etc. State make of Deck when ordering. Chassis size 12-7-3in. Overall size 12-7-6½in. For 200-250 v. 50 c/s. A.C. mains. Output for standard 9-3 ohm speaker. Only 12 millivolts input required for full recording. Only 2 millivolts minimum output required from recording head. Magic Eye recording level indicator. Provision for feeding P.A. amplifier. Negative feed-back equalisation. Linear frequency response ± 3 D.B. 50-11,000 c/s. Facilities for recordings at 15in. 7½in. or 3½in. per second. Automatic equalisation at the turn of a knob. When switching from record to playback position automatic demagnetisation of heads is assured. Separate gain and output controls. Valves type ECC83, ECC83, EL84, EZ80, EM34. Output 4 watts.

Ready for use 12 G.N.S. Carr. 7/6

car. 7/6

Unit supplied with maker's 12 months' guarantee. We know of no other make which represents the same exceptional value. Leaflet 6d. Special Offer. Collaro Deck, LT45, 6½in. speaker, and Studio "Mike" 29 gns. Carr. 10/-.

COLLARO JUNIOR 4 SPEED RECORD PLAYER with separate pick-up having dual point sapphire stylus. Brand new, cartoned. For 200-250 v. A.C. mains only £4/17/6. Carr. 3/6.

COLLARO JUNIOR 4 SPEED RECORD PLAYER

For 200-250 v. 50 c.p.s. A.C. Mains. Overall size only 6½ x 4½ x 2½in. Fitted vol. and Tone Control with mains switch. Designed for use with any kind of single player or record changing unit. Output for 2-3 ohms speaker. Guaranteed 12 months. Only 49/9. Carr. 3/9.

LG3 MINIATURE 3 WATT GRAM. AMPLIFIER

For 200-250 v. 50 c.p.s. A.C. Mains. Overall size only 6½ x 4½ x 2½in. Fitted vol. and Tone Control with mains switch. Designed for use with any kind of single player or record changing unit. Output for 2-3 ohms speaker. Guaranteed 12 months. Only 49/9. Carr. 3/9.

R.S.C. A5 4-5 WATT HIGH GAIN AMPLIFIER

A highly sensitive 4-valve quality amplifier for the home, small club, etc. Only 50 millivolts input is required for full output so that it is suitable for use with the latest high-fidelity pick-up heads in addition to all other types of pick-ups and practically all makes. Separate Bass and Treble controls are provided. There is full long playing record equalisation. Hum level is negligible being 7½ D.B. down 15 D.B. of negative feedback is used. H.T. of 300 v. 26 mA. and L.T. of 6.3 v. 1.5 a. is available for the supply of a Radio Feeder Unit or Tape Deck pre-amplifier. For A.C. mains input of 200-230-250 v. 50 c/s. Output for 2-3 ohm speaker. Chassis is not alive. Kit is complete in every detail and includes fully punched chassis (with baseplate) with the blue hammer finish, and point-to-point wiring diagrams and instructions. Exceptional value at only £4/15/-, or assembled ready for use 25/- extra, plus 3/6 carriage. Or Deposit 22/- and five monthly payments of 22/- for assembled unit.

R.S.C. A7 3-4 WATT QUALITY AMPLIFIER

A highly sensitive 4-valve amplifier using negative feedback and having an excellent frequency response. Pre-amplifier and Tone Control stages are incorporated with separate Bass and Treble controls giving full tone compensation for long playing records. Suitable for any kind of pick-up including latest high fidelity types. H.T. of 250 v. 20 mA. and L.T. 6.3 v. 1 a. available for supply of Radio Feeder Unit, etc. ONLY 40 millivolts input required for full output. Fully isolated chassis with baseplate. For A.C. mains 200-250 v. 50 cycles. Output for 2-3 ohm speaker. Complete kit of parts with point-to-point wiring diagrams and instructions. Only 23/15/-, corr. 3/6, factory built 22/6 extra. Or Deposit 18/6 and five monthly payments of 18/6 for assembled unit.

COLLARO RC457 4 SPEED AUTO-CHANGERS

With studio pick-up with turnover head. **BRAND NEW.** Cartoned, latest model. For 200-250 v. 50 c.p.s. A.C. mains. Very limited number at only £8/19/6. Carr. 5/6.

COLLARO RC54 3 SPEED AUTO-CHANGER

As above unit but for normal 3-speed requirements. Brand new cartoned but for 110 v. 50 c.p.s. A.C. mains. So that the unit can be operated from normal 200-250 v. A.C. mains we are supplying free with every changer a suitable auto-transformer with input and output voltages clearly marked. Limited number only. 7 gns. Carr. 5/6.

PORTABLE CABINETS.

Excepionally attractive design. Finished in two tone rexine. Provision for speaker and amplifier. Inside dimensions 17½ x 12in. Carrage 5/-. Depth 7in. plus lid 1¼in. Carrage 5/-. 59/6 SPECIAL OFFER. Above cabinet LG3 Amplifier 6½in. speaker and Collaro Junior 10 G.N.S. with RC457. 14 G.N.S. Carr. 8/6.

LINEAR L45 MINIATURE 4/5 W. QUALITY AMPLIFIER.

Suitable for use with Garrard, B.S.R. or any other record playing unit and most microphones. Total negative feedback 12 DB. Separate Bass and Treble controls. For A.C. mains input of 200-250 v. 50 c.p.s. Output for 2/3 ohm speaker. Three valves used. Metal valves used. Size 7in. x 5in. high. Chassis fully isolated from mains. Guaranteed 12 months. Only 25/19/6. Or Deposit 22/- and five monthly payments of 22/- Send S.A.E. for leaflet.

PLESSEY DUAL CONCENTRIC 12in. P.M. SPEAKERS

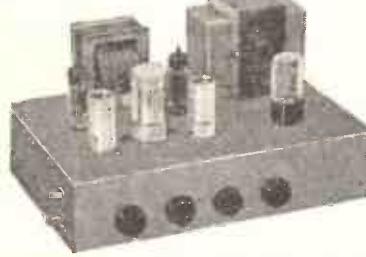
(15 ohms), consisting of a high quality 12in. speaker of orthodox design supporting a small elliptical speaker ready wired with choke and condensers to act as tweeter. This high fidelity unit is highly recommended for use with our A5 or similar speaker. Rating is 10 watts. Price on 25/17/6. Or Deposit 13/- and nine monthly payments of 13/-.

PLESSEY DIATONIC 10-WATT HIGH FIDELITY AMPLIFIER. Incorporating pre-amp. For A.C. mains input 200-230-250 v. 50 c.p.s. A compact attractively finished unit with two separately controlled inputs, and outputs for 3 and 15 ohms speakers. Separate Bass and Treble controls. Five latest type miniature Mullard valves. Only 12 Gns. Send S.A.E. for leaflet and credit terms.

W.B. STENTORIAN HIGH FIDELITY P.M. SPEAKERS. HF1012, 10 watts, 15 ohm (or 3 ohm) speech coil. Where a really good quality speaker at a low price is required, we highly recommend this unit with an amazing performance. £24/10/0. Please state whether 3 ohm or 15 ohm required.

P.M. SPEAKERS. 2-3 ohm 5in. Goodmans 17/9. 7in. Elliptical 19/9. 6½in. Rola, 19/9. 8in. Rola, 19/9. 8in. Goodmans 21/9. 10in. R.A. 28/9. 10-6in. Elliptical 28/9. 12in. Plessey 29/11. 12in. Plessey 3 ohms, 10 watts, 12,000 lines, 59/6.

All ULTRA LINEAR 12-14 WATT AMPLIFIER



NEW 1957 DESIGN HIGH-FIDELITY PUSH-PULL AMPLIFIER WITH "BUILT-IN" TONE CONTROL PRE-AMP. STAGES

Two input sockets with associated controls allow mixing of "mike" and gram. as in A10. High sensitivity. Includes 5 valves, ECC83, ECC83, EL84, 5Y3, High Quality sectionally wound output transformer, specially designed for Ultra Linear operation, and reliable small condensers of current manufacture. INDIVIDUAL CONTROLS FOR BASS AND TREBLE "Lift" and "Cut". Frequency response ± 3 D.B. 30-30,000 c/s. Six position feedback loops. Hum level 60 DB down ONLY 23 millivolts. INPUT required for FULL OUTPUT. Suitable for use with all makes and types of pick-ups and microphones. Comparable with the very best designs. For STANDARD OR LONG PLAYING RECORDS. For MUSICAL INSTRUMENTS such as STRING BASS, GUITARS, etc. OUTPUT SOCKET with plug provides 300 v. 30 m.a. and 6.3 v. 1.5 a. For use with a RADIO FEEDER UNIT. Size approx. 12-9-7in. For A.C. mains 200-230-250 v. 50 c/s. Output for 3 and 15 ohm speakers. Kit is complete to last nut. Chassis is fully punched. Full instructions and point-to-point wiring diagrams supplied. Despite improved performance due to use of latest miniature valves price remains as previous and except input now standard.

Only 8 G.N.S. or factory built 45/- extra.

Carr. 10/-. If required louvred metal cover with 2 carrying handles can be supplied for 18/9. TERMS ON ASSEMBLED UNITS. DEPOSIT 25/6 and nine monthly payments of 25/6.

LINEAR "DIATONIC" 10-WATT HIGH FIDELITY AMPLIFIER. Incorporating pre-amp. For A.C. mains input 200-230-250 v. 50 c.p.s. A compact attractively finished unit with two separately controlled inputs, and outputs for 3 and 15 ohms speakers. Separate Bass and Treble controls. Five latest type miniature Mullard valves. Only 12 Gns. Send S.A.E. for leaflet and credit terms.

W.B. STENTORIAN HIGH FIDELITY P.M. SPEAKERS. HF1012, 10 watts, 15 ohm (or 3 ohm) speech coil. Where a really good quality speaker at a low price is required, we highly recommend this unit with an amazing performance. £24/10/0. Please state whether 3 ohm or 15 ohm required.

P.M. SPEAKERS. 2-3 ohm 5in. Goodmans 17/9. 7in. Elliptical 19/9. 6½in. Rola, 19/9. 8in. Rola, 19/9. 8in. Goodmans 21/9. 10in. R.A. 28/9. 10-6in. Elliptical 28/9. 12in. Plessey 29/11. 12in. Plessey 3 ohms, 10 watts, 12,000 lines, 59/6.

SUPERNET RADIO FEEDER UNIT

Design of a high quality Radio Tuner Unit (specially suitable for use with any of our Amplifiers). A Triode Heptode Freqchanger is used. Pentode I.F. and double Diode Detector, delayed A.V.C. is arranged so that the V.G. distortion is avoided. The Ch. Ch. Sw. incorporate Gram position. Controls are Tuning, W. Ch. and Vol. Output will load most Amplifiers requiring 500 m.v. input depending on A.C. location. Only 250 v. 15 mA. H.T. and L.T. of 6.3 v. 1 amp required from amplifier. Size of unit approx. 9-6-7in. high. Send S.A.E. for illustrated leaflet. Total building cost is £24/15/0. Point-to-point wiring diagrams and instructions, 2/6.

RECORDING TAPE. 1,200ft. Reels Purstone, Medium coercivity, 15/9.

Radio Supply Co. (LEEDS) LTD.

32 THE CALLS. — LEEDS, 2.

Terms: C.W.O. or C.O.D. No C.O.D. under £1. Postage 1/9 extra on all orders under £2, 2/9 extra under £5 unless carriage charge stated. Full Price List 6d. Trade List 5d. Open to Callers: 9 a.m. to 5.30 p.m. Saturday until 1 p.m. S.A.E. please with all enquiries.

G.W. SMITH & CO

(RADIO) LIMITED

Phone: GERRARD 8204/9155

Cables: SMITHEX LESQUARE
334 LISLE STREET, LONDON, W.C.2

A.R.88 WAVECHANGE SWITCHES. Ceramic, 8 bank, 6 position, complete with all screens. Brand new, 17/6 each. P/P. 2/-.

WELDING TRANSFORMER. Input 230 volts. Output 17.5 volts 35 amps. New, 72/6. P/P. 5/-.

L.T. TRANSFORMER BARGAIN. Input 200/250 volts. Output 12 volts 5 amps. Only 12/6 each. P/P. 2/-.

6 VOLT VIBRATOR PACKS

Output 120 volts 30 m/a. Fully smoothed, uses standard Mallory 4-pin vibrator. Supplied brand new and boxed, 12/6 each. P/P. 2/-.

R.1155 SUPER SLOW MOTION DRIVES

Improved version as fitted to Model A, etc. Brand new, 12/6 each. P/P. 1/6.

0-1 MA. METERS

Brand new moving coil meters, round flush mounting with 2½in. scale, calibrated 0/300 volts. Resistance 100 ohms. Supplied complete with rectifier, 25/- each. P/P. 1/-.

"C" CORE E.H.T. TRANSFORMERS.

All new and unused. Input 230 volts. 1. Output 3850 v. 5 ma. 4 v. 2.5 A. 4 v. 1 a. 52/6 each. P/P. 3/-.

2. Output 1250-0-1250 v. 5.5 ma. 6.3 v. 1 A. 6.3 v. 1 A. 4 v. 1 A. 42/6 each. P/P. 2/-.

MIDGET RECORDER MOTORS.

Size only 1½ x 2 x 2½in. Will operate from 4.5 to 24 volt D.C. Fitted with reduction gear.

Supplied brand new, 12/6 each. P/P. 1/6.

BARGAIN 6.3 VOLT FILAMENT TRANSFORMERS

Potted, hermetically sealed, ceramic terminations, all brand new. Made by famous manufacturer.

Type 1. 200/250 volt input. Outputs: 6.3 v. C.T. 5.6 amps., tapped 5 v.; 6.3 v. C.T. 4.8 amps., tapped 4 v.; 6.3 v. C.T. 1 amp., tapped 4 v., 19/6 each.

Type 2. 200/250 v. input. Output: 6.3 v. C.T. 3.3 amps., tapped 5 v.; 6.3 v. C.T. 1 amp., tapped 4 v.; 6.3 v. C.T. 0.9 amp.; 6.3 v. C.T. 0.6 amp., 15/6 each.

Postage both types, 2/-.

A.C. MAINS BLOWER MOTORS.

220/230 volts. 1½in. dia. outlet. Housed in metal box and fitted with dust filter pads. Supplied with 2 lengths of hose, brand new, £4/19/6 each. P/P. 7/6.

MUIRHEAD STUD SWITCHES

Brand new and boxed. 4 banks, each bank 24 positions. Heavy duty contacts. Only 17/6 each. P/P. 1/6.

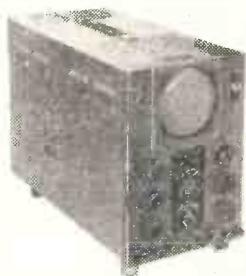
AMERICAN GEARED MOTORS

American 24 volt D.C. motor with built-in precision gearbox giving twin outputs 20 r.p.m. and 6 r.p.m.

Will also operate on 12 v. giving reduced outputs. Size 7in. x 1½in. Shaft dia. ½in.

Supplied brand new only. 19/6 each.

P/P. 3/-.



COSSOR DOUBLE BEAM OSCILLOSCOPE TYPE 339

Operation 110/200/250 volts A.C. 120 watts. Time Base 10 positions. 6 cps. to 250,000 cps. Amplifier 10 cps. to 2,000,000 cps. Sensitivity, Y1.Y2.3.I v. D.C. 1.1 v. rms. X. 2.25 v. D.C. .8 v. rms.

Supplied in good working order £27/10/- each. P/P. £1.

MAINS VOLTAGE REGULATOR TRANSFORMERS.

For A.C. mains 50 cycles. Will give a variable output from 185 volts to 250 volts at 24 amps. £15 each. P/P. 10/-.

Smaller type available 200/240 volts 7.5 amps, 87/6 each. P/P. 5/-.

AMERICAN SUPER LIGHT-WEIGHT HEADPHONES

Magnetic type, res. 50 ohms. Fitted with rubber earmoulds to fit inside the ear. Extremely good quality, ideal for communication receivers, etc., supplied brand new, 15/- pair. P/P. 1/-.

AMERICAN MINE DETECTORS.

Type SCR-625c. Battery operated, portable and supplied complete with instruction book. Ideal for detecting all types of metals £12/10/- each. P/P. 10/-.

SPECIAL OFFER

BRAND NEW AMERICAN / CANADIAN NO. 19 Mk II TRANSMITTER - RECEIVERS. Complete with all valves. Frequency coverage 2 to 8 mc/s, 65/- each. P/P. 10/-

Limited number only available.

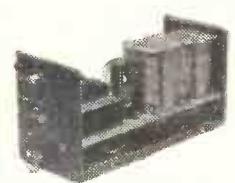
ADMIRALTY 12 VOLT MOBILE AMPLIFIERS.

Separate mic. or gram inputs. Output 10 watts, matched to 3, 15 or 600 ohms. Supplied in good working order, £8/19/6 each. P/P. 5/-.

HEAVY DUTY "C" CORE TRANSFORMER.

Input 230 volts. Outputs, 510/0/510 + 300 m.a. 375/0/375 v. 100 m/a., 6.3 v. 9 a., 2 x 6.3 v. 2 a., 2 x 6.3 v. 1 a., 6.3 v. 1.5 a., 6.3 v. 5 a. 5 v. 3 a. Brand new, 82/6 each. P/P. 5/-.

EDDYSTONE MAINS POWER PACKS



Supplied brand new and unused. Mains input 200/250 volts. Output 175 volts 60 ma. and 12 volts 2.5 a. Double choke and condenser smoothed. 5Z4 rectifier. Housed in grey metal case. Only 32/6 each. P/P. 3/6.

HEAVY DUTY MAINS ISOLATING TRANSFORMERS.

Specifications:—Primary 230 volts 3 amps. Secondary 230 volts 3 amps. (service rating, OK 5 amps.). Ideal for laboratory or workshop use. Supplied brand new in original transit cases, £6/10/- each. P/P. 10/-.

AMERICAN ROTARY TRANSFORMERS

Models available for either 6 or 12 volt D.C. input. Output 250 volts D.C. 80 mA. Ideal for car radios or razors, etc., brand new, 22/6 each. P/P. 3/-.

CHEAP TRANSISTORS
Red spot, 800 kcs/s, 7/6. Yellow/green, audio, 250 mva., 10/-. Yellow/red RF, 1.5-8 mc/s, 21/-.

TRANSISTOR TRANSFORMERS. 1 in. sq., 3 : 1.4.5 : 1.10 : 1, 4/6.

TRANSISTOR CAPACITORS. Electrolytic, 1½ in., 6, 8, 18 or 30 mfd., 3 or 6 volt, 2/9. 001, .002, .005, .01, .02, or .04, 9d.

TRANSISTOR VARIABLE. Jackson, 365pf., 2-gang, 8/6.

MAINS NEON PANEL INDICATORS. Chrome escential. Red, amber, green or clear, 3/9. 42/- doz.

COPPER AERIAL WIRE. Ex-U.S.A. 300ft. reels, 3/6.

HEAVY DUTY SLIDER. 1 ohm, 12 amp., 6/8.

HEATER TRANSFORMERS. Input 230 volts. Output 6.3 v. 1.5a., 5/9. 3 amp., 10/6.

CRYSTAL DIODES, G.E.C. 104. **CRYSTAL SET COILS.** Repaneo dual range, 2/6. Teletron HAX, 3½-. 0003 mfd., variable, 3/10. .0003 mfd. variable, 3/10.

BULGIN SIGNAL LAMPS. M.e.s. red, green, white or clear, 1/9.

ALLADIN COIL FORMERS. 1in. or 1in. with slug, 6d.

ALLADIN COIL FORMERS WITH CANS. 1in., 1½-; 2in., 1½.

EPICYCLIC DRIVES. 5 : 1 ratio, 1/3. Cord drives, 1/3.

BRASS 1in. COUPLERS. 7d.; w/spindle, 9d. Ceramic flexible coupler, 1/6.

LINE CORD. 2a. 100 ohms/ft., 1/9yd.; 3a. 60 ohms/ft 1/9yd.

CERAMIC CAPACITORS. 500 v. w/kg 1 pf. to 5,000 pf., 8d. 001 mfd., 9d.

CARBON RESISTORS. 1/16, ¼, ½ or ¾ w. 3d.; 1 w., 4d., 2 w., 6d.

VALVE HOLDERS. Octal, 6d. Mazda, 6d. 807 6d. Ceramic, 1/4-. Loctal, 9d. B8A, 9d. B5, 6d. BTG, 6d. W/skirt, 9d. BTG cans, 6d. B9A cans, 8d.

ALUMINIUM CHASSIS

Best quality, 18 swg., four sided, reinforced corners. 6 x 4 x 2½in., 3/6; 10 x 7 x 2½in., 5/3; 7½ x 5½ x 2½in., 4/6; 11 x 7½ x 2½in., 6/-; 13½ x 9 x 2½in., 6/9.

0.005 mfd., 2 gangs, 7/6. Large 3 gangs, 8/6. Ditto 4 gangs, 7/6. **TRIMMERS.** Philips beehive, 10 pf. 1/6-. 30pt. 10d. Mica, 50 pf., 6d. 2 x 100 pf., 1/-; 2 x 200 pf., 1/-; Cyldon H/V, 250 pf., 1/-; Air spaced w/spindle, 50, 100 pf., 1/6. **OCTAL PLUGS.**

1/9. **BELLING 7-PIN P/S.** 1/6 pr. **MIDGET JONES.** 8-pin 3.6 pr. 12 pin, 4/6 pr. 21 pin, 7/6 pr. **BULGIN** 3-pin mains, 7/3. 4/6 pr.

ROTARY SWITCHES. Small size, 2 P, 2 W., 1/6.

3 P, 2 W, 1/6. 4 P, 3 W, 2/6. 3 P, 4 W, 2/6. 2 P, 6 W., 2/6. Large ceramic, 2 P, 6 W, 7/6.

TOGGLE SWITCHES. S/P. on/off, 1/9. D/P on/off, 2/6. S/P. c/over, 2/3. D/P. c/over, 3/6.

KEY SWITCHES. D/P. c/over, locking, 2/9. Non-locking one side, 2/3.

POTENTIOMETERS. Wrewound, 100 ohms, 300 ohm 1K, 2K, 2.5K, 5K, 10K, 50K, 100K, 2/6. Carbon, 1K to 100K, 1/9. 250K to 2 Meg, 2/3. All w/spindle.

FUSE HOLDERS. 1½in. Open clips, Single, 5d. double, 10d. Fuses, 150 mpa to 5 amp., 3d.

PAPER CAPACITORS. Tubular, 330 or 500 v., .001 to 1 mfd., 9d. 25 1/4-, 5.1/3.

ELECTROLYTIC CAPACITORS

All new stock

2,200 v.....	1/3	500/500 v	4/6
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16/450 v.....	2/9	8 x 8/450 v	3/6
16/500 v.....	3/3	8 x 16/450 v	3/6
30/450 v.....	3/9	16 x 18/450 v	3/6
40/450 v.....	3/9	16 x 16/500 v	3/6
10/25 v.....	1/-	32 x 32/275 v	3/6
25/25 v.....	1/-	32 x 32/350 v	4/3
50/12 v.....	1/3	32 x 32/450 v	4/6
50/25 v.....	1/-	50 x 50/275 v	3/9
50/50 v.....	1/9	100 x 200/350 v	7/6
100/25 v.....	1/3	32 x 32 x 2/275 v	3/3
500/12 v.....	1/3	50 x 50 x 50/350 v	5/3

RCA. OUTPUT TRANSFORMERS

Completely potted. Centre tapped primary, 8,000 ohms. Secondary tapped, 3, 7.5, 15, 500 or 600 ohms. Separate feedback winding, 15 watts rating. Ideal for 6L6, KT66, EL84's etc., brand new, 27/6 each. P/P. 2/-.

HOURS OF BUSINESS: 9 a.m.-6 p.m. Thursday 1 p.m. Open all day Saturday.

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P.M. LOUDSPEAKERS, 3 OHM

All new and unused.
Plessey, 24-in., 16-in.; R.A. 6-in., 17/8;
Plessey, 12-in., 32/6; Goodmans, 34-in.,
17/8; Elac, 8-in., 19/8; Rola, 7 x 4-in.,
18/6; Elac, 8-in., 17/8; Elac, 19-in.,
27/6; Plessey, 10 x 6-in., 27/6.

ROTARY CONVERTORS. Input
24 volts D.C. Output 230 volts, 50
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cooled. 126 v. 80 mA. 4/3. 250 v. 50 mA.
7/6. 25 v. 85 mA. 9/-. 250 v. 75 mA. F.W.
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350 v. 60 mA. 6/-.

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POWERED TELEPHONES**

This type requires no batteries to operate
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loud buzzing note, and also a neon indicator.
Ideal for field activities, factories, office, etc.
Only 45/- each. P/P. 4/6.

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Sprague, 4 mfd., 600 v., 4/6.

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6/6 12 yds.

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315 kc/s I.P. transformer..... 5/-
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1/9.

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Output 220 v., 25 mA., 6.3 v. 1 amp. 10/6.

SMOOTHING CHOKEs. 10H, 80 mA., 4/6. 15H

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5H, 200 mA., 5/6. 50H, 120 mA., 15/6. 20H, 120 mA.,

10/6. 15H, 300 mA., 10/6. Swinging choke, 3.6/4.2H

250 mA., 10/6. 8/40H 300 mA., 10/6.

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all new and guaranteed.

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IA7 .. 12/6 EZ81 .. 10/6 6AT8 ... 10/6

3A7 .. 4/6 EM80 .. 10/6 6P6m ... 8/6

3A5 .. 10/6 EV51 .. 10/6 6J7m ... 7/8

3Q4 .. 8/6 ECL80 .. 11/6 6L6g ... 10/6

3V4 .. 8/6 ECF22 .. 12/6 6SQ7 ... 8/6

3S4 .. 8/6 ECFS90 .. 12/6 2D21 ... 8/6

3Q5 .. 9/6 ECCR4 .. 12/6 EL32 ... 5/6

5U4 .. 8/6 ECL22 .. 12/6 EA50 ... 1/9

5V4 .. 8/6 EFS1 .. 10/6 ECF80 .. 10/6

6Y3 .. 7/3 E37a .. 10/6 EC85 .. 10/6

6A25 .. 3/6 E37b .. 10/6 ECF85 .. 10/6

6AK5 .. 5/6 ECH42 .. 10/6 ECH35 ... 11/8

6HG .. 1/9 EL11 .. 11/6 ECH31 ... 10/8

636 .. 3/6 EPF1 .. 9/6 E336 ... 4/8

6C4 .. 5/6 EB91 .. 7/6 EF41 ... 11/-

6J5 .. 4/11 12AH8 .. 10/6 EF85 .. 10/6

6K8 .. 9/- PY80 .. 10/6 EL91 ... 7/8

6V6 .. 7/6 PY82 .. 10/6 EAC91 .. 7/6

607 .. 10/6 PY81 .. 10/6 EY91 ... 7/6

6N7 .. 5/11 PY83 .. 11/6 GZ32 ... 12/8

6X5 .. 7/6 PC25 .. 15/6 KT23a ... 9/6

807 .. 6/- PCF80 .. 12/6 6130 ... 4/8

12A6 .. 7/6 PCF82 .. 12/6 UCH42 ... 10/6

25Z4 .. 9/6 PCC84 .. 12/6 UBP80 ... 10/6

24Z4 .. 9/6 UL1 .. 11/8 UBR9 ... 10/6

DK92 .. 9/6 UAF42 .. 10/6 UAB80 ... 10/6

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voltmeter on 2 ranges 0-160 and

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WIRELESS WORLD**MODULATOR 67**

A wonder'ul complete A.C. mains
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350/0/350 v. 200 ma. 6.3 v. 6 a.
5 v. 3 a. Input 230 v. 200 ma.
choke, 5Z4 rectifier. Paper and
electrolytic smoothing condensers. 11
other useful valves. Hundreds of com-

ponents including switches, pots, condensers, resistors, etc. Supplied
brand new with covers.

SPECIAL REDUCED PRICE 39/6 each P/P 7/6.

HEAVY "C" CORE H.T. TRANSFORMERS.

Type 1. Input 230 volts. Output 360/0/350 volts, 200 mA.
360/0/360 volts 65 mA., 6.3 v. ct. 5 a., 6.3 v. ct. 2 a., 6.3 v.
5 a., 5 v. 4 a., 5 v. 3 a., 65/- each. P/P. 4/6.

Type 2. Input 230 volts. Output 350/0/350 volts, 400
mA., 25 v. l.a., 21 v. 5 a., 6.3 v. 5 a., 6.3 v. l.a., 5 v. 4 a.,
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Type 3. Input 23 volts. Output 450/0/450 volts, 250 mA.,
2 x 6.3 v. 5 a., 2 x 6.3 v. 1 a., 5 v. 4 a., 69/6 each. P/P. 4/6.

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Supplied brand new and unused. Input 200/250 v.
Output 300 volts 200 mA. and 12 volts 3 amps. Double
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BENDIX COMMAND TRANSMITTERS. Complete
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Wonderful offer. All brand
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Type H.T.H. size 4½ x 2½in. Output 310/360 volts at
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DYNAMO EXPLODER UNITS. Used for detonating
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Brand new and boxed instru-
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volts on 2 ranges 0-160 and
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inches. Accuracy within
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**TAPPED L.T. TRANSFORMER.**

Input 200/250 volts. Output tapped,
3, 6, 9, 12, 24 or 36 volts 5 amps.,
5/- each. P/P. 3/-.

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Input 230 v. Output 250 v. 50 mA.
6.3 v. 2 a. Fully smoothed, 5Z4
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VR137, EA50 and Y63 valves. 32/6
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Parmeko. Input 230 volts.
Output H.T. 195 volts 85 mA., tapped
130 v. and 65 v. L.T. 6.3 v. 5 amp.
6.3 v. 3 amp. Brand new, 14/6. P/P. 1/6.

**4 SPEED RECORD
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Brand new 1957 model B.S.R. 4-speed
automatic record changers. Only £8/12/6
each. P/P. 3/6.
Brand new 1957 model COLLARO
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Sensitive, ideal for
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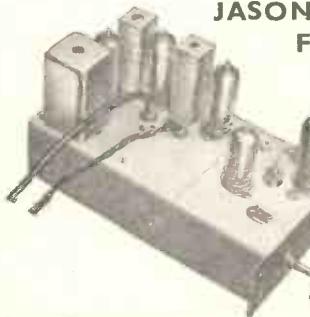
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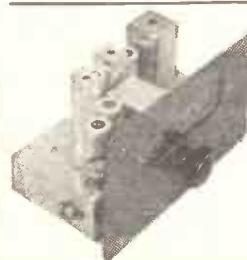
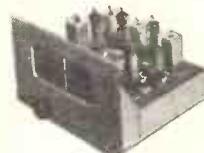
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This excellent unit enables the selection of Home, Light or Third programme at the touch of a switch. Complete freedom from drift is ensured by the incorporation of Automatic Frequency Control. Valve line-up: 4-EP80, 1-ECF80. Front end completely prefabricated. When used in conjunction with a suitable amplifier superb quality is obtainable. The black standard finish and reliability that are the well-known features of the Jason Standard and Fringe Model FM Tuners have been maintained. Instruction booklet and our itemised price list 2/- post free or the complete Kit £9/19/6. plus P. & P. 2/6.

ANNOUNCING OUR NEW F.M. TUNER KIT (printed circuit). This is our printed circuit version of the Osram 912 F.M. Tuner—using T.C.C. printed circuit and condensers, incorporating 5 valves and two germanium diodes. Attractive black and gold dial, with gold escutcheon plate. Dial aperture only 5 x 2in. Osram F.M. booklet plus our additional instructions and individually priced components £2/6 post free or the KIT absolutely complete at £28/8/- plus 2/6 P. & P. Alignment service available if required. We are demonstrating at 18 Tottenham Court Road.



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Based on the booklet by Data Publications Ltd., 2/- post free, including our individually priced parts list. Highly sensitive, free from drift. Incorporates 4 valves 6AM6 and 2 specially graded G.E.C. Crystals. The kit supplied includes all leads with timing condenser, scale calibrated in mcs, and attractive bronze stove-enamelled front plate already mounted (illustrated). Front plate size 8in. x 5in. Chassis 7in. x 4in. x 1 1/2in. Complete standard kit £28/15/- plus 2/6 P. & P. Fringe area kit £27/15/- plus P. & P.

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DULCI

DULCI H.3 AM/FM Chassis (7 valves). Covering Long, Medium and F.M. bands. Most attractive dial in RED and GOLD on BLACK background. £20/17/- plus 5/- c. & p.
DULCI H.4 Push pull AM/FM chassis £29/3/10 plus 5/- p. & p.
All Dulci products available ex stock. Illustrated leaflets and H.P. terms available.
Demonstrating at both branches.

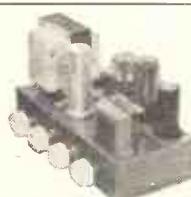
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Full range in stock by WHARFEDALE, W.B., T.S.L. etc.
Your enquiries welcomed.

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This is a very high quality chassis for medium waves and F.M., incorporating 8 of the latest miniature valves, plus DM70 magic eye. Kits are available for chassis complete with output stage at £16/5/- also less output stage but with own built-in power pack at £13/19/6 only. These are high fidelity units and exceptional value at these prices which include all required components and full constructional details. Fully illustrated Data Booklet with full construction details, plus individually priced component list, available per return of post 2/- post free. Both plus 3/6 P. & P.

THE R.C. 3/4 WATT AMPLIFIER KIT. Compare the advantages. Treble, base AND middle controls. For crystal or magnetic pick-up. A.C. Mains 230/250 V. Valve line-up: 6V6GT, 6SG6T metal 6X5GT. Negative feedback. Built on stoved enameled steel chassis, measuring only 8in. x 4in. x 1 1/2in. Four engraved cream knobs are included in the price of the complete kit with all necessary practical and theoretical diagrams at £24/5/- only, plus 2/6 packing and post or Instruction Book fully illustrated for 1/- Post free. This amplifier can be supplied assembled, tested, and ready for use at £25/5/- plus P. & P. Hearing is believing.



THE NEW R.C. TRANSISTOR/RECEIVER KIT

This receiver, covering medium waveband, which can be assembled in about 1 hour, will give amazing volume and tonal quality when used in conjunction with a good aerial and earth. Incorporating PNP Transistor and Germanium Diode. For headphone reception.

Included with the kit of parts is a handsome plastic case in black and white, measuring 4 1/2 x 2 1/2 x 1 1/2in. This case accommodates the complete receiver, including battery.

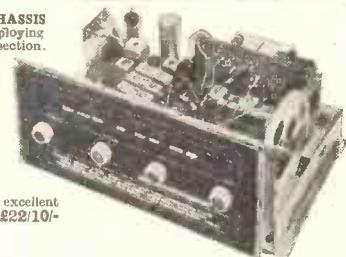
PRICE OF COMPLETE KIT 25/- plus 1/3 P. & P. Lightweight high resistance headphones can be supplied separately at 15/- pair. II, however, the kit is purchased complete with headphones.

It will be supplied at a SPECIAL INCLUSIVE PRICE OF 37/8 plus 1/8 P. & P. Optional extra. 100ft. coil single 7/36 coloured P.V.C. covered wire suitable for both aerial and earth. 2/6 only.



RC4.FAM AM/FM RADIOGRAPHIC CHASSIS

A new style AM/FM Chassis employing a printed circuit F.M. Tuner section. Valve line-up: 8 valves, ECC83, 6B86, 12A8, 6BA6, 6AL5, 6AT6, EL84, 5Y3. Most attractive dial 12 x 5 1/2in. fully illuminated with figures in green, red and white on black background. Four controls: Tuning, Wave-change, and Tone/On/Off. Dimensions (overall): 13 x 9 x 5in. Frequency coverage (four wavebands), 1,000-2,000 m., 200-550 m., 15-50 m., 88-100 mc/s. This is an excellent and very efficient chassis. Price £22/10/- plus 5/- P. & P.



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NEW PLASTIC RECORDING TAPE. 1,200 ft. on plastic spool. 21/2 in. plus 1/6 p. & p. 3 spools for 63/- post free.

DUAL CONCENTRIC CONE LOUD-SPEAKER. 6in. dia., 3-5 ohm speech coil. Excellent quality, few only at 35/- each plus 1/- p. & p.

POCKET VOLTMETER. A very handy instrument for measuring voltages from 1 v. to 250 v. D.C. in two ranges. Contained in well made wallet. Brand new, only 12/6 each plus 9d. p. & p.

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UNIVERSAL AVO MINOR. Eleven D.C. ranges. Complete with test leads and battery. Ex-W.D. but BBAND NEW and fully guaranteed £7/10/- plus 1/6 p. & p.

AMERICAN SUPER-LIGHTWEIGHT HEADPHONES. Magnetic type. Fitted with rubber earmoulds. Impedance 50 ohms. Brand new 15/- pr. plus 1/- p. & p.

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Our advantageous H.P. and Credit Sale terms are available on any single item over £5. Your enquiries invited.

If not stated, please add postage on orders under £1. Cash with order or C.O.D. (charges extra).

THE "SUPERIOR FOUR" KIT. Our superior four-valve receiver A.C. mains, 200/250 v. M. and Long waves. As with our very successful "Economy Four," all required components are supplied. Valve line-up: 2 6SG7, 6 X5GT and 6 V6GT. Cabinet size 10in. x 10in. wide. Maximum depth at base 5in, tapering to 3in at top. Sloping front. Very attractively finished in light walnut and peach. Each component brand new and tested prior to packing. Complete instruction booklet with practical and theoretical diagrams is provided. Booklet available at 1/6 post free. Our price for complete kit £2/9/6. Please add 2/6 P. & C. If preferred, we can supply Cabinet Assembly only, comprising Cabinet and bracket wave-change switch; dial pointer, drum, pulleys, drive spindle, drive spring and knobs, at 45/- plus 2/6 P. & C. N.B.—Our kits are even supplied with sufficient solder for the job.



RAMBLER MAINS UNIT. Enabling the above receiver to be used on A.C. mains. Very easily fitted. Complete kit with assembly fits snugly into battery compartment. PRICE ONLY 47/- plus 1/6 p. & p. This unit is completely self-contained in metal box measuring 7in. x 2in. x 14in. and is ideally suitable for most all-dry portables requiring 90 v. H.T. and 1.5 v. L.T. IMPORTANT: Please state valve line-up when ordering.

THE R.C. 2 AMP. BATTERY CHARGER KIT. Includes handsome well-ventilated stove-enamelled steel box, size: 7in. x 3in. x 3in. Fully shrouded first quality transformer, brand new G.E.C. rectifier. Mains fuse, etc., for charging 6 or 12 v. batteries at 2 amp. Absolutely complete kit with full practical and theoretical instructions. Price 36/6 plus 2/6 P. & P. Can be supplied assembled and tested at 45/- plus P. & P. Heavy duty crocodile clips suitable for car battery lugs, optional extra at 1/6 per pair.

No. 38 TRANSMITTER/RECEIVER.

(popular Walkie-Talkie). We have been most fortunate in obtaining a further supply of these complete stations comprising TX/RX unit, headphones, microphone, phone, aerial junction box, battery sat-

chel and full operating instructions. Range: approx. 5 miles. Frequency coverage 7.4-9 mc/s. ABSOLUTELY BRAND NEW. 65/- plus 7/6 C. & P. Export enquiries invited.

No. 18 TRANSMITTER/RECEIVER UNIT.

We have just taken delivery of a quantity of these fine units, brand new and complete. This is a very good portable, self-contained transmitter-receiver designed for short range telephone. Range approx. 5 miles. Frequency coverage 6 mc/s-9 mc/s. All accessories supplied, i.e., Headphone, Mike, Morse Key, Aerial, comprehensive instruction book with circuit diagram. Valve line-up: 3 AR12, 2 AR8, 1 ATF4. Weight: approx. 2.2lb. Dimensions (overall): 8in. x 10in. x 17in. UNREPEATABLE at 99/6 plus 7/6 C. & P.

CONSTRUCTORS NOTE !!
RADAR DATA BOOKS AVAILABLE, i.e. Valve guide, Colour code, etc. Send stamp for list.

THE "NEW LOOK" RAMBLER

Our most popular All-Dry Portable Superhet Kit is now being supplied with a new cabinet of even more attractive appearance. The new cabinet is covered with "LIONIDE" which is washable and unscratches. Colour: two-tone GREY/RED. The standard cream plastic top panel with dial engraved in red completes the overall "air of quality." This receiver really has everything. Built-in frame aerial high quality, extremely sensitive and very adequate volume from the 5in. loudspeaker. Valve line-up: 3V4, 1R5, 1B5, 1T4. The complete kit, including cabinet, can be supplied from stock at the original special inclusive price of £7/7s plus 2/6 p. & p. (less batteries). Uses Ever Ready 90 v. H.T. type B126 at 10/-. and 1.5 v. L.T. type AD.35 at 1/6. Instruction book available separately at 1/6 post free, contains easy to follow practical diagrams, circuit and individual component price list.

RAMBLER MAINS UNIT. Enabling the above receiver to be used on A.C. mains. Very easily fitted. Complete kit with assembly fits snugly into battery compartment. PRICE ONLY 47/- plus 1/6 p. & p. This unit is completely self-contained in metal box measuring 7in. x 2in. x 14in. and is ideally suitable for most all-dry portables requiring 90 v. H.T. and 1.5 v. L.T. IMPORTANT: Please state valve line-up when ordering.

The R.E.P. 1-VALVE RECEIVER. All day battery operation, for use with headphones, the complete kit is available at 42/-, less battery, plus 2/- P. & P. or full instructions at 9d. post free.

"FAMILY FOUR." Our new T.R.F. kit with handsome brown bakelite cabinet. This receiver gives results comparable to many commercially made receivers costing twice this price. ONLY £4/19/6 plus 2/6 p. & p. Instruction booklet available separately at 1/6 post free.

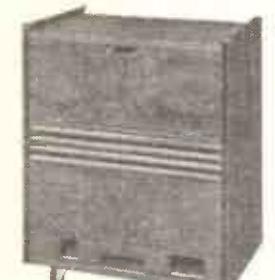
N.B.—All our T.R.F. Kit circuits include specially wound Denco "Max Q" coils on polystyrene formers, improved performance. Price remains the same.

VALVES. We have perhaps the most up-to-date valve stocks in the trade. A stamp will bring complete list of brand new imported valve types, fully guaranteed P.T. paid. Also all usual surplus types available such as 6V6GT, etc.

SURPLUS METER BARGAINS. We have large stocks of meters from 50 microamp to 300 v. and will be pleased to forward a complete list upon receipt of 3d. stamp.

METER RECTIFIERS. 1 ma. and 5 ma. each at 6/6. Brand new.

RETURN OF A WINNER !!! (Exclusive)



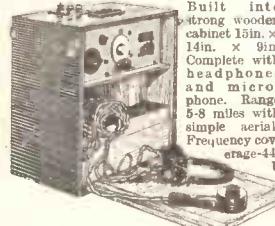
We have been most fortunate in obtaining further limited supply of this fine and popular cabinet. Instantly recognised as being of leading High Quality manufacturer's stock, this trolley-type cabinet is finished in polished dark solid walnut. Can easily be adapted to accommodate tape recorder, amplifier, radiogram, etc. etc. External measurements: 24in. x 16in. x 29in. The whole is mounted upon easy run castors. Unrepeatable at this price £25/19/6 plus 15/- C. & F.

SPECIAL PURCHASE from MINISTRY
BRAND NEW No. 17 Mk. II TRANSMITTER/RECEIVER

Built into strong wooden cabinet 15in. x 14in. x 9in. Complete with headphones and microphone. Range 5-8 miles with simple aerial. Frequency coverage 44-61 mc/s. (5.7metres).

Uses standard 120 v. H.T. and 2 volt L.T. batteries. Complete with full operating instructions. 59/6 plus 3/6 C. & P.

No. 17 Mk. II, as above, but secondhand, in good condition and complete. 45/- plus 3/6 C. & P.



PORTABLE GRAM AMPLIFIERS

RCA. AMPLIFIER. A small high quality gramophone amplifier employing the latest circuitry and highly efficient miniature valves. Very neat chassis finished in

bronze & silver enamel. (overall) 5½ x 4 x 5in. Valves 6X4, ECL82. Output 3 watts max. Controls: Volume, Tone, On/Off. For use on AC mains 200/250 v.

Price £2/19/6 plus 2/- P. & P.

RC2A. Small PRINTED CIRCUIT single valve high gain amplifier for the smaller type of portable. Employs latest type ECL80 valve. Further details on request. Price only 56/- plus 2/- P. & P.

RC3A. A superior quality 3-valve amplifier employing EZ80, EL54 and ECC83. With separate Bass and Treble controls. Further details on request. Price: £2/19/6 plus 2/6 P. & P.

RC4.A. (STALLION). This is supplied complete with high flux 8in. P.M. Speaker and Baffle. Incorporating three octal type valves 607, 676 and 6X5, this robust and well-made unit is ideal for use in the larger type of record player and is equally suitable for use in conjunction with a radio feeder unit. Separate bass and treble controls are provided; also provision is made for an extension speaker and mains supplies to gram. motor. Output approx. 4 watts. Size overall 13in. x 4in. x 9in. high. For use on A.C. mains 100/200/250 v. PRICE £5/19/6 plus 2/6 P. & P. H.P. terms 22/19/6 deposit and four monthly payments of 16/8 per month. Fits our portable cabinet "G" at 85/- without modification.

RECORDER AMPLIFIER.

(Well known manufacturer's surplus.) This is a brand new amplifier designed for use with a famous wire recorder. A simple modification is all that is required to make this unit ideal for use with any Tape Deck.

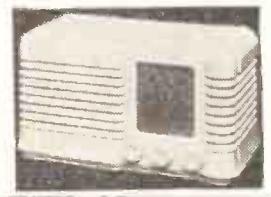
Specifications: Valve line-up 7C5, 2AU7, 6BR7, 6X4. Neon Record Level Indicator. Controls: Volume/Record Level, Tone Control, Record/Playback Switch. High and Low level inputs for Mike and Radio. External Speaker Socket. Built-in 5in. Loudspeaker with High Flux magnet. Dimensions: Amplifier 5in. H. x 11in. W. x 2½in. D. Power Pack: 6½in. H. x 6in. W. x 5in. High (overall). Full modification details are supplied. Price £8/19/6. P. & P. 3/6

mc/s. (5.7metres). Uses standard 120 v. H.T. and 2 volt L.T. batteries. Complete with full operating instructions. 59/6 plus 3/6 C. & P.

plus 3/6 C. & P.

No. 17 Mk. II, as above, but secondhand, in good condition and complete. 45/- plus 3/6 C. & P.

THE "ECONOMY FOUR" T.R.F. KIT. A three-valve plus metal rectifier receiver, A.C. mains 200/250 v. Medium and Long waves. We can supply all required components right down to the last nut and bolt. Valve line-up: 6K7, 637 and 6V6. Chassis ready drilled. Cabinet size 12in. long by 6in. high by 5in. deep—Choice of ivory or brown Bakelite or wooden walnut finish cabinet. Complete instruction booklet with practical and theoretical diagrams. Each component brand new and tested prior to packing. Our price £5/10/- complete. Remember this set is being demonstrated at our shop premises. We proudly claim that our fully illustrated instruction booklet is the most comprehensive available for this type of receiver—Booklet available at 1/6 post free. This is allowed if kit is purchased later. Plus 2/6 packing and carriage for complete kit.



GRAMOPHONE MOTORS are in SHORT SUPPLY

COLLA RO AC 3/554; Three speed, single player for A.C. mains 200/250 v. Cream finish, complete with turn-over crystal pick-up incorporating the well-known high output "T" type head. Strictly limited quantity at £6/19/6 plus 3/6 P. & P.

COLLA RO 4-SPEED single record unit with separate pick-up and HGP59 crystal cartridge. Brand new, few only. £4/19/6 plus 3/6 P. & P.

FOUR-SPEED CHANGERS
Collaro RC456 Mixer Auto-Changer in cream with Studio "OO" design. £8/19/6. B.S.R. Monarch Mixer Auto-Changer, in cream and gold. £8/15/- Both plus 3/6 P. & P. H.P. Terms available. Stocks rapidly diminishing.

THE STAAR "GALAXY"



Four speed Mixer Auto-Changer. Finger-tip stop, start and speed change control. Modern duo-tone finish. Beautifully made and moderately sized to fit almost any cabinet. For A.C. mains operation 110-220 v. Price £8/15/- incl. plus 3/6 C. & P.

RECORD PLAYER CABINETS—to suit all types of single record and auto-changer units. Price from 45/- Send stamp for fully illustrated list.

10in. CABINET SPEAKER
Ideal for P.A. etc. Complete solid wood cabinet complete with carrying handle. Painted dark brown, with built-in good quality 10in. P.M. speaker, 3 ohm speech coil, complete with lead and Igranic Jack plug. Brand new. Price only 45/- plus 3/6 P. & P.

CLYNE RADIO LTD.

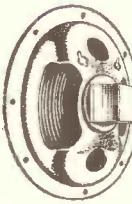


18, Tottenham Court Road, London, W.I.
And at
162, Holloway Road, London, N.7.

LOUDSPEAKER UNITS

Make	Type	Size	Price
Elec	Square	3½in.	19/6 each
Lectrona, Plessey	Round	5in.	17/6 each
Goodmans, Plessey	Round	6½in.	18/6 each
Goodmans, R. & A. Bound	Sin.	19/6 each	
Plessey, R. & A., Elec	Round	10in.	25/6 each
Plessey	Round	12in.	35/- each
Roda	Elliptical	6in. x 4in.	19/6 each
Elec	Elliptical	10in. x 4in.	25/6 each

All the above are PM units with 2 to 3 ohm speech coils.

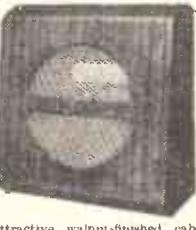


RTCO 12in. heavy duty 20 watts model 15in. ohms	5in. Mains Energised Speaker	17 6
Speech Coil £5 5 0	8in. Mains Energised Speaker	£1 1 0
Gin. Mains Energised Speaker	All have field coils of approx. 600 ohms.	

SPECIAL OFFER

Just a few 5in. units by Goodmans and Lectrona fitted with standard output transformer £1 1 6 each

LOUDSPEAKER CABINETS



This attractive walnut-finished cabinet is available for 5in. or 8in. speaker units. Metal speaker fret, complete with back and rubber feet.
5in. type. Measures 8in. x 8in. x 4in. at base. Price 17/6 each.
8in. type. Measures 10in. x 10in. x 5in. at base. Price 21/6 each.
5in. type. Very similar design. Price 16/6 each.

Postage, any type, 2/- each.



BUILDING A "SECOND" SET

THIS IS THE CABINET TO GIVE YOUR RECEIVER THE COMMERCIAL LOOK. WALNUT FINISHED CABINET. Size: 11½in. x 7in. x 5in. Supplied with Chassis (not out ready) Dial, Back Plate, Drive Cord, Dial Drum, Pointer. Price 27/6 complete Post 3/-.



THE "EKE" QUALITY 3 WATT AMPLIFIER

Three International Octal Valves 6BSG, 6V6GT, 6X5GT. A.C. Mains fully isolated, negative feed back (voltage and current) controls, volume and tone, input network for modern crystal. Really low hum level and even frequency response. Price 94/- plus 9/- packing and post.

W.B. "STENTORIAN" HIGH FIDELITY SPEAKER UNIT

Model H.F. 1012. 10in. die-cast unit, incorporating 12,000 gauss magnet. Handling capacity 10 watts. Frequency response 30 c.p.s.-14,000 c.p.s. Base resonance 35 c.p.s. £4/19/9.

TELEDICTOR TRANSFORMERS, TYPE TED

Small Mains Transformers suitable for Televison Converters, etc. Specification:-

Primary 230 v. 50 c/s

PRICE

Secondary 125 v. 10 m.A.

15/-

Secondary 2. 6.3 v. 1.5 a

Overall Size:

Champ construction, 3.9in. x 2.4in. x 2in over windings. Fixed centres: 3.3in.

WESTINGHOUSE RECTIFIERS

16BC.1-1-16-1	9/- each
16RA.1-1-16-1	6/6 each
16RA.1-1-8-1	4/- each
14RA.2-2-8-3	25/- each
14A.86	13/9 each
14A.97	13/8 each
14A.100	15/- each
14A.124	27/6 each
14B.130	31/6 each
LW7	23/9 each
WX6	3/6 each

CYLDON "TELETUNER." All types available. Stations of your choice. Fit this Converter and your troubles are over. £7/7/- each.

Aerial and Oscillator Coils (All channels) - all frequencies 7/6 pair. Also available from stock, complete range of spares.

CONTROL KNOBS

Long necked knobs for T.V. Receivers in walnut black and cream 1/- each

SUPPRESSORS

Interference kits of condensers and chokes for Interference Suppression. 1 amp. kits 5/6- 2 amp. kits 6/- 3 amp. kits 6/6.

REVISED SECOND EDITION "POINTS ON PICK UPS"

A Replacement Guide to pick up heads cartridges, etc. Over 193 illustrations.

5/- each

Osmor coils for Collaro Type Deck Transistor.

QT6 Bias Filter coil 7/6 each

QT7 Treble Boost coil in Mu Metal can £17/6 each

QT9 Bias Osc. coil 7/6 each

Osmor Coils for the Beginners Shortwave Receiver. Radio Constructor Aug. 1957. SW Q1 31/1 Mcs. 6/- each

SW Q2 12.4 5 Mcs. 6/- each

SCRATCHOFF

Removes scratches from Radio and T.V. Cabinets. In Polythene Dispenser Tubes. 3/- each

All Components in Stock for BBC Television Studio "E" Building your own Radio Set Complete Kit including Headphones, etc. 45/-

PUBLICATIONS

No. 134 F.M. TUNER CONSTRUCTION by W. J. May. ★ Easy to Build ★ Point-to-Point Wiring ★ Super High Fidelity Response ★ 32 pages ★ All components for this Circuit available, ex stock, each 2/6

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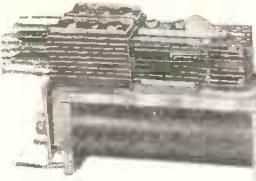
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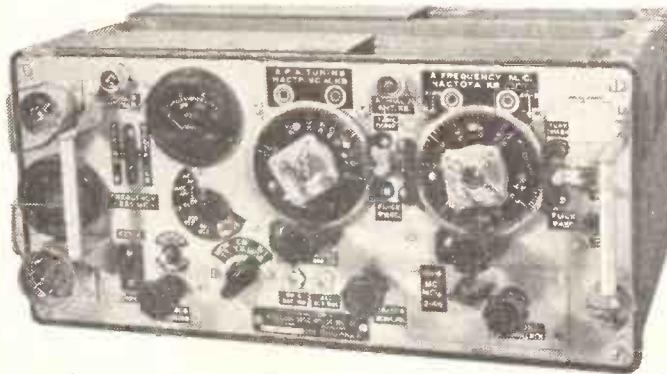
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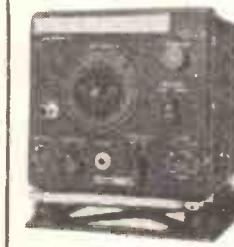
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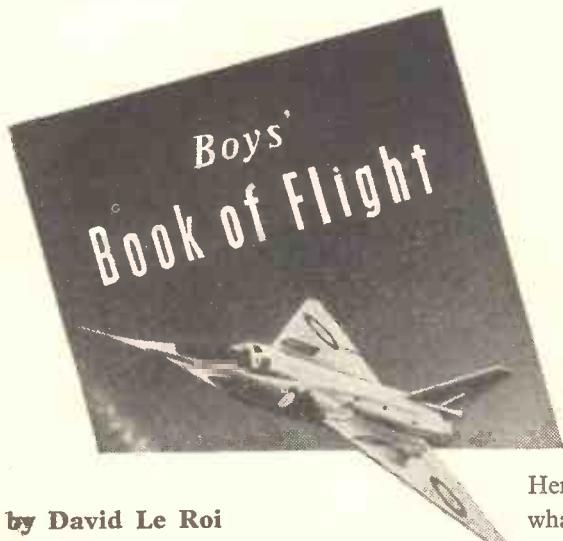
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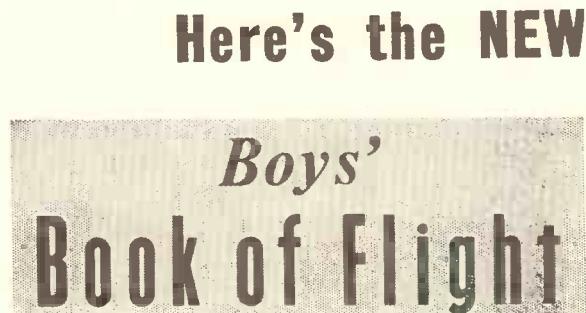
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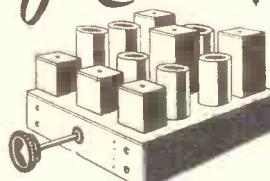
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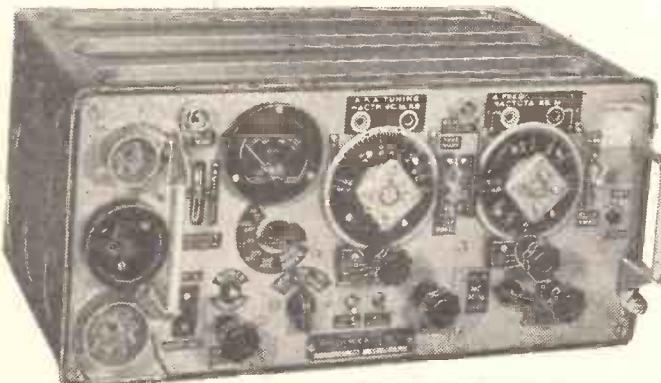
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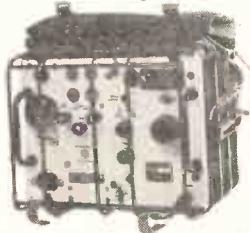
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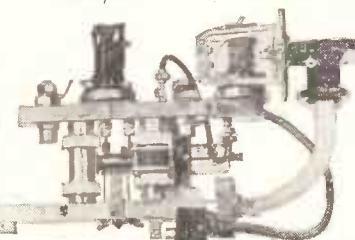
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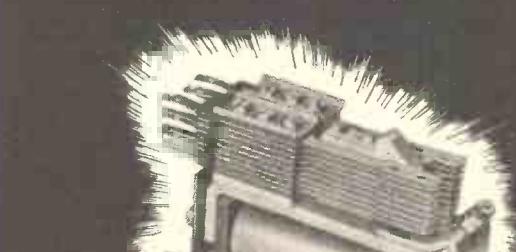
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19v. at 2,800 r.p.m.
6v. at 380 r.p.m.
17/6.
Complete with
blower 22/6.
P. & P. 2/6

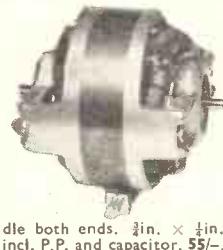


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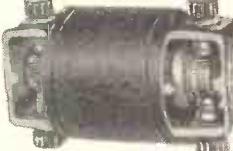
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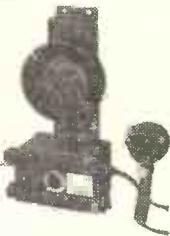
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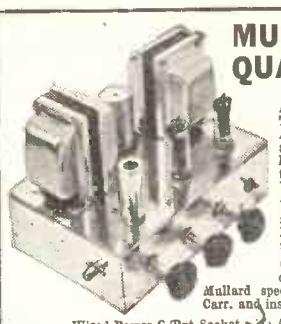
HEAVY DUTY SLIDING RESISTORS. 1 ohm 12 amp slider control 8/6. 300 ohm 1 amp. geared drive 32/6. 1,100 ohm 0.4 amp. horizontal sweep control, 17/6. 5.3 ohm. 8 amp geared drive, 22/6. 0.4 ohm. 25 amp. geared drive, 15/6. 50 ohm. 1 amp., slow motion gear drive, 10/6. 17.5 ohm. 5 amp. fixed, 10/6. 95 ohm. 3.3 amp., no control but fitted with adjustable tappings, 22/6. American 12in. dia field rheostat 38 ohm. 5.6 amp. res. out. 2.1 amp. res. in., 45/-. Postage on all resistors, 3/-.

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MULLARD "3-3" QUALITY AMPLIFIER

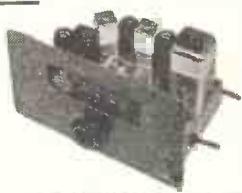
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Variable treble cut and bass boost controls. sensitivity 100 MV for 3-watt output. Frequency response + or - 1db, 40 c/s to 25 kc/s.

Complete amplifier wired and tested with quality sectionalised output transformer to Mullard specification (less speaker) £8.8.0
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F.M. TUNER-UNIT (87 mc/s—105 mc/s) by Jason. As described in Radio Constructor. Designer Approved Kit of parts to build this modern highly successful unit. drilled chassis and superior type dial as illustrated, coils, cans and all quality components, etc., for only 5 guineas, post free. Set of spec. FTS91 or equivalent gives 30% noise free. Illustrated handbook with full details. 2/- post free. Free with Kit. 48-hr. Alignment Service, 7/6 and 2/- p.p. & p.p.

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8+8/500 v. ... 4/6	32+32/350 v... 5/6
16+16/450 v. ... 5/6	32+32/275 v... 4/6
16/450 v. 3/6	50+50/350 v... 6/6
16+16/450 v. ... 5/6	60/80/350 v... 6/6
32/350 v. 4/-	60+250/275 v... 12/6
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72 v. H.T. 1.5 v. L.P. Size 6 x 5 x 1 1/2in.2/6

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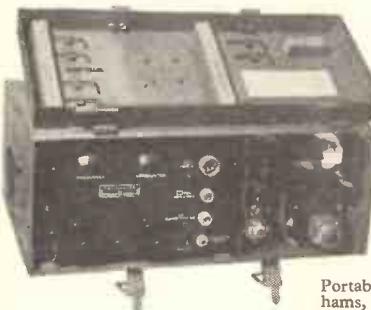
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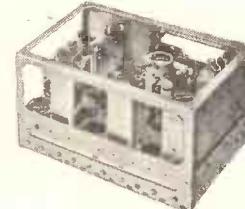
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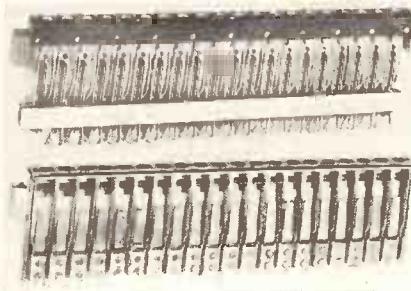
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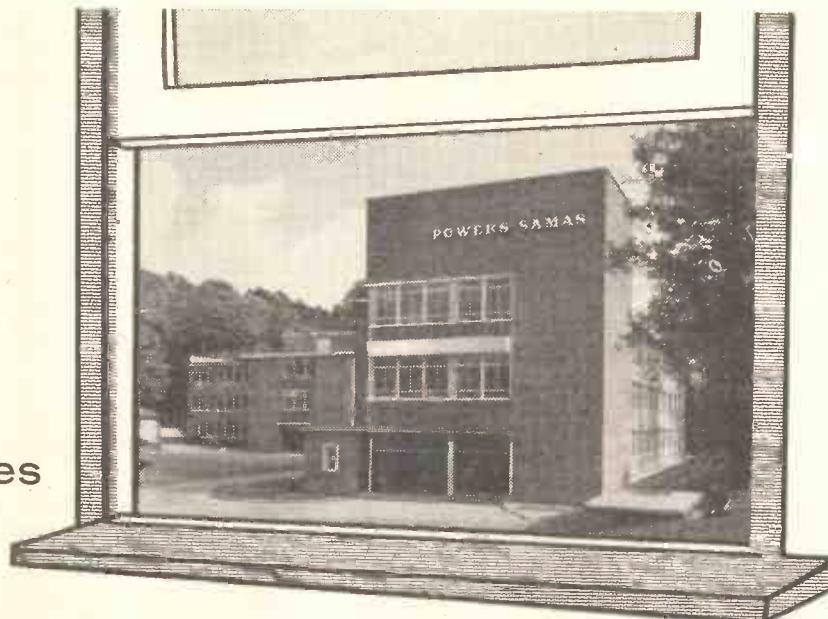
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or write giving full details to Dept.: C.P.S. Marconi House 336/7, Strand, London, W.C.2, quoting reference WW 2970F.

RESEARCH AND DEVELOPMENT

vacancies exist in the Research Department of a large instrument manufacturing organisation in South East Essex for graduate physicists or graduate electrical engineers of merit and some years of industrial experience for the investigation of long-term problems associated with Echo Sounding and Non-Destructive Testing.

The work embraces acoustics and electronics and involves the application of the basic physical principles underlying ultrasonics, telecommunications and computers. Some knowledge in these fields would be an advantage.

The initial salary will be in accordance with experience and qualifications within a scale which allows ample scope for future development. A contributory pension scheme is available, and assistance in housing or removal expenses may be given in suitable cases.

Applications, which may be made in strictest confidence, should give full details of qualifications, previous experience, age and salary required, and be addressed to Box No. 2082—c/o "W. World."

SEMICONDUCTORS LIMITED TRANSISTORS MANUFACTURE

This important Company is shortly to commence manufacture at their new Swindon factory. Applications are invited in respect of the following appointment:

SENIOR ELECTRONIC ENGINEER

To be responsible to Chief Engineer and to be concerned with the maintenance of techniques associated with automatic assembly. In conjunction with other senior engineers (mechanical and chemical) he will be engaged on the improvement of existing techniques in the semiconductor field. An Honours Degree in Electrical Engineering or similar qualification is essential. Age Limits 30—40. In addition, several years' experience in the design and construction of electronic control and test gear is necessary, together with proven executive experience with reputable firms in the optical instrument, process control, radio, radar or computer industries. Applicants should be capable of designing and building test equipment for the environmental life testing of semiconductors. Generous salary according to qualifications.

Applications, which will be treated in the strictest confidence, to

**Personnel Manager,
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PHYSICISTS AND ELECTRICAL ENGINEERS

Progressive positions are open to qualified people of degree standard for work on development and manufacture of special radio valve and microwave devices.

Initial training at the Research Laboratories of the G.E.C. will be available for certain selected candidates.

Canteen, pension fund and social club.

Apply quoting T/1 to:-

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MANUFACTURERS of VALVES for G.E.C.

MULTITONE ELECTRIC CO. LTD.

invite applications from
Intermediate and Junior

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for work on the development and testing of an interesting range of new electronic projects. There are vacancies for engineers with a wide range of qualifications and experience up to and including H.N.C. standard. Experience of development work or fault-finding advantageous. Preferred age range 20/30 years but applications will also be considered from young men who have recently left school with Higher School Certificate in Science. Apply stating age and giving particulars of education, training and experience to 12/20, Underwood Street, London, N.1.

INSTRUMENT ENGINEERS

required in the Electronics and Instruments Section of the Central Electricity Authority, Research Laboratories, Leatherhead. The Section provides an instrument service for all departments of the Laboratories and duties include the maintenance, calibration and repair of the wide variety of physical, chemical and electrical instruments.

Candidates should have the Higher National Certificate and experience in electronic or nucleonic equipment will be an advantage.

Salaries within scales £820-£995 p.a. or £550-£725 p.a.

Write for application form to D. Moffat, Director of Establishments, Winsley Street, London, W.1, to be completed and returned as soon as possible. Quote Ref: W.W./450.

MECHANICAL AND ELECTRICAL DESIGNERS AND DRAUGHTSMEN

required for the design of Plant and Equipment for the processing and testing of electronic valves, C.R. tubes and microwave devices.

There are also vacancies for *Mechanical Designers* on the new development of Special Purpose Machines, and Jigs and Tools. Qualifications: H.N.C. (Mech. or Elec.) or equivalent.

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The successful candidate must have sound theoretical knowledge and practical ability. Several years' laboratory experience is essential, and he should be capable of working on his own initiative. A very attractive salary will be paid consistent with qualifications and experience.

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Housing can be made available to the selected candidates.

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Design and Prototype Development of Audio-Electro Devices and Equipment. Box No. 2336 c/o "W. World"

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Personnel Officer, Ferranti Ltd., Ferry Road, Edinburgh, 5, quoting Ref. RM/59.

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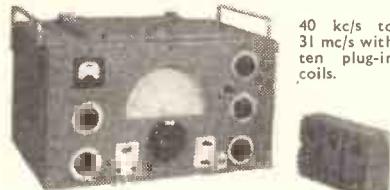
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40 kc/s to
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COILS, range "A" to "J" inclusive 17/6 each.
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MARCONI FIELD TRANSMITTING AND RECEIVING EQUIPMENT F 10 C. 2 to 20 mc/s crystal controlled, output 4 w. MW; 16 w. CW. Consisting of: Transmitter, Receiver and accessory box on aluminium frame; Pedal Generator on aluminium frame; Telescopic aerial, mast aerial, accessories and spares. Details on application.

A.C. MAINS POWER PACKS for 200/250 v. mains. Output 300 v., 200 mA. D.C. and 12 v. 3amps A.C. Size 7½ in. x 7 in. x 13½ in.

PRICE, brand new £3 0 0

Packing and carriage 10/-.

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ARC-I V.H.F. AIRCRAFT TRANSMITTER/RECEIVERS. 10 crystal controlled channels. Price and particulars on application.

Please write for further details of the above equipment and for Complete Catalogues of Radio/Aircraft and Test Equipment to:

Z & I AERO SERVICES LTD.

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Telephone AMBassador 0151/2

We are always buying American Test, Aircraft and Radio Equipment, such as:
BC-221, BC-312, BC-348, BC-342, ARC-I, ARC-3, ART-13, ARN-7, etc.

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RECORD "MINOR" 500 v. INSULATION TESTER £10 0 0
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All the above carry our six months' guarantee.

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Ranges: 0 to 20 mV and 0 to 60 mV.
Calibration:

0 to 1600°C. for Pt-Pt13%Rh

0 to 1300°C for Chromel/Alumel

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PRICE, complete with Standard Cell £32 0 0

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POWER OUTPUT METER. Meter scale 0 to 50 mW and 0 to 17 db; Meter Multiplier 0.1-1.0-10-100; Impedance values: 25-30-40-50-60-80-100-125-150-200 ohms; Impedance Multiplier 0.1-1.0-10-100. PRICE, fully overhauled and guaranteed £32 10 0

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LM SERIES, range as above.

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SIMPLE TWO-DECADE WHEATSTONE BRIDGE

0 to 200 ohms in one ohm steps (no multiplier arms); built-in galvanometer 2.5-0.2-5 millamps.

PRICE £2 10 0
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.10 to 150 v. in 5 ranges resonant frequency 400 mc/s., brand new, in transit case £35 0 0
Service equivalent of the above, overhauled and guaranteed £17 0 0

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C.L.R. Low Impedance, each ... 6 0

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C.H.R., High Impedance, each 13 6

HS-30/U American Army Headsets, lightweight, with miniature plug-in earpieces, each 15 0

R.A.F. Receiver Headgear Assembly comprising: Headband 10A/12160 with Chamois Leather earpads; low impedance earpieces 10A/13466, Connector and Electro-Magnetic microphone type 48

Ditto with High Impedance earpieces 10/12401 £1 10 6

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V.H.F. AIRCRAFT TRANSMITTING AND RECEIVING EQUIPMENT. CRYSTAL CONTROLLED, COVERING THE RANGE OF 115 mc/s to 145 mc/s. Power Output 4 Watts, Total weight 25lbs. THIS EQUIPMENT IS AVAILABLE IN THE FOLLOWING VARIANTS.

4-CHANNEL CRYSTAL CONTROLLED INSTALLATION. (TR 1520)
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44-CHANNEL CRYSTAL CONTROLLED AUTOMATICALLY TUNED INSTALLATION.

ALL INSTALLATIONS ARE COMPLETE WITH CONTROL UNITS, ANTI-FLUTTER AERIALS, MOUNTING RACKS, PLUGS AND SOCKETS AND HEADSET ASSEMBLY COMPLETE WITH MICROPHONE, ALL RELEASED TO A.R.B. REQUIREMENTS. Details, prices etc. supplied on request.

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Rate 7/- for 2 lines or less and 3/6 for every additional line or part thereof, average lines 6 words. Box Numbers 2 words plus 1/- (Address replies: Box 0000 c/o "Wireless World" Dorset House, Stamford St., London, S.E.1.) Trade discount details available on application. Press Day February 1958 issue, Thursday, January 2nd. No responsibility accepted for errors.

WARNING

Readers are warned that Government surplus components and valves which may be offered for sale through our displayed or classified columns carry no manufacturers' guarantee: Many of these items will have been designed for special purposes making them unsuitable for civilian use, or may have deteriorated as a result of the conditions under which they have been stored. We cannot undertake to deal with any complaints regarding any such items purchased.

NEW RECEIVERS AND AMPLIFIERS

LABORATORY-BUILT Hi-Fi amplifier, pre-amp, separate power and radio units, record-changer, 2 wharfdales with cross over units and controls, spare valves, finest components only throughout; £70 complete.—Details, Stubbs, Liberty 1300. [7480]

BUY direct from the makers; we can now supply our R/G chassis and feeder units at keen prices; Model A/P654 an 8-valve AM/FM chassis, 15watts output; Model A/P732 a 7-valve AM/FM feeder; 3d stamp for full details and literature; trade enquiries invited.—Bayly Bros., 46, Pavilion Drive, Leigh-on-Sea, Essex. [7403]

SHIRLEY LABORATORIES, Ltd., 3, Prospect Place, Worthing, Sussex. Tel. 30551. THE TWA/1515 stereosonic tape recording and replay amplifier, separate meter monitoring on record and playback on both channels; 13watts O/P each channel, 96gns; TWA/15 tape recording and reproducing amplifier, 13watts O/P, for Wearite and Collaro decks, 45gns; TW/PA recording and replay pre-amplifier, 30gns; both with valve voltmeter monitoring; type SB/1-15E high-fidelity amplifier, exceptionally wide tone-control system, 40mv sensitivity, 20gns; with two inputs and 3-position gram filter, 22gns; specialized amplifiers for the musical and scientific industries including the Mullard 20watt. [0095]

LOUDSPEAKERS—SURPLUS AND SECONDHAND

SOUND Sales Phase inverter speaker; £5.—Reading, 3, Heronway, Woodford Green, Essex. [7500]

RECEIVERS AND AMPLIFIERS—SURPLUS AND SECONDHAND

QUAD amplifier, pre-amp, and radio, new condition; £35 or offer.—Box 2648. [7483]

ONE B.C. 312 receiver, as new, complete with power pack, also R.F. Unit Type 26; offers.—Box 2190. [7425]

HRO Rx's and coils in stock, also AR88, BC348R, CR100, etc.—Requirements please to R. T. & I. Service, 254, Grove Green Rd., London, E.11. Ley. 4986. [0053]

EX-R.A.F. G.E.C. airfield amplifier equipment incorporating five 175watts, individual amplifiers with priority relay panel; individual power packs, distribution and test panels, complete with valves, and offered on a fully tested basis; £150 ex-works.

GEORGE COHEN'S, Wood Lane, London, W.12. Tel. She. 2070. [7459]

NEW TEST EQUIPMENT

A COMPLETE mains operated unit with three A meters, especially constructed to test Selenium Rectifier Plates singly or in small assembled stacks; £9/9.—Kingston Electrical Supplies, 134, London Rd., Kingston-on-Thames, Kin. 7534. [7437]

TEST EQUIPMENT—SURPLUS AND SECONDHAND

A MATEUR disposing of test gear, amplifiers, etc., cheap.—Tel. Ley. 1932. [7426]

R ADAR dual-band TV signal generator type 405; £45; as new.—Cosmic Radio, Ltd., 6 and 8 Clifton Crescent, Birkenhead. [7475]

SIGNAL generators, oscilloscopes, output meters, valve voltmeters, frequency meters, multi-range meters in stock; your enquiries are invited.—Requirements to R. T. & I. Service, 254, Grove Green Rd., London, E.11. Ley. 4986. [7425]

TEST EQUIPMENT WANTED

WANTED, valve voltmeter (up to £20).—D. Stewart, Chalfont St. Peter, Bucks. Gerrards Cross 2683. [7457]

DYNAMOS, MOTORS, ETC.—SURPLUS AND SECONDHAND

15⁰⁰ cycles alternators 2KVA. 80v.—E.W.S. Co., 69, Church Rd., Moseley, Birmingham. [7275]

NEW COMPONENTS

CRYSTAL microphone inserts (Cosmocord Mic 6/4), in steady demand by Hams and sound engineers, guaranteed newly made and boxed; 15/6 post free.—Radio-Aids, Ltd., 29, Market St., Watford, Herts. [0270]

A new range of

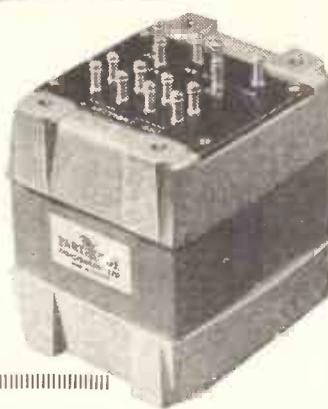
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**P5000 Series 95/-
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- A range of truly "high" fidelity output transformers especially suited to the well-known Osram and Mullard Amplifier designs. The primaries are tapped for ultra-linear connection at 43%, and on certain models at 20% to give optimum performance at various power levels up to 50 watts for operation with such valves as KT88, KT66, EL34, N.709, EL84, etc.
- The series includes a mains transformer of similar styling with specification to suit the Mullard 5-10 and Osram 912 amplifiers.

Write for full details of these and other specified transformers.

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TOLWORTH SURREY**

Phone : ELMbridge 6737/8

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MUSICAL box movements, Swiss; most popular tunes, 25/- and 34/-; or fitted with special pick-up coil and matching transformer for feeding into amplifier, 15/- extra.—Kingston Electrical Supplies, 134, London Rd., Kingston-on-Thames. Kin. 7534. [7470]

COMPONENTS—SURPLUS AND SECONDHAND

METERS, motors, valves; bargains.

0 TO 100 microamp meters, 2½in scale 0 to 1,500yds, 30/-; 0-500 microamp, 2½in scale 500μA, 27/6; ¼amp, RF, thermocouple 8/- 30ma 7/-; post 1/ each.

MOTORS.—24v or 12v, size 2in×2in, 10/6, post 1/; powerful retractable headlight, built-in motor 24v automatically brings lamp through 45° when switched on, limit switches enclosed, only 53/-.

RECHARGEABLE battery type 1545, in wood case, 4 valves ARPI2, VP23; 27/6; post 2/6.

CLOCKWORK units, a temperature compensated precision jewel movement, with contacts that make and break 2 times per sec, basis of an accurate timer; 9/6. Post 6/.

TRANSMITTER receivers, type RT/37/PENR, 214-234mc/s, complete with valves, 5-3AS, 3-1S, 1-IR5, 2-2v vibrator units, in smart haversack with telescopic aerial 9½ft, lightweight headsets, cables, coax, plugs, etc., brand new with manual; only 65/-; post 3/-.

VALVE bargains.

6ACT, SP61, 12J5, CV6, SP41, 7193, S130,

EB34, EA50, at 2/6 ea.; 6J5, EF50, 6SH7, 6SG7, EL32, EF39, TT11, at 3/6; 6SN7, 6SL7, 12SR7,

12SW7, 12SY7, at 6/6; 6L6, EF80, at 9/6; ECL80, PY81, at 9/6; EY51, 10/6.

PHOTO cells, 930 and 927, at 15/- ea.

VALVE holders, Octal, B5, B7, at 6d; 807, B7G,

UX4, 9d.

OSCILLATOR units, 150-220mc/s, in metal case, 5Z, EC52, SP61, split stator tuning condenser, new, boxed, 16/-; post 2/6; distant reading thermometers, 3ft capillary, chrome, £1 ea., post 1/6.

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HEADSETS, brand new, boxed, C.L.R., low res., with cord and plug; 7/6; post 1/6.

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PRE-AMPLIFIERS, in all, neat case, 6SL7, 28D7, relay, mike and output transformers, etc., new with manual; 10/6; 2/- post.

VIDEO amplifiers, 1 valve, type AL-60, res. condensers, coax and miniature 4-pin plugs and sockets; 7/6 ea.

SMALL indicator units, type 277, 1½in tube type CV522, 4v heater, 800v max anode, 4 EF50/S, heat black case; 35/- ea.; post 3/6.

AMPLIFIER units, type 165, contains mike, output and 2 interstage transformers, res. condensers, 5 Octal bases, etc., 5/- each, post 1/9; ditto with .8 TCC metal condensers 7/-, post 1/9.

BATES SURPLUS STORE, 49, Ivy St., Birkenhead. By main Mersey Tunnel entrance. [7415]

SOUTHERN RADIO SUPPLY, Ltd., 11, Little Newport St., London, W.C.2. See our displayed advertisement page 180.

UNUSED transformers, all 250v input.—Secondary, 5,000va, £47; 10v 18a, £5/5;

4v, 15a, 2×4v, 7.5a, £6/10; 10v 100ma, £1/5;

3.500v, 1a, £30; 4v, 15a, 2×4v, 7.5a, £5, 10v 36a, £5; 2 filament transformers, 6v 6a, 10/- each.

SMOOTHING chokes.—9h 1a, £7/10; 10h 1a, £15.

UNUSED valves—4 Ediswan ES 1001 power triodes, £34 each; 8 Ediswan rectifiers ESU 150, £2/7 each.—Box 2338. [7451]

MAGSLIPS at low prices, fully guaranteed.

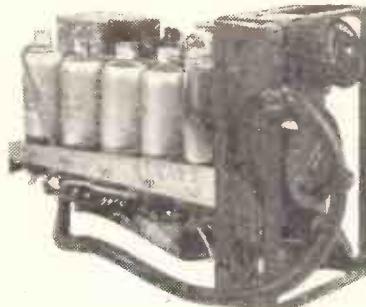
3 in Resolver No. 5 (AP 10861), 50v, 50c/s, unused each in tin, 35/-, post 2/1; large stocks of these and other types.—P.B. Crawshay, 94 Pixmore Way, Letchworth, Herts. Tel. 1851. [0087]

NEW stock clearance, assorted lots, carbon resistors, 12/- 100; silver micas, 15/- 100;

ceramics, 17/6, 100; tag strips (3W to 14W), 16/6 100; Erie 25 & 40 watt droppers, 9/- dozen, plus postage, c.w.o. or c.o.d. Lots other lines free.—A.W.F., 10, Sackville St., Bradford, 1. [0131]

A WALKIE-TALKIE SET

No. 38, Mk. II.



RIGHT IN PRICE AND SIZE—9 x 6 x 3½in.

Ideal for search parties, fire brigades, civil defence, building contractors, etc. Range approximately 5 miles, 7.4-9 mc/s. Brand new condition. Complete with 5 valves, headphones, throat mic, junction box, aerials, harness, signal satchel, and instruction card with illustrations. Operated from dry batteries, H.T. 120/150 v., and L.T. 3 v. (not supplied). Price £4/12/6 each, p. & p. 7/6. Price in stations of 4, £16, p. & p. extra.



G.P.O. ELECTRO MAGNETIC COUNTERS, 5 x 1½ x 1½ in. 4 figures, various voltages D.C. 3/8 v. 18/24 v. 100/110 v. 200/230 v. D.C. 5/- each. 18 v. 7/6 each, p. & p. 1/6.

INTERCOMMUNICATION HANDSETS, self-contained, similar to G.P.O. type, no electricity or batteries required, connect with 2-way bell wire, clear range of several hundred yards. Brand new, 32/6 per pair, p. & p. 2/-.

HIGH SPEED RELAY, 2 bobbins 1,000 ohms each, 5/6, p. & p. 1/3.

U.S. HIGH SPEED RELAY, 300 ohms coil 2.05 v adjustable contacts, 5/6, p. & p. 1/3.

HEADPHONES M/C, complete, 9/6 per set, p. & p. 1/6.

HEADPHONES CLR, complete, 7/6 per set, p. & p. 1/6.

HEADPHONES BAL. ARMATURE, 9/- per set, p. & p. 2/-.

EX U.S. AERIAL, 9ft. spring loaded and fully collapsible complete with cords and guys, ideal as aerial or fishing rod, brand new, 10/6, p. & p. 2/-.

BROADCASTER

Suitable for talking over your own radio, from room to room, by connecting to your radio or gram. Easy to fix, 2 mikes make 2 station house-phone in your own home. 12/6, p. & p. 1/9.



M/C METER, 0-15 and 0-600 v. D.C. 2in. flush mounting ex. equipment. 8/6, p. & p. 1/3.

METER, 2½in., 0-1 amp., projecting type thermo-couple, new and boxed, 6/6, p. & p. 1/3.

U.S. MIDGET MOTORS, 2 x 1½in. Will operate from 6 v. to 24 v. D.C. 12/6 each, p. & p. 1/6.

DITTO, Will operate from 9 v. to 28 v. D.C. 12/6 each, p. & p. 1/6.

(Also reverse types as above, 13/6 each, plus p. & p. 1/6.)

MIC. TRANSFORMER, 2/6, p. & p. 9d.

VIBRATORS, 12 v. 4 pin Mallory type G.629C, 5/-, p. & p. 9d.

U.S. REFLECTOR AERIAL, Omnidirectional antenna, umbrella type. Ideal for transmitting and receiving. Meas. when opened, approx. 4ft. x 3½ft., 4/6 each, p. & p. 1/6.

ACCUMULATOR CUT-OUT, 12 or 24 v. 60 a., ex-R.A.F.

10/6 each, p. & p. 1/6.

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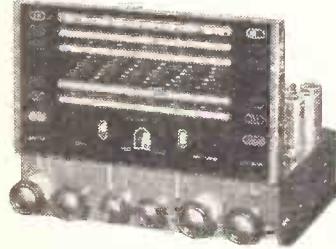
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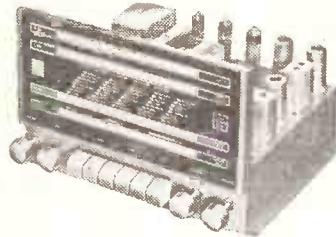


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TRANSRECEIVERS. Type "38" (Walkie Talkie) complete with 5 valves, etc. New condition untested by us but serviceable, no guarantee, 2/6 each.

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[0192]

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½ watt	7d.	2%	1%
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0-300 volts with external res. 50/-.

5 amps, FSD, scale 0-50, 50/-.

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SITUATIONS VACANT UNIVERSITY of Cambridge.

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THE pensionable stipend, which is at present under review, is £750 a year rising by annual increments of £50 to £1,050 a year.

FURTHER details may be obtained from Dr. F. B. Kipping, University Chemical Laboratory, Lensfield Road, Cambridge. Applications close on November 20, 1957. 17460

UNIVERSITY OF SOUTHAMPTON.

AN ELECTRONIC Engineer required for the maintenance of a Ferranti Pegasus Computer and for the design and construction of analogue equipment; previous experience of Computers is desirable but not essential since training will be given; salary in range £750-£850 according to qualifications and experience, plus scheme. Further particulars from the Secretary and Registrar, to whom applications giving age, details of experience and qualifications and the names of two referees should be sent not later than December 14, 1957. [7467]

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TELEMETER equipment, COMMUNICATION receivers and transmitters, NAVIGATIONAL aids, Aerial systems,

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PLEASE write initially giving full details of experience, qualifications and age, to Personnel Department (E.45), Murphy Radio, Ltd., Welwyn Garden City, Herts. [7373]

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TO undertake the official scientific, technical and legal work in connection with patent applications.

AGE at least 21 and under 35 years on 1st January, 1957, with extension for regular Forces' service.

CANDIDATES must have (or obtain in 1957) 1st or 2nd Class Honours in Physics, Organic or Inorganic Chemistry, Mechanical or Electrical Engineering or in Mathematics, or an equivalent qualification and have attended professional qualification, e.g., A.M.I.C.E., A.M.I.Mech.E., A.M.I.E.E., A.R.I.C.E.; for a limited number of vacancies candidates with 1st or 2nd Class Honours degrees in other subjects—scientific or otherwise—will be considered; exceptionally candidates otherwise qualified by high professional attainments will be considered.

STARTING pay for 5-day week of 42 hours in London between £605 and £1,120 (men) according to post-graduate (or equivalent) experience and National Service; maximum of scale £1,345; this salary scale is being increased by approximately 5 per cent; women will pay above £605 slightly lower but is being increased to match equality with men's in 1961; good prospects of promotion to Senior Examiner rising to £2,000 (under review); and reasonable expectation of further promotion to Principal Examiner.

APPLICATION form and further particulars from Civil Service Commission, Scientific Branch, 30, Old Burlington St., London, W.1 quoting S128/57 and stating date of birth. INTERVIEW Boards will sit at intervals, as required; early application is advised. [7411]

AEROPLANE and Armament Experimental Establishment Boscombe Down, requires—SKILLED men to serve as INSTRUMENT and electrical craftsmen, RADIO/RADAR and electronic craftsmen, for laboratory and aircraft installations work. AIRFRAME and engine fitters, for aircraft servicing and fitting of special equipment INSTRUMENT makers and precision machinists. RATE of pay for 44-hour 5-day week 182/4 plus 10/- merit lead or 182/4 plus 38/- merit lead according to experience. Prospects of reassessment of rate within three months, any increase back-dated to date of entry. Merit lead can rise to 70/-. Two weeks (88 hours) paid annual leave. Paid sick leave scheme. APPLY, giving details of apprenticeship and experience, to Air Commodore (Civilian Administration Office (WW)), A. & E. E., Boscombe Down, Amesbury, Wiltshire. [7506]

TELEVISION service engineers required, top rates of pay—bonus; permanent positions. Apply in writing to—

MR. R. COLBY (Manager), Service Dept., Cossor Radio & Television, Ltd., 51, Calthorpe St., W.C.2. [7581]

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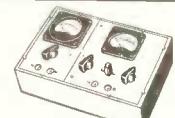
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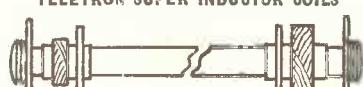
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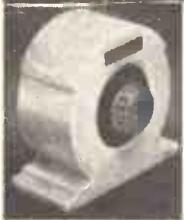


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FREQUENCY METERS type L.M.14. Crystal calibrated 125 Kc/s to 20 Mc/s., accuracy 0.01%. Battery operated, complete with charts and instruction booklet, plugs and sockets. Brand new surplus in original wrapping. Equivalent to the famous B.C. 221. Immediate delivery.

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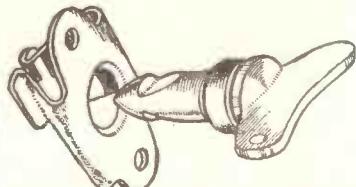
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SITUATION'S VACANT

UNIVERSITY COLLEGE OF NORTH WALES, BANGOR. APPLICATIONS are invited from physicists or electrical engineers for the post of lecturer in the department of electronic engineering. Candidates must have had research experience in some branch of valve, transistor or circuit electronics, or in solid state physics. Teaching experience, although desirable, is not essential. THE salary will be on the lecturer scale, with a maximum of £1,650 p.a., together with a family allowance of £50 per child and F.S.S.U. benefits. A salary at or near the maximum will be offered to a candidate with suitable qualifications. The date of appointment will be arranged with the successful candidate. TWO copies of the application should reach the undersigned, from whom further particulars may be obtained, not later than December 15, 1957.

KENNETH LAWRENCE,
Secretary and Registrar.

CITY OF BIRMINGHAM EDUCATION COMMITTEE. GARRETT'S Green Technical College, Garrets Green Lane, Birmingham, 33.

PRINCIPAL: B. C. Whitehouse, B.Sc., A.R.I.C. APPLICATIONS are invited for the following full-time teaching post. Assistant, Grade A. RADIO service work to Final Certificate standard.

IN assessing the initial salary, increments may be allowed for approved experience in industry or commerce. In addition to increments for training and degree or degree equivalent.

APPLICATION forms and further particulars may be obtained from the Principal (stamped addressed envelope), to whom completed forms should be submitted as soon as possible.

E. L. RUSSELL,
CHIEF Education Officer.

ROYAL AIRCRAFT ESTABLISHMENT, Bedford. FOR the following:-

ELECTRONIC Mechanics to serve as Research and Development Craftsmen Special on the repair and maintenance of aircraft or airfield radio/radar installations. Applicants should be familiar with modern V.H.F., U.H.F. and Micro Wave techniques. Appropriate service experience would be an advantage. Houses will be made available for successful married applicants coming from outside the district. Starting rate 182/4+38/- merit lead for 44-hour 5-day week. Rates are re-assessed within three months and any increase awarded is back-dated to date of entry. Two weeks (88 hours) paid annual leave. Paid sick leave scheme. Applications, giving full particulars of apprenticeship, training (including Forces Service) and experience, to Personnel Officer (F.W.), Royal Aircraft Establishment, Bedford.

ASSISTANTS (scientific).—The Civil Service Commissioners invite applications for pensionable posts. AGE at least 17½, and under 26 years of age on 1st February, 1957, with extension for regular service in H.M. Forces, but candidates over 26 with specialised experience may be admitted.

CANDIDATES must produce evidence of having reached a prescribed standard of education, particularly in a science or mathematical subject. At least two years' experience in the duties of the class gained by service in a Government or other civilian scientific establishment or in technical branches of the Forces essential in one of the following groups of scientific subjects:—

(i) ENGINEERING and physical sciences.
(ii) CHEMISTRY, bio-chemistry and metallurgy.
(iii) Biological Sciences.

(iv) General (including geology, meteorology, general work ranging over two or more groups (i) to (iii) and highly skilled work in laboratory crafts such as glass-blowing).

STARTING pay £355 (at 18) up to £485 (women £454) at 25. Men's scale maximum £665. Women's scale being raised to reach equality with men's by 1961. Somewhat less in provinces. Opportunities for promotion and further education. Five-day week generally.

FURTHER particulars from Civil Service Commission, Scientific Branch 30, Old Burlington Street, London, W.1, quoting No. S59/57.

INTERVIEW Boards sit at intervals as required. Early application is advised.

TRANSLATOR, German-English, free-lance, for electrical and electronic work, technically trained man preferred. Box 2298.

ELECTRONIC Mechanics required to serve as Research and Development Craftsmen Special.

STARTING rate 182/4+38/- merit lead for 44-hour 5-day week; rates are re-assessed within three months and any increase awarded is back-dated to date of entry.

TWO weeks (88 hours) paid annual leave, paid sick leave scheme.

APPLICATIONS, giving full particulars of apprenticeship, training (including Forces training) and experience to Personnel Officer (W.W.), Royal Aircraft Establishment, Bedford.

PART time television service engineer: Essex area: own transport required.—The Television Guarantor Co., Ltd., 3, Farrington Rd., London, E.C.1.

TELEVISION organisation, undergoing big expansion, has vacancies with above average earning potential, for capable, enthusiastic service engineers, in London and suburbs.

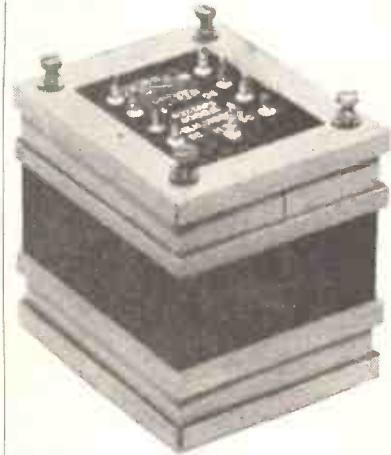
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Designed in 1956 this transformer anticipated future trends and we are confident it will meet the requirements of the most discerning amplifier engineer for a long time to come.

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This transformer is particularly suitable for the Osram 912 and Mullard 510 distributed load amplifiers.

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As used in performance measurements of the KT88 HIGH QUALITY AMPLIFIER.

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Types WO929/4 and WO930/4
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Type Nos. 9-VOLT.

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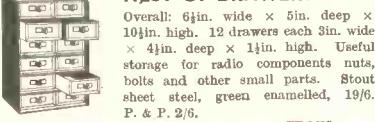
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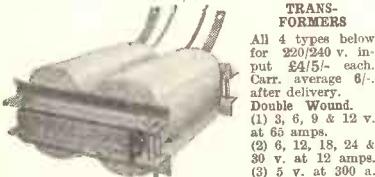
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Uses 1kg & 1.6kg Standard Flux Coated Electrodes. One bundle of each supplied with Welder. Extra Electrodes £1 per bundle.

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Overall: 6½in. wide x 5in. deep x 10in. high. 12 drawers each 3in. wide x 4in. deep x 1½in. high. Useful storage for radio components nuts, bolts and other small parts. Stout sheet steel, green enamelled. 19/6. P. & P. 2/6.



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SITUATIONS VACANT
ELECTRONICS and Instruments Section of Central Electricity Research Laboratories, Leatherhead, Surrey.—
REQUIRE an assistant engineer to assist in experimental testing and development work in the laboratory and in the field on radio and television interference from high voltage transmission lines involving field strength and voltage measurements at radio frequencies, calibration of equipment and analysis of experimental data.
CANDIDATES should have a degree or equivalent qualification and ability to apply a fundamental knowledge to a variety of problems. Salary £280-£295 p.a. according to ability. Application forms from D. Moffat, Director of Establishments, Central Electricity Authority, Winsley Street, London, W.1, to be returned by 31st December. Quote reference WWA/472. [7502]

TELECOMMUNICATIONS Radio and Line Transmission Engineer required by large organisation for position in technical publicity department.

APPLICANTS should be aged between 25 and 35 years and have a good general educational background with ability to write clear concise English; some knowledge of modern telecommunication techniques, including V.H.F. and U.H.F. multi-channel systems, frequency-shift signalling practices and multi-channel carrier telephone and telegraph systems, is essential. The position is on the established staff, with contributory Pension Fund.

APPLICATIONS with full details of age, education, experience to Box 2118. [7413]

HI-FI.—Vacancy for sales assistant with good technical and practical knowledge of all modern Hi-Fi equipment.—Berry's Radio, 25 High Holborn, W.C.1.

CATHODEON CRYSTALS, Ltd. require an experienced electronics engineer in their new research and development laboratories at Linton, Cambridgeshire.

An interesting and progressive appointment surrounding ideal conditions and in pleasant surroundings.

WRITE in confidence for further details, stating age, experience, salary required, etc. to Personnel Manager, Cathodeon Crystals, Ltd., Linton, Cambs.

TELEVISION engineers required with high standard of technical ability; salary £1,000; modern houses provided.—Baker, Murphy Dealer, Aberkenfig, Glam.

ELECTRONIC Engineers who are looking for the opportunity for original design and development work of a permanent nature are invited to apply to Pye, Ltd., Cambridge.

VACANCIES exist for junior and medium grade development engineers and technical assistants to obtain experience on projects involving the combination of the design of V.H.F. and U.H.F. circuits with the requirements of television and sound broadcasting equipment, and also the application of remote control and automatic circuits in this field.

APPLICATIONS should be addressed to the Chief Engineer, Pye, Ltd., Cambridge, quoting TXD.

GRADUATE in electronics or physics to work on spark machining developments; Central London laboratory; pension scheme.—Write, giving full particulars, to Box 2203. [7428]

T/V engineers required; must drive; excellent prospects for right men; salary from £750 p.a.—Apply E. Coyne, Ltd., 120/122, Ladbrooke Grove, W.10. Tel. Bay. 1947. [7424]

SEVERAL attractive and senior positions are offered in the development and industrial application of modern non-destructive testing techniques; the positions will be in the following fields:

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(3) PHYSICAL investigation and measurement. THEY offer good scope to men of initiative and experience in the above fields; salaries will be commensurate with the candidate's qualifications and experience.

APPLICATIONS should be made in writing in the first instance, giving full details of qualifications, previous experience, age and salary required, to Box 1834.

SERVICE Engineers required for leading South Wales firm holding main agencies: progressive position; accommodation if required.—Apply, giving details of experience and wages required, to Box 1967.

DEVELOPMENT engineers required for development of television receivers.—Apply in writing, giving details of experience, qualifications and age, to Personnel Manager, E. K. Cole, Ltd., Southend-on-Sea.

PLANNING engineers to control and co-ordinate electronic and mechanical projects; experience in estimating, planning, time and motion study desirable; a progressive position in expanding firm; high salaries, superannuation scheme.—Box 2317. [7440]

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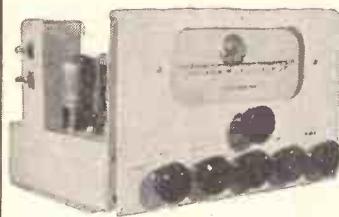
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PLEASE send brief details in confidence quoting reference MW.528, to T. E. Watson, Management Selection Limited, 17, Stratton St., London, W.1. No information will be disclosed to our clients until candidates know their identity and have given permission after personal discussion.

[7495]

MECHANICAL engineer required for leading radio and television works in the Midland area. Must be fully conversant with all techniques in radio and television manufacture.—Write, giving details of qualifications, experience, age, etc., to Personnel Manager, Box 2213. [7429]

TELEVISION Development Engineers (senior) capable of carrying out development projects with minimum supervision up to production stage; write, giving full personal details. Chief Engineer, Rediffusion Vision Service, Ltd., Fullers Way, Chessington, Surrey. [7463]

E. K. COLE, Ltd., Malmesbury, require production testers for testing radio, radar and nucleonic equipment; ex-Service radio and radar fitters suitable; full canteen and welfare facilities; transport from outlying areas.—Applications should be made to Personnel Manager. [7379]

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TECHNICAL writer required to take charge of publications section dealing with Radar, communications and other electronic equipment.—Please write, giving details of experience, qualifications, age and salary expected to Personnel Department (E.46), Murphy Radio, Ltd., Welwyn Garden City, Herts. [7474]

PROGRESS Planning Engineers required with experience of methods to produce electronic telephone and similar equipment; good progressive salary.—Apply with details of age, qualifications and experience to Personnel Officer, British Communications Corporation, Ltd., Exhibition Grounds, Wembley. [7486]

TELEVISION Development Engineer (Senior) with administrative experience required; capable of carrying out development projects with minimum supervision up to production stage.—Write, giving full personal details. Chief Engineer, Rediffusion Vision Service, Ltd., Fullers Way, Chessington, Surrey. [7276]

TELEVISION Development Engineers.—Two senior engineers are required for the development laboratory of an important company in a West London district. Applicants should hold good academic qualifications and have several years' experience in the development of black and white receivers and some knowledge of colour television.

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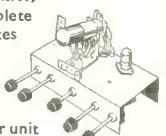
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TAPE Recorder Engineer wanted, must be fully conversant with all leading makes, especially Grundig; this position offers a unique opportunity for a top class engineer interested in advancement and will be extremely lucrative.—Apply by telephone Ealing 9661, or in writing: Edward Radio of Ealing, Ltd., 37-38, Haven Green, W.5. [7416]

ELECTRONIC Engineer with H.N.C. in electronics or equivalent qualifications, required for design of electronics test equipment and supervision of installation and maintenance of same; reply stating age, qualifications, experience and salary required.—Reply to: Personnel Officer, The British Thomson-Houston Co., Ltd., Carholme Rd., Lincoln. [7462]

RADAR and Instrument Fitter Civilian Constructors (male) required by Air Ministry in the provinces; appointments unestablished but good prospects of becoming pensionable; trade training, practical experience and ability to teach are essential; pay 705 at age 26 rising to £870.—Apply to Air Ministry, C.E.4k. (CIV72), London, S.E.1. [7464]

ELECTRONIC development engineers. A Midlands manufacturer has vacancies for junior development engineers for work on domestic television. Experience is preferred and minimum qualification is H.N.C. Those interested should write giving a full account of experience and qualifications to the Personnel Manager (Ref. EDE), Box 2214. [7430]

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RADIO technicians of all grades are invited to apply for interesting and varied positions in car radio servicing, installation and development. Vacancies occur from time to time for our dealers at all parts of the country; a high standard of practical and theoretical knowledge of radio technology is required.—Apply in the first instance to: Personnel Officer, S. Smith & Sons (Radiomobile), Ltd., North Circular Rd., London, N.W.2. [0270]

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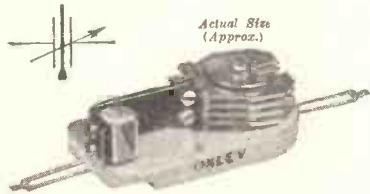
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TECHNICAL assistants (ref. 504) are required for experimental work on development of transistorised radar equipment; candidates should have radar or radio experience and some theoretical background, preferably to O.N.C. standard; these are new and permanent appointments in the expanding guided weapons field.—Write or phone (Elstree 2040) for interviews to Personnel Department, Elliott Brothers (London), Ltd., Borehamwood, Herts. [7450]

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An electronic engineer is required for transistor circuit development; applicants should have H.N.C. and experience of work on transistor circuit development preferred; candidates with experience as development engineers on thermionic valve circuit development will be considered; ability to learn new techniques and to apply this knowledge in circuit development essential.—Please apply to the Personnel Manager (Ref. 96B), de Havilland Propellers, Ltd., Manor Rd., Hatfield, Herts. [7458]

AMASSADOR RADIO & TELEVISION, Ltd., have vacancies for development engineers in their television and radio laboratories. Men of degree standard or its equivalent are preferred, but lack of recognised qualifications will not exclude, providing the applicant has a keen technical interest and possesses initiative; previous experience of this class of work is an advantage, but is not essential.—Write, in first instance, giving details and salary required to Technical Director, Princess Works, Brighouse, Yorkshire. [7501]

ABLE electronic engineers or physicists required for development of circuits associated with ultrasonics, flaw detection, a knowledge of ultrasonics is not necessary, but applicants should be familiar with pulse circuits, amplifiers and time bases, etc. starting salary £900/£1,100, minimum qualifications B.Sc. or H.N.C. with endorsements; interesting and varied work in a congenial team atmosphere.—Write giving details of qualifications, age, etc. to Ultrasonoscope Co. (London), Ltd., Sudbourne Rd., London, S.W.2. [7392]

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JUNIOR engineer required to assist in the development of a number of interesting projects including feedback amplifiers, high-speed pulse circuits, radio receivers and communication systems. This post offers an exceptional opportunity of acquiring knowledge of a new and rapidly expanding branch of Electronics as well as considerable scope for advancement. Starting salary according to age and experience; contributory pension and life assurance fund; applications should be made in writing to: The Personnel Manager, Thorn Electrical Industries, Ltd., Gt. Cambridge Rd., Enfield, Middlesex. [7435]

LEO COMPUTERS, Ltd.—Technical Assistants. There are vacancies in the Design Department for a number of young men to assist qualified design engineers in the design of electronic pulse circuitry used in large scale digital computers; while applicants should have a basic knowledge of electronic principles, theoretical qualifications are not vital; some previous practical experience with electronic circuits will be an advantage; commencing salaries according to age and experience: there is a 5-day, 37½-hour week, with canteen, social club facilities and pension fund.

WRITE stating age, qualifications, experience to: Personnel Officer, Leo Computers, Ltd., Minerva Rd., London, N.W.10. [7455]

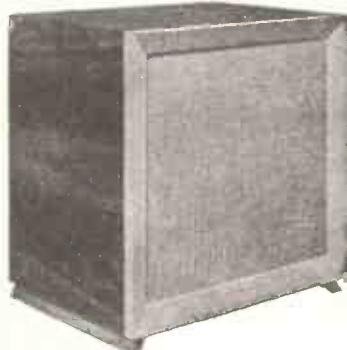
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[7360]

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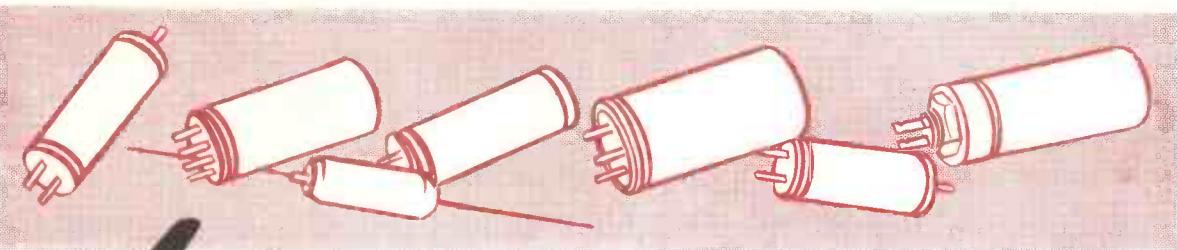
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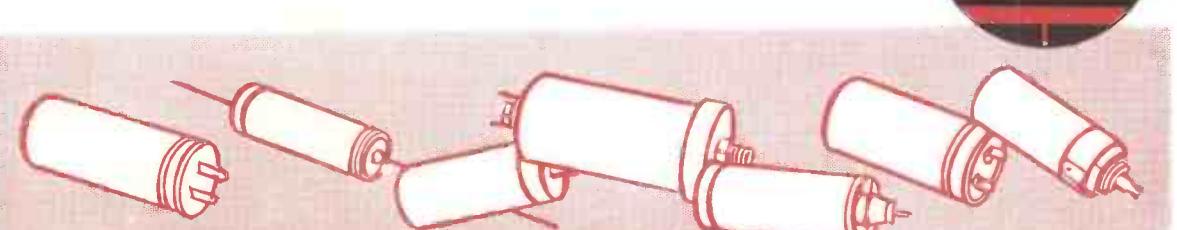
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