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## Wircoless World

ELECTRONICS, RADIO, TELEVISION

## NOVEMBER 1959

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Assistant Editors:
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VOLUME 65 NO. 10

PRICE: TWO SHILLINGS

## FORTY-NINTH YEAR

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#  

The first advertisement in this series discussed the frame grid valve in general terms, and outlined the advantages which it brings in the tuner and i.f. stages of a television receiver. We shall now look at the i.f. stages in more detail, with particular reference to the needs of fringe areas.


A circuit for an i.f. strip using the new frame-grid variable-mu EF183 is shown. It consists of a first i.f. stage which is common to sound and vision, followed by a second i.f. stage in each channel. Apart from component value changes, the only difference from normal practice is the use of $\pm 10 \%$ neutralising capacitors. When the strip is used with the frame-grid PCC89 in a cascode r.f. stage and the conventional PCF80 mixer, adequate gain is achieved for use in fringe areas without the addition of a further vision i.f. stage.
For Band III reception the maximum sensitivity required of a fringe area receiver is $20 \mu \mathrm{~V}$ for a picture of normal contrast level. Even for signals weaker than $20 \mu \mathrm{~V}$ a receiver of this sensitivity will give the best picture possible. (A higher sensitivity will produce excessive noise on the screen.) The Band I requirement is slightly less stringent and will in practice be easily met in a receiver which satisfies the requirements for Band III. With the strip shown, and with the PCC89 and PCF80 in the r.f. and mixer stages, $11 \mu \mathrm{~V}$ at the aerial will provide 2.0 V of video. A typical receiver with a conventional valve line-up (PCC84, PCF80, EF85 first i.f., EF80 sound i.f., EF80 vision i.f.) requires $63 \mu \mathrm{~V}$. Thus the conventional receiver fails to cover the required signal range for fringe areas, and it would need another i.f. stage. The frame-grid receiver, on the other hand, covers the range and has an adequate margin for production tolerances.
It will be noticed that the conventional PCF80 has been retained in the mixer stage. If the frame-grid PCF86 is substituted, then the second i.f. stages can be modified

to take the conventional EF80, with the EFI 83 retained in the first i.f. stage. With this new line-up, a $2 \cdot 0 \mathrm{~V}$ video
output is obtained with $9 \mu \mathrm{~V}$ on Band III and $5 \mu \mathrm{~V}$ on in the first i.f. stage. With this new line-up, a $2 \cdot 0 \mathrm{~V}$ video
output is obtained with $9 \mu \mathrm{~V}$ on Band III and $5 \mu \mathrm{~V}$ on Band I.
The circuit shown provides adequate a.g.c. on sound, and approximately 80 dB vision gain control without serious cross-modulation. Comparable performance is obtained
with the PCF86 variant. Both versions are notably cross-modulation. Comparable performance is obtained
with the PCF86 variant. Both versions are notably superior to conventional line-ups.

## National Science

SCIENCE is a method, a habit of thought which is practised not only spontaneously and individually for its own sake, as a rewarding personal activity, but collectively and deliberately as a means to an end in solving efficiently the problems of technology and economics. Pure science is at the same time infra- and supra-national in the sense that original thought is the work of individuals who have an affinity of interest with other workers in the same field regardless of race or creed. Applied science, on the other hand, has a military and market value and is consequently, and quite properly, a subject of political interest.

Under the pressures of expediency and in circumstances where the well-being of the community as a whole is involved the Government has voted money and accepted responsibility for scientific work of all kinds, from agriculture to atomic energy and from roads to radio. While some of this work is necessarily secret, much that should be more widely known is lost to view because it is considered either too esoteric or too dull to catch the popular fancy. At times like the present when satellites and moon rockets serve to make the man in the street conscious of the vast scale of scientific effort throughout the world it is natural that he should want to know what we in this country are doing to keep pace with the march of events.

Although questions of detail can be put to the Ministers responsible for the separate departments, it is not always easy to find where the responsibility lies because the labyrinth of Government Science is so complex that many of its byways are obscure, even to those with some knowledge of its main structure. The feeling is widespread that not enough is known about the deployment of national resources and effort in the scientific sphere, and this was no doubt partly the reason for the inclusion in the Conservative Party's election manifesto of a promise to appoint a Minister for Science responsible to the Cabinet for the overall promotion of scientific and technological development.
Wisely, we think, the new Government has resisted pressures to form a whole new Ministry of Science. This would have proved altogether too unwieldy and would have involved wholesale shifting of responsibilities, general disruption, and diversion of effort from the main business of research and development. The Government's
policy is to leave the various Departments to get on with their work, but to provide greater facility for the removal of possible antagonisms and to increase co-operation where this would be beneficial.
It is unfortunate, but inevitable, that there must always be a conflict of interest as far as the claims of civil and military science are concerned. In our own field this shows itself in the arguments over the allocation of radio frequencies. Whereas the claims of broadcasting and civil communications must be justified in the greatest detail, those of the fighting services are safe from public criticism behind the wall of "security." As we have said before, these conflicts can be resolved only by a minister of Cabinet rank who can be entrusted with the full facts on either side. In this respect the powers of the Minister for Science will be similar to those which he held as the Lord President of the Council. We hope that they will be exercised and that some means may be found of allaying suspicions that the military are hoarding wavebands as they sometimes do land.

The main functions of the Minister for Science will be to listen sympathetically and to talk persuasively, to release tensions and to reassure, and, if any real malfunction is diagnosed, to recommend treatment. The choice of Lord Hailsham for this post is, we think, a good one. Although not a qualified scientist he has already shown himself, as Lord President of the Council, to be en rapport with the scientific world. He will continue to have first call on the services of the Advisory Council on Scientific Policy and he will maintain contacts with the Royal Society, the Universities, the Ministry of Education and the Research Councils. Already he has said that one of his first tasks will be to forge closer links between Government research stations and the Universities in the belief that both stand to gain in prestige and effectiveness by more intimate association.

Not since the Restoration have the portents for British science been more favourable, and in Lord Hailsham this country has found the man to match the hour. His long political experience, his forthright approach, his interest in science and scientists and his ability to command and hold public attention qualify him not only to do those things which ought to be done, but also to let it be seen that they are being done.

# Travelling-Wave Valves 

## Mechanisms of Interaction Processes between Electrons and Fields

By C. H. DIX*, B.Sc., A.M.I.E.E.

THE object of this article is to describe in a rather more mechanistic way than is usual the interaction processes in the two principal types of travellingwave valves. By a travelling-wave valve is meant a valve in which two essential features are present:-
(1) The valve contains a guiding slow-wave structure which propagates an electromagnetic wave over the frequency range considered at a speed slower than in free space.
(2) There is a continuous interaction between the fields due to this wave and an electron beam.

There is then a convenient and important division which can be made.
(a) " $O$ " Type Valves. These are valves in which the interaction takes place in a region in which there are no d.c. electric fields. In these the electrons are injected at a velocity higher than that of the propagating wave, and cause it to grow by giving up kinetic energy. Focusing of the electron beam is usually maintained by a magnetic field parallel to the electron beam. The best known valve of this type is the helixtype travelling-wave tube, but as will be seen there are many others.
(b) " $M$ " Type Valves. These are valves in which there exist in the region of interaction electric and magnetic fields perpendicular to each other and to the direction of propagation. In these valves the velocity of the electrons in the direction of propagation remains constant, and the electrons can be thought of as providing a pivot for the interchange of potential energy between the d.c. and r.f. fields. Here, undoubtedly the most familiar example is the magnetron.
The nomenclature of " $O$ " and " $M$ " types is due to $R$. Warneche and his colleagues of the Cie. Generale de Telegraphie Sans Fil in Paris, who were prominent early workers in this field, and used the names "Carcinotron O" and "Carcinotron M" for the two corresponding types of backward-wave oscillator.
"O" Type Valves.-In this division the wellknown helix-type travelling-wave tube, due to $R$. Kompfner and J. R. Pierce, provides an easily understood introduction. The action of this can be described in the following way. Consider the r.f. fields due to a wave propagating along a helix.


Fig. 1. Helix dimensions. If the helix is wound so that there are (say) four turns per wavelength, so that approximately $2 \pi a$ $\sec \psi=\lambda_{o} / 4$ where $\lambda_{0}=$ free space wavelength (see Fig. 1), then the instantaneous r.f. electric fields produced in it
will be as shown in Fig. 2. These fields also, of course, extend outside the helix, but we shall only be concerned here with the fields within it

Roughly speaking, a wave propagates along a helix as though it were travelling at the velocity of light along the wire of the helix. The velocity of axial propagation is therefore approximately $v=c \sin \psi$, where $c=$ velocity of light.

Let us now consider a beam of electrons injected at just the velocity of this wave. If we imagine ourselves to be travelling with the electrons and the


Fig. 2. R.F. fields inside helix.
wave, we see that a given electron will experience a constant force due to the r.f. fields. Referring again to Fig. 2, it can be seen that electrons in the region AB will be accelerated towards B , while electrons in the region BC will be decelerated towards B . As the beam and wave move together along the tube, therefore, the electrons in the whole moving region AC will gradually collect in a small bunch at B , and this process will continue until the space-charge forces of repulsion of the electrons for each other intervene. (This repulsion gives rise to a saturation in the output power).

Considering now average velocities over the region in which this has been taking place, the electrons in the region AB have been accelerated by the r.f. field. They have, therefore, absorbed energy from the r.f. field, causing it to decay. Similarly, electrons in the region $B C$ have been decelerated by the r.f. field, and have given up the same amount of energy to it. Thus there is no resultant gain of energy by the r.f. field.
Looking at the beam, two additional properties have been added to it. These are a velocity modulation of the electrons, i.e. a periodic change in electron velocities along the tube, and a density modulation, or bunching of electrons.

Suppose now that the beam is injected at a velocity slightly higher than that of the wave, bunching will still occur, but since the electrons now start with a slight excess velocity, as the bunches start to form, they drift forward relative to the moving wave. Hence the bunches start to form not at B,

[^1]the point of zero r.f. field, as in the first case, but a little in advance of it, in the region BC , and hence are in a retarding r.f. field. We now have more electrons in the retarding r.f. field region than in the accelerating region. These elecirons continue to be retarded by the r.f. field so that there is a resultant gain of energy by this field, thus causing it to grow. The most forward electrons may pass right through this region, having given up only a little energy, and be rapidly accelerated through the next accelerating r.f. field region into the next bunch, when they again give up not only the energy gained in the brief acceleration, but also more of their initial energy. As the fields grow, they are more able to influence the electrons and hence to grow faster, and this can be recognized as typical of an exponential process. The wave then continues to grow as it travels along the helix, until saturation effects occur. The form of the gain curves is shown in Fig. 3, where output power is plotted against input power on logarithmic scales.

This process of bunching of electrons, i.e. ensuring that there are more electrons at places where the r.f. fields are such as to retard them and to gain energy, and less where the r.f. fields are such as to accelerate them and lose energy, is an extremely important and fundamental one, and forms the basis of all amplification by electron tubes.

This is an attempt at a physical description of the interaction in an " O " type travelling-wave tube. It is clear that the energy that appears on the r.f. circuit has come from slowing down the electron beam, i.e. decreasing the kinetic energy of the beam.

The essentials of an " $O$ " type tube would therefore appear to be:-
(1) An electron gun, to form a parallel beam and inject this into the circuit at an appropriate velocity.
(2) A slow-wave circuit, such as a helix, with coupling to a wave-guide or coaxial line input or output circuit at each end.
(3) A collector to receive the beam after it has passed through the circuit.
In addition, two other components are necessary:-
(4) Some means of preventing the beam from spreading out due to space-charge repulsion as it passes along the tube. A uniform magnetic field parallel to the beam is most frequently employed for this.
(5) An attenuator. The necessity for this is seen when it is realized that the bandwidth of the interaction process given by a helix is over an octave. If any reflection occurs at the output end of the tube, the reflected wave will be propagated back along the


Fig. 3. Gain characteristics of helix type tubes.

fig. 4. R.F. fields in a periodic circuit.
helix; if it is then partially reflected at the input end, the reflected part will again be amplified. It can be seen that if the voltage reflection coefficients at the ends are $\rho_{1}$ and $\rho_{2}$ and the voltage attenuation of the circuit is $\alpha$, then oscillation will occur if $\mathrm{G}_{\rho_{1} \rho_{2} / \alpha^{2}}$ is greater than 1 where $G$ is the forward electronic tube voltage gain. Typically we require $G / \alpha$ to be of the order of 50 , hence $\rho_{1} \rho_{2} / \alpha$ must be less than 0.02 over the whole bandwidth, a requirement very difficult to meet for small values of $\alpha$. We therefore arrange to have an attenuating region at least equal to the overall gain, so that, for example, to obtain an overall gain of 30 dB the attenuation might be 35 dB , and the forward electronic gain of the tube 65 dB . Even if total reflection occurs, the combined forward and return cold attenuation is now 70 dB , and the tube will therefore be stable. The attenuation is not usually distributed along the entire circuit, but is concentrated in a relatively short region near the middle of the tube, since if it is placed too near the input, in the region before the growing wave is predominant, it gives an excessive loss, while if it is placed near the output, it leads to a severe reduction in saturated maximum power.

Although a helix has a very great bandwidth it is difficult, especially at high frequencies, to obtain a high thermal dissipation with it. This arises from the fact that if, for a given circuit, we plot gain per unit length against $\gamma a\left(\approx \beta_{0} a\right)$ where $\gamma^{2}=\beta_{0}{ }^{2}+k^{2}$, $\beta_{o}=\omega / v_{n}, \quad k=\omega / c, \quad \omega=2 \pi \times$ frequency,$v_{o}=$ velocity of wave on the circuit, $a$ is the helix radius and $c$ the velocity of light, we find that the gain per unit length has a maximum for most practicable circuits which occurs between $\gamma a=1.4$ and $\gamma a=2$. Thus ra must be maintained between these limits. Now $\gamma a \approx \omega a / v_{o} \approx \omega a / u_{o}$ where $u_{o}$ is the beam velocity. Moreover, as will be shown, there is a maximum value of voltage or beam velocity $u_{o}$ which can be used before oscillations interfere. Hence as the frequency, or $\omega$, is increased, it is necessary to reduce the helix diameter to maintain $\gamma a$ within the required limits. For high powers, therefore, other circuits are used, which permit operation at higher voltages than can be utilised with a helix.
Space-harmonics.-In all our analysis we make the assumption that axial r.f. electric fields vary as exp [ $j(\omega t-\beta z)$ ] i.e. the $z$ variation along the tube is sinusoidal. If, however, we consider a practical circuit, it is seen that this cannot be the case, since at $r=a$ the axial field must be zero along the conducting boundaries. Thus, instead of varying as
shown by the full line in Fig. 4, the axial field will in fact vary as shown by the dotted line. The total :ield, therefore, can be considered as consisting of the fundamental component, our original sine variation, plus a series of fields due to waves having the same frequency, but travelling at different velocities. These are known as space-harmonics and it will be shown later that $\beta_{n}=\beta_{a}+2 \pi n / p$ where $n$ is a positive or negative integer and $p$ the pitch of the circuit. The complete field is then described by

$$
\mathrm{E}=\sum_{n=-\infty}^{n=\infty} \mathrm{E}_{n}(r, \theta) e^{j\left(\omega t-\beta_{o} z\right)} \cdot e^{-j \frac{2 \pi n}{p}}
$$

The important thing to note here is that, since $n$ may be positive or negative, both positive and negative space-harmonic velocities are involved, i.e. although the group velocity of a wave is in the forward direction, some of its space harmonics have phase-velocities in the opposite direction. Now we saw when describing helix interaction that the beam and the wave have similar velocities, and interaction then occurs between the beam and what we now recognize as the fundamental component of the wave. If, however, we had injected the beam with the velocity of the $n$th space harmonic, we should find that the interaction could be quite well described by assuming that it only interacted with that space-harmonic. If we consider field shapes due to periodic boundaries, it can be seen that the spatial distribution of the space-harmonic fields may be quite different from that of the fundamental, and that, in general, higher order fields decay more rapidly as we go away from the circuit.

To consider on a more physical basis how interaction occurs between electrons and space-harmonic fields, consider a circuit which has, at the edge of the beam, periodic conducting regions and gaps. Considering Fig. 5, the condition for forward interaction we have obtained is that the electron should go from A to $B$ in about the same time as it takes the wave to go the same distance, i.e. $n=0$ so that $\beta_{n}=\beta_{o}=$ $\omega / u_{o}$, where $u_{o}=$ electron velocity.

However, if while the electron is in the field-free region between A and B , the field at B reverses $2 n$ times, the electron, on arriving at B will be unaware of this, and will still interact with the field that it


Fig. 5. Space-harmonic interaction.


Fig. 6. Backward-wave interaction.


Fig. 7. Interdigital line backward-wave oscillator.
finds at $B$, since this is just the same field that it met in the synchronous case. If originally the transit time was $t_{0}$, the transit time will now be $t_{0}+n T$ where $T=$ period of r.f., i.e.

$$
t_{n}=t_{o}+\frac{2 \pi n}{\omega}
$$

The velocity will therefore be

$$
\begin{gathered}
u_{n}=\frac{p}{t_{0}+\frac{2 \pi n}{\omega}}(p=\text { pitch of circuit }) \\
=\frac{p}{\frac{p}{u_{0}}+\frac{2 \pi n}{\omega}}
\end{gathered}
$$

Hence $\beta_{n}$, which $=\frac{\omega}{u_{n}}=\frac{\omega}{p}\left(\frac{p}{u_{o}}+\frac{2 \pi n}{\omega}\right)$
i.e. $\quad \beta_{n}=\beta_{0}+\frac{2 \pi n}{p}$

This describes interaction between the $n$th forward space-harmonic, and would lead to broadband amplification somewhat as in the case of the fundamental.
Backward-wave Interaction.-Let us now consider interaction between a beam and a wave travelling in the opposite direction. Using still a similar circuit conception, but considering an electron now moving in the opposite direction as in Fig. 6, we see that as before, if the electron moves at a velocity such that it sees a similar field at each gap, interaction will take place. There is here, however, an important difference, since the wave has its group velocity in a direction opposite to that of the beam. Electrons crossing the gap B cause the wave amplitude at B to increase. This increase propagates to $C$ where a still further increase occurs, and thus we have a wave increasing in the opposite direction to that of the beam velocity. Since the amplified wave interacts with the beam, which then increases the wave further back along the circuit, if the beam current is large enough and the interacting length long enough, oscillation will occur, being initiated by r.f. noise in the beam which is always present at all frequencies. Moreover, this oscillation will occur at a frequency which will depend on the beam velocity, i.e. on the beam voltage, thus giving a voltage-tuned oscillator. Such a device is called a backward-wave oscillator (B.W.O.), and consists therefore of a circuit propagating a wave having a phase velocity in the opposite direction to its group velocity, coupled to an external circuit at the beam


Fig. 8. Cascade backward-wave amplifier.


Fig. 9. Crossed-field interaction.


Fig. 10. Electron motion in crossed fields.
injection end, and terminated in a matched load at the other end. The most frequently employed circuit is the interdigital line used in conjunction with a strip beam as in Fig. 7. The helix also can be used as a backward-wave oscillator circuit, but usually the oscillation frequency is much higher than the frequency which the helix would be used to amplify. As the velocity of the helix beam is increased, however, these two frequencies approach each other, and at a velocity corresponding to a beam voltage of about 10 kV they become equal. Any high-power amplifier would operate at a beam current far in excess of the start-oscillation current, hence such a valve would turn out to be a backward wave oscillator. This seriously limits the maximum powers which can be obtained from helix-type amplifiers.

If the beam current is insufficiently large, or the circuit too short, oscillation will not occur. An input coupling can be added to the other end of the circuit and we obtain instead amplification over a narrow frequency band, whose centre frequency is again determined by the beam voltage. This thus gives a selective voltage-tuned amplifier. Clearly the gain that can be obtained without oscillation will be limited. It may however be increased by the use of successive circuits, in a cascade backward-wave amplifier, depicted in Fig. 8.

A single circuit B.W. amplifier may run at say 0.9 of the oscillation starting current. This can give a useful gain, but with a very limited bandwidth. If the current is reduced, the bandwidth may be improved at the expense of gain. Using two circuits, it is possible to obtain satisfactory gain at about 0.8 of the starting current, hence giving an improved bandwidth, e.g. 10 dB with a few tens of $\mathrm{Mc} / \mathrm{s}$ at $S$-band (around $3,000 \mathrm{Mc} / \mathrm{s}$ ).
Crossed-field Valves (" $M$ "-type) with Linear Injection.-In the O-type valves, the efficiency is limited by the fact that only kinetic energy can be extracted from the electrons and that the process of efficient bunching is limited by the increase of spacecharge repulsion. These limitations are avoided in crossed-field valves, in which potential energy is
interchanged, and in which the r.f. bunching is formed by displacement of the beam without causing an increase in space-charge density.

In the simplest type of crossed-field valve, as shown in Fig. 9, there is an r.f. slow-wave circuit and a linear (parallel) electron beam is injected into the interaction region from a separate electron gun. Over the entire beam, and over the entire region of interaction, there is a static electric field $\mathrm{E}_{\mathrm{o}}$ between the r.f. circuit and another conductor, and a static magnetic field B at right angles to both the electric field and the direction of motion. Strip beams are usually employed, since it is convenient to use an interacting region of rectangular cross-section. The r.f. electric fields produced by the circuit are then of the form shown by the dotted lines in Fig. 9.

As is well known, an electron starting from rest under the action of crossed electric and magnetic fields follows a cycloidal path as shown in Fig. 10 in which the period of each cycloid is $2 \pi / \eta \mathrm{B}=2 \pi / \omega_{c}$ (where $\eta=e / m$ and B is the magnetic field) and in which the mean velocity $V=E_{o} / B$ where $E_{0}$ is the electric field. The distance covered in each cycloid due to the r.f. field $\mathrm{E} \sim$ is therefore

$$
\lambda_{c}=\frac{\mathrm{E} \sim}{\mathrm{~B}} \cdot \frac{2 \pi}{\omega_{c}}
$$

Comparing this with the r.f. wavelength $\lambda_{g}, \lambda_{g}=\mathrm{V} \frac{2 \pi}{\omega}$

$$
\text { i.e. } \lambda_{g}=\frac{\mathrm{E}_{0}}{\mathrm{~B}} \cdot \frac{2 \pi}{\omega}
$$

They are in the ratio

$$
\frac{\lambda_{c}}{\lambda_{g}}=\frac{\mathrm{E} \sim}{\mathrm{E}_{o}} \cdot \frac{\omega}{\omega_{c}}
$$

In a typical device, $\omega_{c}$ is of the same order as $\omega$, but the r.f. field $\mathrm{E} \sim$ is many times smaller than the d.c. field $\mathrm{E}_{0}$. The resultant electron motion is th erefore at right angles to the total electric field, in a series of small cycloids.

To see how the gain mechanism occurs, consider again motion in crossed continuous fields (Fig. 10). Electrons move with a mean relocity $\mathrm{E}_{y} / \mathrm{B}$ in cycloidal paths in a direction normal to both $\mathrm{E}_{y}$ and B . No mean work is done by the E field over any complete number of cycles, since the total electron displace-


Fig. 11. Electron mction in cembined crossed fields.


Fig. 12. Bunching mechanism in crossed-field valves.


Fig. 13. Effect of axial fields in crossed-field valves.


Fig. 14. Displacement of beam in crossed-field interaction.


Fig. 15. Crossed-field backward-wave oscillator.
ment in the direction of the field is zero. Consider now the addition of another field component $\mathrm{E}_{x}$, (see Fig. 11). This by itself will produce net motion in the $y$ direction, at a mean velocity $\mathrm{E}_{x} / \mathrm{B}$. These motions will of course add vectorially to produce net motion at right angles to the total field $\overline{\mathbf{E}}_{x}+\overline{\mathrm{E}}_{y}$ and the resultant motion will be as shown in Fig. 11.

The electron has, however, fallen through the additional potential $\mathrm{E}_{y} . y$ and hence an additional amount of work $e \mathrm{E}_{y} . y$ has been done on it by $\mathrm{E}_{y}$. It has also moved a distance $x$ against the force $e \mathrm{E}_{x}$, and has therefore given an amount of energy $e \mathrm{E}_{x} \cdot x$ to the field $\mathrm{E}_{x}$.

If both $\mathrm{E}_{y}$ and $\mathrm{E}_{x}$ are components of the same steady field E , then $x / y=\mathrm{E}_{y} / \mathrm{E}_{x}$. Hence the total energy interchange is $e\left(\mathrm{E}_{y} \cdot y-\mathrm{E}_{x} \cdot x\right)=\mathrm{O}$, as we should expect.
If, however, $\mathrm{E}_{y}$ and $\mathrm{E}_{x}$ are supplied by different sources, energy is absorbed from one and given up to the other, and the electron acts as a sort of pivot to allow the interchange to take place.
Let us now return to the situation in a crossedfield valve. The r.f. field can everywhere be resolved into transverse and axial components $\mathrm{E}_{t}$ and $\mathrm{E}_{z}$ and in addition we have the steady transverse field $\mathrm{E}_{o}$ (Fig. 12).

The mean axial electron velocity is always $\mathrm{E} / \mathrm{B}=$ $\left(\mathrm{E}_{o}+\mathrm{E}_{t}\right) / \mathrm{B}$. Therefore in the region AB , the electron velocities are increased, while in the region BC , where $\mathrm{E}_{t}$ is in the opposite direction to $\mathrm{E}_{o}$, they are reduced. All the electrons in this whole
moving region AC will thus gradually move towards the plane B, i.e., r.f. bunching will occur.

Now consider the axial r.f. field component $\mathrm{E}_{z}$ (Fig. 13). The mean electron axial velocity $u_{o}=$ $\mathrm{E}_{0} / \mathrm{B}$ is changed in both magnitude and direction to $u=\left(\overline{\mathrm{E}}_{o}+\overline{\mathrm{E}}_{z}\right) / \mathrm{B}$. The electrons again absorb energy from one component of the total field, $\mathrm{E}_{o}$, and give it up to the other, $\mathrm{E}_{z}$, and this process continues until the electrons finally arrive at the r.f. circuit, as shown in Fig. 14.

Summarising, the electrons are formed into bunches axially by the transverse r.f. field components, and at the same time displaced transversely by the axial field components. The beam therefore becomes displaced, as in Fig. 14.
Crossed-field Backward-wave Oscillator. This valve is the best known of linear-injection (parallel-beam) crossed-field valves. Like its O-type counterpart it has a beam which interacts with a wave having a phase velocity in the opposite direction to its group velocity, and is therefore a voltagetuned oscillator. The usual arrangement is as shown in Fig. 15. The curving of the axis is done to minimize the weight of the magnet.
Space-charge Amplification-Diocotron Effect. Even if no r.f. circuit is present, amplification can occur in an electron beam under the action of crossed fields. To see how this occurs, we observe first that a thin sheet of electrons is unstable. If we consider a layer of electrons, all repelling each other, as in Fig. 16, initially the electron at A is in equilibrium due to the forces on it from the other electrons. If, however, it is displaced to $\mathrm{A}^{\prime}$, these forces no longer balance, and it will be accelerated away from the sheet.
Now consider a thin sheet beam in crossed E and H fields, slightly perturbed by some r.f. disturbance. Its initial position is shown dotted in Fig. 17 and it is perturbed to the position shown by the full lines. The space-charge forces at the points $A$ and $B$ will be as shown by the full arrows, and because of the action of the crossed fields, the resultant motions will be as shown by the dotted arrows. There will therefore be an increase in charge density between A and B.
Next, consider a beam in which an r.f. disturbance to the charge density has arisen, as shown in Fig. 18. Due to the increased charge density at C , there will

Fig. 16. Displacement in an electron sheet.


Fig. 17. Effect of r.f. disturbance on a sheet beam in crossed fields.

Fig. 18. Effect of charge perturbation in a sheet beam in crossed fields.

be forces as shown by the full arrows acting on the electrons at A and B, and this will result as previously in motion as shown by the dotted arrows, giving the situation shown in Fig. 17.

Thus it is seen that any displacement perturbation will cause a charge perturbation, which will then increase the displacement perturbation still further, thus leading to a growing wave. Now perturbations are always present at all frequencies in the form of noise, and hence a crossed-field amplifier always acts as a noise amplifier, even without a slow-wave circuit. This limits its maximum useful r.f. gain, and crossed-field devices are principally used as high-power oscillators, or high-power low-gain output amplifiers.

## Continuous-injection Crossed-field Valves.-

 Perhaps the most severe limitation of linear-injection (parallel-beam) valves is the difficulty of designing electron guns with large cathode areas. The maximum current and therefore the maximum r.f. power obtainable is thus limited. However, it is possible to have the cathode at one side of the entire length of the interaction space, supplying electrons as fast as they are removed by the r.f. circuit, as in Fig. 19.This is, of course, done in the magnetron, which we now recognize as a crossed-field travelling-wave oscillator. Since the circuit is now re-entrant, the magnetron will oscillate whether the interaction is


Left: Fig. 19. Con ${ }^{-}$ tinuous-injection cathode.

Below: Fig. 20. Mog: netron.
with a forward or a backward wave.

There are also other types of travel-ling-wave microwave valves, but the " $O$ " and " $M$ " types cover the great majority of the valves now in use.

In the past, travel-
 ling-wave valves have found their main applications in radar and communication systems, and perhaps this will continue to be so, but increasing use is now being made of the much more refined performance offered by modern designs. Microwave television and telephone links, tropospheric scatter systems, aircraft navigation and approach systems, missile guidance and control systems and road traffic speed control are but a few of the increasing number of fields of application of such valves.

# Commercial Literature 

High-Vacuum Equipment including rotary and diffusion pumps, equipment which protects against power supply failures and leaks, solderless couplings, Pirani gauges and Geisler discharge tube pressure indicators. Booklet available from N.G.N. Electrical, Accrington, Lancs.
Regulated Power Supplies giving d.c. outputs from 200 V to 400 V with $6.3-\mathrm{V}$ a.c. outputs from separate transformers (to avoid effects of d.c. load variations). Stability is $0.02 \%$ for $\pm 10 \%$ mains change; ripple less than 1 mV . Details of the range and prices in a leaflet from Brandenburg, 139 Sanderstead Road, South Croydon, Surrey.
Resistors, fixed and variable; a catalogue giving very complete details of the whole range, and including ,rotary plete details of the whed strips, resistive "pills" and ignition suppressors. A price list is included. From Morganite Resistors, Bede Trading Estate, Jarrow, Co. Durham.
Time Calibrator, an electronic instrument producing a crystal-controlled train of marker pulses at intervals of $0.5,1,5,10,50,100,500$ and 1,000 microseconds, for checking timebase generators, pulse lengths, ctc. Specification on a leaflet from Cawkell Research and Electronics, Scotts Road, Southall, Middlesex.
Storage Oscilloscope using a 5 -inch Memotron tube with "infinite persistence" to avoid the need for photographic recording. Writing speed is better than $8 \mu \mathrm{sec} / \mathrm{cm}$. Trace erasure, by push-button or automatic means, takes less than 0.2 sec . Two identical $Y$ channels have a sensitivity of $10 \mathrm{mV} / \mathrm{cm}$ to $30 \mathrm{~V} / \mathrm{cm}$ and a bandwidth of $0-1 \mathrm{Mc} / \mathrm{s}$. Technical details on a leaflet from The Solartron Electronic Group, Thames Ditton, Surrey.
Transistor Portable Superhet for m.w. and l.w., a design using six Ediswan Mazda transistors and a germanium diode, delivering an output of over 200 mW , with a mean sensitivity of $90 \mu \mathrm{~V} / \mathrm{m}$ for 5 mW output. A ferrite rod aerial is used, and the total weight, excluding cabinet, is $3 \frac{3}{4} \mathrm{lb}$. Described in a 20 -page Application Report from Siemens Edison Swan, Radio Division, 155 Charing Cross Road, London, W.C.2.

Waveform Sampling Unit called the Nanoscope is an attachment for oscilloscopes which allows fast repetitive waveforms of a few millimicroseconds duration to be displayed on an ordinary c.r.o. with a bandwidth not exceeding $50 \mathrm{kc} / \mathrm{s}$. Principle was described in the March, 1959, issue
(p. 131). Described in a leaflet from Lion Electronic
Developments, Hanworth Trading Developments, Hanworth Trading Estate, Hampton Road, Feltham, Middlesex.
Epoxy Resin Adhesives, a useful booklet showing how to use Araldite for joining various materials. A table lists the materials and indicates which type of Araldite to use and whether any preliminary treatment is required. Another chart gives the properties of the various resins in the range. From CIBA (A.R.L.), Duxford, Cambridge.

Moisture Meters, based on a capacitor detecting element with a hygroscopic dielectric and capable of indicating 1 part in $10^{6}$ of water vapour in dry air or gas. Response time: 1 second. Illustrated leaflet giving details of a large range of instruments from Shaw Moisture Meters, 31 Market Street, Bradford, Yorks.

Independent-Sideband Transmitter, designed for simplicity of operation and economy in operation. Any one of four spot frequencies in the range $2-20 \mathrm{Mc} / \mathrm{s}$ can be selected readily by an unskilled operator. Output is 250 or 350 watts (peak envelope power) into $50 \Omega$ unbalanced coaxial feeder. Technical summary on a leaflet from Marconi's Wireless Telegraph Company, Chelmsford, Essex.
Portable Audiometer for pure tone threshold measurement by air and bone conduction, with a range of $125-8,000 \mathrm{c} / \mathrm{s}$. A filtered white noise masking generator provides seven separate noise bands for each test tone used, and each noise band has a width of $+5 \%$ of the tone frequency. Described in a folder from Amplivox, Beresford Avenue, Wembley, Middlesex.

Precision Helical Potentiometers, three-turn and ten-turn types, with maximum values between $40 \mathrm{k} \Omega$ and $500 \mathrm{k} \Omega$. They have positive end stops and can be supplied with various bearings and mountings. Linearity is $\pm 0.3 \%$ and resistance olerance $3 \%$ Leaflets from General Controls, $13 / 15$ tolerance Croft, Honywood Road, Basildon, Essex.
Hall-Effect Devices, mainly probes for detecting and measuring magnetic fields, but also including modulators and multipliers. An informative catalogue, including a section on the principles and construction of the devices, from Siemens and Halske (Germany), through the U.K. distributors, R. H. Cole (Overseas), 2 Caxton Street, London, S.W.1. Also a leaflet on Semiconductor Photoelectric Devices of high sensitivity to light.

# Words, Words, Words 

By P. P. ECKERSLEY, M.I.E.E., f.I.R.E.

Polonius: What do you read, my Lord?
Hamlet: Words, words, words.
"FORCE, Energy, Power, whatever you like to call it"-thus a practical man explaining a practical invention. There seemed to be a considerable scope for making a choice, but the need for a knowledge of fundamentals in doing so.

Those who might smile tolerantly at the practical man's naivete, do they always use the right word in the right place? I doubt it and it is my purpose to call attention to some of the solecisms of common usage-and, likely as not, when pointing the sins of others, I shall commit like ones myself. I hope so; the subject needs ventilating.

The accusation of pedantry coming from those whose work depends upon accuracy of concept and execution has a hollow sound. The excuse for abusage that "you know what I mean" neglects those, new to some aspect of technology, who do not.
And now for some examples. Circumstances have lately determined that I should become familiar with electro-mechanical relays. A newcomer, I was surprised to find a general use of the term contact pressure instead of contact force. "Fifty million so and so's can't be wrong!" The point is that normally they are; in this case although "everybody uses it " everybody is wrong. Need I add that pressure is determined by area-and that the area of a contact can vary by thousands of times?

I recently attended a lecture on d.c. amplifiers and listened, with growing astonishment, to an exposition which associated-indeed stressed-the characteristic of "bandwidth" in relation to "d.c." So soon as the cognoscenti had contributed to the discussion I sprang to my feet, asking to be put out of my misery-I said that I had hitherto associated zero frequency with direct current now it seemed that a d.c. amplifier was also an a.c. amplifier-why?
"I suppose," said the lecturer, "that you would expect zero bandwidth." Falling into the urap I said "Yes" and rebuked myself for so doing. An amplifier with zero bandwidth would, of course, never respond to any change of input; I did, however, ask why it was necessary to provide any wider frequency response than would ensure a reasonable build-up time.
The answer, which perhaps many readers know, is that a so-called d.c. amplifier is designed to amplify pulses, i.e. waves in which the rate of change of amplitude over a considerable time period may be zero, but also very rapid over short ones. Why cannot we use the term "d.c.-a.c. amplifier" to describe a device which has to amplify both d.c. and a.c.?

It would be quite possible that anyone discussing the performance of "d.c. amplifiers" would have said that they had to amplify "square waves." Here
is another inaccuracy, a better term would be "rectangular waves."

An affectionate recollection is an old friend (B.A.Cantab.) talking about "Ohm's Law for Alternating Current." To my inquisition "Tell me, what is this Law, what's its nature-indeed its virtue?" the simple reply was "You know, $I=E / \sqrt{R^{2}+X^{2}}$." We now learn that in fact Ohm never postulated a law and that if he had it would not have been one. We are, I think, more concerned here with the interpretation of the word "law" than any question of confusion between impedance and resistance. The O.E.D. defines a " natural law" as a " correct statement of invariable sequence between specified conditions and specified phenomenon" and gives examples such as "the laws of motion, three propositions formulated by New-ton"-I cannot help adding that forty or more years ago I (Certificate of Technology, Manchester) always referred to "Ohm's Law for alternating current." "If age could do and youth but knew."

## Overworking the Bel

The Bel is very elegant, but, like the third person singular, it wants watching. If, basing our calculations on voltage or (less likely) on current ratios, we say that an amplifier has a gain of so and so many dB and if we know the input and output resistance no one can cavil. If however the input resistance is that of the grid to ground resistance of a valve when worked in class $A$ connection there can be some indefiniteness about "dB gain." In my submission the right way to define the input resistance of an amplifier, when the grid to ground circuit is not shunted by a resistor of known value (and therefore is very large or, as some say "infinite") is to say that it is equal to the internal resistance of the source which generates the input voltage. We then postulate an optimum input power matching, even though it may not exist, only in this way have we any right to speak of power gain. The gain, using input volts to represent power, as is too often wrongly done, will seem to be 6 dB greater than the real power gain with the postulated matching at the input.

All this may seem pedantic-it probably is-but so-called pedantry is the only recourse when terms are defined accurately and used carelessly.

A much-respected author of a textbook on radio furnishes us with a glaring example of this carelessness when he publishes a graph showing the gain in current (by cancelling inductive by capacitive reactance) on a scale of decibels. If the gain had been expressed in nepers, a unit which is, by definition, based on a ratio of currents, no one could object.

There does seem to be a modern tendency to enlarge the scope of the decibel: what we seem to lack is an offspring of the neper, with a base of 10 rather than e, when we should be able to express gains on a logarithmic scale but in terms of voltage
and current without the confusion that power too often introduces.

Great fun may be hac with detection and demodulation. My authority (B.S.I. 204:1943) deprecates either "Demodulator" or "Rectifier" for "Detector"-the latter, says the Glossary, is "a device, having non-linear conducting characteristics, used for detection."

I should have thought that there is, in fact, a distinction between a detector and a demodulator. While the detector has " non-linear conducting characteristics" the demodulator essentially has not; it involves a modulator in association with an oscillator (or at any rate demands a source of oscillations) to make it function. The process of disentangling information from the carrier which bears it can be consummated either by a detector or by a re-modulation of the carrier (by a so-called demodulator) and agreeable as it is to deprecate confusion between the processes it is surely right to make a distinction between them when each has the same end product.

The term modulator is defined by B.S.I., not very bravely, as " a device for producing modulation" and modulation is defined, very generally, as "the process by which the amplitude, frequency or phase of a carrier wave is modified in accordance with the characteristics of a signal." The significant word here is "signal," meaning, one supposes, the electrical equivalent of some intelligence that is required to be transmitted or, as some say, " modulated on" to a carrier. On the other hand, there is a usage, in line transmission, which embraces the term "group modulation." The process of group modulation adds or subtracts a constant frequency to or from the several carriers of a group of channels of communication, it is therefore basically a method for frequency changing and yet it is characterised as modulation. We know that modulation does in fact produce a change of frequency and so it is possible to look upon carrier transmission as, at the sender (not transmitter), a means to add a constant carrier frequency to the audio frequencies representing the intelligence and, at the receiver, means to subtract it (by detection or demodulation).

Thus transmission involves frequency changing and frequency changing involves modulation! It is also a pet hobby of mine to demonstrate that the action of a detector can be simulated by modulating the carrier by a rectangular wave of unit amplitude.

The only serious criticism relevant to this aspect of terminology is the use of the term group modulation instead of group frequency-changing or something of the sort.

## Rearguard Losses

I greatly admire the efforts of those who serve the B.S.I.; they are the standard bearers of a regiment fighting a rearguard action in defence of logical terminology against the ponderous army of lazies who prefer abusage and cite usage as their support.
"Habit," said Wellington, " is ten times nature." The lazy lie back on their comfortable cushions. "I've always called it that and I don't care if it is illogical; you know what I mean."

There is no need to despair. For instance, 50 years ago we called the receptacle for an electric charge a capacity or, worse, a condenser; now, except in proper names remembering the past, all but the belligerently conservative call it a capacitor. The
same goes for resistor and inductor. I have yet to hear of the "impedor"; rearguards inevitably suffer their losses.
A friend and colleague, who like myself is sometimes described as pompous when it comes to terminology, seldom misses an opporunity to favour "transconductance" rather than the accepted " mutual conductance." What, he asks, is mutual about it? On the other hand B.S.I. defines "mutual conductance" as "the control-grid to anode transconductance" .. leaving this writer a little puzzled. Would my friend define transconductance as the control-grid to anode mutual conductance? I must ask him.
Another jehad (jihad I am now instructed) which he eloquently fights is against the term space-factor as applied to windings of insulated conductors. "Copper factor," says my friend, "it points the term with far more precision." I have remarked that we do happen to wind insulated resistance wire on bobbins. Perhaps "conductor factor" or "metal factor" would therefore be more to my friend's point.
Do you, gentle reader, plot a graph or a curve? I think you ought to plot a graph otherwise a straight line becomes a curve! Many refer to an oscillograph when it is not making a graph and an oscilloscope when, plotting a graph, the trace may be invisible.

## Ionic Wanderers

I must say I defend the term valve, most of all when it is "hard." Of course the word valve has many meanings, for instance it is "one of the halves or sections of a dehiscent pod, pericarp or capsule (1760)," but in a less esoteric category, it is "that which controls the flow of vapours or liquids" so why not that which controls the flow of electricity? Tube! Pooh!

But I doubt "thermionic," certainly the cathode is hot but does it emit ions or if it does are these what are chiefly present? I was taught to believe that while "ion" is " neut. part. of eimi, to go," it also has an association with a- wanderer. An Ionian was a " member of part of the Hellenic race which occupied Attica, Western Asia Minor, etc." I sense movement of tribes as inquisitive wandering rather than purposive going. So if ions are wanderers and surely electrons, rushing down a potential gradient cannot be classified as such; their movements, once escaped from a space charge, are purposeful; even their bunching is controlled, few are in a condition to wander.
My purpose has been to cire a few examples where usage is either cruel to logic or murders it. There are many more examples, for instance binaural (I always listen to my loudspeaker with both ears), shot noise (it is an effect not a noise), resistance coupling (not so good for a.c. amplification without an associated capacitor), volume control (when used instead of gain control), potentiometer (which measures nothing), mixer (which sounds culinary but is too often a synonym for a frequency changer) the term constant (when coefficient is usual) envelope (when bulb is less pompous) frequency distortion (how do you distort a frequency?) electronic relay (the term relay belongs to electro-mechanics, the similarity to, for instance, a thyratron is too remote)-and so on and so forth.

1. ask for short terms which read as directly as possible on to the concept, or the devices which they
describe. Most of my examples have been concerned with devices; it will be perhaps of some interest to examine some terms of a less concrete, more abstract nature.
With the Editor's consent I will live dangerously and dare to consider the term "wireless". I must condemn its general use (and therefore range myself for once with a majority) but welcome its continuance when forming part of a proper name. Contrary to the implications of the dictum that "a rose by any other name would smell as sweet" I believe the world would lose a very proper name if "wireless" were divorced from it. The same sentiment attaches to the name of a famous company. Names are in a different category from technical terms, they have ancestry, they are property, they preserve tradition and therefore support history.

## Picture Broadcasting

A certain dubiety about using the word television to define picture broadcasting arises from an anticipation of a semantic embarrassment (a truly "precious" sentence!). What name shall we give to it when we can see as well as hear through the telephone? Telegraph, telephone, television-these are names describing a logical evolution of line and radio communication. We do not however describe sound broadcasting as "telephone": why is picture broadcasting called "television"? It would be a quixotic task to attempt to do away with the term television (and its degradation to "the Telly") and I doubt if it will concern me personally when, many years hence, one subscriber to the telephone service may see another when speaking to him (notably her) but, always seeking logical terminology, I am concerned with another defiance of it.

How I dislike the compressions, but I can be sure that the utilitarians will justify their uglies. A product now has "manufacturability," a picture "viewability" (why not fightability or boxability for the man with a fast right hand?) Mocking laughter would doubtless be the only comment on a suggestion that a product was "susceptible to manufacture," that a picture had some particular quality which the lazy writer hides under an ugly compendium word which might just as well be "good" for all it says. For an example of a different nature the hideous plural of spectrum as spectrums is not only a barbarism but offends the modern compulsion to shorten-it has two more letters in it than spectra. But what's the good of being an angry old man? Perhaps jargon is a necessity to those whose minds are crammed full of facts.
I propose now to discuss the art and practice of writing, meaning putting thoughts into sentences which are both clear and concise.
I say (with fear of contradiction) that it is the poet who reaches the heart of the matter more surely than any philosopher, idealogue, or man of science ever does or did. It would be altogether unfair to my thesis to interpret it as denying value to prose writers and thinkers who with their disparate styles and contrasting idioms have contributed so much. I still maintain that the penetration to the heart of the matter is more illuminatingly discovered, more concisely expressed when the poet speaks. In an attempt to lower technical eyebrows let me explain by example. Read Pope's Essay on Criticism, and take as an observation relevant to my text about accuracy
of expression that "a little learning is a dangerous thing "; learning, be it clear, not, as so often misquoted, knowledge. It is the little learning, badly digested and sickeningly regurgitated which offends. Again when the poet wrote that

## " The strongest poison even known Came from Caesar's laurel crown"

was not this the heart of the matter, concentrated into two lines of verse?

What saner outlook upon the evils and joys of drinking than Chesterton's.
"Good drink that is dishonoured by the drunkards of the town"?
And in the admirable example in the lines which follow the dictum about the dangers of a little learning
"Drink deep, or taste not the Pierian spring.
There shallow draughts intoxicate the brain,
And drinking largely sobers us again."
It would be possible to multiply examples page by page but let a simple story suffice. A young man was taken to see Hamlet. Asked what he thought of it he replied, "Not much, it's full of quotations."

Only the "pale cast of thought," the evil of thinking divorced from sensibility can, and probably will, attempt to deny the truth of what I so confidently preach.
The false deduction from my argument that I want all technical writing done in verse would be as silly as it would be unfair. What I am driving at is to ask technical people to take an interest-a deeper interest unfortunately than some modern education permits-in the humanities, in literature, in poetry; because not only will they thereby find more numerous sources of enjoyment but also, when they write about their discoveries, inventions, or the more pedestrian accounts of laboratory experience, they will do it better and enjoy doing it more. The exemplar for any writer is the poet, for, in the final issue, he goes to the heart of the matter, he expresses himself concisely, and his compression gives his words a pungency which for ever preserves them.

I must say, in passing, that I mean by "poet" one whose works are or will be immortal and not one who, for fear that someone will discover the barrenness of his mind or heart, hides all meaning behind a thick shrubbery of words.

## Faraday's " Researches"

There is, in the sense I am trying to express, a poetic quality behind for instance Faraday's "Experimental Researches in Electricity." Here is the proud humility of genius, simply and nobly expressed. I think students of science and technology should be made to commit paragraphs of it to mind and so to heart. Notably those Victorians who studied "natural philosophy" (which was the synonym for what we now call science) always wrote well; some wrote excellently; all of them had an education which embraced the arts; many of them could be described as cultured.

Without wanting even to seem to sneer I would wish that more of those who are growing up to be engineers, scientists, technicians (what you will) were given a better opportunity to study, understand and enjoy the humanities. For it is my conviction that not only would the style of technical writing be improved by more familiarity with the humanities;
but also the value of the work, about which reports might be written.

I sympathize with those who find difficulty in explaining their ideas and observations in writing. Many who excel in talking seem to be overcome by self-consciousness when it comes to the grim business of putting thoughts on paper. There are, of course, cases where a plethora of speech disguises a " little learning" and when writing reveals a vacuum, and other cases where the hand which holds the pen becomes either paralysed or overstimulated. Did I hear a whisper?

The first principle in writing technical reports is simplicity; the first sin, prancing. Simplicity says "the cat sat on the mat," prancing might say "a member of the feline species, classified among the small mammals, took up a recumbently characteristic position upon the fibrous and movable floor covering." A second principle is order, meaning the logical development of the story from its basic simplicities to its more complex aspects and so to a clearly expressed conclusion. For instance, signposting the way for a development report, I would suggest this order, namely, objective, methods of achieving the objective, difficulties encountered, the outcome, and so a conclusion.

I have used the word prancing to describe what is to me an altogether abhorrent style of writing. Rather than attempt precisely to define what I mean by the term I will give an almost perfect example of it. The writer is concerned with an explanation of why a thermistor does not produce amplitude distortion in alternating currents flowing through it; he writes:-
"Now the current arising from the application of an e.m.f. if allowed to flow long enough (the writer's italics) will cause a change (of) resistance and therefore voltage/current ratio. By a process of confused thought this change is often adduced as a reason for saying that the device is a nonlinear resistor, but, in the interests of clarity, this error should be avoided."
Here is a pawky sentence, smarmed over with tautology, that ends up (by "a process of confused
thought") in arriving at a totally wrong conclusion. Maybe it's just forgivable to get all superior when you are right, it's damnable to prance publicly when you are all wrong.

It is, however, not so easy to explain the action of the thermistor simply, but a good exercise to try. In attempting the difficulty we might say that the resistance of a transistor varies markedly with its temperature and hence with the amplitude of a current flowing through it. However, the mass of material comprised by a thermistor is large enough to prevent its resistance from following rapid changes of current amplitude. Thus when the currents passed through a transistor are alternating the resistance of the device attains a mean value and therefore does not cause sensible waveform distortion; albeit a thermistor is properly classified as a non-linear resistor.

My objection to the original, apart from its sneer at those who "often adduce" a reason for saying what is in fact true, is that it combines tautology with pretentiousness; we do know the relationship between resistance and the voltage/current ratio and generally speaking there is no need to talk down to us.

But when all's said and done, writing, be it of belle-lettres or technical reports, is beset with difficulties. Someone described it as "chipping words out of one's breast bone "; the sharper the pen the more painful the process. It is the very fact of its difficulty which makes the practice of writing so fascinating, so worth while. Moreover, as many have discovered and many more will discover, the business of attempting to write a description of a technical process, a device, a discovery, or whatever often proves to the writer that he may not understand the subject he is forced to write about as clearly as he thought he did.

Coming to an end of this preaching and reading over what has been written leaves me with the usual dissatisfactions. If I have, here and there, given to any one reader the desire to do well what, without false modesty, I feel I do not do well enough, then perhaps a labour of love is not lost.


THE full-line curves indicate the highest frequencies likely to be usable at any time of the day or night for reliable communications over four long-distance paths from this country during November.

Broken-line curves give the highest frequencies that will sustain a partial service throughout the same period.

............ fREQUENEY BELOW WHICH COMMUNICATION SHOULD BE POSSIbLE
FOR $25 \%$ OF THE TOTAL TIME
—— - predicted median standard maximum usable frequency
—_ frequency below which communication shoulo be possible
ON ALL UNDISTURBED DAYS

## Public Radio-Telephone Service

THIS country's first mobile radio-telephone service linking suitably equipped cars with the public telephone system was inaugurated by the new Postmaster General, Mr. Reginald Bevins, on October 28th. Initially the pilot scheme is limited to cars operating in the southern half of Lancashire, the Wirral and parts of north Cheshire. These areas are covered by two base stations, one at Liverpool and the other near the I.T.A. television station at Winter Hill, near Horwich.

The service is conducted on five channels around $160 \mathrm{Mc} / \mathrm{s}$ with a $50-\mathrm{kc} / \mathrm{s}$ separation. One channel is used for calling, for which a loudspeaker is fitted in the receiver. The conversations are conducted on one of the remaining four channels; the exchange operator advising the occupier of the vehicle to which he should switch, depending on the position of the car in relation to the two stations. Frequency modulation is used and the standards employed are those adopted for the v.h.f. maritime services-a maximum deviation of $\pm 15 \mathrm{kc} / \mathrm{s}$, pre-emphasis and de-emphasis of 6 dB per octave within the band 300 $3,000 \mathrm{c} / \mathrm{s}$ and frequency tolerances of $\pm 2 \mathrm{kc} / \mathrm{s}$ for the base station and $\pm 3 \mathrm{kc} / \mathrm{s}$ for the mobile station.
Transmitters and receivers for the base stations have been supplied by Pye, whose mobile equipment, Type PTC8205, has received Post Office approval for fitting into vehicles. The car installation costs £195, or it can be rented at 30 s a week. The Post Office licence for the "Radiophone" service, as it is called, is $£ 710 \mathrm{~s}$ a quarter. A three-minute call costs 2 s 6 d .

## Technical Training

IT has become the tradition for the new president of the Institution of Electrical Engineers to review in his inaugural address the sphere of industry with which he has been most closely associated. The new president, Sir Willis Jackson, who, to use his own words, "is identified with the preparation of young people for careers in electrical engineering," did not depart from this practice at his installation on October 9th, and took for his subject "The making of professional engineers." Having first reviewed the contribution made by schools, universities and colleges to the education of technologists, Sir Willis went on to discuss the shortage of industrial training facilities which has become "the Achilles' heel of our national plans for the further development of technological and technical education."
In the past comparatively few firms have "had the foresight to provide training facilities," but "responsibility for training the increasingly large national pool of technologists and, no less important, of technicians and craftsmen " cannot continue to be carried by these few firms. Sir Willis stressed once again that this problem could be solved only if the smaller and more specialized firms will collaborate in the organization of group schemes in which their limited individual resources are properly coordinated.

## B.B.C. Annual Report

REFERENCE is again made in the annual report of the B.B.C.*-as it was last year-to "the very serious threat to television reception in Eand I" which the continued expansion of forward-scatter services represents. The interference is particularly bad in areas served by stations operating in Channel 1. Guidance has been given by the B.B.C. to dealers on methods of reducing the effect of the interference which depends to some extent on the design of the receiver, and the attention of set manufacturers has been drawn to this point.
The 161-page report covers most aspects of the Corporation's work and administration. Here are some points:-
A total of 26,689 schools (about $71 \%$ of the country's total) were registered as listening to school broadcasts in the year under review.

The Corporation's income from licence fees increased by over $£ 2 \mathrm{M}$ to $£ 27,323,115$ and its net revenue from publications rose to $£ 1.14 \mathrm{M}$.

Of the $£ 7.29 \mathrm{M}$ expenditure under "engineering" for the national sound and television services $£ 4.62 \mathrm{M}$ was for television-an increase of $£ 0.75 \mathrm{M}$ during the year.

Rental paid to the Post Office for lines exceeded £1M.
*"Annual Report and Accounts of the B.B.C. 1958-59"
Cmnd. 834, H.M.S.O. 8s.

## Broadcasting in Kenya

SINCE 1931 the broadcasting service in Kenya has been conducted by Cable and Wireless and its predecessor Imperial and International Communications. The 25 -year charter held by Cable and Wire-


ESTIMATED SERVICE AREA of the two I.T.A. stations which will serve the south-west of England is shown (shaded) in relation to the primary and secondary service areas of the St. Hilary station. The two stations, one near Axminster and the other near Liskeard, will be operated jointly by one programme contractor. They are planned to be in service early in 1961.
less, which was extended for a further three years, expired on September 30th and the Kenya Broadcast:ng Service set up by the Kenya Government came into operation the following day. The director of broadcasting is C. P. Jubb and the chief engineer Grahan Phillips, both seconded from the B.B.C.
Four new $10-\mathrm{kW}$ transmitters at the main transmitting station at Langata, near Nairobi, have been supp'ied by Marconi's-two for operation in the m.f. band and two in the h.f. band. The service also uses a number of existing transmitters at Mombasa, Kisumu and Nyeri, which have been transferred from Cable and Wireless.

Test Card C.--Since our correspondent, K. Dice, wrote his letter (see page 507) referring to "Diallist's" recent plea for more test card transmissions, the B.BC. and I.T.A. have announced a new schedule. This provides that at any time during the morning trade tests from 10.0 to 1.0 a Test Card C will be available from one or other of the two stations (B.B.C. or I.T.A.) serving an area.
I.T.A. Northern Ireland television transmitter at Black Mountain, outside Belfast, was brought into service on October 31st. It operates in channel 9 using horizontal polarization. The directional aerial on the $750-\mathrm{ft}$ mast is nearly 1700 ft above sea level and gives an e.r.p. of from 20 to 100 kW according to direction. Ulster Television Lid. are the programme contractors for the station which has been equipped by Marconi's.
E.I.B.A.-Among the donors listed in the annual report of the Electrical Industries Benevolent Association are the Radio Industries Club (London and Manchester), the B.B.C., British Radio Equipment Manufacturers', Association; British Radio Valve Mayufacturers' Association; Electronic Engineering Association; Radio and Electronic Component Manufacturers' Fede:ation and many firms in the radio and electronics industry. During the past twelve years the number of people helped by the Association has grown almost ten times and last year totalled 2,392 .

University College of North Wales' Department of Electronic Engineering has taken over a new building in Bangor. The present head of the department, which was until last year known as the Dept. of Electrical Engineering, is Professor M. R. Gavin. Power engincering and hydro-electricity, as such, have largely disappeared from the course which is at present being taken by 70 students. The new building can accommodate 120 students.

Press Communications.-The Army Wireless Reserve Squadron, formed some years ago to recruit those interested in radio communication for part-time training as operators and technicians, has a new name. It is in future to be known as 404 Signal Squadron AER (Press Communications). Details of the training are obtainable from Capt. J A. Bladon (G3FDU), 28 Jack Lane, Davenham, Northwich, Cheshire.

Receiving Licences.-Combined television and sound licences in the U.K. increased by 90,815 during September, bringing the total to $9,718,472$. Sound-only licences totalled 5,199,421, including 405,732 for car radio.

Ekco Lightweight Radar.-The weight of the new E190 airborne search radar was incorrectly queted in our review of the S.B.A.C. Exhibition, Farnborough (p. 431, October issue). The correct weight of this set is only 56 lb .

Mullard Films.-Three more Mullard films"Modern magnetic materials," "The manufacture of junction transistors," and "The junction transistor in radio receivers"-have been added to the list of films available free from the Central Film Library of the Central Office of Information, Government Building, Bromyard Avenue, Acton, London, W.3.

Gold Medal of the Institute of Navigation for 1959 has been presented to J. E. Clegg, for the development in this country of the Doppler system of air navigation.

The Institute's citation records that "The originality, drive and foresight of Clegg has been the major factor in putting the Royal Air Force ahead in the installation of Doppler equipment in operational aircraft." Mr. Clegg, who was at one time at T.R.E. (now R.R.E.), went to Australia in 1952 to join the Weapons Research Establishment of the Australian Department of Supply, Salisbury, where he is now superintendent of the Trials Division.

H.R.H. The Duke of Edinburgh presenting the Institute of Navigation's goid medal to J. E. Clegg at the Institute's annual meeting on October 22nd.
Institute of Navigation.-Although the Institute records in its annual report for $1958 / 59$ a continued small increase in membership bringing the total to 1,755 , the Council appeals for a substantial increase so that it can "acquire the stability which its work demands." The honorary membership of the Institute has been granted to Sir Robert Watson-Watt, who was president in 1949/50. J. Wikkenhauser, chief development engineer of Kelvin and Hughes, is among the five members elected into Fellowship.

Microwave Radio Links.-A coloquium on microwave commun cation, arranged by the Hungarian Academy of Sciences and the Scientific Society on Telecommunication, opens in Budapest on November 10th for four days.

Australian Television.-On November 2nd, Queensland's first non-commercial television station-operated by the Australian Broadcasting Cimmission in Brisbanewas brought into service. The State now has three transmitters, two commercial stations having opened in Brisbane in the last few months. The estimated population within the station's service areas is about 700000. Australia now has eleven television stations-eight commercial and three national.

Educational Walichart.-The latest wallchart issued by the Mullard Educationa! Service is entitled "The Te.evis:on Picture Tube." It illustrates the principle and construction of the cathode-ray tube and shows how the electron beam is formed, focused and deflected The coloured chart, which measuses 43 in by 30 in , is available to educational establishments free of charge from the Mullard Educational Service, Mullard House, Torrington Place, London, W.C.1.

International Study Groups. -The titles of two of the U.K. study groups listed in the note on the work of the C.C.I.R. on page 432 of our October issue were inadvertently transposed. The title of Study Group IV, of which Dr. R. L. Smith-Rose is charman, is soace vehicles, and that of Study Group V, of which Dr. J. A. Saxton is chairman, is groundwave and tropospheric propagation.

## Personalities

Professor R. L. Russell, D.Sc., who has succeeded Professor J. C. Prescott, D.Eng., M.I.E.E., in the Chair of Electrical Engineering at King's College, Newcastle upon Tyne, had been on the staff of the University of Bristol since 1946. For the past four years he has been reader in electrical engineering. In 1938 he graduated in mathematics at the University of Leeds, from which he received the degree of D.Sc. earlier this year. Soon after graduating he joined the Admiralty Degaussing Department and then for a few years was lecturer on radio, first at the Royal College of Science and Technology, Glasgow, and later at Robert Gordon's Technical College, Aberdeen. Immediately prior to going to Bristol in 1946 Dr. Russell was in the research department of B.T.H. at Rugby.
P. D. Canning, of the Plessey Company, has been appointed chairman of a new sub-committee (12-7) formed by the International Electrotechnical Commission (C.E.I.) to deal with climatic and durability testing of telecommunications equipment. He recently led the U.K. delegation to Ulm, in Western Germany, for similar sub-committees on electronic components, and also acted as secretary of sub-committee (40-5) on basic testing procedures for electronic components. The C.E.I., with its headquarters in Geneva, is affiliated to the International Organization for Standardization, its main object being to facilitate the co-ordination and unification of electrotechnical standards.

R. C. McCormick, B.A., M.Sc., has joined Airtech Ltd., of Haddenham, Bucks, as chief electronics engineer. After graduating with first class honours in experimental physics from Dublin University in 1949, he was employed as assistant engineer in the Department of Posts and Telegraphs, Ireland. He later joined Mullard Research Laboratories to work in the line communications section. Immediately prior to joining Airtech Ltd., he was with Ultra's special products division as executive engineer.

Bernard R. Greenhead, who joined A.B.C. Television, the I.T.A. programme contractors, as technical controller in June, 1958, from Alpha Television Studios, Birmingham, has become general manager of Iris Productions Ltd., an A.B.C. associated company concerned with the production of TV programmes. He started his career as a research engineer in television and radar with E.M.I. Ltd. before the war. He joined the B.B.C. in 1950 and in 1956 went to Alpha Television Studios, Birmingham. Mr. Greenhead is a director of the London Video-Tape Recording Centre.
A. N. Christmas, superintendent of the Armament Research and Development Establishment of the Ministry of Supply at Fort Halstead, Kent, since 1954, has been appointed Director, Guided Weapons Research and Development (Techniques). Mr. Christmas, who received a first class honours degree in electrical engineering from London University in 1935, joined the Government service in 1937 as an assistant engineer with the G.P.O. In 1946 he went to the Royal Aircraft Establishment's Guided Weapons Department, to work on control systems for beam-riding missiles. In 1951 he was appointed to the British Joint Services Mission in Washington, U.S.A.
D. J. E. Ingram, M.A., D.Phil., reader in the Electronics Department of the University of Southampton since 1957, has been appointed Professor of Physics at the University College of North Staffordshire. Dr. Ingram, who is 32, was for three years demonstrator in the Clarendon Laboratory, Oxford, before joining the staff of the University of Southampton in 1952. He is author of the book "Spectroscopy at Radio and Microwave Frequencies" (Butterworth).

The appointment of the following three new directors to the board is announced by Ferranti Ltd. : -
E. Grundy, O.B.E., B.Sc.Tech.(Hons.), M.I.E.E., who is 53 , joined the company's Instrument Department in 1921 and has been general manager of the Moston factory since 1949 ;
J. Prince, M.I.E.E., 56, who joined Ferranti's from Salford Electrical Instruments in 1926, was appointed chief engineer of the Meter Department in 1935 and has been manager of the department since 1939; and
O. M. Robson, M.A., M.I.E.E., 56, who after coming down from Cambridge joined Ferranti's in 1925, serving in Transformer Designs and since 1944 has been general sales manager.
M. L. Whelan, M.A., Ph.D.(Cantab.), of the Crystallographic Laboratory, Cavendish Laboratory, Cambridge, has been awarded a Royal Society Research Fellowship to carry out investigations of metals by transmission electron microscopy at the Department of Physics, Cavendish Laboratory.
R. Linton is appointed engineer-in-charge of the B.B.C.'s new television and y.h.f. sound transmitting station near Peterborough, which was brought into service on October 5th. He joined the B.B.C. in 1943 as a maintenance engineer at the short-wave transmitting station at Daventry, becoming an instructor in the Engineering Training Department in 1946 . For the past eleven years he has served at a number of the Corporation's high-power transmitting stations including Holme Moss and Sutton Coldfield.
C. Glover, until recently sales manager of the United Insulator Division of the Telegraph Condenser Co., has been appointed general manager of the division. The new sales manager is B. E. I. Honey, who was with the R. H. Symonds Group of Companies for thirteen years.
J. E. Green has joined General Controls Ltd., of Basildon, Essex, as chief development engineer. He will be engaged on the development of the range of precision potentiometers to be manufactured in this country. They will be similar to those produced by the parent company in the U.S.A. Until recently Mr. Green was with Taylor Controls Ltd., of Walthamstow.
F. W. Newell, who joined the Marconi Marine Company as a sea-going radio officer in 1940 and for the past three years has been an inspector, has been appointed marine manager of the Brazilian associate company, Companhia Marconi Brasileira. He is now residing in Rio de Janeiro.
C. G. Hutchinson is appointed general sales manager of Data Recording Instrument Co. Ltd., an associate company of International Computers \& Tabulators Ltd.
J. Reginald Bevins, M.P., the new PostmasterGeneral, entered Parliament in 1950 as member for Toxteth (Liverpool) which he still represents. For two years, 1951 to 1953, he was Parliamentary Private Secretary to Mr. Macmillan and was Parliamentary Secretary, Ministry of Housing and Local Government, in the last Government. He is 51. The new assistant P.M.G. is Miss Mervyn Pike, M.P., member for Melton.
R. J. Halsey, C.M.G., B.Sc.(Eng.), F.C.G.I., D.I.C., M.I.E.E., who, as announced in our last issue, has been appointed a director of Cable and Wireless Ltd., is well-known for his work on the planning and engineering of the first transatlantic telephone cable. He was made Director of Research in the Post Office last year, and will continue in this position. After five years' apprenticeship at fortsmo in Lockyand he won a Royal Scholarship to the City and Guilds College, London, and took an honours degree in engineering in London University in 1925. Two years later, at the age of 25 , he entered the engineering department of the Post Office and was posted to the Research Station at Dollis Hill. In 1947 he became head of the line transmission division and in 1953 was appointed an assistant engineer-in-chief.

## OUR AUTHORS

J. G. Spencer, author of the article describing the application of a new type of f.m. limiter and discriminator, joined the Research Department of the B.B.C. in 1946. Much of his work since then has been concerned with frequency modulation, commencing with the early laboratory and field tests which preceded the establishment of the v.h.f. service.
C. H. Dix, B.Sc., A.M.I.E.E., contributor of the article on travelling-wave tubes in this issue, has been on the staff of the G.E.C. Research Laboratories since 1951 and, for the past five yea:s, leader of the travellingwave tube group. He served for five years in the Royal Signals before going to London University, where he took B.Sc. general and special physics degrees in 1950 and 1951, gaining first-class honours in both.
D. E. O'N. Waddington, who describes a transistor stopwatch on page 521 , came to this country from South Africa in 1957, since when he has been an electrical design engineer with Marconi Instruments. Two years before coming to this country he joined Marconi (South Africa), Ltd., at Baragwanath. He is 29.
J. Skinner, author of the article on page 509 describing a simplified method of transformer testing, is manager, electronics and transformer production, at Radford Ele-tronics Ltd, of Bristol, where the system he desscribes is in use. He joined the company in 1955.

## OBITUARY

Dr. Balthazar van der Pol, director of the International Radio Consultative Committce (C.C.I.R.) from its formation in 1948 until 1956, died on October 6th at the age of 70 . Dr. van der Pol, who was born in Utrecht, spent three years in this country during the First World War studying under Fleming at London University and J. J. Thomson at Cambridgt. From 1922 until his C.C.I.R. appointment he was director of research at Philips, Eindnoven, and for the last ten years of his service with Philips he was also Professor of Theoretical Electricity in the Technical University, Delft. In 1952 he was awarded the Valdemar Poulsen gold medal by the Danish Academy of Technical Sciences for his theoretical and practical work on the propagation of radio waves. In a tribute to his work on his retirement from the C.C.I.R., the fournal of the International Telecommunication Union emphasized that "as a man of science he could conceive of no frontiers . . . as an international official he systematically overlooked the nationality of the technical experts he had occasion to meet and treated them exclusively as scientists and engineers with whom ideas and information could be exchanged."

# News from the Industry 

Cossor.--The Marquess of Exeter, in his report as chairman of A.C. Cossor Led., said that the elimination of Cossor Radio and Television Ltd. as a subsidiary has had a marked effect on the accounts for the year ended last March. They show a group profit after taxation of $£ 139,411$ compared with a less of $£ 37,134$ the previous year. He concluded: "We have cut out, not without cost, the main source of the unsatisfactory position of the group in recent times; The result has been a comparatively successful year."

Pye.-The report of the directors of Pye Ltd., and its subsidiaries records a trading profit for the year ended last March of $£ 2,834,841$ and a profit before taxation of $£ 1,885,423$. The consolidated profit of £ 945,128 after taxation is some $£ 150,000$ above the previous year's figure.

Gas Purification and Chemical Co., of which Grundig, Wolsey and A.B. Metal Products are among the subsidiaries, had a net group surpius during the past year of $£ 505,336$ before taxation. The year's sutplus of $£ 296,876$ after deducting all charges has been set against the previous year's deficit of $£ 469,392$, which leaves a deficit of $£ 172,516$ to be recovered.

Radio and Television Trust Ltd., of which Airmec is the manufacturing subsidiary, announce a profit for the fifteen-months ended in June of $£ 138,482$ before taxation. This was about $£ 34,000$ up on the previous year's profit. As announced last month, the controlling interest in the company has been disposed of by Crompton Parkinson Ltd., and it has been acquired by D. D. Prenn, of 'Truvox.

Hagan Contro's Ltd. has been formed jointly by Plessey L.td., who hold $90 \%$ of the shares, and Hagan Chemicals and Controls Inc. of Pittsburgh, Pa . The company which is operating from Ilford, Essex, has the manufacturing and selling rights in Great Britain and the Commonwealth (except Canada) for the entire range of Hagan automatic control equipment for the maintenance of physical conditions within given tolerances, and "Kybernetes" data processing equipment.

Plessey Froducts Directory lists all the products manufactured by the Plessey group of companies alphabetically and also under the division or associated company manufacturing them. The directory also gives the location of the various manufacturing units and laboratories.

Nash \& Thompson Ltd. are now the exclusive selling agents in the U.K. and the Commonwealth for KOVO, the foreign trade corporation for the import and export of precision engineering products made in Czechoslovakia. Among the instruments that will be imported into the U.K. for the first time are the Polaroscope and Polarographs designed at Professor Heyrovsky's Research Institute in Prague. Other apparatus includes the Tesla B.S. 242 intermediate electron microscope, telecommunication equipment, spectrophotometers and electrolytic analysis apparatus.

Beam-Echo International Ltd., with offices at 820 Greenwich Street, New York 14, has been formed by H. M. Rahmer, managing director and founder of BeamEcho Ltd. Mr. Rahmer is vice-president of the American company, of which Michael Muckley, a Canadian, is president. New showrooms for demonstrating BeamEcho equipment were recently opened in London at 8 Eccleston Street, S.W.1.

Irish magnetic recording tape, which is manufactured by ORRadio Industries Inc., of Opelika, Alabama, U.S.A., is now available in this country from Wilmex Ltd., who have been appointed sole concessionaires for the U.K. Their address is: 131 Sloane Street, London, S.W. 1 (Tel.: Sloane 0621).

Gate Electronics Ltd. have moved from Hackney, London, to a new factory at Maylands Avenue, Hemel Hempstead, Herts. (Tel.: Boxmoor 6464.) They are manufacturers of the Gate telephone answering machine and television distribution amplifiers and produce a number of different types of tape recorder for various companies.

Hursant Electronics Ltd., of 13-14 The Mall, Ealing, London, W.S, has been formed by D. C. Adams and R. C. Lever, until recently, respectively, sales manager and chief engineer of Hivolt Ltd. The company is initially producing a range of sub-assemb!!es for bui'ding up a wide variety of high- and low-voltage supply units.

Hall Electric Ltd., exporters of receiving, transmitting and special valves, have moved to new premises at Haltron House, Anglers Lane, Kentish Town, London, N.W. 5 (Tel.: Gulliver 8531). The new premises will enable them to increase their present stock of over 3,000 different types of valves.


TAILOR-MADE gravity convevors constructed from Dexion slotted angle and "Glidewhee's" are being used on the television receiver assembly line at the Southend-on-Sea foctory of E. K. Cole Led.

Levell Electronics Ltd., consulting and manufacturing electronic engineers, have moved from Edgware, Middlesex, to $10-12 \mathrm{St}$. Albans Road, Barnet, Herts. (Tel. : Barnet 5028).

## EXPORT NEWS

Signal Generators.-A second contract for the supply of telecommunication measurement equipment has been placed with Marconi Instruments by the Canadian Department of Defence Production. The order is for 123 a.m. signal generators type TF 801D which will be used in the maintenance of ground-to-air v.h.f. multi-channel equipment of the Royal Canadian Air Force.
A 4 MeV linear accelerator for X -ray treatment of deep-seated tumours is being built by Mullard Equipment Ltd., for the Cancer Institute Board of Victoria, Australia. Valued at $£ 60,000$ it will be installed at the Board's Peter MacCallum Clinic in Melbourne in the middle of next year. This will be the fourth medical linear accelerator to be built by the Company, and the first to be exported.
Radar Defence System.-Contracts for the design and supply of the electronic equipment valued at approximately $£ 1.5 \mathrm{M}$ for Sweden's new air defence system, have been awarded to Marconi's. The system has been evolved by Marcon's in collaboration with the Swedish Air Force. Security forbids a detailed description but it is known that the heart of the system is a very highspeed computer which solves a large number of interception problems simultaneously

Airborne search radar equipment has been ordered from Ekco for use in two de Havilland Comet 4B jet airliners of Olympic Airways of Greece.

Shock Mounts.-Cementation (Muffelite) Limited, manufacturers of anti-vibration and shock control equipment, have received a $£ 5,000$ order from Australia for the supply of Barrymount shock mounts for signals equipment fitted to military vehicles.
"British Design," a display of nearly 500 U.K. products, being staged in Copenhagen from November 20 th to 29 th, includes some radio and sound reproducing equipment. Among the items to be shown are an amplifier and "Transhailer" by Pye, radio tuner units by Acoustical Manufacturing and Jason and a Cossor record player.

Aviation Transmitters.-A £55,000 contract for 37 transmitters for beacons and communication: services at Yugoslavian airports, has been placed with Redifon.

## CLUB NEWS

Bexleyheath.-The history, development and manufacturing techniques of the Avometer will be described by J. A. Thomas (Avo) at the meeting of the North Kent Radio Society on November 12th. A fortnight later A. O. Milne (G2MI) will deal with the work of the International Amateur Radio Union. Meetings are held at 8.0 at the Congregational Hall, Bexleyheath.
Reading.-A description and demonstration of modern oscilloscopes will be given to members of the Calcot Radio Society on November 19th by E. D. Taylor of Solartron. On December 10th S. Woodward will give a demonstration lecture comparing mono and stereo sound reproduction. Meetings are held at 7.45 at St . Birinus Church Hail, Calcot, Reading.
Wellingborough.-"Aspects of Tape Recorders" is the title of the talk to be given by G. B. Shaw at the November 19th meeting of the Wellingborough and District Radio and Television Sociery. Meetings are held each Thursday at 7.30 at the Silver Street Club Room.

## RUSSIAN TV PRODUCTION

SOME RECENT FACTS AND FIGURES



Cathade-ray tube production in the U.S.S.R. is typified by this photograph taken in one of the factories of the Moscow Electric Lamp Works.


The transistor receiver "Sputnik-2" has a 10 -inch screen and weighs about 141 b . (Courtesy Brit.I.R.E. Journal.)

TRANSISTOR television sets are planned for mass production in the U.S.S.R. in 1961-62. For this purpose a 17 -inch model has been developed which can be powered from batteries or the a.c. mains. The picture above shows a 10 -inch model with 30 transistors, the "Sputnik-2," which was developed last year. It has a resolution of 500 lines and a sensitivity of $100 \mu \mathrm{~V}$, and is intended to run from a 12 -volt car battery.
Speaking at the Brit.I.R.E's Cambridge convention on television engineering, B. A. Berlin, of the U.S.S.R. State Committee for Radio Electronics, gave further information about the present production of valve receivers. In January of this year, he said, about $3 M$ sets were in use in the Soviet Union. It is expected that 1.2 M will be produced in 1959 and that by 1565 the annual output will be 3.5 M . In six years' time a total of 18 M sets should be in operation.

Manufacturing processes and circuit units are standardized in order to keep prices down and simplify servicing, and the public has a choice of three main classes of receiver. The first class are 21 -inch high-quality sets, the second (and most popular) are 17 -inch models, while the third are small cheap sets with screen sizes up to 14 inches. There are different cabinet designs within each class, and all first- and second-class models have f.m. sound reception. Small quantities of profection and extra high-quality receivers are also being produced. The last-mentioned sets incorporate sound receivers, tape recordars and record players.

Wide use is made of automatic control and stabilization circuits, and present development aims at introducing a.f.c. for tuners. Picture tubes have $70^{\circ}$ deflection angles at present, but a transition to $110^{\circ}$ tubes is due to take place this year.

On the transmitting side, the smaller towns are being equipped with 5 kW e.r.p. stations and the larger ones with 50 kW e.r.p. stations. In 1961 Moscow will have a new transmitter with a power of 200 kW e.r.p. and a giant aerial about $1,400 \mathrm{ft}$ high. Translator equipments are used for the smallest towns and villages. Colour television development continues, and about $40 \%$ of transmission equipment is intended for this purpose.

# F.M. Receiver Using New 

LOW-COST LIMITER/DISCRIMINATOR GIVING GOOD A.M. REJECTION

IN an ideal f.m. receiver, changes of amplitude of the input signal should produce no response at the output; while this condition cannot be achieved in practice, adequate suppression of amplitude modulation is essential if the performance of the receiver is to be satisfactory. In particular, a signal received in conditions of multipath propagation contains both a.m. and f.m. components of distortion; if the former is adequately suppressed the total distortion is considerably reduced ${ }^{1}$ and for this purpose an a.m. suppression ratio of some 35 dB is required. $\dagger$

The simpler types of domestic f.m. receivers usually rely for their a.m. suppression on a ratio detector unassisted, at least over the lower range of input levels, by any other form of limiting. The a.m. suppression ratio achieved is seldom as high as 35 dB and is often considerably lower, with the result that their performance, while satisfactory under most conditions, can be poor in the presence of multipath propagation.

The receiver here described incorporates a recentlydeveloped limiter and discriminator circuit ${ }^{2,3}$ and, while it is comparable in cost and complexity with the simpler types of ratio-detector receiver, it achieves better a.m. suppression characteristics without either requiring increased i.f. amplifier gain or sacrificing sensitivity.

The circuit diagram of the receiver is shown in Fig. 1. Apart from the limiter and discriminator the d.sign differs little from established practice; V1 i; an ECF80 triode-pentode, the triode section
†1H d.in. suppicssivin ratio oi a recenver is detined tor the purpose of this article, as the ratio of the output due to $\mathrm{f} . \mathrm{m}$. to that due to a.m. when the input carrier is simultaneously frequency modulated $\pm$ $30 \mathrm{kc} / \mathrm{s}$ and amplitude modulated to a depth of $40 \%$
operating as a grounded-grid r.f. amplifier and the pentode section as a self-oscillating mixer. V2 and V3 are two 9D7 i.f. amplifiers; part of the cathode bias resistor of each stage is undecoupled to compensate for changes of input capacitance with variations of a.g.c. bias voltage. The intermediate frequency is $10.7 \mathrm{Mc} / \mathrm{s}$ and the local oscillator frequency is below that of the signal. Three germanium diodes, one Type O.486 and two Type OA91, are used in the limiter and discriminator circuit; V4, an ECL82 triode-peatode, is the audiofrequency amplifier and output stage.
Limiter and Discriminator.-The theory of the limiter and discriminator used has been dealt with fully elsewhere, ${ }^{2}$ but can be sumnarized as follows. Amplitude-limiting devices are generally voltage operated and require input levels of one volt or so for satisfactory operation. Such levels do not normally occur in stages before the discriminator unless extra amplification is introduced specifically to drive a limiter. However, the required voltage is normally available at the discriminator transformer itself and, if limiting can be performed there, the extra amplification is not needed. In the design of the Foster-Seeley discriminator it is assumed that it is fed from a high impedance source, i.e., one approximating to a constant-current generator, and the amplitude/frequency response of the transformer is utilized to control the linearity of the transfer characteristic. Thus, a limiting of either the primary or secondary voltage or of a combination thereof would be unsatisfactory. The circuit proposed to overcome these limitations is shown in Fig. 2. In this circuit $\mathrm{L}_{2} \mathrm{C}_{2}$ and $\mathrm{L}_{3} \mathrm{C}_{3}$ are the p mary and secondary circuits respectively of a conv: ntio., 1

Fig. 1. Theoretical circuit diagram of receiver incorporating new limiter.


## Dynamic Limiter

## By J. G. SPENCER*

This receiver was designed primarily to show that a low-cost receiver can be produced with the type of a.m.rejection characteristics usually associated with expensive equipment. The limiter and discriminator section (from V3 anode to V4 triode grid) is eminently suitable for inclusion in new or existing f.m. receivers, where it will offer better performance than even the best ratio detector whilst not requiring the addition of extra i.f. stages or a separate limiter valve.
phase discriminator; $\mathrm{L}_{1} \mathrm{C}_{1}$ is a parallel resonant circuit across which is connected a voltage limiting device. The presence of this limiter makes the shunt impedance across $L_{1} C_{1}$ very low but if $L_{1}$ is loosely coupled to $\mathrm{L}_{2}$, the coupling acts as an impedance inverter and the discriminator is effectively fed from a high impedance source. Thus, although limiting is carried out at the voltage level of the discriminator, the two functions are independent and the presence of the limiter imposes no restrictions on the design of the discriminator.

The limiting device could take any one of several forms; one possibility is a biased diode which conducts when the peak i.f. voltage across $L_{1}$ exceeds the bias threshold. The limiter used here is based on the dynamic-diode type. ${ }^{4}$ It employs a diode in series with a load consisting of a resistor and capacitor in parallel, the time constant of the combination being longer than the period of the lowest audible frequency. With this arrangement, amplitude changes having a period shorter than the time constant are suppressed by variation of the loading on the limiter tuned circuit. When the signal increases in amplitude the diode-load voltage cannot change, so the diode current increases very sharply, with a resultant increase in the loading. Conversely, when the signal decreases in amplitude the diode tends to cut off, thus reducing the loading. One disadvantage of this type of limiter is that it gives no protection against a slow amplitude change whose period is


Fig. 2. Basic circuit of limiter and discriminator.


Fig. 3. Equivalent circuit of limiter and discriminator.
long compared with the diode-load time-constant; the load voltage follows the signal ampitude and the loading imposed by the diode circuit is constant. This limitation has been overcome in the receiver described by using the voltage across the limiter-diode load for automatic gain control.

The practical des ${ }^{\text {g }}$ n of the limiter can best be considered with reference to Fig. 3. The following symbols will be ust d; the remaining symbols given in Fig. 3. are self-expana. ory.

$$
\begin{array}{ll}
\mathrm{Q}_{\mathrm{p}}=\frac{\mathrm{R}_{p}}{\omega_{0} \mathrm{~L}_{i}} & k=\frac{\mathrm{M}}{\sqrt{ }\left(\mathrm{~L}_{1} \mathrm{~L}_{-}\right)} \\
\mathrm{Q}_{\mathrm{s}}=\frac{\mathrm{R}_{\mathrm{s}}}{\omega_{0} \mathrm{~L}_{\mathrm{s}}} & \mathrm{Q}=\sqrt{ }\left(\mathrm{Q}_{;}, \mathrm{Q}_{3}\right)
\end{array}
$$

where $R_{p}=$ total shunt losses of discriminator primary, including diode loading; $\mathbf{R}_{\mathbf{s}}=$ total shunt losses of discriminator secondary, incuding diode oading; $\mathrm{R}_{\mathrm{L}}$ $=$ total shunt osses of limiter tuned circuit, excluding load ng due to limiter diode, and $\omega_{n}=2 \pi f_{0}$ where $f_{o}$ is the intermediate frequency.

[^2]

Fig. 4. Correct dynamic-limiter characteristics for various input levels and effect of mis-tuned harmonic filter (two-kneed curve) and absence of filter (dotted
curve).
can be dealt with is increased, but the discriminator slope is reduced; this parameter is therefore a comprom'se between overall gain and the depth of modulation that can be handled.
The limiter in the form shown in Fig. 3, with an OA86 crystal diode, gives an a.m. suppression ratio of some $30-35 \mathrm{~dB}$; bur if a parallel-tuned circuit, resonant at the frequency of the third harmonic of the i.f., is inserted in series with the limiter diode, a further increase in limiting efficiency is obtained. The action of this harmonic filter is to modify the shape of the current pulses through the diade in such a way that its effective dynamic impedance is reduced. The limiter circuit actually embodied

At the mid-band frequency the input impedance of the discriminator, i.e. the circuit to the right of $\mathrm{C}_{\mathrm{e}}$, is

$$
\mathrm{R}_{\mathrm{p}}^{\prime}=\frac{\mathbf{R}_{\nu}}{1+(k \mathrm{Q})^{2}} .
$$

The shunt impedance reflected into the limiter circuit at mid-band is therefore

$$
\mathrm{R}_{\mathrm{o}}=\frac{\mathrm{X}_{\mathrm{c}}^{2}}{\mathrm{R}_{\mathrm{p}}^{\prime}}
$$

where $\mathrm{X}_{\mathrm{c}}=1 / \omega_{\mathrm{o}} \mathrm{C}_{\mathrm{c}}$. The resulting shunt impedance across which the limiter operates is

$$
R_{L}^{\prime}=\frac{R_{L} R_{o}}{R_{L}+R_{o}}
$$

If we assume a rectification efficiency of $100 \%$ in the diode limiter, the effective shunt loading of the limiter circuit by the diode, with a constant amplitude input, is $R_{\mathrm{a}} / 2$. The ability of the limiter to cope with upwards modulation is virtually unlimited, but the maximum downwards modulation which can be dealt with is determined by the ratio between $\mathrm{R1}_{\mathrm{L}}$ and $\mathrm{R}_{\mathrm{d}} / 2$. In order to deal with a fractional depth of modulation $m$, we require that

$$
\mathrm{R}_{\mathrm{L}}^{\prime} \geqslant \frac{\mathrm{R}_{\mathrm{d}}}{2}\left(\frac{m}{1-m}\right)
$$

If this condition is not fulfilled the limiter diode will cut off in the troughs of amplitude modulation and the input to the discriminator will not be stabilized over that part of the modulation cycle. It should be noted that when this occurs the discriminator diodes continue to function, in contrast to the ratio detector in which, if the maximum possible modulation depth is exceeded, the discriminator diodes are cut off over part of the modulation cycle.
Taking as typical values $\mathrm{R}_{\mathrm{d}}=10 \mathrm{k} \Omega, \mathrm{R}_{\mathrm{L}}=50 \mathrm{k} \Omega$, $\mathrm{R}_{\mathrm{p}}^{\prime}=2 \mathrm{k} \Omega, f_{0}=10.7 \mathrm{Mc} / \mathrm{s}$, it follows that to achieve satisfactory amplitude modulation suppression for values of $m$ up to $0.8, \mathrm{C}_{\mathrm{c}}$ is required to be 1.8 pF . The impedance reflected across the discriminator primary from the limiter circuit is $X_{c}{ }^{2} / R_{x}$ where $R_{x}$ is the effective dynamic impedance of the limiter and its load. Measurements indicate that $R_{x}$ is about $500 \Omega$, so that with the conditions specified $\mathrm{X}_{\mathrm{c}}{ }^{2} / \mathrm{R}_{\mathrm{x}} \approx 130 \mathrm{k} \Omega$. This is sufficiently high, compared with $\mathrm{R}_{\mathrm{n}}$, to be neoligible. As $\mathrm{C}_{\mathrm{c}}$ is reduced, the downwards amplitude modulation depth which
in the receiver differs from Fig. 3 in three respects:(i) The third-harmonic filter is included.
(ii) The limiter-circuit inductor is wound as a closecoupled transformer; this isolates the limiter from the h.t. line and permits the limiter load to be earthed, thus simplifying the provision of an a.g.c. voltage.
(iii) A delay voltage is applied to the diode to improve the a.g.c. characteristic and hence the suppression of slow amplitude fluctuations.

Dynamic input/output curves of the limiter as embodied in the receiver, for input levels of $30 \mu \mathrm{~V}$, $100 \mu \mathrm{~V}$ and 1 mV , are given in Fig. 4, together with the $1-\mathrm{mV}$ curve of the basic limiter without the third-harmonic filter. All curves are normalized to the same operating point and the effective reduction of amplitude modulation by the limiter is shown by the ratio of the slope of the dynamic curve to that of the line passing through the origin and the operating point. These curves also demonstrate the reduced capacity to handle downwards modulation at low signal-input levels; this is due partly to the delay voltage applied to the limiter, and partly to the rise in the impedance of the diode at low currents.

## Construction and Alignment of Limiter and Discriminator

Details of the construction of the coils in the limiter and discriminator circuits are given below. In all cases the cores used were Neosid Grade 900, Type $6 \times 1 \times 12$.
Limiter Transformer: Neosid Type 5000A/6E former


Fig. 5. Tuning characteristic with (a) narrow-bond discriminator, (b) wide-band discriminator.


Fig. 6. Circuit modifications to obtain tuning indicator drive from discriminator.
(7.6 mm dia.). Two single-layer solenoids, each 50 turns 38 s.w.g. enamelled wire, close wound, one over the other and separated by one layer of cellulose tape. The external connections are arranged so that the low i.f. potential ends of the two windings are adjacent.
Third-harmonic Filter: Neosid Type 3500 former ( 7 mm dia.) 25 turns 38 s.w.g. enamelled wire, close wound.
Discriminator Transformer: Neosid Type 5000B/6E former ( 7.6 mm dia.) Primary: 15 turns 30 s.w.g. enamelled wire wound with $1 / 1$ space ratio. Secondary: 20 turns 30 s.w.g. enamelled wire close wound. The space between adjacent ends of the primary and secondary windings is 6.5 mm .

Alignment of a limiter and discriminator of this type is most conveniently carried out in two stages. First, the third-harmonic filter is short-circuited and the limiter transformer tuned to the intermediate frequency by adjusting for the maximum d.c. voltage across the limiter load: the discriminator can then be aligned in the usual way. To give an oscilloscope display of the limiter input/output curve, the receiver is fed with a $100 \%$ amplitude-modulated signal and the $Y$ input of the oscilloscope is connected through a suitable "isolating" resistor (minimum value, $100 \mathrm{k} \Omega$ ) to one side of the discriminator transformer secondary, thus using one discriminator diode as an a.m. detector. The X input to the oscilloscope is obtained from the signalgenerator modulating voltage. This will produce on the oscilloscope a limiter curve similar to those shown in Fig. 4. The short circuit is now removed from the third-harmonic filter and the final adjustment of the limiter-transformer tuning, harmoniccircuit tuning and limiter-to-discriminator coupling is made. The limiter transformer is tuned to obtain the maximum downwards limiting, the value attainable being determined by the limiter-to-discriminator coupling capacitance. The harmonic filter is tuned principally for maximum flatness of the top of the curve, that is, maximum a.m. suppression; but also to ensure maximum downward limiting. Thus it will be found that as the tuning inductance is increased from the optimum value the flat top of the dynamic curve begins to tilt, while if the inductance is reduced, the downward limiting threshold is raised. The adjustment is not unduly critical; a variation of some $+20 \%-10 \%$ of inductance from the optimum could be tolerated in the prototype receiver without serious impairment of the limiter performance. Gross mis-tuning, however, causes a considerable deterioration, the effect of an increase
of inductance of $80 \%$ above the optimum value is shown in Fig. 4. Having set up the limiter, the discriminator tuning should be checked to complete the alignment.
Tuning the Receiver.-One difficulty in tuning an f.m. receiver is to distinguish between the side responses and the central response of the discriminator. If no tuning indicator is fitted it is essential, in order to avoid confusion, that these side responses are either sufficiently low in amplitude or are recognizable by their poor signal-to-noise ratio. Curve (a) of Fig. 5 gives the tuning characteristic of the receiver with an input signal of 1 mV , frequency modulated to $\pm 30 \mathrm{kc} / \mathrm{s}$. If better suppression of the side responses is required, it may be obtained by increasing the discriminator bandwidth, and curve (b) shows the performance under the same input conditions with a discriminator having a peak separation of $\pm 200 \mathrm{kc} / \mathrm{s}$. The use of the wider discriminator bandwidth entails a reduction of about 3 dB in adjacent-channel suppression and some loss of gain, but this may be thought justifiable for greater ease of tuning. A difficulty that remains, however, is that of obtaining the best tuning position within the central response.

A better approach to the problem of simplifying


Fig. 7. Potential derived from discriminator to feed tuning indicator (solid line); ImV constant input to receiver. Dotted line shows response of discriminator alone.
tuning is to provide some kind of indicating device, preferably one which shows the centre point of the discriminator response and is unaffected by the shape of the i.f. amplifier response.

With the normal phase-discriminator circuit the outputs of the two diodes are combined in such a way that a null-point indicator is required. It is possible, however, by making minor modifications to the circuit, to obtain a d.c. output from the discriminator which is suitable for operating a conventional " magic eye "t tuning indicator. These modifications, shown in Fig. 6, involve the addition of three resisto:s, $R_{a}, R_{b}$ and $R_{c}$ and two capacitors, $C_{b}$ and $C_{b}$. The discriminator secondary circuit is now earthed to modulation frequencies by the capacitor $\mathrm{C}_{\mathrm{a}}$, but the d.c. earth is at the junction of $R_{a}$ and $R_{b}$, with the result that a voltage equal to the mean of the rectified voltages across the two diode loads appears at the junction of $R_{c}$ and $C_{b}$. The variation of this voltage with carrier frequency is shown in Fig. 7. The dıp in the middle of the curve provides a precise indication of the centre of the discriminator response; because the discriminator is outside the a.g.c. loop,


Fig. 8. Circuit modificasions to obtain tuning-indicator drive from combination of a.g.c. and discriminator voltages.


Fig. 9. Potential derived for tuning indicator from combined a.g.c. and discriminator action (solid line). The broken line represents o.g.c. voltage. Indicotor drive voltage is relative to that ot midbond frequency.
while any variations in the i.f. amplifier response are compressed by the action of a.g.c., the accuracy of the indication is not greatly impaired by asymmetry of the i.f. response.
The disadvantage of this system is that it requires the user to adopt an unusual criterion in observing the tuning indicator. This can be overcome, at some sacrifice of accuracy, if the circuit is rearranged as shown in Fig. 8, with the lower end of the resistance $\mathrm{R}_{\mathrm{c}}$ connected to the negative end of the limiter-diode load, and the tuning-ind cator voltage obtained from the junction of $R_{a}$ and $R_{b}$. With this arrangement the indicator is operated by the difference between the a.g.c. voltage and the discriminator mean voltage. The shape of the resultant curve is shown in Fig. 9; for comparison the curve of the a.g.c. voltage alone is also shown, normalized to the same amplitude at the tuning point.

## Performance Tests

It should be noted that all ratios of signal to noise, hum or interference quoted were measured with a mean-square meter preceded by an aural-sensitivity weighting network based on the C.C.I.F. (1934) curve for broadcast-relay circuits. ${ }^{5}$ Unless otherwise


Fig. 10. Variation of harmonic distortion with deviation.
stated all signals levels refer to the open-circuit voltage from a $75-\Omega$ source.
Absolute Sensitivity.-This is the minimum inputsignal amplitude, deviated $\pm 35 \mathrm{kc} / \mathrm{s}$ at a frequency of $2000 \mathrm{c} / \mathrm{s}$, which will produce an output of 50 mW with the receiver gain control at maximum.
The measured value was $8 \mu \mathrm{~V}$.
Maximum Deviation Sensitivity for $10 \%$ Harmonic Distortion.-This is the minimum input-signal amplitude, deviated $\pm 75 \mathrm{kc} / \mathrm{s}$ at a frequency of $400 \mathrm{c} / \mathrm{s}$, which produces a total harmonic distortion of $10 \%$ or, if that figure is less than the input required to satisfy the previous test, the distortion occurring at the absolute sensitivity input level.

The distortion at $8 \mu \mathrm{~V}$ input level was $5 \%$.
Sensitivity for Standard Signal-to-Noise RatioThis is the minimum input signal amplitude, deviated $\pm 35 \mathrm{kc} / \mathrm{s}$ at a frequency of $2,000 \mathrm{c} / \mathrm{s}$, which will produce an output signal-to-noise ratio of 40 dB .

The measured value was $10 \mu \mathrm{~V}$.
Variation of Harmonic Distortion with Deviation.Fig. 10 shows the total harmonic distortion as a function of deviation with the receiver gain control set to give 50 mW output with $\pm 30 \mathrm{kc} / \mathrm{s}$ deviation at $400 \mathrm{c} / \mathrm{s}$. The input signal level was 10 mV .

Maximum Output Power for $10 \%$ Total Harmonic Distortion.-The measured value was 1.5 watts.

Modulation-frequency Characteristic.-After correction for a $50 \mu \mathrm{sec}$ pre-emphasis time-constant, the response relative to that at $400 \mathrm{c} / \mathrm{s}$ was within the limits $\pm 1 \mathrm{~dB}$ from $30 \mathrm{c} / \mathrm{s}$ to $15 \mathrm{kc} / \mathrm{s}$.

Selectivity.-The suppression ratio for an interfering signal is measured objectively as the ratio of unwanted-to-wanted signal amplitudes giving an output signal-to-interference ratio of 40 dB when the interfering signal is frequency modulated at $2,000 \mathrm{c} / \mathrm{s}$ with a deviation of $\pm 35 \mathrm{kc} / \mathrm{s}$. The results for adjacent-, second- and third-channel interference (i.e. with 200,400 and $600 \mathrm{kc} / \mathrm{s}$ frequency separations respectively) are given in Table 1, together with the measured ratio for the image channel. The wantedcarrier level in each case was 1 mV .
For comparison with the figures in Table 1, the measured frequency response curves of the i.f. amplifier and discriminator are shown in Figs. 11 and 12.

Local-oscillator Drift.-Local-oscillator drift was found to be comparable with that of the discriminator: the relative drift of local oscillator and ciscriminator (that is the change of input-signal frequency required to maintain zero d.c. output from the discriminator) was steady at about $30 \mathrm{kc} / \mathrm{s}$ after one hour from

TABLE 1

| Frequency of unwanted carrier, relative to wanted carrier | $-2 \mathbf{M c / s}$ | $-600$ | $\begin{gathered} -400 \\ \mathrm{kc} / \mathbf{s} \end{gathered}$ | $-200$ | $\begin{aligned} & +200 \\ & \mathrm{ke} / \mathbf{s} \end{aligned}$ | $\begin{aligned} & +400 \\ & \mathrm{kc} / \mathrm{s} \end{aligned}$ | $\begin{aligned} & +600 \\ & \mathrm{kc} / \mathrm{s} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ratio of unwanted to wanted-carrier levels (dB) | +28 | $>+40$ | +35 | +6 | +5 | +34 | $>+40$ |

switching on. Maximum drift was about $38 \mathrm{kc} / \mathrm{s}$, occurring at about 8 minutes from the switching-on. Local-oscillator Radiation.-In this test the voltage at the input terminals of the receiver due to the local oscillator was measured, the input terminals being terminated in 75 ohms.

The measured voltage was 1.7 mV .
Co-channel Suppression Ratio.-As for the test of selectivity, but with the interfering signal frequency differing from the wanted signal by less than $1 \mathrm{kc} / \mathrm{s}$.

The measured value was -6.5 dB .


Fig. II. I.F. amplifier frequency response.


Fig. 12. Discriminator frequency response. Output is in arbitrary units.

TABLE 2

Input Signal Level
A.M. Suppression Ratio
$30 \mu \mathrm{~V}$
$100 \mu \mathrm{~V}$
$300 \mu \mathrm{~V}$
1 mV
10 mV

100 mV

35 dB
38 dB
41 dB
43 dB
48 dB
49 dB

Suppression of Amplitude Modulation.-The a.m. suppression ratio is the ratio between the output due to a carrier which is frequency modulated $\pm 35 \mathrm{kc} / \mathrm{s}$ at $2,000 \mathrm{c} / \mathrm{s}$ and that due to a carrier which is simultaneously amplitude modulated to a depth of $40 \%$ at $2,000 \mathrm{c} / \mathrm{s}$ and frequency modulated $\pm 30 \mathrm{c} / \mathrm{s}$ at $100 \mathrm{c} / \mathrm{s}$, the $100 \mathrm{c} / \mathrm{s}$ output being rejected by a highpass filter. The results for various input signal levels are shown in Table 2.

Dependance of Output on Signal Level.-This is shown in Fig. 13.
Impulsive Interference Performance.-Fig. 14 shows


Fig. 13. Variation of a.f. output with input level. Output is referred to ImV and input level is open-circuit voltage from $75-\Omega$ source.


Fig. 14. Infut/outfut cherecteristic for in:fulsive interference. Input corrier level $500 \mu \mathrm{~V}$, imfulse p.r.f. 2,500 isec; relative output is referred to outfut with $\pm 35 \mathrm{kc} / \mathrm{s}$ deviotion at 2 kc 's and impulse input amplitude is referred to $1 \mu V$ peak per kc/s bandwidth.

TABLE 3

the output due to impulsive interference, relative to that due to $\pm 35 \mathrm{kc} / \mathrm{s}$ deviation at $2,000 \mathrm{c} / \mathrm{s}$, for various input impulse amplitudes. The measurements were made in the presence of an input carrier of $500 \mu \mathrm{~V}$, firstly unmodulated and secondly frequency modulated with $\pm 30 \mathrm{kc} / \mathrm{s}$ deviation at $12 \mathrm{kc} / \mathrm{s}$.

Subjective Measurements of Selectivity and CoChannel Suppression Ratio.-For these tests the receiver was fed with two signals, a wanted signal of 1 mV and an interfering signal of controllable amplitude which was set in turn to frequencies within $1 \mathrm{kc} / \mathrm{s}$ of, and spaced by $\pm 200 \mathrm{kc} / \mathrm{s}$ and $\pm 400 \mathrm{kc} / \mathrm{s}$ from, the wanted signal. Both signals were frequency modulated with programme in accordance with standard B.B.C. transmitter practice, the wanted programme being speech and the interfering programme light-orchestral music which gave a consistently high level of modulation. The

## TABLE 4

| Frequency of interfering signal relative to wanted signal (ke/s) | -400 | -200 | < ${ }^{+1}$ | +200 | +400 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Amplitude of interfering signal relative to wanted signal (dB) to give "P" $\left\{\begin{array}{l}\text { Mistuned } \\ \text { high }\end{array}\right.$ | $>+40$ | +14 | -25 | -5 | +28 |
| interference with receiver mistuned as shown $\quad \begin{gathered}\text { Mistuned } \\ \text { low }\end{gathered}$ | +28 | -11 | -25 | +18 | $>+40$ | gain. for adjacent-channel signals.

improved aerial system than with increased receiver
The selectivity more than meets the requirements of the planning standards for v.h.f. broadcasting in the United Kingdom, i.e. a protection ratio of 0 dB

The a.m. suppression ratio is maintained at or above the specified target figure of 35 dB down to an input level of $30 \mu \mathrm{~V}$. The a.g.c. is also operative over a similar range of input levels. While the constancy of output is not as good as that obtained with a static limiter, an input/output characteristic of the type shown in Fig. 13 does enable the user select the local transmission by tuning to the loudest programme. With a static limiter the output level is independent of signal strength and it is possible, particularly in periods of abnormal tropospheric propagation, to tune inadvertently to a distant transmitter on an adjacent channel with consequent fading and poor quality.

The performance in respect of local-oscillator frequency stability and radiation is somewhat below that which obtains in some current commercial receivers. Further development time spent on the r.f. portion of the circuit could have resulted in an improvement, but this was regarded as a side issue, since the design is primariiy concerned with illustrating the potentialities of the limiter and discriminator circurt.

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## New Mullard Filmstrips

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# Automatic Pattern Recognition 

NEW MORPHOLOGICAL SYSTEM USING A DIGITAL COMPUTER

By R. L. GRIMSDALE,* M.Sc., Ph.D., Grad.I.E.E.

THE human eye and brain are so efficient at recognizing printing and handwriting that it is not generally realized that recognition is a particularly difficult operation. Various patents have been filed in the past for machines which can read and for devices for aiding blind persons. The ma;ority of these schemes were not exploited, and it is only in recent years, with the advent of digital computers, that the interest in this problem has been revived.

A number of machines have recently been produced commercially in this country and in America. The principal applications are the reading of information printed on cheques and other documents used in commerce. In addition to these applications there are many other important potential fields for more sophisticated reading machines. Intensive programmes of work are now directed towards obtaining systems for the mechanical translation of languages, but it would appear that it is essential, for economical working, to provide an input mechanism which can take the information direct from the printed page.
Another interesting possible future application is the sorting of mail. This might necessitate the printing of the names of the towns with reasonable clarity. However, this problem is not quite so difficult as it might appear, because use may be made of the fact that the town names include a considerable amount of redundant information; there would, for example, be no difficulty in recognizing MA ${ }^{*} \mathrm{C}^{\star *}$ STER or ${ }^{\mathrm{I} I V}{ }^{\star}$ RPOOL, and the machine could be arranged to reject all envelopes which it failed to identify with certainty.

A further application is that of feeding instructions and information to a digital computer, which at present is done via the medium of punched paper tapes or cards.

Before describ:ng the operation of the present system, some features of other systems will be considered. One of the earliest, the Optophonet, a

device to assist blind people to read printed matter, consists of a set of five photocells, each controlling a separate audio frequency tone. As the device is moved across a line of illuminated print, the letters are efectively scanned by five horizontal lines and the tones vary as the parts of the letters are crossed. It is not beiieved that the device is widely employed because of the difficulties in using it. However, the Optophone cannot be regarded as a true recognition device, because all it does is to convert information from one form to another, with considerable loss of detail. The user must perform the recognition task from the sounds which he hears.

## Comparison of Symbols

A large number of the recognition machines which have been devised or constructed are based on the principle of comparison of the unknown symbol with a set of standard symbols. In one particular version, the standard symbols take the forms of cut-outs round the periphery of a rotating disc. The remainder of the apparatus consists of a lamp, a lens system, and a photocell. As the disc rotates, images of the standard symbols fall on the unknown symbol. If the symbol is printed in black ink on white paper, varying amounts of light are reflected as the disc rotates. Recognition of the symbol is possible if the amount of light reflected from the image of one particular standard symbol is much less than from any other. The determination of the number of distinct symbols which can be identified is a problem of information theory, and a great deal of work has been done on designing specially formed symbols for maximum discrimination.

The modern counterpart of the rotating disc uses special symbols printed in magnetic ink on cheques. The symbols are recognized by passing them first through a field which magnetizes them, and then under a reading head. The waveform of the induced e.m.f. is strobed and examined and from this information the symbols are identified. This system, which has been adopted for reading cheques in the U.S.A., and is being developed in this country, is limited to the recognition of about a dozen-specially formed symbols. In another system produced by Solartronf, the symbol is. effectively divided into a number of areas and signals are produced depending on whether each of the small areas is black or white. The

[^3]symbols are then identified by a set of logical circuits.

In all these systems the symbols are effectively identified by a geometrical comparison. There are definite restrictions on the shape, size, and form of the symbols, and they must be correctly oriented in relation to the identification equipment. The new system which has been developed has, as its basis, the recognition of patterns by their shape or form. The system is very versatile because a $P$, for example, is recognized as a semi-circle and a straight line joined in a particular manner. This description is independent of the way in which the $P$ is drawn and its size. The system is in no way limited to letters or numbers, but can be used for all simple patterns composed of straight lines and curves, and can be extended to include a wide range of patterns of diverse forms.
This morphological approach, or recognition by the shape of the pattern, may closely resemble at least one of the ways in which human readers recognize patterns. The resemblance is particularly apparent when a reader is presented with a strangely written or upside-down letter. In these cases a conscious study is made of the form of the symbol. Even with normal letters the human reader may carry out a detailed study of the shapes, although the process is so rapid that the reader is not conscious of the operation. However, in normal reading, a great deal of use is made of the context and whole words may be guessed before the individual letters are recognized.

## Characteristic Features of Patterns

"The name "patsern recognition," as opposed to "character recognition," distinguishes the new system from those already devised. Character recognition implies the identification of one out of a given set of symbols, each symbol having a definite form and size, as produced, for example, by one particular typewriter. Pattern recognition, on the other hand, is not restricted to a particular set of symbols. The patterns are recognized because they have certain characteristic features. The pattern of a letter R , for example, can be recognized even when written in different ways by several people. Furthermore, no special restrictions are imposed on the size of the pattern. Another useful feature is that the pattern need not be correctly orientated when presented to the recognition machine, provided it lies within its "field of view."

In order to demonstrate the working of the pattern recognition system, it has been simulated using a universal digital computer. This technique is one which is of great value as it enables the operation of complex systems to be demonstrated and studied at low cost, prior to the construction of specialpurpose equipment.

## Scanning System

The operation of the system is divided into a number of stages. First of all the pattern is transferred from the paper on which it is drawn to the store of the computer, a flying-spot scanner being used. The scan elfectively divides the picture area into a matrix of points. According to the amount of light reflected, each point is classed as "black" or "white" and can then be rep:esented by a binary digit having the value " 0 " or " 1 " (Fig. 1). The
pattern is stored within the computer as an array of points (" 1 " digits) on a background of " 0 " digits.
Although the pattern is stored, the machine cannot yet "see" its shape. The precise way in which the machine examines the pattern is dictated by the type of instructions available on the computer. In general the examination proceeds from bottom to top and from right to left. The pattern is subdivided into divisions of the type shown in Fig. 2 (a). Each division is specified by the length, and the slope or curvature of its edges. The information concerning the latter is determined by forming the values of $\frac{\mathrm{d} x}{\mathrm{~d} y}$ and $\frac{\mathrm{d}^{2} x}{\mathrm{~d} y^{2}}$ for the points at the edge of the division. Since the edge may be very irregular, due to the imperfections of the figure, an averaging technique is employed.

Figure imperfections may give rise to other difficulties. A break in the figure may result in two divisions being formed where there should only be one. To overcome this, use is made of a noise factor which gives a measure of the amount of imperfection which may be tolerated. The value of the noise factor is set automatically by a trial scan which determines the overall size of the figure. The noise figure subsequently may be modified if an unduly large number of divisions is produced.

In the next stage of the process the various divisions of the figure are assembled into the basic curves and lines of the figure. It is clear that if the same figure is presented to the flying-spot scanner at a different angle an entirely different set of divisions will be produced (Fig. 2 (b)). The present process is designed to ensure as far as possible that the same result will be obtained for all orientations. The result of this process is recorded as a statement of the number and type of component lines and curves of the figure and the way they cross or join.

At this stage the true recognition process begins. The action so far has effectively reduced a twodimensional pattern to one-dimensional form. The statement can be considered as a one-dimensional form of pattern because it consists of a succession of symbols which describe the original figure. The true recognition process amounts to the comparison of the new statement with those stored within the machine. The comparison is done on a very flexible basis and a score is given for each test. This method permits the amount of agreement to be determined between the unknown pattern and a range of patterns which have already been-presented to the scanner.

An important feature of the system is the ability to learn new patterns. In contrast with the methods for character recognition using geometrical comparison there are no built-in representations of the pat-


Fig. 2. Pattern divisions produced during examination ; (a) with normal orientation, (b) when presented ot a different angle to the scanner.
terns. Every pattern which is shown to the machine is converted to the statement form and compared with statements previously obtained and stored. If a satisfactory comparison is obtained the name of the pattern is printed out on the teleprinter attached to the computer. If, after having obtained the statement describing the shape of a new pattern, the machine is unable to find a sufficiently similar stored statement, it will indicate its inability to identify the new pattern. The machine can then be given the name of the new pattern. This act is equivalent to teaching the machine a new pattern, because at any subsequent time the machine will be able to identify this pattern even if it is drawn by a different person.

A valuable feature is the way in which the machine indicates its confusion between two or more possible identifications of a pattern. This will arise when a new statement registers high scores with two or more statements belonging to patterns already "known" to the machine.

## Economical Storage

The reduction of the two-dimensional pattern to the one-dimensional statement form leads to an economical method of storing the patterns. A pattern with a resolution equivalent to a 50 -line television picture and having an information content of 2,500 bits can be represented by a statement with 40 to 80 bits.

As the number of patterns which the machine "knows" become large the time to compare a new statement with all existing statements would become excessive. To reduce this time, a classification system is employed. Thus all patterns with four ends or two curved lines would be stored in separate classes. A new statement is only then compared with members of suitable classes. The definition of "suitable" is again based on a scoring system. The success or failure in finding the right answers in a short time is used to modify the scores, so that the machine "learns" to recognize faster.

The simulation of this system was programmed for the now obsolescent Manchester Ferranti Mark I
M P x A


9

Fig. 3. Example of patterns which the system has shown itself capable of recognizing.
computer and the time to identify a pattern was about 1 minute. Using the Ferranti Mercury computer it can be done in 3 seconds. The provision of a more elaborate scanner, now under construction, with greater facilities for examining the patterns, will reduce this time to under one second, and finally a special-purpose digital computer, working in conjunction with this scanner, will give a further hundredfold increase in speed.

Whereas some of these times may appear long in relation to character recognition devices employing geometrical comparison, it must be remembered that the present system has very great versatility and can deal with any line pattern that can be resolved by the scanner. It has already demonstrated its ability to recognize such patterns as those shown in Fig. 3, some of which have been drawn by hand. It appears possible to be able to recognize good handwriting by a development of the same technique. It is wellknown that bad handwriting presents considerable difficulties even to human readers, and it is only possible to recognize certain words by reference to the context in which they are written. Thus the complete recognition of even average handwriting is a formidable task to perform by machine, but might be possible with the development of linguistic study used in the machine translation of languages.

## Nicrowave Data Tables

CALCULATIONS relating to a single specialized field of study tend continually to involve the same few basic mathematical functions of the quantities concerned. A considerable amount of routine sub-calculation can thus be saved by the use of specialized tables in which such functions have been already worked out. Such tables have up till now not been too readily available for microwave data, but this lack has now been remedied by the appearance of the book "Microwave Data Tables" by A. E. Booth, M.I.R.E., Grad.I.E.E. The author is a microwave development engineer for Sir W. G. Armstrong Whitworth Aircraft, Ltd.

Some of the tables in this book are of general as well as specialized interest. An example is the very extensive series of decibel tables which includes decibel gain or loss against power, voltage or current ratios. Also given are tables of v.s.w.r. (voltage standing wave ratio) - to voltage and power reflection coefficients. We also meet some familiar tables appearing in a new guise corresponding to their more specialized use. For instance reciprocals appear as v.s.w.r. $(<1)$ to v.s.w.r. ( $>1$ ), and squares as voltage-to-power reflection coefficients. More specialized tables include frequency to guide wavelengths for the $\mathrm{TE}_{10}$ mode in 9 standard

British sizes of rectangular guide, and a list of 28 standard British rectangular guides giving their dimensions, cut-off frequency, recommended operating range of frequencies and c.w. power rating. The contents of theselatter tables illustrate the waveguide bias which has been given to this book.

In these tables measurable quantities are always chosen for the independent variables and these are tabulated to the normal limits of measurement accuracy. The corresponding dependent variables are given to one more figure than is normally required, so as to avoid imposing any accuracy limitations in practical design and development work. Notes on the use of each table are included, and the formule used in calculation stated.

The conditions under which this book is likely to be used have not been forgotten: the tables are clearly printed on stout paper and strongly bound so as to stand up to constant use in the design office or laboratory.

The book contains 61 pages and 26 tables. It is available from booksellers $2 t 27 \mathrm{~s} 6 \mathrm{~d}$ or direct from our publishers, Iliffe and Sons Ltd., at 28s 8d including postage.

# Voltage-Tuned Oscillator 

Five-to-One Frequency Range with Grid Bias Variation Point

By G. W. SHORT

THE oscillator to be described in this article is an R-C oscillator of the "Wien bridge" variety. This makes use of the frequency-selective properties of the network shown in Fig. 1. When connected as shown, the output is a maximum, and the phase shift is zero, at one frequency $f_{0}$ given by $1 / 2 \pi \sqrt{ }\left(\mathrm{R}_{1}\right.$ $\mathrm{R}_{2} \mathrm{C}_{1} \mathrm{C}_{2}$ ). If such a network is used as a positive voltage feedback path in an amplifier of adequate gain, oscillation takes place at $f_{0}$.

By using valve internal resistance for $R_{1}$ and $R_{2}$ (Fig. 1.) it is possible to achieve electronically-controlled variation of frequency. The most suitable internal resistance is that ooking into the cathode of a cathodefollower or an earthed-grid amplifier, since this comes in convenient sizes and varies very widely with gridbias voltage, being approximately equal to $1 / g_{\mathrm{g}}$. If a valve with a slope of $5 \mathrm{~mA} / \mathrm{V}$ under its published normal-working conditions is chosen, then the cathode impedance varies from $200 \Omega$ to infinity (when the valve is cut-off). The frequency range is thus, in theory, infinite; but in practice the cathode impedances are always shunted by finite resistances, so giving a finite frequency range.

The frequency-selective circuit is obtained as shown in Fig. 2. The cathode impedances are shunted by $R_{1}$ and $R_{2}$, which are made as large as possible. The grid-to-cathode voltages, and hence the slopes of the two valves, are changed simultaneously by applying variable positive (with respect to earth) grid bias. If $C_{1}=C_{2}=C$, and the valves have the same slope, then $f_{0}=g_{\mathrm{m}} / 2 \pi \mathrm{C}$, neglecting the effect of the actual cathode resistors. (A formula including the effect of these is given in the Appendix).

The easiest way to inject a signal into the circuit is to apply it to the grid of the left-hand valve. The output can then be taken from the right-hand cathode. However, it seems a pity not to use the amplifying properties of the valves as a means of obtaining the loop gain necessary to cause oscillation. This leads to the circuit of Fig. 3, which is a complete oscillator. .. V2 then becomes an earthed-grid amplifier to which the network output is applied,

and V1 is a cathode-follower for driving the network. In a Wien-bridge network with both resistors and both capacitors equal, the network output is about a third of the input, so a gain of 3 is sufficient for oscillation. This requires a V2-anode load of less than $1 \mathrm{k} \Omega$ when the valve slopes are maximum, but when they are low a much greater load .s necessary. The load resistance is therefore fixed by the low-slope condition, but this results in too large a gain at the high-frequency end of the band where the slopes are high, and the circuit tends to behave as a multivibrator. For this reason a limiter is included. This takes the form of two point-contact germanium diodes connected back-to-back effectively across the amplifier load. The resistance of a typical diode is about $10 \mathrm{k} \Omega$ under zero-bias conditions; but it falls when a signal is applied, reaching perhaps $300 \Omega$ when 1 mA flows. The form of the grid voltage of V1 now approximates to a square wave, and we rely on the frequency-selective properties of the network and amplifier to get rid of the harmonics, taking a voltage output from the cathode of V2. Other methods of amplitude control may give a lower harmonic content in the output. However, ordinary methods such as grid-leak biasing cannot be used, since changing the grid bias also changes the frequency of oscillation. (If particularly-low harmonic content is required, $\mathrm{R}_{3}$ can be adjusted so that

Fig. 1. (a) "Wien bridge" frequency-selective network and (b) its amplitude and phase responses.


Left: Fig. 2. (a) Proctical arrangement for achieving voltage-controlled variation of $R_{1}$ and $R_{2}$. (b) Equivalent circuit. showing where the input voltoge con be injected. $R_{\mathrm{k}}$ should be much larger than $1 / g_{m}$.


Fig. 3. Complete oscillator circuit. The diodes $D_{1}$ and $D_{2}$ form a limiter to prevent multivibrator action.
oscillation just occurs, but a different setting is required for each frequency).
An oscillator was constructed using the circuit of Fig. 3 with $\mathrm{C}_{1}=\mathrm{C}_{2}=500 \mathrm{pF}$. The theoretical frequency (neglecting the effects of $R_{1,2}$ and the anode load of V 2 ) now becomes $\mathrm{g}_{\mathrm{m}} / \pi \mathrm{Mc} / \mathrm{s}$, and this and the measured frequency are shown in Fig. 4. (In this formula $\mathrm{g}_{\mathrm{m}}$ is in $\mathrm{mA}_{i} \mathrm{~V}$ and C is in pF .)
Having got so far, it was of interest to find out the hignest frequency at which oscillation could be obtained. At high frequencies, the gain falls off because of the shunting effect of stray capacitances, so there is no point in using high-value resistors. The anode and cathode resistors were reduced to $4.7 \mathrm{k} \Omega$, and oscillation was still obtained with anode currents of about 10 mA . The capacitors $\mathrm{C}_{1}$ and $\mathrm{C}_{2}$ were progressively reduced until oscillation ceased. This raised the maximum frequency of oscillation to about $8 \mathrm{Mc} / \mathrm{s}$; but it was felt that this could be improved upon. A frequency of about $13 \mathrm{Mc} / \mathrm{s}$ was obtained using $\mathrm{C}_{1}=50 \mathrm{pF}$. and nothing except the circuit strays for $\mathrm{C}_{2}$. The reason why this unequal combination of capacitances gives better results appears on re-examination of Fig. 1(a). As $\mathrm{C}_{1}$ is increased, or $C_{2}$ reduced, the ratio $E_{o r t} / E_{i n}$ gets bigger; because the impedance of the bottom part of the network relative to that of the top increases. Thus less loop gain is required when $\mathrm{C}_{1}$ is greater than $\mathrm{C}_{2}$, and vice versa. It should be possible, with careful component layout, to improve on the figure of $13 \mathrm{Mc} / \mathrm{s}$ somewhat. If much-higher fre quencies are aimed at, then a valve of higher slope, such as the E88CC $(12.5 \mathrm{~mA} / \mathrm{V})$ should be used.

If mechanical control of frequency is required to provide the main sweep, either or both capacitors $\mathrm{C}_{1}$ and $\mathrm{C}_{2}$ can be made variable. It is generally easier to make only one capacitor variable, namely $\mathrm{C}_{2}$, since the rotor then can be earthed. The frequency ratio $f_{\text {max }} / f_{\text {min }}$ is then reduced to $V^{\prime}\left(\mathrm{C}_{\text {max }} / \mathrm{C}_{\text {mul }}\right)$, which is typically a little over 3. A suitable value for the fixed capacitor $\mathrm{C}_{1}$ is $\sqrt{ }\left(\mathrm{C}_{\text {max }} /\right.$ $\mathrm{C}_{\mathrm{min}}$ ) which is about 160 pF when an ordinary variable capacitor ( $\mathrm{C}_{\max }=500 \mathrm{pF}$ ) is used.


Fig. 5. (a) R-L circuit for avoiding use of cathode resistors.
(b) Equivalent tuning network.

(b)


Fig. 6. Transistor-oscillator circuit (equivalent to Fig. 3).
tions, reasonably-high frequency-stability is required. The stability of the oscillator described here is obviously very poor by normal standards, since the frequency can be pushed about by changing the circuit voltages. However, when a stabilized h.t. supply was used the stability was better than expected, bearing in mind the fact that the frequency is a function of the valve slopes. The reason is probably that the mutual conductance of a valve is a function of the cathode current, and in the present circuit, the cathode current is rigidly controlled by the heavy d.c. negative feedback due to the large-value cathode resistors. To a first approximation, the current is simply $V_{g} / R_{b}$, where $V_{g}$ is the external bias voltage. The accurate expression is, of course $\left(A V_{k}+v_{g}\right) / R_{k}$, $v_{g}$ being the actual grid-to-cathode bias and A the "gain" of the valves as cathode-followers. It is unlikely that $\mathrm{v}_{\mathrm{g}}$ will vary by more than a fraction of a volt as a result of normal short-term emission and heater voltage variations, and since $V_{g}$ may be as much as 100 V , the variations are small in comparison to the total voltage.

The d.c. supplies must be well smoothed as well as stabilized, otherwise hum voltages will frequencymodulate the oscillator, although it may be convenient to dispense with stabilization for the main h.t. supply provided that it is reasonably well regulated; the required tuning potential ( 100 V ) may then be developed across a gas-discharge stabilizer, such as a VR105/30. Other causes of f.m. are heater-tocathode leakage, heater-to-grid leakage, and heater emission, the first being particularly undesirable because of the high-value cathode resistors. A possible way out would be to use an L-R tuning network (Fig. 5) and negative grid bias, or to "tie" the heater supply to the slider of $\mathrm{R}_{5}$. But a more attractive method would be to use transistors instead of valves and avoid the possibility of cathode hum altogether. The circuit of Fig. 6 is suggested as a basis for experimental determination of circuit values.

The frequency ratio of five-to-one obtained in the experimental oscillator does not represent the practical limit. At the high-frequency end of the range, the frequency can be raised as far as the valve slopes will allow. If the slope of the valves used had been $10 \mathrm{~mA} / \mathrm{V}$, the top frequency would have been over twice that obtained with $5-\mathrm{mA} / \mathrm{V}$ valves. The lowfrequency limit can be extended by increasing the value of the cathode resistors when the largest convenient values for $C_{1}$ and $C_{2}$ have been reached.

## APPENDIX

The effect of $R_{k 1,2}$ in the circuit of Fig. 2(b) is neglected above, and so is the effect of the anode load of V2 on the cathode input impedance of V2. The effects on frequency can easily be allowed for. Referring to the equivalen circuit shown in Fig. 7, where $r_{k}$ stands for the impedanr


Fig. 7. Equivalent R-C oscillator network.
looking into the cathode, the frequency is obtained by calculating the resistance of $R_{k 1}$ and $\mathbf{r}_{\mathbf{k} 1}$ in parallel and substituting this for $R_{1}$ in the usual formula $f_{0}=$ $1 / 2 \pi \sqrt{ }\left(\mathrm{R}_{1} \mathrm{R}_{2} \mathrm{C}_{1} \mathrm{C}_{2}\right)$ and calculating $\mathrm{R}_{\mathrm{k} 2}$ and $\mathrm{r}_{\mathrm{k} 2}$ in parallel and substituting for $R_{2}$. The effect of the anode load, $R_{a}$, of $V_{2}$ on $r_{k 2}$ is to increase the impedance looking into the cathode so that it becomes $\left(R_{a}+r_{a}\right) /(1+\mu)$ instead of just $r_{s} /(1+\mu) \approx 1 / g_{m}$. The effect of the actual cathode resistors is to increase $f_{0}$, and that of $r_{k 2}$ is to reduce $f_{0}$, so to some extent they offset one another.

A more serious effect of $R_{k 1}$ is that it increases the attenuation of the network. $\mathrm{E}_{\mathrm{in}} / \mathrm{E}_{\text {out }}$ becomes:-

$$
1+r_{\mathrm{k} 1} / \mathrm{r}_{\mathrm{k} 2}^{\prime}+\mathrm{r}_{\mathrm{k} 1} / R_{\mathrm{k} 1}+\mathrm{C}_{2} \mathrm{r}_{\mathrm{k} 1} \mathrm{C}_{1} \mathrm{R}_{\mathrm{k} 1}+\mathrm{C}_{2} / \mathrm{C}_{1}
$$

where $r^{\prime}{ }_{k 2}$ is the parallel combination of $R_{k 2}$ and $r_{k 2}$. This has its greatest effect at the low-frequency end of the range, where $r_{k 1} / R_{k 1}$ is greatest. But in practice one can easily make $R_{k 1}$ ten times $r_{k 1}$, and the effect is then negligible for most purposes.


CLOSED-CIR CUIT TELEVISION at Dublin Airport forms part of a system, undergoing trial by Aer Lingus, for the remote display of weather information: this saves the pilots as much as a 20 -minute journey to the Met. Office. Installed by Philips Electrical (Ireland) Ltd. the television equipment comprises two camera chains; also two-way speech facilities and a Muirhead facsimile-transmitting ond receiving system are provided. A 21 -in television display fed by a coaxial cable in the Operations Room provides direct information (the photograph shows the transmission of a weather briefing) and the "Mufax" is uses to produce a detailed information folder which is carried in the aircraft.

# Transistor A.F. Oscillator 

For Use as a Morse Practice Set or a Bridge Source

By H. B. DENT

REQUIRING a small and compact audio frequency oscillator for general-purpose use in place of a rather cumbersome external mains-driven affair, thoughts naturally turned to the use of a transistor. A search through the available literature revealed a surprising lack of practical details of oscillators of this kind, except for one forming part of a larger equipment,* and it appeared that the only course open was to make a few preliminary bench tests of likely circuits before deciding on the final layout.

The first circuit tried is shown in Fig. 1 where an OC70 transistor is used with an orthodox feedback circuit using a triple-wound transformer. The tertiary winding was included to isolate the oscillator from external equipment and so minimize the effect of this equipment on the frequency of oscillation.


Fig. 1. Transistor oscillotor circuit using triple-wound transformer.

It was required to find a suitable value for the resistor $R$, which determines the base-bias current of the transistor, as the few published circuits encountered had shown very wide difference in values for this resistor, even when a similar battery voltage was employed.

The battery lead was broken at the point $x$ and a $0-1 \mathrm{~mA}$ meter inserted. Fig. 2 shows the current taken by the transistor (oscillating) with different values of resistance at $R$. A pair of headphones connected across the output winding served for monitoring the audio signal. Unfortunately no means were available at the time of actually measuring the a.f. output as correlating its magnitude with the d.c. input to the transistor would have provided useful data.

In view of the high value of resistance used for R in all cases it can be assumed that the bulk of the *"Transistor Transmitte;," by L. F. Shaw, Wireless Worl', May 1958, p. 242.
current measured by the meter is the collector current $\left(I_{c}\right)$. The information gained from the curve is interesting as with R of $100 \mathrm{k}!2$ or less quite small minus tolerances in resistance can produce very large increases in collector current, so that with this type of osciliator the series resistor in the base circuit ought not to be less than $150 \mathrm{k} \Omega$ with a nominal collector voltage of 4.5 V . Preferably it should be nearer $220 \mathrm{k}!2$, under which conditions the collector current is about 150.4 A . This oscillator would be quite satisfactory for many purposes, especially where only a relatively small a.f. output is required.

These crude measurements served their purpose, however, by emphasizing the desirability of a more sure stabilization of the d.c. bias for the base and this led to a trial of the circuit shown in Fig. 3.

The component values were arrived at largely by

fig. 2. Collector current with different values of resistor $R$.


Fig. 3. Oscillator circuit with base current stabilized.


Fig. 4. A convenient form of construction for the transistor oscillator. Components can be identified from Fig. 3.
trial and error, although the working conditions were approximately determined from the maker's data sheets for a current load not exceeding 0.5 mA with a $4.5-\mathrm{V}$ battery. This presupposed a base current of less than $10 \mu \mathrm{~A}$ so that the potential divider $R_{1}$ and $R_{2}$ need not consume more than about $100 \mu \mathrm{~A}$ leaving about $400 \mu \mathrm{~A}$ for the collector current. With the base voltage set to be just slightly more negative than the emitter the nearest preferred 20 - \% tolerance resistors for $R_{1}$ and $R_{2}$ were $2.2 \mathrm{k} \Omega$ and $33 \mathrm{k} \Omega$ respectively. $R_{1}$ was bypassed by a $0.1-\mu \mathrm{F}$ capacitor and $R_{3}$, which is included as a further safeguard for d.c. stability, by a $25 u F$ capacitor.

With the particular OC70 transistor employed the total current through $\mathrm{R}_{2}$ was $115 \mu \mathrm{~A}$ and the collector current was $260 \mu \mathrm{~A}$, making a total battery drain of $375 \mu \mathrm{~A}$. The af. output was uncomfortably loud in high-resistance headphones and thus judged adequate for the purpose of energizing a CR bridge.

No value has been marked for $C_{1}$ as this depends on the particular use to which the oscillator is put. For energizing a CR bridge, which is but one of several applications subsequently found for similar units, any capacitance from $0.1 \mu \mathrm{~F}$ to $10 \mu \mathrm{~F}$ or more can be used. When, however, the oscillator is used as a Morse practice set, and the key inserted in place of the on/off switch (Fig. 3), $C_{5}$ should not be larger than $0.1 u \mathrm{~F}$. If it is oscillation does not stop immediately the key is released after a dot or dash but is maintained by the charge on $C_{1}$. If $C_{4}$ is only slightly too large it puts a "tail" on dots and dashes which upsets the relative spacing of the Morse characters and if speed is attempted dots and dashes merge and the signals become unintelligible.

The small transformer was made specially for this oscillator and consists of a 0.4 -in stack of No. 74 N " E " and "I" "no-waste" stampings (Mag. netic and Electrical Alloys) but any similar sized core will do $\left(1 \frac{23}{3} \times 2 \frac{1}{16} \times 0.4 \mathrm{in}\right)$. Thin sheet Paxolin
was used for the end cheeks of the bobbin glued (Durofix) to a core tunnel made from thin cardboard covered with several turns of gummed paper. It was made on a wooden mandrel a shade larger, as regards width, than the tongue of the " E " stamping.
The base winding A was put on first and consists of 50 turns of No. 38 s.w.g. enamelled copper wire. Winding B, with 1,000 turns of the same wire, followed and finally winding C with 200 turns. The black dots adjacent to one end of A and B windings (Fig. 3) indicate the beginning (or inner) of each, all windings being in the same direction. No marking is required for winding C as its phasing with the other windings is not important, but correct phasing is essential for A and B or the circuit will not oscillate.
With windings and components as specified the frequency of oscillation is about $1,000 \mathrm{c} / \mathrm{s}$, but any frequency within reasonable bounds can be generated by using a suitable value of capacitance for $\mathrm{C}_{2}$.
The oscillator in its final form is shown in Fig. 4, which should be self-explanatory. The annotation enables the various components to be identified by reference to Fig. 3. With perhaps the exception of $C_{3}$ the capacitors are physically much larger than they need be as 150 -volt working type was used whereas 6 - or 12 -volt types would be adequate. All resistors can be $\frac{1}{4} \mathrm{~W}$ or smaller.

## MOON REFLECTION TESTS

THE transmitter used at Jodrell Bank for the successful communication tests during last May with the Air Force Research Centre at Massachusetts via reflections from the moon was designed and built by Pye Telecommunications, Ltd., Cambridge. It has an


Part of the Pye f.m. transmitter used at Jodrell Bank. output of 1 kW at $201 \mathrm{Mc} / \mathrm{s}$ and is frequencymodulated with peak deviations variable from $2 \frac{1}{2}$ to $15 \mathrm{kc} / \mathrm{s}$. The $250-\mathrm{ft}$ aerial has a gain of 40 dB and a beam width of $1_{1}{ }^{\circ}{ }^{\circ}$ at $200 \mathrm{Mc} / \mathrm{s}$ (angle subtended by the moon is $\frac{1^{\circ}}{}{ }^{\circ}$ ).

The receiver used for monitoring at Jodrell Bank had a noise factor of 6 dB and bandwidths of $\pm 2 \frac{1}{2}, 5$ or $10 \mathrm{kc} / \mathrm{s}$. Measured signals at the input varied between 0.2 and 1.5 V which is in good agreement w it h 0.7 V derived from a calculated p ath loss of 250 dB .

# LIETTERS TO THE EDITOR 

The Editor does not necessarily endorse the opinions expressed by his correspondents

## "Audion"

IN "Free Grid's" article of September he makes a reference to de Forest's "Audion" and the derivation of the word.
de Forest first used the word for his original twoelectrode valve, a device not very dissimilar to the Fleming valve.

I was present in New York at de Forest's lecture on his two-electrode Audion at the American Institute of Electrical Engineers meeting in 1906 and I remember very distinctly the criticism made after the lecture by the famous loading coil inventor Dr. Pupin. Pupin concentrated entirely on the word, objecting to it strongly as a mixture of Latin and Greek-in fact he said it was a bastard-as he used the word with some emphasis it caused much laughter.

London, E.C.1.
H. J. ROUND.
"FREE GRID," in your September issue, wonders about the derivation of the term "Audion."

Over 40 years ago, I read an article in Mr. Hugo Gernsback's journal Electrical Experimenter written by Dr. Lee de Forest, in which the doctor wrote, as far as I can remember:
" My laboratory assistant, Mr. Harvey L. Gainer, suggested the beautiful and not inappropriate name "Audion," derived from the Latin "audio" (I hear) and "ion," the latter being the carriers of the electric current in a vacuum."
Unfortunately, I cannot at the moment find my copy of the magazine, to make the quotation strictly verbatim, but believe "Free Grid" can rest assured that this was the origin of the name.

Electronic communications had not then advanced to the point where it was necessary to make distinctions, such as audio, i.f., r.f., v.h.f., etc., to indicate different range: of frequencies.

Windsor, Ont., Canada.
H. S. GOWAN.

Canadian Pacific Communications.

## Long-distance V.II.F. Reception

IN the September issue your correspondent J. E. Le B. Terry invited opinions on the subject of long-distance v.h.f. reception.

Here in Aylesburv, which is situated about 65 km North West of London, Italian f.m. broadcasts are generally received between the months of May and September. This year they were heard on June 14th, 20th, 25th and 26 th and again on July 22ad. Reception was particularly good on June 14th with Italian stations heard here from 0930 until 1358 G.M.T. At least 26 were being received at 1240 G.M.T. between 88 and $98 \mathrm{Mc} / \mathrm{s}$.

Italian stations on Band II have been received as early as 0715 and as late as 2220 G.M.T. The best periods of reception being the mid-morning or afternoon.

I entirely agree with Mr. Terry that the behaviour of tirese signals is totally different to that associated with tropospheric propagation.

My own observations have shown that after remaining steady for a short period, signals will go into a sudden deep fade, returning almost immediately to their original strength.

In view of the distance involved, I find it hard to believe that the right type of weather conditions could maintain
tropospheric reception over such an area. Long-distance tropospheric reception rarely exceeds $900 \mathrm{~km} ; 500$ to 600 km being more usually observed by the writer. It would seem therefore that the reception of signals at considerably greater distances than the above can only be via the ionosphere.

It is interesting to note that long-distance reception in Band II occurs at the time of the year when sporadic-E is known to propagate television signals over similar distances in Band I. The theory that sporadic-E cannot reflect signals higher in frequency than about $60 \mathrm{Mc} / \mathrm{s}$ may therefore prove incorrect, especially in view of the fact that amateur radio operators in this country have made contact this year with Italian amateurs on the twometre band ( $144-146 \mathrm{Mc} / \mathrm{s}$ ).

I trust that these notes may interest your correspondent and other readers and in concluding I would like to thank the various European broadcasting organizations who have verified my reception reports of their f.m. stations.

Aylesbury, Bucks.
A. H. UDEN.

## Finnagle's Law?

WITH reference to the availability of Test Card " C " ("Diallist," Sept. issue), it may not be generally known that this problem may be resolved mathematically as follows:

If the number of receivers to be set up is N , then-

$$
\mathrm{N}^{2}+c f=\frac{t c}{d+t f}+a
$$

where: $d$ is the average distance in miles between sets.
$t$ is the total time available in hours.
$t f$ is the Traffic Frustration Factor.
$c$ is the Coefficient of Asynchronization (this is an expression relating to the frequency with which the B.B.C. will transmit the Test Card whilst the I.T.A. is not so transmitting (or vice versa),
cf is the card recurrence frequency.
$a$ is the accuracy in \% loss or gain, of the service engineer's watch.
N.B.-Serious students of this and similar aspects of servicing, are referred to the standard work on the subject, "Alsoarbeitsitzundweytz-Eine Teleteufelhandlungsphilosophie" (Ewigkeit u. Ewigkeit, Hamburg, Rm 65). This should be read in the original-some of the subtler nuances being virtually untranslatable.
Canterbury.
K. DICE.

I wOULD like to add, if I may, to Mr. J. Darr's delightful article on Finnagle's Law. The I.P. of I.O. (Innate Perversity of Inanimate Objects) is immortalized in a little verse which I heard a long time ago. The authorship escapes me, but the lines run thus:

I never had a piece of toast
Particularly long and wide,
But fell upon the sanded floor,
And always on the buttered side.
By the way, in our laboratory, the Fiddle Factor is never referred to as such; we always give it the more exalted tit'e of "Cook's Constant."

Chelmsford.
W. R. MASEFIELD.


Transistor A.G.C. Circuits present some problems which are not met in designing valve receivers-the major difficulty being that the transistor cannot effectively reduce the signal below a certain limit. In I.R.E. Transactions on Broadcast and Television Receivers for January, 1959, F. J. Banovic and R. L. Miller discuss two methods of applying a.g.c. to transistor i.f. amp'ifiers and they describe a new method invented by J. A. Worcester. The simp'est and most common arrangement is to feed back the d.c. developed at the detector to the base of the first i.f. amplifier, which is connected in the earthedemitter mode. An improvement to this circuit is the addition of an "overload diode," as shown immediately below. This gives some measure of delay, as the voltage drop across the i.f. amplifier collector

resistor holds the diode cut-off until a certain signal level is reached. When the voltage drop is reduced by the action of the simple a.g.c. on the i.f. amplifier the diode conducts, shunting the mixer o.p.; but this point depends on the d.c. amplification of the transistor, so an individual adjustment of the collector resistor has to be made for the best performance. The new method does away with the need for an overload diode and individual adjustment by reconnecting the i.f. amplifier as an earthed-base stage to i.f. and earthed-emitter to

d.c., with the a.g.c. applied to the base. This causes the i.f. input impedance (input to the emitter) to vary widely with the a.g.c. action: thus, on a strong signal, the input impedance of the i.f. trazsistor is increased as its gain is reduced. The increase in input impedance disturbs seriously the matching of the i.f. amplifier to the previous stage (usually the mixer) to which it is matched for maximum signa'-power transfer at maximum sensitivity, so reducing the signal transfer and giving the effect of a.g.c. applied to two stages. Alloy-junction transistors are more suitable for this jircuit than rate-grown types, as alloyjunction transistors exhibit a greater change of input impedance for a given change in emitter current.

## Real'stic Interference Generator

 has been developed by Mullard Research Laboratories as an instrument for testing the performance of television sets in unfavourable reception conditions. Realism of ignition interference is achieved by generating sparks with a motor-car sparking plug, while the mains-borne type of interference is provided by an electric shaver motor. Interference signols are picked up by a coil from the sparking plug and by a resistor from the motor and fed to $75-\Omega$ coaxial output sockets via separate attenuators and matching networks. The sparking plug voltage is generated bya valve pulse generator, using a television line-output valve working into a step-up transformer. This generator (a multivibrator) can either be repetitively gated to give bursts of pulses, or varied in p.r.f. by a sawtooth sweep waveform from a Miller transitron circuit. The gate circuit can be locked either to an external $50-\mathrm{c} / \mathrm{s}$ signal or to the supply mains (in either phase), and a phantas:ron delay circuit allows the timing of the gate pulse to be adjusted so that the burst of interference pulses can be located anywhere in the television frame period including the frame sync pulses. Duration of the inter-ference-pulse burst can also be controlled. The p.r.f. of the interference pulses is made variable (between about $30 \mathrm{c} / \mathrm{s}$ and $170 \mathrm{c} / \mathrm{s}$ ) to simulate the effects of gear changes in a motorcar, which, of course, are accompanied by changes of engine r.p.m. and ignition-spark frequency.

Silicon Solar "Batteries" of high efficiency are now available to provide the same power output, watt for watt, as dry-cell and mercury-cell batteries. Supplied by the International Rectifier Co. (Great Britain), the units are intended for powering transistorized equipınent during daylight operation and for charging storage batteries for continuous day and night operation. Each silicon solar battery contains five series-connected $1 \mathrm{~cm} \times 2 \mathrm{~cm}$ solar cells, encapsulated in an epoxy resin to provide a strong, weatherproof housing. The output voltage is 1.75 volts at a temperature of $30^{\circ} \mathrm{C}$ and 1.5 volts at $65^{\circ} \mathrm{C}$ (typical ope:ating temperature in direct sunlight). Direct replacement may be achieved by substituting one solarcell unit for each 1.5 -volt dry-cell battery, and adding as many in parallel as may be required to sungly the necessary load current. Each unit will supply a load current of

approximately 35 mA in direct sunlight. In applications calling for the charging of storage batteries, the solar-cell units can be used in conjunction with sealed nickel-cadmium accumulators.

By J. SKINNER*

THE testing method described in this article was developed to meet the requirement of rapid, accurate testing of large quantities of small power and audio transformers.

In Fig. 1 the arrows represent the relative instantaneous direction of the terminal voltages of each transformer winding. It is obvious that the series connection of the two secondary windings will produve either the sum or difference of the two voltages, depending on the phase of connection. Thus if the number of turns on each secondary are supposedly identical, then zero voltage will appear at the terminals if the windings are connected anti-phase. If a voltage does appear, then the cause is due either to the windings not being identical, or to a non-sinusoidal waveform.

Waveform distortion readings may be eliminated by the use of a non-saturating flux density. Values found to be suitable are (i) 8-9 kilogauss (kg) for silicon iron, (ii) $13-14 \mathrm{~kg}$ grain oriented material, (i:i) $15-16 \mathrm{~kg}$ for C-Cores. Any measurable reading should now be due entirely to turns differences, the magnitude of error being generally in proportion to the voltage developed.

Fig. 2 shows an alternative and more versatile arrangement. Transformer $A$ is a perfect specimen and is retained as a standard, while $B$ represents the unit to be tested, both units, of course, are expected to be identical. We are, of course, not limited to a single secondary winding. In fact, any number of wiadings and taps may be tested.

Returning once again to the zero voltage obtained from balanced windings, there is a possibility that one winding is open circuited, or that there is no supply voltage. In fact, the test is a negative one. In addition, a faulty winding will certainly produce a voltage, but the same voltage will be produced by either a negative, or a positive, turns error. Fortunately, all doubts can be easily dispelled by a simple modification. It is apparent that an "out of ba!ance" vo tage will be the result of a turns error in either the secondary winding, or in the primary winding.

* Radford Electronics, Ltd.


# Defects Revealed by Connecting 

Output Windings in Anti-phase
with Standard Component.

Furthermore, if we deliberately introduce a temporary error in the primary side of our standard unit, then "out of balance" voltages should appear at all test points. The voltage actually appearing at each point is predictable, and errors in turns ratio will be indicated by either an increased or by a decreased reading, thus indicating polarity of error.

It should be observed here that the indication of an error depends upon the turns ratio of the unit, and is therefore quite independent of variations in supply voltage. The magnitude of voltage readings


Fig. 2 Bosis of testing procedure described in the text. Transformer $A$ is a standard, transformer $B$ the one under test.
are, however, subject to variations in proportion to the mains fluctuation.

The final form of our test set is as shown in Fig. 3. The deliberate error in standard unit $A$ is effected by means of the tapped auto-transformer C. A switch is used to select either the under-voltage, which can be described as "Test Volts," or the ratio balance test voltage, which is described as "Test turns."
Finally a word of warning. If the unit " $B$ " is accidentally connected "in phase" with the appropriate winding of "standard A," then the voltage applied to the indicator will be double that of each


Fig. 1 Relative instantaneous voltages in a transformer is shown by arrows.

Fig. 3 Final arrangement of the test set-up as described in the text.
secondary. If the indicator is a moving-coil meter, adjusted to give a measurable reading of even $10 \%$ VA error, then a $200 \%$ VA overoad will cause considerable damage. Alternative instruments, such as a valve-voltmeter, could, of course, be utilized, or a limiting device may be used.

Accuracies of the order of $\pm 0.5 \%$ have been achieved by this method of testing, as many as seven test indications being made in one operation. Several
sets have actually been constructed by the author, and are still in use. They have been proved to be sensitive, accurate and extremely simple to use, even by unskilled operatives.
Acknowledgment.-The author expresses his appreciation of the facilities afforded for the development of this method by A. H. Radford, of Radford Electronics, Ltd., and for his assistance in producing this article.

# Elements of Electronic Circuits 

## 7.-AMPLIFYING DIFFERENCE VOLTAGES

By J. M. PETERS, B.Sc. (Eng.), A.M.I.E.E., A.M.Brit.I.R.E.

THE cathode-coupled paraphase amplifier is sumetimes known as a "cathode inversion circuit" or, more commonly, as a "long-tailed pair." Although it can perform a variety of rôles its main function is to accept and amplify the difference between the voltages appearing at the two grids, and to present them at the anodes as a balanced push-pull voltage.

The basic circuit is shown in Fig. 1. Two similar


Fig. I valves, with equal loads, $\mathrm{R}_{\mathrm{L}}$, and similar mutual conductances, have a common cathode resistor $\mathrm{R}_{\mathrm{k}}$. For the correct functioning of the circuit it is necessary for the cathode current (i.e., the total valve currents) to be as nearly constant as possible and independent of any changes caused by varying inputs to the grids. To achieve this, one end of $\mathrm{R}_{\mathrm{k}}$ is taken to a large negative voltage and the value of $R_{k}$ is adjusted to give the required current sufficient for Class A bias in the absence of signal. A constant-current valve (pentode) can be used instead and is preferable. The constant current in $R_{k}$ divides equally between $V_{1}$ and $V_{2}$; therefore if the anode current in $V_{1}$ is caused to rise, the current in $V_{2}$ must fall by a corresponding amount.

A symmetrical voltage applied to both grids will produce no effect in the anode circuits. Now suppose an asymmetrical voltage is applied to the grids, $+v$ to $\mathrm{V}_{1}$ and $-v$ to $\mathrm{V}_{2}$ :
$\mathrm{I}_{a_{1}}$ will increase to $\mathrm{I}_{a_{1}}+\mathrm{g}_{m} v$
$\mathrm{I}_{a_{2}}$ will decrease to $\mathrm{I}_{a_{2}}-\mathrm{g}_{m} v$
(Note that the total current remains constant.) The result of this is that the difference voltage is amplified and appears as a balanced push-pull signal at the anodes. The voltage between the anodes is ex-
pressed by the relationship $\mathrm{g}_{n} \mathrm{R}_{\mathrm{L}}$ multiplied by the difference voltage at the grids.
Now suppose the voltage on $V_{2}$ grid is fixed while the voltage on $\mathrm{V}_{1}$ grid is permitted to increase. Ulimately all the available current will flow in $V_{1}$, and $V_{2}$ will become cut-off. The cathode voltage will continue to increase and follow the voltage on the grid of $V_{1}$, in other words the cathode voltage will always tend to follow the more positive grid.
An important application of the cathode-coupled paraphase amplifier is to computer circuits, as a means of obtaining sum and difference voltages. Suppose we apply positive-going pulses to the grids of $V_{1}$ and $V_{2}$. The difference in voltage appearing at the anodes is proportional to the difference between the input voltages. The voltage appearing at the cathode is proportional to the sum of the input voltages. Two trains of voltage pulses occurring at different intervals and applied to the two grids of the amplifier will therefore result in the production at the cathode, and between the anodes, of waveforms proportional to the sum and difference of the input trains.
Before passing on, next month, to somewhat different subjects, it is perhaps appropriate at this point to mention another useful type of two-valve circuitthe cascade amplifier. On account of the very high amplification which can be obtained with the minimum of positive Miller feedback from output to input, the cascade method of connecting two triodes, as shown in Fig. 2, is quite often adopted as an alter-


Fig. $<$
native to the use of pentodes in wideband amplifiers.
By connecting two triodes having similar mutual conductances in cascade, it is possible to obtain an effective anode impedance of value approaching that of a pentode, thereby permitting the use of large anode loads. If the two triodes have individual slopes $=\mathrm{g}_{m}$, amplification factors $=\mu$ and anode impedances $=R_{a}$, then when connected in this manner the composite circuit behaves as if it were a single valve of slope $\mathrm{g}_{n}$, anode impedance $\mu \mathrm{R}_{\mathrm{a}}$ and amplification factor $=\mu^{2}$.

It is theoretically possible to connect more than two valves in cascade, thereby obtaining very high amplification factors-the index by which $\mu$ is raised depending on the number of valves connected in this way.

If the circuit in Fig. 2 is examined it will be noted that the grid of $\mathrm{V}_{2}$ is held at a fixed positive poten-
tial. The input signal is applied to the grid of $\mathrm{V}_{1}$ and appears at the anode of $V_{1}$ in opposite phase but not amplified. The reason for this lies in the fact that the impedance presented to $V_{1}$ by $V_{2}$ is low. The anode load of $\mathrm{V}_{1}$ is actually the cathode impedance of $V_{2}$ which approximates to $1 / g_{m_{2}}$. As this is a small load for $V$, the approximation $g_{m}, R_{r}$. can be assumed as representing the gain of stage $V_{1}$. Substituting $1 / g_{m_{2}}$ for $R_{\mathrm{L}}$, we have that the gain of stage $V_{1}=g_{m_{1}} \times 1 / g_{m_{2}}$, but as $V_{1}$ and $V_{2}$ are arranged to have identical slopes, i.e., $\mathrm{g}_{m_{1}}=\mathrm{g}_{m_{2}}$, therefore the gain of stage $V_{1}=g_{m_{1}} \times 1 / g_{m_{1}}=1$. The stage $V_{1}$ does not amplify.

The inverted input signal appears at the anode of $V_{1}$ and hence at the cathode of $V_{2}$. As the grid voltage of $V_{2}$ is held at a constant value, the $V_{2}$ cathode voltage variations appear at the anode of $\mathrm{V}_{2}$ reversed in phase but amplified.

# AMMONIA-MASER PROGRESS 

SEALED-OFF OSCILLATOR UNDER DEVELOPMENT

THE development of a small, robust and lightweight frequency standard with a stability of better than 1 part in $10^{\circ}$ is a thing many people dream of for use in navigation and communications. At present two devices-the ammonia maser and the caesium clock --offer the required stability, but until recently both have been regarded as research-laboratory items, rather than pieces of appara!us that could, for instance, be used in an aeroplane or at a u.h.f. communications link.

Ammonia masers have been demonstrated publicly*; but, although the size of the maser itself has been acceptable, it has been continuously pumped; the vacuum pumps and other ancillary apparaius bringing the total bulk up to that of a small wardrobe. However, work in progress at Glass Developments, Ltd., indicates that a sea'ed-off maser and its control and supply equipment will be possible within a volume of about $1 \mathrm{cu} . \mathrm{ft}$., the maser itself being abnut 12 -in long and 3 -in diameter. Several improvements in internal design have made this possiblefor instance, the shortening to a few inches long of the "tunnel" in which electrostatic separation of the active from the inactive molecules is carried out. The basic principle of oyeration of the sealed-off maser is that a charge of ammonia gas is placed in the device and frozen in a reservoir behind the collimator, which consists of an array of parallel tubes. As the gas evaporates it passes through the collimator to form a molecular beam which enters the electrostatic separator in the normal manner of the ammonia masert. The unwanted "inactive" molecules are condensed on the liquid-nitrogen-cooled sides of the maser envelope. After about 100 hours of operation the stored ammon'a is exhausted; then the maser is simply inverted in the nitrogen bath. The reservoir behind the collimator is now the coldest part of the

[^4]maser and, as the gas evaporates from the sides of the vessel it passes back into the reservoir and is frozen there. This re-circulation of the ammonia can be carried out any desired number of times and takes about one hour to complete.

Due to the re-circulation process, it may be possible to use ammonia compounded with the relatively expensive nitrogen isotope $\mathrm{N}^{1.5}$ instead of the more common $\mathrm{N}^{\prime \prime}$. Swiss work indicates that this will increase the stability of the maser output because the frequency spectrum exhibited by $N^{13}$ ammonia is much narrower than that of the $\mathrm{N}^{14}$ variety, thus reducing the frequency-pulling effect that can be exerted by the cavity.

The high-voltage supply for the separator and the cavity-temperature control equipment will use transistors, and these items, together with a frequency divider to give outputs at integral frequencies such as $30 \mathrm{Mc} / \mathrm{s}, 10 \mathrm{Mc} / \mathrm{s}, 1 \mathrm{Mc} / \mathrm{s}$ and $100 \mathrm{kc} / \mathrm{s}$ locked to the maser, make up the rest of the equipment.

## "Wireless World" Diary

TECFINICAL and general information of the kind so often needed by radio men but seldom readily available will be found in tab!oid form in the 80-page reference section of the 1950 Wireless World Diary. Some idea of the diversitv of information it includes will be gathered from this selection from the contents: aerial dimensions and aerial sharing circuits, licensing regulations, addresses of radio organizations in this country and abroad, world television standards, radar frequency bands, comoonent coding, U.K. television and v.h.f. sound broadcasting stations and tabulated base connections for ove: 70c, current receiving valves.

The Diary costs 6 s 3 d (leather) or 4 s 6 d (Rexine), including P.T. Overseas prices, including postage, are, respectively, 5 s 8 d and 4 s 2 d .

# Reception of Space Diversity 

THE British Broadcasting Corporation recently provided a series of transmissions to test the effectiveness of transmitter space-diversity on reception at distant points. Both very wide'y-spaced and relatively closely-spacsd transmitters were used in the tests. The trans aissions were at a frequency of $9,510 \mathrm{kc} / \mathrm{s}$, directed towards the east coast of the United States. Transmitting conditions were switched at intervals of approximately fifteen mirutes during the testing period each day.

Observations of the received signals were made at the National Bureau of Standards Laboratories in Boulder, Colorado, from November 3, 1958 to November 14, 1958. The recordings obtained during these observations have been analyzed for fading characteristics and intelligibility, and the results of the analysis are given in this article.
Test Procedures, B.B.C. Transmissions.-The transmitters were located at Daventry and Woofferton in England. Two transmitters at Daventry were used for close-spaced diversity tests and one at Daventry and one at Woofferton for the wide-spaced diversity tests. Centre-to-centre spacing of the two antennae systems at Daventry was $1,540 \mathrm{ft}$ with one antenna SSW of the other. The wide-spaced diversity transmitting systems were separated by approximately 65 miles in an east-west direction and all antenna arrays were directed on a bearing of $294^{\circ}$. The schedule of transmissions during the test period each day was as follows:-
2345 to 0015 G.M.T.-Daventry transmitter A 0015 to 0030 G.M.T.-Daventry transmitters A and B
0030 to 0045 G.M.T.-Daventry transmitter A
0045 to 0100 G.M.T.-Daventry transmitter A and Woofferton transmitter C
The transmitter carrier frequencies were all phase locked to each other.
N.B.S. Receiving Arrangements.-A horizontal half-wave receiving antenna, elevated one-half wavelength above the ground, was used for the observations at Boulder. The audio output of a Type SP600 receiver was fed to a magnetic tape recorder; this receiver had an intermediate frequency bandwidth of $8,000 \mathrm{c} / \mathrm{s}$. A second SP600 receiver, with an intermediate bandwidth of $800 \mathrm{c} / \mathrm{s}$, was used for carrier-envelope recordings. The a.g.c. voltage of this receiver was used to operate a strip-chart recorder. Receiver linearity and recorder-circuit time constant are such that voice modulation did not noticeably affect these recordings. The receiving system for the strip-chart recorder was calibrated on the basis of available received power in a matched load at the antenna terminals.
Results of Observations.-Rapid flutter fading, at about 5 to $10 \mathrm{c} / \mathrm{s}$, occurred on six of the twelve days that observations were made. A section of the greatcircle path from Eng'and to Boulder is near the zone of maximum auroral activity, and flutter fading is characteristic of high-frequency ionospheric-pro-


Fig. 1. Theoretical distribution of signal envelope.


Fig. 2. Distribution of signal envelope amplitude.

## Transmitters

## THE USEFULNESS OF THE SYSTEM

pagated signals passing through auroral disturbed regions. Critical analysis of the received signals was carried out only for days when the flutter fading did not occur.
The variations in the received envelope amplitude for a signal propagated by the ionosphere are expected to have a Rayleigh distribution in time ${ }^{1}$. The fading signal may then be represented by the formula:-

$$
\mathrm{P}=100 \exp \left(-x^{2}\right)
$$

where $P$ is the percent probability that the signal voltage will exceed the value $x$. This expression is plotted as the curve labelled $P_{1}$ in Fig. 1. The curve labelled $P_{2}$ is a plot of the expression:-

$$
P_{2}=100\left(1-\left[1-\exp \left(-x^{2}\right)\right]^{2}\right)
$$

This is the percent probability that one of two uncorrelated Rayleigh fading signals will be greater than $x$. If a system is operating as a two-order diversity system, the amplitude distribution of the received signal envelope would be expected to approach that of curve $\mathrm{P}_{2}$.

The amplitude distributions of the received signals are plotted in Figs. 2 and 3 for all conditions of the test transmissions on November 5, 6,7 and 12 . The plotted points were obtained by sampling the strip-chart recordings at one-second


Fig. 3. Distribution of signal envelope amplitude.
intervals. It is to be noted that the received signals are very nearly Rayleigh distributed during all periods. This indicates that the depth of fades did not change appreciably for any condition of transmission.
Variation of Median Signal Levels.-The variation of received median signal levels from one transmission condition to the next is given in Fig. 4. It is noted that in most instances the level is 5 to 6 dB higher with two transmitters than with one. It is not known at the time of writing whether or not all transmitter powers and antenna systems were the samef. If they were, there is an apparent directive gain towards Boulder with two transmitters operating; otherwise a 3 dB increase in signal level would be expected.
Fading Rates.-The observed fading rates (positive median crossings) are given in the following table.

TABLE

| Average Fading Rates Obscrved on B.B.C. Transmissions at $9,510 \mathrm{kc} / \mathrm{s}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Observation period-G.M.T. | $\begin{aligned} & \text { Nov. } \\ & 5, \\ & 1958 \end{aligned}$ | $\begin{gathered} \text { Nov. } \\ 6, \\ 1958 \end{gathered}$ | Nov. 7 1958 | Nov. 12, 1958 |
|  | c's | c/s | c's | c/s |
| 0010-0015 | 0.943 | 2.11 | 1.08 | 1.66 |
| 0015-0020 | 0.806 | 1.33 | 0.98 | 1.61 |
| 0030-0035 | 0.905 | 1.19 | 1.40 | 2.08 |
| 0045-0050 | 0.714 | 1.38 | 1.26 | 1.66 |



Fig. 4. Median signal level variotions.

[^5]There is no significant difference in fading rate for any transmission condition.
Recordings.-Tape recordings of the received audio signals were reproduced for several observers. After comparative listening tests most observers indicated a preference for the transmissions when two transmitters were operating simultaneously. The difference in intelligibility and quality was not great, and it is believed the small improvement noted was due to the higher average signal level rather than to any significant difference in fading characteristics.
The rapid flutter fading observed for all transmission periods on some of the days caused a sharp
decline in intelligibility, and there was no real difference between any of the transmission conditions.
Conclusions.-There is apparently no advantage to transmitter space diversity for transmission over long distances via the ionosphere. The signals from the two transmitters combine in such a manner that the resultant field at the receiver is Rayleigh distributed; hence there is no realizable diversity gain. The fading rate was not significantly changed for any method of transmission.

## REFERENCE

1 "Ionospheric Radio Propagation," National Bureau of Standards Circular 462, p. 108, June, 1948.

## Stereophony in the Open Air

A SUCCESSFUL sound-reproducing system was installed by Telefunken at the Federal Horticultural Show held this year in Dortmund.

In view of the limited knowledge available of open-air stereophony, tests were first made on a building site in Hannover and the results obtained from these series of trials were used as the basis for the design of the Dortmund installation.
A power of 300 watts is provided for each stereophonic channel. Sound columns, which comprise a total of

1. General view of the open air stage at Dortmund. In the right foreground a technician with microphone and transistor amplifier is giving instructions for quality control and balance. 2. Plan of the Telefunken open-air stereo installation at Dortmund. 3. Pair of column loudspeakers mounted on the sides of the stage. 4. Separately mounted column loudspeaker at one end of the 100 -metre stereo base line.

48 units are used as loudspeakers. These sound columns are distributed over a base of 100 metres and permit stereophonic sound reproduction over an area with space for about

6,000 persons. The installation can be used either for sound reinforcement of the live orchestra on the stage or for reproduction of stereo records.



Wireless World. November 1959

# MISSING SIGNPOSTS 

By 'CATHODE RAY'

IT DOESN'T ALWAYS DO TO ASSUME EVERYONE KNOWS THE WAY

IAAST June, while holding a joint post-mortem with my daughter on her A-level physics and maths papers, I found myself at one with her in disapproval , though not always for the same reason. If I had had to sit the exams (which, thank goodness, I hadn't) I'd have quite often wanted to ask the tight-lipped invigilator what one was supposed to assume. To me, some of the questions were by no means unambiguously put. The actual candidate, having for months past been practising on an endless succession of similar (though, she assured me, much easier) questions, was less worried by that particular aspect. It seems the assumptions were pretty well established according to some unwritten rules of exam papers.

Being rather slow on the uptake myself, perhaps I am excessively sympathetic with students about things they are supposed to know without being told. Nevertheless I feel sure quite a lot of apparent stupidity is really the fault of the teachers.

Take vector diagrams. Fig. 1 (a) and (b), showing an a.c. circuit and its vector diagram, come from a recently published elementary textbook on electrical engineering. I want you to notice particularly the arrow-heads in both diagrams. (But not the blackingin to distinguish current from voltage, which is my own fancy.) Having looked up a number of other books, both British and American, elementary and advanced, and leaning either to power or electronic engineering, I can assure you that in this respect at least these diagrams are typical; so if the author recognizes them he will have the satisfaction of knowing he sins in bad company.

The accompanying text explains that OA represents the p.d. across $R^{\star}$, and so on, ending with OE as the voltage V across the whole lot. And we are supposed to know (but how often are beginners told?) that the arrow-heads in the vector diagram are there to show which ends are not the pivots, not which way anything is moving.

What about those on the corresponding circuit diagram? The one marked " $I$ " is presumably meant to show the direction of current flow (in the conventional sense, as a flow of positive electrical charges) which the author of the diagram has chosen to regard as positive. So if the vector diagram were to show that at any given moment the current was negative it would mean that it was flowing against the arrow-head. This device is commendable, especially if backed up by its consistent use for the other quantities involved.

How then about the arrows each side of " $V$ ". According to the system for "I", they would mean that the voltage was acting both ways at once! Perhaps (someone suggests brightly) they are to show that the voltage is alternating. Driving a d.c.? Notwithstanding the one-way current arrow, the generator symbol with its little picture of a sine wave makes

[^6]the a.c.-ness of the circuit quite clear. No; evidently the " $V$ " arrows are used in yet another sense-to indicate the points between which V exists. Then why, if the author has taken the trouble to show us which he has chosen to be the positive direction of current flow, has he left the matter completely ambiguous as regards voltage?

Why, indeed!
Not having any of the numerous authors who do this sort of thing at hand for interrogation concerning the strangeness of their habits, I must try to guess what they might say. And as I don't find any of these guesses really adequate or convincing, we must hope that some spokesman will come forward to supply the missing key (if any) which so far seems to have been withheld.


Fig. I. A typical a.c. circuit diag ram and corresponding vector dicgram. What are all the arrow-heads for?

One reason (they might say) is that as soon as a choice has been made for "I," the nature of the circuit determines the direction of the voltage, as the vector diagram shows. If, before making a vector diagram or examining the circuit, a direction were assigned to "V," it would be pre-judging the result.

Well, of course, these authors might be excused for resenting my putting such a feeble excuse into their mouths, but I'm doing my poor best for them in very difficult circumstances. If they're not satisfied I'd be delighted if they would conduct their own defence.

Reverting to the role of prosecutor, I would reply that in many circuits (including the one under discussion) a current in one direction is accompanied during each cycle by voltage of both polarities.
"Splendid! splendid!" exclaim the authors, " That's just what we meant by the two-faced direction sign for V !"

But it really won't do. The sort of thing I want the vector diagram to tell me-and which, I imagine, is what most other people expect from it, too-is which terminal of the generator is positive at some phase of the cycle; say the one depicted, at which the current is just changing over from negative to positive.

The authors-or at least the one responsible for
this particular diagram-would probably then retort that if I had read his painstaking explanation of how this vector diagram was constructed, or if I had the least clue to elementary a.c. theory, I would know perfectly well that the e.m.f. of the generator would then be acting around the circuit in the direction of the current arrow, and so the left-hand terminal would be positive.

To which I would reply that if the only purpose of the vector diagram was to show something that was already abundantly obvious (or, alternatively, if if were not obvious, something that one had to go all through the construction of the vector diagram to find out) it would be about as much good as a portable signpost which needed a knowledge of where the roads led before it could be correctly set up.
If Fig. 1(a) had been supplied with an earth symbol attached to the right-hand terminal of the generator, then one could reasonably have been expected to gather that the polarity of the vector representing V was the polarity of the left-hand and relative to the other. But it just wasn't supplied. And even if it had been there would have been uncertainty about voltages between points not earthed.

It might be that our authors in the dock would take a different line of defence. They might point out to me (slowly and clearly, as to a small child or mentally retarded pupil) that a positive voltage would be that which, when in phase with a positive current, was in the same direction. That could settle the matter if more information were available than is in fact vouchsafed by the authors in question. Consider Fig. 2, together with the information from a vector diagram or otherwise that the voltage is in phase with the current. Which wire is positive; top or bottom?

If the "voltage" we have been talking about is an e.m.f.-the e.m.f. driving the current I-and its source is in one of the boxes in Fig. 2, and if we know which box, then we know the answer. If not, we don't.

Whichever wire is positive with respect to the other, each box inevitably has a voltage between its terminals equal and opposite to the voltage in the other box in its direction around the circuit. So linking the voltage between two points with a current


Fig. 2. Which connecting wire is positive when the current is positive?
arrow gives (in absence of further information) two exactly opposite answers. Such confusion would be avoided by the simple act of omitting one of the arrow-heads associated with V in Fig. 1(a). With Fig. 1(b) as it is, the right-hand arrow-head would be the one to go. If, however, the author had not been such a clever man that he knew it all before he started, but guessing blind had happened to put his one "V" arrow on the right, it would have meant that all the voltage vectors in Fig. 1(b) would have had to point the opposite way. That might not have been conventional but it would have been quite right.

Right, that is, according to the conventions of this particular author, which are not followed by all. They could easily be a cause of confusion in circuits


Fig. 3. Alternative and more helpful version of Fig. I.


Fig. 4. Another and still more helpful version, if you know the conventions.
which, unlike this one, are not simply a single source of e.m.f. feeding current to passive circuit elements. His convention is to make each voltage vector represent the e.m.f. (coming from elsewhere) needed to drive the current through that part of the circuit. Adding them all up gives the total e.m.f. of the generator.

Personally I prefer to work according to Kirchhoff's Second Law in the form "The algebraical sum of the voltages around any closed loop is zero," because it is based on the obvious fact that the same point cannot be at two different potentials at the same time. So in Fig. 1(a) the e.m.f. of the generator would be equal and opposite to the sum of the separate voltages across $R, L$ and $C$. This version is given as Fig. 3.

But that is only a compromise. The one completely unambiguous, consistent and universal system of vector diagrams, free from d.c.-like arrows and coincident vectors (I might as well be hung for a superintendent as a constable) is my own, expounded in the July-September, 1954, issues. Fig. 4 is how the same circuit looks in that version.

In such a simple circuit it doesn't matter much which system one uses; what does matter is that when the system is applied to circuits about which the vector diagram, once constructed, tells people something they can't easily see otherwise, it leaves no room for uncertainty or error. The circuits I am thinking of particularly are those containing more than one source of e.m.f., so that one cannot assume that the current will be flowing externally from the positive to the negative terminal of any source; some other source may be driving current back through it.

A very simple example of how useless the com"on system is can be seen by comparing the triode "equivalent circuit" in the same book with the valve circuit it is supposed to represent. They both appear here as Fig. 5. We only have to ask one simple question, to which we might reasonably expect
(Continued on page 517)
a clear and unmistakable answer: When $E_{i}$ is positive, is $V_{0}$ positive or negative? Or, since the diagrams are so drawn that the statement that $\mathrm{E}_{\mathrm{i}}$ (or $\mathrm{V}_{\mathrm{o}}$ ) is positive hasn't even any meaning, let's try to be co-operative and word it this way (though we really ought not to be put to such trouble): When $E_{i}$ is such that the grid is positive with respect to the filament, which end of the load resistance is positive?

Well, this equivalent circuit diagram can't even tell us that! We have to go back to electronics and work it out for ourselves. So what use is the diagram? It does tell us the amount of voltage amplification. But not its sign. If, in the absence of any help from the author, we were to do a bit of reasonable guessing, and assume that he was following the customary convention of reckoning the lowest part of the circuit diagram as "earth," tinen positive $E_{i}$ would mean a relatively positive grid, and the end of R not earthed would (according to the diagram) be positive. Which is wrong.

When the system breaks down so lanentably with even such an extremely simple circuir as this, what hope is there with really complicated ones, having numerous branches, unearthed points, negative resistance, fecdback, mutual inductances, etc? I just wouldn't know, and that was why I was driven to invent my own system. However, at this moment I'm not asking people to accept that but just to use any system so long as they put in all the necessary signposts.

There is one difference between these electrical signposts and the geographical sort that makes them either easier or more difficult-I'm not sure which. If the local authorities of York set up a signpost in their city marked "LONDON $\rightarrow$ ", travellers couldn't be blamed for complaining if the direction so marked led straight to Edinburgh. The fact that all the other signposts in Great Britain were similarly reversed would hardly be considered satisfactory. But we have just had occasion to remark that electrical signposts can all be reversed without giving any proper ground for complaint. Considering that in a.c. circuits all the currents and voltages are continually reversing themselves, that is not surprising. The comparison does, however, emphasize the contrast between things that are necessarily so (facts) and things that can be as we choose (conventions). Quite a lot of confusion and argument result from failure to appreciate this.

Take language. "When $I$ use a word," Humpty Dumpty said, "it means just what I choose it to mean." And (if Humpty Dumpty is taken to represent the people who speak any particular language) he was perfectly right. Although the present Eng-lish-speaking people make the word "prevent" mean something quite different from what those living 300 years ago did, neither lot of people can be declared wrong, because both chose to make the word mean those things. The trouble comes when different people choose to make it mean different things at the same time without making that fact clear. "Democracy" is a notable example.

It would be extremely awkward (though perhaps a valuable discipline?) if everyone had to explain what they meant by all the words they used; and so we try by means of dictionaries and otherwise to achieve the maximum agreement, as a matter of practical convenience. We also try to achieve agreement in the use of mathematical symbols, but to make sure almest any reputable scientific book or

(a)

(b)

Fig. 5. Simple valve circuit and its "equivalent." In this form, does it really help?
paper is preceded by a list of those used and their meanings.

In all conventions it is desirable that they should be (1) accepted and used by all concerned, (2) convenient, and (3) logically based. Sometimes they are tolerated when they are inconvenient or illogical on both, because they are so widely used that great confusion would be caused trying to alter them. (As readers may have noticed, I am less impressed by this argument than some.) Sometimes, as with words such as "infer," " protagonist," and "anticipate," all three requirements are overthrown by sheer weight of ignorance, and one is never sure whether the correct-by-dictionary use of them will be properly understood.
More trouble comes when conventions and facts are confused. I mentioned some time ago the celebrated controversy about the nature of white light. Does the spectroscope develop coloured light from it, or does it pick out colours already there as ingredients? These alternatives were later seen to be two different ways of looking at the same thing, and the question of right or wrong shouldn't have arisen. In the same way one person might argue that a metal sheet reflects radio waves, preventing them from proceeding further; another might contend that the waves do go on, but are neutralized by waves reradiated both forwards and backwards by the metal. It would be a pity to come to blows over it. Or over vector diagrams. But do, please, let all necessary signposts be present and their conventions made clear.

## I.E.E. PREMIUMS

OVER half the premiums recently awarded by the I.E.E. for 1958 are for papers on radio or electronic subjects. The Institution's premier award, the Kelvin Premium ( $£ 25$ ), was given to Dr. P. N. Butcher (R.R.E.) for his paper "Theory of three-level paramagnetic masers." The Blumlein-Browne-Willans Premium (L20) is awarded to Dr. D. Gabor, Dr. P. R. Stuart and P. G. Kalman for "A new cathode-ray tube for monochrome and colour television "; and the Heaviside Premium ( $£ 15$ ) to Z. Godzinski, of Poland, for two papers on groundwave propagation.
The Electronics and Communications Section's Duddell Premium (£20) goes to Dr. A. E. Karbowiak for "Microwave aspects of waveguides for long-distance transmission "; and the Ambrose Fleming Premium ( $£ 15$ ) to G. D. Monteath for "The effect of the ground constants, and of an earth system, on the performance of a vertical medium-wave aerial."

## Manufacturers' Products

NEW ELECTRONIC EQUIPMENT AND ACCESSORIES

## Two Tweeters

IN two new Burne-Jones treble loudspeaker units fixed curved-sided cones in front of the speaker cones provide uniform distribution of the sound in a plane at right angles to cones' axis and also some loading of the sound. The magnetic flux density in the speakers is 7500 gauss, and the recommended crossover frequency $900 \mathrm{c} / \mathrm{s}$.
In the "Treble 20 " the single loudspeaker faces downwards on to two cone reflectors, the upper reflector having a central hole and being for the sound from the outer part of the loudspeaker cone, and the lower being for the sound from the voice-coil dome and inner part of the cone. When this loudspeaker unit is stood on a flat sound-reflecting surface, this surface acts to some extent as an extension of the lower cone reflector. This unit gives a uniform horizontal distribution of sound.

In the "Treble Twin" two nominally similar loudspeakers are used, thus giving a larger radiating area. Because the sound from the two speakers is combined, any differences between their responses are evened out. The two loudspeakers are connected electrically in phase and face each other; each also faces a single cone reflector as in the photograph. This arrangement gives a uniform distribution of sound in the plane at right angles to the loudspeaker and reflector cone axes (this plane is vertical and at right angles to the paper for this photo-


Burne-Jones "Treble Twin " tweeter.
graph). Moreover, the sound is beamed within a few tens of degrees ( $\pm 20^{\circ}$ at $4 \mathrm{kc} / \mathrm{s}$ ) of this plane. The bracket for mounting this loudspeaker unit on the wall is shaped so as to allow the plane in which the sound distribution is uniform to be made horizontal or vertical, thus giving a choice between uniform or beamed sound in a horizontal plane.

The Treble Twin costs £9 10s 4d, and the Treble 20 £7 (both sums include purchase tax). These units are available from Burne-Jones \& Co., Ltd., of 18 Brunswick Rd., Sutton, Surrey.

## Amateur V.H.F. Transmitter-Receiver

THE equipment illustrated is a complete 2 -metre trans-mitter-receiver designed for either mobile use in a car or as a fixed station. Designated the "Communicator Mark $2 "$ it utilizes 16 miniature valves, 11 being in a double-superhet receiver covering 143 to $147 \mathrm{Mc} / \mathrm{s}$ and 5 in a crystal-controlled transmitter, which together with loudspeaker are housed in a metal case measuring 13 in $\times$ $5 \frac{1}{2}$ in $\times 8$ in only. The transmitter output valve is a QQVO3-10A double tetrode operated at 15 watts with screen and anode modulation. Input impedance of the

R.E.E. 2-metre amateur transmitter-receiver, microphone and power unit.
receiver, and output impedance of the transmitter, is $75 \Omega$.

A press-to-talk switch on the hand microphone actuates relays in the equipment which make the necessary circuit changes for send and receive.
Power for mobile use is supplied by a 12 -volt rotary converter taking 4 A on receive and 5 A on transmit. For fixed station use an a.c. mains power unit is available.

The price is $£ 90$ including rotary converter; the a.c. mains power unit costs $£ 12$ extra. The equipment is made by R.E.E. Telecommunications, Ltd., 15A, Market Square, Crewkerne, Somerset.

## Diode Test Meter

RANGES from $50 \mu \mathrm{~A}$ to 5 A and 3 to 1200 V for a fullscale meter deflection are provided in the Thompson (Instruments) Type ED8 diode tester for simultaneous current and test voltage measurements at dissipations


Thompson diode test meter.
up to 15 W . A polarity reversal switch is provided so that both forward and reverse characteristics can be obtained without disconnecting the diode under test. This instrument costs $£ 525 \mathrm{~s}$, and is manufactured by R. E. Thompson \& Co. (Instruments) Ltd, Hersham Trading Estate, Walton-on-Thames, Surrey.

## Sub-Miniature Coaxial Connectors

A RANGE of precision-made r.f. connectors to take subminiature coaxial cables of between 0.08 in and 0.155 in outside diameter are now obtainable from the Sealectro


Sealectro "Conhex" sub-miniature coaxial connectors Types: 3000 and 3001.

Corporation. Known as the "Conhex" series they are made of brass with beryllium-copper sockets and Teflon insulation. Metal parts are gold plated and the connectors are said to be suitable for use at microwave frequeacies.

The connectors are available for cables of 50,75 or $95 \Omega$ characteristic impedance and the matching is such that over the frequency range 1 to $9.3 \mathrm{Gc} / \mathrm{s}$ the voltage-standing-wave ratio is claimed to be within 1.1 and 1.3. Insulation resistance is better than $10^{6} \mathrm{M} 52$.

The sample illustrated comprises a Type 3000 plug and Type 3001 socket and is a cable-to-cable connector measuring only $l_{16}^{7}$ in long overall and $\frac{7}{32}$ in diameter. Other types for chassis mounting are also available. When mated plug and socket parts are secured by a captive screwed collar.

Further details can be obtained from the Sealectro Corporation, Hersham Factory Estate, Lyon Road, Walton-on-Thames, Surrey.

## Measuring Oscilloscope

IN the Marconi Instruments TF1330 the d.c. Yamplifier has a frequency response 3 dB down only at $15 \mathrm{Mc} / \mathrm{s}$ and a maximum sensitivity of $50 \mathrm{mV} / \mathrm{cm}$. The time-base sweep speed is variable from $1 \mathrm{~cm} / \mathrm{sec}$ to


Marconi Instruments TFI 330 Measuring oscilloscope.
$10^{7} \mathrm{~cm} / \mathrm{sec}$ in 15 ranges and can be increased up to $5 \times 10^{7} \mathrm{~cm} / \mathrm{sec}$ using the X-expansion control. Both times and voltages can be measured to within $\pm 2 \%$. If the trace should be deflected off the screen, a pushbutton switch is provided to reduce the sensitivity in a non-linear manner so as to return the trace to a corresponding position near the edge of the screen. The trace can then be easily returned to the centre of the screen using the shift controls. This instrument costs $£ 300$ and the address of its manufacturer is Marconi Instruments Ltd, St. Albans, Hertfordshire, England.

## Transistorized Car Radio

TO the Radiomobile range of car radio receivers is now added a new series of hybrid units and a compact singleunit set, also of hybrid type.

Known as the 500T the units consist of a sensitive receiver, or control unit, giving push-button selection of five stations in the medium and long wavebands, as well as full coverage by manual tuning, and operating directly from a 12 -volt d.c. supply. This employs four valves and an a.f. driver transistor. With this unit can be used one of two alternative transistor power-output amplifiers; either the Model A, which employs a single transistor giving 2.5 watts output, or the Model B which has push-pull transistors and gives 5 watts output. As can be seen from the illustration the power transistors are, in each case, mounted externally on finned aluminium " heat sinks."
The single-unit version, Model 507, consists of a four-valve receiver with a single transistor output stage giving 1.75 watts, the whole consuming only 1.2A on a 12 -volt d.c. supply. Manual tuning only is provided but medium and long wavebands are covered, although there is a model ( 52 T ) which is for medium waveband only. Likewise, in the unit series there is a medium waveband only unit, the 502T, for use where long waves are not required.

These units and sets occupy little space, the 500 T receiver, for example, measures only 7 in $\times 7$ in $\times 2$ in while the associated amplifier ( $A$ or $B$ ) Measures $2 \frac{5}{10}$ in $\times$


Smith's Radiomobile 500T series cor receiver with alternative transistor power amplifiers alongside.
$7 \mathrm{in} \times 2 \mathrm{in}$. The overall size of the model 50 T is $7 \frac{1}{8}$ in $\times$ 7 in $\times 2$ in. Six-volt versions are also available.
Current prices are: Model 500TA (receiver with "A" amplifier) $£ 21$, plus $£ 72 \mathrm{~s} 10 \mathrm{~d}$ U.K purchase tax; 500 TB ("B" amplifier) £23 1s 6d, plus £7 16s 11d U.K. purchase tax. The makers are, S. Smith and Sons (Radiomobile), Lts., Goodwood Works, North Circular Road, London, N.W.2.

## Two Very Low Frequency Generators

OUTPUT frequencies from $100 \mathrm{c} / \mathrm{s}$ down to $10^{-4}$ or $10^{\circ} \mathrm{c} / \mathrm{s}$ can be obtained from the Servo Consultants Model 111 or 110 generators respectively. In both


## Servo Consultants very low frequency generotor.

these generators the distortion is $1 \%$ at the maximum output of 30 V and 10 mA ; the output impedance is $250 \Omega$. The main part of both generators consists of a resolver whose rate of rotation is the signal frequency, $f$ say, and whose stator is supplied with a 30V carrier signal at $2400 \mathrm{c} / \mathrm{s}$. The rotor output at a time $t$ is then proportional to $30 \sin 4800 \pi t \sin 2 \pi f t$. The signal frequency $f$ is obtained by rectifying this output using a phase-sensitive detector synchronized by the carrier signal. With this method of generation the amplitude of the output signal does not depend on its frequency but only on the carrier amplitude. This type of generator can also start and stop at any point on the waveform without introducing transients. Both these generators cost $£ 265$ and are manufactured by Servo Consultants Ltd, of 17 Woodfield Road, London, W.9.

## Combined $C$ and $R$ Decade Box

DECADES of capacitance and of resistance are not usually combined in a single box but where bench space is strictly limited the combined unit has many advantages. A decade box of this kind introduced by R. E. Thompson and Company contains three decades of capacitance and four of resistance. In the general-purpose model the increments of capacitance are in steps of $0.001 \mu \mathrm{~F}, 0.01 \mu \mathrm{~F}$ and $0.1 \mu \mathrm{~F}$, while those of resistance are in steps of $100 \Omega$ $1,000 \Omega, 10 \mathrm{k} \Omega$ and $100 \mathrm{k} \Omega$ respectively. Other combinations can be supplied by arrangement.
Normally polystyrene dielectric capacitors of $1 \%$ tolerance are fitted, but silvered-mica or other types can be substituted. All capacitors are normally 350 -volt working and resistors high-stability $\frac{1}{2} \mathrm{~W}, 1 \%$ tolerance. There is an electrostatic screen connected to the "earth" terminal on the box between capacitance and resistance decades. Separate terminals are fitted for capacitance and resistance.
The box is made of stove-enamelled sheet steel with welded seams and measures $9 \frac{1}{2}$ in $\times 6$ in $\times 5 \frac{1}{2}$ in. Price


A combined capacitance and resistance decade box made by R. E. Thompson and Co
depends on the particular combination and type of components fitted, but the general-purpose model costs $£ 18$ The makers are R. E. Thompson and Co. (Instruments), Ltd., Hersham Trading Estate, Walton-on-Thames: Surrey.

## Coil Bonding Equipment

ONE method of securing the turns of a coil wound with one of the new self-bonding wires is to pass an electric current through the coil. Sometimes it is advisable first


Avo coil bonding timer.
to check the insulation between coil and the mandrel (if metal) on which it is wound in order to ascertain what magnitude of bonding voltage is permissible.

The Avo "Bonding Timer" has been introduced to serve the dual functions of insulation measurement and time control of the bonding voltage. Insulation resistance can be measured up to $500 \mathrm{M} \Omega$ and the application of heating current set for automatic control for periods ranging from 0.75 sec to 2.5 min .

The equipment is a.c. operated and mains voltage is normally used for coil heating, but provision is made for applying, if necessary, bonding voltages of lower value from an external source.

The makers are Avo Ltd., Avocet House, 92-96, Vauxhall Bridge Road, London, S.W. 1

## Miniature Moulded Signal Lamp

THE small panel-mounting signal lamp fitting illustrated is a one-piece, thermoplastic moulding with metal inserts to take a low-voltage L.E.S.-cap bulb of the Hivac, Philips or Vitality with rating up to 1.2 W . The ribbed plastic lens is a snap-in fit and is available either clear or in colours.

The signal lamp requires a hole approximately $\frac{5}{16}$ in in


Bulgin miniature moulded panel-mounting signal lamp.
diameter and it fits panels up to $\frac{3}{16}$ in thick. It is secured in position by a simple but effective push-on grip washer. Connection to the lamp is by means of two 3 -in fly leads at the back. The body colour is normally black but alternative colours are available by arrangement with the makers, A. F. Bulgin and Co. Ltd., Bye Pass Road, Barking, Essex.

# Transistor Stopwatch 

By D. E. O'N. WADDINGTON,* Grad.Brit. I.R.E.

Measuring Time Intervals from 0.5 m sec. to 5 sec .

SINCE the development of escapement mechanisms, especially those using resonant control, mechanical methods of time measurement have been developed to a very high pitch. However, mechanical methods suffer from the disadvantage that they are slow to operate and measurement of short time intervals has passed largely into the hands of the electronic engineer. Many electronic interval timers have been designed, most of them having very high accuracy, but some are necessarily complicated and require special instruments for their adjustment. It is possible however to make a relatively simple "timer" which is not too difficult to set up.

There are two main "electronic" methods of measuring time interval. The first method approximates to the clepsydra, or water clock, in that a capacitor is charged through a resistor during the time interval to be measured, and then the resultant voltage across the capacitor is a function of the time. This method, although ideal for simple valve-operated timers is impracticable with transistors as the required high reverse impedances cannot easily be realised. The second method consists of counting the number of pulses of known repetition rate during the period to be measured and displaying this number either by means of a digital presentation or on a meter.


Fig. 1. Block diagram of transistor stopwatch.

The second method lends itself very well to transistor circuitry and it is used in the "Transistor Stopwatch." Owing to the complexity of a digital presentation a meter is used to indicate the time interval and it was found necessary to use two battery-operated valves to do this.

The transistor stopwatch is the electrical analogue of the mechanical stopwatch in that it counts the number of impulses of known frequency between the start and stop signals. However, it has an advantage over its mechanical counterpart as the " inertia " of the system is very low and a higher pulse repetition rate may be used. This factor allows measurement of very small time intervals with good accuracy. In the mechanical stopwatch there is only one pulse repetition rate available; but in an electronic device it is possible to vary this rate almost at will, so making it possible to use one meter scale for all ranges by switching the frequency of the pulse source.

The instrument may be sub-divided into six separate circuits and this breakdown is shown in block form in Fig. 1.

[^7]Oscillator and Switch Circuits.-The pulse source is a free-running multivibrator (V3 and V4, Fig. 2). As the shortest time to be measured determines the highest frequency to be used, the type of transistor used limits the accuracy of the instrument. However, by using a count of 200 cycles for fullscale deflection of the meter on any time range, the uncertainty error is reduced to $\pm 0.5 \%$ and a top frequency of $20 \mathrm{kc} / \mathrm{s}$ permits a full scale reading of 10 msec on the shortest time scale. The uncertainty error is due to counting a free-running frequency source instead of one which starts with the timing pulse. Hence it is possible to count one too many or too few cycles. There is little difficulty in making a $20-\mathrm{kc} / \mathrm{s}$ oscillator with commercial "audio" transistors although the waveform tends to deteriorate. As this is compensated for later in the circuit it has no deleterious effect on the operation of the stopwatch. The required frequency for any tim? scale is given by:-

$$
f=n / t
$$

where $n$ is the number of pulses for f.s.d. and $t$ is the time interval to be registered as f.s.d. In this instrument 200 pulses correspond to f.s.d. and the frequencies equivalent to the chosen time scales are given in Table I.

Table I

| Time Scale |  |  |  | Frequency |
| :---: | :---: | :---: | :---: | :---: |
| 5 sec |  | . |  | 40 cs |
| 1 sec |  |  |  | 200 cs |
| 500 msec |  |  |  | 400 cs |
| 100 msec |  |  |  | 2,000 c/s |
| 50 msec |  |  |  | $4,000 \mathrm{c} / \mathrm{s}$ |
| 10 msec |  | . | . | $20,000 \mathrm{c.s}$ |

The different frequencies are obtained by switching the base-collector capacitors $C_{1}$ and $C_{7}$ together to keep the mark-to-space ratio and the output amplitude constant. As the frequency stability of this circuit controls the accuracy of the instrument its supply should be kept constant and this is done by a Zener-diode voltage stabiliser (D3, on Fig. 2). The other cause of frequency variation is due to a change of base current with a change in temperature and this is reduced to a minimum by using a relatively-low-value base resistor. These measures limit the frequency variation to about $\pm 2 \%$.

Usually only impulses are available from the external control circuit so some form of bi-stable circuit must be used for switching the timer on and off. This is done very simply by using a transistorised version of the Eccles-Jordan flip-flop circuit (V1 and V2, Fig. 2). A positive-going pulse of one volt will trigger the circuit quite effectively--shorting
the run or stop inputs to earth has the same effectso that either electrical or mechanical switches may be used.

A single transistor can be made to act as a very effective gate (V5, Fig 2). When the base is biased towards the positive line the emitter-to-collector resistance is high and when it is biased sufficiently negative it acts almost as a short circuit. Thus by interposing this gate between the output of the multivibrator and the input to the amplifier, it is possible to switch the signal on and off quite simply.

The limiting amplifier (V6 and V7, Fig. 2) is a conventional two-stage direct-coupled amplifier. As the output waveform should be square with a constant peak-to-peak amplitude sufficient input is applied to the first stage so that it switches the second stage on and off. Thus the output is switched from the earth line to the $4.7-\mathrm{V}$ negative line which is stabilised by means of the Zener diode. As a rapid response is important r.f. transistors are used.
Display Circuits. - The diode-pump integrator is used widely in frequency discriminators and pulserate meters. Here it is used as a pulse counter. In this application special precautions must be taken to ensure that the reverse resistance of the shunt diode is very high, of the order of thousands of megohms. It is difficult to find even silicon diodes which reach this requirement, so a vacuum diode had to be used; but here again difficulty was experienced as there is no suitable battery-operated vacuum diode readily available. Furthermore most vacuum diodes suffer from "splash" current which could easily cause erroneous readings. However, the writer has found that splash current can be reduced appreciably by running the filament of a battery pentode at half the specified filament voltage and connecting the control and screen grids to the negative side of the filament. This strapping does not impair the diode ection of the valve in its application in the pulse-
counter. The capacitor which is charged from the diode pump must be a high-quality low-leakage type as any path liable to discharge it must be eliminated where possible. In this circuit the total parallel resistance is approximately $500 \mathrm{M} \Omega$.

An electrometer valve would have been ideal for the valve-voltmeter as it has an extremely-high input resistance, however, electrometer valves are expensive so a conventional output pentode (V6) is used in a slightly unconventional circuit. As in the diode pump, the filament is run at half its normal supply voltage from a battery which is isolated from all other supplies. This allows the centre tap of the filament to be used as a neutral point from which the bias resistor is connected to earth. To set the zero, the meter is connected between the anode and a resistive chain and the sensitivity is adjusted by means of a variable resistor connected in parallel with the meter.
Photoelectric Trigger Circuit.-Although this is not essential for the operation of the stop watch it is a very-useful accessory, particularly when it comes to calibration. Normally a photoelectric cell does not produce a pulse of sufficient amplitude to operate the timer when the amount of light falling on it is changed so it was incorporated in a Schmitt trigger circuit. Under operating conditions the light falling on the OCP71 photo-transistor (connected as a photodiode) causes a current to flow through it with the result that the base of V10 is biased towards the negative line, so switching it on and hence switching off V11. When the light intensity is reduced, the current through the phototransistor is reduced; consequently the bias on the base of V10 will be reduced, switching it off and switching V11 on. This causes the voltage on the collector of V11 to move towards the positive line, thus giving the requisite pulse to trigger the stop watch. As the device will almost certainly be used in varying degrees of illumination a sensitivity



Fig. 3. Photoelectric trigger unit circuit. Note that OCP7I phototransistor is used as photodiode, i.e. base connection is left "floating."
control is included: this allows the sensitivity of the photo-cell circuit to be set so that a small reduction in illumination will operate the trigger.
Notes on Construction.-With the exception of the diode-pump and valve-voltmeter circuits there is nothing critical in the construction of the instrument. The transistor circuits may all be wired on tagboards. The best grouping consists of wiring the electronic-switch section on one tagboard, the pulse source, gate and limiting amplifier on another and the photoelectric trigger on a third.:
It was found necessary to use either porcelain or p.t.f.e. valve holders for the pentodes and the $1-\mu \mathrm{F}$ integrating capacitor was mounted on porcelain standoff insulators to reduce leakage. A locking device was fitted to the "meter-sensitivity" control to prevent accidental "readjustment" as this would lead to erroneous readings which would not be immediately obvious. The lead from the grid of the voltmeter pentode to the "reset" switch was screened and kept away from the oscillator circuit. A high-grade lead and switch were used to reduce leakage.
Calibration.-The first operation carried out was to check the frequency of the multivibrator. For this an oscilloscope and a calibrated a.f. oscillator were used with the output of the multivibrator connected to the Y amplifier of the oscilloscope and the a.f.-generator output to the $X$ amplifier. The frequency of the oscillator was then adjusted until a stationary square trace appeared on the screen. The frequency of the multivibrator was adjusted by selecting the condensers $\mathrm{C}_{1}$ and $\mathrm{C}_{7}$ (larger capacities reduce the frequency and smaller ones increase it). It is not essential that the frequencies should be exact provided that the ratio between them is correct and Table II gives the relation of frequencies for various errors, including a lowest frequency of $50 \mathrm{c} / \mathrm{s}$ (for calibration from the mains supply).

TABLE II

| Correct | 2.5\% low | 2.5\% high | $\mathbf{1 0 \%}$ high |
| :---: | :---: | :---: | :---: |
| 40 | 39 | 41 | 50 |
| 200 | 195 | 205 | 250 |
| 400 | 390 | 410 | 500 |
| 2,000 | 1,950 | 2,050 | 2,500 |
| 4,000 | 3,900 | 4,100 | 5,000 |
| 20,000 | 19,500 | 20,500 | 25,000 |

The standard time signals from Ruguy, WWV or ZUO could be used for setting up the time scale; but this would involve the use of more complicated circuitry than is contained in the stopwatch. A pendulum was adopted as being the easiest and most practical method.
To minimise the errors, the longest time scale was used, i.e. 5 secs. It is, unfortunately, impractical to obtain f.s.d. directly as the pendulum required for a 5 -second half cycle is about 81 -ft long! However, a pendulum having a period of 2 sec . is quite practical. The required length is given by the formula:-

$$
t=2 \pi \sqrt{ }(l / g)
$$

where $t$ is the period, $l$ the length and $g$ the acceleration due to gravity.
Thus a $2-\mathrm{sec}$ pendulum would be 99.45 cms . or 39.16 in. from the support to the centre of gravity of the bob. A pendulum was made by tying a $1-\mathrm{lb}$. weight to one end of suitable length of light thread and securing the other end to a rigid support. A light source and the photoelectric trigger were then arranged so that the pendulum hung between them. The time-scale calibration arrangement is shown in Fig. 4.


Fig. 4. Arrangement of apporatus for setting up time scale. Pendulum interrupts light beam when in the position occupied when at rest.

The setting up procedure used was as follows:-

1. Switch the stopwatch on and press the reset switch to discharge the condenser.
2. Set the zero of the meter and switch to the $5-\mathrm{sec}$. range.
3. Move the bob of the pendulum about 4in. from the rest position and release it. It will swing through the light beam, triggering the timer.
4. After the pendulum has completed $2 \AA$ cycles operate the changeover switch so that the, output of the trigger is connected to the "stop" input.
5. At $2 \frac{1}{2}$ cycles (i.e. 5 sec .) the timer will be stopped. Then adjust the sensitivity control so that the meter indicates full-scale deflection.
6. Repeat the above procedure as a check.

As a further check switch to the 1 -sec range and time one-half cycle of the pendulum. If the meter does not indicate full scale correctly, the oscillator frequencies should be re-checked.
The meter scale is very nearly linear (within 3\%) but if the refinement of an exactly-calibrated scale is required the calibration points may be calculated from the formula:-
$\mathrm{V}=\mathrm{E}\left\{1-\left[\mathrm{C}_{2} /\left(\mathrm{C}_{1}+\mathrm{C}_{2}\right)\right]^{n_{\}}}\right.$
where V is the voltage measured by the valve voltmeter, $E$ is the supply voltage, i.e. 4.7 V, $\mathrm{C}_{1}$ is the series condenser, i.e. $\mathrm{C}_{13}$ in Fig. 2, $\mathrm{C}_{2}$ is the shunt condenser, i.e. $\mathrm{C}_{14}$ in Fig. 2, and $n$ is the number of charging pulses.
The instrument was originally designed to measure the speed of arrows shot from a bow. The start
pulse was obtained by the feather cutting a beam of light, thus operating the photo electric trigger and the stop pulse was obtained from a microswitch on the target which shorted the "stop" input to earth. This, however, is not the only use for the instrument as it can be used to measure the speeds of camera shutters (using two photo electric
triggers), the speed of relay operation, etc. In fact, the limit is usually set by the detecting arrangements; but as the run and stop inputs are at low impedance, it is possible to use long lengths of cable to operate them with no fear that the capacity will damp the pulses. Leads up to 100 yds. long have been used.

## "MONO" TAKES A TOSS

AT the Colston Hall, Bristol on October 9th Mr. G. A. Briggs introduced his 17 th concert of live and recorded music. In addition to his own evident enjoyment of any experiment in sound Mr. Briggs found three additional pretexts for this occasion: (1) to satisfy many requests from sound reproduction enthusiasts living in the West Country; (2) to offer for judgment for the first time by a public audience a comparison between live performances and mono and stereo reproductions of the same works; (3) to make amends to Harold Blackburn for the admittedly unsuccessful reproduction of his fine bass voice at the Festival Hall concert last May.

Special tape recordings were made at the Abbey Road Studios of E.M.I., using the best available microphone techniques for both single-channel and stereo, of excerpts from piano trios by Dvorak and Mendelssohn played by Gerald Gover (piano), Kenneth Popperwell (violin) and Terence Weil (cello), and also solos by Harold Blackburn. Wireless World was privileged to hear playbacks of these recordings both at E.M.I. Studios and in the Colston Hall, with the live performances for reference in both cases. In the small monitoring rooms at Abbey Road there seemed little to choose between mono and stereo, and opinions among those present were equally divided. In the Colston Hall, on the other hand, there could be no doubt of the superiority of stereo reproduc-
tion, and this was conclusively supported by a show of hands in the mixed audience. Although neither system could quite compete with the rich quality of Harold Blackburn's voice we had thought earlier that, in the monitoring studio, single-channel came nearest, but this decision was reversed at Bristol where stereo gave a much more natural rendering. Yet the conditions at Bristol, with large omnidirectional speakers, spaced widely apart in the large hall, would be considered by most people to be much less favourable than those of the monitoring studio with only three or four seats placed in the optimum position relative to the loudspeakers.

Although perhaps of less scientific interest than Mr . Briggs' own objective and carefully prepared experiments, a comparison of mono and stereo recordings (Archive) of the Geraint Jones choir singing a Handel chorus was illuminating. The mono recording, which was played first, was completely satisfying from a musical point of view, but the stereo recording which followed put a fire and vitality into the sound quality which was then quite evidently missing from the singlechannel record.

Mr. Briggs is once again to be congratulated on a very successful and enjoyable concert, and for his unsparing efforts to find the best in sound reproduction-this time, as it happened, in two-channel stereo.

## JERSEY AIR TRAFFIC CONTROL

TO meet the requirements of air traffic control at the busy airport at Jersey in the Channel Islands, a Marconi S264 radar system has been installed and was, on 26th

June, 1959, inaugurated by H.R.H. Princess Margaret. In addition to very heavy holiday traffic for which a new air lane (Blue One) is proposed between London and Jersey, there is responsibility at Jersey for overflying aircraft on route Blue 32 (Paris to Shannon) and also for supervision of the Channel Islands control zone.

The $S 264$ radar is 50 kW installation with provision for conversion to 500 kW if necessary. It operates on 50 cm (for rain penetration) with a large aerial system of wide vertical aperture, giving coverage up to $40,000 \mathrm{ft}$ at distances of up to 100 miles on medium-sized aircraft.

Marconi S264 long-range and terminal area surveillonce radar system ot jersey Airport.

## NOVEMBER MEETINGS

Tickets are required for some meetings; readers are advised therefore to communicate with the secretary of the society concerned.

## LONDON

11th.
Brit.I.R.E. - " Physiological and acoustical aspects of hearing" by Dr. R. P. Gannon at 6.30 at the London School of Hygiene and Tropical Medicine, Keppel Street, W.C. 1.
lith. Physical Society Colour Group.--Discussion on the recent work of Dr. Edwin Land on colour projection at 3.30 at Institute of Ophthalmology, Judd Street, W.C.1.

12th. Physical Society Acoustics Group.-" The propagation of Rayleigh waves" by G. Mott at 4.0 at Imperial College, Prince Consort Road, S.W.7.

18th. Brit.I.R.E.-Half-day symposiunn on "Electronic digitizing techniques" at 3.0 and 6.0 at the London School of Hygiene and Tropical Medicine, Keppel Street, W.C.1.
20th. Institute of Navigation." Radiometry, radio-astronomy and infra-red techniques" by C. M. Cade at 5.15 at The Royal Geographical Society, 1 Kensington Gore, S.W.7.

20th. I.E.E. Graduate and Student Section.-" Plastic, cables in the telecommunications industry" by G. J. Waddon at 6.30 at Savoy Place, W.C. 2.

20th. Television Society.-" Television film production" by J. K. Byers (B.B.C.) at 7.0 at the Cinematograph Exhibitors' Assoc'ation, 164 Shaftesbury Avenue, W'.C.2.

20th. B.S.R.A.-"Loudspeakers" by S. Kelly at 7.15 at the Royal Society of Arts, John Adam Street, W.C.2.

23rd. Radar \& Electronics Association Student Section.-"Marine and air radar simulators" by P. Tenger (Solartron) at 7.0 at the Norwood Technical College, Knight's Hill, S.E.27.

24th. Radar \& Electronics Associa-tion.-"Waveguides for long-distance communications" by Professor H. E. M. Barlow at 7.30 at the Royal Society of Arts, John Adam Street, W.C.2.
25 th. I.E.E.-" Radio aspects of the International Geophysical Year" by Dr. R. L. Smith-Rose at 5.30 at Savoy Place, W.C. 2 .

30th. Royal Institution.-" Faraday, through his manuscripts" by Dr. L. Pearce Williams at 5.30 in the Long Library, 21 Albemarle Strect, W.1.

## ABERDEEN

13th. I.E.E.-" The application of transistors to line communication equipment" by H. T. Prior, D. J. R. Chapman and A. A. M. Whitehead at 7.30 at Robert Gordon's Technical College. BIRMINGHAM

13th. Society of Instrument Tech-nology.-"Ultrasonic inspection techniques" by W. B. Emms at 7.0 in the Lecture Theatre of the Byng Kendrick Suite, Gosta Green College of Technology, Aston Street.

23 rd. I.E.E.-" Learning machines" by P. Huggins at 6.0 at the James Watt Institute.

## BRISTOL

18th. Brit.I.R.E.-" Data recording and presentation" by D. W. Thomasson at 7.0 at the School of Management Studies, Unity Street.

## CHELTENHAM

27th. Brit.I.R.E.-" A vidicon television camera channel " by B. J. Pover at 7.0 at North Gloucestershire Technical College.

## DUNDEE

12th. I.E.E.-" The application of ransistors to line communication equip-
ment" by H. T. Prior, D. J. R. Chapman and A. A. M. Whitehead at 7.0 in the Electrical Engineering Department, Queen's College.

## EDINBURGH

9th. Institute of Physics.-"Light waves, radio waves and photons" by R. M. Sillito at 7.15 at the University.

12th. Brit.I.R.E.-"The transistor and its use in communication and control equipment" by $E$. Wolfendale at 7.0 at the Department of Natural Philosophy, The University.

## GLASGOW

10th. Institute of Physics.--" Light waves, radio waves and photons" by R. M. Sillito at 7.15 at the University.
llth. Brit.I.R.E.-" The transistor and its use in communication and control equipment"" by E. Wolfendale at 7.0 at the Institution of Engineers and Shipbuilders, 39 Elmbank Crescent.

25th. I.E.E.-Faraday lecture on "Electrical machines" by Professor M. G. Say at 6.0 at St. Andrew's Hall.

## halifax

16th. Institution of Production Engin-eers.-" Electronic copying on machine tools" by R. Lawson at 7.30 at Percival Whitley College, Francis Street.

## LIVERPOOL

10th. Brit.I.R.E.-" The use of transistors in commun:cations and control" by E. Wolfendale at 7.0 at the University Club.
llth. I.E.E.-" Vision and position -two electronic aids to marine navigation" by Dr. R. B. Mitchell and C. Powell at 6.0 at The Temple, Dale Street.

## MANCHESTER

12th. Brit.I.R.E.--" Progress in permanent magnet materials" by J. E. Gould at 6.30 at the Reynolds Hall, College of Technology, Sackville Street.

## MIDDLESBROUGH

12th. Society of Instrument 'Tech-nology.-"Analogue computers" by R. E. Hare at 7.30 at the Cleveland Scientific \& Technical Institute, Corporation Road.

## NEWCASTLE

llth. Brit.I.R.E.-" Electronic welding controls" by C. R. Bates at 6.0 at the Institution of Mining and Mechanical Engineers, Westgate Road.

18th. Society of Instrument Tech-nology.-"The principles and manufacture of junction transistors" by P. I. Nicholson at 7.0 at The Conference Room, Roadway House, Oxford Street.

## NEWPORT

25th. Society of Instrument Tech-nology.--"Transistors" by S. S. Goldberg at 6.45 at the Newport \& Monmouthshire College of Technology.

## READING

23rd. I.E.E.-" An introduction to electronic computers" by R. C. M. Barnes at 7.15 at the George Hotel, King Street.

## SALISBURY

11th. I.E.E.-" The planning and installation of a television transmitting station" by D. B. Weigall at 6.30 at S.E.B. Showrooms, 17 New Canal.

## WOLVERHAMPTON

11th. Brit.I.R.E.-" Recent developments in semiconductor rectifiers" by J. Bulman at 7.15 at the College of Technology, Wulfruna Street.

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## 

THE Editor, wearied of etymological alarums and excursions, and wishing to terminate them, has asked me to bring them to a close by commenting on the following notes he has received condemning my remarks in the correspondence columns of the July/August issue. Mr. Mark Thornton writes:
"Free Grid's exegesis on the word $\phi \omega \nu \dot{\prime}$ may s sem very erudite, but on closer inspection it fails to convince in almost every detail. I will go through the more controversial things he says point by point. (a) povn' cannot, as every Greek scholar knows, be derived from a verb with an a stem like $\phi \alpha^{\prime} \omega$, for the a and the $o$ would contract into $\omega$ (as they do in $4 \omega \nu \dot{\eta}$ ) not into $o$. The word is in fact derived from a verb $\phi \cdot \hat{\varepsilon} \nu \omega$ (never in fact found in the present tense) which is a by-form of ptiva, meaning both 'to slay' and 'to beat.' (All this is to be found in Liddell and Scott's Greek LexiconNinth (latest) edition.)
(b) $\phi \omega \nu \dot{\prime}$ is derived from $\phi \eta u^{\prime}$ (I speak), which is related to pod. ${ }^{\phi}$. Thus it will be seen that фo $\dot{n}$ and $\phi \omega \nu \dot{n}$ are in no way connected.
(c) фovn may be transliterated 'phone ' by ' Free Grid,' but it does not occur as such in any English word. The 'phone' in English is ゅ $\omega \nu \eta$.
(d) There is not a hint in the whole of classical Greek literature that $\phi$ o 1 n has anything to do with mouths; the only evidence that 'Free Grid' can adduce in support of his theory is an exceedingly unconvincing passage from Exodus. I admit that the Authorised Version translates this verse ' on the edge of the sword,' but this is erroneous for two reasons. First, ' $\epsilon\rangle$ '. means 'in' not 'on'; secondly, in no other passage does фovi' mean 'edge.' No Greek scholar worth his salt would hesitate to translate this phrase 'in a slaughter wrought by the sword.' Clearly,


Readers' etymological excursions.
'Free Grid's' translation of goyin as the 'mouth of the sword' is nothing more than a red herring. (e) Similarly, classical Greek never used कwyr' in the phrase 'voice of the sword.' The nearest to it is Homer's 'battle-cry (p, $\omega \nu n$ ) of the Trojans and Achaeans.' Homer, as in that phrase, always used $\phi$ whn of people. Considering that he is the earliest extant Greek author, we may take it that 'voice' is the original meaning of $\phi \omega \nu \eta$. Indeed, Liddell and Scott only quote one example of an inanimate use of $\phi$ wh,' in the whole of classical Greek prose-Plato talks of the ' voices of musical instruments,' just as we do.
(f) This being so, 'Free Grid's' remarks about battles are rather pointless; and anyway in a battle surely the battle cries (animate) come before the clash of arms, not the clash of arms first as 'Free Grid ' suggests. In a word, 'Free Grid's' case rests on nothing more than a mistranslation of $\phi$ oun and a distortion of the meaning of $\phi$ wiv. There is therefore no need for anyone except 'Free Grid' to think of a monophonic gramophone as a 'one sound reproducer.' No doubt 'Free Grid' is still opposed to the word because it ' does not call to mind . . . the rich polyphonic sounds of music and well modulated voices '-but after all is it meant to? Monophonic does refer to the gramophone and not to the music. The polyphony of the music is important but in this case irrelevant."
Naturally I feel a little flattered at being condemned in such illustrious company as the translators of the Authorised Version whose interpretation of Exodus XVII, 13, the Editor's correspondent says is erroneous, and my quotation of it unconvincing.

He tries to " rub it in good and proper" when he says that no Greek scholar worthy of his salt would hesitate to translate this passage in the manner he suggests. But he rather overreaches himself for, of necessity, he condemns not only the translators of the A.V. of 1611 but also the equally learned men who endorsed the A.V. translation of this passage when they gave us the Revised Version in 1881, to say nothing of later translators such as the late Monsignor Ronald Knox, a scholar of no mean reputation who, as recently as ten years ago gave us his own independent interpretation in which he suggested only one trivial alteration-the substitution of "point" (of the sword) for "edge."
But the editor's correspondent stands self-condemned in the two reasons he gives for castigating the A.V. translators, and also myself for quoting them. He gives as his first
"reason the alleged fact that iv means "in" and not "on." Unfortunately his own champions Liddell and Scott, for whom I have the greatest respect, let him down for they tell us that $\epsilon^{\prime} \nu$ means " in," " on," "with" and several other things according to the context in which it is used.

This correspondent's second reason is that in no other passage does фovn' mean " edge"; but once more Liddell and Scott fail him as they give three other passages, namely, Numbers XXI, 24; Deuteronomy XIII, 15; and Deuteronomy XX, 13; but, of course, it must be admitted that these passages are all the work of the same "erroneous" translators.


Back to the very origins of Greek.
As for $\ddagger 0 \nu \eta^{\prime}$ having no connection with $\phi a \dot{\omega}$ (and, therefore, with $\phi \omega \psi \eta)$, Parkhurst, a learned Cambridge scholar of the 18 th century, thought otherwise although he did not, of course, deny that its next of kin was $\phi_{\epsilon} \nu \omega$ just as $\phi_{\eta \mu i}$ is the next of kin of $\phi \omega \nu \grave{\eta}^{\prime}$. Parkhurst takes us right back to the old Cadmean alphabet and the very origins of Greek in the second millennium s.c. in which the unhellenistic letters $\omega$ and $\eta$ did not exist, which, incidentally, Plato mentions in his Cratylus.

Some centuries later came Homer (circa 900 B.c.) by which time the new letters, and the new word spellings they brought with them, had thoroughly settled down, complete with all the etymological rules with which the Editor's correspondent is obviously so very familiar.

Finally, this correspondent appears to have read his Wireless World as carelessly as he has his Liddell and Scott, otherwise he would know that I never said anything about the "rich polyphonic sounds of music and well-modulated voices" as he obviously implies. We must, I think, agree to differ like the learned mental specialists in a recent cause célebre in the Courts.

The Editor has also passed to me a very interesting letter from Dr. Leslie Knopp who writes:
"Free Grid's reply to Mr. Pawley's letter is both misleading and inaccurate, although Mr. Pawley's statement is not strictly correct.
"The primary meaning of $\phi$ wyn' was the sound of the voice (principally of men) subsequently it was used to mean any articulate sound, and by some careless writers, to mean any sound or tone. $\phi \omega \nu{ }^{\prime}$ should be used only for articulate sound as opposed to $\psi\langle\phi 0 \leqslant$ for inarticulate sound and, Mr. Editor, you can kindly inform Master Free Grid that the Greek texts of LXX are very corrupt-but a literal translation of Theodotion's version of Ex. XVII, 13 would be:
"Whereafter the chosen [men of] - Joshua made uncomfortable Amalech [and his] people with the slaughter swords [which have very sharp edges] or $\phi \omega \nu \dot{y} \boldsymbol{\sigma} v \rho \boldsymbol{\gamma} \gamma \gamma \omega \mathrm{~F}$ for sound from inanimate objects.
"Free Grid had better get off his war-horse! Although Xenophon used $\phi \omega \nu n^{\prime}$ to mean the cry of men in battle, фúxomis is more correct for din of battle or $\phi$ Noórßos for confused noise.
" $\phi$ ovi' means slaughter or murder (always in the plural) and comes from the verb фové $\omega$ which has nothing whatever to do with the anatomy."

Dr. Knopp makes criticisms similar to some, but not all, of those put forward by Mr. Thornton but he condemns also those people responsible for certain corrupt texts of the Septuagint, and in this I have a sneaking sympathy with him. Since this contentious Greek text of Exodus XVII, 13 has proved such a stumbling block, I have reproduced it at the head of these notes in Hebrew, the tongue in which it was originally written. This should make everything clear to everybody. [If not, will they kindly join with me in calling it a day! -ED.]

## Cacophonous Caterwauling

WHY is it that nothing seems to be done about the irritating whistles from neighbouring television sets which plague listeners to programmes on the medium-wave band of " blind" broadcasting? Every reader of Wireless World knows its cause and the technical problems surrounding its absolute removal; but why don't we who have passed the "eleven plus" and therefore prefer the civilized musical programmes of blind broadcasting to the prdomoous puerilities of so many television programmes raise such a clamour that the P.M.G. is forced to co something about it under the powers which he undoubtedly has? Don't tell me that the obvious answer is to listen on the v.h.f. band; there are some of us who prefer our music from the continent.

## DEPENDENT ON SIGNALS



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# RANIDOM RADIAMIONS 

## By "DIALLIST"

## Service Without Tears

ABOUT this time last year, if I remember aright, I praised the steps that some radio and television manufacturers had taken to make things easier for the serviceman when he's engaged in trouble-tracking. I'm glad to see that the good work goes on this year. There are sets which can be removed easily from their cabinets, hinged panels and many other aids to getting quickly at their innards. But I still don't like to see four-contact components, such as transformers, soldered into sockets in printed circuits. As one dealer put it, to get them out you really need a soldering iron with four adjustable bits! There's always the risk, too, that when they're being removed or replaced the printed wiring may be accidentally damaged. However, there are some components on the market which overcome the disconnection problem by using spring-loaded contacts. One of the latest examples is a potentiometer with spring-loaded contacts on the printed-circuit chassis of R.G.D. and Regentone sets. The interesting point is that the potentiometer is mounted so that the contacts are applied to the edge of the printed circuit board, not to its face. Actually, they fit into little indentations cut along the edge of the board. When the solder in each indentation is melted the contact springs away from the printed circuit.

## TV Totals

OFFICIAL figures for the increase of television receivers in Europe since 1954 make interesting reading. The latest figures are naturally a little stale, for it takes some time to collect and publish the information. Our own G.P.O.'s licence figures, for example, are generally a good few weeks behindhand. However, at the end of 1954 there were 3,239,000 TV sets in Europe this side of the Iron Curtain and the latest figure is $14,291,000-$ an amazing advance in about four and a half years. Our own country has always been at the head of the list, with Western Germany, whose sets increased from 1,211,935 to $2,125,130$ during 1958, next, but a long way behind. Third comes Italy with 1,098,899, and fourth France, where
receivers numbered 988,594 when the list was drawn up, and are now probably well above the million mark. At first sight it's rather surprising that there should be only 50,304 sets in a prosperous country like Switzerland; but there must be large tracts of mountainous country where reception is still impossible unless the Italian scheme of a fly-power satellite station for almost every valley is adopted.

## Not Too Loud

IN 1952 the Society of Music Enthusiasts (of which P. G. A. H. Voigt was at one time chairman) was founded in Toronto. Until recently it was a flourishing concern; now lack of support has forced it to close down, which is a pity. It's rather surprising, too, considering what a vogue there is for hi-fi. Talking of hi-fi-which to some people too often means excessive volume-calls to mind some verses by Christine Britton issued some time ago by the Society of Music Enthusiasts. Her "Neighbour's Lament" is very much to the point.

> Nowadays, it's smart to be
> Hep to high fidelity;
> Run and buy them, do not falter-
> Naked chassis, plywood altar!
> Learn the jargon; rant and rave About the baffles that you crave,
> Speak of speakers reverently
> Own a minimum of three.
> Twist the knobs eternally
> Speaking sonic symmetry
> Accept the plaudits of the town-
> But for S.M.E.'s sake TURN IT DOWN!

## It's Skill You Pay For

"THE dealer replaced a component costing 1 s 3 d and charged me 10 s 6 d for the job." One often hears that sort of grouse from people who don't believe that the serviceman has to be paid for all the time he's away from his workshop, if he comes to your house, that he has to have some pretty expensive testing and measuring instruments available and that above all a fault in a sound or television set may take a long time to track down. There's too much competition nowadays for dealers to be tempted to make excessive charges. There may be odd ones here and there who do, but they don't as a rule stay long in the game, for a bad reputation is soon built up and that's
their undoing. What people are apt to forget is that they're paying a good man for his skili.

## Bogus Degrees

ANYONE who looks at the advertisement pages of some American papers and magazines can't help being struck by the number of concerns which offer to help those who enrol with them to get degrees or qualifications in a vast variety of subjects. The American Council on Education has recently made an exhaustive survey and reports that whilst there are many reputable organizations there are swarms of dishonest concerns which, they reckon, are cheating students in other countries to the tune of $£ 25 \mathrm{M}$ a year-and getting away with it. Such students, officially estimated at 750,000 every year, are induced to "pay good money for a completely "phoney" degree, not worth the price of the paper on which the diploma is engraved. I don't imagine that many of the victims who become alleged Masters of Electronic Technology, or Doctors of this, that or the other come from this country, for they'd find it very hard to get their spurious qualifications accepted by prospective employers here. Still, one never knows.

## Bankers and Electronics

THE Big Banks are becoming very electronics minded these days. Closed-circuit television enables the manager to have your account put before his eyes when you go to his office in the hope of increasing your overdraft. And recently one of the Big Five has placed an order for a transistor Emidec computer. It is to be installed at a central point in London and will deal with the 40,000 accounts of 15 branches. Each branch will send in its facts and figures via the teleprinter and the answers will be returned to it in the same way. The cost is pretty big- $£ 125,000$ for the computer alone and additions and gadgets may bring it up to nearly double that figure. But it will save a lot of time $\Rightarrow$ and time, we're told is money. Electronic devices have a great deal to offer to big businesses and it's good to see that this is becoming more and more widely appreciated.



# The most advanced 

## voltage reference tube in the world...

## the NEW

## Mullard 83A1

For technical details of the 83A1 fill in and post this coupon


aII angles . . this is a fine loudspeaker


DU120 DUPLEX CoAXIAL FULL RANGE LOUDSPEAKER
Price £19. 10s. Od.
Vitavox. Limited - Westmoreland Road, London, N.W. 9 - Telephone: COLindale 8671

# Transistorized <br> UNIVERSAL <br> COUNTER 

TIMER

## Frequency Measurement

## Random Counting

## Frequency Division

## Time Measurement

Frequency Standard

C INTEL


This fully transistorized portable equipment provides for a wide range of time and frequency measurement as well as facilities for counting, frequency division and the provision of standard frequencies. The facilities available are briefly listed below:

TIME/UNIT EVENT (1 LINE) : For the measurement of the time interval between two occurrences in a continuously varying electrical function in the range $3 \mu \mathrm{sec}$ to 1 sec . The time for 1,10 or 100 such events can be measured.

TIME/UNIT EVENT (2 LINE): For time measurement in range $1 \mu \mathrm{sec}$ to 2777 hrs . of any interval defined by a positive or negative going pulse in any combination.

EVENTS/UNIT TIME: For frequency measurement in range $30 \mathrm{c} / \mathrm{s}$ to $1 \mathrm{Mc} / \mathrm{s}$ over period of $0.001,0.01$, $0 \cdot 1,1$ or 10 secs. Crystal accuracy $\pm 2$ parts in $10^{6} /$ week. For mains or $12 \mathrm{Vd} . \mathrm{c}$. operation.

Full technical specification available on request.

## RANK CINTEL LIMITED

WORSLEY BRIDGE ROAD • LONDON • SE2G HITHER GREEN - 4600


## The Racal TA. 84 Linear Amplifier

is ideal for long-distance ground-air links, marine shore stations, meteorological stations, fixed and semi-mobile military uses, national security networks and mediumdistance $R / T$ circuits-indeed for nearly all radio links. It gives a power amplification of at least 10 times with an R.F. output of 5 kW P.E.P. from an R.F. input of 500 W or 3 kW
R.M.S. Its simplicity of operation and tuning accuracy demand little or no skilled attention in the transmitting station. It is designed to comply fully with Joint-Services Specification K. 114 (Protected Ground Equipment), soundly constructed and fit for the most adverse climatic and operating conditions. Full specifications and details on request.

## BAGAI

RACAL ENGINEERING LIMITED
WESTERN ROAD, BRACKNELL, BERKS, ENGLAND Tel.: Bracknell 941 'Grams/Cables: RACAL BRACKNELL BERKS
Overseas agents in most territories



## rine JEerpramiti  riype D101

The need for instruments capable of measuring voltages with a high degree of accuracy and with a fast reading time has long been apparent. The Ferranti 3 digit voltmeter has been developed to meet this requirement. The advantages of this precision instrument will undoubtedly prove attractive to those engaged in the fields of automatic testing and monitoring, analogue to digital conversion, calibration of moving pointer instruments and many similar applications.

## Special Feafures

## - Automatic Ranging and Polarity <br> - High Accuracy and Resolution <br> - Fast Reading Time <br> - Complete Reliability

## SPECIFICATION

Display Three digit plus automatic polarity Indication and automatic decimal placement.

## Automatic

D.C. Volts in 3 ranges
$0.01-9.99 \mathrm{~V}$
Ranges $10.0-99.9 \mathrm{~V}$ $100 \mathrm{~V}-999 \mathrm{~V}$

Accuracy $0.1 \%$ of full scale reading on any range.
Average Reading Time 0.7 seconds.
Input Impedance at Balance 10 Megohms.
Input $\quad 110-250 \mathrm{~V}$ A.C. $50-60 \mathrm{c} / \mathrm{s} 50 \mathrm{~W}$.
Weight 50 lbs . approximately.
Style Bench cabinet $17^{\prime \prime} \times 13^{\prime \prime} \times 10 \frac{1^{\prime \prime}}{}$ high with optional brackets for standard rack mounting.

In view of continuing development, the right is reserved to alter the specification or design of this instrument.

FERRANTILTD<br>FERRY ROAD<br>E<br>$D \| N B \cup R G H$<br>5

## ADVANCED *TRUE <br> DOUBLE-BEAM OSCILLOGRAPH

## CATHODE-RAY TUBE

Cossor 4 in . ( 10 cm .) double-beam, p.d.a., type 93D with green fluorescence, operating with overall accelerating potential of 3 kV or 6 kV .

## YI AMPLIFIER

$1 \mathrm{c} / \mathrm{s}$ to $10 \mathrm{Mc} / \mathrm{s}(30 \%$ down). Rise-time : $0.04 \mu \mathrm{sec}$.
Output deflection: $6 \mathrm{~cm}(4 \mathrm{~cm}$ at $10 \mathrm{Mc} / \mathrm{s})$. Sensitivity : calibrated $100 \mathrm{mV} / \mathrm{cm}$ to $10 \mathrm{~V} / \mathrm{cm}$. Sensitivity control : in steps $3: 1$ and $10: 1$ with continuously variable intermediate control. Input Attenuator impedance : $1.2 \mathrm{M} \Omega$ and 65 pF .

## Y2 AMPLIFIER

Identical with YI amplifier.

## SIGNAL DELAY

200 musec approximately. Not more than $10 \mathrm{~m} \mu \mathrm{sec}$ differential between channels.

## PRE-AMPLIFIER (2)

Gain 10. $5 \mathrm{c} / \mathrm{s}$ to $200 \mathrm{kc} / \mathrm{s}(30 \%$ down) Input Resistance: $3 \mathrm{M} \Omega$.
One for A1 amplifier, the other for A2 or X amplifier.

## PROBES (OPTIONAL EXTRA)

Frequency-compensated "L" attenuator. Input impedance: $6 \mathrm{M} \Omega$ and 15 pF . Insertion loss: 10:1.

## TIME-BASE

## Triggered.

Range: $0.03 \mu \mathrm{sec} / \mathrm{cm}$ to $15 \mathrm{msec} / \mathrm{cm}$ in eleven steps. Triggered from positive or negative signals derived externally or from Y1 amplifier.
Sensitivity: pulse-1 cm . deflection or 2 V external. Sine wave- 2 cm deffection or 2 V r.m.s. external at frequencies up to $5 \mathrm{Mc} / \mathrm{s}$. Expansion amplifier, continuously variable gain up to 5 times. Time-base output available at front panel on slow speed ranges. Delayed time-base: continuously variable delay $2 \mu \mathrm{sec}$ to $150 \mu \mathrm{sec}$. Delay jitter not greater than 1 part in 1,000. Sensitivity pulse -1 cm deflection or 2 V external.

## X AMPLIFIER

$10 \mathrm{c} / \mathrm{s}$ to $750 \mathrm{kc} / \mathrm{s}(30 \%$ down).
As time-base amplifier: continuously variable expansion up to 5 times.
As independent $X$ amplifer: sensitivity variable from $1 \mathrm{~V} / \mathrm{cm}$ to $100 \mathrm{~V} / \mathrm{cm}$ in 5 ranges.

## CALIBRATION

Voltage measurement: internal calibrating voltage (square wave) referred through sensitivity control of the amplifiers. Accuracy $\pm 3 \%$. Time measurement: by directly calibrated $\mathbf{X}$ shift control ( $\pm 5 \%$ ) and/or by $20 \mathrm{~m} \mu \mathrm{sec}( \pm 3 \%$ ) black-out pips (for accurate measurement of rise-time).

## POWER SUPPLY

Mains: 100 V to 130 V and 200 V to 250 V . Frequency: $50 \mathrm{c} / \mathrm{s}$ to $100 \mathrm{c} / \mathrm{s}$.
Consumption: 550 W .
Internal supplies are stabilized where necessary.

## SIZE AND WEIGHT

| Height | $17 \frac{1}{2} \mathrm{in}$. | $(43.2 \mathrm{~cm})$. |
| :--- | :--- | :--- |
| Width | $12 \mathrm{in}$. | $(30.5 \mathrm{~cm})$. |
| Depth | $24 \frac{3}{\mathrm{in}} \mathrm{in}$. | $(62.9 \mathrm{~cm})$. |
| Weight | 80 lb. | $(36.3 \mathrm{~kg})$. |

## ACCESSORY

Camera Model 1428.

## 

The Instrument Company of the Cossor Group

# Four first-class performers 

These four Cossor Oscillographs, each designed for an important range of applications, offer first-class performance backed by rigid adherence to published specifications.

## MODEL 1065 PULSE OSCILLOGRAPH

Tube: single-beam, P.D.A. Bandwidth: d.c. to $15 \mathrm{Mc} / \mathrm{s}$ (-50\%).
Sensitivity: $250 \mathrm{mV} / \mathrm{cm}$. Overshoot: less than $3 \%$. Time-base: triggered or repetitive over range $40 \mathrm{~cm} / \mathrm{sec}$ to $5 \mathrm{~cm} / \mu \mathrm{sec}$. $X$ Amplifier: gain 5 , continuously variable. Time-base delay: 2 ranges, continuously variable.
Calibration: voltage and time, by calibrated shifts Probe: $1.5 \mathrm{M} \Omega, 12 \mathrm{pF}$


MODEL 1058 FOR THE TV \& RADIO ENGINEER

Tube: single-beam Bandwidth: dec. to $6 \mathrm{Mc} / \mathrm{s}(-50 \%)$. Sensitivity: $250 \mathrm{mV} / \mathrm{cm}$. Time-Base: triggered or repetitive, over range $30 \mathrm{~cm} / \mathrm{sec}$ to $1.5 \mathrm{~cm} / \mu \mathrm{sec}$. Special facilities for triggering from TV line or Frame pulses on IV.D.A.P. composite video waveform. $X$ Amplifier: gain 5 , continuously variable. Calibration: time and voltage calibration facilities.


MODEL 1035 GENERAL PURPOSE DOUBLE-BEAM OSCILLOGRAPH
$Y$ Amplifiers: A1: $5 \mathrm{c} / \mathrm{s}$ to $5 \mathrm{Mc} / \mathrm{s}(-30 \%)$. Maximum gain 3,000. A2: $5 \mathrm{c} / \mathrm{s}$ to $250 \mathrm{kc} / \mathrm{s}(-30 \%)$ at gain 30 , with trace inversion facility. Time-base: repetitive or triggered in 9 sweep ranges from 100 msec to $10 \mu \mathrm{sec}$. Time-base delay and pulse bright-up facilities. $X$ Amplifier: gain 5, continuously variable. Calibration: voltage and time, by calibrated shifts.

MODEL 1049 INDUSTRIAL DOUBLE-BEAM OSCILLOGRAPH
$Y$ Amplifier: Al: dec. to 200 kc s $(-30 \%)$ at gain 900: A2: dec. to $400 \mathrm{kc} / \mathrm{s}(-30 \%)$ at gain 30.
Time-Base: repetitive or triggered in 18 ranges, down to $7.5 \mathrm{sec} / \mathrm{sweep}$. Intensity modulation: three modes including beam bright-up. Calibration: time and voltage, by calibrated shift ( $X$ and $Y 1$ ) and multiplier (Y2).
Let us send full details of Cossor Instruments or arrange for a representative to discuss your special needs.


## COSSOR'instruments tito

The Instrument Company of the Cossor Group
COSSOR HOUSE, P.O. BOX 64, HIGHBURY GROVE, LONDON, N.5.
Teieptione CANonbury 1234 ( 33 lines)
Telegrams: Cossor, Norphone, London.


20 QUEEN ANNE STREET, LONDON W. 1
Telephone: IMPerial 6000
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## the key to information

and advice on:
$\star$ Electronic and nuclear instruments
$\star$ Navigational and survey equipment

* Optical and ophthalmic instruments
$\star$ Laboratory, medical and X-ray apparatus
* Instruments for process control and automation
* Kinematograph and allied instruments
$\star$ All industrial instrumentation
Space donated by: COSSOR INSTRUMENTS LTD.
OSCILLOGRAPHS AND ELECTRONIC INSTRUMENTS


## 路 <br> World's most advanced Valve Performance Analyser

First model delivered to The United Kingdom Atomic Energy Authority


The new Cossor Valve Analyser provides the electronic engineer with very much fuller information on valve behaviour than has previously been obtainable. It submits valves to the conditions under which they will actually operate in modern 'pulse' type circuits in, for example, radar and computer equipment and reveals their precise characteristics when so operated. The Instrument is particularly valuable in investigations of positive grid drive operation of such valves.
Now being manufactured to meet a demand from all over the world, Model 1070 is a fine example of Cossor technical development in the Instrument field.


## COSSOR <br> Cossor Model 1070 <br> Pulse Operating Valve Analyser



## new small and miniature standard cases at really LOW PRICES!

15 new Imhof standard cases with panel sizes from $6^{\prime \prime} \times 4^{\prime \prime}$ to $24^{\prime \prime} \times 10 \frac{1_{2}^{\prime \prime}}{}$ Just look at these examples . . . compare the new low prices. Here's real value for money! Whatever the size-whatever the quantityall these new cases are built to the same, robust specification and high finish as the existing Imhof Standard Range. Top quality and rock-bottom prices result from Imhofs streamlined methods and full tooling for large-scale production in Europe's most modern factory fully equipped for quality manufacture of cases, racks and consoles

## TMITOES

These new cases have been designed as a result of the fast development in miniaturisation of electronics and electrical instruments. The cases are of two types: with sloping front panels, and rectangular cases with vertical front panels. Both types are available in standard duo-tone finishes. Imhofs have also produced a new type chassis incorporating fixing brackets especially for these new cases

## 7 days delivery - generous quantity discounts !

STOP PRESS! Now available, 9 new ultra_ miniature cases-MINIBOXES-of two-piece construc. tion. Sizes from $3^{\prime \prime} \times 18^{\prime \prime} \times 2 \frac{1}{" 1}^{\prime \prime}$ to $17^{\prime \prime} \times 4^{\prime \prime} \times 5^{\prime \prime}$. Prices from $6 / 9$ to $25 /$-. Complete details on request

## Alfred Imhol Ltd Dept M 11 Ashley Works Cowley Mill Road Uxbridge Middx Uxbridge 6231

Export \& London Showrooms: 112 -116 New Oxford Street WCI Museum 7878


IMHOFS AGENTS OVERSEAS

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PORTUGAL: Projectos e Construcoes Lda, Lisbon

SWEDEN: Elektronlund $A B$, Malmo $C$ SWITZERLAND: Walter Blum, Zurich 2/39
U.S.A.: Bud Radio Inc,

Cleveland 3, Ohio
BRIT. GUIANA: Davsons Carribbean Agencies Ltd, Georgetown


The introduction of Mullard "Magnadur"' magnets has resulted in the development of quite revolutionary designs in many types of apparatus, amongst which the design of permanent magnet motors is an outstanding example.


Photograph of d.c. motor using " Magnadur" rins magnets in place of the normal field windings.

This design uses a "Magnadur 1" cylinderinside a mild steel shell which forms the return magnetic path. This assembly is diametrically magnetised to provide the maximum pole area. Due to the high intrinsic coercive force and low recoil permeability of "Magnadur 1 " (which are of the order of 3,200 oersteds and 1.2 respectively), a comparatively large air gap, (for example of $0.1^{\prime \prime}$ ), can be employed without appreciable loss in the field strength measured in the gap, or reduction in performance, or efficiency of the motor.
The graph indicates the typical performance obtained from a motor similar to the one illustrated.

No. 19

## D.C. Motors

Advertisements in this series deal with general design considerations. If you require more specific information on the use of permanent magnets, please send your enquiry to the address below, mentioning the Design Advisory Service.


Other advantages of this design are:-

1. Commutation troubles due to armature reactionare eliminatedas "Magnadur" has practically unit recoil permeability.
2. Eddy-current and hysteresis losses are eliminated from the stator.
3. The armature can be removed and replaced withoutaffecting the motor performance, making inspection and maintenance a simple routine operation.
4. The coil ends on the armature can very easily be arranged to cut magnetic flux, so that extra torque and efficiency are achieved.
5. The temperature rise of the motor on continuous running tests is lower than for a similarly rated motor using an energised field coil.
6. The motor is reversible without the necessity of switching field windings and will give high torque and efficiency with virtually sparkless commutation in either direction.
7. High power-to-weight ratio.

In addition to the above odvantages, it is generally found that in quantity production, a considerable saving in cost can be made when compared with conventional types of motors.

If you wish to receive reprints of this advertisement and others in this series write to the address below.


[^8]
## Avartir

## AUDIO AMPLIFIER STANDARD

Suitable for use as:

* Laboratory Standard
* Test amplifier for microphones, pick-ups, loudspeakers, pre-amplifiers, tape decks etc.
* Recording amplifier.
* Broadcast Transmitter Modulator.

The Avantic DL7-35, originally designed as a high fidelity amplifier, has proved to be of such advanced design that it has remained unsurpassed. During the three years it has been manufactured the high performance laid down in the design has been consistently maintained. It can now be regarded as a Laboratory Standard of the utmost reliability.

## AVANTIC DL7-35 POWER AMPLIFIER

Harmonic Distortion:
$<0.05 \%$ at 20 watts sine wave output.
Intermodulation Distortion:
$0.7 \%$ at 20 watts
$1.0 \%$ at 29 watts
$\mathrm{fm}=40 \mathrm{c} / \mathrm{s} . \mathrm{fc}=10 \mathrm{kc} / \mathrm{s} . \mathrm{fm} / \mathrm{fc}=4$
Hum and Noise:
-85 dB relative to 20 watts output with $10 \mathrm{k} \Omega$ source resistance.
Load Impedance:
$4 \Omega, 8 \Omega, 16 \Omega$ switch selected with automatic feedback compensation.
Damping Factor:
50
Rise Time:
$5 \mu$ secs.
Power Inputs:
$105,117,125,210,233,251$ V. a.c. $40-60 \mathrm{c} / \mathrm{s}$.




H.T. fuse.

Distributed Load Push-Pull Output Stage.
High stability resistors in input stage.
Power outlets of 6.3 V . at 2.5 A . a.c.
Price: 30 gns.

* Suitable pre-amplifiers available to increase sensitivity to $3 m V$.

TOMORROW'S

## INSTRUMENTATION

TODAY

For many years B \& K Laboratories have been privileged to supply and maintain advanced instrumentation for numerous important research and engineering applications.

We are proud that this work is contributing to the international success of many British products from the best high-fidelity sound equipment to the finest in modern transportation.

In the past, B \& K Laboratories’ instruments were often installed after other equipment had been tried; initially the cost of higher accuracy did not appear justified, and only by experience did the need for more precise results become evident.

Nowadays however, with improved instrument versatility and increased production, the cost disparity between "'very good" and "excellent" has diminished considerably.

For voltage and current measurements, a wide range of instruments is produced. The C. 31 electrometer (illustrated) will detect currents of the order of $1 \times 10-17$ amperes and will measure 0.02 mV . At the other end of the scale the J. 1003 v.t.v.m. is designed for measurements up to over 200 kilovolts from $10 \mathrm{c} / \mathrm{s}$ to $20 \mathrm{Mc} / \mathrm{s}$.

For radioactivity studies we offer a fully integrated range including scalers, ratemeters, automatic sample changers and print-out timers.



For metallurgical work, the M. 800 Portable Transistorized Thickness Gauge will determine plating or sheet thicknesses from $0.0005^{\prime \prime}$ to $0.1000^{\prime \prime}$ with high accuracy. The " Radac " M. 302 equipment will determine deviations from standard hardness, strength, purity and alloy composition.

For phase angle measurements the model FB. 120 (illustrated) provides accurate meter indications over the frequency range $0.2 \mathrm{c} / \mathrm{s}$ to $50 \mathrm{Kc} / \mathrm{s}$. Other types enable similar measurements up to $500 \mathrm{Mc} / \mathrm{s}$.

For special purpose instrumentation not listed, enquiries are welcomed with details of any measurement problems.

The "Elema" Industrial Version Direct Ink-Writing Oscillograph with its unique ability to accurately reproduce traces at frequencies up to and beyond $1,000 \mathrm{c} / \mathrm{s}$, enables highest precision conversions at lower frequencies. Traces from multichannel types can overlap and several chart speeds are provided up to 2 metres per second. No photographic developing devices or chemicals are needed and ordinary chart paper may be used.


SIGNAL SOURCES
KSS Series, 10 Units cover from 1,050 to $17,500 \mathrm{Mc} / \mathrm{s}$.
EHF Series, 9 Units cover from 18,000 to $50,000 \mathrm{Mc} / \mathrm{s}$.

SIGNAL GENERATORS

MSG-1
MSG-2
MSG-34
PMX (2)
PMK (2)
SG-1218
EHF (7)

950 to $2,400 \mathrm{Mc} / \mathrm{s}$. 2,000 to $4,600 \mathrm{Mc} / \mathrm{s}$. 4,200 to $11,000 \mathrm{Mc} / \mathrm{s}$. 4,450 to $11,000 \mathrm{Mc} / \mathrm{s}$. 10,000 to $21,000 \mathrm{Mc} / \mathrm{s}$. 12,400 to $17,500 \mathrm{Mc} / \mathrm{s}$. 18,000 to $39,700 \mathrm{Mc} / \mathrm{s}$.

## SWEEP GENERATORS

CSG Series, 5 Units cover from 1,000 to $16,000 \mathrm{Mc} / \mathrm{s}$.


## SPECTRUM ANALYSERS

TSA-1 10 to $1,000 \mathrm{Mc} / \mathrm{s}$.
TSA-2 910 to $4,560 \mathrm{Mc} / \mathrm{s}$.
TSA-3 4,370 to $22,000 \mathrm{Mc} / \mathrm{s}$.
TSA-4 21,000 to $33,000 \mathrm{Mc} / \mathrm{s}$.
TSA-5 $\quad 33,000$ to $44,000 \mathrm{Mc} / \mathrm{s}$.
Interchangeable tuning units cover each band using the same basic display unit and power supply.
*SA-84, Multiband covers $10-40,880 \mathrm{Mc} / \mathrm{s}$. DA-70, 50,000 to $100,000 \mathrm{Mc} / \mathrm{s}$.

## MICROWAVE RECEIVERS

R. Eight plug-in tuning units cover 400 to $46,700 \mathrm{Mc} / \mathrm{s}$.
FIM covers $\mathrm{L}, \mathrm{S}, \mathrm{M}$ and X bands.
SPECIAL INSTRUMENTS include :-
K-200 Microwave Tube Tester.
P-3 Transistorized Power Meter.
VS-2 Ratio Scope.


The SL range of waveguide test equipment comprises automatic standing wave indicators, direct «reading frequency meters, motorised waveguide switches, sliding screw tuners, adjustable shorts, rotating joints, double stub tuners, mixers, attenuators, etc., for frequencies from 2,450 to $18,000 \mathrm{Mc} / \mathrm{s}$.

The DB range of waveguide test equipment includes adaptors, attenuators, standing wave indicators, wave meters, reference cavities, mounts, mixers, multipliers, couplers, elbows, filters, horns, phase shifters, rotating joints, movable shorts, waveguide switches, etc., for frequencies up to $140,000 \mathrm{Mc} / \mathrm{s}$.

## $16 d$



Beat Frequency Oscillator 1014 can feed subjects under test directly or via constant sound sources (e.g. 4211, 4215) using compressor circuit through sweep range $20 \mathrm{c} / \mathrm{s}-20 \mathrm{Kc} / \mathrm{s}$. Synchronous frequency response measurements are obtained using Level Recorder 2304, with additional items where required. (Other types for $2 \mathrm{c} / \mathrm{s}-2 \mathrm{Kc} / \mathrm{s}$ and $200 \mathrm{c} / \mathrm{s}$ $200 \mathrm{Kc} / \mathrm{s}$ ).


Calibrated Accelerometers (sensitive up to $70 \mathrm{mV} / \mathrm{g}$ for temperatures up to $250^{\circ} \mathrm{C}$ ) may be used with integrating Preamplifier 1606 for readings of acceleration, velocity and displacement.

Level Recorder 2304 will automatically record spectra from test pieces, Measuring Microphones, Accelerometers, Strain Gauges, etc., by means of electrically synchronised Octave / Third-Octave Spectrometer 2111, containing $16 \mathrm{c} / \mathrm{s}$ $35 \mathrm{Kc} / \mathrm{s}$ filters and special v.t.v.m. Selfcontained Audio Frequency Response Tracer will provide a c.r.t. spectrum display where desired.

All main instruments are available separately or combined, (e.g. for 19" rack mounting with tape recorder for frequency multiplication, etc.). A complete range of accessories, (e.g. linear and logarithmic potentiometers, polar diagram attachments, test boxes, switches, inverters) is available for direct interconnection.

# THE COMPLETE SYSTEM FOR ACOUSTIC AND VIBRATION ANALYSIS, ABSORPTION AND REFLECTION MEASUREMENTS AND FREQUENCY RESPONSE DATA 

Standard Measuring Microphones with special amplifiers $2603 / 2605$. Associated equipment includes Artificial Ear 4141, Calibration Apparatus 4151, and Noise Reference Source 4240.

## Standard Automatic Vibration

 Exciter Control 1016, $5 \mathrm{c} / \mathrm{s}-5 \mathrm{Kc} / \mathrm{s}$ and $5-10 \mathrm{Kc} / \mathrm{s}$ with 44 -speed selective scanning sweep. Accelerometer feedback with computation for mode control (acceleration, velocity or displacement) with provision for automatic changeover.


The P.S. 200 Series Instrumentation Magnetic Tape Data Recorder/Reproducer (illustrated) supersedes the more bulky laboratory recorders and offers greater convenience and dependability. Up to 14 tracks of information can be recorded at speeds from $1 \frac{7}{8}$ i.p.s. to 60 i.p.s. Speed control accessories are available for synchronised playback. The data can be recorded in direct, FM, PWM or digital form. This equipment is designed for tape instrumentation applications demanding the highest degree of accuracy. The unique transport design incorporating a self-threading magazine with precision reels, eliminates time-consuming tape threading and at the same time offers the facility of endless-loop recording by means of a simple change of magazine.
Shock mounts enable the instrument to be used as an airborne recorder ; Grant slides are available for $19^{\prime \prime}$ rack mounting. A 7 -channel recorder measures only $17 \frac{1^{\prime \prime}}{} \times 15 \frac{1^{\prime \prime}}{} \times 10^{\prime \prime}$, weighs 65 lbs. and requires 250 watts of power ( 30 watts on stand by) and can be supplied for 24 V DC operation.

For advanced digital magnetic tape applications, the Potter Series 908 Tape Handler operates at speeds up to 150 i.p.s. with character transfer rates up to $45 \mathrm{Kc} / \mathrm{s}$ on $\frac{1^{\prime \prime}}{}{ }^{\prime \prime}$ tape and $90 \mathrm{Kc} / \mathrm{s}$ on $1^{\prime \prime}$ tape. A higher pulse packing density is made possible by a unique precision guide system. Forward and reverse capstans allow differing speeds without acceleration delays. Stop distance: $0.125^{\prime \prime} \pm 0.035^{\prime \prime}$. Incorporates folded vacuum tank slack loop system. Several other models are produced, with fully transistorized electronics. Associated equipment includes computer tape testers, very high speed a/phanumeric printers ( 48,000 characters per minute) counters and magnistors.

For basic instrumentation applications, various models are available for direct record/ reproduce applications using $\frac{1}{4}$ " tape with various tape speeds. Frequency Response $\pm$ 2 dB from $30 \mathrm{c} / \mathrm{s}-17 \mathrm{Kc} / \mathrm{s}$ at $7 \frac{1}{2}$ i.p.s., with signal to noise 56 dB and flutter and wow better than $0.2 \%$ r.m.s.

Periodically B. \& K. Laboratories have new vacancies for engineers for electro-mechanical, acoustics, tape recording, microwave and nuclear applications.
Engineers are invited to submit details of experience and background for future consideration. Please write to the Technical Director, B. \& K. Laboratories Limited, 4 Tilney Street, Park Lane, London, W.1.


## $16 f$

 twenty years design experience.
They meet all current specifications for important and exacting test applications the world over. Each part of the systems is created and supervised by the same organisation to provide guaranteed overall performance. (Catalogue MB 423).

For resistive strain gauge measurements, Strain Gauge Apparatus 1516 provides direct readings of strain irrespective of gauge factor, with a variable $3 \mathrm{kc} / \mathrm{s}$ carrier voltage transformer fed to the bridge. Measuring range $100 \mu$ strain to $30,000 \mu$ strain f.s.d. A special Balancing Unit (1530) provides for accurate remote reading. Multipoint manual and automatic selectors and panels enable a large number of consecutive measurements to be made. With provision for external recording or display. (Ask for B. \& K. TR/157).

## BASIC TEST INSTRUMENTS FOR PRODUCTION TESTING, LABORATORY \& SERVICE SHOP USE

A range of basic test instruments (voltmeters, megohmeters etc.) built on the same precision standards as the more specialised instruments is available for general use. (Catalogue B. \& K. ES/8).

Various instruments are available for production testing in different fields of application. The Deviation Bridge (1504) illustrated, is used extensively for electronic component testing. High speeds are attainable by the use of Test Jig (3902). Four models with interchangeable scales cover extensive $R, C$ and $L$ ranges, for accurate impedance and phase angle measurements. (Catalogue B. \& K. ES/8).


## FIRST STAGE RECONDITIONING

 OF C.R.T.sFor the reconditioning of C.R.T.s we supply the complete outfit as an additional service to our customers. This Equipment can only be purchased with our Pumping Units and is not available for sale on its own.

Additional items obtainable: Heater Box for Gun Assembly; Assembly Jigs. All spares for Pumping and Auxiliary Equipment.

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SECOND STAGE Of reconditioning C.R.T.s (washing, settlling, aquadag coating, drying, baking and Aluminising plant) is also obtainable from us. We design, manufacture and supply Vacuum Machinery to Major Companies in Great Britain and Overseas.

## A new standard of quality, by which other machines will be judged "

## Angus McKenzie in TAPE RECORDING AND HI .FI MAGAZINE



* Automatic, in the Simon sense, is meant to be taken literally: it means continuous replay-the machine stops, reverses and changes to the other rack with only a two-second pause, and with no necessity to touch any -ontrol. Similarly, up to three hours' continuous recording can be made without attention, the machine automatically stopping at the end of the second track.

This is the enthusiastic opinion of an expert, an independent reviewer, after thoroughly testing the Simon S.P.4. Throughout the Hi-Fi world, this superb new tape recorder, with its combinaton of high performance and range of exclusive features, is sparking off similar praise from those who have seen and heard it. Look at this list of star features-then come and see it for yourself at your nearest dealer-try it, test it and you too will join the crowds of Simon enthusiasts.

SIMON AUTOMATIC DECK fully 'pushbutton con trolled "
AUTOMATIC TAPE REVERSAL without touching controls
3-WAY MIXING FACILITIES on both record and playback
BASS AND TREBLE LIFT AND CUT with independent controls
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10 WATTS OUTPUT from ultra-linear push-pull amplifier PUSH-PULL OSCILLATOR for noise and hum suppression
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Presented in elegant real hide case with tasteful gold relief. Can be assembled in 4 to 6 hours and you have a set in the top flight of the $25-30$ guinea class. Prealigned I.F. transformers, printed circuit and a 7in. high-flux speaker..........
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VARIABLE FREQUENCY OSCILLATOR KIT

Model VF-IU


For all Amateur Bands, $160-10$ metres. Ideal for Heathkit DX-40U and similar transmitters ......................... $£ 10.12 .0$

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This sensitive headphone set is a fine introduet:on to electronics 'or :ny youngster. (Not illustrated)

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A versatile high-quality self-contained STEREO/MONAURAL Amplifier with adequate output for a living room-or with which to convert a favourite (monaural) radiogram into a stereo-radiogram. 3 watts per channel; $0.3 \%$ distortion at 2.5 w/chnl. ,
20 dB N.F.B. Inputs for Radio (or Tape) 20 dB N.F.B., Inputs for Radio (or Tape) and Gram, Stereo or Monaural; Ganged controls.
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This extremely useful, low priced device will extend the use of your single-beam oscilloscope for duties otherwise only in the province of the double-beam tube.
In short, at a nominal cost, the Heathkit model S-3U will give you the advantages of a double (or other multiple) beam 'scope, while retaining all the advantages of your present single-beam instrument.
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$300 \mathrm{Me} / \mathrm{s} . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . ~$
$\mathbf{K}$
AMATEUR TRANSMITTER KIT Model

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||||||||||||||| |||| |||

## DX-I00U

The world's most popular "Ham" TX Kit
-Completely self-contained, compact "Ham" Transmitter.

- Built-in, highly stable VFO and all Power Supplies. -TVI: Careful design has reduced TVI to a minimum by use of effectively sereened frequency-generating stages and pi tuned circuits at the input and output of the PA stage, and by 11 chokes and pi network filters to all outlets from the cabinet. No fewer than 35 disc ceramic by-pass capacitors help to achieve the exceptlonal stability and high-performance for which this Transmitter is noted.
-The KT88 high-level anode and screen modularor stage gives over 100 watts of audio from less than 1.5 mV . input.
- Adjustable drive and clamp control ensure that valves are only driven sufficiently to maintain the required output.
- Keying on CW is via the VFO and buffer amplifier cathodes; the other RF valves are biased mond cut-off. When zero-beating the TX with signals, the exciter stages only may be run wheyt the final amplifier being switched on.
- Provision has been made for remore control operation. - VFO slow-motion drive is very smooth and back-lash free.
- Covers all Amateur bands up to $30 \mathrm{Mc} / \mathrm{s}$. phone or CW.
- VFO or Crystal control.
£78.10.0


## MATCHED HI-FI STEREO KIT

4-speed Transeription Record Player
\& $1210 \quad 0$
6 w. Hi-Fi Amplifier, Model S-33 .............. \&II 80
Twin Stereo Speakers System Model SSU-I... 620 II 0
Total cost if purchased separately............... \&44 9 0 YOURS for $\varepsilon 42 / 10 /$ if all ordcred together or $\mathbf{c 8 / 8 / -}$ deposit and 9 monthly payments of $64 / 3 /$-. Pedestal speaker legs $\mathbb{C 2} / 14 /$ - optional extra.

## excellent



## TRANSCRIPTION RECORD

 PLAYER Model RP-IUWith 4 -speed A.C. motor unit and Stereophonic Pick-up completely assembled on plinth.
High performance at low cost.
This attractive Transcription Record Player incorporates many new features which make it suitable for all types of recordings on dises. It has the new Collaro RP. 594 unit with the Ronette Stereo Pick-up and gives excellent results on stereo or mono (33, 45 L.P. or 78 r.p.m.)
gramophone records.
£12.10.0

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" HAM" TRANSMITTER KIT Model DX-40U

Covers all amateur bands from 80 to 10 metres. Power input 75 watts C.W. 60 watts peak controlled carrier phone. Output 40 wates to aerial. Provision for V.F.O. $\begin{aligned} & \text { Filters minimise T.V. inter- } \\ & \text { ference. }\end{aligned}$
\&29.10.0 ference.

Our Technical Consultation and Service Departments are always ready to help in the unlikely event of your experiencing any difficulty.


Specially developed to meet the varying needs of different homes. It will house Tape Deck and/or Record Player, F.M. Tuner and Stereo Amplifier. In addition for the convenience of those to whom space is an overriding consideration, it is possible to house speaker systems at each end. For this purpose a loudspeaker kie, comprising two 4 in . plus 8 in , speaker systems, balance unit, speaker grille, cutting template, padsaw and mounting details is also available. Neutral hardwoods have carefully been selected so that the finished product can be stained and polished to individual choice. There is storage space for records, tapes, etc., also for power amplifiers.
Mk. I for Tape Deck or Record Player......... \&15 is 6 Mk. II for both T/O and R/P............................ \& 1788


## thoroughly



## COTSWOLD SPEAKER SYSTEM KIT

This acoustically designed enclosure measures $26 \times 25 \times 13$ in. and houses a special 12 in. bass speaker with 2 in , speech coil, elliptical middle speaker together with a pressure unit to cover the full frequency range of $30-20,000 \mathrm{c} / \mathrm{s}$. Its polar distribution makes it ideal for really $\mathrm{Hi}-\mathrm{Fi}$ Stereo. Delivered complere with speakers, eross-over unit, level control, Tygan grille cloth, etc. Left " in the white" for finish to personal taste, all parts are precut and drilled for ease of assembly.
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## STEREO-HEAD BOOTSER KIT

## Model USP-I

Hi-Fi Stereo Pre-amplifier for low-output Hi-Fi P.U.s. Input 2 mV . to 20 mV . Output adjustable from 20 mV . to 2 V . 40-20,000 c/s..

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*Sold separately ............................Total $\$ 13126$


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This Direct-Reading Capacitance Meter is a very low priced, time-saving instrument which is so useful that it should be part of the general equipment of every electronic laboratory and production line. Easily built in a few hours. $0-100 \mu \mu \mathrm{~F}, 0-1,000 \mu \mu$, $0-0.01 \mu \mathrm{~F}, 0-0.1 \mu \mathrm{~F}$. The meter has $4 \frac{\mathrm{y}}{2} \mathrm{in}$. scale and can be used by an unskilled op arater after a few minutes instruction \$14.10.0

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Arices include free delivery in U.K.


## THE NEW 嶰 HEAVY DUTY MULTICON PLUGS AND SOCKETS

This new Painton range is fitted with covers of cast alloy for strength and rigidity in heavy duty applications.
It is available in $4,6,8,12,18,24$ and $33^{*}$ pole sizes. Illustrated is the 24 pole size.
*33 pole model available shortly.



1 Terminal numbers are moulded into plug and socket bodies, both next to soldering tags and on mating face. This facilitates wiring and cableform testing without removing covers.
Socket clips have split limbs so that 4 areas are in contact with each plug blade. Contact resistance is low and constant, providing a high standard of contact reliability and a minimum life of 10,000 operations.解 plug and socket assemblies the same two-part covers are used. One part carrying the cable clamp is attached to the body moulding and need not be removed. The outer enclosing part is only fastened down after joints and wiring have been checked.
4. A wire retaining loop clips over the radiused corner of the cover and engages positively with a cast groove.

British Patent 700999


Write for full catalogue
 Megaphone weighs only 5 lb . The transistor amplifier gives more than 3 watts output. It uses standard torch batteries which last. about six months.
The Portable Electronic Megaphone with adjustable stand and separate microphone is suitable for all temporary occasions. It can be stood, mounted at an angle or easily carried. It is similar to the Hand Portable and is completely self-contained.


10 WATTS The Portable Transistor Amplifier weighs only $5 \frac{1}{2} \mathrm{lb}$. and measures $8^{\prime \prime} \times 3 \frac{\frac{1}{2}^{\prime \prime}}{} \times 6^{\prime \prime}$. It will deliver 10 watts output for a consumption of 1.8 amps from a 12 volt battery. It is ideal for use in moving vehicles or on sites where a mains supply is not available. A comprehensive selection of microphones and loudspeakers is available.



Brief Specification
PTC 8001/2: 10 watt F.M PTC 2001/2: 5 watt A.M.
Available from 25-174 Me/s. Simplex or Duplex operation "Split-channel" selectivity Up to 6 switch-selected channels Power supply: Models for 6, 12 or 24 volts operation.

ay appointment
TO M, M, DUKE OF EDINBurgh SUPPUEAS OF
gadio telephone equipment ere telecommunications hro.
> "Ranger" v.h.f. dashboard mounting Radiotelephone

The Pye "Ranger" radiotelephone has been designed to meet the specifications of the American F.C.C. and the British G.P.O. It is suitable for use under all climatic conditions and is vibration proofed. Its features include light weight, low battery drain and low cost of installation and maintenance. Optional features are alternative channel spacing; public address and rebroadcast facility on A.M. types; and a choice of fist microphone or telephone handset. The PTC 8001/2 and PTC 2001/2 form part of a complete series which include boot-mounting types and fixed stations.

# PYE TELECOMMUNICATIONS LIMITED NEWMARKET ROAD - CAMBRIDGE 



FEATURING PYE TELECOMMUNICATIONS EQUIPMENT


## Video Transmission Oscilloscope

## Brief Specification:

"Y" Amplifier:
Frequency response: $1 \mathrm{c} / \mathrm{s} .-10 \mathrm{Mc} / \mathrm{s} . \pm 1 \mathrm{~dB}$.
Sensitivity: $50 \mathrm{mV} . / \mathrm{cm}$.
Waveform response: $\mathrm{K}=0.25 \%$
Time Base:
Range: $1 \mu$ sec. $-100 \mathrm{~m} . \sec$.
Trigger:Internal, External or Free Running.
Delayed Trigger: Variable, 5-85 $\mu$ secs.

The Pye PTC 1205 Video Transmission Oscilloscope is designed for testing video performance of transmitters, microwave links, land lines, repeater stations and studio equipment. Standard graticules simplify testing when the instrument is used in conjunction with the Pye PTC $1201 / 3$ Pulse and Bar Waveform Generator.
Special features include internal calibration of amplitude and frequency, calibrated delay scan, hum filter, $10 \mathrm{kc} / \mathrm{s}$ square wave oscillator ànd timing wave generator frequencies of $\mathrm{I}, 6$ androMc/s. As the response of the amplifiers is sensibly flat up to $10 \mathrm{Mc} / \mathrm{s}$, the instrument is suitable for use on 405,525 and 625 line systems.

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the E.E.V. Cir 33 has the same specifications as the 4 PR60A. It also meets all the requirements of military and commercial specifications with the additional advantage of smaller bulk. Conditioning at 30 kV and rigorous testing ensure thoroughly reliable operation right up to the maximum peak anode voltage and current ratings of 25 kV , 18 A .

## 'ENGLISH ELECTRIC'

## Typical Operation

| D.C. Anode Voltage | 20 kV |
| :--- | ---: |
| Peak Anode Voltage | 25 kV |
| Screen Voltage | 1.25 kV |
| Grid Voltage | 600 V |
| Pulse Anode Current | 16 A |
| Peak Anode Current | 18 A |
| Pulse Output Power | 300 kW |
| Duty Cycle | 0.00 I |
| Pulse Length | $2 \mu \mathrm{secs}$ |

Abridged Data

| Type | Plug-in replacement for | Overall <br> Length <br> Max. | Overall <br> Diameter Max. | Net Weight | Heater <br> Voltage | Anode <br> Voltage Max. D.C. | Peak <br> Anode <br> Voltage <br> Max. | Peak Anode Current Max. | Screen Voltage Max. | Anode Dissipation Max. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \mathrm{ClI}_{13} \\ (\mathrm{CV} 2416) \end{gathered}$ | $\begin{array}{r} 4 \mathrm{PR} 60 \mathrm{~A} \\ 715 \mathrm{C} \\ \text { CV427 } \end{array}$ | 152 mm | 65 mm | 9 oz. | 26 | 20 kV | 25 kV | 18 A | 1500 V | 60 W |
| Cirir | $\begin{gathered} C V 2752 \\ 715 \mathrm{C} \\ \text { CV } 427 \\ \text { CV } 398 \\ \hline \end{gathered}$ | 152 mm | 65 mm | 9 oz. | 26 | 17.5 kV | 20 kV | 15 A | 1500 V | 60 W |

## Voltage Stabilisers and Reference Tubes

## ENGLISH ELECTRIC VALVE CO. LTD.

The most extensive range provided by any manufacturer in Great Britain.
Send for full technical data.


| 安 |  |  | $\frac{8}{2} \frac{8}{0}$ | Striking volcage (V) |  |  |  |  |  |  |  | \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | - | - |  |  |  |  |  |  |  |
| OA2 | QSI207 | OA2 | CVI832 | 185 | 225 | 150 | - | - | 30 | 5 | 6.0 | B7G |
| OA2WA + | QSI210 | OA2WA | CV4020 | 165 | 225 | 150 | - | - | 30 | 5 | 5.0 | B7G |
| OA3 | QSI205 | OA3 | CV3798 | 105 | 160 | 75 | $\cdots$ | - | 40 | 5 | 6.5 | Int. Octal |
| OB2 | QS1208 | OB2 | CVI833 | 133 | 210 | 108 | - | - | 30 | 5 | $3 \cdot 5$ | B7G |
| OB2WA+ | QS1211 | OB2WA | CV4028 | 133 | 210 | 108 | - | - | 30 | 5 | 3.0 | B7G |
| OC2 | - | OC2 | - | 115 | 145 | 75 | - | - | 30 | 5 | 4.5 | B7G |
| OC3 | QSI206 | OC3 | CV686 | 133 | 210 | 108 | - | - | 40 | 5 | 4.0 | Int. Octal |
| OD3 | QSI50/40 | OD3 | CV216 | 180 | 225 | 150 | - | - | 40 | 5 | 5.5 | Int. Octal |
| QS75/20 | - | - | $\begin{gathered} \text { CV284 } \\ \text { (CV5083) } \end{gathered}$ | 110 | 160 | $\begin{aligned} & 75 \\ & (70) \end{aligned}$ | - | - | 20 | 2 | 6.0 | B7G |
| Q575/60 | - | - | CV434 | 117 | - | 75 | - | - | 60 | 5 | 5.0 | B8G |
| QS83/3 | - | $\sim$ | Improved CV449 | 115 | 160 | 83 | - | - | 8 | I | 1.5 | B7G |
| QS92/10 | - | $\cdots$ | $\begin{gathered} \text { CV188 } \\ \text { (CV1070) } \end{gathered}$ | 140 | - | $\begin{gathered} 92 \\ (100) \end{gathered}$ | $\longrightarrow$ | - | 10 | 1 | 5.0 | British 4-pin |
| Q595/10 | - | - | CV286 | 110 | - | 95 | 150 | 0.25 | 10 | 2 | 5.0 | B7G |
| QS108/45 | - | - | CV422 | 120 | - | 108 | 150 | 0.10 | 45 | 5 | 5.0 | B8G |
| QS150/15 | - | - | CV287 | 170 | - | 150 | 240 | 0.25 | 15 | 2 | 5.0 | B7G |
| QS150/45 | - | - | CV395 | 170 | - | 150 | 200 | 0.10 | 45 | 5 | 5.0 | B8G |
| QSI200 | - | - | CV2225 | 180 | 225 | 150 | - | = | 15 | 5 | 5.0 | B7G |
| QS1201+ | - | - | - | 110 | 160 | 75 | - | - | 15 | 2 | 4.5 | B7G/F |
| QS1202+ | - | - | CV4052 | 133 | 210 | 108 | - | - | 15 | 2 | 3.0 | B7G/F |
| QSi203+ | - | - | CV4053 | 180 | 225 | 150 | - | - | 15 | 2 | 4.5 | B7G/F |
| QSI204 | - | - | - | 133 | 210 | 108 | - | - | 25 | 5 | 3.0 | B7G |
| $\begin{gathered} \text { QS1209/ } \\ 5651 \end{gathered}$ | $\begin{aligned} & 5651 / \\ & \text { QS1209 } \end{aligned}$ | 5651 | CV449 | 115 | 160 | 84 | - | - | 8 | 1 | 3.0 | B7G |
| QSI212+ | - 5 | $5651 \mathrm{WA}{ }^{\text {\% }}$ | CV4048 | 115 | 115 | 85 | - | - | 10 | 1 | 40 | B7G |
| QS1213+ | 一 | - | CV4054 | 115 | 115 | 85 | - | - | 10 | 1 | 4.0 | B7G/F |

+This is a rugged and reliable type. B7G/F denotes flying leads. O In normal lighting.
Stabilovolts

| E.E.V. <br> type | Service type | Gap | Striking voltage min. (V) | Operating voltage (V) | Anode current max. (mA) | Cathode current min. (mA) | Regulation <br> per gap <br> over full <br> current <br> range <br> (average) $(V)$ | Base |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\dagger$ STV280/40 | CV1068 | A4 to K | 420 | 280 | 35 | 5 | 4.0 | B5 |
|  |  | A3 to K | 320 | 210 | 40 |  |  |  |
|  |  | A2 to K | 210 | 140 | 60 |  |  |  |
|  |  | Al to K | 110 | 70 | 60 |  |  |  |
| + STV280/80 | CVI069 | A4 to K | 420 | 280 | 70 | 10 | 4.0 | B5 |
|  |  | A3 to K | 320 | 210 | 70 |  |  |  |
|  |  | A2 to K | 210 | 140 | 90 |  |  |  |
|  |  | Al to K | 110 | 70 | 100 |  |  |  |

† Indicates a recent addition to the range

## all round <br>  <br> COMMUNICATIONS RECEIVER Type C864

the world $<$


All round the World this Airmec receiver is known and used for its remarkable performance at an extremely low cost.

Superior Sensitivity Superior Signal-to-Noise Ratio Superior Second Channel Rejection



Main tuning control showing a portion of the seven frequency scales, the coarse and fine logging scales and the movable cursor.

- Frequency coverage from $15-45 \mathrm{kc} / \mathrm{s}$ and $100 \mathrm{kc} / \mathrm{s}-30 \mathrm{Mc} / \mathrm{s}$.
- Frequency setting accuracy better than $1 \mathrm{kc} / \mathrm{s}$.
- Film scale giving actual scale length of 4 ft . on each frequency range.
- $90: 1$ slow motion drive with logging scale.


## ADDITIONAL FEATURES

- Separate incremental tuning control for use with crystal calibrator.
- Double frequency changer circuit.
- Stabilised local oscillator H.T. voltages.
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- 2 watts output.

Turret band switching.

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## TRANSISTOR!

This new Sylvania-Thorn NPN Germanium Alloy Transistor Series GT 422 has been designed and made in Britain for power switching applications. It is precision built of hermetically-welded construction in a rigidly-controlled production environment; its reliability and long life is ensured by careful inspection and testing at all stages of manufacture.

## JUNCTION MAXIMUM JUNCTION TEMPERATURE: <br> > MAXIMUM COLLECTOR CURRENTS UP TO <br> <br> MAXIMUM COLLECTOR <br> <br> MAXIMUM COLLECTOR CURRENTS UP TO

 CURRENTS UP TO}$85^{\circ} \mathrm{C}$

6 AMPS.
MAXIMUM COLLECTOREMITTER VOLTAGES UP TO 60 V

Several ratings are available. Write for further details to:

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## SYLVANIA-THORN <br> 

## MAXIMUM RATINGS

|  | GT <br> $\mathbf{4 2 3}$ | GT <br> $\mathbf{4 2 2}$ | GT <br> $\mathbf{4 2 4}$ | GT <br> $\mathbf{4 2 5}$ | GT <br> $\mathbf{4 2 6}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| MAXIMUM COLLECTOR- <br> EMITER VOLTAGE <br> ITransistor COnducting) | 60 V | 60 V | 60 V | 36 V | 36 V |
| MAXIMUM COLLECTOR <br> CURRENTI | 6 A | 6 A | 3 A | 6 A | 3 A |
| DC CURRENT GAIN <br> AT RATE <br> COLLECTOR-CURRENT |  |  |  |  |  |
| MAXIMUM: | 120 | 35 | 60 | 35 | 60 |
| MINIMUM: | 35 | 11 | 18 | 11 | 18 |



## Stabilized

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## PD1 <br> THERMIONIC <br> VALVES

£150 NETT IN U.K.
Leaflet W60

- High-power $0-600$ volts stabilized $\mathbf{3 0 0} \mathrm{mA}$ max.
L.T. supplies stabllized - two independent outputs at $6 \cdot 3$ volts 4 amps.
H.T. source resistance less than 0.1 ohm at d.c. and less than 0.5 ohm up to $30 \mathrm{kc} / \mathrm{s}$.
- H.T. source resistance may be varied up to a maximum of 40 ohms.
D- Mains ripple of up to 6 volts can be superimposed on H.T. Jine.
- Overload protection of H.T. line by resettable cut-out.
Advance
COMPONENTS LIMITED


Two new stabilized power packs with outstanding features for the development engineer.
The Type PP. 1 has the unique features of stabilized L.T. voltages, variable H.T. source resistance, and mains ripple injection on the H.T. line.

The Type PP. 3 is fully transistorized and provides simul-
 taneous d.c. voltages of either polarity, and is fully protected against accidental short-circuit.


We shall be pleased to arrange for our Nrea Sales Engineer to demonstrate these models to you.


THE EDISWAN S11E12 (CV4060)
Special Quality Beam Tetrode

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## . <br> newcomer with

a first class reference

The SirEi2 is the latest addition to the range of Ediswan valves designed specifically for use in series or shunt control circuits.
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| Heater Voltage (volts) | $\mathrm{V}_{\mathrm{h}}$ | 6.3 |
| :--- | :--- | :--- |
| Heater Current (amps) | $\mathrm{I}_{\mathrm{h}}$ | 1.6 |
| Anode Voltage, maximum (volts) | $\mathrm{V}_{\mathrm{a}}$ (max) | 800 |
| Screen Voltage, maximum (volts) | $\mathrm{V}_{\mathrm{g}_{2}}$ (max) | 300 |
| Mutual Conductance (mA/V) | $\mathrm{gm}_{\mathrm{m}}$ | 13.5 |
| Anode Dissipation (watts) | $\mathrm{P}_{\mathrm{a}}$ (max) | 28 |
| Cathode Current (mA) | $\mathrm{I}_{\mathrm{k}}$ (max) | 300 |

The new valve is specially designed to resist shock and is quality tested at all stages of manufacture to ensure maximum reliability and life expectancy. It is available from stock. Further information on this and other valves in the CV 4000 range will be gladly sent on request.

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## High frequency-High gain

## Computing Transistor

The OC23 is designed and specially tested for driving square-loop ferrite computing elements and storage matrices. Its high $f_{\alpha}$ and power handling capabilities, however, suit it for a number of additional computing applications.

- Ferrite drive transistor providing 1-amp pulses with rise time $<0.8 \mu$ sec.
- Half and full current pulse generator transistor for ferrite stores of up to 40,000 bits capacity.
- Gating transistor for use with ferrite stores.
- Clock pulse generator transistor for medium speed computers.


Drive A

$\rightarrow$ Pis
<0.5 us
012345678910111213141516 H3
Pulse generator circuit for square loop ferrites

High quality industrial A.F. Transistor
The $f_{\alpha}$ of $2 \mathrm{Mc} / \mathrm{s}$ of the 0 C 22 ensures that the negative feedback used in quality a.f. amplifiers does not cause h.f. oscillation. In addition, the $\alpha^{\prime}$ gives a generous final gain even allowing for the inevitable reduction through negative feedback, thus reducing the power required from the drive stage. An extremely linear $\alpha^{\prime} / I_{c}$ characteristic is yet another reason for using the OC 22 in transistorised industrial a.f. equipment where quality is of paramount importance.

## 0 C24 Communications Transitor

The OC24 is particularly suited for communications applications. Two of these transistors are, for example, used in the outputstage of a marine distress transmitter where they provide 4 watts c.w. at $500 \mathrm{kc} / \mathrm{s}$. The OC24 can, of course, be used for modulated c.w. or telephony.
Another example of the application of the OC24 in the feld of communications is a 12 ahannel telephone repeater amplifier which conforms to the full C.C.I.T. Specification. This amplifier has an output of 0.5 watt at $120 \mathrm{ke} / \mathrm{s}$.


4-watt experimental a.f. amplifier circuit
Total harmonic distortion at 4W output
(measured at $400 \mathrm{c} / \mathrm{s}$ )
Frequency response ( $400 \mathrm{c} / \mathrm{s}$ ref. Ievel) $\cdots . . .<1.0 \%$
Feedback factor (with $25 \mathrm{k} \Omega$ souree) to $20 \mathrm{ke} / \mathrm{s}$
Feedback factor (with $2.5 \mathrm{k} \Omega$ source) $\ldots \quad 30 \mu$


4-watt $500 \mathrm{ke} / \mathrm{s}$ Transmitter

## Power transistors

## 10 watts dissipation $2 \mathrm{Mc} / \mathrm{s}$ average $\mathrm{f}_{\alpha}$

High frequency cut-off, high $\alpha^{\prime}$, high dissipation and low bottoming voltage are all combined in the Mullard OC23-a leading transistor of its kind in the world.

The OC23 and its companion types OC22 and OC24 are now being made by Mullard in extremely large quantities and are immediately available at economic prices. Telephone or write Mullard House for full information and assistance in selecting the type most suited for your particular application.


Cermanlum P-N-P Alloy Junction Transistors
Characteristics (at $\mathrm{T}_{\text {function }}=25^{\circ} \mathrm{C}$ ) for $0 \mathrm{C} 22,0 C 23$ and 0 C 24 .
GROUNDED BASE

| Collector Leakage Current $\text { (at } V_{c}=-10 \mathrm{~V}, \mathrm{I}_{\mathrm{e}}=0 \text { ) }$ |  | $\mathrm{I}_{\mathrm{c}}(0)$ | Typical <br> $30 \mu \mathrm{~A}$ | Max. $100 \mu \mathrm{~A}$ |
| :---: | :---: | :---: | :---: | :---: |
| Emitter Leakage Current $\text { (at } V_{e}=-10 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=0 \text { ) }$ | .. | $I_{\text {e(0) }}$ | $20 \mu \mathrm{~A}$ | $100 \mu \mathrm{~A}$ |
| GROUNDED EMITTER |  |  |  |  |
| Collector Bottoming Voltage (at $\mathrm{I}_{\mathrm{c}}=1.0 \mathrm{~A}, \mathrm{I}_{\mathrm{b}}=30 \mathrm{~mA}$ ) |  | $\mathrm{V}_{\mathrm{ce}}$ | -400mV* | - |
| Current Amplification Factor |  |  | Typical | Min |
| (at $\mathrm{V}_{\mathrm{C}}=-2 \mathrm{~V}, \mathrm{I}_{\mathrm{c}}=100 \mathrm{~mA}$ ) ... |  | $\bar{\alpha}^{\prime}$ | 200 | - |
| (at $\mathrm{V}_{\mathrm{c}}=-2 \mathrm{~V}, \mathrm{I}_{\mathrm{d}}=1.0 \mathrm{~A}$ ) . | .. | $\bar{\alpha}$ | 150 | 50 |

- -400 mV for OC 23 and OC 24 only. $O C 22=-600 \mathrm{mV}$.


MULLARD LIMITED Semiconductor Division Mullard House - Torrington Place London W.C. 1 - LANgham 6633

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## RCA



SSB-L1 Fixed Station. 60 watt ( 500 watt double sideband equivalent) eight channels $3-15 \mathrm{mc} / \mathrm{s}$.

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* Anti-static
* Freedom from curl and stretch

| Type | Tille | Size | Length approx. | Price in EMICASE | $\begin{gathered} \text { Price } \\ \text { without } \\ \text { EMICASE } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 88/3 |  | $3^{\prime \prime}$ dia. | $175{ }^{\prime}$ | - | 76 |
| 99/3 |  | $3^{*}$ dia. | $250^{\prime}$ | - | 9 |
| 88/3N | Message" | $3 \chi^{\prime \prime}$ dia. | $175{ }^{\prime}$ | - | 76 |
| 99/3N |  | $31^{\prime \prime}$ dia. | $250^{\prime}$ | - | 9 |
| 88/6 | 3"Junior" | $5^{\prime \prime}$ dia. | $600^{\prime}$ | £1 3 | £1 1 |
| 99/9 |  | 5" dia. | $850^{\circ}$ | £1 10 | £1 8 |
| 88/9 | 3'Continental" | 58" dia. | 850 | £1 10 | £1 8 |
| 99/12 |  | $53^{\prime \prime}$ dia. | 1200' | £1 176 | £1 15 |
| 88/12 |  | $7^{\prime \prime}$ dia. | $1200^{\prime}$ | £1 176 | £1 15 |
| 99/18 | tandard | $7^{\prime \prime}$ dia. | $1800^{\prime}$ | £2 126 | £2 10 |
| 88/18 | ssional" | $81^{\prime \prime}$ dia. | $1750^{\prime}$ | - | £2 17 |
| 99/24 | essional | $8 ¢^{\text {r dia. }}$ | $2400^{\prime}$ | - | £3 12 |

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[^9]
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## A new simultaneous

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The Ferrograph Series $3 \mathrm{C} / \mathrm{FN}$, illustrated here, is a simultaneous dual-channel instrument, using staggered heads, which offers special facilities to those engaged in medical, aeronautical and other scientific research. Besides the normal ability to record simultaneously time pulses on one track and intelligence on the other, it becomes immediately obvious that many forms of comparative measurement, stereophonic sound, or indeed, any two activities capable of being translated into electrical phenomena (within its
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Our wide experience in the design, manufacture and application of high precision magnetic tape recording equipment in Industry will be made freely available to you on request.

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Manufacturers are invited to write for details of our complete range of components


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> Frequency measurement up to $/ \mathrm{Mc} / \mathrm{s}$
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Output Capacity ..... 25W .............. 25W

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| Output Voltage ...... 6 V | ... 6 V |
| Output Capacity ..... 25W | - 25 W |
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## Standard resistance values

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Rating (total track........... $\frac{1}{4}$ watt at $55^{\circ} \mathrm{C}$
(subject to max. voltage not being exceeded)
Maximum voltage . . . . . . . . . . . . . . . . . . 500 V
Terminal resistance ............... $50 \Omega$ max.
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$\mathrm{Vh}=6.3 \mathrm{~V} \quad \mathrm{Ih}=0.55 \mathrm{~A}$

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Va2 210 to 320 V
$\mathrm{Vg} \quad-28$ to -65 V
Sx $\quad 20 \mathrm{~V} / \mathrm{cm}$
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Input amplifier band width-3dB at 2,500 \& 3,500 c.p.s.
Effective limiter range.......... 110 dB
Meter scaling-"Peak wow"... 0 to $+1 \%$ (centre zero)
"Wow and Flueter"... 0 to 1\% R.M.S. and 0 to $2 \%$
Crossover frequency............ 20 c.p.s.
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C.R.O. output frequency
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system of staff location

Additional Faciliťes

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". The results are really excellent. . Would you also let me have the various brochures that you have about this as another of my friends is very interested."
"...I am delighted with the results obtained from using the 'Symphony Stereophoner' on mv own equipment, and have decided to buy another for use in connection with a music group I am responsible for organising at the local Y.M.C.A."
". . . I have now given this instrument what I consider to be a fair test, by playing some very early L.P records, and I must admit that I was somewhat startled at the difference the "Stereophoner' makes. My first impression was that a film had been lifted from the surface of the record. The high soprano notes of artists-such as Madame Callas and Madame Tebaldi came out with ringing clarity, whilst with the deep bass notes a vibration was felt within the room itself. Truly, a remarkable little instrument."

- . 1 must say that 1 am highly pleased with the results. I shall certainly booaricast the claims of your 'Stereophoner.' It certainly does all if claims to do and the results are truly astonishing. There is no 'hole in the middle'-and it excels everything I've heard from what they call 'true stereo' (with its two amplifiers, two speakers and stereo pickup). The 'Stereophoner' gives one stereo for a fraction of the cost."
*. . It is an amazing little box of tricks and I am delighted with the results. My 'hook-up, (as I told you) was very efficient before-now, with this addition it is all that one could desire and the reproduction from radio, tape and records really excellent. I must admit I was a bit sceptical but your advertisement is justified by the efficiency of the magic box |"
"...I must say that 1 am very pleased with its effects, if certainly gives depth and one cannor pin-point, the emission of sound as coming from one speaker or the other."

A friend of mine recently purchased one and is astounded at the improvement in the quality of the sound from both his at the improvement in the qualit

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- Disks are permanent and cannot easily be erased or mutilated
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Send for details of MSS disk cutting accessories ; amplifiers; hot stylus unit; swarf collector ; mixer; control unit; microscope.


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*Other MSS disk cutter features include modulation indicator, radius compensator, press-button scrolling, cutter head muting switch, accurate cutter location in the recording head.
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T. E. IVALL

VOLUME 65 NO. 10

PRICE: TWO SHILLINGS

FORTY-NINTH YEAR OF PUBLICATION

NOVEMBER 1959

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Offices: Dorset House, Stamford Street, London, S.E. 1 Please address to Editor, Advertisement Manager.
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PUBLISHED MONTHLY (4th Monday of preceding month) by ILIFFE \& SONS LTD., Dorset House. Stamford Street, London, S.E.1. Telephone: Waterloo 3833 ( 65 lines). Telegrams: "Iliffepres, Sedist, London." Annual Subscriptions: Home and Overseas, $£ 115 \mathrm{~s} .0 \mathrm{~d}$. Canada and U.S.A., 85.00 . Second-class mail privileges aut horised at New York, N.Y. BRANCH OFFICES: BIRMINGHAM: King Edward House, New Street, 2. Telephone: Midland 7191, COVENTRY: 8-10, Corporation Street. Telephone: Coventry 25210. GLASGOW: 26b, Renfield Street, C.2. Telephone: Central 1265. MANCHESTER: 260, Deansgate, 3. Telephone: Blackfriars 4412. NEW YORK OFFICE: U.S.A.: 111, Broadway, 6. Telpphone: Digby 9-1197.

## 

The first advertisement in this series discussed the frame grid valve in general terms, and outlined the advantages which it brings in the tuner and i.f. stages of a television receiver. We shall now look at the i.f. stages in more detail, with particular reference to the needs of fringe areas.

to take the conventional EF80, with the EF183 retained in the first i.f. stage. With this new line-up; a $2 \cdot 0 \mathrm{~V}$ video output is obtained with $9 \mu \mathrm{~V}$ on Band III and $5 \mu \mathrm{~V}$ on Band I.
The circuit shown provides adequate a.g.c. on sound, and approximately 80 dB vision gain control without serious cross-modulation. Comparable performance is obtained with the PCF86 variant. Both versions are notably superior to conventional line-ups.

A circuit for an i.f. strip using the new frame-grid variable-mu EF183 is shown. It consists of a first i.f. stage which is common to sound and vision, followed by a second i.f. stage in each channel. Apart from component value changes, the only difference from normal practice is the use of $\pm 10 \%$ neutralising capacitors. When the strip is used with the frame-grid PCC89 in a cascode r.f. stage and the conventional PCF80 mixer, adequate gain is achieved for use in fringe areas without the addition of a further vision i.f. stage.
For Band III reception the maximum sensitivity required of a fringe area receiver is $20 \mu \mathrm{~V}$ for a picture of normal contrast level. Even for signals weaker than $20 \mu \mathrm{~V}$ a receiver of this sensitivity will give the best picture possible. (A higher sensitivity will produce excessive noise on the screen.) The Band I requirement is slightly less stringent and will in practice be easily met in a receiver which satisfies the requirements for Band III. With the strip shown, and with the PCC89 and PCF80 in the r.f. and mixer stages, $11 \mu \mathrm{~V}$ at the aerial will provide 2.0 V of video. A typical receiver with a conventional valve line-up (PCC84, PCF80, EF85 first i.f., EF80 sound i.f., EF80 vision i.f.) requires $63 \mu \mathrm{~V}$. Thus the conventional receiver fails to cover the required signal range for fringe areas, and it would need another i.f. stage. The frame-grid receiver, on the other hand, covers the range and has an adequate margin for production tolerances.
It will be noticed that the conventional PCF80 has been retained in the mixer stage. If the frame-grid PCF86 is substituted, then the second i.f. stages can be modified


## 



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| CURRENT SURGE SUPPRESSION and circuit protection | $\begin{aligned} & 1 \text { max }>1.0 \mathrm{~A} C Z 4, \mathrm{CZ} 2 \mathrm{~A}, \mathrm{CZ11,CZ12} \\ & 1 \text { max } 0.1 \text { to } 1.0 A, C Z 1, C Z 2, C Z 3, C Z 6, C Z 8 \\ & 1 \text { max <0.1A CZ10 } \end{aligned}$ |

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 Type 71* cartridge for instance, fits many popular arms and plays a key part in converting conventional players into stereo. ACOStereo Type 73 is an outstandingly successful universal cartridge for stereo, LP and standard records, extensively used in many leading instruments.

* AC.OStereo Type 71 is now fitted with a diamond stylus at no increase in price.


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## "BELLING-LEE" NOTES

## No. 10 of a Series

In No. 9 we mentioned various tests that have to be carried out on a component before it can be said to be suitable for use in an equipment that might have to serve in, say, the Navy, Army, or Air Force, in any part of the world, from tropical swamps to the Arctic, from the beaches to 65,000 feet, or higher. There may be special applications calling for special properties, for example, in missiles exceptionally high temperature may be met. Components in missiles must have a long "shelf-life." We hope they will never be used, but if, in ten years they go into action, they must not fail. Reliability over a long period is of prime importance. This means that contact surfaces must not tarnish, springs must not tire and seals must remain seals.
Components for use in atomic reactors may have to withstand intense radiation as well as intense heat-and they may not be accessible. Generally components come into two classes, those for professional use and those for domestic use. The greatest hazard to which domestic plugs have to stand up to is the sweeper.
Below we show photographs of some of the test equipment in constant use in our laboratories.

(At ove left). In the foreground is a slotted line used for voltoge standing wave ratio (V.S.W.R.) measurements up to $3000 \mathrm{Mc} / \mathrm{s}$.
(Above right). This device is used for the mechanical endurance testing of plugs and sockets. Designed and made in our own workshop, it is entirely automatic and will engage unipole components with a rotating action.
(Left). This piece of apparatus simulates altitudes over $100,000 \mathrm{ft}$. A selection of components is about to be lowered and sealed to the low-pressure chamter. High-voltoge stand-off insulators are available to enable voltoge breakdown tests to be carried out.

Advertisement of BELLING \& LEE LTD., Great Cambridge Rd., Enfieid, Middx.


## "BELLING-LEE" UNITOR

## PLUGS \& SOCKETS

These plugs and sockets were first designed for and type-approved by the Ministry of Supply as inter-unit connectors. The addition of covers and retainers make them suitable as cable connectors. Applications include guided missiles, electronic computers, aircraft, '"potted"circuits, communications equipment, electromedical equipment, radar equipment, atomic energy research, and television transmitting stations.
Unitors are available in $4,8,12$ and 18-pole assemblies, each including two large pins. Also in 25 -pole assemblies including four large pins.

Specification: D.E.F.532I.

## Current rating:

Small pins: 3 amp . each
Large pins: 10 amp . each
Max working volts: 500 V . peak
Insulation resistance:
Greater than 100 megohms at 500 V . after tropical exposure.
Contact resistance (initial):
Small pins: 2 milliohms Large pins: 1 milliohm
Contact resistance (after cycling): Small pins: 5 milliohms Large pins: 3 milliohms
Insertion and withdrawal force:
1 lb . per contact pair (max.)
Colour: Black
Finish:
Pins, silver-plated. Sockets, beryllium copper.
Solder spills, tin-dipped
Most "Belling-Lee" products
are covered by potents or registered
designs, or applications

## The very best connections

## ... secured by Plessey



SUB-MINIATURE COAXIAL CONNEGTGRS
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Designed for the matched impedance coupling of high frequency coaxial cables operating in the super high frequency bands, these connectors* have a working voltage of 650 volts Peak at sea level, and matched impedance coupling of 50 ohm lines is accommodated.

* have hard gold plated contacts on silver plate to give maximum performance with minimum voltage drop.



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* Plug pins and socket inserts are polythene shrouded to dispense with gaskets and ensure insert anchorage.
* Mismating is prevented by corner pins and corner sockets.
* Extreme simplicity of wiring, demands lessskilled operation than the orthodox methods of soldering pins in situ.

For further information, please write for Publication numbers 128 and 114.

## Plessey

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## Aspects of design

This is the Sixteenth of a series of special features dealing with advanced problems in television and radio circuit design to be published by Siemens Edison Swan. The Ediswan Mazda Applications Laboratory will be pleased to deal with any questions arising from this or other articles, the Seventeenth of which will appear in the December 1959 issue.

# 16 <br> DRIVE CIRCUITS <br> FOR SCANNING OUTPUT STAGESLINE DRIVE CIRCUITS 

## REQUIREMENTS

The drive circuit for a modern line output stage serves to generate a waveform which determines the timing and duration of conduction of the output valve. The drive circuit can take many forms determined mainly by economic considerations. Foremost among these considerations is whether the circuit is to be synchronised directly by line synchronising pulses or to be controlled by a phase detector in a "flywheel" synchronising circuit. With direct synchronisation we have to consider ease of synchronising with readily available synch signals and the possibit:'y of feeding back line frequency voltages to the frame scan stage via the synch source. If we decide on a flywheel circuit we have to be sure that it lends itself to frequency control by a slowly varying control voltage. High sensitivity of frequency to control voltage is not necessarily the thing to aim at because circuits with high sensitivity to control voltage usually show high sens.t'vity to unwanted interference such as hum and microphony. We should, rather, look for low sensitivity to valve ageing and supply voltage changes.

The waveform supplied to the output stage must fulfil the following requirements: (1) the output valve must be cut off rapidly and must remain cut off for the duration of the flyback interval, (2) because of the high voltage pulse on the anode of the line output pentode a much greater negative voltage is required for cut-off during flyback than during the rest of the trace. Accordingly line drive stages should be capable of driving the grid of the output valve to at least -135 volts during the flyback interval.

## Circuits available

The drive waveform is generated by first allowing a capacitor to charge exponentially through a high resistance from the H.T. line and then discharging it by a switching circuit on receipt of a line synchronising pulse. The switching ci.cut also determines the repetition frequency when synch pulses are absent. This circuit usually takes one of three forms: (1) a blocking oscillator, (2) a multivibrator or (3) a discharge valve (usually a triode) in which oscillation is maintained by feedback from the line output transformer. Basic representative circuits are shown in Figures 1, 2 and 3 respectively.

## 1. Blocking Oscillator

In this circuit (Fig. 1) a conventional blocking oscillator circuit generates the output waveform by drawing its pulses of anode current from the output capacitor $\mathrm{C}_{1}$. Between discharge pulses the capacitor charges towards H.T. through $R_{1}$. If we are to obtain a rapid cut-off of the line output valve the blocking oscillator must come to full conduction rapidly and hence the time of conduction must be fairly short. I ypical conduction times for the blocking oscillator are from two to three microseconds which means that after this time the voltage on the output capacitor begins to rise again and may be quite high by the time the voltage on the output valve anode has reached its peak. This explains why it is usually more difficult to ensure complete cut-off of the output valve with this circuit.


## 2. Multivibrator

A multivibrator, either anode coupled or cathode coupled can be designed so that one valve conducts for say $10 \%$ to $15 \%$ or the pernod and the other vasve tor $90 \%$ to $85 \%$. The valve with the short conduction period can, accordingly, be used as the discharge valve for the capacitor $C_{1}$ on which the druve wavetorm is formed (see Fig. 2). Between conduction puses the capacitor charges towards H.T. through the anode load resistor $R$, of the valve. The discharge valve is brought rapidly into conduction and conduction is maintained for a long period $(10-15 \mu \mathrm{~S})$. In this way we can achueve a fast cut-off of the output valve and also maintain the grid at the negative extreme of voltage for the whole flyback period.

FIG. 2


## 3. Feedback from Output Transformer

In thus circuit (Fig. 3) the positive pulse fed back from the output transformer during flyback drives the discharge triode $V_{1}$ hard into conduction ensuring rapid discharge ot $C_{1}$ and produces a flow of electrons into the grid capacitor $C_{1}$. After the end of flyback this accumulated charge on $C$, holds $V$, cut off whilst the output capacitor $\mathrm{C}_{3}$ charges towards H.T. through $\mathbf{R}_{1}$. The charge on $\mathrm{C}_{2}$ gradually leaks away through $\mathrm{R}_{1}$ until $V_{1}$ again conducts. The discharge currents are of longer duration than in the blocking oscillator so that it is easier to maintain cut-off during flyback. In this respect the carcuit is superior to the blocking oscillator but not so good as the multivibrator. It is often difficult to ensure self-starting with the circuit although it can be improved by including the feedback (shown dotted) from the screen grid of the output valve. There may also be large differences between synchronised and free running frequencies.


## Comparisons

The blocking oscillator and anode coupled multivibrator both lend themselves to control by a phase discriminator but the cathode coupled multivibrator is rather more sensitive to hum and microphony and is therefore not so suitable.

In directly synchronised circuits the blocking oscillator often causes difficulties because it presents a low impedance to the synch source and there is a high inductive transient at its anode after firing. These difficulties are not so severe in the multivibrator.

Suitable valves for line drive circuits are the Ediswan Mazda $6 ; 30 \mathrm{~L} 2$ double triode or the triode portion of the 30FL1.

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Anode Dissipation (watts)
.. $\mathrm{p}_{\mathrm{a}(\max )}$
Screen Dissipation (watts)

- $\mathrm{P}_{\mathrm{g}=(\max )}$

Anode Voltage (volts) $\quad . \quad . \quad . \quad V_{\text {gatmax }}^{\text {Screen }}$
250
250
Heater to Cathode Voltage (volts r.m.s.)

INTER-ELECTRODE CAPACITANCES (pF)
Grid 1 to Anode (with external can) .. $\mathrm{C}_{\mathrm{g} 1-\mathrm{a}} \quad 0.0017$
Grid 1 to Anode (without external can) $\mathrm{c}_{81} \cdot \mathrm{a} \quad 0.0019$
Anode to Earth (without external can) $\mathrm{C}_{\mathrm{g}} \cdot \mathrm{E} \quad 4.3$
Grid 1 to Earth (without external can) $\quad \mathrm{c}_{\mathrm{g}_{1} . \mathrm{E}} \quad 5.0$
Inter-electrode capacitances measured in fully shielded socket.
TYPICAL OPERATION

| Anode Voltage (volts) | $\mathrm{V}_{\mathrm{a}}$ | 175 | 175 |
| :---: | :---: | :---: | :---: |
| Screen Voltage (volts) | $\mathrm{V}_{\mathrm{g} 2}$ | 100 | 175 |
| Grid Bias Voltage (volts) | $\mathrm{V}_{\mathrm{g} 1}$ | $-1.3$ |  |
| Anode Current (mA) | $\mathrm{I}_{\mathrm{a}}$ | 12 |  |
| Screen Current (mA) | $\mathrm{Ig}_{\mathrm{g}}$ | 3.5 |  |
| Mutual Conductance (mA/V) | $\mathrm{gm}_{\mathrm{m}}$ | 4.4 |  |
| Bias to give Mutual Conductanc $100 \mu \mathrm{~A} / \mathrm{V}$ (volts) | $\mathrm{V}_{81}$ |  | -19.5 |
| Valve Anode Resistance $\left(\delta v_{a} / \delta i_{i}\right)(\mathrm{k} \Omega)$ | $\mathrm{r}_{5}$ | 400 |  |
| Input Capacity Working (Hot) (pF) | $\underline{\operatorname{cn}(\omega)}$ | 7.1* |  |
| Change in input capacity produced by biasing valve to cut off ( pF ) . . | $\Delta c_{\text {in }}$ | 1.7* |  |
| Input Loss at $38 \mathrm{Mc} / \mathrm{s}$ with cathode pins strapped (k $\Omega$ ) |  | 16 |  |

pins strapped (k $\Omega$ )
16
Note: If only one cathode pin is required it is recommended that pin 3 be used.

* Inter-electrode capacitance with holder capacitance balanced out.

MAXIMUM DIMENSIONS (mm)

$$
\begin{array}{ll}
\text { Overall Length } & 56 \\
\text { Seated Height } & 49 \\
\text { Diameter } & 22.2
\end{array}
$$

Characteristic Curves of Average Ediswan Mazda Valve Type 10 F18


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Maximum Peak.or Mean Collector/Base Voltage (Common Base Circuit)
(volts) -16
(volts) -35
Maximum Peak Collector/Emitter Voltage with Base driven to cut off (Common Emitter
Circuit) or with $\mathbf{R}_{\text {b.e }}<500 \Omega$
(volts) -35
Maximum Peak or Mean Emitter/Base Voltage (volts) - 12
Minimum d.c. $\beta$ at $I_{c}=-200 \mathrm{~mA}, V_{c}=-1 \mathrm{v}$
40
Minimum d.c. $\beta$ at $I_{0}=-50 \mathrm{~mA}, \mathrm{~V}_{0}=-1 \mathrm{v}$
Maximum Junction Temperature
Thermal Resistance in Free Air


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(volts) - 16
Maximum Peak or Mean Collector/Base Voltage (Common Base Circuit) (volts) -35
Maximum Peak Collector/Emitter Voltage with Base driven to cut-off (Common Emitter Circuit) or with $\mathrm{R}_{\mathrm{b}-\mathrm{e}}<500 \Omega$ (volts) - 35
Maximum Peak or Mean Emitter/Base Voltage (volts) -12
Minimum d.c. $\beta$ at $\mathrm{I}_{\mathrm{c}}=-200 \mathrm{~mA}, \mathrm{~V}_{0}=-1 \mathrm{v}$
Minimum d.c. $\beta$ at $I_{c}=-50 \mathrm{~mA}, \mathrm{~V}_{\mathrm{c}}=-1 \mathrm{v}$ 48
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THE COS8OR PRINTED CIRCUIT MODEL 701 K VHF/FM Radio Receiver kit ORIGINAL PRICE 15 Gns.

PRICE Kit is easily assembled and

* Weight including batteries $5 \frac{1}{2} \mathrm{lb}$. * Size only 8 in $x 8$ in $\times 4$ in

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B.S.R. Monarch U.A.8. 4-speed auto changer

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MAY BE
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 REISTORS-FULL RANGE 10 ohms-


 $2 \%$

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TYGAN FRET (Contemporary pat.), $12 \times$ LOUDSPEAKERS P.M. 8 ohms, 2 in. Elac., $17 / 6.3$ in. Goodmans, $18 / 6$; 5ln.
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12 v. operation Med. \& Long Waves


Valve Line-up: ECC85,
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Three Waveband and Switched Gram positions. Med. 200VHF/F'M 88-95 Mc/s. Phillp's Continental Tuning Insert Fith permeability tuning on FM and comblined AM/FM $\begin{array}{ll}\text { IF transformers, } \\ \text { and } \\ 10.7 \mathrm{Mc} / \mathrm{s} \text {. } & 460 \mathrm{Ko} / \mathrm{s} \\ \text { Dust } \\ \text { core }\end{array}$ tuning all coils. Iastest clrcuitry including AvC and
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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
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8 /- & V P 133 \\
26 / 6 & \text { VR22 (P }
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 EL33
EL38
EL41
EL42
EL8I
EL84
EM84
EM80
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EY5I
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[^14]

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(c) 12 months $\varepsilon 3 / 3 / 10$.
(d) The BRENELL Mk, V 3 Speed Deek. Deposit: $\varepsilon 10 / 6 /$ -
(o) The WEARITE MODEL $4 A$ Tape Deck. Deposit: $£ 12 / 4 /$ -
(0) The WEARI 12 months $£ 4 / 9 / 5$.............................................

STERNS MULLARD TYPE GG\%

## TAPE PRE-AMPLIFIER-ERASE UNIT

## NCORPORATING

NEW FERROXCUBE THE CORE PUSH-PULL OSCIL. LATOR and 3 SPEED TREBLE EQUALISATION by means of the latest FERROXCUBE POT CORE INDUCTOR.
PRICES COMPLETE KIT E 14.0 .0 ASSEMBLED AND 217.0 .0

Doposit $£ 3 / 8 /-$ and 12 months of $£ 1 / 4 / 11$. Assembled unit only.
ALSO AVAILABLE EXCLUDING POWER SUPPLY UNIT FOR
£11.15.0 and \&14.10.0 respectively. (Carr. and Ins. 5/-extra) Send S.A.E. for leafler or $2 / 6$ for Complece Assembly Manual WHEN ORDERING PLEASE STATE MAKE OF TAPE DECK TO BE USED We present this "Hi-Fi"' Pre-amplifier strictly to Mullard's specifieation etc., incorporating ONLY NEW HIGH GRADE COMPONENTS and the SPECIFIED NEW MULLARD VALVES. It comprises a COMPLETELY SELFCONTAINED UNIT, all components and valves being contained in a well ventilated Box-Chassis neatly finished in Hammered gold with a very attractively engraved PERSPEX FRONT PANEL.

## FOR PERMANENT HIGH QUALITY INSTALLATIONS

WE ALSO OFFER (excluding Case) the following
(a) The COLLARO MK. IV TAPE DECK and the MULLARD

TYPE "C" PREAMPLIFIER \& Power Unit assembled, tested H.P. Deposit $£ 7$ and 12 months $£ 2 / 11 / 4$
(b) As In (a) above but the Type " C " supplied as COMPLETE
(b) As In (a) above b
(c) The TRUVOX MK. VI TAPE DECK and the assembled

Type " C" Preamplifier and Power Unit
H.P. Deposic $£ 8 / 0 / 0$ and 12 months $E 2 / 18 / 8$.
(d) As above but the Type " $\mathbf{C}$ " supplied as complete KIT
(e) The BRENELL MK. V DECK and the assembled Type H.P. Deposit $£ 9 / 4 /-$ and 12 months $£ 3 / 7 / 6$.
(f) As above but the Type " C " supplied as complete KIT OF PARTS
(g) The WEARITE $4 A$ DECK with Type " $C$ assembled
235.0.0
£32.0.0
\&40.0.0
£36.10.0
\$46.0.0
£43.0.0
and tested $\dddot{H} . \mathrm{P}$. Deposit $£ i 1 / 4 / 0$ and 12 months $\varepsilon 4 / 2 / 1$.
(Carriage and Insurance on above quotes $10 /$ - extra.)
PLEASE ENCLOSE S.A.E. WITH ALL CORRESPONDENCE.
STERN RADIO LTD. 109 \& 115 FLEET ST., LONDON, E.C. 4

Telephone: FLEET STREET $5812 / 3 / 4$


YOU CAN BUILD A COMPLETE HIGH QUALITY RECORDER 4 LIKE THIS
FOR £39.15.0
(a) The COLLARO Mk. IV TAPE DECK with the assembled $£ \mathbf{3 4 . 1 0 . 0}$ and tested HF/TR3 Amplifier
£30.15.0
(b) As above but the HF/TR3 supplied as KIT OF PARTS... 30.15 .0 up the Deek Switch backs. We will do this for fl or supply a wiring diagram to the Home constructor.
(c) The TRUVOX Mk. VI TAPE DECK with the assembled and tested HFTTR3 amplifier
\& 239.10 .0
H.P. Deposit $£ 7 / 18 /-$ and 12 months $E 2 / 17 / 1 i 1$.
(d) As above but the HF/TR3 supplied as KIT OF PARTS
e) The BRENELL: Mk. V DECK with the assembled and costed HFTTR3 amplifier
236.0.0
\&45.0.0
H.P. Deposit 69 and 12 months $\mathrm{C3} / 6 /$ -
(f) As above but the HF/TR3 supplied as KIT OF PARTS..
\&41.10.0
g) The PORTABLE CASE illustrated here (E5), 1,2001t. EMITAPE (35/-), ACOS CRYSTAL MIKE (35/-), ROLA
$10 \times 6 \mathrm{in}$. LOUDSPEAKER ( $30 /-$ ) ALL FOR $10 \times 6 \mathrm{in}$. LOUDSPEAKER ( $30 /-$ ) ALL FOR
£9.0.0
Carriage and Insurance on each above $10 /$ - extra

## THE MODEL HF/TR3 TAPE AMPLIFIER

## Incorporating

3-SPEEDTREBLE EQUALISATION by means of the latest FERROXPRICE for COMPLETE KIT OF PARTS........ \$12/15/ FULLY ASSEMBLED $£ 16 / 10 /=$ ANDE PURCHASE: Deposit
$€ 3 / 6 / 6$ and 12 months at $€ 1 / 4 / 2$
A very high quality amplifier based on the very successful Type "A" design completed in the MULLARD LABORATORIES. ONLY NEW HIGH-GRADE COMPONENTS are incorporated including MULLARD MALVES and a GISON OU Magic Eye Recording Head indicator-Effective Tone Control-Monitoring and Extension Speaker Sockers-has own Power Supply and can be used as independent Amplifier for direct reproduction of Gram. Records or from Radio Tuner. Overall size $11 \times 6 \times 6 i n$.-Truvox-Collaro-or Brenellplease specify which. Send S.A.E. for leaflet or $2 / 6$ for Assembly Manual.

WE HAVE THE NEW 2 SPEED TWIN TRACK
TRUVOX Mk. VI Tape Deck in stock $£ 26.5 .0$ Deposit $\mathbb{\text { E5.5.0 }}$ It concorporates PRECISION REV. COUNTER and PAUSE CONTROL and operates at $3 \frac{3}{4}$ and $7 \frac{1}{2}$ inch $/ \mathrm{sec}$. speeds. It fully maintains the general high standard of all Truvox equipment, introducing refinements in appearance and ensures high quality recording, accurate ciming and editing. The very popular COLLARO Mk. IV "TRANSCRIPTOR" GRENELL Mk. Deeks are also available from stock.

## THE NEW B.S.R.

## "MONARDECK"

INCORPORATING A CORRECTLY MATCHED PREAMPLIFIER PRICE \&17.17.0 Deposit $E 3 / 12 /$ - 12 month
Designed to operate through the Pick-up
Sockers of the standard RADIO RECEIVER
Sockets of the standard RADIO RECEIVER
through which first-class results are obtained. It
consists of a single speed Twin Track Tape Deck
consists of a single speed Twin Track Tape Deck,
incorporating matched Preamplifier, and operates at $3 \mathrm{z} \mathrm{in} / \mathrm{sec}$. speed.
it uses 5 in . Tape Spools thus providing up to $1 \frac{1}{2}$ hours L.P. Tapes or I hour on the standard 5 in. Tapo ${ }^{1 \frac{1}{2}}$ hours' playing time on The equipment is supplied fully tested. Tape Spools.
attractive an existing plinth. It can therefore be dropped directly into and the Pick-up Sockets, for which purposes "floating ". leads suply incorporated on the Preamplifier.

## ghune OFFER!

Our supersensitive "FAMILY FOUR" T.R.F. Receiver for home construction. Covers Long and Medium Wavebands, is housed in very smart plastic table cabinet in Brown or Black. For A.C. Mains $200 / 250$ v. Comprehensive assembly instructions provided, including practical and theoretical diagrams, which are easy to follow and will enable you to complete this receiver which
will be the envy of your friends,
ALL NECESSARY COMPONEN ALL NECESSARY COMPONENTS ARE BEING OFFERED FOR LIMITED PERIOD ONLY AT THE REMARKABLE PRICE OF ONLY 79/6, plus $2 / 6$ p. \& p.
Instruction book available separately if you wish to study before purchase at $1 / 6$ post free

## NEW LOOK ECONOMY FOUR



Our very popular three valve mains T.R.F. receiver is now avaitable with a new De uxe cabinet with polished Walnut finish and Cream trimming (as illustrated). Brief Spec: Valve line-up 6J7, 6V6, and concact cooled rectifier. Ready drilled chassis, good quality 5 in . loudspeaker, Special Denco Coils. Covers Medium and Long Wavebands. Overall dimensions: 12 in. $\times 6 \mathrm{in} . \times 5$ in high. A.C. $200 / 250 \mathrm{v}$. Simple construction with guaranteed results. Easy to follow practical and theoretical diagrams supplied, All necessary components, down to the last nut and bolt, are offered at a SPECIAL INCLUSIVEPRICE OF $£ 5 / 10 /-$, plus $5 / \mathrm{p}$. \& P. Instruction book available separately $1 / 6$, post free. Aiso available with plastic cabinet in IVORY or BROWN if preferred at ONLY $£ 5 / 5 / \%$, plus $p . \& \mathrm{p}$.
PRINTED GIRCUIT DE-LUXE SUPERHET
Housed in any of the above cabinets and employing the latest circuitry, assembly technique and miniature valves. Incorporates ferrite aerial and covers Medium and Long Wavebands. All required components at special inclusive price of $£ 7 / 19 / 6$ (or $5 /$ - extra for new style cabinet) plus $5 \% \mathrm{p}$. \& p. Instruction book with full description, itemised price list etc., available separate at $1 / 6$ post free.

THE NEW LOOK RAMBLER PORTABLE


This wonderful little Medium and Long wave battery superhet incorporates IR5, IT4; IS5, 3V4 miniature valves, 5 in speaker and frame aerial Housed in smart two tone Red/Grey cabinet. All required com$\begin{array}{lll}\text { ponents at only } \\ £ 7 / 7 / 0 \text { plus } 2 / 6 & \text { p. } \&\end{array}$ $67 / 7 / 0$ plus $2 / 6$ p. \& p. or with the latest " 96 range" valves at $£ 7 / 15 / 6$ plus $p$. batteries AD35 (1/6), B126 (9/-). Full descriptive instruction book with itemised price list, diagrams, etc. available separately at $1 / 6 \mathrm{~d}$. post free. MAINS UNIT FOR RAMBLER PORTABLE. Fits into battery compartment. A.C. 200/250 v. All required components at ONLY $47 / 6$ plus $1 / 6 \mathrm{p} . \& \mathrm{P}$. or assembled and tested at $£ 3 / 5 /-$ plus p. \& p. (Also suitable for many other portables.)

## LEADING THE

## In equipment for

THE CONSTRUCTOR and HI-FI ENTHUSIAST SEND STAMP FOR FULL LIST including F.M. Tuners, Receivers, Amplifiers, Stereo Amplifiers, Tape Pre-Amplifiers, Transistor Porzables, Crystal Receivers, Battery Charger, Baby Alarm, etc., etc.
NOTE: ALL components supplied, including valves (even if surplus types) are guaranteed to be BRAND NEW ! I !

## JASON "EVEREST" TRANSISTOR

 We are prout to be able to offer two new Jason all-transistor portable receivers designed to provide the highest possible standards of per formance in theirclass. These are
the "Everest-6" and "Everest-7" both covering Medium and Long wavebands, and incorporating ferrite rod aerial and special top grade loudspeaker. A printed circuit is employed and Mullard transistors are used throughout. An excellent quality output of 500 mw . is obtainable. Housed in a most attractive easily carried case with handle, finished in Blue/Grey "Vynaire" with Gold trimmings. The Everest-7 is exceptionally sensitive and well suited to car use (aerial socket provided) and has improved AVC action due to the additional tage. All necessary components for building these wonderful receivers are offered at the these wonderful receivers are offered at the EVEREST-6 (six transistor) $£ 13 / 19 / 9$, plus $3 / 6$ EVEREST-6 (six transistor) $¢ 13 / 19 / 9$, plus $3 / 6$ P. and P. EVEREST-7 (5even transistor), ¢ $5 / 18 / 9$, plus $3 / 6 \mathrm{p}$. and $p$. Fully descriptive booklet with comprehensive assembly instructions available separately if required at 3/6 post free.

COSSOR BATTERY ELIMINATOR Type MU2 Sultable for conDry Battery receiver, employing 1.5 v . H.T and modern low consump A.C. Mains oper ation, $200 / 250 \mathrm{v}$ Contained in two separate
 units (L.T. \& H.T.) which are idencical in size to the AD35 and B126 (or equivalents) bacteries. Fully stabilised L.T. supply of 1.5 v , at $125 \mathrm{~m} . \mathrm{a}$, H.T. 90 v , at $10 \mathrm{~m} . \mathrm{a}$. These units are BRAND NEW and packed in manufacturer's original carton. UNREPEATABLE PRICE OF ONLY $37 / 6$, plus $1 / 6$ p. \& p. (List price 3 gns. ) $37 / 6$, plus $1 / 6$
Guaranteed

SUPER TRANSISTOR/CRYSTAL - RECEIVER

Our amazing extra sensitive transistor/crystal
receiver for local stations, with buitt-in ferrite receiver for local stations, with built-in ferrite aerial, can be supplied for home construction
at ONLY $27 / 6$ for all necessary components inc. pen eorch batt. P. \& P. 2/-extra. Simple to inc. pen torch batt. P. \& P. $2 /$-extra. Simple to
construct, excellent in performance, most attractive in appearance.
Instruction envelope available separately if required at $1 /$ post free. Suitable Deaf-aid ear piece for above, 12/6.

## THE NEW JASON FM TUNER

The latest addition to the impressive JASON range, and like all JASON equipment can be depended upon for OUALITY, RELIABILITY and PERFORMANCE.


Incorporates the very latest features in design to ensure simplicity of operation and faultess performance. Housed in smart metal shelf mounting cabinet in pastel green with grey plastic dial. Built-in power supplies enable connection to any amplifier or radio fitted with Plick-up sockets, without complication. Two versions are available, i.e., Standard or Fringe Area. ALL NECESSARY COMPONENTS SUPPLIED AT SPECIAL INCLUSIVE PRICE OF: STAN. DARD TUNER $68 / 19 / 6$ : FRINGE AREA TUNER £ $10 / 19 / 6$, both plus $3 / 6$ p. \& p. Comprehensive Assembly instructions with full description and itemised price lists are available separately if required at $2 / 6$ post

Full range of JASON equipment available ex-stock

PRINTED CIRCUIT CAR RADIO


We are proud to be able to offer this New type Car Radio employing up to the minute circuitry, special 12 volt valves and transistorised output stage,
The highest degree of sensitivity is The highest degree of sensitivity is
assured by the incorporation of Perassured by the incorporation of Per-
meability Tuning and a tuned R.F. meability Tuning and a tuned R.F. bands. NO VIBRATOR PACK IS REQUIRED. This is a really compact receiver that will fit any car. Comprehensive assembly instructions are provided with all necessary components, including valves and transistor at a plus $3 / 6 \mathrm{p} . \& \mathrm{p}$. Instruction booklet wich itemised price list, full description dimensions, etc., available separately at $1 / 6$ post $f r e e$.
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COSSOR KITSI A unique opportunity to obtain a firt-elass ampllier and/or the latest type VHFIFM receiver ot the most reasonable price ever.

COSSOR AUDIO AMPLIFIER KIT 562K. This excellent amplifier supplied in kit form in manufacturer's original presentation carton comprising: Pre-assembled printed-circuit board, valves: 6V4, 68 Q5, EF86 output transformer, two loud-speakers, 4 in . circular and
$10 \times 6$ in. elliptical, wiring wire, nuts, boits, $10 \times 6$ in. elliptical, wiring wire, nuts, boits, attractive escutcheon and contro knobs, mounting brackets and fully illustrated assembly Instructions. With negative feedback incorporated, and the high performance loudspeakers provided, a really high quality output
is assured. Suitable for use with radio tuners. is assured. Suitable for use with radio tuners, microphone, or gramophone units. For A.C. 200/250v. operation, BRAND NEW AND
COMPLETE AT ONLY $£ 5 / 19 / 6$ plus $3 / 6$ P. \& P. (List price E9/15/-.)

COSSOR VHF/FM RECEIVER KIT 70IK. A first-class receiver of the latest type for the reception of B.B.C. VHF/FM programmes, and suitable for use on AC or DC mains supply, supplied in kit form, in manufacurer's original presentation carton, comprising: printed circuit (with all connections elearly marked), 6 valves: UCC85, UF89,
UF89 UABC80, UL84, UY85. AII necessary components including nues, bolts, wiring wire, solder, etc., and an excellent quality Goodmans 10 in. $\times 6$ in. elliptical loudspeaker. A fully illuselliptical loudspeaker. A fully ilusprovided with the aid of which the receiver can be completed in approx. COMPLETE ATONLY E8/19/S plus $3 / 6$ P. \& P. (List price $E 15 / 5 /-$.)

## RECORDER AMPLIFIER

(Well known manufac-
curer's surplus.) This is curer's surplus.) This is a brand new
amplifier de-
signed for use
with a famous
wire recorder.
A simple modi-
fication is all
that is required to
make this unit ideal
for use with any Tape
Deck. Specifications: Valve
line-up 7C5, 2AU7, 6BR7,
68R7, 6X4. Neon Record Leve Indicator. Conerols: Volume/Record Level. Tone Control, Record/Playback Switch. High and Low level inputs for Mike and Radio. External Speaker Socket. Built-in Sin. Loudspeaker with High Flux magnet: Separate Power Pack. Dimensions: Amplifier 5 tin. H. xllif. W. x 2 fin . D. Power Pack: $6 \frac{1}{2} \mathrm{in} . \times 6 \mathrm{in} . \times 5 \mathrm{in}$. High (overall). Full modification details are supplied. Price. £6/19/6. P. \& P. $3 / 6$.
 ilt fittings of $\boldsymbol{E} \mid$. Send stamp for furcher decalls.

## LIMITED SUPPLIES OF THIS FINE AND POPULAR CABINET

 instantly recognised as being of leading High Quality manufacturers' stock, this trolley-type cabinet is finished in polished dark walnut. Can easily be adapted to accommodate tape recorder, amplifier, radiogram, etc., etc. Exrernal measurements: 24 EXin. $\times 16 \mathrm{in} . \times 29$ in. The whole is mounsed upon "easy run" castors. Subiect to beins unsold E5/19/6, plus 15/C. \& P.
## Collaro Mark iv Tap

ranscriptor Dec De Luxe Cabinet with CollaroMike(orsimilar)

TOTAL 15/- extra. Full assembly instructions provided. Note: We shall be pleased to wire the tape deck switches at extra charge

A SUPERB TABLEGRAM
CABINET! (Limited stocks CABINETI (Limited stocks only.) This beautful cabinet
finished in highly polished dark walnue with gold poliping. wingle record unit single record unir, amplifier and 7 in . $\times 4 \mathrm{in}$. elliptical loudspeaker. (The motor-board is supplied cut for the Garrard
4 SP player, but is easily 4SP player, but is easily
modified for the Collaro modified for the Collaro
Junior, B.S.R. TU9 etc.). Overall dimensions are: $15 \% \mathrm{in}$. wide $\times$ $13 \mathrm{in}, \times 7$ tin. high. Clearance above motor-board (inc. Iid) 3 fin . Clearance below motor-board $3 \frac{1}{2} \mathrm{in}$. This is a most attractive proposition for anyone who requires small but good quality equipment. Priced at ONLY $5 \% / 6$ plus $6 / 6$. (Do not miss this ourstonding bargoinlI!) Also available to accommodate autochanger at $79 / 6$ plus $6 / 5 P$ \& \& $P$.

PORTABLE GRAM AMPLIFIERS RC2A. Small PRINTED CIRCUIT single-valve high-gain amplifier for the smaller type of porrable. Employs latest type ECL82 valve. Full details on request. Price 59/6 plus $2 /-\mathrm{P}$. \& $P$. RC3A. A superior quality 3 -valve amplifier employing EZZ0, EL84 and ECC83. With separate bass and treble controls. Price E3/19/6 plus 2/6 P. \& P. O.P. Transformer available at $4 / 6$ extra. table, tape deck, amplifer etc. Te
for lliustrated leaflets of full range.


## A QUALITY RECORDER

 FOR 39 GNS. $8 \times 6$ in. loudspeaker $\$ 1100$ ,200ft. EMI tape OUR SPECIAL INCLU-SIVE PRICE ONLY 39 GNS. if all items purchased together. Terms: 64/19/- dep. and 12 monthly payments of $\varepsilon 3 / 6 / \%$. C. \& P.

## EXTRA SPECIAL OFFERII

## A small three-valve PORTABLE

 RECORD-PLAYER AMPLIFIER mounted on baffle $12 \times 7 \mathrm{in}$, with High Flux $6 \frac{1}{2}$ in. Loudspeaker, Valve line-up ECC83, EL84, EZ80. Incorporates separate bass and treble controls. Max. output 3 watts. Will match all types of high impedance pick-up. Ready to use, $65 / 12 / 6$ plus $3 / 6$ P. \& P. NEW STYLE CABINET finished in two-tone Leatherette. Will accommodate above Amplition, also me without modilcaEquipment. Overall size $18 \times 13 \frac{1}{2}$ $x$ Bfin. Fitted with carrying handle, $63 / 9 / 6$ plus $5 /-\mathrm{P}$. \& P . NOTE. If both items pur. chased cogether they will be supplied at a special inclusiveprice of $E 8 / 7 / 6$ plus $6 / 6 \mathrm{P} . \& \mathrm{P}$.

RECORD PLAYERS $\rightarrow$

## THE LATEST COLLARO

 "CONQUEST"' Stereo 4 -speed auto-changer in cream with Stereoinsert. Brand new, fully insert. Brand new, fuly
teed. $8 / 19 / 6$. P. \& P. $3 / 6$. MONAURAL "CONQUEST" with Studio "O" insert, ET/19/6, wius P. \& P. $3 / 6$.
B.S.R. UA8 MONARCH. 4 -speed Mixer Autochanger complete with curnover crystal insert and sapphire styli. Few only, now at $£ 6 / 19 / 6$ plus $3 / 6$ P. \& P. Brand new and fully guaranteed.
GARRARD RC. I2ID MK.II STEREO MONAURAL 4-SPEED AUTO. CHANGER. Complete with GC8 plug-in crystal head and sapphire styli plor monaural records. Brand new fully guaranteed. Limited stocks. ONLY Ell/0/6, plus 5/-P. \& P. NOTE: Garrard L.P. Stereo plug.in head for above available as optional extra for $\varepsilon 2 / 1 / 9$ inc. able as optional extr
P.T. Terms available. P.T. Terms available.
GARRARD RC120/4

GARRARD RC120/4H. 4-speed autochanger with GC2 insere. Brand new. fully guaranteed. $69 / 19 / 6$. P. \& P. 3/6.

## COLLARO JUNIOR. A-speed

turntable and pickup comp picte with cartridge and sapstyli, StyECIAL OFFER at only 75/- plus $2 / 6 P$. \& P. or TURNTABLE and MOTOR only at $52 / 6$ plus $2 / 6$ P. \& P. PICK. Only at $52 / 6$ plus $2 / 6$ P. \& P. PICK.
E.M.I. 4-SPEED STEREO SINGLE RECORD UNIT. Complete with Stereo Head and Sapphire Styli. Brand New and Fully G'teed. ONLY ES/19/6 plus $3 / 6$ P. \& $P$ whilst stocks last. VERDIK "QUALITY $10^{\circ}$. superb Hi-Fi amp. and preamp. with 10 watt push-pull ultra linear output. Beautifully finished in grey-green stove enamel. Controls: Bass, Treble, Volume and inpur selection for Radio, Mike, Tape, Std. and L.P. Records. Limited stocks at only $£ 14 / 19 / 6$ plus $7 / 6$ P. \& P. (List 20 gns .). Terms available.
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CABINETS. We carry large stocks of cabinets to suit all types of equipment at prices ranging from $45 /$. Suitable for housing all types of turntable, tape deck, amplifier etc. Terms available if required. Send stamp

SPECIAL CELESTION $8 x$ 6in., elliptical high flux loudspeaker 30/- plus 1/- P. \& P.
VERY ATTRACTIVE PORTABLE CABINET in Red and White polka dot for accommodating the above items and ancillary
equipment, $75 /-$, plus $5 /-$ P. \& P.

## DECCA PORTAGLE AM-

 PLIFIER. As supplied in famous DECCAMATIC ili. Complete with small cream knobs. Full range tone and volume controls. Employs ECL82 valveSize $3 \times 3 \frac{1}{2} \times 8 \neq \mathrm{in}$, Only 5970 Size $3 \times 3 \frac{1}{x} \times 8$ ?
plus $216 \mathrm{P} . \& \mathrm{P}$.

NOTE. Supplied post free if all above items purchased cogether.

SEE OVER FOR MORE
 BARGAINS $\rightarrow$

## JASON TEST EQUIPMENT


ruction. AUDIO GENERATOR AGIO. Covers rom $10 \mathrm{c} / \mathrm{s}$, to $100 \mathrm{Kc} / \mathrm{s}$, in four ranges. Max output 10 volts. Min, output 100 microvoles. Square wave output with excellent rise time makes this generator very useful for checking all Audio equipment. Housed in attractive metal shelf mounting case measuring $11 \frac{1}{2} \mathrm{in}, x$ $6 \frac{1}{3}$ in. $\times 5$ in. high. All necessary components 6 inin. $x 5$ in. high. All necessary componenis of $\mathrm{\varepsilon} 14 / 5 / \mathrm{s} /$, plus $3 / 6 \mathrm{p}$. and p .
of $£(4 / 5 /-$, plus $3 / 6 p$. and $p$.
ully descriptive booklec with comprehensive assembly instructions available at $2 /$-post free.

OSCILLOSCOPE OGIO. This is a general purpose Oscilloscope based on a "Mullard" circuit employing a DG7-32 3in. cathode ray tube. A sensitivity of 100 mierovolts fer $\mathrm{c} . \mathrm{m}$. with a band width of $2 \mathrm{c} / \mathrm{s}$. to $2.5 \mathrm{mc} / \mathrm{s}$. makes this a useful unit for T. Y. servicing as well as audio amplifier checking. Housed in smart netal case complete with earrying handle. All necessary components avaipice booklet with comprehensive assembly instructions available separately at $3 / 6$ post free.

```
CLYNE CATHODE RAY OSCILLOSCOPE for Home Construction
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The latest addition to our comprehensive stocks of quality equipment for the constructor. This is an exceptionally sound and robust instrument of the most versatile type, that will be a boon to the seriously minded amateur, serviceman or constructor. Specifications: 8-Range Time Base, switched from $20 \mathrm{c} / \mathrm{s}$ to $160 \mathrm{Kc} / \mathrm{s}$. Y-Plate Ampli$20 \mathrm{c} / \mathrm{s}$ to $160 \mathrm{Kc} / \mathrm{s}$. Y-Plate Ampli -
fier has a sensitivity of 50 mV , and fier has a sensitivity of 50 mV , and
frequency response of $20 \mathrm{c} / \mathrm{s}$ to frequency response of $20 \mathrm{c} / \mathrm{s}$ to
$600 \mathrm{Kc} / \mathrm{s}$ with a gain of 150 . A call$600 \mathrm{Kc} / \mathrm{s}$ with a gain of 150 . A call-
brating voltage of $6.3 \mathrm{~V}, 50 \mathrm{c}$ 's is brating voltage of 6.3 V .50 e is is
provided. Employs ECR30 2 I In . provided. Employs ECR30 $2 / 1 \mathrm{in}$. 2/ECFBO, I/EF91, I/EZ35, $6 \times 5$. Controls: X-shift, Y-shift, Focus,
Width, Brilliance, ON/OFF. Time
Base Frequency (Fine) Time Base Frequency (Course). Sync. Selector. Sync, Amplitude. Y-input selector. X-input selector. Amplifier Gain. Operates from $200 / 250 \mathrm{v}$. or 110 v . A.C. Mains. All required components for the construction of this wonderful instrument, including comprehensive assembly instructions, available at a SPECIAL INCLUSIVE PRICE OF ONLY $\mathbb{E} / 2 / 19 / 6$ plus $5 /$ - carriage and packing.

## A HIGH QUALITY 4WAVEBAND AM/FM CHASSIS

## By famous manufacturer). BRAND NEW

A really first-class AM/FM Chassis, which is in great demand by the discerning enthusiast. Brief spec.: 9-valves, ECC85, ECH81, EF89, EABC80, 2/EL84, ECC83, EZ8I, EM34. Covers Long, Medium, Shor and FM Wavebands. Power pack and output stage (Push-Pull) mounted on separate chassis. Independent Bass and Treble Controls. Volume Control on flying lead. Available with Vertical or Horizontal edge lit dial. Flywheel tuning. Facilities for quality tape recording or playback. Pick-up and extension speaker sockers provided. PRICE WHILST STOCKS LAST ONLY $£ 17 / 19 / 6$, plus $5 /-$ p. and P. Terms: Deposit $39 / 6$ and 12 monthly payments of $29 / 4$.

## A.M. GRAM CHASSIS SPECIAL!

(By famous manufacturer)
This special offer chassis is being offered for a limited period only and represents the best possible value for money. Spec.: 3 wavebands, Long, Medium and Short. 5 miniature valves-6C7, 6F15, 6LD20, N108, Ul07. Attractive vertical glass dial ( $13 \mathrm{in} . \times 3$ in.) in red, green and gold on black background. Two-speed dial drive. Full range tone control. Output approx. 4 watts to mateh 3 ohm speaker, For A.C. mains $110 / 250 \mathrm{~V}_{\text {. }}$ Overall size 13 in . $\times 6 \frac{1}{2} \mathrm{in}, \times 6 \frac{3}{4} \mathrm{in}$, high. WHILST STOCKS LAST, E//19/6 ONLY, plus $7 / 6$ P. \& P.

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No. 17 Mk. II TRANSMITTER/
RECEIVER. Bulle into strong wooden eabinet 15 in . $\times 14 \mathrm{in}, \times$ in. Complete with headphones and microphone. Range 5-8 miles with simple aerial.
Freq. range $44-61 \mathrm{mc} / \mathrm{s}$. ( $5-7$ metres) ses standard 120 V. H.T. and 2 v . plete with full operating instrucplete with ull operating instruc-
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12in. BAKERS SELHURST LOUDSPEAKERS 15 ohms, 15 watt, $30.14,000$ eps. Brand new. 4/10/-. P. \& P. 3/6.
6 VOLT VIBRATOR PACK. Ex-W.D. Output 140 r.@ 30 ma . Fully smoothed. Size: 6 fin. $\times$ Sin. $\times 2$ tin. As ne
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SEE ALSO PAGES 156-157

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Type A. Low Lesisage windings, Optloma! Boont $25 \%$
and $50 \%$. Tapped msina primaries
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OUR LATEST SUPERIOR PRODUCT. TyPE AR
Eigh Quality. Low eapacity. $10 / 15 \mathrm{pt}$. $16 / 6$
Optional boost $25 \%, 50 \%, 75 \%$.
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WIREWOUND POTs, 4 w
Standard size Pots, long Standard size Pots, long spindle High Grade, A
Values 100 okms to 50 K 616: 100 E. ${ }^{716}$. ${ }^{71}$.
 WW EXT, SPEAKER
CONTROL $20 \Omega$ 3/\%. O/P TRANSFORMERS. Heavy Duty 50 mA., 4/6. Multitite push-pull, 76 , Miniature 3 V4, etc., 4 6. Hygrade Pusb-pull 10 watts, 15/6. MULLARD " 510 " 6 k or 8k 30 . 10 R 150 ma . 14/.
MAINS TRANEFORMERS 200,250 7 . A.
$\begin{aligned} & \text { tapped } 4 \text { v. } 4 \text { a. Rectiter } 6.3 \\ & \text { v. } \\ & 1 \text { a., tapped, } \\ & \text { s.v. }\end{aligned}$

MIDGET, 250 च. 45 mA . 8.3 F .2
3 MALJ, $250-0-250100 \mathrm{~mA} ., 6.3 \mathrm{v}, 3.5$ n
 GEATER TRANS., 8.3 v. 1 , a, 7/6. 3 amp.
GENERAL PURPOSE LOW VOLTAGE. Outpu 6, 8, 0, 10. 12. 15. 18. 24 and 30 ซ. at 2 A. $22 / 6$ ALADDIN FORMERS and cores, $\frac{\text { in }}{6 \text { dif }}$ Iin. 10 N .3im or tin $x$ llin with core
 TYANA. Midget soldering Iron, 230 จ. $40 \mathrm{~W} ., 16 / 9$
REMPLOY INSTRUMENT IRON, 230 v. $25 \mathrm{w}, 17 /$ REMPLOR INSTRUMENT $1 R O N, 230 \mathrm{~F} .25$ W., $17 / \mathrm{e}$
MADS DROPPERS. $3 \times 1$ in. Three Adj. Sliders, .3 sm. MADNs DROPPERS. $3 \times 1!$ in. Three Adj. Sliders, 3 smp
750 ohms, $4 / 3.2$ amp., $1,000 \mathrm{ohm}, 4,3$.
 per $100 \mathrm{~h}, 2$ way, 6 d . per toot,. 3 way, 7d. per loot.

CRYSTAL MIKE INSERT by Acos $6 / 6$

$\begin{array}{llllll}\text { MIKE TRANSF. } & 50: 1, & 3 / 9 & \text { ea,. } & \text { 100:1 } & \text { Potted, } \\ \text { LOUDSPEAKERS } & \text { P.M. } & 3 & \text { OHN. } & \text { 5in., } & \text { Rola } \\ 17 / 6 .\end{array}$ Gin. $\times$ tin. Rola, 18\%. 7in. $\times 4$ in. R.A. $21 \%$ $10 \mathrm{in} . \times 6 \mathrm{in}$. Rola, $27 / 6$ Rola, 21/ 8in. Plessey, $19 / 6$ HI-FI TWEETERS, 4in. 25/a. 21/\% 12in. Plessey, $30 /=$ 12in. Baker 15 mt . 3 ohm and 15 oh modols 105
1 isin. Beker loam suspension 15 w. 15 ohm , £
12in. Baker 15 ohm Plessey 10 wi.. $45 /$ -
1.F. TRANSFORMERS $7 / 6$ pair $485 \mathrm{ke} / \mathrm{s}$. alug tuning ministure can $2 \mathrm{t} \times 1 \times 1 \mathrm{in}$. High $Q$ and good bandwidth By Pye Radio. Data sheet supplifed.
Wearite M800 L.F. Miniature $465 \mathrm{ke} / \mathrm{s}$. $12 / 6$ pair
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CEYETAL DIODE G.E.C. 2/- GER34, $4 /$ /. 40 Circuits, $3 /$ H.R. HEADPRONE3, 4,000 ohms, brand new, $16 / 6$ pair 8WITCH CLEANER FInid, squirt spout, $4 / 3$ tin. TWIN GANG CONDENSERS. 365 pl. Mnnature, 1 in $\times 1+i n . \times 1 / \mathrm{in} .10 /-.0005$ Standard with trimmers $100 \mathrm{pf} .150 \mathrm{pf} .7 \mathrm{~F} /-$. Solid dielectric $100,300,500 \mathrm{pl}, 3 / 6$ VALVE BOLDERS. Pa. int. Oct. 4d. EFEO, EA5O, 8d B12A, CRT. 1/3. Eng. and Amer. 4, 5, $6,7 \mathrm{pin}, 1 / 2$,
MOULDED Marda and Int. Oct. 6d., B7G, B8A, B8G, B8A 9 d B7a with oan. 1/6: B12A, 1/3. B9A with can, 19
 5 in. $10 /$-. Tygan 54 in . wide. 10/- It. 27in. wide, $5 /-\mathrm{It}$ Eamples, S.A.E, SWITCEES.
e p. 2-way, 3 p. 2-way, short spind
p.

 3 wafor 16'- 4 waler 19/6: 5 waier $23 / 6 ; 6$ water $28 / 6$ TOGGLE SWITCHES S.P., $2 /-$ - D.P. $3 / 6$; D.P.D.T. $4 /-$ MORSE KEYS, qood quality. $2 / 6$.
SOB-MINIATURE ELECTROLYTIS ( $15 . v.), 1,2,4,5,8$, 95, 50 midd. 3'- B8eh

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pull. $10 /=$ xato Goltop Power Vib/iop, up to 10w with bast siak 20/.


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W. $16 \mathrm{~m} .-50 \mathrm{~m}$.
five valve M. W. $200 \mathrm{~m} .-550 \mathrm{~m}$ W. $800 \mathrm{~m} .-2,000 \mathrm{~m}, \quad$ ECH81, EF89; EBC81
 Feedback, 4.2 watts. Chrssis 13 the $x$. 5 in Nogativi Glass Dial Size $10 \times 4$ 4m, horizontal or vertleal. 2 Pilo Lamps. Four Knobs. Wainat or Ivory, alugned at

- 10

BRAND NEW £9.10.0 Garr. 4/s


SUPERIOR FM-AM MODEL Six Mallard Valves, ECC85. ECH81. EF89. EABC80. EL84 EZ800. W. H.F. $108-87$ Me/s. Med. $190-650 \mathrm{~m}$. Lonk 1000 1900 m. Gram input. Ready for use. A.C. Mains 200
250 v . Isolated ohassis. Output point for use as $\mathrm{Hi}-\mathrm{F}$ Tuner, is month guaraniee. Circuit supplied.

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+ GARRARD 4-SPEED RECORD CHANGER8 RC121/D MKII MODELS $t$ Brand new and fully guaranteed 12 months AUDIO PERFECTION
Designed to play 18, 33, 45, 78 r.p.m. Recorde 7io., 1012. 12in. Witb plug-to NORMAL HEAD
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LATEST COLLARO AUTOCHANGER


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Suitable player cabinets (uncut boards)
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 MODEL TAMK II 88 - 10 \{ Serere Heads MODEL 4 HEt18
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 Cong shidgot size: ong spiadio. Guaras. weed year. All values No Switoh. D.P. Sw. 3/- or Log Tracks84 cänía Lioaxıal Poal Id. per yapd Seml-air spaced, tha dis
Ideal Hanl 111 . $6^{\text {d. }}$ $0_{y}$ AIRSPACED.... 1/- 7 d COAXIAL PLUGS …...1/ LEAD SOCKETS ANEL SOCKETS …1/- OOTLET BOXES .... 4 BALANCED TWTN FEEDER por Yd. $6 d .8$ or $80 \Omega$ or
TWLN SCREENED BALANCED FEEDER 16 yd., 80 okm
ALUMINIUM CHASsls. 18 3.wok. Plan, and Wlect with a aides, riveted with 2 hn gides, $x$ in aners and latice finag hoves. With 2 亿ın. sides, $7 \times 4 \mathrm{in}, 4 / 6: 9 \times 7 \mathrm{in} .5 / 9: 11 \times 7 \mathrm{~mm}$.
$69: 13 \times 9 \mathrm{in} ., 8 / 6: 14 \times 11 \mathrm{in} ., 10 / 6: 15 \times 14 \mathrm{in}, 12.6$ 6 6: $18 \times 9$ in., $8 / 6: 14 \times$
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BLACK CRACKLE PAINT. AIT drying, 3P.V.C. CONN. WIRE, A colours, single or stranded. pe. 7d CORED SOLDER RADIOGRADE 4 d . Jd., the 2/6

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 $50 \mathrm{~mA} .7 / 66$, $10 \mathrm{~mA}, 8 / 6 ; 85 \mathrm{~mA} .9 / 6 ; 200 \mathrm{~mA} ., 21 /$ 300 mA ., $27 / 6$; Full Wave $120 \mathrm{~mA} . .15 /$ "Q" type ads. duat core trom $4 /$ ench all ranges. Hidgai "Q " type ad). dust core from $4 /$ each All ranges. FERRITE ROD AERIALS. MW., 8/g; M. L., $18 / 6$
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 $51 / 8 ; 1 / 350$ v., $8 \mathrm{~d} . ;-1 / 1.100 \mathrm{v} ., 1 / 9 ; 0.1 \mathrm{mid}$.
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$1 / 350 \mathrm{~F}$.

$4 / 450 \mathrm{v}$.
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$8 / 450 \mathrm{v}$.
$8 / 500 \mathrm{v}$.
$8 / 500 \mathrm{v}$.
$16 / 450 \mathrm{v}$.
$16 / 500 \mathrm{v}$
$16 / 500$.
$32 / 450 \mathrm{v}$

| $25 / 25$ |
| :--- |
| $50 / 25$ |


A BRIDGR/GELENIUM REOTIFIERS $2,12 / 0$
 CHARGER IRANSFORY, Tapped inpitt $200 / 2607$


| NEW a | aod ooxed | VALVES | unudav mearantan |  |
| :---: | :---: | :---: | :---: | :---: |
| 185 | 8/616LAG | 10/6 EA50 | $1 / 6 \mathrm{ET51}$ | 12/6 |
| 195 | $8 / 6$ 6N7M | $7 / 6$ EA BCA | 10/6 Ez8l | $8 / 6$ |
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| 6BE6 | $7612 \mathrm{AT7}$ | 1016 ECLS | 1216 PEN25 | 86 |
| ¢BH6 | 10/6, 12AUT7 | 9/6 EF39 | $716, \mathrm{PL} .82$ | 10/3 |
| 6BW6 | $10 / 612 \mathrm{AX} 7$ | 9.6 EFIL | $10.8{ }^{\text {' PY80 }}$ | $8 / 8$ |
| 6D6 | $7 / 612 \mathrm{BAG}$ | 9.6 EF50 | . 516 PY 81 | 106 |
| $6 \mathrm{~F}^{\prime} 6 \mathrm{C}$ | $7 / 612 \mathrm{BE} 6$ | $9 / 6$ EFRM | -rif PY82 | $8 / 6$ |
| 6H6GT | T 3/612K7 | 8.6 EF86 | 14/6 *1'61 | 56 |
| 6J5M | $6 / 6.12 Q 7$ | 816 EF98 | $5 / 6$ UBC41 | 10,8 |
| 6.56 | 7835 L 6 | 9/6 ELas | 56 UCH 42 | 106 |
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to 550
$\mathrm{ke} / \mathrm{s}$. to $550 \mathrm{ke} / \mathrm{s}$. Complete with ${ }^{6}$ valves, ${ }^{3-}$ 125K7, $12 \mathrm{K8}$, 12SR7, 1246 $85 \mathrm{ke} / \mathrm{s}$ I.F.T Supplied brand n e w
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An extremely useful instrument pro viding the followIng facilities: I, Xtal controlled osc. giving fixed frequency signals of $500 \mathrm{kc} / \mathrm{s}$ and harmonics to 30 $\mathrm{Me} / \mathrm{s}$; 2, An addisional swirched osciflazor ( 250 . $500 \mathrm{ke} / \mathrm{s}$ ) enabling all intermediate frequencie from $500 \mathrm{kc} / \mathrm{s}$ so $10 \mathrm{Mc} / \mathrm{s}$ to be produced Compact size, $7 \times 7 \frac{1}{7} \times 4$ in. Utilises $2-\mid T 4$
IRS and CV286 valves and $500 \mathrm{kc} / \mathrm{s} \times$ Xal $\begin{array}{lll}\text { IRS and CV286 valves, and } 500 \mathrm{kc} / \mathrm{s} & \mathrm{Xtal} \\ \text { Supplied with instructional hand book. } & 59 / 6\end{array}$ each. P/P $3 / 6$.

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Bin., 3 ohm Quality Speaker mounted in atcractive black crackel case to match AR88 Receivers, etc. 45/- each. P/P 3/6.

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400 microamp basic mov. Seven A.C.JD.C. volt ranges 0 to $5,000 \mathrm{v}$. D.C. current i mA. $10 \mathrm{~mA}, 100 \mathrm{~mA}, 1$ amp. Res. 160 ohms, 100 K ohms and 1 mag. Decibels. Supplied brand new with test prods, batteries and inscructions. $63 / 19 / 6$ each. P/P $2 / 6$.

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WESTON 772 TESTMETERS. Sunplied in perfect working order, with leads and bateries, $\epsilon 7 / 10 /$ each. $P / P$ 4/6.


A.C. voles: 2.5 v . $10 \mathrm{v}, 50 \mathrm{v} ., 250 \mathrm{v}$. 1,000 v. D.C. volts | 2.5 |  |
| :--- | :--- | :--- |
| 250 v., 1.000 v. | 50 v.C. | 250 v., 1,000 v. D.C. $1 \mathrm{~mA}, 10 \mathrm{~mA}, 50 \mathrm{~mA}$. $1 \mathrm{~mA}, 10 \mathrm{~mA}, 50 \mathrm{~mA}$, $100 \mathrm{~mA}, 500 \mathrm{~mA}$ Output Meter A.C Currens: 500 mA 1 amp, 5 amp. Re sistance: 100 ohms 1,000 ohms, 100 k ohms, 10 megohm.



## TERS

12 v. D.C. ${ }_{230}$ volt Apus. 150 wates 50 cyeles outpue Housed in wooden case and fitted with voltage control slider esistance. switeh, pluzs and A.C mains volege output check meter. Supplied in perfect condltion, individually tested $=9 / 19 / 6$ each. P/P 10/.


RCA PADDED MOVING COIL HEAD. PHONES. Brand new boxed. Finest tonal quality, low impedance. Fitted with std. jack plug. 19/6 per pr. P/P 1/6.


RCA PLATE TRANSFORMERS npue 200/250 volts. Ourpue 2,000/0/2,000 volts 500 mA . tapped 1,500/01 1,500 volts. Supplied brand new boxed, c6/10\% each. carriage $10 \%$.


## 24 VOLT ROTARY CONVERTORS.

Inpur 24 volts D.C.
Output 230 voles A.C. 50 crcles, 100 watts. Housed in metal carrying case with inlet/ outlet plugs. Brand new, $92 / 6$ each. $P / P \quad 7 / 6$.



FERRANTI TESTMETERS TYPE $Q$
D.C. A.O. D.C. Obme

 ${ }_{8000} \mathrm{~F}$. 1060 \% 750 ma 500 ohms per volz on all ranges B.S.S first-grade accuracy on all self contained ranges. Supplied in perfect working order complete with leads. battery. instruccions and rexine covered carrying rexine covered carryink
case. Price $52 / 6$ each. case.
P/P $2 / 6$.


ADMIRALTY POWER UNITS 234A. $200 / 250$ volt A.C. Input. Ourput 250 volts 150 mA , and 6.3 volts 6 amps . Fully smoothed double choke and paper condensers, fused and fitted with input and output plugs. Sockets are provided on the front panel for meter check. Housed in grey metal case for standard 19in. rack mounting. Supplied brand new. 59/6 each. P/P 7/6.

CR. 100 SPARES KITS. 15 valves, resistors, pots, o/p trans. condensers, all new boxed, $59 / 6$ per set. P/P 3/6.

ADVANCE CONSTANT VOLTAGE TRANSFORMERS. 190 to 260 vole input. Constant 230 volts output. 150 watts. Brand new, $88 / 10 /-$ each. P/P 5/.

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NIFE ALKALINE ACCUMULATORS. 12 volt 45 ampere. $£ 4 / 19 / 6$ each. $P / P 7 / 6$.

PARMEKO TABLE TOP

R.II55 COMMUNICATIONS RECEIVE: S.


STANDARD MODEL B. Fitted with improved N type drive, perfect order realigned, etc. E7/19/6 each. Carriage 7/6. COMBINED POWER PACK AND OIIPPUT STAGE, to suit above, 85/- evtra. Illustratod nstructior boot with il receivers


BATTERY CHARGING OR MODEL RECTIFIERS AND TRANSFORMERS


Rectifiers. All full wave and bridged. $12 / 18$ volt 1.5 amp . $1 / 3 ; 12 / 18$ volt 2.5
amp., $6 / 9 ; 12 / 18$ volt 4 amp., 9/9: 12/18 volt 6 amp.; 18/6: $24 / 30$ vole $i$ amp., 12/6: 24/30 volt 4 amp., 22/6; 24/30 vole 15 amp. . $62 / 6$.
Transformers. All primaries capped 200/250 volts. $3.5,9$ or 17 vols $1 \mathrm{amp} ., 9 / 9 ; 3.5,9$ or 17 volt $2 \mathrm{amp}, 14 / 3 ; 3.5,9$ or 17 vole 4 amp . $16 / 6 ; 9$ or 17 voli 6 amp., 26/-; 3, 4, 5, 6, 8, $10,12,15,18,20,24$ or 30 volt $2 \mathrm{amp} .118 / 6$. Please add postage on all above items.


HALLICRAFTEM 5.27 U.H.z. COMMUNICATIO* RECEIVERS. F.M. or A.M.coverage 27 to $143 \mathrm{mc} / \mathrm{s}$. on 3 bands Incorporates $\$$ meter, variable sel. b.i.o. a.n.i. etc. Output for phone or speaker. Operation 110 or 230 volts A.C. Supplied in good work. ing order, $97110 \%$ each pip $10 \%$


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## "THE TRANSISTOR-8"

$\star$ Tunable over medium and long wavebands

* 250 mW output push-pull
* Internal Ferrite aerial
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$\star$ Top Band 150 metres $\star$ 3-Transistor * Size $4 \frac{1}{2} \times 3 \times 1$ in.
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All parts 57/6. P. \& P. 1/6 Free List and diagrams (See "R.C." Jan. 1960)

TRANSISTORS AND
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Complete set of parts including cabinet and all components. Now £10.19.6
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Combined Portable/Car Radio Push-Pull Portable Superhet


## AMERICAN VALVE

 VOLTMETERR.C.A. TYPE $165-\mathrm{A}$ ( 110 to $250^{\circ}$ V. A.C. Input)
D.C. ELECTRONIC VOLTMETER.

6-Ranges. $3-10-30-100-300$ and 1,000 volts. Input res: 11 -meg. constant on all ranges. Sensitivity: $3,666,666$ ohms per volt on 3 v . scale.
A.C. VOLTMETER.

5-Ranges. $0-10-30-100-300-1,000$ volts. Sensitivity: 1,000 ohms per volt.
ELECTRONIC OHMMETER.
6 -Ranges, from 0.1 ohms to 1.000 megohms.
Movement. 200 microamperes. D.C. accuracy $\pm 2 \%$.
Conplete with Instruction Book and Test Prods, Brand New.
ONLY £|2/10/- P.P. 3/6 SPECIAL PURCHASE
LIMITED STOCKS

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## TRANSMITTER/RECEIVER

## Army Type 17 Mk. II

Complet with Valves, High Resistance Headphones, Handmike and Instruction Book and circuit. Frequency Range
44.0 to $61 \mathrm{Mc} / \mathrm{s}$. Range approximately 3 to 8 miles. Power requirements: Standard 120 v. Hor Civil Defence communications.

BRAND NEW
45/= P.P. 5/-

44-61 Mc/s. Calibrated Wavemeter for same. 10/- extra. P.P. 2/-.

## V.H.F. TRANS/RECEIVER TYPE TR1920

 $\star 9.72 \mathrm{MC} / \mathrm{S}$ IF ${ }^{\text {\& }} 4 \mathrm{CH}$ CHNNEL CRYSTAL CONTROLLED $\star+40 \mathrm{KC} / \mathrm{S}$ BANDWIDTH $\$ 40 \mathrm{KC} / \mathrm{S}$ 8ANOWIDTH $\quad$ * 100 to $120 \mathrm{MC} / \mathrm{S}$ COVERAGE Unit complete with 21 valves: crystal; 24 volt rotary power unit, etc., in metal case. In new condition with full circuit diagram£6/10/- carr. 10/6. $\qquad$ Circuits separately, $1 / 9$ post free.

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$\star 9.72 \mathrm{MC} / \mathrm{S}$ IF +10 -CHANNEL CRYSTAL CONTROLLED $\star 23 \mathrm{KC} / \mathrm{S}$ BANDWIDTH $\quad 124.5$ to $156 \mathrm{MC} / \mathrm{S}$ COVERAGE

Sub-units
TRANSMITTER
RECEIVER
If Amplifier
Modulator .......
24 v Rotary unit
24 v. Rotary unit
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lo-way Control unit ........
All the a bove are in absolure 382

## VACUUM GAUGES

 Edwards Type M3 Gauge Heads Complete with individual calibrator. $69 / 6$ P.P. 2/-.R.C.A. 8in. P.M. SPEAKER Black crackle case. Brand New. 45/- P.P. 3/6.

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Complete with vernier dial in black crackle case; 500 UA $2 \frac{1}{2}$ in. meter: 150 to $235 \mathrm{Mc} / \mathrm{s}$ Battery operated. Includes circuit. IS5 valve.

45/- P.P. 5/6

## SMITHS 8-DAY CLOCKS

BARGAIN OFFER II 1
BRAND NEW SEALED IN SMITHS CARTONS. Gin. dial 8-day clock with detachable adjustable time switch.

ONLY 95/- P.P. 5/-
DYNAMOTORS AND CONVERTORS
24 volt D.C. to 230 v. A.C. $50 \mathrm{c} / \mathrm{s}$. 100 watts. $£ 5 / 10 /-$ P.P. $7 / 6$. 28 volts D.C. to 250 volts 60 mA ., 12/6. P.P. 2/6. 12 volts D.C. to 220 volts 165 mA ., $32 / 6$ poss free.


## QUARTZ CRYSTALS FROM 5/- EACH

From $6 \mathrm{Kc} / \mathrm{s}-47 \mathrm{Mc} / \mathrm{s}$. FT243, FT241, $10 \times 1$ and B7G. Send for list 500 types
ALL TYPES FOR ALL PURPOSES

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CRYSTAL CONTROLLED OSCILLATORS: 10 $\mathrm{Kc} / \mathrm{s}, 100 \mathrm{Kc} / \mathrm{s}$ and $1 \mathrm{Mc} / \mathrm{s}$. On/OFF MODULATOR. With handbook. Unused. ONLY 79/6.
P.P. 2/6

## 1933 RECEIVER CONTROL UNIT

BARGAIN OFFER
18 MINIATURE
VALVES!!!! 8-EF91; 6-EF92; 2-EB91; EL91; IF's; RELAYS, ETC., ETC. IN CASE.

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95 /-\quad \text { Р.P. } 3 / 6
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## CATHODE-RAY TUBES

| 2 API | lin. | 25/- |
| :---: | :---: | :---: |
| VCRI39A | ${ }^{2} \frac{3}{3} \mathrm{in}$. | 35/- |
| 38 PI | 3 in . | 301- |
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P.P. 2/- any type.

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Complete scope indicator unit with amplifier; aerial switching unit; full scope controls. Inaerial switching unit; full scope controls.
cludes $3 P B I$ Tube; $6 S N 7 G T ; 6 K 6 G T ; 6 G 6 T ;$ cludes 3 3PBI
$2 \times 2 ; 6 \times 5 G T$.

" 372 " MINIATURE IF STRIP $9.72 \mathrm{Me} / \mathrm{s}$


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A.C., D.C., R.F. METERS
free complete list on request

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3-channel U.H.F. Receiver; uses plug-in crystals (not supplied): operating on 332.6; 333.8; .cd $335 \mathrm{Mc} / \mathrm{s}$. Unit contains 7-6A15; 28D7; 2I2SN7: I2SR7: Relays, etc. BRAND NEW and boxed; a bargain at

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WAVE GUIDE 3 cm , mounted on a carrying board consisting of: (I) directional coupler. (2) 90 degree bend. (3) co-ax to wave guide adaptor type N. (4) British to W.916. (5) Co-ax to wave guide adaptor circular flange. (6) Circular to American adapt in carrying ease with coaxlal cable. Price 60/-. Carr. 10/-.


MIDGET ROTARY TRANSFORMERS. 2 tin, dia. $\times 4 \frac{1}{2}$ in. Input 11.5 volt. Output $310 / 365$ volts at 30 mA . Brand new. $12 / 6$ each. P. \& P. I/6.


TELEPHONE SETS TYPE F. Portable telephones each in an individual carrying case containing telephone handset, telephone unit, ringer, bells and complete with langlife batteries. Each set perfect, tested, guaranteed working. Has a range of up to 5 miles, ideal for factories, building sites, farms, etc. ideal for factories, building sites, farms, et
Price $£ 7 / 10 \%$ per pair. Carr. England $9 / 6$.

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AERIAL AS ILLUSTRATED. Ideal for Car. Overall length 33 in., khaki, with flexible shaft which enables the aerial zo be fixed firmly in any position. Price $8 / 6$, plus P. \& P. $1 / 6$.

NEW WIRE WOUND RHEOSTAT ON CERAMIC. 58 ohms, 50 watt, complete with instrument knob. Price 8/6. P. \& P. $1 / 6$

HIGH SPEED RELAY. Siemens, two bobbins, 1,000 ohms each. New, $10 / 6$ bobbins, 1,000 .
U.S.A. 27 -volt 4-pole CHANGEOVER RELAYS. Brand new and boxed, 5/6 each. P. \& P. 6d.

SOLENOID OPERATED MAGNETIC RELAY. TYpe 5, 5CW/3942 with 4 make, 4 break 25 Amp. contacr, D.C. coil resistance 160 ohms, 24 v. operation. Housed in metal screening can 2 in. $x$ lin. $x$ lisin. Brand new. $7 / 6$ each. P. \& P. 6d.


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 TRANSFORMERS. Type 2762 C Core: Input Output $350-0-350$ at 375 mA .25 v . at 1 amp., 21 v. at $.5 \mathrm{amp} ., 6.3 \mathrm{v}$. at it amp.., 6.3 v. at 5 amp.. 5 V. at 4amp. Price $65 /$. Carr. 6/6.

Type 2759 C Core Type 2759 Core
Input 230 v. $45 / 65$
eycles. Output 361-0-361 at 200 mA . 361 -0361 at 65 mA .5 .16 v . at $4 \mathrm{amp}, 5.16 \mathrm{v}$. at $3 \mathrm{amp}, 3.25-0-3.25$ at $2 \mathrm{amp}, 6.5 \mathrm{v}$, at 5 amp . 3.25-0-3.25 at 5 amp . Price $65 /$. Carr. 6/6.

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Input 230 v. $45 / 65$ cycles. Ourput 0-70 v. 75 v . 80 v., at 4 amp . Price $42 / 6$. Carr. $3 / 6$.


WHEATSTONE
BRIDGE UNIT. 4-stud switches $0-10,0-100$ ohms, galvanometer centre zero, F.S.D. 2.5 mA . In oak carrying case $16 \times$ $7 \frac{1}{2} \times 6 \mathrm{in}$., 401 each. P. \& P. 3/6.

EVERSHED AND VIGNOLES: Circuir testing Ohms

case. Guaran-
teed perfect.
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TRIPLE RANGE VOLTMETER. 0-5 25-250 v. D.C. M/C 3tin. meter 3in. scale, mounted in bakelite carrying case $7 \frac{1}{2}$ in. $X$ $4 \frac{1}{2} \mathrm{in}, \times 3 \mathrm{in}$. complete with handle and test leads. 27/6 each. P. \& P. 2/-.

12 V. D.C. AMPLIFIER, as new, for operation on 12 v . ear battery, torted output, with 6 L 6 valves in push-pull. Mikel Gram input, tap
 ped output $71,15,62,100,250$ or 500 ohms E12/10/- each. Carr. 15/.


TRUYOX OUD HAIL. ERS, brand new complete with ransformer and ondenser. Impedance $7 \frac{1}{2}$ ohms tandling capa city 8 watts Ideal for speech. Price: 18/6. P. \& P. 3/6. Pair 42/ postage paid.

## VARIABLE

 VOLTAGE TRANSFOR.
## RR

400 cycles, maximum input 180 v Output variable from 0 to 180 v . t maximum 15 mpere. Brand new in original manuficturers cases. Price El 10. Carr. 12/6.


## METERS BRAND NEW GUARANTEED PERFECT

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$7 \frac{1}{2}$ amp. D.C. M.I. 32 in . proj. il in. fl. and $6 / 5$
Voltmeters
2 v. D.C. M.C. 2 in. proj. rnd. ......... $8 / 6$
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30 v. M.I. 3in. proj. rnd. .................. $10 / 6$
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150 v. D.C. M.C. fl. rnd. $2 \neq i n$.
250 v. A.C. rectified moving coil linear 35/-
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Milliammeters
2 mA. M.C. $2 \underline{1} \mathrm{in}$. fl. rnd. ................... 14/6
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10 mA . M.C. 3x in. fl. rnd
30 mA . M.C. 2 in.
50 mA . M.C. 2 in. f . sq.
200 mA . M.C. 2 in. fl. rnd
200 mA. M.C. $2 \frac{1}{2} \mathrm{in} . \mathrm{fl}$. rnd.
500 mA. M.C. $2 \frac{1}{2} \mathrm{in} . \mathrm{fl}$. rnd.

## Microamp

100 microA. M.C. 21 in. rnd. fl. ......... 42/6
200 microA. M.C. $2 \frac{1}{2}$ in. rnd. fl. (cali-
50 mierod $0-50$ ) in, square, sidefitting 3
50 mieroA. 21 in , square, sidefitting 3
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NEW UNCHARGED UNFILLED 12
VOLT ACCUMULATOR 9 ampere in Unspillable plastic unspiltable plastic
cases Comprises cases
$6 \times 2$ V. separate ceils connected by ceils connected by erminal
$\times 5 \frac{1}{2} \times 4$ trips. over $\times 5 \frac{1}{2} \times 4$ in, over
terminals. P. Price 2/9. Wooden carrying case for same rying case for same
with lid and strap price $3 / 6$


ROTARY TRANSFORMERS made by Delco. Input: dual voltage 12 or 24 v . Output: 265 v. $120 \mathrm{~mA} ., 500 \mathrm{v}$. 26 mA . Price $27 / 6$ each. P. \& P. 3/6.


MINIATURE MOVING COIL DIFFERENTIAL RELAY. Two coils 350 ohms each. Operating current
 minimum 140 micromicroamp, maximum 8 milliamp. One pole two way, or, centre stable. Two way contact current 100 mA at 50 V . A.C. or D.C. Size $14 \times 1 \times \frac{3}{1}$ in. Price: $22 / 6$ each.


MINIATURE P.M. MOTOR. 12/24 volt, reversible. 1 itin. dia. New. Price P. $1 / \%$ each. P. \& P. 1/-.

AIRCRAFT CINE CAMERA G45B Mk. Ill. Fully modified, firted Fully modified, fitted
with $\$ / 3.5$ triple anastigmatic lens, takes 25 ft . of 16 mm , film, fitted with 24 V .
motor. 16 exposures per sec Brand new, original packing, $£ 4 / 10 /$ each. P. \& P. paid.


CRYSTAL CALIBRATOR No. 10 erystal controlled 4 -valve high-grade instrument in the same category as the famous B.C.221. Directly calibrated, does not require cross reference or charts-functions as follows
(I) A crystal controlled oscillator which provides fixed frequency signals of 500 KC and all harmonics of 500 KC to beyond 10 Meg , and up to 30 Meg.
(2) A variable oscillator from 250 KC to 500 KC , this enables all intermediate frequencies between $250 \mathrm{Kc} / \mathrm{s}$. and 30 Meg . to be produced and modulated.
The instrument is supplied complete with 3 spare valves, all leads and maker's instruction book in carrying haversack. The complete outfit is brand new-repeat NEW. Price: 44/19/6. Carr. 3/-


MuIRHEAD PreciSION, 4 bank, 1 pole, 24 position Stud Swirch. Heavy duty contacts, brand new, each. P. \& P. I/-.
CERAMIC PRECISION SWITCH. 2 pole, 6 way, 4 banks. New in manufaceach. P. \& P. I/6.


20 WAY STRIP containing standard Post Office telephone Jack Sockets, overall size $11 \times$ $31 \times \operatorname{tin}$. New. Price $15 /$ - each. P. \& P. $/ / 6$ 10 WAY STRIP standard Posi Office telephone Jack Sockets, spacing allowing Igranic jack Plugs. New. Price $10 / \%$. P. \& P. $1 / 6$.
LATEST MOST MODERN TYPE OF EX W.D. MINIATURE HEADPHONES As illustrated. Brand new, low impedance. Price: $10 / 6$ plus P. \&
P. $1 / 6$. NEW MOVING COIL HEAD. SETS, Complete wand microphone wi
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AUTO TRANSFORMERS. Step up, step down, $110-200-220-240 \mathrm{v}$. Fully shrouded. New. 300 watt type £2/2/- each. P. \& P. 2/6. 500 wate type 63/3/- each. P. \& P. 3/9. 1,000 wate type $£ 4 / 4 /$ - each. P. \& P. 6/6. Also 60 watts, $19 / 6$ each. Plus P. \& P. 2/
MARCMING COMPASS Mi. 1. Brand new ex W.D. Price $!4 / 6$. P. \& P. I/-.

L.T. TRANSFORMER. Input 230 V . Output Adiustable by reg Adjustable by reg
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BRAND NEW SELENIUMFULL WAVE BRIDGE ERS, in manufacturer's original packing. D.C. output 36 ४. 10 amp., made up of $12 \times 110 \mathrm{~mm}$. dia plates. These firted in cooling funnel (removable) Size (removable). Size Price $45 / \mathrm{in}, \mathrm{P}$ \& 4 in . Price
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PLATE F.W. BRIDGE CON-
NECTED RECTI. NECTED RECTI.
FIER mounted on FIER mounted on
$200 / 250$ volt A.C. input transformer Output $36 / 40$ volt D.C. at 1.2 amps. New, perfect Price
$16 / 6$. P. \& P. $3 / 6$. SPRING LOADED FUSED TEST PRODS, complete with wire leads and spade terminals. Price $4 / 6$ per pair. P. \& P. $1 /=$

MUIRHEAD VER NIER DRIVE. Scaled 0-180 degrees, as fitted to R.F. 26 as fitted to R.F. 26
units. Complese with lampholder. In minaturers ortr. inal packing. New, New,
$3 / 6$ each. $P$. P P. $1 / 6$,

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All sizes except 10 in . Completely rebuilt gun assembly, new cathode, heater, etcs., giving the high standard required for long picture life, quality and value. Carr. \& Ins. 15/6.
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$\star$ EXPRESS DESPATCH SERVICE $\star$ Please 'phone to confirm Tube in stock. Send Telegraph Money Order. Tube despatched Passenger Train same day. This service only available with remittance by a Telegraph Money Order and cash salk, not terms.

## SUPER SUPERIOR RADIO <br> 8916



4 waveband. 5valve superhet radio. 2 -tone covered metal cabinet. 4 control knobs. Positions for gram p.u. and extension speaker. A.C. only. Size $24 \frac{3}{4} \times$ $12 \times 10 \mathrm{in}$. deep. Ins. carr. $8 / 6$.

## FAMILY RADIO

99/6
5-valve (octal) superhet. A.C. 3 waveband and gram. position. 4 controls. Modern attractive catinet size $15 \frac{1}{4} \times 18 \times 10 \frac{1}{2}$ in. in cream and brown. Carr. \& Ins. 8/6.
POWER PACK and AMPLIFIER 19/6 R.F. E.H.T. Amplifier stage 6V6 with O.P. trans. 3 ohms matching. Smoothed H.T. 350 v at 250 mA .6 .3 v . at 5 amp. 22 v . at 3 amp . 6.3 v . at 4 amp . and 4 v . centre tapped. Less valves. Drawings free with order. Size $14 \frac{1}{2} \times$ $8 \times 7 \mathrm{in}$. Ins. carr. 5/6.
POWER PACK and AMPLIFIER
Output stage 6V6 with O.P 12/6 Choke smoothed H. T 350 .P. trans. 3 ohms at 5 amp .22 v , at 3 amp. 6.3 v 250 mA .6 .3 v . at 5 amp, 22 v . at 3 amp . 6.3 v . at 4 amp, and
4 v . centre tapped. Less valves. Ins. cars. $5 / 6$. COLVERN PRESET POTENTIOMETERS $2 / 9$ krand new. 200 ohms. 10 K . and 20 K . P Erand ne
$\&$ P. 9d.

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Brand new 38 mm shift control. P. \& P. $1 / 3$.
SGANNING COILS
Low imp 10/6 SGANNING COILS $15 / 9$ Wide angle 90 deg. 38 mm . Low impedance. P. \& P. $1 / 3$.


## SUPER CHASSIS

79’6
5-valve Superbet chassis including 8 in P.M. speaker and valves. Four control knobs (tone, volume, tuning, w/change switch). Four wavebands with position for gram p.u. and extension speaker. A.C. Ins. carr. 5/6.

## SOLO 12/6 <br> SOLDERING TOOL

$110 \mathrm{v} ., 6 \mathrm{v}$., or 12 v (special adaptor for $200 / 250$ v. 101 extra). Automatic

solser feed including a 20 ft . reel of Ersin (iu/40 solder and spare parts. It is a tool for clectronic whiluring or car wiring. Revolutionary in design. finsininly ready for use and cannot burn. In lught metal case with full instructions for usc. rost 3/6.

## * TRANSFORMERS *

## orop through type

350-0-350 $V_{1}$ at 250 mA ., 12/9
6.3 v . at 4 amp ., 6.3 v . at 4 amp., 4 v . at 3 amp., 22 v , at. 3 amp., 4 volt centre tapped at 1.5 amp Primary $200-250$ v. 50 cycles. P. \& P. $3 / 9$.
350-0-350 v, at $250 \mathrm{~mA} ., 12 / 9$
6.3 v . at $5 \mathrm{amp}, 4 \mathrm{v}$. at $4 \mathrm{amp} ., 4 \mathrm{v}$. at 7 amp ., 4 V . centre tapped at 1 amp . Primary 200-250 v. 50 cycles. P. \& P. 3/9.
T.V. AERIALS

23/6
For all I.T.A. channels. Outdoor or loft. 3 elements. P. \& P. 2/6.

## AERIALS

15/6
B.B.C. indoor type. Folded dipole with 12 ft co-ax calle fitted. Post $1 / 9$.
T.V. AERIALS

For all channels. Complete with co-ax cable. For use indoors or in the loft. Postage $1 / 3$.
CAR AERIALS
Plated. 50in. 6/9 liin. One hole fixing. Post $1 /$ -
CO-AX CABLE
6d. yd.
Good quality. Cut to any length. 1/6 postage on 20 yds .


HOME RADIO 79'6
AC/DC Universal mains 5 -valve octal superhet. 3 waveband receiver can be adapted to gram p.u. In attractive wooden cabinet. $9 \frac{1}{6} \times 18 \frac{1}{2} \times 11 \frac{1}{i n}$. Ins. carr: $4 / 6$.

## CHASSIS

1/-
6 or 8 valve latest type midget valve design for A.M. or F.M. Brand new. Cadmium plated. Size $12 \frac{1}{4} \times 7 \frac{1}{4} \times 2 \frac{7}{8}$ in. P. \& P. $1 / 9$.

## GANG CONDENSERS

1/9
Salvage guaranteed. Standard size two gang. .0003 and .0005 . All tested and guaranteed P. \& P. 1/3.

INSULATING TAPE
1/6
Finest quality tape $75 \mathrm{ft} . \times \frac{1}{2} \mathrm{in}$. wide in sealed metal container. Post 9d.
T.V. MASKS

12in. round. Soiled. P. \& P. 1/6.
1/9
T.V. MASKS $7 / 9$

17in. Brand new. Grey plastic. P. \& P. 2/-
T.Y. MASKS

10/9
17in. brand new. Latest pastel shades.
Pink and blue. Post $2 /$
T.V. MASKS

21 in ., as above. Post $2 /$ -
R.F. E.H.T. COIL

7-10 KV. R.F. irequency approx. $22 \mathrm{Kc} / \mathrm{s}$. Uses 6V6 or P61 as osc., suitable for Ultra model V600, W700 and many other sets or replacing E.H.T. mains transformers. Ideal when using a larger tube. Size $44 \times 2 i n$. dia. Base $4 \times 4 \mathrm{in}$. Circuit drawings avallable with order. P. \& P. 2/6.

## REGTIFIERS

250 v. 100 mA . Full or half wave. Salvage guaranteed. P. \& P. 1/3.
SOUND/VISION and I.F. STRIP
7/9 Plessey. 1.1 's $10.5 \mathrm{Mc} / \mathrm{s}$ sound. $14 \mathrm{Mc} / \mathrm{s}$ vision. 8 valve holders. Less valves. Size $8 . \times 5 \times$ $4 \frac{1}{\mathrm{in}}$. Circuit incl. The tuner unit plugs directly into this chassis. P. \& P. 2/6.
SOUND/VISION and I.F. STRIP
2/9
salvaged. Complete sound and vision strip. \& valve holders. Less valves. $1 . \mathrm{F}^{\prime} \mathrm{s} 16-19.5 \mathrm{Nc} / \mathrm{s}$. Size $8 \frac{1}{2} \times 4 \frac{1}{2} \times 4 \frac{1}{2} \mathrm{in}$. Drawings free with order. P. \& P. $2 / 6$.

8OUND/VISION and I.F. STRIP $2 / 9$ Salvaged. Superhet. 8 valve holders. Less valves. I. F's $7.25 \mathrm{Mc} / \mathrm{s}$ sound. $10.75 \mathrm{Mc} / \mathrm{s}$ vision. Vision complete from inpat up to vidio output. Sound complete from input to A.F. Amplifier. P. \& P. 2/6.

## TIMEBASE

Containing scanning coils. line transformer, elc. less valves. Drawings free with order. P. \& P. $2 / 6$

## 17" T/V 19 GNS. CASH PRICE <br> features

$\star$ Beautiful latest finish cabinet in contemporary style. and washable.
$\star$ Polished legs 18 in . optional extra for 25/-


* 17in. Rectangular Tube. Guaranteed fully for 12 months.
* 12 channels. "Turret Tuned"-ITV/BBC (Extra coils at only $7 / 6$ a pair (with order))
$\star$ Chassis. 14 B.V.A. Valves-Salvaged but reconditioned and guaranteed 3 months. Carr. \& Ins. $30 /-$
Due to overwhelming demands, some delay may occur. Please. enquire when ordering. TERMS: 36 weeks at $11 / 1$ OR 20/7 and 19 weekly payments of $19 / 11$.
(4 ueakly payments required in advance, plus carr. \& Ins.)


## * LATEST ADDITION TO OUR CHASSIS RANGE

## A COMPLETE AND WORKING I7" T/V CHASSIS 24 GNS.

Latest chassis including 17 in . tube, per manent magnet speaker, 13 channel Turre+ Tuner (any two selected channels fitted). Other channels supplied on request at 7/6 each.
13 valves. Line up as follows: 5-EF80s; 1-ECC84; 1-ECF8); 2-ECL80s; 1-PL81; 2-EB91s; 1-EY51. Chassis and valves guaranteed for 3 months. CRT for 12 months full guarantee. Sound I.F. $19.5 \mathrm{Mc} / \mathrm{s}$. Vision $16 \mathrm{Mc} / \mathrm{s}$. A.C. only. Ready and working to fit into your own cabinet. Carr. \& Ins. $25 /$..
As above with 14 in . tube complete and working £19/19/-

## T/V CHASSIS AT CLEARANCE PRICES

THE PJPULAR 12 in . PLESSEY CHASSIS $9 / 6$
A bargain for anyone wanting to make up their own T.V. at a very low cost. A chassis $\ln$ one unit. Less valves and tube. Chassis size $12 \times$ $14 \frac{1}{2} \times 11 \mathrm{in}$. I.Fs. $10.5-14 \mathrm{Mc} / \mathrm{s}$. Can be adapted for a 12 channel Turret tuner and modified to take a larger tube. Carr. \& Ins. 10/6.

## 14in. T.V. GHASSIS, TUBE and 11 Gins. SPEAKER

With 14 in . rectangular tube. 12 months guaran tee on Tube. 3 months guarantee on chassis and valves. Chassiz with Tube and speaker (less valves) 11 Gns. Complate and working with valves and Turret Tuner 15 Gns. Ins. carr. (incl. tube) $25 /$.
NODARK OVERLOAD CUT-OUT SWITCH $8 / 9$ This will stop the search for that illusive fuse wire and the annoyance of repairing the fuse. Accidental crossing of wires or faulty connections uill autonatically throw the switch of the Nodark cutting the current to the fuses. It now only remains to rectify the fault and switch on the No a:k. $200-250 \mathrm{v}$. maximum load. 2-5 amps. A traction of the list price. P. \& P. 1/6.
13 CHANNEL TURRET TUNER
Brand new. Well-known manufacturer. $38 \mathrm{Mc} / \mathrm{s}$. Complete with valves PCFP80 and PCC84. .3 series line up and channel coils covering channels , $2,3,4,5,8$ and 9 . Carr. \& Ins. 3/6.

DUKE \& CO.


## R．S．C．HI－FI TAPE RECORDER KIT Build a high quality recorder in the $\mathbf{6 7 0}$ class for only $29 \frac{1}{2} \underset{\substack{\text { ans } \\ \text {（Carg } \\ \text {（c／（6）}}}{ }$

H．P．TERMS，Deposit 3 Gns and 12 monthly payments of $53 / 9$ ．

Cssh price if settied in 3 montbs．
incorporating the latest me．iv collaro tape transeriptor the linear ltas high quality tape amplifier．A high flux $7 \times 4$ in．LOUDSPEAKER，5in．Reel of Best Quality TAPE．Spare Tape Spool，a Portable Cabinet，size spproz． $18 \times 13 \times 9$ in．，tinisbed in Veneered walnat and connection diagram for wirtng amplitier to transcriptor．

FEATURES INCLUDE
$\star 3$ speeds．$*$ Frequency response 50－11，000 e．p．s． ＊switched negative feedback equalization for each gPEED．＊OUTPUT 4 WATTS．$\star$ MAGIC EYE RECORDING LEVEL INDICATOR．$\star$ TWIN TRACK OPERATION．Both bottom and top traoks can be recorded or plaged brek withont removing tape．$\star$ instantaneous ceanges can be made from one tradik to another．Fast rewind in aither direction．$\star$ tape measuring and calibrating device．$\star$ takeg full 7in．dlameter beels of tape．$\star$ negligible hum．$\rightarrow$ Entire－ ly efrective erasure．
Full degcriptive leaflet aupplied on receipt of \＆．A．E

## HI－FI 8 WATT AMPLIFIER SPECLAL PURCEASEX DPELAAL TO CANGEALED EXPORT ORDER FOr $200-250$ v．A．O．mains． £4－19－6

a remarkable opportunity
Puah－pull output．Iateat high effelency B．V．A．valvee． Dual separately controlled inpots for milke and gram． Separate basg nad treble controls．High mensitivity．Output and in perfect worting order．

VALVES！Fuill rangé at really competitive prione
REPANCO COKSTRUCTIONAL ENVELOPES AND COM－ PONENTS ALWAYS IN STOCK
All parta for：One Tranistor Receiver 25／－：Two Tranaintor Recelver 42\％； 3 Dee ${ }^{\text {I }}$ Transistor Recelver $E 3 / 19 / 8$ Mini 7 Seven Transistor Pocket Portable Recelver $19 / 19 / 6$ Major 7 Seven Transiator Portable Meceiver 15 kn ior Mini 7 and Major 7 Recel vers．
Constructional Envelopes． 3 Dre 9d．，Mini 3 Pocket Pon－

．THE SKY FOUR T．R．F．RECEIVER


A deesign of
ralve
$200-250$ calve 200－250 $\quad$ ． A．C．mains．L．and
M．wave
T．R．F． M．wave T．R．F．
recelver with selen－ fum rectider．For Incluation in cabinet llustrated or wal－ nut veneered type． It employs valres
0K7，8P61，BF6
deajged for almplicity in wiring．Senaitivity and qually are woll up to standard．Polnt－to－Point wiring diagram． Inatructions and parts list $1 / 9$ ．This receiver can be bullt for a mazimam of $t 4 / 19 / 6$ including cabinet．Arallsble

## R．S．C．BATTERY TO MAINS CONVERSION UNITS

Type BMl．An all dry battery ellminator．Size $5 \$ \times 4\} \times 21 \mathrm{n}$ ．approx．Com 50 cle replaces batteries bupply $1.4 \mathrm{\nabla}$ ．and 20 จ．Where A．c．mains $200-250 \mathrm{~V}$ and 00 Thlc．Suitable tor ail battery portable receivers requiring 14 ． diagram $39 / 9$ or rendy for une $46 / 9$ ．
 BOTH LT BATTERTES AND HT．THEREBY COMPLETELY REPLACNC
 RECEIVERA normally uing 2 v．accumulator
Complete kit with disgrams and instructlons． $49 / 9$ or ready for nac 59／8．


## COSSOR V．H．F．F．M．RADIO RECEIVER KITS

Brand New Bored with 6 valves，printed elrcuit and $10 \times 6 \mathrm{in}$ ．Goodmans Speaker．Normal price 15 Gng ，Only $£ 8 / 19 / 6$

R．S．C．PORTABLE TAPE RECORDER
A completely assembled unit in attractive two－tone rexine covered cabinet．Acos crystal microphone，reel of best quality tape，and empty spool are supplied．
$\star$ Single speed 3 in．per sec．
t Takes up to $5 \frac{3}{3} \mathrm{in}$ ．spools．
＊Incorporates high flux $7 \times 4 \mathrm{in}$ ． speaker．
$\star$ Excellent frequency response．
\％Output of 3 watts．
High Sensitivity．
＊Inputs for Radio／Gram，or micro phone．

Or Deposit 35／－ and 12 monthly payments of $34 / 6$
$\star$ Fast rewind．
太 Automatic erase．
＊For $230-250$ v． 50 c．p．s．A．C． mains．
＊Covered by our usual 12 months＇ guarantee．

## ACOS HI－FI CRYSTAL＇MIKES＇

33.1 hand or Desk
mpe
35／9（
350.1 stck type
$39 / 6\left(\begin{array}{c}\text { Lunto } \\ 5 \\ 80.0\end{array}\right)$
Limited number．


## EXTENSION SPEARER8

Limited number in hand some Walnut veneered cab－ neils． 2.3 gins speech $\begin{array}{ll}\text { coils，} & 6 \frac{1}{2} \text { in．} \\ 35 / 9, & 10 \text { in．} \\ 56 / 9.9\end{array}$
DRY SHAVERS．Brand new in carrying case． Operation from 3 U2 batteries，fitted in case．Just the thing for travel．Only $59 / 6$（approx．half price）．
REGORDING TAPE．GEVASONOR Best quality L．P． 5 in ． 850 ft ．reels $22 / 6,7 \mathrm{in}$ ． $1,700 \mathrm{ft}$ ．reels $35 /-$ ， Less than wholesale price．

[^16]

AM／FM RADIOGRAM CHA88I8，HIGH QUALITY． PUSH－PULL．6－8 WATT OUTPUT．Current manufacture． 12 months guarantee．For 200－250v． mains．Covers L．and M．wavebands plus F．M． Includes 8 latest type miniature B．V．A．valves． Only 22 gns．plus $7 / 6$ carr．Or deposit $£ 2 / 12 /-$ and 8 monthly payments of $\varepsilon 2 / 12 /$ ．
E．M．1．4－Speed Single Plasers with hi－A T／O crystal pick－up head for Btereo and Monaural．$£ 7 / 15 /$－．Carr． $4 / 6$ ．

GARRARD 4－SPEED AUTO－CHANGER8 Type RO／120H．Limited number
price）．Carr． $5 / 6$ ．Brand new．

## R．S．C．TRANSFORMERS fully guaranteed

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Primaries $200 \cdot 230-250$ ㄷ． $50 \mathrm{c} / \mathrm{s}$ ．
FOLLY giEROUDED UPRIGRT MOUNTING



$350-0-360$
3
3 338

TOP SHROUDED DROP－THEODGE TYPE





 ELIMINATOR TRANSFORMERS Primarice 200－250 $\mathrm{\nabla} .50 \mathrm{c} / \mathrm{s}$ ．

90 v． $15 \mathrm{~mA} ., 6 \cdot 0.6 \mathrm{r} .250 \mathrm{cmA}$
Primaries 200－250 ч． 60 o／s．


OUTPUT TRANSFORMERS
Midget Battery Pentode $66: 1$ for 354，etc
Bmall Pentode 5,000 o to 30
Standard Pentode $5,000 \Omega$ to $3 \Omega$
Standard Pentode $8,000 \Omega$ to
Standard Pentode $8,000 \Omega$ to $3 \Omega$
Push－pull 8 watte 6 V 6 to 3 ohme
Push－pull 8 watts EL84s to 15 ohms
Push－pull 10.12 watts 6 V 6 to $3 \Omega$ or 15 D
Push－pull $10-12$ watta to match 6V8 to $3-\delta-8$ or $150 \quad 16 / 9$
Puah－pull EL84 to 3 or 15 ohrad ．．．．．．．．．．．．．．．．．．．．．． $17 / 9$
Pusb＝pull 18.18 watto sectionally wound，6LB．
Push－pull 20 watt high－quality sectionality wound，
6L6，KTi6，etc．to 3 or $15 \Omega$ ．．．．．．．．．．．．．．．．．．．．．．．．．47／8
SMOOTHMNG CHOKES
$\begin{array}{llll}250 \mathrm{mLA}, 5 \mathrm{H} ., 100 \mathrm{o} & 11 / 9 & 80 \mathrm{~mA}, 10 \mathrm{H}, 350 \mathrm{n} \\ 150 \mathrm{~mA} .7-10 \mathrm{H} .250 \mathrm{~g} & 11 / 9 & 80 \mathrm{~mA}, 10 \mathrm{H}, 400 \mathrm{ol}\end{array}$ 4／18 $\begin{array}{lll}100 \mathrm{~mA} ., 10 \mathrm{H} .200 \mathrm{~B} & 11 / 9 & 80 \mathrm{~mA} .10 \mathrm{H}, 400 \\ 1 \text { amp．} 0.5 \mathrm{~B} \text { LT tspe }\end{array}$

## PHILCO F．M．RADIO TUNERS

With self－contained power pack．A 6 －valve de luse unit housed in beautiful walnut venoered cabinet．For $110-200-250 \mathrm{~V}$ ．A．C．mains． Magic eye tuning indicator $2 \frac{1}{2}$ ans．Carr． $5 /-$
Or Deposit $22 / 6$ and 12 monthly payments of $22 / 8$ ．

## R.S.C. A.IO ULTRA LINEAR HIGH FIDELITY I2-I4 WATT 30 WATT AMPLIFIER


gram, etc, etc., can be simultaneously gpplied for miring purposes. AN OUTPUT SOCKET WITH PLUG IS INCLUDED FOR SUPPLI OF 300 จ. 20 mA , and 6.3 . 1.5 A . FOR A RADIO FEEDER UNIT. Price in kit form with eary-to-follow wiring diagrams.
Only Only 14 Gns. payments of 24/8.
Cover as lllustrated
Type 807 output valves are used with High Quality Sectionally wound output tranaformer upecially deaigned for fitra Linear 18/9 extra. $\qquad$ TO MOST 20 D.B. in main loop. CERTIFIED PERIORMANCE IGURES ARE EGUAL TO MOST EAPENSEA $\pm 3$ D.B. $30 \cdot 20,000 \mathrm{c} / \mathrm{cs}$. Tone Controls $\pm 12 \mathrm{D.B}$, at $50 \mathrm{c} / \mathrm{cs} .+12 \mathrm{D.B}$. to $-6 \mathrm{D.B}$.

Chissis finish biue hammer. Overall size $12 \times 9 \times 9 \ln$. approx. Power consumption 150 watts. For A.C. malns $200-250 \%$. 50 c/s. Outputs for 3 and 15 ohra speakers. EQUALLY
SUITABLE FOR TERE CONNOISSEUR OR FOR LARGE EALLS, CLUBS OR OUTSIDE
 GLECTEONIC ORGAN, GUITAR, etc. FOR DANCE BANDS, GARRISON THEATRES, otc, oto, We can supply Microphones, Speake
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LNEAR "DLATONIC" 10 WATT HGGE FLDELITY AMPLIFLER. A compact attractrely Anished unit. 12 gns. Clash. Send B.A.E. for leaflet. F.P. Termas. Dep. $22 / 3$ and
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LNEAR L5/5 HIGH QUALITY STEREO AMPLIFIER. Total output 10 watts Handsome Perspex Facia Plate. All controls ganged. Only 11 Gns.

LINEAR L45 MINIATURE $4 / 5 \mathrm{~W}$. QUALITI AMPLIFIER. Sultable for use with any record playing unit and most microphones. Negatve feedback 12 D.B. Base and Treble controls. For A.C. uaina input of $200-250 \times$. 00 c.p.s. Output for $2 / 3$ ohm speaker. Three Guaranteed 12 months. Only $£ 5 / / 9 / 6$ or Deposit $22 /=$ and 5 monthly payments
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LG3 Miniature 3 WATT GRAM AMPLIFIER
For $200-250$ т. 50 c.p.6. A.C. mains. Overall size only $6 \$ \times 4 \frac{1}{} \times 2 / \mathrm{in}$. Fitted vol, and Tone Dontrol with maing switch. Deslgned for use with any kind of single player or record change ing anit. Output for $2-3$ ohm speaker. Guaranteed 12 months. Only $57 / 9$
R.8.C. A\% 3-4 WATT QUALITY AMPLIFIER. Apec. exactly as $\Delta 5$ below with exception R.8.C. A\% 3-4 WATT QUALITY AMPLAFLER. 8pec. exactly as A5 below with exception
of output wattage. Complete kit of parts, diagrams and Instructions $£ 3 / 15 /$, carr. $3 / 6$.

## R.S.C. A5 4-5 WATT HIGH GAIN AMPLIFIER

A hlghly sensitive 4. Falve quality armplifier for the home, amall club, etc. Only 50 milliolts input is required for full output 80 that it is sultable for use with the latest highAdelity pick-up beads in sddition to sil other types of pick-upa and practically all mikea. sepmate Bass and Treble controls are provided. These give foll long playing record
 091. 15 D.3. of negative feedback is used. H.T. for the sapply of a Radio Feeder Unit or Tape Deck pre-amplifer. For A.C. mains input of $200-250 \mathrm{~F}$. $50 \mathrm{c} / \mathrm{es}$. Output for 2.3 ohm apenker. Chaseis is not Klive. Kit is complete in every detail and includes
iully punched chassia (with baseplate) with the blue iully punahed chasgis (with baseplate) with the blue
hammer falish. aud polnt-to-point wiring diagraina and inssructions. Exceptional value at only £415/or assembled resdy for use $25 /$ extra, plus $3 / 6 \mathrm{car}$ riage. Or Depposit $28 / \mathrm{L}$ and five monthly payments of


TWEETRRS. 4in. Plessey, 3 ohms, 18/9. Rula/Celestion 7.5 ohms, $25 / 9$.
P.M. SPEAKERS. $2-3$ ohm 24 in . Perdio 21/9. 5in. Goodmans $17 / 9.7 \times 4 \mathrm{in}$. R.A. EHp. tical 19/8. 6itin. Rola 19/9. 8in. Kola 19/9. 8 in . Goodmans $21 / 9,8 \times 6 \mathrm{in}$. Elac with high flux magaet 25/8. 10 im . R.A. 28/9. $10 \times 6 \mathrm{in}$. Etliptical Goou
collaro coneuest 4-speed AUTOCOLLARO CONQUEST 4-SPEED AUTOturnover head. BRAND NEW. Cartoned latest model. For 200-250 マ. A.C. mains. fy/19/6. Cart. 4/6.
GRAM MOTOR with Turntable and plekup, etandard 78 r.p.m. Brand new. Omly 25/8.

ACOS Cryatal Microphone Inserts. Brand new. Only $5 / 11$ ea. Ex. Equlp. $4 / 11$ ea ACOS HGP58 Hi-Fi Crysual Cartridges. (Turnover type with sapphire stylus.) Standard replacement for Garrard and Collaro. Only $19 / 8$. B.8.R. Ful-il $17 / 9$ Garrard GC2 $19 / 8$.
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Open to callers at following branches:-5-7 County Arcade, Leeds, J.
54-56 Morley St., (next Majestic Ballroom) Bradford. 8-10 Brown Street, (Market St.) Mar chester, 2.

TERMS: C.W.O. or C.O.D. No C.O.D under \&1. Postage $1 / 9$ extra on all orders under $22,2 / 9$ extra under 25 unless carriuge stated. Trade supplied. Post orders to Mail Order Dept.
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GUITAR AMPLIFIERS
JUNIOR 5 WATT. High Quallty Output. Separate Senaitivity $15 \mathrm{~m} . \mathrm{v}$, High Five 8 In . 1/8peaker. Input sockets for Radio/Tape or Gram Fick-up and Mike Iostrument Pick-up. Handsome atrongly made cabinet (Bize approz, $14 \times 14 \times 7 \operatorname{lns}$.). Finished io satin wainut and fitted carrying handie.
$68 / 19 / 6$ Carr. $7 / 6$. Or Deposit $t 1$ and aime Send S.E for leafyments $£ 1$.

SENIOR 10 WATTS. Eigh Flielity Push Pull output. Separate Bass and Treble "cut" and "boost" controls. Twin separately controlled Guitar and String Bass ean be used at the same time. Two Loudgpeakers are incorporated, a 12 in . P. M. for Bass notes, and a $7 \times 4 i n$. elliptical for
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$23 / 6$ and 12 monthly payments $23 / 6$. Both modela for $200-250$. A.C. man.

STAAR GALAXY 4-SPEED MIXER A UTO-CHANGERS. Brand New, cartoned. Turhover kapphire gtyll. Many exelusive features. Unique deaign motor virtualiy free from runble.
For 200.250 . A.c. mains. Limited number tested and guaranteed $65 / 19 / 6$. Carr, $4 / 6$.

## PORTABLE CABINETS

For Record Piayers or Tape Recorders. Rexine corered. Wide seleetion of athrative designo | and colour combinatioas |  |
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## 12in 10 WATt HIGB QUALITY LOUDSPEAKER IN

 POLISHED WALNUT FINISHED CABINETGauss 12,000 lines. Speech coll 3 ohms or 15 ohms. Only $\mathbb{C} 4 / 19 / 6$. Carr. 5/--
Termas: Deposit $11 /$ and 9 monthy payments of $11 /$ Terma: Deposit $11 /$ and 9 monthy psyments of $11 /$-. $18 \times 8 \mathrm{in}$. $£ 7 / 19 / 6$ or Deposit $13 / 10$ and 12 monthly payments $13 / 10$.

PORTA BLE CA BINETS. Attuactive desigu Two-tone rexine covered. Win take Collaro,
B.8.R. Garrard or Btaar Auto-Changer B.8.R., Garrard or Blaar Auto-Changer, amplifeer and 7in. $\times 4 \mathrm{in}$. or
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## SPECIAL OFFER

Above cabinet Staar Changer, Gram amplifer, and fin. or
$6 \mathrm{in} . \times 4 \mathrm{in}$. speaker $69 / 19 / 8$ Cart. 10/, speaker $\mathbf{O r}$ with B.S.R. chauger in lieu of Btaar 11
Gns. Carr. 10\%.

ACOS EMGK FIDELITT PICK-UPS. QP64 with HGP59/52 Cartridge. Turs-
over sapphire 8 gtyli, cream finlsh. Limited nurober at approx. half price. Only $29 / 11$.

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\begin{aligned}
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& 6 \text { v. or } 12 \text { v. } 4 \text { amp. with }
\end{aligned}
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$$
\begin{aligned}
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80 sq. in. & \(5 /-\) & 208 sq. in. & \(9 /-\) & 336 sq. in. & \(13 /-\)
\end{tabular}
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\begin{tabular}{|c|c|c|c|c|}
\hline \multicolumn{5}{|c|}{SINGLES} \\
\hline Capacity & Wkg. & & & \\
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\end{tabular} & 275 & \[
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\] & W/8 & \({ }_{1 /}\) Price \\
\hline 8 & 12 & 13/32 \(\times 1\) & M & 1/4 \\
\hline 2 & 275 & \# \(\times 1\) & w & \(1 /-\) \\
\hline 4 & 150 & [ \(\times 1\) & T/8 & 1/- \\
\hline \({ }^{4}\) & 150 & \(\underline{41}\) & & 1/- \\
\hline 5 & 250 & ¢ \(\times 1\) & Worw/8 & 181/3. \\
\hline 8 & 150 & \(1 \times 1\) & T & 10d. \\
\hline 8 & 200 & \({ }^{1} \times 1\) & \(\stackrel{\text { w }}{ }\) & \\
\hline 8 & 250 & 1 \(\times 1\) & Worw/ & 181/- \\
\hline 8 & \({ }^{275}\) & ( \(\times 1\) & W & 1/3 \\
\hline 8 & 350 & \(1 \times 2\) & P & 1/6 \\
\hline & 450 & | \(\times 1\) & W/8 & \(1 / 11\) \\
\hline 10 & 750 & 13/32 \({ }^{11} \times 1\) & \({ }_{\text {c }}^{\text {c }}\) & 1/4 \\
\hline 10 & 15 & - \(\times 1\) & T/8/R/ & \(1 / 6\) \\
\hline 10 & 25 & \(1 \times 1\) & T/8 & 1/3 \\
\hline 10 & 200 & \({ }_{1} \times 1 ;\) & \({ }^{\mathbf{w}}\) & 1/3 \\
\hline 10 & 450 & \(1 \times 2\) & & \(1 / 9\) \\
\hline 12 & 25 & 13/32 \(\times 1\) & M/R & /6 \\
\hline 16 & 150 & \(1 \times 11\) & T/8 & \\
\hline 18 & 275 & \({ }^{1} 2\) & T & 10 d \\
\hline 16 & 350 & \(3 \times 2\) & & 1 - \\
\hline 20 & 12 & 8 \(\times 1\) & W/8 & 1 \\
\hline 20 & 150 & \(13 / 32 \times 1\) & T & 10.4. \\
\hline 20 & 450 & \(1 \times 2\) & W/8 & 1/9 \\
\hline 25 & 12 & 13/32 \(\times 1\) & M/R & 1/6 \\
\hline 25 & 25 & \(13 / 32 \times 1\) & M & 1/4 \\
\hline 25 & 25 & & W & 1/6 \\
\hline 25 & 50 & \(1 \times 17\) & T & - \\
\hline 25 & 50 & \(1 \times 1\) & W & 119 \\
\hline 85 & 350 & \({ }^{1} \times 1 \frac{1}{1}\) & W & 119 \\
\hline 32 & 275 & \(1 \times 2\) & & 1/6 \\
\hline 40 & 150 & ¢ 2 & w/8 & 6 d \\
\hline 40 & 350 & \(\times 2\) & P & \(1 / 9\) \\
\hline 50 & 6 & \(13 / 32 \times 1\) & M & \(1 / 4\) \\
\hline 50 & 12 & 13/32 \(\times 1\) & M/R & 1/6 \\
\hline 50 & 12 & ¢ \({ }^{1}\) & W & 1/6 \\
\hline 50 & 25 & + & w & 1/6 \\
\hline 50 & 50 & [ \(\times 14\) & T & 1/6 \\
\hline 60 & 275 & \(1 \times 3\) & W & 1/9 \\
\hline \({ }_{84}^{60}\) & \({ }_{275}\) & \(1 \times 2\)
\(1 \times 3\) & \({ }_{P}^{\text {T/8 }}\) & \(21 /\) \\
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8
Wkg.
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\hline 5 & \(1 \times 11\) \\
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\hline 0 & \(11 \times 3\) \\
\hline 6 & \(1 \times 2\) \\
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\hline 6 & \(1 \times 2\) \\
\hline 12 & \(4 \times 1\) \\
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\hline 5 & \(1 \times 2\) \\
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\end{tabular}
 DOUBLES
\begin{tabular}{llll|r}
350 & \(1 \times 2\) & C & \(2 / 3\) & \(80+250\) \\
450 & \(1 \times 2\) & W & \(2 / 9\) & \(100+300\) \\
450 & \(1 \times 1 \%\) & \(\mathrm{~W} / \mathrm{B}\) & \(3 /-\) & \(100+100\) \\
450 & \(1 \times 1\). & \(\mathrm{W} / \mathrm{B}\) & \(3 / 8\) & \(100+100\) \\
450 & \(1 \times 2\) & \(\mathrm{~W} / \mathrm{B}\) & \(2 / 6\) & \(100+100\) \\
275 & \(1 \times 2\) & P & \(1 / 6\) & \(100+100\) \\
275 & \(1 \times 2\) & C & \(2 /-\) & \(100+100\) \\
275 & \(1 \times 2\) & C & \(1 / 6\) & \(100+200\)
\end{tabular}
Capacity
(MIds
\(12+28\)
\(16+16\)
\(18+18\)
\(16+18\)
\(16+18\)
\(20+10\)
\(20+20\)
\(20+20\)
\(20+20\)
\(24+24\)
\(25+95\)
\(30+30\)
\(32+32\)
\(32+32\)
\(32+32\)
\(32+32\)
\(32+32\)
\(32+38\)
\(32+32\)
\(32+32\)
\(32+32\)
\(40+20\)
\(40+40\)
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\(50+50\)
\(50+50\)
\(50+50\)
\(50+200\)
\(80+100\)
\(60+100\)
\(60+200\)
\(60+250\)
\(80+300\)
\(100+65\)
\(100+100\)
\(100+100\)
\(100+100\)
\(100+100\)
\(100+100\)
\(100+200\)
\begin{tabular}{|c|c|c|c|}
\hline Wkg. Volts & Size* & Type & Price \\
\hline 275 & \(1 \times 2\) & P & \(1 / 6\) \\
\hline 150 & - \(\times 1 \frac{1}{6}\) & T/S & 1/- \\
\hline 275 & \(1 \times 2\) & P & 21- \\
\hline 350 & \(1 \times 2\) & 0/8 & 31- \\
\hline 450 & \(1 \times 2\) & W/8 & 4/- \\
\hline 450 & \(1 \times 3\) & C & 3/- \\
\hline 275 & \(1 \times 2\) & P & 21- \\
\hline 460 & \(1 \times 3\) & W & \(3 / 6\) \\
\hline 450 & \(1 \times 3\) & P & 3- \\
\hline 350 & \(11 \times 2\) & C & 21- \\
\hline 300 & \(1 \times 2\) & \(\mathbf{P}\) & 1/6 \\
\hline 150 & \(1 \times 17\) & W/8 & 1 - \\
\hline 180 & \(1 \times 2\) & C & 1- \\
\hline 150 & \(1 \times 2\) & W/8 & 1/- \\
\hline 150 & \(1 \times 3\) & P & 10 d \\
\hline 250 & \(1 \times 2\) & PC & 1/6 \\
\hline 275 & \(1 \pm \times 2\) & 0 & 2/6 \\
\hline 275 & \(1 \times 2\) & C & \(2 / 6\). \\
\hline 350 & \(11 \times 2\) & C/B & 4/- \\
\hline 350 & \(1 \times 2\) & P/S & 3)- \\
\hline 450 & \(11 \times 3\) & W/S & \(4 / 6\) \\
\hline 150 & \(1 \times 2\) & P & 10 d. \\
\hline 150 & \(1 \times 3\) & P & 10 d \\
\hline 275 & 11×2 & c & 1/6 \\
\hline 300 & \(1 \times 2\) & PC/S & 2/- \\
\hline 450 & \(11 \times 3\) & W & 3/- \\
\hline 150 & \(1 \times 2\). & O & 1/- \\
\hline 200 & \(1 \times 3\) & P & 1/- \\
\hline 250 & \(1{ }^{1} \times 2\) & P & 1/- \\
\hline 275 & \(11 \times 2\) & P & 1/9 \\
\hline 275 & \(11 \times 8\) & 0 & 1/6 \\
\hline 275 & \(1 \times 34\) & PC & 1/9 \\
\hline 300 & \(11 \times 2\) & 0 & 21- \\
\hline 275 & \(1 \pm \times 3\) & O & 4/6 \\
\hline 275 & \(1{ }^{18} \times\) & P & \(2 / 6\) \\
\hline 350 & \(11 \times 41\) & 0 & 5/6 \\
\hline 275 & \(11 \times 4\) & 0 & \(3 / 6\) \\
\hline 275 & \(12 \times 4\) & 0 & \(3 / 6\) \\
\hline 275 & \(1{ }^{1} \times 4\) & - & \(3 / 6\) \\
\hline 250 & \(11 \times 3\) & P & 2/- \\
\hline 12 & \(1 \times 2\) & c & 1/- \\
\hline 25/12 & \(1 \times 2\) & P & 1/- \\
\hline 275 & 11 \(\times 3\) & O & \(2 / 6\) \\
\hline 300 & 1) \(\times 3\) & P & 3/- \\
\hline 300 & \(11 \times 3\) & P & 31- \\
\hline 25 & \(1 \times 2\) & \(\mathbf{P}\) & 1/- \\
\hline
\end{tabular}
Capacity
(MIds.)
\(100+200\)
\(100+200\)
\(100+250\)
\(100+300\)
\(100+400\)
\(150+30\)



\author{

}

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MOULDED TROPICAI PAPER CONDENSERS Small, non-inductive, insuiated, bigh-grade Capacitors \(1 / 3.2 \mathrm{Mid} .1 / 9.2 \mathrm{Mfd} .10 \% 1 / 10.250 \%\). Wkg., 068 Mrd ,








\section*{VALVE HOLDERS}

4 pin Brit. Pax, 8d. 4 pin UX. Amp. 7 d 5 pin Brit, Pax. 2d. 7 pin Brit. Pax. 3d. 7 pin 1 srit. Amp. 4 d . Int. Octal Pax. 3d. Mazda Octal Yax. 3d. Loetals Amp. 6d. B7a
Pax. 6d. B7G P.T.F.E. 8d. By Cer. with maidie and Pax. Gd. B7G P.T.F.L. 8d. Byg Cer. with nadidie and
valve retaining spring 1/-, B8A Pax. 4 d . B8A Amp. 6d. Falve retaining gpring 1/-. B8A Pax. 4d. B8A Amp. 8d.
B8A Cer. 8d. B9A Pax. 6 d . B9A Amp. 6d. B8A Cer. 10 d . B0A Cer. with saddle and vaive retaining spring \(1 / \mathrm{G}\) 89A Cans 6d. EY86 High voltage holders 1/3.

VARIABLE GANG CONDENSERS
 Min. Twin Gang, .0005 MFD. \(24 \mathrm{in}, \times 1\) inn. \(\times 1 / \mathrm{in}\), Min. Twin Gang. \(0005 \mathrm{MFD} .2 \frac{\mathrm{in} .}{} \times 1 \mathrm{in} . \times 11 \mathrm{in}\),
Spindle in. with trimmers, \(6 / 6\).
AM/PM 2-dang Condensers, \(500+20\) pi., \(3 / 6\).

DISC CERAM1C CONDENSERS \(500 \mathrm{\nabla}\). Wkg. 500 PF. . 001 MFD. 0025 MFD., 008 MFD,, . 003 MFD.

\section*{TRANSISTOR COMPONENTS}

SUB MINIATURE ELECTROLYTIC CONDENSERS -SLEEVED-All at \(2 / 3\) each.
\(.1 \mathrm{mfd} .12 \nabla, 25 \mathrm{mfd} .15 \quad \nabla, .5 \mathrm{mfd} .2-8-8-10 \mathrm{mfds}\). 30 mfds. 12 v., 2 mfds., 8 mfds., 15 v., 8 mfdd. 16 mfds., 30 v.. 2 mfds. 70 v.

SUB mINIATURE TRANSISTOR COILS Get of 3 1.F. Transformers \(470 \mathrm{Kc} / \mathrm{s}\) plus Oscillstor As specified for Mulard Circults \(23 / 6\) complete. As specified for Mazda Circuit \(23 / 6\) complete. \(4 / 6\) each. WTC \(470 \mathrm{kc} / \mathrm{s} 1 . \mathrm{F}\). Transformers, \(4 /\) each, 4/6 each.
\(7 / 6\) palr.

SUB MINIATURE CARBON POTS \(5 \mathrm{~K}, 50 \mathrm{~K}, 220 \mathrm{~K}, 330 \mathrm{~K} .1 \mathrm{M}, \mathrm{Q} / \mathrm{-}\) each. 5 M with switch. \(4 / 8.5 \mathrm{~K}, 1 / 8.500 \mathrm{~K}\) preset \(1 / . \mathrm{IM}^{1 \mathrm{M}}\) Tran. sistor Pots, 2/-. \(5 \mathbb{K}\) Transistor Pots, \(1 / 6\).
SUB MINLATURE METALLISED PAPER CON. DENSERS If. \(\times 1 \mathrm{ll} .100 \mathrm{v}\). working . 005 MFD.. 0022 MFD., 002 MFD. . 001 MFD., 8 d . each. 01 MFD., 02 MFD , Price 9 d . each.

TRANSISTOR GANG CONDENSERS With intermediate screen as specified for MOLLARD Tranalator circuita, \(9 / 6\).
As above with switch for L.W, pre-selection, 11/-。
MIN. POLYSTYRENE CONDENSERS


\section*{TV PRESET CONTROLS}

Knurled knob sid 8BA firing holew. Dism. Hin. 5K, 25K, \(50 \mathrm{~K}, 100 \mathrm{~K}, 250 \mathrm{~K}, 600 \mathrm{~K}, 2 \mathrm{M}, 13\) anch 25 K , wirewound 50 K,
\(1 / 6\).

SWITCHES ROTARY
Size \(1 \frac{8}{18} \mathrm{in}\). dia.-2in, spindles. Price \(2 / 11\) each 1 pole 10 way. 1 pole 12 way, 2 pole 2 way. 2 pole 3 way. 2 pole 4 way. 2 pole 5 way. 2 pole 6 way. 3 pole 3 way. 3 pole 4 way. 4 pole 3 way.

\section*{POTMETERS CARRON-HI-GRADE} Moulded Tracks. Diam., \(11 \mathrm{n}, 2 \mathrm{Hn}\), spindles, \(5 \mathrm{~K}, 10 \mathrm{~K}\), or Linear, less switch, \(2 / 6\) each. With switch, \(4 / 6\).

\section*{TRANSFORMERS}

Audio Output Types. \(6,000 \Omega\) to \(3 \Omega, 3 / 6,10,000 \Omega\) to \(3 \Omega\),
 Universal CRT Boosters with tapped primarles \(2 \mathrm{v} .6 .3 \mathrm{\nabla}\). \(13 \nabla ., 25 \%\) booat all tapa, 10/6. Filament transformers, centre tapped, \(6.3 \mathrm{\nabla}\). output, \(1.5 \mathrm{amp} ., \mathrm{E} / 9 ; 3 \mathrm{mmps}\). 9/6.

MODERN TV COMPONENTS
Ferros Line \(0 / \mathrm{P}\) transtormers, \(16 \mathrm{~K} \mathbf{V}\). U25 19/6. Frame O/P transformera to match \(4 / 6\). Scanning Colls to match 15/e Panel containing 6 preset pots. 5/- 8moothing
Chokes: \(2 \mathrm{Ey} .250 \mathrm{ma} .3 / 11\). \(1.9 \mathrm{Hy} .250 \mathrm{~ms} 2 / 11.1 .3 \mathrm{Hy}\). Choses: 2 Hy. \(250 \mathrm{ma} .3 / 11.1 .9 \mathrm{Hy} .250 \mathrm{~ms} 2 / 11.1 .3 \mathrm{Hy}\). G.E.C. Metal Rectifler 250 v. \(250 \mathrm{ma} .10 / \mathrm{m}, 34 \mathrm{Meg}\) I.F.T. G.E.C. Metal Rectifter 250 v. 250 ma . \(10 / \mathrm{m} .34 \mathrm{Meg}\). I.F.T.
\(1 / 6\) es, 38 Meg. I.F.T. (Hnk) \(2 /-\mathrm{ea}\). Masks \(14 / \mathrm{n} ., 17 \mathrm{im} .\), and 1/6 es, 38 Meg. I.F.T. (Hnk) 2/- ea.
2/in. 2/6.3/6. \(4 / 6\) (plus 2/8 p.p.).

\section*{MISCELLANEOUS}

Cenuine oc71 Transibtors 6/6. Crocodlle ellpa 4d. Coar. Pluga and Sockets \(2 / 2\) per pair. Condenser clipg 1 in . and 3/G. 500 pf . 15 Kv moulded Condensers 2/6. WX25 Westector Bd. Eiliptical Bpentera \(7 \mathrm{in} . \times 4 \mathrm{in}\). \(12 / 6\). 100 assorted first class Erie reaistors 12/6. Transistor twin gang condensers \(387+168\) pl., ex equip. 4/6. Vibrator
We have an extenive rabge of Waxed Paper Condenaure average price 5d. ea.), MeLullised Paper Comdenmer average price 11 d . each) and wirewound reastore 5/6/7

\title{
Wilkinsons \({ }^{\text {mim }}\)
}

METERS GUARANTEED

\section*{F.S.D.}

50 Microamps
100 Microamps
500 Microamps
500 Microamps
1 Milliamp
1 Milliamp
30 Milliamps
100 Milliamps
200 Milliamps
500 Milliamps
5 Amperes
15 Amperes 25 Amperes D.C. 50-0-50 Amp. 30-0-30 Amp.
20 Volts
\begin{tabular}{|c|c|c|}
\hline Size & Type & Price \\
\hline \(2 \frac{1}{2}\) in. & MC/FR & 70/- \\
\hline 31in. & MC/FR & 701- \\
\hline 2 in . & MC/FR & 25/- \\
\hline \(2 \frac{1}{2}\) in. & MC/FR & 37/6 \\
\hline 2 in. & MC/FS & 27/6 \\
\hline \(2 \frac{1}{2} \mathrm{in}\). & MC/FR & \(35 /-\) \\
\hline \(2 \frac{1}{2}\) in. & MC/FR & 12/6 \\
\hline 2 in. & MC/FR & 12/6 \\
\hline \(2 \frac{1}{2}\) in. & MC/FR & 12/6 \\
\hline 312. & MI/FR & 301- \\
\hline 2 in . & MC/FS & 27/6 \\
\hline 2 in . & MC/FR & 10/6 \\
\hline \(2 \frac{1}{2}\) in. & M1/FR & 7/6 \\
\hline 2 in . & MC/FS & 12/6 \\
\hline 2 in. & MC/FR & 15/6 \\
\hline 2 in. & MC/FS & 10/6 \\
\hline 2 in . & MC/FS & 10/6 \\
\hline \(2 \frac{1}{2}\) in & MI/FR & 25/- \\
\hline
\end{tabular}
 300 Volts

2TIn. MI/FR
\(25 /-\)

\section*{A large and comprehensive stock of WIRELESS AND ELECTROHIC COMPOHELTS}

6TELEPHONES Easy to fix Wring diagram Free

\section*{TELEPHONE SET TYPE "A" Ringing and speaking both ways} on a 4 -core cable. Very loud and clear over any distance. The handsets are as illus. and the set is complete except wire. 4 -core at 8 d . per yard or 2 -core at 3 d . per yard extra. Price 75/set, post \(3 / 6\).
8. Two headphones connected to breast microphones, with with two wires and 8ET "C" Similar to set "A". Instead of P.O. Type handsets, two P. Desk Type Instruments are supplied with usual drawer in base. Complete ready for use. Price \(150 /=\), post \(7 /\) -


\section*{10 AMP BATTERY CHARGER}
here is your chance to purchase a brano NEW UNIT WORTH £40! FOR OUR SPECIAL PRICE
£17.10.0
Carriage 20/-. Input \(200 / 250\) v. A.C. 50 cy . Output 10 amps., 22
volts D.C. Controlled by two 4 -position switches for fine and coarse control which enables 6 to 24 volt for fine and coarse control which enables 6 to 24 volt
batts. to be charged. Brand new with \(0 / 12\) ammeter. batts. to be char
BATTERIE8. Portable Lead Acid type, 6 volts 125 ampere hours. In metal case \(16 \mathrm{in} \times \operatorname{8in} . \times 1.1 \mathrm{in}\). (Two will make an ideal power supply for our 12 volt Rotary Converters). Uncharged £6/10/- each, carriage 15/-. 24 volt 85 ampere \(£ 15 /-1\) - each, carriage \(15 /-\).
UNI-PIVOT GALVANOMETER by Cambridge Instruments, 50-0-50 microamps., dia. 4 in. Knife pointer, mirror scale. Complete with leather carrying case. Ideal for laboratory use. \&10, carriage 3/-.
case. Ideal for laboratory use. 10 , carriage \(3 / \%\)
FLIGHT TO GROUND \(8 W\) ITCHES. \(5 C / 2828\) as used on aircraft. Very FLIGHT TO GROUNO \(8 W\) ITCHES. \(5 C / 2828\) as used on aircraft. very
robust, will carry a very heavy current \(25 /-\) each; or in pairs with auxiliary robust, will carry a very heavy current \(25 /-\) each; or in pairs with auxiliary
swith \(50 /=\), post \(3 /-\) OSCILLOSGOPE. Type 43. With \(3 \frac{1}{2}\) in. C.R.T. 138A, 4-617, 3-VR54, 5Z.4, VU120. Brand New with usual controls., power-pack and leads. Suitable for
SIGNAL GENERATOR TYPE S2A. Input 230 volt 50 cycles, complete with leads, dummy antenna. Brand new in transit case. 6 to \(52 \mathrm{Mc} / \mathrm{s}\). inclusive in 4 bands with calibration charts. Coarse and fine at tenuators. Int. and ext. mod. Output \(n .5\) volt to 100 mv .. impedance 70 and 100.210 . Carriage \(10 /-\)
earh. post \(1 / 6\).
SYNCHRONOUS MOTOR. 200/250 volts A.C. 60 r.p.m., suitable for electric clocks. etc. \(25 /=\), post \(2 / 6\).
MAINS MOTORS. Capacitor 230 v. A.C. \(1 / 40\) th hp 1,400 r.p.m. \(55 /-\) post \(3 /\) GEARED MOTOR for model maker, small but powerful, \(12 / 24\) volts A.C./D.C. 4/8 r.p.m.. 35/- post. 2/6.
GEARED MOTOR \(220 / 240 \mathrm{v}\) AC 175 r.p.m. torque 15lb.in. Klason, 810 , cge \(15 /\) MAINS TRANSFORMER WITH RECTIFIER mounted on top. Giving 2 D.C. output of approx. 30 to 40 volts 1 amp. Price \(27 / 6\) each, post \(2 / 6\). SELENIUM METAL RECTIFIERS.
Charging Rectifters Full Wavo Bridge
12 Volts 1 Amp \(8 / 6\) each 24 Volts 1 12 Volts 2 Amps \(13 / 6\) each 24 Volts 2 Amp 12 Volts 3 Amps \(16 / 6\) each 24 Volts 3 Amps 12 Volts 3 Amps \(16 / 6\) each 24 Volts 4 Amps \(20 /\) each 24 Amps

13/- each
24/-each

Discounts for quantities of above charging rectifiers.
MAINS TRANSFORMERS to suit above rectifiers
12 Volts 1 Amp \(12 / 6\) each 12 Volts 4 Amps MT5 25/-each 12 Volts 2 Amps 24/- each CT109 12 Volts 4 Amps CT107 29/6 each

RESISTORS EX STOCK IN QUANTITY WIRE WOUND, HIGH
STABILITY GARBON ETC., BEST MAKES AT LOWEST PRIGE.


> ELECTRO-MAGNETIC COUNTERS COUNTJNG UP TO 9999

Type 16A
2,300 ohms \(75 / 230\)
15/- each. Post \(1 / 6\).
3 ohms \(2 / 6\) Vype 17A.C. \(15 /=\) each 3 ohms 2
Post \(1 / 6\).
VEEDER-ROOT MAGNETIC COUNTER. General purpose type with zero re-set K00 counts per minute up to 999999.48 volt D.C. \(55 /\), post \(2 / 6\). re-set. KKO counts per minute up to 999999 . 48 volt D.C. \(55 /-\) post \(2 / 6\).
MAP READING LAMPS, EX.R.A.F. NAVIGATOR'S CHART MAGNIMAP READING LAMPS, EX-R.A.F. NAVIGATOR'S CHART MAGNI-
FIERS 3in. lens complete with batteries, bulb and dimming switch \(12 i n\) long. FIERS 3in. len
\(37 / 6\), post \(2 / 6\).
\(37 / 6\), post \(2 / 6\).
THERMOSTAT SATCHWELL, 12 in . stem \(0 / 250\) volt A.C./D.C. 15 amps A.C. 10 to 90 degrees cent. \(25 /-\), post \(2 / 6\).

ROOM THERMO8TAT. Adjustable between 45 and 75 deg. Fahr., 250 v 10 amp. A.C. Ideal for greenhouses etc., \(35 / \mathrm{p}\), post \(2 /\) -
THERMOstAT. For frost protection, on at 34 deg . F., off at 49 deg . F., \(1 \frac{1}{2}\) amps. at 250 volts, adjustable, \(4 / 6\), post \(1 /\) -
8immerstat BY 8UNVÍC Plug-in type with knob control, 15 amps 3 -pin, \(200 / 250\) volts. \(35 /-\), post \(2 /-\)

\section*{L WILKIMEON (CiOYDON) LTD. \\ I? LANSDOWNE RD. CROYDON SURREY \\ Grams: WILCO CROYDON}


\section*{AEIGNMENT ANALYSER TYPE MC12}
A.C. MAINE, 2001250 Volts. Prorides:-
"WOBBTLATOR"
(8WEPT FREQUENCY) "WOBBULATOR" (SWEPT FREQUENCY) OPERATION, for PM/TV allgument Inew tranuency aweep up to 12 me/s. From \(400 \mathrm{kc} / \mathrm{m}-8 \mathrm{mc}\) m. CAPACITANCE \(0-80\) pf and \(0-120\) pf. BPECIAL FACILLTY enables true resonant frequency of any tuned uct, 1.P. tranabormer etr. to be fapidy determined. Cash price \(£ 6.19 .8\) and \(5 \%\) P. \& P. H.P. Lermi, 251 - depocit and \(\overline{51}\)

B.S.R. MONARCH UA8 with STEREO HEAD


4 -apeed playe 10 recomis 12 tn . 10 in ., or 7 in . at 33,45 or 78 r.p.m. Intermixes 7 in . 10 in . and 12 in . records of the eame speed. Eas manual play position; colour sbove baseboard 4 inn., below laseboand 2 fin. Fitted
 W. \& P. (Btandard Head £6.19.6 Plus 5/- P. \& P.)


\section*{player cabinet}

Finighed in 2 -tone leatherette, will take B.s.R. UAs, Fith rooro for amplliter and 7 in
Similar to the ahove in POLISHED WALNUT, will take Collaro.

3916 Pчиョノ- P. \& P.

\section*{13 CHANNEL TUNER incremental type}

34 to 38 Mc/e. complete with PCP80 and PCC84. Tested and guaranteed. Complete with atting instructions and knobs.

39/6 Plus 3/6 P. \& P.

AC/DC POCKET MULTI-METER KIT


Comprising 21n. moving coil meter, scale callbrated in A.O.ID.C. volts, ohmes and milliamps. Voltage range A.C. D.C. \(0.50,0-100,0-250,0-500\). Front panel, range switch, wire-wound pot (for obma zero setting), toggle switch, reaistors and metifler. Basic movement, 2 mA . In grey hammer finiah case.
196 г. Plos.
Bullt and tested
Point-to-point wiring diagram \(1 /-1 / 8\) extra.

MAIRS TRANSFORMERS

 and Decking on the above 3 .

\section*{SIGNAL GENERATOR}


Coverage \(100 \mathrm{Kc} / \mathrm{s} .100 \mathrm{Mo} / \mathrm{s}\). on fundamen tale and \(100 \mathrm{Mc/a}\). \(\mathbf{L o} 2 \mathrm{~mm} \mathrm{Mc/s}\) on harmonica.
 mer finiah. Itcorporsting tbre ministure
valves and Metal Bectifer. A.C. Mains 2onf 250 v . Interaal Modulation of 400 c c.p.d to \(a\) depth of \(30 \%\). Mndalated or untuod. ulated R.F. output contlunously variable 100 millivolts 0. .W. and mond. Bwitch, pariable A.F. outpat. Incnrpnrating magiceye
as output lndicator. Accuracy plins or minus ns output ladicator. Accuracy plas or minus

46/19/6
Or 25/- deposit and \(\begin{aligned} & \text { Post } \& \text { Packing 51- extra. }\end{aligned}\)

\section*{SIGNAL GENERATOR}

Coverage \(120 \mathrm{Kc} / \mathrm{s}-230 \mathrm{Kc} / \mathrm{s} ., 500 \mathrm{Kc} / \mathrm{s}\) \(900 \mathrm{Kc} / \mathrm{s} ., 900 \mathrm{Kc} / \mathrm{A} .-2.75 \mathrm{Kc} / \mathrm{s} ., 22.75 \mathrm{Mc} / \mathrm{B}\). \(-8.5 \mathrm{Mc} / \mathrm{s} ., 8 \mathrm{Mc} / \mathrm{s} .-28 \mathrm{Mc} / \mathrm{s}\). , if Mc/s. -58 \(\mathrm{Mc/s}, 24 \mathrm{Mc} / \mathrm{s} .-84 \mathrm{Mc} / \mathrm{s}\). Metal case 10in. \(x\) \(6 \mathrm{ln} . x 4 \mathrm{pin}\). Size of scale 6pin. \(x 3 \mathrm{hin}\). 2 Faives and rectifler A.C. mains \(230-250\). Internal modulation of 400 c.p.s to \& depth of 30 per cent. modulated or unmoduiated
Outout conttonoualy variable 100 millivoltis C.W. and mod-gwitch variable A.F. output and moviag coll output meter. Grey hammer \(\begin{aligned} & \text { Aninh case and whire panel. } \\ & \text { Accuracy plus or minus } 2 \%\end{aligned} \quad 8 / 4 / 19 / 6\)


\section*{SIGNAL \& PATTERN}

\section*{GENERATOR}
£6/19/6 \({ }^{\text {P. \& }}\) \& \({ }^{\text {P. }}\)
Or \(25 /\) deposit. P. \& P. 8/- and 6 monthly payments of \(21 / 8\).
8.-210 Mefs. In tive bands an on fundamentala, siow cootion tuning sudio output. 8 vertical and tinriznntal hars, log ging scale. In grey hammer tamished case wit \(\underset{200-250}{ }\) carring handle. Accuracy \(\pm 1 \%\) A.O. maln


\section*{F.M. TUNER UNIT}

Permeability tuned by famous German Manufactunar. Coverage 88-100 Mc/s Cormplete with ECCB5. 8ize 4in. \(\times\), 2in. \(\times 21 \mathrm{D}\).
\[
25^{\prime} \text { - Plus P. \& P. } 1 / 8 \quad \begin{aligned}
& \text { Ciccult diagram } \\
& \text { free with unit. }
\end{aligned} /=
\]

8 WATT PUSH. AMPLIFIER


COMPLETE WITH CRYSTAL MIKE AND SII. A.C. mina \(20012500^{2}\) Bize 10
 output pena, and rectifler. For une with alis makes and types of pich-up and mike. Negative feed-back. Two inpats. mise and gram. And controle for same. Reparate controlo for Bume sid Treble uft. Reepponse flat frnm 40 cyclee to
\(15 \mathrm{Kc} / \mathrm{s}_{\mathrm{s}} \pm 2 \mathrm{db}: 4 \mathrm{db}\). down at \(\mathrm{Kc} / \mathrm{fa}\). Outpue 8 watter at \(\delta \%\) totsl diktortion. Woise level 40 dh . down, all hum. Output transformer tapped for 3 and 15 obm speench ooils. For une with gtd. or P. records, musical linstrumente such the
£4.19.6
Plos P. \& P. 7/6.


\section*{6 watt PUSH-PULL AMPLIFIER}
A.C. malns \(220 / 250 \mathrm{p}\). Incorporating 4 velves and metal rectifer, 2 Inpata, h gh and low, and controls for same. Separate controle for Baes and Treble lift. Bise of chasest Ithn. « 4
\[
59^{\prime} 6 \quad P_{\&}^{P 10 a} \text { P. St. }
\]

2-TRANSISTOR POCKET RADIO
Plus Germanium dinde, fully tuneable over medium and ming waves. Bize sjin. * 41 in . x tha. Complete net of componenta tncinding came. 2 transistors and earplece rig disgratn 1/6. (Froo with kit.)
\[
196 \text { р. \& \& PR. } 1 / 1 / .
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\section*{PUSH-PULL OUTPUT STAGE}

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Foyle, \(\mathrm{W}_{\text {. }}\) \& G., Ltd.
Fringevision, \(\mathrm{L} t \mathrm{t}\).
Quartz Crystal Co. Ltd

These ranges of miniature condensers are additional to the many types of T.C.C. electrolytics already available, and will appeal to all concerned with the design and servicing of equipment in which space is limited.

They are constructed similarly to the well-proved T.C.C. Micropack Electrolytic, with aluminium tube and neoprene-faced disc end seals. Terminations are 22 s.w.g. wires, \(\mathrm{I}_{\frac{1}{2}}{ }^{\prime \prime}\) long, hot solder coated, making them suitable for printed circuit assembly.

The short length of these condensers permits horizontal mounting on printed circuit panels with hole centres as close as \(\mathrm{I}^{\prime \prime}\). Insulating Sleeving to cover the metal case (as illustrated in the top photo) is desirable for horizontal mounting and should be specified in such applications.

Temperature Rating : ability to work satisfactorily at \(70^{\circ} \mathrm{C}\) without voltage derating.


\section*{Types CE 132 and CE 134}
\begin{tabular}{|c|c|c|c|c|c|c|}
\hline \multirow[t]{2}{*}{Capacity in \(\mu \mathrm{F}\)} & \multirow[t]{2}{*}{\begin{tabular}{l}
Capacity \\
Tol in \%
\end{tabular}} & \multirow[t]{2}{*}{Peak Wkg. Volts DC.} & \multirow[t]{2}{*}{Ripple mA.} & \multicolumn{2}{|l|}{Dimensions in inches} & \multirow[t]{2}{*}{T.C.C. Type No.} \\
\hline & & & & Length & Diameter & \\
\hline 100 & \(-20+100\) & 6 & 15 & 15 & \(\frac{3}{8}\) & CEI32AE \\
\hline 100 & \(-20+100\) & 12 & 35 & \(\frac{15}{10}\) & \(\frac{1}{2}\) & CEI34BE \\
\hline 50 & \(-20+100\) & 12 & 15 & \(\frac{15}{16}\) & \(\frac{3}{8}\) & CEI32BE \\
\hline 50 & \(-20+100\) & 25 & 35 & \(\frac{15}{16}\) & \(\frac{1}{2}\) & CEI34CE \\
\hline 25 & \(-20+100\) & 25 & 15 & \(\frac{15}{16}\) & \(\frac{3}{8}\) & CE132CE \\
\hline 25 & \(-20+100\) & 50 & 35 & \(\frac{15}{16}\) & \(\frac{1}{2}\) & CEI34DE \\
\hline 12 & \(-20+100\) & 50 & 15 & \(\frac{15}{16}\) & \(\frac{3}{8}\) & CEI32DE \\
\hline 8 & \(-20+50\) & 150 & 30 & \(\frac{15}{16}\) & \(\frac{1}{2}\) & CEI34FC \\
\hline 4 & \(-20+50\) & 150 & 15 & \(\frac{15}{16}\) & \(\frac{3}{8}\) & CEI32FC \\
\hline 2 & \(-20+50\) & 350 & 7 & \(\frac{15}{16}\) & 3 & CE132LE \\
\hline 1 & \(-20+50\) & 450 & 7 & \(\frac{15}{16}\) & \(\frac{3}{3}\) & CEI32PE \\
\hline
\end{tabular}
A. sub-miniature range for hearing aid and transistor circuitry is also available.

\title{
SAVBIIT SOLDER GIVES UP TO TEN TIMES
}


The left hand bit was used with Savbit alloy and has made 10,000 joints. The centre bit was used for 1,000 joints and the bit on the right for 7,500 joints, each with a standard tin/lead alloy.

A small percentage of copper in Ersin Multicore Savbit Type 1 Alloy prevents absorption of copper from the bit itself. This extends the life of copper bits up to ten times.
There is no reduction in soldering speed. On the contrary, soldering efficiency is actually increased by the good condition in which the bits are kept. Savbit has been tested on many production lines and has proved itself superior to copperless solder. Please write for further information to the Multicore Service Department.

\section*{SAVBIT FOR THE} SMALL USER
'The. Size' I Garton contains approximately 53 ft . of I\& S.W.g. SAVBIT. It is also supplied in 14 s.w.g. and 16 s.w.g. Obtainable from-radio and electrical stores. Ersin Mufticore 5 -Core Solder is also supplied in 4 specifications of Standard Tin/Lead alloys. Price 5/- each (subject).

\section*{SAVBIT FOR FACTORIES}

Ersin Multicore Savbit Type \(I\) alloy containing 5 Cores of non-corrosive flux is supplied to factories flux is supplied to factories
at bulk prices on 7 lb . reels. at bulk prices on 7 lb . reels. 16 and 18 s.w.g. are the diameters most suitable for the majority of soldering processes. Supplies are also available on I lb. reels.

\section*{STANDARD TIN/LEAD ALLOVS}

Ersin Multicore 5-core Solder is available in the following standard alloys:
\(60 / 40,50 / 50,45 / 55,40 / 60,30 / 70\), and 20/80 and in 9 gauges on 7 lb . and 1 lb . reels.

\section*{SPECIAL HIGH AND LOW MELTING POINT SOLDERS}

Comsol (Melting point \(296^{\circ} \mathrm{C}\) )
P.T. (Melting point \(232^{\circ} \mathrm{C}\) )
L.M.P. (Melting point \(179^{\circ} \mathrm{C}\) )
T.L.C. (Melting point \(145^{\circ} \mathrm{C}\) )

\section*{SAVBIT FOR THE SERVICE ENGINEER}

Approx. 170 ft . of 18 s.w.g. SAVBIT is supplied on a 1 lb. reel packed in a carton. Price 15/- each (subject).

\section*{HOME CONSTRUCTOR'S 2/3 PACK}

Now available containing alternative specifications: I9 ft. of 18 s.w.g. \(60 / 40\) alloy or, for soldering printed circuits, 40 ft . of 22 s.w.g. 60/40 alloy. Both wound on Reels. \(2 / 6\) each (subject).

\section*{Bib RECORDING TAPE}

\section*{SPLICER}

Recording enthusiasts can effect considerable tape economies with this splicer. It makes the accurate jointing of tape so simple and quick that every scrap can be used. \(18 / 6\) each (subject).

A free copy, of an interesting article "How to Edit Tape Recordings" will be sent you if you will kindly send us a stamped addressed envelope.```


[^0]:    (C) Iliffe \& Sons Ltd. 1959. Permission in writing from the Editor must first be obtained before letterpress or illustrations

[^1]:    * G.E.C. Research Laboratories.

[^2]:    *B.B.C. Rescarch Departmerit.

[^3]:    *University of Manchester. A more detailed account of the system is $\bar{q}$ ven in ${ }^{\text {a }} \mathrm{A}$ System for the Autois g ven in A Aysten Patterns," by ${ }_{\text {R. L. L. }}^{\text {mecogimstale. }}$ F. H. Sumner,
     C. J. Tunis and Part 106 , p .210 (March. I.E.E., Part B, 106, p. 210 (March, ${ }^{1959) .}$
    $\dagger$ Fournier D'Albe. Proc. Royal Soc.,., 90 (1914).
    $\ddagger$ ""Reading , by Electronics," Wireless World, April, 1957.

[^4]:    * See Wireless World. Vol 65, p. 126 (March. 1959).
    " "Masers" by "Cathode Ray," Wireless World, Vol. 65, p. 197 (April, 1959).

[^5]:    - Boulder Laboratories, National Bureau of Standards, U.S.A
    + From information obtained antenna gains were aimost identical t From information obtained antenna gains were anmost ransmitter outputs were not the same, however, some being 50xW others 70kW. Ed.

[^6]:    * Incidentally, how few books warn their readers that the - vectors" used in a.c. diagrams are not vectors at all in the strict sense! Without such a warning, one may well wonder how a non-vecturial quantity such as p.d. manages to appear in a diagrarn as a vector.

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