

37-way moulded-on polypole coupler.

## custom-built



# Wireless World 

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and so Mullard will be bringing you many interesting details of What's New in the New Sets - new devices, new developments, and the latest production techniques in Mullard's constant endeavour to contribute to better radio, television and sound reproduction.

## BY 100 high

## performance

## silicon

 rectifier

Mullard have released a new silicon diffused junction rectifier, type BY100, for use as a mains rectifier in television receivers. This rectifier has a maximum recurrent peak inverse voltage rating of 800 V and will pass a maximum average forward current of 550 mA at an ambient temperature of $50^{\circ} \mathrm{C}$. The maximum forward voltage drop is 1.5 V at 5 A and the maximum ieverse current is $10 \mu \mathrm{~A}$ at 800 V . The small size of the BY100 is an obvious advantage and allows greater flexibility in positioning the device in the receiver and in effecting a reduction of localised heating.

## Improved Cathodes

## For Television Frame-Grid Valves

All television frame-grid valves manufactured by Mullard now use locked-seam cathodes in place of drawn and pressed cathodes. The new cathode is made on an automatic four-slide machine which cuts and folds a nickel strip into the appropriate size and shape. This new process has reduced contamination of the nickel and has made possible adjustments to the amounts of trace elements used in the preparation of the nickel strip. These adjustments give improved insulation between the electrodes while maintaining the level of emission and length of emission life. In fact, over the periods of life expected in a television receiver, these valves, when used under normal operating conditions, show a negligible rate of failure from emission faults.

## - <br> What's Behind Automatic Brightness Control

Now a feature of many sets, automatic brightness control adjusts the television receiver to give the best picture for the room lighting conditions. The control consists of a photoconductive cell, for example, Mullard types ORP12 or ORP60, mounted on the front of the receiver. Alterations in the room lighting change the electrical characteristics of the cell and these changes are used to control the picture brightness and contrast.

# Polyester Foil Capacitors 

The recent introduction of a new range of capacitors is the result of the Mullard Research Laboratories' continuous study of new materials likely to be of use to the electronics industry.
Following an investigation into plastic materials,? the new range of capacitors was developed, using a plastic material, a polyester, as their dielectric.

This material can be manufactured in the form of very thin homogeneous films having a higher insulation resistance and dielectric strength than the more usual paper foils. These properties are maintained to high temperatures making them particularly suitable for use in modern compact television receivers. To make full use of the high temperature
properties of the film, the capacitors are coated with a special waterproof and high melting point lacquer.


Two voltage ratings are available, namely $125 v$ and 400 v D.C. with capacity values ranging from $.00 \mu \mathrm{~F}$ to $1 \mu \mathrm{~F}$.

## Fair of the Air

THIS year the National Radio Show reflects the atmosphere of expectancy which for some time now has surrounded the workings of the Pilkington Committee. In many cases expectancy has been followed by active anticipation and sets have been produced to receive the u.h.f. bands and dual line standards which many people think the Committee may propose and the Postmaster General may or may not approve. The B.B.C., too, will be showing what they could do in colour if only they were given the green light.

Some people will stigmatize these moves as tendentious, an attempt to force the hand of the Pilkington Committee; others will point to the inconsistency of manufacturers who collectively, through their associations, advocate the retention of 405 lines, but who will be demonstrating 625 -line receivers at Earls Court on signals provided by Radio Exhibitions Ltd., an off-shoot of B.R.E.M.A. As we see it there is nothing inconsistent in advocating and hoping for stability, but at the same time hedging against inflation-whether it be of monetary values or of line standards. In any case many of the 625 -line sets will be ostensibly for export only.

The demonstrations of colour will be a great success and will give many members of the public who have so far only read about it the pleasure of seeing the technical excellence of the pictures which can be transmitted-and received in areas of good signal strength.

Comparative demonstrations of 405 - and 625 -line standards will, we think, provide plenty of good clean fun. It will be amusing to try to guess, from the size of screens used and any differences in the degree of interlace, into which camp any particular manufacturer has wittingly or unwittingly placed himself. Seriously, we think the differences in picture quality will be marginal and we would suggest that if demonstrations on the floor of the hall are inconclusive a visit to the gallery and a glance at the monitor screens through the windows of the R.I.E. control room might help to give the casting vote. Many of the 625 -line receivers on show will be export models and so the signals distributed to the stands will be on one or other of the Continental 625 -line standards. It should not be forgotten, however, that the Television Advisory Committee in its 1960 report recommended modifications to those standards in the event of the adoption of 625 lines in the U.K. The improvements may be "marginal but definite" and we only mention them here to underline our main point, that the demonstrations
which will be put on for our enjoyment at the Show should not be used at this stage to form hard prejudices.

The general public, for whom the Show is primarily intended, will be unaware of and therefore not unduly perplexed by these considerations and will tend to see these things metaphorically in black and white (and literally, too, for the line structure will not be so apparent in colour). They are likely to be more confused by the association of famous names-hitherto rivals for their custom-on the stands of some of the new and even larger company groups. At one time these associations were kept as quiet as possible, on the principle that if a customer gave a bad name to brand $\mathbf{X}$ you still had the chance of selling him virtually the same set under brand Y . These days are past, largely due to the motor manufacturers who make no secret of selling the same car under different names. But the customer still has the choice of a different radiator grille, and knows that the initial price and the cost of service and spares would probably be much higher but for the rationalization of basic production.

Last year we deplored the fact that the Pye Group had decided to hold their own Show outside Earls Court and we are glad to see them once again in the main exhibition. This year it is the turn of G.E.C. (with Sobell and McMichael) to invite us to make the journey to another part of London in order to see their products and their own demonstration of colour television. Once again we think it a pity that last minute differences between the organizers and some of their principal cxhibitors cannot be resolved in time to make a national show truly representative of all that this country has to offer in television and sound broadcasting.

## Brit.I.R.E.

BY an Order in Council dated 2nd August Her Majesty the Queen has granted a Royal Charter to the British Institution of Radio Engineers. Since it was founded in 1925 the technical standard of its meetings and published papers has not only reached but has been sustained at the highest level. It has drawn the support of many eminent figures in radio and electronic engineering and has formed a focal point for workers in these professions throughout the Commonwealth. We offer congratulations to the members and administrative body of the Institution on this authoritative recognition of their efforts and achievements.

# Listening in the Next Room 

WHy There is an apparent Improvement in sound quality

By J. MOIR, M.I.E.E.

IIANY people have noted that "my loudspeaker sounds better when I listen in the next room", and have wondered why this should be so. Clearly a difficult question to answer when we do not understand all the factors that result in one loudspeaker "sounding better" than another one, though the reasons for the gross differences are, of course, well understood.

Whether a loudspeaker does sound better in an adjacent room is clearly a matter of opinion. In most instances the judgement has been the result of a casual observation rather than a laboratory experiment, but the view has been independently expressed so frequently that it probably has some significance. I have also noted the same phenomena, and, in consequence, decided to explore the objective performance of a loudspeaker playing in an adjacent room to see if there is any reasonable explanation of the reported improvement.

In every instance sound quality was reported to improve only when orchestral music was being played. Comment about speech reproduction


Fig. 1. Effect of microphone/loudspeaker spacing on frequency response.
varied, but in no instance was any significant improvement noted when the listener moved into the adjacent room. Under these conditions, speech required more concentration (i.e. intelligibility was lower) but there was some comment that "speech sounds very natural". In every instance the communicating door between the two rooms had to be wide open to achieve an improvement in sound quality, all those questioned being in agreement that with the door closed or even slightly open the top response suffered. Again, all were in agreement that sound quality was adversely affected when judged in the room above that in which the loudspeaker was playing.
"Sounding better" is a rather nebulous description of a change in sound quality. An improvement in quality may result from a modification in the effective frequency response at the listening position, or from some reduction in the intrinsic distortions produced by the loudspeaker. As a third alternative the sound may be improved by some advantageous change in the acoustic environment
resulting from listening in the adjacent room. These suggestions will be examined in turn.

The frequency response as measured at a remote listening position may differ radically from that measured nearer the loudspeaker, particularly if the rooms have widely different furnishings. As the measuring microphone is moved away from the loudspeaker the contribution of the direct sound from the loudspeaker to the total acoustic intensity at the measuring position becomes less significant. The indirect sound, the result of room reverberation, then constitutes the major part of the total acoustic power at the listener's ears. Now the energy spectrum of a complex sound wave is modified at each reflection from a boundary surface, the general effect being a reduction in the high-frequency content, for most wall finishes and furnishings are more effective absorbants at the high audio frequencies than they are at the low-frequency end of the spectrum. Thus the measured frequency response will generally exhibit a progressive reduction at the high-frequency end as the microphone is moved away from the loudspeaker. This is illustrated by Fig. 1 which shows the result of some measurements on a Quad electrostatic loudspeaker in a well-furnished room.

## Coupling Between Rooms

There is a second effect that may also introduce some frequency discrimination. An opening between two rooms does not transmit sounds of all frequencies with equal efficiency. At low frequencies the standard door opening ( 6 ft 6 in by 2 ft 6 in ) is a fraction of a wavelength and thus gives a relatively inefficient coupling between two rooms. The actual coupling efficiency is a function not only of the area of the opening, but also of the size and shape of the two rooms and the position of the communicating opening in the common wall. At the top end of an audio spectrum a standard door opening is many wavelengths wide and is likely to give efficient coupling between the rooms.

The increase in coupling efficiency at the higher audio frequencies tends to offset the increase in room absorption in the same part of the audio spectrum, and thus the frequency response as measured in the second room may not differ widely from that found in the loudspeaker room. A calculation of the overall result is difficult and probably pointless in view of the many variables, but Fig. 2 illustrates the results of measurement in two rooms in the writer's house.

The curve was obtained by driving the loudspeaker (not the speaker used to obtain the data for Fig. 1) from a white-noise source and measuring the sound pressure level in bands one-third of an octave wide between $50 \mathrm{c} / \mathrm{s}$ and $10 \mathrm{kc} / \mathrm{s}$. The measurements were carried out in two adjacent


Fig. 2. Speaker frequency response in loudspeaker and listening rooms.
rooms. In this particular instance the top response is not appreciably attenuated in the second room, but the bass response below about $160 \mathrm{c} / \mathrm{s}$ shows an increasing loss. Unless further tests showed this to be typical it would not appear to be very significant.

There seems no reason to expect that the intrinsic distortions introduced by the speaker will be reduced by the presence of the second room, but they may become less noticeable when heard in an adjacent room. A non-linear relation between electrical input and the resultant sound pressure implies the appearance of harmonically related tones and, when a complex wave is being reproduced, the introduction of inharmonically related intermodulation products. Harmonics do not result in any very significant subjective annoyance, but the accompanying intermodulation products introduce roughness, and create "blurr", and this is extremely annoying. Listening in the adjacent room may well reduce the high-frequency response, and this will reduce the amplitude of the higher harmonics, but it will do little to modify the intermodulation distortion products, for being difference tones many of these will be close in frequency to the primary tones. Thus there is no very good reason for expecting that any improvement in sound quality due to listening in the adjacent room is the result of a reduction in nonlinear distortion.

Doppler distortion, the introduction of frequency modulation products as a result of the use of a single diaphragm sound radiator, may well be slightly reduced by listening in an adjacent room. These distortion products are concentrated in the direct sound on the speaker axis and do not exist in the plane of the diaphragm. Any change in the acoustic environment that results in a decrease in the ratio of direct to reverberant sound will reduce the annoyance created by this form of distortion. Normally it does not make a very significant contribution to the total distortion, so it is unlikely that any reduction due to adjacent room listening will result in any very noticeable improvement in overall sound quality.

Significant annoyance can be created by the presence of lightly damped, mechanically resonant elements in a loudspeaker cone or chassis. Such elements continue to "ring" after the driving impulse ceases and thus colour the reproduction to an extent quite out of proportion to their effect on the steady-state response curve. Their subjective effect is likely to be reduced by listening in an adjacent room merely because any room introduces ringing of the same general kind and two rooms introduce twice as much distortion of this type as one room. An increased amount of room ringing might
dilute similar distortion introduced by the speaker itself, but while it is impossible to be dogmatic, reduction of the effect of speaker ringing is not thought to make a significant contribution to any improvement in sound quality that results from listening in an adjacent room.

The sound transmission loss introduced by a standard wooden door or the usual board-on-joist ceiling is so frequency-dependent that it might be expected to result in unacceptable sound quality in an adjacent room or in a room above. A typical plywood door will introduce a loss at $10 \mathrm{kc} / \mathrm{s}$ (relative to the loss at $1 \mathrm{kc} / \mathrm{s}$ ) of about $10-12 \mathrm{~dB}$, while a plasterboard joist and board ceiling will result in a relative loss of 25 dB . Average values for doors and ceilings are shown in Fig. 3, but the sound insulation value of a door is critically dependent upon the leakage through cracks round the jamb.

Measurement of the attenuation introduced and observations on the sound quality that results from listening in an adjacent room under "door closed" conditions are at least in fair agreement.

## Reverberation Change

On reviewing the previous discussion it seems reasonable to suggest that none of the factors mentioned is likely to account for the reported improvement in sound quality due to listening in an adjacent room. The effect on frequency response should, from the conventional viewpoint, only result in a deterioration in sound quality, but in this particular instance the change is probably too small to be significant. However, let us look at some of the more predominantly acoustic factors that affect the quality of reproduction.

An æsthetically satisfying orchestral performance is only secured when the direct sound reaching the ears without any reflection is softened and rounded by the presence of a proportion of reverberant sound. The ratio of direct to reverberant sound is generally adjusted at the studio either by placing the microphone at a suitable distance from the orchestra or


Fig. 3. Average transmission loss due to doors and ceilings.
by mixing into the output of a microphone close to the orchestra a suitable amount of sound from some more remotely placed microphones. There is some evidence that even when the optimum spacing of microphone and orchestra for a monophonic transmission is achieved, the result is less satisfying than that obtainable from a two-channel transmission.

At the receiving end, the amount of reverberant sound can be increased by moving away from the loudspeaker, though a limit to the effect is set by the reverberation time of the listening room. Any further addition can only be achieved by moving out of the room and into the adjacent room. The imme-
diate result will be to produce a listening space of increased volume and having (possibly) a longer reverberation time.

There is no simple method of calculating the combined reverberation time of two rooms coupled by a communicating opening, for the combined value is a function of the area and position of the communicating opening, and of the relative positions of loudspeaker and microphone. As a simplification that applies when two typical domestic-sized rooms of roughly equal size and similar furnishing are coupled by a standard door, it can be said that the reverberation time of the combined volume is roughly $\sqrt{ } 2$ times that of either room. This would not hold if the reverberation time of the individual rooms differed appreciably.

Thus both the physical and acoustic size of the listening environment is increased by moving into an adjacent room. This is thought to be a significant advantage. As a result of listening tests carried out some years ago, the author came to the conclusion that good sound quality could not be secured in a room having a volume less than (roughly) 1,600 cubic feet and that between rooms of about 1,000 cubic feet and 1,600 cubic feet there was a very rapid improvement in sound quality with increase in room volume. Above about 2,500 cubic fect the rate of change of quality with further increase in volume decreased, though the quality continued to improve with increase in room size.

It may well be that in most of the instances of improvement that have been reported, the volume change produced by adding the second room happened to fall on the steep portion of the sound quality/room volume relation suggested above.

## Room Resonances

However, in my own personal experience, the subjective effect of listening in an adjacent room is that one is in a room very much larger than a single room having the volume of the combined rooms. The change is one of character rather than quantity of reverberation. This may be due to the following properties of coupled rooms.
Any room exhibits a series of room resonances (eigentones is the fashionable word) the frequencies of which are determined by the room dimensions. Resonance occurs at each of the frequencies at which the length, width and height are half a wavelength, and at harmonics of these frequencies. Thus there are three independent series of resonances, one for each of the three axes of the room. In addition there are other series of resonances corresponding to the combination of the three axial dimensions, though there is some cvidence that these are not particularly important in determining the acoustic character of a room.
Rayleigh deduced an equation relating room dimensions and resonance frequencies

$$
f=\frac{\mathrm{V}}{2} \sqrt{\frac{\mathrm{~A}^{2}}{\mathrm{~L}^{2}}+\frac{\mathrm{B}^{2}}{\mathrm{~W}^{2}}+\frac{\mathrm{C}^{2}}{\mathrm{H}^{2}}}
$$

where L is the length, W the width, H the height, V the velocity of sound and A, B, C independently any of the integers $0,1,2,3,4$, etc. For a typical room ( 15.3 ft by 1 lft by 8.2 ft ), Fig. 4 shows the first 10 resonant frequencies. This room is perhaps larger than the average listening room, but it will be seen that all the resonances fall in the lower part of


Fig. 4. Typical eigentone spectrum for a small room.
the audio band. For a smaller room the resonance frequencies would appear at correspondingly higher frequencies and their effect would be subjectively more obvious.

It will be noted from Fig. 4 that the resonances in the bwer end of the range are well spaced apart, the spacing decreasing with increase in frequency. Apart from changing the shape of the room, nothing can be done to modify the spacing of the resonances or to decrease the gaps between the individual resonance frequencies. However, if one listens in an adjacent room coupled by a relatively small opening, the eigentones corresponding to each room exist separately. When the dimensions of the listening room differ from that of the loudspeaker room, the eigentone spectra of the two rooms will interlace and tend to reduce the gaps that exist in the resonance spectrum of any single room.
All the eigentones corresponding to the sum of those characteristics of the separate rooms will not exist in the coupled rooms, for the coupling between rooms will be weak for those modes of resonance in which the air particles are moving parallel to the door opening. Nevertheless, in a typical example the number of modes that are excited will be much greater than that of either room considered alone, or in a single room having a volume equal to that of the combined rooms. Thus the overall acoustic performance of two coupled rooms is considerably smoother than that of any single room unless the single room is so large that the first ten (approximately) resonance frequencies are approaching the sub-audible, and thus have no very significant effect on the sound quality.
The acoustic performance of a small (domestic size) room is determined almost entirely by the eigentone spectrum and particularly that part of the spectrum below about $200 \mathrm{c} / \mathrm{s}$. Any smoothing of the spectrum should make the small room performance approach that of a much larger room; it should in fact convert a domestic sized room into the domestic equivalent of a small hall.
Finally, there is the possible effect of the size of the sound source. When listening in an adjacent room the effective source of sound tends to be the door opening and not the loudspeaker. This increases the source size by a large factor, an area increase in the region of two hundred times taking the example of a 12 -in speaker and a standard 6 ft 6 in by 2 ft 6 in door. Not all critics are in agreement on this point but I believe that a large sound source results in a softness and lack of irritation in listening that cannot be achieved with a small source. The reason for this is not particularly clear and in the situation being discussed it may not be particularly important, but at least the change in size is a change in the direction of improving the sound quality.

A number of possible explanations for the improvement in sound quality have been discussed, and there may be others, but it is impossible to be sure which, if any, of the suggested mechanisms of improvement is really significant. The coupling between a room and the loudspeaker is so poor that the intrinsic performance of a speaker is unlikely to be affected by the relatively small change produced by opening a door into a second room. This suggests that it is the acoustic environment of the listener that is significantly changed when he moves into an adjacent room. Of the explanations discussed, smoothing of the eigentone spectrum appears most likely to result in an improvement in sound quality, but the apparent lengthening of the reverberation time (using the conventional definition) may also contribute. Both these effects are characteristic of a small hall and this agrees with the subjective assessment of the effects produced by moving into an adjacent room.

The absence of any suggestion that speech "sounds better" and the comment that "speech
sounds very natural " is qualitatively consistent with the improvement on music being due to smoothing of the eigentone pattern rather than to any increase in reverberation time.

The only experimental observations that may be at variance with the suggested explanation of "eigentone spectrum smoothing" is that I have never met an example where sound quality was improved by opening a door into a second room while listening in the first room. In my experience this almost invariably results in a degradation in sound quality though I have no other observers' comments on this listening condition.

Any well-founded conclusion would require an extensive investigation first to decide whether there really is an improvement in sound quality when listening in a room adjacent to that containing the speaker system. If this was confirmed then a fairly large number of specific examples would have to be examined in detail to see whether there were any common factors. An interesting but unremunerative project.

## SCOUT SATELLITE EQUIPMENT

THE photograph on the right shows an e.h.t. generator producing 1.6 kV for the counter tubes used to detect X-radiation in the Scout research satellite, UK Scout 1. Designed by Bristol Aircraft for the Space Research Group at University College, London, the generator will have to supply power for as long as a year and maintain the voltage stable in the face of a variation of supply of $\pm 15 \%$.

A single-transistor $8-\mathrm{kc} / \mathrm{s}$ oscillator, drawing 80 mW at 6.5 V , has its output stepped up by a transformer and quadrupler rectifier. The high voltage is then smoothed to contain less than $0.005 \%$ ripple and stabilized by a corona stabilizer tube to within 1.5 V at 1.6 kV .

The completed unit is $5 \frac{1}{2}$-in in diameter and the components are coated with polysulphide rubber and "potted" in foamed synthetic resin. This will prevent discharges during the reduced air-pressure phase encountered as the Skylark rocket lifts UK Scout 1 into orbit.

The photograph below shows an eight-channel capacitor data storage unit for electron density measurements made in the same satellite. This unit has been developed by G. \& E. Bradley Ltd., for the Electron Physics Department of Birmingham University.


Dato store.

E.h.t. generator.

Information on the maximum electron density in the first ten seconds of each sixty-one second period is gated into the store. It is read out towards the end of this period either to the telemetry system for immediate transmission to earth or to magnetic tape for subsequent transmission at a more convenient time. The sequence of operations is erase, gate, read in, store and read out, the timing being obtained from the satellite master clock.

This unit contains 180 components (mostly silicon diodes and transistors) in a space $1 \frac{1}{4}$ in by $5 \frac{1}{4}$ in diameter. It weighs about 8 oz , unencapsulated.

Radio Valve Data: A.E.I, have asked us to point out that the address of their Electronic Apparatus Division was omitted from p. 123 of the seventh edition of Wireless World "Radio Valve Data." All enquiries concerning semiconductor products listed as "A.E.I." should be sent to Associated Electrical Industries, Ltd., Electronic Apparatus Division, Carholme Road, Lincoln.

# Transistor V.H.F. Amplifier 

FRINGE AREA F.M. RECEPTION

By F. BUTLER

UNTIL recently the high cost of v.h.f. transistors has discouraged their use in domestic broadcast receivers, although a study of the characteristics of such types as the Philco/Semiconductors 2N502 and Texas Instruments 2 G 101 or 2 G 102 shows that they should perform well in the $80-100 \mathrm{Mc} / \mathrm{s}$ frequency range. Data sheets ${ }^{1}$ have in fact been produced by Texas Instruments giving designs suitable for use at $100 \mathrm{Mc} / \mathrm{s}$ and also at $200 \mathrm{Mc} / \mathrm{s}$.

In the autumn of 1960, Semiconductors Ltd. released technical data on a range of inexpensive transistors, including one, Type T 1832, having a maximum frequency of oscillation around 1,300 $\mathrm{Mc} / \mathrm{s}$. Substantial price reductions of the Texas transistors have also been made. Samples of all these units have been tested by the writer in a simple 2 -stage tuned amplifier designed to form the front end of a conventional f.m. tuner (Eddystone Type 820), in order to increase the sensitivity sufficiently for use in fringe areas with a simple indoor dipole aerial.

With minor modifications this unit has been in continuous use for some months and has made a worth-while improvement in the performance of the tuner, particularly during periods of poor v.h.f. wave propagation.

A single-stage tuned amplifier using a good transistor in the common-emitter connection will give a gain of $15-20 \mathrm{~dB}$ and will have a noise figure around 5-7 dB. For stability with this high gain the amplifier must be neutralized or unilateralized. Extra components are required and the adjustments become tedious unless a fair amount of test equipment is available. If very high $Q$ coils are used the bandwidth may be inadequate for high quality f.m. reception while the use of broad-band lossy circuits will cause a substantial decrease in gain. An alternative is to use two low-gain broadband stages in
tandem. Under favourable conditions one can then dispense with the neutralizing components. Experience shows that with purely resistive terminations it is easy to construct a stable high gain amplifier using two grounded base transistors in cascade but that when an aerial is connected to the input through a transmission line, and when the amplifier output is connected to a receiver instead of a pure resistance load, a rather drastic gain reduction may be required to maintain stability. The judicious use of damping resistors backed by a careful choice of component values will normally result in stable operation over a wide range of temperature and supply voltage changes.

A recent paper ${ }^{2}$ on the measurement of transistor power gain and noise figure at frequencies up to $100 \mathrm{Mc} / \mathrm{s}$ contains much information of value to the circuit designer and indicates the performance which can be achieved using currently available transistors. With some types an increase of emitter current results in a substantial increase in gain, accompanied by a reduced noise figure. With all types there is a progressive reduction in gain as the operating frequency is raised from 30 to around $100 \mathrm{Mc} / \mathrm{s}$. Gain and noise figure are not the only factors which must be considered in designing a transistor amplifier. It will be found that in respect of cross modulation the performance of transistors is much inferior to that of conventional valve amplifiers. Too much gain will also bring in a number of unwanted continental v.h.f. transmissions and unless the first oscillator and mixer stages are very well designed there may be some pulling or f.m. of the oscillator frequency. There may also be a degradation of the receiver performance in respect of a.m. suppression and in the degree of reduction of impulsive interference.

Before considering a practical amplifier circuit it


Fig. 1 Circuit diagram of v.h.f. preamplifier. The transistors can be Semiconductors T/832 or 2N502, or Texas Instruments 2GIOI or 2GIO2

Layout of the preamplifier, seen from below the chassis. The sides, shown flat, should be bent upwards 'out of the page'

is worth comparing the merits of tunable versus broadband amplifiers. The tunable version is clearly acceptable if it forms an integral part of a complete receiver, since its tuning mechanism can be ganged to the oscillator control. It is a nuisance if it is used with a separate receiver because tuning then calls for the manipulation of two controls. Against this, cross-modulation is likely to be worse with the broad-band amplifier and, for transistors with a limited gain-bandwidth product, the gain is necessarily lower than for a narrow band amplifier. On balance, it may be advisable to accept the necessity for additional controls when a fairly high gain with a reasonably low noise figure are the prime requirements.

## Practical Amplifier Circuit

The complete circuit diagram of an experimental amplifier is shown in Fig. 1. The arrangement is entirely conventional and calls for little comment. Both amplifier transistors are operated in the earthed base mode and the bias network components are chosen to ensure thermal stability over a wide temperature range. The input impedance of $Q_{1}$ is rather higher than the characteristic impedance of the 75 -ohm coaxial cable from the aerial, but the mismatch is not so serious as to warrant the inclusion of a broadband transformer. Instead, a supplementary resistance may be used to terminate the cable. Its value should be in the range of 100-200 ohms.

The aim to be achieved in the design of the interstage and output circuits is to get the maximum possible gain consistent with stability and at the same time to ensure that the loaded $Q$ of the circuits is low enough to give the necessary bandwidth for distortionless f.m. reception.

The coupling network between the two transistors is required to match the output impedance of the first stage to the input impedance of the second. For use at a single frequency a pi-network consist-
ing of a coil and two capacitors is convenient for this purpose: Design data for such networks can be found in Terman, "Radio Engineers' Handbook," Ist Edition, p.p. 208-214. The simple pi-network is less suitable for use in an amplifier which is required to be tunable over a range of frequencies by variation of a single capacitor. A satisfactory compromise is to use a hybrid coupling system in the form of a pi-section with a variable capacitor only at the input end and to secure an impedance match by connecting the load to a suitable tap on the tuning coil. The transistor standing collector-current is fed through a 560 -ohm resistance into the network at a lowimpedance point without serious reduction of the unloaded Q of this circuit.

The output tuned circuit provides an impedance match between the second transistor and the input impedance of the f.m. tuner connected to the output end. Except for one coupling capacitor ( 820 pF instead of 41 pF ), the components in both networks are identical. Each circuit is tuned by one element of a 2 -gang, $3-50 \mathrm{pF}$ tuning capacitor which in fact covers a frequency range well in excess of the f.m. band $85-100 \mathrm{Mc} / \mathrm{s}$. This allows considerable latitude in the construction of the associated tuning coils. If desired, smaller variable capacitors may be used in conjunction with some fixed parallel capacitance so that the desired band is just covered by the full range of capacitance change.

The choice of tapping points on the tuning coils is not at all critical and a centre tap is actually used. This gives sufficient damping to guarantee stability and the bandwidth is well in excess of the f.m. requirement. Higher gain, with a correspondingly smaller bandwidth, requires the tapping point to be brought nearer to the output end of the network. Lower gain (and less risk of instability) will result if the tap is made nearer to the input (collector) end of the tuned circuit.

The remaining components on the diagram in-
clude coupling capacitors, decoupling components and filtering elements. The values of these are not particularly critical although it is possible that more precise matching could be achieved by a more carcful choice of coupling capacitors.

## Construction and Alignment

The amplifier is assembled on a small aluminium chassis $\sin \times 3 \frac{1}{2}$ in $\times 1 \frac{1}{2}$ in deep, the ends being left open for easy access when wiring. The 2-gang tuning capacitor is mounted on the flat top and the rear panel carries the battery terminals and the coaxial input and output sockets.

Two 6 -way ceramic insulated tag strips serve to support most of the components, ground connections being made to low-inductance copper straps bolted to the metal chassis.
The two tuning coils are self-supporting and each consists of six turns of 18 S.W.G. enamelled copper wire wound on a $\frac{5}{6}$ in round former $1 \frac{1}{4}$ inches long. Before winding, the enamel covering should be scraped from the middle of each length of wire and the cleaned portion carefully tinned to simplify the subsequent connection of a centre tap. The point-topoint wiring diagram in Fig. 2 is self-explanatory. For clarity the folded sides of the chassis are shown developed flat. They are actually bent through a right angle along the dotted lines.
Alignment consists simply of tuning to a programme nearest to the high frequency end of the range and squeezing or expanding turns on the tuning coils until the maximum signal is received, re-tuning the capacitor after each operation on the
coils. Tracking will then be found to hold over the remainder of the range.

## Performance

At $90 \mathrm{Mc} / \mathrm{s}$ the power gain between 75 -ohm resistive terminations is at least 30 dB and the amplifier remains quite stable. This gain figure is an artificial one and must be regarded with caution if the amplifier is used between a reactive source and load. Under some conditions the use of an excessively high collector voltage will provoke instability at frequencies around the maximum of $100 \mathrm{Mc} / \mathrm{s}$. Even with reactive terminations, stability can always be achieved at one selected frequency by coniugate matching at both input and output of the amplifier. In principle this is a simple operation, calling for equal resistances and equal but opposite reactances on both sides of the matching terminals. In practice, the adjustment required is a function of frequency and is difficult to maintain over a wide range of frequencies. Except in the case of gross mismatching of impedances, a moderate reduction in collector voltage and current is sufficient to ensure unconditional stability.

## REFERENCES

1. Texas Instruments, Ltd. Application Note No. 2: "Operation of V.H.F. Transistors with Collectors Earthed." Application Note No. 4: " V.H.F. Amplifiers Using Diffused-base Mesa Transistors."
2. Transistor Measurements: Power Gain and Noise Figure at Frequencies up to $100 \mathrm{Mc} / \mathrm{s}$. B. N. Harden and R. W. Smith, Electronic Technology, February 1961, p. 58.

## S.B.A.C. EXHIBITORS

WHEN one considers that some $20 \%$ of the capital cost of "military" aircraft such as the Buccaneer is for its electronic and radio equipment, it is not surprising that this aspect of aeronautics will be well represented at the Farnborough Air Show (4th-10th Sept.), organized by the Society of British Aircraft Constructors. Almost $40 \%$ of the exhibitors in the static exhibition are showing electronic or radio equipment (see list below). As already announced, we hope to include in our next issue a survey of the trends in aeronautical electronics as seen at the show.
A.E.I.

Airmed
Airscrew Co \& licwood
Amalgamated Wireless (Aust.)
Amphenol-Borg
Amplivox
B.I. Callender's Cables

Bakelite
Bell Precision Engg. Co
Belling \& Lee
Beme Telecommunications
British Aircraft Corp.
British Communications Corp.
British Mftd. Bearings Co.
Brown, S. G
Bryans Aeroquipment
Burgess Products C .
Burgess

Canadian Marconi Co
Cementation (Muffelite)
Chloride Batteries
Ciba (A.R.L.)
Cole, E. K.
Cossor, A. C

Cossor Radar \& Electronics Curran, John

Decca Navigator Co
Decca Naviga
Decca Radar
Delaney Gallay, Switches
Ekco Electronics
Elliott Brothers (London)
English Electric Co.

## Ferranti

Fibreglass
Formica
G.E.C.

General Precision Systems
Girdlestone Pumps
Godfrey, Sir George
Goodmans Industries Graseby Instruments Grundy \& Partners

Hawker Siddeley Aviation Hellerman
Hendrey Relays
Honeywell Controls

Imhof, Alfred
Integral

K.L.G. Sparking Plugs<br>Kelvin \& Hughes<br>Ketay<br>Lucas, Joseph<br>Lucas Gas Turbine Equip.<br>M.L. Aviation Co.<br>Marconi Instruments<br>Marconi's W/T Co.<br>Marston Excelsior<br>Micanite \& Insulators Co.<br>Microcell<br>Ministry of Aviation<br>Murphy Radio<br>Negretti \& Zambra<br>Newmark, Louis<br>Newton Brothers (Derby)<br>Optical Measuring Tools

Plannair
Plessey
Pullin, R. B., \& Co
Pye
Rank Cintel
Redifon
Rotax
Royston Industries

Salford Electrical Instruments Sanders, W. H. (Electronics) Sangamo Weston
Savage, W. Bryan
Semiconductors
Short Brothers \& Harland
Short Brothers \& Harland
Smart \& Brown (Machine Tools)
Smart \& Brown (Machine To
Smiths Aircraft Instruments
Smiths Air
Solartron
Solartron
Solus-Schal
Solus-Schall
Southern Instruments
Sperry Gyroscope Co
Standard Telephones \& Cables
Stone, J. \& Co. (Deptiord)
Taylor, Taylor \& Hobson Tecalemit
Technograph Electronic Prods
Thermionic Products
Thorn Electrical Industries
Tucker Eyelet Co.
Ultra Electronics
Vactric (Control Equipment)
Venner
W.S. Electronics

Ward, Brooke \& Co
Waymouth Gauges \& Instruments
Western Manufacturing
Westinghouse Brake \& Signal Co Westland Aircraft
Whiteley Electrical Radio Co.
Wireless Telephone Co.

## CHANGE OF PRICE

AS from this issue the price of Wireless World is increased to 2 s 6 d . The U.K. and sterling area subscription rate will in future be $£ 2$ p.a., and for the U.S.A. and Canada $\$ 5.50$.

## AIR-TRAFFIC CONTROL AID

BEARINGS given by ground-based direction finders working from an aircraft's v.h.f. radio contacts can, by triangulation, indicate position and identity of an aircraft. Manual methods, though, are too slow for use in a modern air-traffic control organization and resort is made to automatic triangulation of the bearings from several stations, the results from distant points being transmitted by land line to the central a.t.c. point.

Last year S.T.C. demonstrated an automatic triangulation apparatus at the S.B.A.C. exhibition at Farnborough; this relied upon the optical combination of maps and of bearing lines displayed on a bank of c.r.t.s, and the resultant composite picture was distributed by closed-circuit television.

Recently a further development of the principle was demonstrated at the Ministry of Aviation's Experimental Unit at London Airport; here the system was used to identify surveillance-radar paints on the p.p.i.-display tube.
A marker blip, which can be controlled in position by a "joystick", is fed into the auto-triangulation apparatus where it appears on one of the c.r.t.s whose displays are combined; this marker is also fed into the radar-display system. The joystick operator watches a television display of the triangulation and he lines up the marker with the intersection of the bearings, the marker on the p.p.i. zube moves correspondingly and so identifies the aircraft paint.

This system thus provides identification for aircraft


Auto v.h.f. direction-finding triangulation coupled to primary surveillance radar as demonstrated by S.T.C. On left is TV screen displaying triangulation: right-hand tube is primary radar screen on which identifying marker appears.
carrying the minimum of radio equipment required by law-a v.h.f. R/T set-and, although: it takes advantage of co-operation of the aircraft, it does not demand anything other than the ordinary procedural use of R/T.

# FLYING TV CLASSROOM 

EDUCATIONAL television in the U.S.A. took a further step forward (or should we say upward?) recently when a regular airborne schools TV service covering six States in the Mid-West was introduced. Videotape recorded lessons are radiated on two channels ( 72


The retractable 24 -foot aerial on a DC-6 used for the airborne television station is stabilized to keep it vertical to the earth even wien the plone is banking at angles of up to $20^{\circ}$. (Right) The airborne transmitter, which radiates on two channels in the u.h.f. band, and video tape equipment.
and 76) in the 818 to $848 \mathrm{Mc} / \mathrm{s}$ band. The " stations", flying at a height of $23,000 \mathrm{ft}$ in the vicinity of Montpelier, Indiana, are said to give an effective coverage to an area of up to 200 miles radius-approximately sixteen times the area covered by a ground station. The Western Electric's "Stratovision" system is employed in the two planes equipped for the service which is intended to provide instruction for various grades of schools and colleges in Indiana, Lllinois, Michigan, Ohio, Wisconsin and Kentucky. A relatively small number of aircrafi could provide a coast-to-coast service in the U.S.A. In this country three "stations" would probably suffice for a national service.


Cold-cathode Thyratrons which do not contain mercury and thus can be used for high currents without a runin period for mercury vaporization have been developed by Cerberus A.G. of Switzerland (agents in the U.K.-Walmore Electronics Ltd.). Known as "Arcotrons," these valves are gas filled at relatively high pressure. Near the cathode is an auxiliary anode consisting of a perforated disc: between this and the cathode a small arc discharge is struck and maintained with an arc drop of some 25 V . The grid is another perforated plate and viewed from this point the cathode-cum-auxiliary-anode structure appears as an electron-emitting cathode. With the grid negative, a space charge is built up in the manner of an ordinary valve; but, when the grid potential is positive with relation to the real cathode, the anodevoltage field can extend through the grid and electrons are accelerated into the anode region, causing ionization and breakdown. Arcotrons are available for mean currents of up to 6A and working voltages up to 700 (direct) and 500 (alternating).

Power Rheostat.-The illustration shows a printed-circuit step-variable resistor developed by Mills \& Rockley in association with Lucas. The resistance element itself is of $10^{-3}$-in thick cupro-nickel, having a total resistance of 15』. The element is bonded to epoxy-resin cum glassfabric insulator which in turn is bonded to the $-\frac{1}{32}$-in thick aluminium

base, which increases the dissipation of heat and can be fixed to a larger surface. This method of construction is, of course, applicable to fixed
resistors also and the power rating of the component shown (about 1 -in across) is 15 W . The address of Mills and Rockley's printed-circuit division is Swan Lane, Coventry.

## Increased TV-Aerial Bandwidth is

 useful when several transmitters on different channels are available. A technique known as "doubledriving" has recently been employed by Antiference to increase the bandwidth of a Band-III Yagi array designed primarily for the export market. Double driving involves the use of two folded-dipoles spaced some $\lambda / 4$ along the boom, connected in parallel by a length of open line formed by two parallel tubes. An ordinary Yagi design can be used usually on adjacent channels only, whereas the double-driven array is claimed to cover a major part of Band IIIBeam-Width Modulation devices are discussed in an article by H . Lashinsky in the May, 1961, issue of the IR.E. Transactions on Electron Devices (p. 185). Referring to the diagram (based on Fig. 1 of this article) the voltage on the perturbing apertured grid just beyond the cathode gives the beam electrons a transverse velocity. Due to the longitudinal magnetic field this results in the beam taking up a scalloped aspect in which the scallop amplitude is determined by the magnetic field and the perturbing voltage and the scallop wavelength is determined by the magnetic field and the cathode-anode accelerating voltage. An apertured anode is used so that the intercepted beam current depends on the longitudinal position of this anode relative to the scallops. If then the anode voltage is modulated, the scallops move longitudinally relative to the aperture so that an a.c. component is produced in the intercepted beam current. Such a device can be used as a frequency multiplier by modulating the anode voltage so deeply that an integral number of scallops swing back and forth through the anode aperture. Two advantages of this type of multiplicr are that the power is concentrated mainly in a single harmonic and that the harmonic number can be altered simply by altering the anode modulating voltage. Unfortunately, it can be shown that any harmonic frequencies obtained in this way must be less than the frequency of cyclotron motion of the electrons in the magnetic field. If the anode is square-wave modulated, a number of current pulses are

produced depending on the squarewave amplitude. This arrangement thus provides analog-to-digital conversion. Mixing of two frequencies is possible by applying one to the anode and the other to the perturbing grid. One general disadvantage of this type of modulation is that its efficiency is low. This is because most of the anode current must produce heat, it being essentially the loss current which is modulated. Transit time conductance effects can be shown to be minimized because the grid current is small, the electron motion being mainly at right angles to the field between the grid and cathode. The deflection sensitivity decreases at high frequencies because the electrons remain in the grid field for an appreciable fraction of a modulating cycle. This effect can be reduced both by moving the grid close to the anode aperture and by shielding the grid so that the transverse field is applied only over a very short part of the electrons' path.
"Frictionless" Bearing obtained by magnetic "levitation" is discussed in an article by F. T. Backers in Vol. 22 No. 7 of Philips Technical Keview (p. 232). The bearing shaft has a number of magnetic rings on it (made, for example, of Ferroxdure): these rings are radially magnetized alternately inwards and outwards. Inside the bearing housing is a similar set of oppositely magnetized rings: the repulsion between the housing and bearing rings keeping the shaft suspended in radial equilibrium. Unfortunately this system does not in itself produce axial equilibrium, and this was obtained by fitting Ferroxcube magnetic disks to the ends of the shaft and using any unbalance between the self inductance of two coils in the housing opposite these disks to energize electromagnets at the ends of the shaft so as to correct any axial displacement.

## DOUBLE-BASE-DIODE

 OSCILLATORBy P. LLOYD*

SIMPLE CIRCUIT USING CAPACITOR, RESISTOR AND SEMICONDUCTOR

THIS oscillator was demonstrated at a recent exhibitiont and uses a General Electric 2N489 double-base-diode semiconductor device in conjunction with a metal-film resistor and a newly developed tantalum capacitor of the dry oxide-film type $\ddagger$.

A general view of the oscillator is shown in photograph. With a supply voltage of 4.5 V , the output is 350 mV at a frequency of $300 \mathrm{kc} / \mathrm{s}$. As can be seen from the circuit diagram given in Fig. 1(a)

(b)

Fig. I (a) Oscillator circuit, using pictorial representation of the unijunction. (b) Symbol that has been used for double-base diode
use of the double-base diode, or unijunction transistor as it is sometimes called, makes possible the construction of an oscillatory circuit using the minimum of components.

Physically, the double-base diode consists of a bar of n-type semiconductor with two ohmic contacts, bases 1 and 2, made at the ends and at an intermediate position a third contact, the emitter, forming a p-n junction with the bar. The operation of this device when used in the circuit of Fig 1(a) is analogous to that of a thyratron relaxation oscillator and can be described as follows:-

The capacitor $C$ is charged from the supply through resistor $R$; when the emitter potential reaches a sufficiently high value the $p-n$ junction starts to inject minority carriers into the bar, causing the resistance in the base 1 region to become negative. This action, which is cumulative, results in a rapid discharge of the capacitor through base 1. When the discharge is complete the emitter potential has returned to the cut-off condition and the cycle recommences ${ }^{1,2}$.

In the oscillator described above the capacitive clement consists of a very thin film of tantalum oxide as the dielectric, sandwiched between two

[^0]aluminium electrodes. The aluminium and oxide layers are deposited, under vacuum, upon an insulating substrate; the former by evaporation and the latter by a process known as "reactive sputtering" ". This process is an extension of the technique of cathodic sputtering, whereby metal is deposited from its parent cathode under the influence of an ionizing discharge occurring under vacuum. Now if oxygen is leaked into the vacuum chamber there is a chemical "reaction" and the sputtered deposit forms as an oxide of the cathode metal. The effect has been employed in optical applications such as lens-blooming; but is a new development in the electronic components field.

Reactively sputtered tantalum-oxide capacitors of the type used in the double-base-diode relaxation oscillator have a capacitance of 0.01 uF and a $\tan$ $\delta<0.01$ at $10 \mathrm{kc} / \mathrm{s}$. The dimensions of the two aluminium electrodes are $\frac{1}{8} \times \frac{1}{8}$ in and the total thickness of the capacitor element, excluding the substrate, is only 0.00002 in .

Micro-miniaturization of electronic circuitry, especially for transistor applications is being advanced further by the development of com-

(Crozun Copyright)
Double-base-diode relaxation oscillator.
ponents such as these, and it will be appreciated from the sizes given that the circuit elements employed are virtually two-dimensional.

## References

1. General Electric Transistor Manual-G.E. Co., New York, 1959.
2. Double Base Expands Diode Applications by J. J. Suran, Electronics, March 1955, p. 198.
3. Reactive Sputtering and Associated Plant Design by
L. Holland and G. Siddall, Vacuum, 3, 1953, p. 245.

## WORLID OF WIRELLESS

## I.E.E. and Electronics

BECAUSE of "the increasing importance of electronics in electrical engineering, and the part being played by electronics engineers in the work of the Institution" the I.E.E., at a meeting on June 22nd, decided on a major reorganization to "demonstrate unequivocally the significance of electronics in the Institution's affairs." In place of the existing four specialized sections (Electronics \& Communications, Measurement \& Control, Supply, and Utilization) there will be three Divisions representing "electronics," "power," and "general," the latter covering activities of common interest to all electrical engineers, such as basic measurement and technological education.
Each of the divisions will comprise a number of technical groups designed to cover specializations within its field.
It is planned to bring the new scheme into operation in October next year.

## G.E.C., Sobell, McMichael

A SEPARATE exhibition of the G.E.C. group of companies is being held from August 19th to 24th inclusive at the New Horticultural Hall, Westminster, when the full ranges of radio and television receivers will be shown.
In addition there will be live and film shows of colour television demonstrating the 405-line N.T.S.C. receivers developed by G.E.C. and also the SECAM system (on 625 lines) developed in conjunction with the French company, Compagnie Générale de T.S.F. and its associate Compagnie Française de Télévision.
Other demonstrations will enable the public to compare monochrome pictures on 405 - and 625 -line standards, and there will be supporting displays illustrating the wide activities of G.E.C. in engineering, atomic energy, telecommunications, etc.

Brit.I.R.E. Graduates.-The rise in the number of candidates entering for the Graduateship Examination of the Brit.I.R.E. in May was not reflected, however, in the number of passes. Of the 210 candidates who sat section A 94 were successful and of the 170 sitting section B (all of whom bad previously passed section A) only 42 passed. In view of this it is interesting that the Institution is holding a whole-day symposium on the subject of its new graduateship syllabus on September 27 th at University College, London. The morning session ( 10.30 to 1.0 ) will be devoted to the syllabus itself and the afternoon session ( 2.30 to 5.30 ) to the Institution's recommendations for practical training.
B.E.A.M.A. Electronics Board.-The British Electrical and Allied Manufacturers' Association, which recently formed an Industrial Electronics Equipment Section, has now established an Electronics Board "to represent that part of the B.E.A.M.A. membership directly concerned with electronic engineering." The initial membership of the Board is:-L. Bagrit (Elliott Bros.)-chairman, O. W. Humphreys (G.E.C.)-vice-
chairman, E. B. Banks (English Electric), W. S. Steel (A.E.I.), S. Z. de Ferranti (Ferranti), C. Metcalfe (E.M.I.), and W. Gregson (Ferranti)-chairman of the Industrial Electronic Equipment Section. The plan is designed "to provide within the framework of the B.E.A.M.A. an organization to safeguard the interests of British manufacturers concerned with electronic engineering, but it is not intended to assume on behalf of BEAMA members responsibility for other sectors of the electronic engineering industry, e.g., telecommunications and components which are already dealt with by existing Associations."
S.I.M.A. Officers.-The new president of the Scientific Instrument Manufacturers' Association is A. W. Jones (Fleming Radio), with R. E. Burnett (Marconi Instruments) as vice-president and president-elect; G. C. Ottway (W. Ottway \& Co.) vice-president; Major WIm. Logan (Avo) hon. secretary; and G. S. Sturrock (Kelvin and Hughes) hon. treasurer. The newly elected members of the Council are: J. E. C. Bailey (Baird \& Tatlock), A. G. Peacock (Mervyn Instruments), L. B. Lambert (Negretti \& Zambra), J. E. T. Haile (Rank Precision Industries), I. C. M. Worsfold (W. H. Sanders Electronics), H. Wyn Griffith (Shirley Developments), and A. Richardson (Stanhope-Seta).

Scientific Instrument Makers.-The new master of the Company of Scientific Instrument Makers is A. E. Evans, managing director of Evans Electro-Selenium. The senior and junior wardens elected for 1961/62 are respectively Paul Goudime, managing director of Electronic Instruments, and F. W. Dawe, managing director of Dawe Instruments.

Standards and Measurements.-The third in a series of biennial conferences on Standards and Electronic Measurements will be held next August (14-16) at the Boulder, Colorado, laboratories of the National Bureau of Standards, which is one of the sponsors. Further information is obtainable from: Dr. John M. Richardson, Chief, Radio Standards Laboratory, National Bureau of Standards, Boulder, Colorado.

Lugton's, the well-known London wholesalers, are celebrating their Diamond Jubilee this year. As part of their celebration they are holding an exhibition at the Café Royal, London, W.1, from August 22nd to 24 th and 28 th to 31 st . It will be open daily from 9.30 a.m. until 9 p.m.

Rockets.-Paul Adorian, managing director of Associated Rediffusion, has had a paper reprinted on the technique of rocket propulsion which he read in January, 1929, before the Engincering Society of the City and Guilds (Engineering) College, where he was then a student. In the Introduction he says: "While there is little original matter in the paper, it is thought that it may be interesting to read this particular approach to rocket propulsion as presented more than thirty years ago." The proceeds from the sale of the reprint, which is available from the author at 21 Denmark Street, London, W.C.2, price 8s, will be given to the Henry Tizard Memorial Fund.

Soviet production of TV sets during the first half of this year totalled 934,000 , which was a $17 \%$ increase on the same period last year. Sound radio and radiogramophone reproduction totalled 2.1 M (a $3 \%$ increase).

Another V.H.F. Station.-The B.B.C.'s 21st v.h.f. sound broadcasting station which serves the south-east corner of England was brought into operation on August 8 th. The Dover station which is of the translator type operates unattended and re-radiates the Wrotham transmissions on different frequencies but without demodulation. The station operates on $90.0,92.4$ and $94.4 \mathrm{Mc} / \mathrm{s}$ with an e.r.p. of 3.5 kW . It is on the same site as the Dover television station.

Industrial Research Fellowships.-A scheme of research fellowships "which may contribute to furthering the collaboration between Universities and industry" has been introduced by J. Langham Thompson Ltd. The research workers appointed to the fellowships, normally on a two-year tenure, will follow "their own line of research" at the company's laboratories at Watford, Herts.
"Mathematics-Friend or Foe?" is the title of the first annual lecture of the British Conference on Automation and Computation (B.C.A.C.) which is to be given by Dr. D. G. Christopherson on September 27th at 5.30 at the Institution of Electrical Engineers, Savoy Place, London, W.C.2. Tickets are obtainable free from the Hon. Secretary, B.C.A.C., c/o the I.E.E.

Colour Television.-A refresher course of lectures on colour television will be given on the six consecutive Monday evenings from September 18th in the Lecture Theatre at the London School of Hygiene and Tropical Medicine, Keppel Street, W.C.1. The lecturers will be S. N. Watson (B.B.C. Designs Dept.) and G. B. Townsend and P. Carnt of the G.E.C. Hirst Research Centre. The course is organized by the Television Society (166 Shaftesbury Avenue, London, W.C.2) from which enrolment forms are obtainable. Fee for non-members is 2 gn .

Three conferences or symposia have been arranged by the Institute of Physics and the Physical Society for September. The first, on "some aspects of the physics of space research," will be from the 20th to 22 nd at the Royal Military College of Science, Shrivenham, Wilts. The second, at the University College of North Wales, Bangor, on 21 st and 22 nd , is on "radiospectroscopy of solids," and is being organized jointly with the British Radio Spectroscopy Group. During the conference, Dr. D. Shoenberg, F.R.S., will deliver the Guthrie lecture on "The de Haas-van Alphen affect and the electronic structure of metals." The third is on the 28th and 29th at the Town Hall, Leamington Spa, and is entitled "the physics of gas discharge devices." The Institute and Society is also holding a one-day symposium on "some aspects of vacuum science and technology" at Imperial College of Science and Technology, London, on January 5th. Further details are obtainable from 47 Belgrave Square, London, S.W.l.

The Transit Navigation Satellite System will be discussed at a whole-day meeting to be held jointly by the Institute of Navigation and the Electronic Engineering Association on September 26th from 10 a.m. The meeting, which is open and for which there is no fee, will be held at the Royal Geographical Society, 1, Kensington Gore, London, S.W.7.

Stereophonic concerts are to be given in the Cripplegate Theatre, Golden Lane, London, E.C.1, each Monday evening from September 18th to December 18th. New records will be used for each of the concerts which begin at 6.30 and will last about two hours. Admission will cost 2 s .

Tabulated lists of colleges in Manchester and district showing the types of courses they provide are given in the booklet "Engineering Education" published by the Manchester and District Advisory Council For Further Education, Deansgate, Manchester 3.

Radio Hobbies Exhibition, which is sponsored by the Radio Society of Great Britain, will be held at the Royal Horticultural Hall, Vincent Square, London, S.W.1, from November 22nd to 25th.

Receiving Licences.-The June figure for combined TV/sound receiving licences in the United Kingdom of $11,440,884$ shows an increase of nearly three-quarters of a million in the past twelve months. Sound-only licences, including 488,759 for sets fitted in cars, totalled $3,856,884$-a decrease of over half a million, during the same period.


SERVICE AREAS of the I.T.A.'s "Border" stations ot Caldbeck, which begins regular transmission in Channel II on September Ist, and its unattended satellite transmitter near Selkirk, which is planned to be brought into service in Channel 13 at the end of the year. Also shown are the service areas of the Authority's N.E. Scotland stations at Durris (Chonnel 9), to be opened on September 30th, and Mounteagle (Channel 12)

## Personalities

Sir Hamish MacLaren, K.B.E., C.B., D.F.C., until recently Director of Electrical Engineering at the Admiralty, has been appointed a consultant to Associated Electrical Industries Ltd. After graduating at Edinburgh University in 1921 he joined British Thomson Houston Co., Rugby, as a student apprentice. Under a B.T.H. Fellowship he spent one year (1923-24) with the G.E. Company of Schenectady, U.S.A., and joined the Admiralty as assistant electrical engineer in 1926. Sir Hamish is the $1960 / 61$ president of the I.E.E.
C. F. Bareford, Ph.D., M.Sc., A.M.I.E.E., who joined Vickers Ltd. in 1956 as head of electronic research and has been managing director of Vickers Research Ltd. since its formation in January 1959, has been appointed Controller of Research of Vickers Ltd., and will retain his present position. Dr. Barcford was for 10 years at the Admiralty Signal Establishment before joining Mullards as head of their research laboratory at Salfords, Surrey, in 1946. From 1953 until he joined Vickers he was chief superintendent of the Long Range Weapons Establishment at Woomera, South Australia.
J. A. Saxton, deputy director of the D.S.I.R. Radio Research Station, Slough, is going to the United States in September, where he has accepted a year's visiting professorship at the University of Texas Radio Research Establishment. Dr. Saxton, who has been in the scientific civil service since 1938, has twice served in the U.K. Scientific Mission in Washington.


Dr. J. A. Saxton

A. W. Jones
A. W. Jones, recently installed as president of the Scientific Instrument Manufacturers' Association of Great Britain, is managing director of Fleming Radio (Developments) Ltd., which he formed in 1945. He joined Orr Radio (now Invicta Radio) as an inspector, in 1933 at the age of 19 becoming ultimately technical manager. During the war he was working on radar research and development with Pye who acquired Invicta in 1938 . Mr. Jones was vice-president of S.I.M.A. for $1960-61$ and was also chairman of the Electronics, Telecommunications and Electrical Instruments Section to which 70 S.I.M.A. members belong. He is a founder member of the Livery Company of Scientific Instruments Makers.

Grp. Capt. A. Foden, C.B.E., Command Signals Officer, R.A.F., Germany, since last September, has become Director of Telecommunications, Air Ministry. He has been a signals specialist throughout his Service career, which began in 1939. Hc is 47.
T. H. A. Llewellyn, A.F.C., M.A., has been appointed chief executive, and L. S. White, technical adviser, of British Telemeter Home Viewing Lid. These are the first executive appointments made by the company which was formed last year jointly by a number of companies, including Granada TV Network and British Lion Films, to operate subscription television. Mr. Llewellyn, who is 51 and a graduate of Trinity College, Oxford, has been adviser to a number of companies in the fields of engineering and applied physics and was at one time chief executive of Taylor, Taylor \& Hobson. Mr . White has for the past six years been with Rediffusion, for most of the time as chief engineer of one of its operating companies. For seven years before joining Rediffusion he was with Standard Telephones and Cables Pty., Australia, prior to which he was for six years in the Anti-submarine Warfare Division of the Royal Navy. He is 48.

Trevor C. Standeven, who left Radio \& Allied Industries in 1958 to join Ultra and was appointed managing director of Ultra Radio \& Television Ltd. when it was acquired earlier this year by Thorn Electrical Industries, has resigned and joined G.E.C. (Radio \& Television) Ltd. as managing director. In his new position he will again be associated with Radio \& Allied Industries which recently became a subsidiary of the General Electric Company.

Hugh S. Pocock, M.I.E.E., managing editor of Wireless World and managing director of our publishers Iliffe Electrical Publications Ltd., has been appointed a director of Associated Iliffe Press Ltd. Mr. Pocock, who has been with $W . W$. since 1913 , is also managing editor of our sister journals Electronic Technology and Electrical Review.
S. N. Ray, M.Sc., B.Sc.(Eng.), M.I.E.E., F.Inst.P., has been appointed principal lecturer (applied electronics) in the Department of Electrical Engineering and Physics, Borough Polytechnic, London, which he joined in 1939 and where he has been senior lecturer in radio engineering. Born in Calcutta in 1902, Mr. Ray came to this country after receiving his M.Sc. degree from Calcutta University in 1925 and continued his studies for his B.Sc. (London) and the Diploma of Faraday House. For 11 years from 1928 he was in the radio industry, for the major part of the time with Dubilier and subsequently as chicf engineer of the Magnavox Division of Benjamin Electric.
L. H. Griffiths, M.A., B.Sc., A.M.I.E.E., who joined the B.B.C. in 1951, has been appointed head of the Film Unit, Television Studio Section, Planning and Installation Department. Mr. Griffiths has been largely responsible for the design and planning of the central telerecording area at the London Television Centre. He is co-inventor with F. W. Nicholls of an improved photographic telerecording system, which has been incorporated in the design of $35-\mathrm{mm}$ rapid pull-down telerecording equipment used by the B.B.C.
A. H. Campbell, M.A., M.I.E.E., who has been a director of Hilger \& Watts since 1951 and general manager since 1954, has been appointed joint managing director with G. A. Whipple, M.A., M.I.E.E., F.Inst.P. Mr . Campbell was for some time before the last war with the Cambridge Instrument Company. During the war he was with the Royal Corps of Signals, finally as Licutenant-Colonel commanding 8 Corps Signals.
J. M. Briggs, M.A., A.M.I.E.E., the new Director of Electronics, Research and Development (civil aviation) at the Ministry of Aviation, has been superintendent in the Ground Radar Deparment of R.R.E. since 1955. He graduated at St. John's College, Cambridge in 1935 and spent 18 months in the G.E.C. carrier communications development laboratory before joining the Government service at the Royal Aircraft Establishment. He transferred to T.R.E. in 1940 and was closely associated with the development of A.S.V. For a period after the war he was chairman of the Inter-Services Radio Measurement Committee.
J. R. Mills, recently appointed head of the Radio Department at the Royal Aircraft Establishment, Farnborough, was from 1954 to 1960 superintendent in the Airborne Radar Department at the R.R.E., Malvern. For a few months prior to his present appointment he was the assistant director at the Ministry of Aviation concerned with electronic problems of civil aviation. Mr. Mills has been in the scientific civil service since 1940. He was a member of the team set up in 1946 at T.R.E. to develop electronic systems for civil aviation, his particular interest being D.M.E.
A. Robert Enshaw has been appointed executive director in charge of the Government Contracts Department of Plessey. He joined the company in 1946 and was, until his present appointment, manager of the Telephone Apparatus Department. Plessey also recently announced the following appointments:-A. A. Farrell becomes director and general manager of Plessey Ireland Ltd., and also a director of Plessey Sales Ltd., Dublin; A. W. Henderson, Ph.D., B.Sc., previously with CIBA (A.R.L.) and Ferranti, is now Plessey's chief chemist-metallurgist; and L. Walker is appointed chief inspector of the Plessey group of companies.
R. J. Keir, O.B.E., B.Sc., A.M.I.E.E., has been appointed engineer-in-charge of the B.B.C.'s External Services short-wave transmitting station at Skelton, Cumberland. He joined the Corporation in 1937 and from 1956 until early this year was resident engineer of the B.B.C.'s Far Eastern Broadcasting Service at Tebrau, Singapore. Since his return to this country he has been asst. e.-in-c. at Skelton where he succeeds H. F; Bowden, Assoc.I.E.E., who is retiring after 36 years' service. Mr. Bowden has served at a number of stations including the television station at Alexandra Palace and has been at Skelton since 1945.

Peter Frost, Dip.Tech., Grad.I.E.E., personal assistant to the manager of the capacitor division at the G.E.C. Telephone Works, Coventry, has been awarded a $£ 90$ travel scholarship from the Department of Electrical Engineering at the Birmingham College of Advanced Technology. He joined G.E.C. in 1955 as a student apprentice and received his Dip. Tech. after a sandwich training course. He hopes to use the scholarship to study the manufacture of electronic components, management organization and technical education in Europe.
G. A. Graham, A.M.Brit.I.R.E., has been appointed to succeed the late W. J. Chalk as engineer (frequency allocations) in the B.B.C.'s Engineering Information Department. He has been with the Corporation since 1947 and had been assistant to Mr. Chalk since 1958. He was a member of the U.K. delegation to the recent V.H.F./U.H.F. Broadcasting Conference in Stockholm.

Aubrey Harris, A.M.I.E.E., A.M.Brit.I.R.E., who has been associated with the Ampex Corporation of Redwood City, California, since November, 1958, has joined Ampex Electronics, Ltd., in Reading, Berkshire, as senior engineer. He started his career at the Post Office Research Station, Dollis Hill, later spending over five years with Marconi's on research and advanced development of television equipment. In 1957 he went to Bermuda as chief engineer of television station ZBM-TV.

## OUR AUTHORS

A. T. Ferguson, who describes in this issue an instructional radio receiver, is lecturer at the South Shields Marine and Technical College, where he started his teaching career in 1947. From 1937 he was for eight years a marine wireless operator with Marconi's and from 1945 he spent two years in the Post Office Radio Service.
J. M. Winwood, M.A., author of the article on page 491, is in charge of the group concerned with travellingwave devices at the Mullard Research Laboratories, which he joined in 1955. After graduating at Cambridge in 1952 he worked for two years on the production of magnetrons and travelling-wave tubes at the English Electric Valve Company in Chelmsford.

Peter Lloyd, Grad.I.E.E., who describes a double-base-diode oscillator in this issue, has been at what is now the Royal Radar Establishment, Malvern, since 1945. He has been in the technical services department of the Establishment since 1956 and for the past three years has been concerned with capacitor development. Mr. Lloyd, who was a student apprentice with E.M.I. at Hayes for four years before going to Malvern, is a member of the Inter-Services Radio Component Research \& Development Committee for Fixed Capacitors.

## OBITUARY

H. V. Slade, O.B.E., J.P., chairman of the Garrard Engineering \& Manufacturing Co., died on July 19th ai the age of 72 . He founded the Garrard Company, of which his sons Hector and Kenneth are respectively managing director and sales director, 46 years ago and although the company's productions have been very varied, his main interest had always been the gramophone.
R. W. Hall, chief sales executive of the Aerial Division of Antiference which he joined in 1952, died on July 21 st aged 47.

## News from Industry

British Space Development Company.-Two more companies, making eleven in all, have joined this consortium of aircraft and electronics companies. They are Elliott-Automation L.td. and C. A. Parsons \& Co., who are represented on the company's technical committee by W. R. Thomas, B.Sc., M.I.E.E., and H. M. Finniston, Ph.D., B.Sc., respectively.

Elliott-Automation, Ltd.-The 1960 gross profit of the group, of which Elliott Brothers (London), Ltd. is now the largest subsidiary, was $£ 1,776,510$. Of this sum the Rheostatic Company, acquired during the year, contributed over $£ 0.5 \mathrm{M}$. Excluding this figure the E-A profit increased by nearly $24 \%$. Taxation took $£ 816,863$.

Ferranti's accounts for the year ended March 31st show a group net profit of $£ 1,661,023$ compared with $£ 2,123,390$ the year before. Taxation charged in arriving at the $1960 / 61$ figure was $£ 1,740,000$. The company recently opened a Northern Computing Service in Manchester based on a Pegasus general purpose digital computer. Clients wishing to use the service may prepare their own programmes or leave the programming to the computing staff.

Associated Electrical Industries are terminating semiconductor development, production and sales by their Radio and Eleetronic Components Division. Thus Ediswan-Mazda semiconductors will cease to be available, but A.E.I. will honour existing commitments and orders and will be able to supply devices for a short time from stock. Semiconductor devices produced by AsE.I.'s Electronic Apparatus Division at Carholme Road, Lincoln, are not affected by this announcement. Exact electrical equivalents to some Ediswan-Mazda devices are available from R.C.A. Great Britain, Ltd., and also Ferranti, Ltd., who are to produce some types of R.C.A. transistors under licence from the Radio Corporation of America.

Thorn.-Group trading profits of Thorn Electrical Industries Ltd. for the year ended March 31st amounted to $£ 4,113,907$, compared with $£ 3,916,990$ the previous year. After deducting all charges the net profit is £ $1,548,769$ ( $£ 1,525,988$ ).

Thorn-A.E.I. Radio Valves \& Tubes, Ltd., is the name of the company formed as a result of the merger of the Thorn and A.E.I. interests in the manufacture and sale of c.r. tubes and valves "for the entertainment industry" announced on p. 406 last month. Thorn Electrical Industries Ltd. is responsible for management.
A.T.V.-The profit of the Associated Television Group for the year ended on April 30th, before making provision for taxation, was $£ 6,411,899$ compared with $£ 5,388,330$ for the previous year.

Radio and Television Trust, Ltd., of which Airmec and British Communications Corp. are operating subsidiaries, announce a consolidated profit for the year to 31st March of $£ 265,782$ compared with $£ 118,060$ for the previous nine months. The charge for taxation is $£ 127,266$, leaving a net profit of $£ 138,516$. D. D. Prenn is chairman and managing director of the Trust and chairman of the two operating companies, and Dr. I. C. Simmonds is managing director of Airmec and of B.C.C., and is deputy managing director of R.T.T.

Cossor and Raytheon.-A cash offer has been made by the Raytheon Company, of Lexington, Mass., for the issued share capital of A. C. Cossor, Ltd. The prices offered for the shares puts the overall purchase price at over $£ 2 \mathrm{M}$.

Pye-Ling Ltd. has been formed jointly by Pye Ltd., and Ling Temco Electronics Inc., of Dallas, U.S.A. It will embrace what was the Vibration Division of $W$. Bryan Savage Ltd., a member of the Pye group, and its products will include both the Savage and Ling ranges of vibration test equipment.

Amalgamated Electric Services, Ltd. has been formed as a subsidiary of Philips Electrical Industries to take over the service activities at the Central Service Departments of Cossor Radio \& TV, Philips Electrical and Stella Radio \& TV at Waddon, Surrey. In addition, the new company will be service agents for Peto Scott Electrical Instruments and Ajax Domestic Appliance Co. The address is Waddon Factory Estate, Croydon, Surrey (Tel.: Croydon 7722).

Hilger \& Watts, Ltd. have acquired the whole of the issued share capital of Microwave Instruments, Ltd., well known for their wave-guide components and microwave test equipment. J. Bilbrough, A.M.Brit.I.R.E., will continue as managing director of Microwave Instruments whose factory is at North Shields, Northumberland.

Bradmatic, Ltd., makers of tape recording equipment, of Witton Lane, Aston, Birmingham, wish to make it clear that the acquisition by Birmingham Sound Reproducers of their former associate company Bradmatic Productions, Ltd. (now Tape Heads, Ltd.) does not affect them. They still operate independently.
U.K.-U.S.A. Telemetry Tie-Up.-S.E. Laboratories (Engineering) Ltd., of Feltham, Middlesex, are to represent Electro-Mechanical Research Inc., of Sarasota, Florida, in the U.K. The American company's main activities are in the field of frequency and time-division multiplexing equipment, for use in telemetry and data acquisition and processing applications for both airborne and ground-based use.
Aga Dictating Machine Co., of 146, New Cavendish Street, London, W.1, have been appointed distributors in the U.K. and certain Commonwealth countries, of Aga domestic sound receivers and radio-grams manufactured by Svenska AB Gasaccumulator, of StockholmLidingö, Sweden. They are also sole distributors for Agavox dictating machines.

Walmore Electronics Ltd., who are agents for several American companies including Eitel-McCullough, National Electronics and Vacap, have been appointed U.K. distributors for the products of Motorola Semiconductor Products Inc. Walmore Electronics are now at 11-15 Betterton Street, Drury Lane, London, W.C. 2 (Tel.: Temple Bar 0201).

Aveley Electric Ltd. have been appointed sole U.K. agents for the Hudson Tool \& Die Co. Inc., of Newark, New Jersey, makers of drawn and pressed metal enclosures for electronic components.

Ortofon.-Metro-Sound Manufacturing Co., of 19A Buckingham Road, London, N.1, have been appointed sole U.K. agents for the Danish company Ortofon S.A. They are setting up a service department for the fitting of diamond and sapphire styli.

## NEW ADDRESSES

Mallory Batteries Ltd. have transferred their works from Dagenham, Essex, to Gatwick Road, Crawley, Sussex.
Lexor Electronics Ltd. have moved their head office and production unit from 25 to 31 Allesley Old Road, Coventry (Tel.: Coventry 72614). The laboratories are remaining at the old address.

Ferrograph.-The London offices, showrooms and service department of The Ferrograph Company, British Ferrograph Recorder Company, Rendar Instruments and Wright \& Weaire have been moved from Horseferry Road, S.W.1, to 84 Blackfriars Road, London, S.E. 1 (Tel.: Waterloo 1981).
J. \& S. Sieger Ltd., previously known as I.E.C.-Sieger Ltd., manufacturers of amplifiers, electronic gas detectors and other electronic equipment, have moved from Bournemouth to Stanley Green Road, Poole, Dorset (Tel.: Poole 1130).
Mullard's Government and Industrial Valve Division is now at 80 New Oxford Street, London, W.C. 1 (Tel.: Langham 5522).
Jason Electronic Designs Ltd. have moved from the West End to Kimberley Gardens, Harringay, London, N. 4 (Tel.: Stamford Hill 5477).

Magnavox.-The head office of Magnavox Electronics Ltd. has been transferred from 129 Mount Street, London, W.1, to Magnavox House, Alfred's Way, Barking, Essex (Tel.: Rippleway 5533).

Cossor Radio \& TV Ltd. have moved from 71 Endell Street, London, W.C.2, to 233 Tottenham Court Road, W.1. The telephone number is unchanged-Gerrard 2931. The showroom in Kingsway has been closed.

Lasky's Radio, the well-known retailers, have moved from 42 to 33 Tottenham Court Road, London, W.1, and have also added a demonstration studio to their premises at 207 Edgware Road, W.2.

# Impedance-Magnitude Measurement 

PRECAUTIONS WHEN USING THE SUBSTITUTION METHOD

By R. C. WHITEHEAD, A.M.I.E.E.

THE measurement of the magnitude of an impedance is a very common laboratory requirement, and although the simple method which follows is apparently very obvious, it remains a fact that many techniques which are more complex and less satisfactory are commonly employed.

Fig. 1 shows the basic circuit. A signal generator drives a current through two impedances $Z_{u}$ and $\mathrm{Z}_{8}$ in series. $\mathrm{Z}_{n}$ is the impedance the magnitude of which is to be measured and $Z_{s}$ is a calibrated adjustable standard. It is only necessary to adjust $\mathrm{Z}_{s}$ until the high-impedance voltmeter V (usually a valve-voltmeter) gives the same reading in both positions of the switch, then to read, on the calibrated scale of $Z_{s}$, the magnitude of the impedance of $Z^{2}$.

This is simple enough if all or most of the components are effectively earth-free. Fig. 1 shows alternative earthing points A and B to be used according to whether the signal generator or the voltmeter is earthed. Either of these conditions will cope with $Z_{u}$ being earthed.

In the event of both the generator and the voltmeter being earthed then we can only cope with a


Fig. 1. The basic measuring circuit. The earthing point may be either $A$ or $B$, depending on whether the signal generator or valve voltmeter is earthed.
$Z_{u}$ which is not earthed and Fig. 2 shows the basic idea of the new arrangement. If the voltmeter gives similar deflections when the circuit is arranged as at (a) and at (b) then once again the two impedances will have similar magnitudes.

Fig. 3 shows the practical circuit with $Z_{u}$ and $Z_{s}$ connected to a double-pole double-throw switch which produces in its two positions the two circuits of Fig. 2. Again the testing procedure consists of adjusting $Z_{s}$ until there is no change in the meterreading when the switch is operated. Then the magnitude of the impedance of $Z_{u}$ may be read on the calibrated dials of $Z_{s}$.

Now we must consider the possible loading
effects of the voltmeter impedance. If this is very high in comparison with the magnitude of the impedance of $Z_{u}$ (say 100 times as great) then its loading effect may usually be ignored, irrespective of the relative phase-angles of $Z_{u}$ and $Z_{s}$.
But is this very high ratio of impedances always necessary? A moment's consideration will show that if finally the magnitudes and phase-angles of $\mathrm{Z}_{u}$ and $\mathrm{Z}_{s}$ are identical, then the voltmeter loading should not materially affect the final result.
If the voltmeter impedance is purely resistive then it will have similar loading effects in turn upon $Z_{u}$ and $Z_{s}$ providing that these have the same magnitudes of phase angles, irrespective of their signs. E.g., if $\mathrm{Z}_{u}$ is an inductor and $\mathrm{Z}_{s}$ is a capacitor they will be loaded similarly by a resistive voltmeter. This is a condition which might apply at frequencies below $100 \mathrm{kc} / \mathrm{s}$ using a rectifier and moving-coil meter.
If, as is usually the case at high frequencies, the input impedance of the voltmeter is predominantly capacitive, then impedances $Z_{u}$ and $Z_{s}$ will be loaded differently if their phase-angles are different either in magnitude or sign. Thus a capacitor is best


Fig. 2. The circuit used when both signal generator and valve voltmeter are earthed.


Fig. 3. The practical arrangement of Fig. 2.
balanced against a capacitor, an inductor against an inductor and a resistor against a resistor. If, however, the input impedance can be kept really high, then the magnitude of the error can be kept small.
Finally a little care in the operating procedure will expedite the measurement.

Consider first the case where $Z_{u}$ and $Z_{s}$ are both resistive or both reactive. The switch should first be set to produce the circuit of Fig. 2b, i.e. $Z_{s}$ should be connected to the live side of the generator.

The magnitude of $Z_{s}$ should now be reduced to zero and the voltmeter reading noted. The magnitude of $Z_{s}$ should then be raised until the voltmeter reading is halved. Finally the switch should be operated simultaneously with fine adjustment of $\mathrm{Z}_{s}$ to produce identical readings in the two positions.

Where one of the impedances is resistive and one reactive, then the value of $Z_{s}$ should be adjusted until the voltmeter reads about $1 / \sqrt{2}=0.7$, not half, of its original setting.

# LETUNERS TO THE EITTOR 

The Editor does not necessarily endorse the opinions expressed by his correspondents

## Transistor Parameters

SQN. LDR. de Visme (in your June issue) is worried over the complications arising from his three sets of transistor parameters. These three (Hybrid, T, and Mullard) date back to the period when transistors were in the main low-frequency devices, and recent work, naturally directed towards higher frequencies, has produced a further crop of parameters.

Moreover, though his equations may look numerous and involved enough, they are simplicity itself when compared to the full expressions, including the transistor capacities (up to six in all) which must be used in all serious work other than at audio frequencies.

Let him produce the complete expressions relating his three sets of parameters (including capacities) with each other, and with the two circuits currently most in usethe Y parameter circuit and the Hybrid - $\pi$ equivalent circuit. This must, of course, be performed in triplicate (for emitter, base and collector grounded). For good measure, he could include also the $\pi$ equivalent and the $Z$ parameters, and he should take into account the effects of lead inductance which are important at v.h.f.
In addition, he should include a list of equivalent symbols (e.g. $r_{11}^{\prime}$ is also written $r_{1}, R_{11}, r_{i}, r_{i n}, r_{i e p}$ etc., with or without primes), and should write many of his equations in two forms, one in terms of $\alpha$, and the other of $Y_{m}$
${ }^{m}$ Then he will know what real worry is!
Southend-on-Sea.
M. V. CALLENDAR

## The author replies:

Had the whole of the June issue been at my disposal, instead of only two or three pages of it, I might have been able to satisfy Mr. Callendar's demands!

I am afraid I contented myself by saying that in general the $h$-parameters must be considered as complex functions of frequency, one of those rather vague statements which are true but not ever so useful. All the $r$ 's and $a$ 's expressed in terms of these parameters therefore likewise become complex functions of frequency.

Mr. Callendar has shown, far better than I could have done, the extreme difficulty of formulating circuits consisting of well-behaved elements which shall be equivalent, over a useful range of frequency, to a fragment of impure semiconductor. I wish him well in his efforts.
G. de VISME

## Testing Tunnel Diodes

THE circuit of Fig. 1 is useful for quick checks of tunnel diodes. It can be used to make reasonably accurate measurements of the quantities indicated in Fig. 2;
i.e., the peak and valley currents $\mathrm{I}_{p}, \mathrm{I}_{v}$, and the corresponding voltages $\mathrm{V}_{p}, \mathrm{~V}_{v}$.

Unless $R_{1}$ and $R_{2}$ are very small (a few ohms), and unless care is taken to keep the circuit inductance low, the circuit will be unstable when the operating point lies in the negative-resistance region BC. For routine checks, it is not worth while trying to preserve stability, because the required quantities can be measured without doing so.

The measuring technique is as follows. Start with the slider of $\mathrm{R}_{1}$ at the negative end and turn the control slowly so as to increase the diode current. The operating point now moves from A towards B. Almost as soon as it has passed B the circuit becomes unstable, and the operating point jumps to somewhere on the negative


Fig. 1.


Fig. 2.
Wireless World, September 1961
resistance segment $B C$. The jump is easily seen on the meter, and by going back towards A and approaching the critical point slowly it is possible to read $I_{p}$ or $V_{p}$. To read the valley current and voltage $I_{v}$ and $V_{v}$, adjust $R_{1}$ so that the working point lies in the stable region CD , as denoted by a smooth rise in the meter reading to something greater than the "peak" value. Then reduce current again. Just after point $C$ is passed the circuit again becomes unstable, and the operating point again changes abruptly. Thus $\mathrm{V}_{v}$ and $\mathrm{I}_{v}$ can be measured by the same technique as was used for measuring $V_{p}$ and $I_{p}$.

The writer has used this method for testing only one type of tunnel diode (the STC JK19A) but, given a suitable choice of resistance values, it should be of general use.

Croydon.
G. W. SHORT.

## Thoughts on Inductance

READERS of the interesting article by Thomas Roddam in your April issue, "Some Thoughts on Inductance," may also be interested in the graphical construction for current in a series inductance/resistance circuit.


The left-hand curve shown (FGCAJ) represents the variation of time constant, $\mathrm{L} / \mathrm{R}=\tau$ seconds, with current (vertical axis) for an inductance based on a grain-oriented silicon steel ring core. This is a theoretical curve derived from the static hysteresis loop, by plotting $\mathrm{dB} / \mathrm{dH}$ (proportional to $L / R$ if resistance is constant) against current and is similar to Fig. 2 (Mr. Roddam). F represents the lower residual point (approx. -0.85 weber/sq. m.) and as the current is increased through $G, C$, to $A$, the near vertical section of the hysteresis loop is traversed until the peak flux density ( +1.0 weber/sq. m.) is reached at J.

If a steady voltage, $\mathrm{V}_{0}$, is applied to the circuit with the core initially at $F$, the final current, is $V_{0} / R$, represented by the horizontal from J (a current chosen, in this case, just sufficient to drive the core to the peak at J). Let

$$
\mathrm{V}_{0} / \mathrm{R}=\mathrm{I}_{0} \text { then }
$$

$$
\mathrm{d} i / \mathrm{d} t=\left(\mathrm{I}_{0}-i\right) / \tau
$$

This equation defines the construction. Commencing with zero current, a line is drawn from the value of $\tau$ at $\mathrm{F}\left(\tau_{0}\right)$ to $\mathrm{I}_{0}$ at J. If now another line parallel to $\tau_{0} \mathrm{~J}$ is drawn from $i=0, t=0$, this represents the initial portion of the current/time graph. Consider point $i_{1}, t_{1}$, when $L / R$ has changed at $G$ to $\tau_{1}$. The line $\tau_{1} \mathrm{~J}$ is drawn and then another parallel to it from $i_{1} t_{1}$. At $t_{2}$ the current has increased on this line to $i_{2}$, and the equivalent value of $\mathrm{L} / \mathrm{R}$ is $\tau_{2}$ and so on. Thus the slope of the line joining $\mathrm{I}_{0}$ (at J) to any point on the curve for $\tau$ represents the rate of increase of current from the corresponding value on the graph of $i$. If sufficient points are taken a smooth curve will result, as shown.

The curve obtained for current/time should be compared with Fig. 4, 5 and 6 in the article by Mr. Roddam.

This graphical construction was originated by W. E. Sumpner in 1888 (Phil. Mag., Serial 5, 25, p. 453).

A further point, often not evident from some textbooks, is that the dynamic hysteresis loop is normally wider than
the static loop and increases in width with frequency. It may be important to obtain a magnetization characteristic obtained under similar conditions to those artually being considered.

## Devizes.

C. F. AMOR

## Museum Pieces

I AM much in agreement with practically everything that Mr. Munning has said about the modern domestic receiver. The last table model with an r.f. stage that I saw, which also had a 10 -inch speaker (Pye P33TQ), apparently didn't sell, and was rapidly withdrawn; and unfortunately I failed to buy one. In this part of the world, unlike London which I recently left, my bedside t.r.f. performs quite as well as my superhet.

I disagree with him, though, about the provision of short-wave bands. I can sympathize with the anxiety of the transistor manufacturers to show thrat their devices will function up to $30 \mathrm{Mc} / \mathrm{s}$, but they should have got over this in a couple of years. To me the completely unacceptable feature of domestic short-wave broadcast reception is not the presence of second-channel interference, drift, or distortion, nor the absence of logging scales (preserve us from "verniers"), but the absolute drivel that all the propaganda and "goodwill" stations churn out.

Strathaven, Lanarkshire.
J. B. ROSCOE

## CONVENIENT VALVE-BASE REFERENCE

THE photograph shows RCA's Triple Pindex in use. It consists of three separate identical references to valvebase connections bound up on the same spiral backing so that three different bases can be kept before one whilst, say, planning, wiring or repairing a piece of apparatus. The fingers and thumb in the picture indicate the frequency-changer (6BE6), i.f.. amplifier (6BA6) and detector (6AT6) of a hypothetical receiver, but the possibilities within the bounds of the valves listed are very wide. For instance, line oscillator, output stage and efficiency diode or r.f., frequency changer and i.f. stages of a television receiver might be displayed together. Triple Pindex's utility is not confined to American-type valves, because at the back is a list of "foreign" valves which includes many popular British types. Even though use of this increases the time taken to look up a series of valves, use of the Pindex still saves time and trouble; in any case, it is soon remembered that, say, an EF91 is the same as a 6AM6, whereas the base connections themselyes are not so easily memorized.

The Triple Pindex is available from Radio Corporation of America, Commercial Engineering, Electron Tube Division, Harrison, N.J., U.S.A. (price \$175), or, in the United Kingdom, RCA Great Britain, Ltd., Lincoln Way, Windmill Road, Sunbury-on-Thames, Middlesex.


## National Radio Show Guide

COLOUR television on 405 lines and monochrome 625line television are being featured at the 28th National Radio and Television Show which opens at Earls Court, London, on August 23rd with a preview for overseas visitors and invited guests the day before. The colour demonstration is being given by the B.B.C.

Of the 24 television set manufacturers exhibiting 21 of them are demonstrating 625 -line receivers. The signal is being distributed to the stands on channel 11 , and for those exhibitors with u.h.f. receivers convertors are provided raising the frequency to $495 \mathrm{Mc} / \mathrm{s}$ (channel 17).

Signals for 405 -line monochrome receivers are distributed on channel 4.

For the demonstration of broadcast receivers there is a Band II f.m. sound service distributed to stands and also a long-wave induction system.
A feature of the Audio Avenue on the first floor is the E.M.I. display "Milcstones in Recording," stand 409, which traces the history of sound recording from 1888. The usual training and servicing feature in which a number of manufacturers are participating is on stand 316 on the first floor.

## ALPHABETICAL LIST OF EXHIBITORS

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Advance Components
Aerialite
Air Ministry
Alba
Alberice
Antiference
Astley Vulcan Finance
Audix
B.B.C.

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Hacker Radio
Heathkit
His Master's Voice
Hobday
Invicta

## J-Beam

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K.B.

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Kerry's
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Linguaphone
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* Composite stand; see "Trade Technical Section" in Show Guide.



## NATIONAL RADIO SHOW

## Guide to the Stands

## A.E.I. SOUND (412)

The main emphasis on this stand will be on sound reproduction equipment for industrial and club use. This includes a pre-amplifier, 30 -watt amplifier and two 18 -watt 12 -in loudspeakers in three portable cabinets, a 5 -ft line-source loudspeaker and a table model record player and amplifier.

Also shown are a stereo control unit and $2 \times 10$ watt amplifier and the DC12 dual-concentric loudspeaker with its horn-loaded h.f. diaphragm.
A.E.I. Sound Equipment Ltd., Crown House, Aldwych, London, W.C.2.

## ADMIRALTY (304)

The communications network used by a Royal Marine Commando Force establishing a beach-head is the main feature on this stand, where there will also be found examples of modern Naval communications and navigation equipment.

Admiralty, Whitehall, London, S.W.1.

## AERIALITE (6)

Coaxial cables, using a longitudinal foil screen, especially designed for relay working are a feature of the display of communal-aerial equipment on this stand. A new coaxial cable particularly suitable for car-radio-aerial use has a capacitance of only $9.5 \mathrm{pF} / \mathrm{ft}$.

Another feature of the display is, of course, a wide range of aerials for indoor and outdoor mounting for reception of television, f.m. and medium- and long-wave broadcasting.

Aerials and fittings for overseas markets are shown.
Aerialite Ltd., Aerial and Electronics Division, Hargreaves Works, Congleton, Cheshire.

## AIR MINISTRY (305)

The central feature of the Royal Air Force stand, which occupies over 7,000 square feet, is a display comprising two air traffic control rooms typical of those employed at an R.A.F. airfield. A radar simulator with remote control facilities is employed to show the uses of search and precision approach radars. Other exhibits include a simulated representation of airborne interception radar.
Air Ministry, Whitehall, London, S.W.1.

## ALBA (9)

Incorporated in the new range of 19 -in and 23 -in television receivers is the " Concord" remote control unit. The device gives the viewer full control over programme selection, volume, contrast and mains on/off and when not in use, is held in place magnetically on the side of the set. All the television receivers on display employ plug-in modules for ease of servicing. Also exhibited is a range of transistor radio receivers, record players and radio-grams, some of which offer reproduction of stereophonic records.
Alba (Radio Er Television) Ltd., 52-70, Tabernacle Street, London, E.C.2.

A.E.I. Sound portable 30 -watt amplifier/pre-amplifier and two 18 -watt 12 -in loudspeakers.

## ALBERICE (204)

Slot meters for " pay-as-you-view" television are the feature on this stand. Both fixed-tariff ( $6 \mathrm{~d} / \mathrm{hour}$ ) and variable-tariff types are shown and are available both to the trade and the public (for saving towards a replacement receiver, for instance).
Alberice Meter Co., 87-89 Sterte Avenue, Poole, Dorset.

## ANTIFERENCE (59, X21)

The whole of Stand 59 is this year devoted to a display of television, f.m. and medium- and long-wave aerials and aerial equipment for both the home and export markets (trade visitors are welcomed at the adjoining Demonstration Room X21). The aerial display includes some new models, the established ranges of aerials and a wide assortment of accessories: of particular interest are car-radio aerials.

Antiference Ltd., Television Go Radio Aerial Division, Bicester Road. Aylesbury, Bucks.

## AUDIX (402)

This company is showing a wide range of public address and club sound reproducing equipment. This includes combined receivers and amplifiers, a five-channel mixer, 15watt transistorized amplifiers, and valve amplifiers (with ratings ranging up to 60 watts) which incorporate four-input-channel mixer/pre-amplifiers and also level indicators. Also displayed are column, re-entrant horn and cabinet loud speakers, and movingcoil and ribbon microphones.

Audix B.B. Ltd., Bentfield End, Stansted, Essex.

## B.B.C. (301, 302, 303)

Closed-circuit colour television is featured by the B.B.C. on stands 301 and 302 where transmissions from a glass-sided studio are displayed on six 21 -in monitors. Each colour monitor has a 21 -in monochrome monitor beside it to demonstrate compatibility. The system employed is the 405-line Anglicized version of the American N.T.S.C., the principles of which are shown graphically on the stand. The Corporation is featuring the growth of its sound and television services with maps of the coverages and another map shows the $2,000-$ mile route taken for the first direct TV transmission from the U.S.S.R. via Eurovision.
British Broadcasting Corporation, Broadcasting House, London, W.1.


Alba T877 19-in television receiver, with its remote control unit in its stowage on the side.


Bush TP. 50 tape-recorder. The singlespeed deck incorporates a digital counter.

## BELLING-LEE (51)

Well-known for their already wide range of decorative in-the-room television and f.m. aerials for strong- and not-so-strong signal areas, this company introduce a new model called the " Monitor." This has provision for u.h.f. reception and pre-set pushbutton tuning to realize maximum signal. Other new types include the "Envoy"-claimed to be a descendant of the popular "Doorod" aerial-and a range of folding aerials for loft mounting. Many types of outdoor aerials are exhibited.

Communal-aerial and relay equipment of advanced design is on show, as is a wide range of accessories.

Belling and Lee Ltd., Great Cambridge Road, Enfield, Middlesex.

## GRIMAR (64, X17)

Valves and cathode-ray tubes are displayed on this stand, the cathoderay tubes including twin-panel types with bonded safety shields made from Diakon, anti-reflection coated glass and plain glass. A working demonstration emphasizes the advantages of these types of c.r.t.

New valves on show include the EMM802 double " magic eye" designed for f.m.-set tuning and for stereo tape recorders.

Brimar, Ltd., Footscray, Sidcup, Kent.

"Monitor " push -button-tuned television aerial (BellingLee).

BUSH (38, $\times 25$ )
A new departure for Bush is the introduction of a tape-recorder-the TP50. This uses a 4-track, singlespeed deck, playing at $3 \frac{3}{4}-\mathrm{in} / \mathrm{sec}$; simple controls are provided. Another new introduction is the VTR103 nine-transistor portable radio, which operates on f.m. and a.m. and has a telescopic aerial for use at v.h.f. The VHF91 is a valve receiver covering three wavebands. Two speakers are used and separate bass and treble controls are provided. New television sets, the TV10jc and T102c, use 19 -in and 23-in tubes respectively.

Bush Radio Limited, Power Road, London, W. 4.

CLARKE \& SMITH ( 406,414 )
H.M.V. high-fidelity equipment displayed includes an a.m./f.m. tuner and separate and combined stereo pre-amplifiers and amplifiers. An unusual feature of two of these-the 556 comprehensive pre-amplifier and the 555 combined pre-amplifier and $2 \times 10$-watt amplifier-is the provision of a cr.t. level indicator for indruting correct balance or checking the frequency response using a frequency test record. Another unusual feature of the 556 is the provision of a signal (oblained by mixing both sterco channels and approximately 16 dB down on each) for feedıng a central loudspeaker to reduce " hole in the middle "effects.

Clarke $\mathfrak{E}$ Smith Manufacturing Co., Ltd., Melbourne Works, Wallington, Surrey.

## COSSOR (52)

The CR1501A stereo radio-gram incorporates two double-cone 8 -in speakers with a balance control. The Philips 4 -speed autochanger is buttoncontrolled, and the amplifier is

equipped for use with a tape-recorder. The name " Melody Maker" is again used, this time for an a.m./f.m. radio. Built-in aerials are provided for both transmissions and external aerials may be used. A portable 4 -speed stereo record-player, the CR1800A, has detachable speakers and the pickup contains a turnover stereo head with two sapphire styli.

Cossor Radio Go Television, Ltd., 233, Tottenham Court Road, London, W.1.

## DANSETTE (39)

Several portable transistor receivers and a very wide range of fifteen mains and battery (transistorized) mono record reproducers and portable radio-grams will be on show. An unusual feature of one of thesethe TRG/45-is that the radio is automatically switched off when the record player is started. Also exhibited is the stereo A35 record reproducer with its separate second loudspeaker.

Dansette Products Ltd., 112/116 Old Street, London, E.C.1.

DECCA ( $22,418, \times 29$ )
The wide range of gramophones and radio and television receiving equipment shown here culminates in the stereo Decola. New stereo radiograms Types 550 and 650, together with the 700 are of particular interest: push-pull amplifiers are used in the 650 and 700 . Television receivers use 19 - and 23 -in tubes and the new DR29/C has tambour doors over the c.r.t. New radio receivers include a mains "consolette " (DMR!88) of unusual design and a 6-transistor m.w. and 1.w. set, the Debonette.

In the Audio Avenue is shown the


New Ekco "radiostereogramophone" SRG 395 has high-quality 8 -in loudspeakers and affords reception of f.m. and a.m. transmissions.
new SRG700 a.m./f.m. stereo radiogram. The three four-inch middle and upper frequency (crossover frequency $\approx 350 \mathrm{c} / \mathrm{s}$ ) loudspeakers for each stereo channel are internally mounted on two baffles and-an unusual feature-each baffle can be rotated about a vertical axis through up to $55^{\circ}$. This allows adjustments to be made to the apparent width and direction of the sound field.
Decca Radio and Television Ltd., 15-17 Ingate Place, Queenstown Road, London, S.W. 8.

## DEFIANT (2)

A range of sound reproducers includes the HF3 automatic player, which has three speakers and covers $50 \mathrm{c} / \mathrm{s}-15 \mathrm{Kc} / \mathrm{s}$ at $3 \frac{1}{2} \mathrm{~W}$. The T12 tape recorder is a $3 \frac{3}{4}-\mathrm{in} / \mathrm{sec}$ model with a frequency response of $100 \mathrm{c} / \mathrm{s}$ $8 \mathrm{kc} / \mathrm{s}$ at 3 W output and has superimpose facilities. Automatic stabilization of picture height is provided in the 9A35 19in television receiver, which has a forward-tilted screen to reduce reflections.

Co-operative Wholesale Society, Ltd., Radio $\mathcal{E}$ Television Dept., Alma Park, Warley Street, Upminster, Essex.

## DESIGN FURNITURE (30)

Exhibited on this stand is a range of equipment, record storage and loudspeaker cabinets, and also television tables. New introductions include two loudspeaker cabinets which have been tested and approved for use with their speakers by Goodmans, and a combined cocktail/record cubinet.

Design Furniture, Ltd., Carnwath Road, London, S.W.6.

## DOMAIN (113A)

A range of display stands for television receivers, tape recorders, etc., include free-standing and peg-board
shelves, and a special trolley for the Mullard valve tester. A lettering and pricing system for peg-board displays is also exhibited. New to the range is the BUK display stand, which can take many forms, the frames being joined by means of plastic "pushon " connectors.

Domain Products, Ltd., Domain Works, Barnby Street, London, N.W.1.

## DYNATRON (27)

Shown is the attractively styled new "Planet" range of television receivers, features of which are their adaptability to 625 -line or u.h.f. transmissions, should these be provided. Available for this range is a " wire-less" remote control unit for channel-selection, volume and brightness. Other new introductions include valve and transistor a.m./f.m. receivers. A feature of the valve model-the Pathfinderis that it gives continuous coverage from medium waves down to the 12 -metre band (as well as covering long waves). Among notable stereo radiograms is the Queen Anne which also incorporates a tape recorder. Also shown are mains and battery (transistor) record reproducers and the Cordova three-speed tape recorder.

Dynatron Radio Ltd., St. Peter's Road, Furze Platt, Maidenhead, Berks.

## E.A.R. (56)

The main emphasis on this stand is on the recently-introduced range of " $1000-\mathrm{M}$ " one-watt output battery (cordless) transistor units. Included in this range are the Astor receiver (which also features a relatively-large ( $5-\mathrm{in}$ ) loudspeaker and slow-motion tuning) and the AutoBat automatic four-speed transistor record reproducer (also available with radio included). Also shown are mains record players and repro-


Elizabethan "Corsair" a.m. transistor receiver.
ducers in the MusicMaker, Bantam and Triple-Four ( 4 controls, 4 speeds, 4 loudspeakers) series. Stereo and mono record listening booths for shops are also displayed.

Electric Audio Reproducers Ltd., The Square, Isleworth, Middlesex.
E.M.I. RECORDS (62, X19)

Shown on this stand are $33 \frac{1}{3}$ r.p.m. 10 and 12 in , and 45 r.p.m. 7 in microgroove records under the labels of Capitol, Columbia, H.M.V., M.G.M., Mercury, Parlophone and Top Rank. A record query answering service will also be operated.
E.M.I. Records, Ltd., E.M.I. House, 20 Manchester Square, London, W.1.

## EASCO (417)

On show will be a selection of this company's specialized audio equipment. For marine use this includes a 10 -watt loudhailer, talkback intercom panels, a transistorized combined talkback and telephone system, amplifiers for sound relay applications, and an amplifier capable of operating from 110 V d.c. (giving eight watts
(Continued on page 465)
output). Another specialized item is a talkback intercom system for fire engine ladders.

Easco Electrical (Holdings), Ltd., 6 and 8 Brighton Terrace, Brixton, London, S.W.9.

## EKCO (33, X6)

Television receivers in the three main " styles"-traditional, contemporary and Continental-are one of the features on this stand. All television receivers have provision for internal fitting of an add-on unit to cater for a change of standards, should this come about: four new models have motor-driven tuning. Radio and gramophone equipment of particular interest is a transistor a.m./f.m. portable receiver with a tape recorder outlet and a new "radiostereogramophone". Also on show are car radios, a tape recorder and range of record players and radio receivers.
E. K. Cole, Ltd., Ekco Works, Southend-on-Sea, Essex.

## ELIZABETHAN (3)

This company has recently entered the transistor receiver and (valve) record reproducer market and a second record reproducer is introduced at this show. A four-track version of the inexpensive singlespeed ( 3 isin $/ \mathrm{sec}$ ) Popular de Luxe and a two-track version of the threespeed F.T. 3 are additions to this company's wide range of tape recorders. This range also includes two- and four-track versions of the "Major" recorder with its special features of six-watts push-pull out-
put, bass and treble loudspeaker system and meter level indicator. Elizabethan Tape Recorders Ltd., Bridge Close, Oldchurch Road, Romford, Essex.

EMBER (J|6)
Shown on this stand are a range of inexpensive single-channel, 12 -in $33 \frac{1}{3}$ r.p.m. and 7 -in 45 r.p.m. microgroove popular and jazz records. This company holds the licence to produce in this country all records and film sound tracks of the American 20th Fox Record Corporation.

Ember Records (International) Ltd., Central House, 12 Great Newport Street, London, W.C.2.

## EVER READY ( $\mathbf{2 8}, \mathbf{X 4}$ )

The full range of Ever Ready and Berec portable and table model transistor receivers will be on show. Also displayed is the recentlyintroduced dual purpose portable and car radio. This, on being plugged into its special screen container in the car, is automatically connected to the car aerial, car battery (which supplies a higher voltage and thus increases the power output), and an 8 in $\times 5$ in loudspeaker in place of the corresponding internal units. Also exhibited are ranges of batteries for various purposes.

Ever Ready Co. (Great Britain) Ltd., Hercules Place, London, N.7.

## FERGUSON (20, X5)

With one exception (a 7 -valve a.m./ f.m. set), all Ferguson's radio receivers are transistorized, but valves are used in the radiogramophones,
two of which (660RG, 661RG) have headphone sockets for personal binaural listening. All new television receivers contain switching for conversion to $625-\mathrm{line}$ u.h.f. reception, should the occasion arise: additional components required will include a sub-chassis and u.h.f. tuner.
Other new items include two tape recorders and a personal portable radio.

Ferguson Radio Corporation, Ltd., Thorn House, Upper St. Martin's Lane, London, W.C.2.

FERRANTI (14, X2)
New television receivers on show use the square-cornered 19- and 23in c.r.ts. and this company's first 23 -in table model features remote control. For radio reception the PT. 1065 is of interest. This is a 9transistor portable receiver covering v.h.f./f.m., and medium and long waves. A relescopic aerial is fitted and the carrying handle can be detached so that the set presents a neat appearance as a table model.

The 19-in "Homemaker" television receiver is claimed to be suitable for conversion to 625 -line reception should the need arise.

Ferranti Radio \&o Television Ltd., 41-47 Old Street, London, E.C.1.

## FIDELITY (8)

Half of the range of auto and nonauto record players, transistor receivers and Argyll two- and fourtrack tape recorders on show are new models. Also exhibited are the inexpensive Coronet transistor receiver (featuring a 90 mW push-


Wireless World, September 1961
pull output, two i.f. stages and a socket for private earphone listening or tape recording) and the RG-26 a.m./f.m. radio-gram (which features a four-watt output).

Fidelity Radio, Ltd., 11-13 Blechynden Street, London, W.11.

## FUND FOR THE BLIND (312)

Equipment and appliances designed or modified to help blind people to overcome their handicap are displayed on the stand which features the service of installing and maintaining radio sets for the blind. The Fund helps the civilian blind of Greater London by collecting and distributing money to fourteen institutions and associations.

Greater London Fund for the Blind, 2 Wyndham Place, London, W.1.

## G.P.O. (306)

A feature of the telecommunications display mounted by the Post Office is the part the $500-\mathrm{ft}$ tower to be erected near Tottenham Court Road, London, will play in the future development of micro-wave radio links for the telephone service. A look still further into the future is provided by a display depicting the use of earth satellites in international telephone links.

General Post Office, Headquarters Building, St. Martins-le-Grand, London, E.C.1.

## GARRARD (36)

Recent introductions by this company include the Autoslim and Auto-slim-de-luxe record changers, which have been specially designed to occupy minimum height, and the Laboratory Series automatic record player type A with its unusual sandwich constructed turntable and weight-counterbalanced pickup arm. Also shown are the well-known magazine loading single-speed ( $33 \mathrm{in} / \mathrm{sec}$ ) two- and four-track tape decks, SPG3 stylus pressure gauge, TPA12 pickup arm and 301 adjustable-speed transcription record turntable. A range of crystal and ceramic stereo and mono pickups is also available.

Garrard Engineering \&o Manufacturing Co., Ltd., Newcastle Street, Swindon, Wilts.

## GRAMOPHONE COMPANY (408)

Shown on this stand is the latest version of the E.M.I. " Voicemaster" tape recorder-the 65A. The use of four tracks and separate record and replay heads and amplifiers allows (with extra switching) rerecording to be carried out (from one track to another)-a facility normally only possible with two tape recorders. Also displayed is the E.M.I. EPU100 variable-reluctance stereo pickup and arm with its special features of sideways and longitudinal balance about the single viscous-damped pivot and very low
effective stylus tip mass (approximately 1 mgm ).

Also exhibited are a range of E.M.I. record reproducers, the Glyndebourne IV a.m./f.m. stereo radio-gram with suitable external loudspeaker systems and, for the home constructor, the 985 record turntable (available in mains or battery versions and with pickup and arm) and DLSU bass and treble loudspeaker systems.

Gramophone Co., Ltd., Blyth Road. Hayes, Middlesex.

## HACKER (55)

Newly introduced by this company is an f.m.-only receiver which features three i.f. stages, a seven-watt pushpull output, and adjustable local station markers on the tuning scale. Also shown are transistor portable receivers, record reproducers and radio-grams which feature one-watt push-pull outputs and large ( $8 \times 5 \mathrm{in}$ ) resistive-slot loaded loudspeakers. The receiver-the Herald-is also unusual in incorporating a treble tone control and 2000 -ohm input for a microphone (to provide a baby alarm) or pickup.
Hacker Radio Ltd., Norreys Drive, Cox Green, Maidenhead, Berks.

## heathkit (ili)

The full range of Heathkit highfidelity, test gear and radio kits is shown, with several additions. The GC-1U transistorized communications receiver covers the range $550 \mathrm{kc} / \mathrm{s}$ to $30 \mathrm{Mc} / \mathrm{s}$ and over most of the range gives better than 10 dB signal-to-noise with $2 \mu \mathrm{~V}$ input. An inexpensive l.f. oscillator-the AO1 U —works from $20 \mathrm{c} / \mathrm{s}-150 \mathrm{kc} / \mathrm{s}$ in four ranges at an output of up to 10 V r.m.s. The square wave output is $20 \mathrm{c} / \mathrm{s}-50 \mathrm{kc} / \mathrm{s}$ at a maximum output of 80 V p-p. The $200-400 \mathrm{~V}$ stabilized power supply-HSP-1has an output impedance of less than $0.5 \Omega$ at $500 \mathrm{kc} / \mathrm{s}$ and a total noise of less than 1 mV . Singlesideband adaptor SB-10 covers $10-80$ metres and requires less than 3 W r.f. input for 10 W peak envelope power.
Daystrom Lid., Bristol Road, Gloucester.

HIS MASTER'S VOICE $(23, \times 28)$
Incorporating a socket for carradio aerial and another for output to a tape recorder, the Model 1424 receiver-a medium- and long-wave portable-employs seven transistors, three of which are the diffused-alloy type giving high gain. A mains a.m./f.m. table model, the 1379, has two $8 \times 5$ in loudspeakers, one on either side of the dial.

A new a.m./f.m. radio-cum-stereogramophone (Model 1644) incorporates a "spring" reverberation unit and on radio and " mono" the two stereo channels are operated in push-pull.

In the range of television receivers the 1922 is of particular interest as it employs a motorized tuner (which is adaptable for u.h.f.) with only one push-button for control. The field, as well as the line, timebase is stabilized.

British Radio Corporation Ltd., 21 Cavendish Place, Cavendish Square, London, W. 1.

## HOBDAY (53, X13)

In association with Ultimate Television Rentals this company is illustrating a rental scheme for Alba television receivers. An information counter on Stand 53 enables members of the public to obtain full details of this scheme. As wholesalers, Hobday exhibit a wide range of radio and television receiving equipment and sound-reproducing apparatus distributed by them to the retail trade.

Christopher Hobday Ltd., Hobday House, Southchurch Road, Southend-on-Sea, Essex.

## INVICTA (I7)

New 19-in and 23-in television receivers on show incorporate motordriven, push-button tuning and re-mote-control units available give control of volume, brightness and channel selection. Several new transistor portable radios are displayed.
Invicta Radio Ltd., 100 Great Portland Street, London, W.1.

## J-BEAM (18)

For use with a portable receiver the C.R.P. 6 aerial is of interest: this has two p.v.c. suckers which enable it to be attached to any suitable surface, such as the bodywork of a car. Television and f.m. aerials are on show, including arrays using JBeam's specialities, the end-fed BandI dipole and the Band-III skeleton slot. From the company's associates, Radio Telephone Aerial Systems, come communications aerials proofed against adverse weather conditions by an epoxy-resin enamel.
f-Beam Aerials Ltd., Westonia, Weston Favell, Northampton.

## JASON (411)

Newly introduced by this company for use with tape recorders are a twochannel unit with separate record amplifiers and playback pre-amplifiers, erase and bias (available ready built or in kit form) and also, in kit form only, a tunable transistor a.m. tuner. The range of f.m. tuner kits on show includes fringe and a.f.c. models.

Ready-built units displayed include stereo and mono combined comprehensive pre-amplifiers and 10 -watt amplifiers and also tuners covering f.m. and TV sound (switched tuning) or f.m. only (variable tuning).

Fason Motor Eo Electronic Co., Kimberley Gardens, Harringay, London, N.4.


Above: Gorrord "Autoslim-de-Luxe" record changer.

His Master's Voice battery portable receiver Model 1424 has socket for taperecording.


## K.B. (50)

An addition to the range of transistor portables is the "Cavalier," which is a 7 -transistor set with sockets for caraerial, tape-recording and baby alarm. Three new transistor record players are shown and the "Nocturne" small stereo radio-gram is on view. A full range of television receivers from 19 -in to 24 -in is displayed and a newcomer is the $4-$ track, $3 \frac{3}{4}-\mathrm{in} / \mathrm{sec}$ tape recorder.

Kolster-Brandes Ltd., Footscray, Sidcup, Kent.

KERRY'S (43)
This wholesaler will display a comprehensive range of television and radio receivers, radio-grams, record players, record storage cabinets and television tables from Alba, Berec, Dansette, E.A.R., Elizabcthan, Ever Ready, Fidelity, Marconi, Perdio, Philips, Regentone and W.B.

Kerry's (Great Britain) Ltd., Warton Road, Stratford, London, E. 15 .

## LEE PRODUCTS (415)

This company's standard range of equipment includes two and fourtrack tape recorders using the singlespeed ( 3 in $\mathrm{in} / \mathrm{sec}$ ) B.S.R. "Monardeck", valve and transistor four-speed record reproducers (the latter with a 1-watt, push-pull output), an a.m. f.m. radio-gram chassis and a 10 -watt amplifier. It is also hoped to introduce a new range of audio equipment which includes a.m./f.m. and f.m.
tuners and stereo and mono amplifiers and pre-amplifiers.

Lee Products (Great Britain) Ltd., Elpico House, Longford Street, London, N.W.I.

## LINGUAPHONE (209)

Recorded language courses in 38 languages, many of them now on 45 r.p.m. discs, are available from the Institute. For technical students the Institute provides supplementary printed courses after the basic language has been mastered.

Linguaphone Institute, Ltd., Linguaphone House, 207-209 Regent Street, London, W.1.

## LOWTHER (413)

Horn-loaded loudspeaker systems shown include the well-known TP1 and Acousta mono units and also the stereo Acousta-Twin-which features variable reflectors for positioning the apparent sound sources. General features of the loudspeaker drive units exhibited are their high-flux magnets and the usc of a fixed central "stabilizer" to load the inner of the two cones and to reduce interference between sound radiated from its various parts. Also shown are a comprehensive control unit and two power amplifiers-the latter including feedback to an unusual point in the output valves (their suppressor grids).

Lowther Manufacturing Co. Ltd., Lowther House, St. Mark's Road, Bromley, Kent.

## MARCONIPHONE (4I)

Called their " Diamond Jubilee Range" (as it was in 1901 that Guglielmo Marconi succeeded in spanning the Atlantic by wireless), Marconiphone are showing many new models. Among these are the VT170 television receiver with a 19 -in c.r.t. and preset fine tuning, the T98B transistor table model a.m. receiver and the RG95 six-valve a.m./f.m. radiogramophone.

The T84 is an a.m./f.m. table model mains receiver tuning over long and medium waves and Band II.
British Radio Corporation Ltd., 21 Cavendish Place, Cavendish Square, London, W. 1.

## MARKOVITS (113)

The exhibit comprises a selection of die-cast, electroplated nameplates and emblems for the radio and electrical industry. Also on view is a new type of metal nameplate with a decorative plastic insert.
I. Markovits Ltd., Premier House, 8 Golden Square, London, W.1.

## METROPOLITAN POLICE (308)

A variety of equipment used by the Police is shown on the stand on which are featured mobile equipment and headquarters radio operating positions. The recently introduced " specially equipped traffic accident car" (SETAC), which on show, is fitted with a 7 -channel transmitter-
receiver which has a transmitter output of 10 watts.
Metropolitan Police, New Scotland Yard, London, S.W.1.

MULLARD ( $46,316, \times 24, \times 26, \times 26 A$ )
As last year, the main stand (46) comprises a cinema. This year two films are shown simultaneously illustrating the advantages accruing from the possession of a "second" set; also featured are recent developments in Mullard valves, c.r.ts and components employed in domestic apparatus.
The always popular " Home Constructor Centre" is this year at X26A, where the full range of Mullard technical publications is available, as is technical advice on Mullard designs and the use of Mullard valves, semiconductors and c.r.ts.

Other Mullard stands are X24 (for setmakers) "and X26, " Dealer Rendezvous."
Mullard Ltd., Mullard House, Torrington Place, London, W.C.1.

## MULTICORE (65, X16)

Shown for the first time are solder rings, washers and pellets in several alloys, with or without flux, for automatic assembly of computers and sub-units. New alloys containing silver are shown and additions to the range of tin/lead alloys are specially low and high melting-point solders. Several new packs of solder are shown, and the range of Bib tape-recording accessories is exhibited, including the popular Bib splicer.
Multicore Solders, Ltd., Maylands Avenue, Hemel Hempstead, Herts.

## MURPHY ( $16, \times 1$ )

This company, which was the first to introduce tunable television receivers with a preset fine-tuner control, this year present their "Astra" range which, when fitted with v.h.f. radio facilities, provide push-button tuning of Home, Light and Third programmes. The new 19- and 23 -in c.r.ts are used and the receivers are claimed to be capable of conversion from 405 to 625 line transmissions should the need arise at some time in the future.
For radio reception new sets include a pocket-size personal portable tuning over m.w. and v.h.f./f.m. and a transistor table model whose back repeats the front design, thus ensuring neat appearance from any angle.

Murphy Radio Ltd., Welwyn Garden City, Herts.

## N.E.V. (109)

The " Nev Mini-Eye Transistor "a transistorized closed-circuit television camera-is being demonstrated. This camera has no external controls and is available for export in 525 - and $625-$ line versions.

Also on show is the "Nev Eye" low-cost camera, and the company's range of cathode-ray tube repair and manufacturing plant will be displayed.
Nottingham Electronic Valve Co., Ltd., Main Street, East Bridgford, Notts.

PAM (21, X3)
The complete range of radio and television receivers and sound equipment is on view. A range of transistor radio receivers includes the TB77, a table model using seven transistors on a printed circuit. The range of television receivers incorporates transistor synchronization and remotecontrol units, and all the types shown can be converted to operate on 625 lines. Stereophonic reproduction is provided by the RG630 radio-gram, which incorporates a four-speed autochanger and medium wave/v.h.f. radio receiver.
Pam (Radio and Television) Ltd., 295 Regent Street, London, W.1.


Portogram " Varsity Model B" record reproducer.

## PAMPHONIC (58)

The Domestic Natural Sound division are showing an advance model of their "Slim Line" stereo radio-gram designed to operate with the new Pillar speakers. This speaker is a tuned column containing two cones, one covering the range $45 \mathrm{c} / \mathrm{s}-12 \mathrm{kc} / \mathrm{s}$ and the other $1 \mathrm{kc} / \mathrm{s}$ upwards. The Reflectograph tape recorder is now manufactured by Pamphonic and is on view. The Beamed Sound division exhibit kits from which can be assembled sound reinforcement systems for halls, churches, etc. A 4 -ft. indoor line source loud-speaker is shown.

Pamphonic Reproducers, Ltd., 17 Stratton Street, London, W.1.

PERDIO (I)
The range of transistor receivers made by this company includes the Mini-Six-features of which are its small size ( $4 \frac{1}{8}$ in by $2 \frac{3}{4} \mathrm{in}$ by $1 \frac{1}{8} \mathrm{in}$ ), light weight ( 8 oz ) and 200 mW pushpull output, and the Multi-Band 102 -which is unusual in that it gives

"Diadem," Model 619 by R.G.D., has push-buttons at top to avoid movement of set when operating controls. gram with a.m./f.m. radio and four-speed turntable.

continuous coverage from medium waves to the 11-metre band (as well as covering the long-wave band) and that it uses amplified a.g.c. General features of this company's range are the provision of sockets for car aerial and for private earphone listening or tape recording.

Perdio Ltd., Perdio House, Bonhill Street, London, E.C.2.

## PETO SCOTT (26)

Motorized tuning and automatic contrast control are features of new television receivers. The ARG71 stereo radio-gram uses nine valves and will play both mono and stereo records; an a.m./f.m. radio receiver is incorporated. A 4 -track, singlespeed tape recorder and a transistor portable are shown.

Peto Scott Electrical Instruments Ltd., Addlestone Road, Weybridge, Surrey.

PHILCO (35, $\times 27$ )
"Selectaflash" is the name given Philco's latest remote control system for television. This uses an ordinary hand torch as the controlling device, the beam being directed to either of two sensitive spots on the set. The receivers also incorporate switching for conversion to 625 -line working, should the need arise.

Other new items include radio receivers, three radiogramophones, record players and a portable tape recorder.

Philco (Gt. Britain) Ltd., 21 Cavendish Place, London, W.1.

PHILIPS ( $10,15,316,401, \times 30$ )
Television receivers on view include the 19 TG 108 U 19-in model with side-mounted controls and hinged chassis, and the $23-\mathrm{in}$, 23 TG 107 U which has automatic fine tuning. Several transistor portable radio receivers are shown, including the 303T medium- and long-wave model. The speaker is 5 -in diameter and the handle folds for indoor use, while a socket is provided for use with a car aerial. A range of sound equipment is on display.

In the Audio Avenue the exhibit comprises mono and stereo recordplayers and radio-grams, including the full range of "Disc Jockey" players.

Philips Electrical, Ltd., Century House, Shaftesbury Avenue, London, W.C.2.

## PITRIE (108)

As in previous years, Pitrie are welcoming trade visitors to discusss their range of replacement cathoderay tubes. Also shown is a range of components.
Pitrie Ltd., 21 Noel Street, London. W.1.

## PORTOGRAM (416)

Shown on this stand are tape recorders (incorporating the Collaro "Studio" three-speed and B.S.R.
"Monardeck" single-speed decks) and a range of record players and reproducers. Prominent among the latter is the "Varsity" Model B which features the continuously-variable speed Lenco turntable, Collaro Studio pickup, an automatic device for lowering the pickup on to or raising it from the record, and a six-watt pushpull amplifier. An unusual feature of the AutoGram is the "Panoramic" tone control which allows treble boost with bass cut or bass boost with treble cut.

Portogram Radio Electrical Industries Ltd., Audio Works, Paxton Road, Tottenham, London, N.17.

## PYE (32, $\times 7$ )

A full range of $19-$ in and 23 -in television receivers are shown, which incorporate push-button automatic tuning and, as an accessory, remote control. All receivers in the range use transistors in the time-base synchronizing circuits, hence the name, the "Transista Range." Also on view are portable radio receivers and a range of car radios includes the TCR $3000 / \mathrm{E}$, which covers $1600 \mathrm{kc} / \mathrm{s}$ to $17.4 \mathrm{Mc} / \mathrm{s}$ in nine wavebands.
Pye, Ltd., Cambridge.

## R.G.D. (44, X10)

The "Diadem" range of television receivers, which have an octagonal mask claimed to reduce eyestrain, and a leather-cased transistor portable receiver tuning over medium and long waves, are among the new models shown on this stand. Also on show is a wide range of radio receivers, radiogramophones and record players. Another new set is a 7 -valve mains a.m./f.m. set with sockets for connection of a tape recorder (Model 37). This set has a plastics-moulded case and a $7 \times 4$-in loudspeaker.
Radio Gramophone Development Co., Ltd., Eastern Avenue West, Romford, Essex.

## R.S.G.B. (315)

Exhibits of both home-constructed and commercial gear for the amateur transmitter and short-wave listener are shown on this stand. There will also be found the latest editions of the books and pamphlets issued by the Society, including "Amateur Radio Call" Book" and "Radio Amateurs' Examination Manual ".

Radio Society of Great Britain, New Ruskin House, Little Russell Street, London, W.C.1.

## R.T.R.A. (202. 316)

In addition to the information bureau for both the trade and the public on its main stand R.T.R.A. is featuring its apprenticeship scheme in the Trade Technical Section on the first floor.

Radio and Television Retailers' Association, 15-17 Goodge Street, London, W.1.

## REGENTONE (45)

Shown on this stand is a wide range of television and radio receivers, record players and radiogramophones. New items include the TV191 and 192 19-in television receivers, the 191 having turret tuning and the 192 push button. Two new transistor radio receivers are the BT16 and BT18, the BT18 being a "pocket" personal set having a linear tuning scale.

Regentone Radio E Television, Ltd., Eastern Avenue West, Romford, Essex.

## REHABILITATION OF

DISABLED (313)
Details are available on this stand of the work of the Council for $\mathrm{Re}-$ habilitation of the Disabled whose primary function is, through training courses, to facilitate the return to work of injured and disabled people. Among the courses provided by the Council is one covering radio maintenance.
British Council for Rehabilitation of the Disabled, Tavistock House (South), Tavistock Square, London, W.C.1.

ROBERTS (63, $\times 18$ )
Transistor receivers shown on this stand include the R200 and RT7. Features of the RT7 are its large ( $8 \times 5$-in) loudspeaker, one-watt push-pull output and treble tone control. Features of the R200 are its $\frac{1}{2}$-watt push-pull output and relatively-large ( 5 -in) loudspeaker. Protective carrying cases are available for both these receivers.
Roberts' Radio Co., Lid., Creek Road, East Molesey, Surrey.

## ROLA CELESTION (210)

The main feature of this stand is the Colaudio II loudspeaker system. The 12 -in bass unit in this is unusual in having a "solid" rather than a hollow cone. This is made of "exploded" polystyrene to achieve a high stiffness-to-weight ratio. This loudspeaker also has a very low freeair fundamental resonance (about $10 \mathrm{c} / \mathrm{s}$ ) so that although the cabinet volume is only 1.8 cu ft , this resonance is not raised to more than about $40 \mathrm{c} / \mathrm{s}$. A $2 \frac{1}{4}$-in pressure-driven tweeter crossing over around $2 \mathrm{kc} / \mathrm{s}$ is also used.
Also displayed are domestic loudspeakers with diameters ranging from $2 \frac{1}{2}$ in to 15 in . Among commercial loudspeakers will be shown new bowl diffusers.

Rola Celestion Ltd., Ferry Works, Thames Ditton, Surrey.
s.t.c. (410)

This company is showing its range of high-quality microphones. These include moving-coil units with cardioid or, in the case of the well-known "ball and biscuit" 4021, omni-
directional polar responses. Ribbon microphones include the 4038 as well as the 4104 close-talking noisediscriminating unit. A combined ribbon and moving-coil microphone which can be switched to give alternative figure-of-eight, omnidirectional or cardioid polar responses, the $4033-\mathrm{A}$, is also displayed.

Standard Telephones © Cables, Ltd., Connaught House, 63 Aldwych, London, W.C.2.

## SAGA RECORDS (118)

Recordings shown by this company include mono microgroove $33 \frac{1}{3}$ r.p.m. 12 in and 45 r.p.m. 7 in records (the latter including the Dandy series for children), mono $3 \frac{3}{4} \mathrm{in} / \mathrm{sec}$ and stereo and mono $7 \frac{1}{2} \mathrm{in} / \mathrm{sec}$ pre-recorded tapes.

Saga Records Ltd., 127 Kensal Road, London, W. 10.

## SIMON (II7)

An addition to the range of tape recorders is the high quality SP5 twin track, two speed instrument, which is sold in either mono or stereo versions, with easy conversion. The deck operates at $7 \frac{1}{2} \mathrm{in} / \mathrm{sec}$ or $3 \frac{3}{4} \mathrm{in} / \mathrm{sec}$ and at the former speed, the frequency response is $30 \mathrm{c} / \mathrm{s}-20 \mathrm{kc} / \mathrm{s}$. The recorded signal, which may be monitored through the internal speaker, or by earphones, can be transferred from one track to the other, and mixing, fade and pause controls are incorporated. A 2.5 -in meter indicates the record level, and this can also be switched to read the bias level.

Simon Equipment Ltd., 46-48 George Street, Portman Square, London, W.1.

## SLINGSBY (24)

Trucks and trolleys designed for the easy and safe moving of heavy apparatus are manufactured by this company.
H. C. Slingsby, Ltd., 89, 95 \& 97 Kingsway, London, W.C.2.

## SOUTHGATE TUBULAR PRODUCTS

 (205)Shop display equipment shown includes a new battery-powered turntable, which is 6 -in diameter and carries a load of four pounds; four weeks' continuous operation is obtained from two U. 2 batteries. Several new fittings for the Unipole display stand are on view.

Southgate Tubular Products, 148 Chase Side, Southgate, London, N.14.

## STELLA (40)

Valve and transistor radio receivers, television receivers and sound reproducers are shown. The ST243U mains radio is a 6 valve a.m./f.m receiver with a hank aerial for v.h.f. reception and a loop aerial for medium and long waves. A special balance control is used for stereo balance in the ST 314 A radio-gram,
which uses the Philips 4-speed automatic changer and push-button function switch. A v.h.f. radio is incorporated. Mono and stereo record-players are on view and the ST562A employs a high-fidelity stereo pickup.

Stella Radio and Television Co. Ltd., Astra House, 121-123 Shaftesbury Avenue, London, W.C.2.

## T.C.C. (54, X14)

A very wide range of capacitors is on view, among the new additions being ranges of wet and dry solid sintered capacitors for operation in extremes of temperature. Vertical mounting is adopted in the Elkomold range of miniature electrolytics and mounting feet are moulded into the case. Tubular capacitors shown work in the range $-40^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ and comply with H.I requirements; a considerable size reduction is achieved. Printedcircuit boards displayed contain plated-through holes, and flushbonded panels in silver and rhodium are available.

Telegraph Condenser Co., Ltd., Wales Farm Road, North Acton, London, W. 3.

## TAPE RECORDERS (405)

New tape recorders introduced include two and four-track single and three-speed models using the B.S.R. "Monardeck" and Collaro "Studio" decks respectively. Also shown are the Connoisseur with its built-in fourspeaker system, and the four-track, three-speed Soundmaster with its special features of push-pull erase oscillator, level indication by recording meter, separate record and play back amplifiers, low-noise transistor play back pre-amplifier and 10 -watt "low loaded" push-pull output stage.

Also shown is the Sonocolor range of magnetic tapes and associated equipment.
Tape Recorders (Electronics) Ltd., 784-788 High Road, Tottenham, London, N. 17.

TAYLOR (110)
The full range of test equipment is displayed, with several recent additions. For the dealer, Sweep Oscillator 92B covers the frequency range $4-210 \mathrm{Mc} / \mathrm{s}$ on fundamentals and has a maximum output of 300 mV . The 45C Valve Tester is capable of testing over 5,000 valve types, and will check 12 V car radio valves. A range of multimeters and valve voltmeters is shown, and the display of panel meters includes miniature edgewise mounting types.

Taylor Electrical Instruments, Montrose Avenue, Trading Estate, Slough, Bucks.

## TELENG (107)

Specialists in the field of wired television and v.h.f./f.m. relay and communal-aerial systems, this com-
pany is showing a wide range of equipment for these applications. New items include a repeater with a novel a.g.c. system, which is claimed to avoid the picture degradation inherent in the use of mean-level a.g.c. Another item of interest is a ferrite-cored directional transformer for the splitting of one coaxial feed into two. Whilst the forward loss is only 3.5 dB , the reverse loss is at least 14 dB .

Teleng Ltd., Teleng Works, Church Road, Harold Wood, Romford, Essex.

## TELERECTION (34)

A wide range of television and f.m. aerials catering for conditions ranging from swamp signal to extreme fringe is shown together with new combined arrays and a spring-assembly feature for Band-III elements. The name "FM Clipper" is given to Band-II attachments for v.h.f./f.m. use.

Telerection Ltd., Antenna Works, Lynch Lane, Weymouth, Dorset.

## TELESURANCE (5)

In addition to providing details of its maintenance-insurance scheme Telesurance has organized a composite display of television receivers.

Telesurance Ltd., 14 Windmill Street, London, W.1.

## TERRITORIAL ARMY (3I7)

The 65th Signal Regiment (T.A.), formerly No. 1 Special Communications Regt., is showing some of the equipment used for training in such trades as $\mathrm{W} / \mathrm{T}$ operator, radio mechanic and line mechanic in this signals unit.

Territorial Army (65th Signal Regt.), 79-85 Worship Street, London, E.C.2.

## TEXPEX (314)

This firm offers a specificationwriting service to the radio and electronics industry. The stand functions. as an enquiry office.

Texpex, Ltd., 110 Kennington Road, London, S.E.11.

## THORN-A.E.I. $(29, \times 8)$

Mazda valves and cathode-ray tubes are displayed on this stand. Notable are the new 19- and 23-in twin-panel television c.r.ts which have the safety glass bonded to the tube face.
Preferred ranges of valves for a.m./ f.m. sets are shown and another feature is the illustration with typical circuits of the use of valves and c.r.ts.

Thorn-A.E.I. Radio Valves and Tubes, Ltd., 155 Charing Cross Road, London, W.C.2.

## TRADE TECHNICAL SECTION (316)

A number of firms and associations are showing equipment and services provided for the serviceman. On this stand is also shown the winning. entries and runners up in the com-

Pilot (on the Ultra stand) "Coffee Table" radiogram, tuning over medium and long waves, is about 3 ft bin long.


Above: Simon SP5 twin-track tope recorder. The record-level meter may be switched to read bias level.

petition for servicing ideas sponsored jointly by our sister journal Wireless $\mathcal{E}$ Electrical Trader and the exhibition organizers.

Radio Industry Exhibitions Ltd., 59 Russell Square, London, W.C.1.

## ULTRA (4, X31)

Most visitors to the show will know that the Ultra TR70 transistor radio won the Duke of Edinburgh's Prize for Elegant Design: this set and many other radio and television receivers and gramophones are on show. Two new 23 -in TV sets are claimed to be capable of conversion to 625 -line reception, should this be necessary. New Pilot models include a "coffeetable "style medium- and long-wave radiogramophone which has a bassreflex mounting chamber for the loudspeaker.

Ultra Radio and Television Ltd., Television House, Field End Road, Eastcote, Ruislip, Middlesex.

## WHITELEY (66, X15)

A prominent feature of the display on this stand is the wide range of Stentorian high-fidelity equipment. This includes loudspeakers available to suit a wide variety of requirements in cone construction, magnet strength, speech-coil impedance and size (from

13 to 18 in in diameter), loudspeaker enclosures (including the "Breakdown " range for home constructors) and matching equipment cabinets, stereo and single-channel amplifiers and an f.m. tuner. Some loudspeaker cabinets will be shown with Perspex fronts so that their internal construction can be examined. A recently-introduced compact bass"reflex loudspeaker system is the "Clumber".

Also displayed are industrial sound reproducing equipment, and ranges of transformers and chokes.

Whiteley Electrical Radio Co., Ltd., Radio Works, Victoria Street, Mansfield, Notts.

WIRELESS FOR THE BEDRIDDEN (60) Space for the stand of the "Wireless for the Bedridden" Society, which exists to provide free radio facilities to needy bedridden, housebound and aged invalids, has been given by the exhibition organizers. The Society has so far provided and maintains over 8,000 receivers and relay facilities and it is now also providing television receivers to Voluntary Old Peoples' Homes, etc.
"Wireless for the Bedridden" Society, 20 Wimpole Street, London, W.1.

WOLSEY (37)
The wide range of radio and television aerials and accessories on show includes several new aerials of improved performance and a new pre-assembled lashing bracket of very strong construction.

A new "in-the-room" television aerial, called the Hermes, is designed to give increased " gain "so increasing the range at which this type of aerial can be used.

Communal-aerial and relay network equipment and accessories are on show.

Wolsey Electionics Ltd., Cray Avenue, St. Mary Cray, Orpington, Kent.

ZONAL (404)
This company is showing the Zonatape range of standard and longplaying magnetic recording tapes, a feature of which is the incorporation of a coating lubricant for reducing head wear. Bases used in this range are diacetate, p.v.c., or polyester. Also displayed is the Zonastripe range of magnetically-striped films. A fluid which toughens film by replacing the moisture in the emulsion by organic compounds-Permafilm-is also exhibited.

Zonal Film (Magnetic Coatings) Ltd., The Tower, Hammersmith Broadway, London, W.6.

## JAPANESE VIDEO RECORDER

TELEVISION picture recording on tape, until recently, scemed to have stabilized on the system developed by Ampex. However, a different approach on the part of workers at the Tokyo Shibaura Electric Company Ltd. has resulted in the appearance of another system, which was described recently* in the Journal of the Society of Motion Picture and Television Engineers.

The Toshiba system uses only a single head rotating in a cylindrical guide drum round which the tape is wrapped, forming one turn of a helix (Fig. 1). Thus rotation of the head with the tape stationary will result in a track being drawn out by the head, slantwise from one edge of the tape to the other, at an angle of about $4^{\circ}$ to the edge of the tape (Fig. 2). This track is 26.5 inches long by just under one-hundredth of an inch wide and contains one whole field (frame) of the picture starting and finishing in the sync period: the effective tape-speed past the head is consequently about $1,600 \mathrm{in}$ / sec and the head-disk speed is $3,600 \mathrm{r} . \mathrm{p} . \mathrm{m}$.

To synchronize the sweep of the head with a track


Fig. I. Simplified diagram of tape-transport and (inset) head arrangements. Tape wraps round cylindrical guide containing rotating head disk so that head crosses between start and finish of spiral where top and bottom edges of tape are adjacent. (Based on diagrams in the original paper.)
on the tape, a position-indicating pulse is produced from the head drive by the passage past a coil of a piece of magnetic material on the spindle. This pulse is "compared" with the field sync pulse and the error signal is used to control the angular position of the head disk, which is driven from a supply derived from the sync pulses. On playback, the field-sync pulses from the head are fed into the phase comparator. Naturally, "cleaning-up" of the sync pulses is carried out and this removes noise generated during the short period when the head is crossing the slight gap between the two tape edges. Compressed air is blown through holes in the cylinder to reduce tape wear.

So far, no mention has been made of reel-to-reel, or lateral, tape speed-in fact, for a still picture it is not necessary to move the tape. As described above, the recorder can record one field and then reproduce it until the tape wears out. The normal tape speed is $15 \mathrm{in} / \mathrm{sec}$; but this obviously can be varied to give "slow-" or "fast-motion" effects and, most conveni-

[^1]

Fig. 2. Layout of tracks on tape. Measurements given are approximate and, for clarity, only two scans of the rotating video head are shown. (Based on diagrams in the original paper.)
ently, the tape can be kept stationary for editing purposes.

Other important advantages are that, as a "picture" is complete in one track, scalloping of vertical lines cannot occur; head switching is not required, thus there is no danger of switching transients imposing themselves on the picture and the replaying of registered colour signals is made easier.

The sound channel and a control track are recorded directly in the usual way along the edges of the tape with the head gaps at right angles to the tape motion. Now on the tape at these points is a part of the video signal; but, because the heads are not in line with the video tracks and an f.m.-carrier system is used for the picture, no mutual interference is apparent. The a.f. signal-to-noise ratio on the prototype machine was given as 45 dB -in the region of that which one would expect from an ordinary professional machine-and this has since been improved slightly.

## Tape Recorder "Replacements"?

NOT the least of the problems confronting the longsuffering tape recorder service engineer is the number of foreign bodies which find their way into machines, often deliberately introduced as "replacements". Some "museum pieces" which have been extracted from Grundig tape recorders returned to them for further service are, reading from left to right in the photograph, screw fitted in place of a fuse, fuse with a rating one hundred times too high, two gadgets for connecting knobs to their spindles, record and erase heads worn right through to the plastic behind, two broken belts mended with thread and, in the second row, the charred remains of a family of cockroaches and three improvised drive belts, the first of unknown origin, the second a bottle closure and the third from a vacuum cleaner.


By A. T. FERGUSON*

## INSTRUCTIONAL RADIO RECEIVER

WHEN a particular task has to be performed it is done with the tools available but if the task has to be done many times it is often worth while to produce a new tool or instrument that will make the work easier. The subject of this article is a radio receiver that has been designed to help with the training of apprentices who are studying for the Radio Trades Examination Board examinations in radio and television servicing.

The need for a receiver of this type became apparent when preparatory work for practical sessions of a training course was considered in detail. During a practical instruction period, two and a half or three hours, the student has to locate and clear faults on a receiver and it is obviously desirable that he should work by himself and not in a group of two or three persons. In this way he will get the maximum amount of practice and, through this, confidence in his work. However, even if there are classes of only fifteen students, each with his own receiver, there would be a considerable amount of time occupied in placing two or three faults on each receiver. The situation becomes more complex if these receivers are required for a different group of students the next day, which is quite likely if there are part-time day classes and evening classes being held for the same year of a course. It is not unreasonable to expect that any one radio receiver may have ten different faults put on and removed in any one week. A way of reducing the amount of preparation has been introduced into the practical examination itself; this method consists of putting one fault on a receiver and making the students diagnose the trouble, in turn and in a given time. This is a helpful idea and it gives practice in fault diagnosis; it does not however, give the student the satisfaction of clearing a fault after he has located it. The new R.T.E.B. practical examination may use fault simulator cards and this, perhaps, makes it more important than ever to see that students receive adequate time training on actual equipment. The cards are a clever and

[^2]useful substitute when equipment is not readily available but it should be the aim of training establishments to provide equipment first.

The circuit diagram, Fig. 1, illustrates the type of the receiver. The medium frequency broadcast band only is covered. With the exception of the valves and loudspeaker all the components are readily available from two well-known suppliers; the chassis, tuning condenser, reduction drive coils from one and the remainder of the components from the other. Additionally, mild steel strip is required for the chassis brackets and plywood and perforated metal for the speaker. The total cost of all the parts for each receiver can be kept to about $£ 8$. The use of separate loudspeakers and power supplies was considered and rejected; although satisfactory for some equipment the idea was not considered practicable from the point of view of handling, storing and issue. As far as possible each component has been mounted between a separate pair of tags, which have slots, rather than holes, and the connecting wires of the components are touched in with solder without being wrapped around the tag; this enables components to be replaced in a matter of seconds. Criticism about this method of fastening components could be made but this is a receiver for training and its utility would be greatly impaired if connections were made in the usual fashion. Separate instruction in soldering methods ensures that the student has a proper knowledge of the correct way to wire in components. The connecting leads from tag to tag are fastened by wrapping and soldering in the usual fashion.

Little difficulty was experienced with the construction of the receivers. Additional capacitors, 56 pf , had to be added to the intermediate frequency transformers to tune them to $470 \mathrm{kc} / \mathrm{s}$, and these are mounted inside the screening cans. A tendency to "motorboat" with maximum volume was removed by inserting a little fixed resistance into the tone control circuit. The values of capacity associated with the output stage were selected by considering the performance with the type of output transformer


Fig. 1. Circuit diagram of the receiver and component layout

Bottom view of the chassis. Ease of access and component replacement is evident.

used. The leads to the voiume control are screened. A cardboard washer should be inserted between the perforated zinc speaker fret and the wooden mounting to prevent vibration of the metal.

In practice the application of these receivers has more than justified the small amount of time taken to design and construct them; they are ideal for demonstration purposes on account of the accessibility of every component and the ease with which its value may be altered; many basic experiments can be performed with them. All essential voltages can be measured with a $0-250 \mathrm{~V}$, single range D.C. instrument without there being any risk of damage to either the meter or the receiver. The accuracy of the readings is sufficient on a single range meter if it has, at least, a two and a half inch scale.

Faults are put on the receiver by replacing a good component with a defective one which blends with its surroundings and looks normal. The student has to locate this, replace the defective component and then check the performance of the receiver. The provision of defective components requires a considerable amount of effort; various manufacturers have been asked if they could supply dummy or defective parts but their polite and understandable reply was to the effect that it is not in their nature to produce such articles. One firm that produces resistors has, however, been kind enough to supply unmarked resistors; these are painted to indicate the value of the resistor which they will represent in the circuit. Painting the colour code on by hand needs a little practice at first, thereafter it can be done quickly and expertly:' Small tins of enamel paint, such as those obtainable from handicraft centres, are used. The supply of open circuit dummy capacitors is the most difficult to provide; the markings on the dummy must be identical with those of the original, otherwise the student will quickly see the fault without having to test for it. An estimate of the number of students training for the R.T.E.B. examinations is about ten thousand and as each of these will require dummy components in the course of their training, perhaps some far-sighted organization will see its way to provide for the demand; this does not, of course, rule out the R.T.E.B.

The circuit diagram of the receiver should be duplicated on foolscap paper and then pasted on to pieces of thin hardboard cut to a size just smaller than the foolscap, the paper projecting at each edge. After drying the edges are sandpapered off. The surface of the paper is then given two coats of cellulose paste to seal it and, after drying, two coats of transparent lacquer. Diagrams protected in this way will be serviceable for many years and are immune from the effect produced by the momentary application of a hot soldering iron.

## Commercial Literature

Pencil Tubes-valves designed to provide low capacitances, low inductances and close element spacings-made by RCA are suitable for efficient u.h.f. use. A coaxial electrode construction is employed and most types are little bigger than the familiar $B 7 G$ miniature valves. Further details from (in U.K.) RCA Great Britain, Ltd., Lincoln Way, Windmill Road, Sunbury-on-Thames, Middlesex, or Radio Corporation of America, Electron Tube Division, Harrison, N.J., U.S.A.

Toroidal Suppression Inductors, as their leakage field is very small, offer valuable advantages in closely packed equipment or near sensitive apparatus. Technical Data Sheet MM/ 102 from Standard Telephones and Cables Ltd., Connaught House, Aldwych, London, W.C.2.
Communal Aerial equipment for up to 40 outlet points is described in Rainbow Radio's "Major Dumec" leaflet. Four-stage amplifiers are used for Band-I and -III TV and f.m., each with separate gain control. Rainbow Radio (Blackburn) Ltd., Mincing Lane, Blackburn, Lancs.
$110^{\circ}$ C.r.t. Deflection techniques are described by B. Eastwood in a reprint of his Television Society paper. In the reprint deflector-coil, line-output stage and frame timebase design are considered: copies may be obtained from Associated Electrical Industries Ltd., Radio and Electronic Components Division, 155 Charing Cross Road, London, W.C.2.
Instruments made by Dawe Instruments Ltd., Harlequin Avenue, Great West Road, Brentford, Middlesex, and marketed in France by Promesur, 19 rue Eugene Carriere, Paris 18 e , are described in French in an abridged catalogue.
Attenuators suitable for motor drive or manual operation are dealt with in a leaflet from Hatield Instruments Ltd., Burrington Way, Plymouth, Devon. Maximum frequency is $500 \mathrm{Mc} / \mathrm{s}$ in power ratings of 0.5 and 5.0 W : 50 - and $75-\Omega$ types are available in 1 and 10 dB steps.

# Single-Transistor Receivers 

SOME CIRCUITS FOR USE WITH HEADPHONES

By S. W. AMOS* B.Sc.(Hons.), A.M.I.E.E.

THE advent of transistors has made possible the construction of small receivers with low power requirements. For example a multi-transistor a.m. receiver driving a miniature loudspeaker and operating from a 9 -volt battery can fit into a jacket pocket. Several designs for home-constructed superheterodyne receivers of this type have appeared in the technical press.

Not so much attention has, however, been paid to much simpler receivers employing a single transistor and intended to drive headphones. Such a receiver can give excellent reception of a number of medium-wave signals and can be constructed very simply. Moreover, its power requirements are so modest that battery life is more easily expressed in years than in months. The construction of such a receiver provides excellent practice for those seeking experience with transistors and associated circuitry. For example such a receiver is well within the abilities of a teen-age schoolboy to construct and the performance of the finished receiver is quite satisfying. Moreover, if the receiver stimulates enthusiasm, an a.f. stage can be added to make loudspeaker operation possible and later an r.f. stage can be added to improve sensitivity and selectivity.

This article is, however, confined to singletransistor receivers and suggests a number of circuits which can be used, itemising their advantages and disadvantages. Perhaps the most obvious method of using a transistor in a receiver is to employ it as an a.f. amplifier, following a diode detector. A suitable circuit is given in Fig. 1. $\mathrm{R}_{1}$ is the diode
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Fig. I. Circuit employing a diode detector followed by a singletransistor a.f. amplifier.
load and the a.f. signal developed across this is amplified by the transistor. $\mathrm{C}_{1}$ is a d.c.-blocking capacitor and $R_{2}$ provides base bias current for TR1. The headphones may have an impedance of, say, 10 kilohm and the conditions in the collector circuit of TR1 should be adjusted for an optimum load of this value. For example, if the collector supply voltage is 4.5 volts, then the collector current should be $4.5 / 10,000 \mathrm{~A}$, i.e. 0.45 mA . A collector current swing of 0.45 mA is then accompanied by a voltage swing of 4.5 volts and the transistor characteristics are used to maximum efficiency. If the $\alpha^{\prime}$ (sometimes called $\beta$ ) of the transistor is 50 , the quiescent base current will be $0.45 / 50$, i.e. 0.009 mA . The base potential of a transistor is very nearly equal to the emitter potential and the voltage across $R_{2}$ is thus 4.5 giving the required value of $\mathrm{R}_{2}$ as $4.5 /\left(9 \times 10^{-6}\right)$, i.e. 0.5 megohm. As the $\alpha^{\prime}$ of the transistor used is not likely to be known with accuracy it is best to adjust the value of $\mathrm{R}_{2}$ empirically to give the required 0.45 mA collector current.

Purists may object to the simple biasing circuit advocated for the transistor on the grounds that it provides no protection against thermal runaway. If, however, the d.c. resistance of the headphones is 4,000 ohms (as is common), then the collector current cannot appreciably exceed 1 mA under any conditions. However, if a more stable operating condition is required, it can be obtained by biasing the transistor by the potential-divider method described later.

Such a receiver has the advantage that TR1 can be an a.f. transistor but there are the following disadvantages:

1. The diode detector cannot operate under good conditions. The input resistance of the a.f. stage is of the order of 2 kilohm and this puts an upper limit on the value of $\mathbf{R}_{1}$. To minimise peak clipping $R_{1}$ should be small compared with the input resistance but such a low value would lead to inefficient detection and to very heavy damping of the tuned circuit. With a value of $\mathrm{R}_{1}$ of 4.7 kilohm, as suggested in the circuit diagram, diode damping is still high and the diode should be tapped down the tuned circuit as shown to provide adequate selectivity.
2. A good aerial is essential to provide good results and an earth connection is also desirable.
A natural development of the diode plus triode circuit is to eliminate the diode and to use the base-emitter junction of an r.f. transistor for detection. This leads to a circuit of the type shown in Fig. 2, which could be described as that of a leaky grid transistor detector. The performance of this detector is unsatisfactory in practice and it is instruc-


Fig. 2. Circuit of a leaky-grid transistor detector deduced by analogy with its valve counterpart : the performance is unsatisfactory.
tive to consider the reasons. In a valve leaky-grid detector the grid-cathode structure operates as a diode and a negative potential, proportional to the carrier amplitude, is developed on the grid. The valve is required to operate as an audio amplifier and for this purpose a negative grid bias voltage is required. The value of this bias is not critical because the a.f. signal generated on the grid is normally small compared with the grid base. Thus the detector can function well in spite of variations in input-signal amplitude.

Now consider the performance of a transistor as a leaky-grid detector. As a result of detection in the base-emitter junction, the base is driven positive to an extent proportional to the input carrier amplitude. A transistor, however, does not require a positive base bias. As shown in Fig. 3(b) a pnp transistor is cut off by a positive base-emitter voltage: for satisfactory operation a negative baseemitter voltage is required. Thus leaky-grid operation is not satisfactory with transistors. Nevertheless the circuit illustrated in Fig. 2 does produce results although admittedly not very good ones. Moreover, the collector current of the transistor behaves in an unexpected manner when a signal is tuned in. For a leaky-grid detector the anode or collector current should fall on receipt of a signal: in Fig. 2 the current increases! The reason for this is not difficult to explain. An increase in current is a characteristic of an anode-bend detector and it is clear from Fig. 3(b) that the $I_{c}-V_{b}$ curve for a transistor inevitably gives rise to this type of detection. Thus in the circuit of Fig. 2 leakygrid and anode-bend detection occur simultaneously and as one mode of action tends to increase the collector current and the other tends to decrease it, the poor performance is not surprising. Examination of the transistor characteristic in Fig. 3(b) shows that it has no linear portion comparable with that of a valve. The transistor curve is, in fact, closely exponential in form and anode-bend detection therefore occurs at any point on the characteristic. If the transistor is forward-biased, the efficiency of anode-bend detection is increased and a suitable circuit for a detector working on these principles is illustrated in Fig. 4. This gives results comparable with those obtainable from the circuit of Fig. 1 but the anode-bend circuit is
simpler and does not require a diode: moreover the anode-bend circuit lends itself very simply to the application of reaction and this produces a great improvement in performance. On the other hand the anode-bend circuit does require the use of an r.f. type of transistor and this should preferably be of the type recommended for use as frequency changer in super-heterodyne a.m. receivers.

In the circuit of Fig. 4 the collector current is stabilised against thermal runaway by the potential divider method. $\mathrm{R}_{1}$ and $\mathrm{R}_{2}$ form a potential divider which applies a negative potential, say 1 volt, to the base of the transistor. There is normally very little difference in the potentials on base and emitter of a transistor and the emitter also takes up a potential of -1 volt. Thus a potential difference of 1 volt is established across the emitter resistor $R_{3}$. By choosing the value of $\mathrm{R}_{3}$ appropriately we can make the emitter current almost any desired value: for example if $\mathrm{R}_{3}$ is made 1 kilohm, the emitter current is 1 mA . Morcover the emitter current-and hence the collector current-remain at the determined values in spite of variations in collector leakage current due to temperature changes. To avoid loss of amplification as a result of negative feedback $\mathrm{R}_{3}$ must be decoupled and a large-value electrolytic capacitor is connected across $\mathrm{R}_{3}$.

One refinement-and a most valuable one-can be added to the circuit of Fig. 4. This is reaction or controlled positive feedback and is achieved by returning r.f. energy from the collector to the base circuit. This improves sensitivity and selectivity



Fig. 3. Input voltage-output current characteristic of (a) a valve and (b) a transistor.


Fig. 4. Basic circuit for an anode-bend transistor detector.


Fig. 5. Circuit for complete receiver using the detector of Fig. 4 with reaction.


Fig. 6. Improved version of the circuit of Fig. 5 with better control of reaction.
considerably. Many of the circuits advocated for reaction require an additional coil coupled to the tuning inductor or tappings on the tuning inductor but it is possible to avoid both by using a circuit based on that of the Colpitts oscillator and described by the author* some years ago. A detector circuit using an anode-bend detector and reaction of this type is illustrated in Fig. 5. The equivalent of a tapping point on the tuning inductor is achieved by use of the two capacitors $C_{1}$ and $C_{2}$ connected in series across it. The transistor is connected across $C_{1}$, the larger capacitor, and reaction is obtained by use of the variable capacitor $\mathrm{C}_{3}$ connected between the collector

[^3]and the high-potential end of the inductor. For an OC44 transistor a suitable value of collector current is 0.6 mA and the values of $\mathrm{R}_{1}, \mathrm{R}_{2}, \mathrm{R}_{3}$ and battery voltage given in the diagram give approximately this value of current.

The effective maximum tuning capacitance in parallel with the tuning inductor is less than 500 pF and if a standard medium-wave inductor of approximately $160 \mu \mathrm{H}$ is used, there is some curtailment at the low-frequency end of the band, the minimum frequency receivable being about $600 \mathrm{kc} / \mathrm{s}$ (500 metres). For many applications this reduced coverage may not matter but if it is desired to tune to 550 $\mathrm{kc} / \mathrm{s}$ an inductor of $200 \mu \mathrm{H}$ is required. A number of commercial medium-wave inductors have adjustable magnetic cores which enable this value of inductance to be reached: one suitable coil is Teletron type BA2.

Satisfactory results can be achieved using an aerial consisting of a few feet of vertical wire connected to the high-potential end of the tuning inductor as shown in Fig. 5. An earth connection, though helpful, is not essential. Naturally results are better if a longer aerial is used: such an aerial is better connected to the low-potential end of the tuning inductor or alternatively can be connected to the high-potential end via a small fixed capacitor of say 20 pF capacitance.

The tuning inductor can be replaced by a winding on a ferrite rod, and, in fact, a standardf errite-rod aerial (for use with a tuning capacitor of $500-\mathrm{pF}$ maximum capacitance) can be employed with some restriction in coverage at the low-frequency end of the band. By increasing the number of turns on the ferrite rod it is, of course, possible to achieve complete medium-wave coverage. However, the receiver is not so sensitive with a ferrite rod aerial as with a vertical aerial.

One slight disadvantage of the circuit of Fig. 5 is that adjustment of the reaction capacitor $\mathrm{C}_{3}$ causes slight mistuning. This arises because $\mathrm{C}_{3}$ is effectively in parallel with the tuning capacitor $\mathrm{C}_{2}$. the mistuning is hence most marked at low settings of $\mathrm{C}_{2}$, i.e. at the high-frequency end of the band. This causes difficulty in tuning particularly for a weak signal which requires a considerable degree of reaction, but it is of little consequence if the receiver is used only to receive strong signals. The mistuning effect can be virtually eliminated by using a fixed capacitor for $\mathrm{C}_{3}$ and by controlling reaction by adjustment of the mutual conductance of the transistor. The mutual conductance is measured by the slope of the $I_{c}-V_{b}$ characteristic and the exponential slope of this curve illustrated in Fig. 3(b) shows that the conductance is proportional to the collector current. Thus by adjusting the collector current we can control the conductance. A convenient way of doing this is to make the emitter resistor variable as shown in Fig. 6. A 470 -ohm fixed resistor is included to give an upper limiting value of approximately 1.2 mA to the collector current and a 3 -kilohm variable resistor is included to enable the current to be reduced to about 0.25 mA . This arrangement gives smooth control of reaction with very little disturbance of tuning.

The values of $C_{3}$ and $C_{5}$ given on Fig. 6 give good control over reaction over the whole of the medium waveband for the particular specimen of OC44 used by the author-and the transistor was not specially
(Continued on page 479)
selected. Other OC44s may have higher or lower values of $\alpha^{\prime}$ and alpha cut-off frequency: thus reaction may be too fierce or too weak. If control of reaction is not satisfactory, it may be desirable to depart from the values of $\mathrm{C}_{3}$ and $\mathrm{C}_{5}$ specified.

This receiver can be used to cover the long waveband by using a suitably-large tuning inductor for $L_{1}$ and one advantage of the circuit is that this is the only change necessary: $\mathrm{C}_{1}$ and $\mathrm{C}_{2}$ ensure that reaction is available on the new waveband. If, however, the receiver is required to operate on the short wavebands, then a number of changes are advisable:

1. Firstly a different type of transistor is necessary,
for the OC44 is not intended to operate at such high frequencies. A transistor such as the OC170 is suitable for use on short waves and, of course, this transistor is quite satisfactory at medium and long waves also.
2. It is desirable to reduce the values of $C_{1}$ and $C_{2}$ for use in a short wave receiver in order to keep a high dynamic resistance. Some experimenting with the ratio of $C_{1}$ and $C_{2}$ might be desirable to obtain smooth control of reaction.
3. The tuning inductor should be chosen, in conjunction with the net capacitance of $C_{1}$ and $C_{2}$ to tune over the frequency band required.

# Low-voltage Stabilizer Using Semiconductors 

By D. E. O'N. WADDINGTON*, Grad.Brit.I.R.E. and M. R. AINLEY*, b.Sc., Grad.i.e.e.

WITH the advent of transistorized equipment, the need for stabilized low-voltage power supplies has become very apparent. This is so because batteries, the most obvious power source, are not stable over their useful life and it is thus necessary to check equipment designed for battery operation over the range of voltages likely to be encountered under operational conditions. A further case in which a stabilized supply is essential is where the equipment will not function efficiently unless fed from a constant-voltage source.

## Definition of Characteristics

Before discussing stabilizers it is necessary to define certain characteristics of power supplies. The first consideration is the stabilization characteristic or stabilization factor which may be defined as the ratio between the percentage change in input voltage and the corresponding percentage change in output voltage. Thus a supply having a stabilization factor of 50 will produce a $0.4 \%$ change in output voltage for a $20 \%$ change in supply voltage. The other consideration is the load characteristic or the incremental slope resistance of the supply and this may be defined as the ratio between the change in output voltage and the corresponding change in load current. By having a knowledge of these two factors together with the output voltage and current,


Fig. 1. Simple semiconductor stabilizer using Zener diode.
it is possible to assess whether a circu t is suitable for the application envisaged.

The simplest shunt stabilizer for low-voltage work is, of course, the Zener diode in Fig. 1. Its advantages are that it is compact, efficient and easy
*Murconi Insiruments, Lid


Fig. 2. Stabilizer performance is improved and powerhandling capacity raised by transistor fed from Zenerdiode reference.


Fig. 3. Furller improvements in stabilization factor and incremental slope resistance are provided by errorsensing circuit and error-signal amplifier.


Fig. 4. Circuit incorporating provisions of Fig. 3. Note npn transistor (VI) error-sensing and amplifying stage.


Fig. 5. Emitter follower (V5) isolates VI from loading of V4 and resistor $R_{4}$ feeds Zener diode from stabilized supply to improve stabilization factor.
to use. However it has several shortcomings which make it unsuitable for use in many applications. Not the least of these is the fact that the output voltage is fixed by the diode's characteristics, with the result that the user wishing to change the output voltage can only do so by replacing the diode with another one having the desired voltage rating. The designing of supplies using Zener diodes tas been well covered (see, for instance, Ref. 1). The follow-


Fig. 6. Variation of temperature coefficient of Zener diodes against Zener-voltage rating.
ing are typical figures measured on supplies tested in the laboratory:-

Stabilization Factor 20-40.
Incremental Slope Resistance $1 \Omega-20 \Omega$ (depending on diode used).
In order to improve the incremental slope resistance and the power handling capacity of the stabilized supply a transistor may be added to the circuit as shown in Fig. 2. Here the diode acts as a reference source which keeps the base at a constant potential with respect to the collector. As the emitter-to-base voltage is of the order of 0.15 V and relatively independent of the current through the transistor, the voltage between the collector and emitter of the transistor will remain constant. This circuit produces little or no improvement in the stabilization factor but the incremental slope resistance is improved. In a practical circuit this is of the order of 0.6@. Like the straight-forward Zener diode circuit, this type of stabilizer does not give an easily adjustable output voltage.

## Use of Error-sensing Circuit

Further improvements in the stabilization factor and incremental slope resistance can be made by


Fig. 7. Circuit arranged to overcome temperature variation problems. VI and V2 form " longtailed pair "' error-sensing circuit ond Zener diode of zero temperature coefficient is used.


Left. Fig. 8. Circuit of final stabilizer design. Here temperature coefficients of sensing transistor and Zener diode are equal but of opposite sign. so minimizing temperature effects.
building a stabilizer of the form shown in Fig. 3. In this an error-sensing device compares the output voltage with the reference voltage. The "error" is then amplified and applied to the shunt transistor in such a sense as to reduce the error. A circuit in which this is done is shown in Fig. 4. The n -p-n transistor V1 acts as the error-sensing device as it compares the voltage at the junction of $R_{1}$ and $R_{2}$ with the reference voltage developed across the Zencr diode connected in serics with the transistor's emitter. The values of $\mathrm{R}_{1}$ and $\mathrm{R}_{2}$ will be chosen such that

$$
v_{\text {rei }}=v_{\text {out }} \times \frac{\mathrm{R}_{2}}{\mathrm{R}_{1}+\mathrm{R}_{2}}-v_{\text {ve }}
$$

Thus any reduction of the output voltage will appear as an error voltage at the base of V1: this will reduce the current flowing through the resistor $\mathrm{R}_{3}$ and hence increase the voltage at the base of V 4 , so increasing the output voltage. An increase in the output voltage will have the reverse effect. Thus it is seen that this feedback system has had the effect of reducing the incremental slope resistance considerably.
As the circuit stands it still has two main disadvantages. The first lies in the fact that, as the load current is decreased, the current through V4 increases thus increasing its base current and hence the loading on V1. In order to overcome this, an emitter follower is included between V1 and V4 (see Fig. 5). So far no action has been taken about improving the stabilization factor of the supply but we now include the resistor $\mathrm{R}_{\text {}}$. This provides the main feed for the Zener diode from a stabilized source which improves the stabilization factor two or three times.

## Temperature Changes

Up to now we have regarded the Zener diode as a reference element whose characteristics do not change with temperature. In practice, however, we find

Right. Fig. $9(a)$. Change in output voltage ( $m V$ ) plotted against load current for stabilizer shown in Fig. 8. (b) Change of output voltage ( $m V$ ) plotted against change in input voltage, expressed as a percentage, for the same stabilizer. (c) Effect of temperature variation.

(a)


that the diode voltage changes with temperature and that the temperature coefficient is a function of the voltage rating of the diode (see Fig. 6). The effect of this variation will be to make the output voltage change with temperature variations. The temperature problem is further aggravated by the fact that the base-to-emitter voltage of a germanium transistor reduces at the rate of approximately $2 \mathrm{mV} /{ }^{\circ} \mathrm{C}$.

There are two ways of reducing these errors. The first is to make the circuit more complicated (see Fig. 7) and use a balanced system for the error-sensing device. The effect of this is to make changes in the emitter-to-base potentials of V1 and V2 cancel each other out. Temperature stability is then achieved by using a zero-temperature-coefficient Zener diode which may be either a single diode or two diodes with opposing temperature coefficients connected in series.

The second method of overcoming the temperature drift is to make use of a Zener diode which has a temperature coefficient which exactly cancels the temperature effects in the base-to-emitter voltage of the error-sensing transistor, i.e., to use a Zener diode whose reference voltage increases at a rate of $2 \mathrm{mV} /{ }^{\circ} \mathrm{C}$. Examination of the characteristics of Zener diodes shows that diodes having a voltage of approximately 6.2 volts satisfy this requirement. As a result the practical circuit shown in Fig. 8 was evolved. The graphs of Fig. 9 show the performance characteristics of this circuit.

## Practical Details

It will be seen that the practical circuit includes three extra components which have not been discussed so far. Their functions are as follows: $\mathrm{C}_{1}$ is included to prevent the circuit from oscillating at high frequencies, a trouble which often occurs in volttage stabilizers. $\mathrm{C}_{2}$ increases the a.c. feedback in the circuit with the result that any ripple on the supply is reduced by the stabilizer action. The function of the variable resistor $R V_{1}$ is to enable the user to set the output voltage to the required level. This
is necessary because there is nearly always a tolerance of $5 \%$ on the actual voltage of the Zener diode.

In a practical stabilizer circuit it may be necessary to provide some form of cooling for the shunt transistor so that it is not damaged by over-heating. The dimensions of the heat sink required will depend on the power dissipated in the transistor ${ }^{2}$, the ratings of the transistor and the maximum ambient temperature in which the supply is to be operated. In the circuit shown the power dissipated in the transistor under " off-load" conditions is of the order of 5 W . From the manufacturer's information it may be shown that, in this case, it is not essential to mount the transistor on a heat sink for the normal range of ambient temperatures. However, it is both convenient and desirable to mount the transistor on a rigid metal bracket.

The $24-V$ supply for the stabilizer may readily be obtained from a centre-tapped transformer having a secondary rating of $20-0-20 \mathrm{~V}$ r.m.s. feeding two semiconductor diodes in push-pull (bi-phase or "full-wave" circuit). Smoothing is conveniently provided by a single capacitor $(1,000 \mu \mathrm{~F}, 50 \mathrm{~V}$ working) connected across the output.

Readers may wonder why the authors have chosen the shunt regulator in preference to the series regulator. Much thought was given to this decision before work was started and they came to the conclusion that it must be possible to short circuit the supply without damaging the circuit. If a series regulator had been used some form of protection device would, of necessity, have had to be included; but with a shunt stabilizer, the series resistor $\mathrm{R}_{8}$ may be rated to withstand the dissipation when the output is subjected to a short circuit.

## References

I "Stabilization by Zener Diodes," by J. Pereli; Wireless World, p. 537, vol. 64 (November, 1958).
2 "Heat Sink Design," by O. J. Edwards; Mullard Technical Communications, p. 258, vol. 3, No. 29 (March, 1958).

SHORT-WAVE CONDITIONS


Prediction for September


THE full-line curves indicate the highest frequencies likely to be usable at any time of the day or night for reliable communications over four long-distance paths from this country during September.
Broken-line curves gives the highest frequencies that will sustain a partial service througheat the same period.
***** FREQUENCY BELOW WHICH COMMUNICATION SHOULO BE POSSIBLE FOR $25 \%$ OF THE TOTAL TIME

-     - PREDICTED MEDIAN STANDARD MAXIMUM USABLE FREQUENCY
—— FREQUENCY BELOW WHICH COMMUNICATION SHOULD BE POSSIBLE ON ALL UNDISTURBED DAYS


## ELECTRONIC MUSIC

By F. C. JUDD

## SOUND SOURCES AND TREATMENT

THE methods of producing Electronic Music an 1 its closely allied Musique Concrête are similar, it is only the source of the sound which differs. In purely Electronic Music almost all the sounds are obtained from tone generators used in conjunction with electronic circuits. In Musique Concrête the sounds are derived mainly from those picked up by a microphone; sounds such as machinery noise and bell chimes, or those produced by traditional musical instruments and the human voice. Composers can and do sometimes combine clectronically-produced tones with sounds picked up by a microphone. There is in fact no real dividing line between these


Fig. 1. Controlled attack by tape cutting.
two forms of new music. Electronic Music, sometimes called "Radiophonics", should not be confused with conventional music performed on "electronic" instruments such as the Hammond organ, or the Aetherophone developed by Leon Theremin.
Magnetic Tape Manipulation.-Magnetic tape provides the composer of Electronic Music and Musique Concrête with a foundation on which to present his work and is an aid to special forms of transformation that cannot be carried out electronically. For example, he can remove the portion of tape on which the "attack" of a sound is recorded. Sounds can also be given a new degree of attack (or decay) by cutting the tape at certain angles. For example a hard attack is produced by a straight cut as in Fig. la; a softer degree of attack can be produced by cutting at a steep angle as in Fig. 1b. This particular cutting technique is only practicable with full-track recording.

Other transformations are obtained by using different recording and playback speeds. This alters the pitch of a sound without changing the relative strength of its harmonics. Continuous variation of tape speed can produce unusual gliding-tone effects and allow the production of arpeggios with a pre-
cision quite beyond that of a human musician. The replay direction of magnetic tape can of course be reversed so that recorded sounds end on the attack.

By using additional replay hcads as shown in Fig. 2 , recorded signals can be returned to the tape via the recording amplifier for the production of artificial reverberation. Echoes and pre-echoes obtained by this method sound hard and somewhat unreal; their intensity can be controlled by means of volume controls in the return circuits.

Sound Sources and Treatment.-Of the electronic sound sources, the sinewave generator is most used because it provides the composer with pure tones covering a wide range of frequencies and with variable amplitude. Its lack of harmonics gives a sine wave a rather unearthly sound. With continuously variable control over frequency almost any desired scale can be used.
The multivibrator is a device familiar to electronic engineers and since it generates harmonics up to about the 31st, the tones have a rich sound when reproduced via a loudspeaker. Its output can of course be integrated or differentiated by simple R-C networks in order to produce still further varieties of tone colours.

The white noise generator is a source of sound which is distinctive because of its continuous spectrum. Owing to its constant energy distribution with frequency, its sound is, musically, somewhat uninteresting. Used in conjunction with filters, however, sounds with definable pitch can be produced.

There is also a rather mixed group of "electronic" sound sources which generate tones by electromechanical methods although these can only be reproduced electro-acoustically. Two sources belonging to this group were used by H. Badings in the production of his "Cain and Abel" electronic ballet music. These were the electronic drums and an electronic clavichord. In one of the drums the drum


Fig. 2. Method of obtaining artificial reverberation.


Fig. 3. H. Badings and J. W. De Bruyn operating the Optical Siren used in the production of electronic music for the "Cain and Abel", ballet. (Photograph by courtesy of N. V. Philips, Gloeilompenfabrieken, Eindhoven, Netherlands, Technical and Scientific Literature Department.)
diaphragm was simply used also as the diaphragm of a condenser microphone.

An equally unusual sound source used by Badings was a so called "Optical Siren" (Fig. 3). The tones produced by this apparatus depended on the speed of a slotted rotating plate which was used to scan a pattern of oscillations drawn on paper. The scan was translated into electrical oscillation by means of a light beam and photo-electric cell (Ref. 1).

A few conventional electronic circuits have also been adopted for the treatment of sounds used in electronic music. The ring modulator (Fig. 4) is commonly used, the difference tone which it provides being the favoured one for composers. When a tone and white noise are passed through a ring modulator "hard" sounds are produced which are also used by composers. The "gating" principle has been adopted and a circuit such as Fig. 5 provides a considerable degree of control over the attack and decay of signals fed into it. The circuit requires no critical adjustment and any medium-impedance triode valve will operate successfully. The diode can be a crystal type such as the GEX 34. Varying degrees of attack and decay can be produced by different settings of VR1 and VR2. A tone is only allowed through the gate when the key Sl is quickly closed and opened again. Various kinds of R-C and L-C filters are also used in conjunction with tone sources, or with the amplifiers associated with recording and re-recording processes, to eliminate harmonics to filter off unwanted sound.
The stereophonic effect is frequently used to simulate movement of sound in such a manner that a listener's acoustical impression is made to differ from any natural visual impression. This technique alone has contributed something new to the development of both electronic and traditional music and was used in Le Corbusier's Poéme Electronique at the 1958 Brussels Exhibition.

Various devices have been invented for electronic music creation and of these the "Phonogene" which was produced by Pierre Schaeffer and Jacques Paulin in 1951 is interesting. It employed a number of record/playback heads and could transpose the pitch
of sounds automatically in the chromatic scale. It was in fact coupled to a keyboard from which the pitch could be selected in the same way as notes on a pianoforte.
Electronic Music Composition.-The composer's equipment, his new orchestra, consists of audio sig-


Fig. 4. Ring modulotor (see Radio Engineering by E. K. Sandeman. Vol. I, p. 542 (Chapman \& Hall)).


Fig. 5. Gating Circuit for controlling attack and decay.


Fig. 6. Audio cquipmen, used by the writer for producing electronic music.
nal generators, tape recorders, loudspeakers and other electronic equipment (Fig. 6). From these he produces his music and determines each note by its pitch, duration and intensity. He no longer has only 70 to 80 different intervals, intensities from pianissimo to fortissimo, and time values in terms of crochets and quavers. The entire audio range of frequencies is at his disposal with possibly 60 controlled dynamic levels and an infinite range of duration values, which are measured in terms of centimetres of tape.

Composers of electronic music are well aware of the tremendous possibilities that these factors afford. They can think in terms of what they call "microstructures" which are exceedingly small differences in pitch, intensity and time, not possible with musical instruments. For example, between the note of A natural at $440 \mathrm{c} / \mathrm{s}$ and the next whole tone of $B$ natural at $492 \mathrm{c} / \mathrm{s}$ there are 50 other frequencies (441, $442,443 \mathrm{c} / \mathrm{s}$ and so on) which can be utilized. From these approximately every fourth step is an audible and therefore new interval.
The complex forms and range of electronically produced sounds cannot be notated as in a traditional music score and therefore have to be presented in the form of an "acoustical diagram" (Fig. 7). A score for electronic music is written in terms of frequency (cycles per second) intensity (measured in decibels) and time (centimetres of tape).
Although experiments with electrically produced music began almost with the invention of the radio valve, its full potentialities only became possible with the introduction of magnetic tape recording. Most of the earlier work with tape was carried out by Herbert Eimert and Karlheinz Stockhausen of the Cologne studios of the West German Radio. Electronic music studios have since been established in other European countries and in the U.S.A. In this country there is, of course, the B.B.C. Radiophonics workshop, but this is only available to composers by invitation.
A few "concerts" of electronic music have been given in the U.K. and in the United States there are "Vortex Music" concerts, most of which are broad-


Fig. 7. Opening of "Incontri di Fasce Sonore", a score for ejectronic music by Franco Evangelisti (by kind permission of Universal Edition).
cast over the radio networks. Recordings of electronic music, many of which originate from the European countries, are available in the U.K. (Ref. 6). Readers particularly interested in the æsthetics and composition of electronic music, or in the more practical application of the electronic elements, are referred to the two publications given as Refs. 2 and 3 respectively.

## References

${ }^{2}$ Electronic Music by H. Badings and J. W. de Bruyn, Philips Technical Review Vol. 19 (1957-58), No. 6 (issued with a 45 r.p.m. disc containing examples of Electronic Music).
${ }^{2}$ die Reihe-Electronic Music-by H. Eimert and K. Stockhausen, Universal Edition.

Electronic Music and Musique Concrête by F. C. Judd, A.Inst.E., to be published shortly by Neville Spearman Ltd.
${ }^{4}$ Musica ex Machina by F. K. Prieberg (survey of the studios of electronic music), Allstein Verlag.
${ }^{3}$ Scores of Electronic Music:-Essay by G. M. Koenig, Incontri di Fasce Sonore by Franco Evangelisti and Studie 2 by K. Stockhausen, all Universal Edition.

Records of Electronic Music:-LP16132-Introductory talk (in German) with examples and elementary composition by H. Eimert, LP16133-Pieces by K. Stockhausen, LP16134-Pieces by E. Krenek and G. M. Koenig (all Deutsche Grammophon), and Philips abel0073-Cain and Abel (electronic music for ballet) by H. Badings.

Pre-recorded Tapes of Electronic Music:-Bi-Tapes ATR134 (3 3 i.p.s.)-Power of Music by F. C. Judd (based on a poem by John Dryden) and Bi-Tapes ATR135 (33 i.p.s.)-Experiment in Sound by F. C. Judd, (contains examples of electronic music and demonstrates the techniques employed).
${ }^{8}$ Electronic Music Instruction:-Dartington Summer School of Music, Dartington Hall, Nr. Totnes, Devonshire and the Rose Bruford College of Speech and Drama, Lamorby Park, Sidcup, Kent.

# "COLOUR TELEVISION" 

TEXTBOOK OF PRINCIPLES AND PRACTICE APPLICABLE TO ALL LINE STANDARDS

FOR a long time in this country people have been talking about the system chosen by the America's National Television Systems Committee for colour television; but apart from widely scattered articles in the technical press and papers presented to learned institutions and societies, there has been no British reference book. However, Mr. Carnt and Mr. Townsend, in their book "Colour Television," have not only remedied this situation but they have done so in an eminently readable and interesting way.

The reader with a knowledge of television but no priming on colour will find little that is not explained clearly, whilst to the man already "in the field," whether by interest or profession, the book should be of immense value for the full treatment and as a ready reference source. To these ends the authors have introduced each chapter by exposing clearly the problem and explaining it in general terms; they then proceed to detailed analysis and the means for carrying out the desired function at the transmitter or receiver with practical illustrations from equipment of proven design.

After dealing with such principles of colour as are necessary to the understanding of colour TV, giving a brief résumé of various display methods and means of providing basic colour-television signals, the authors progress logically through the system. Chapters on transmitter encoding and specification of colours in the N.T.S.C. system are followed by consideration of receiver design, with particular emphasis on de-coding and reference-frequency generators. An example of the authors' complete treatment (which, incidentally, extends to 525 - and 625 -line systems as well as 405) is given by the chapters on test equipment, receiver installation and fault finding, whilst the last two chapters deal with monochrome reception of the colour signal and an analysis of the shortcomings of the N.T.S.C. system. They are, for instance, to be congratulated on explaining clearly why a positive-modulation, a.m.-sound television system is preferable to the negative-modulation f.m.sound type for the transmission of N.T.S.C. colour and also on their gathering together of mathematical treatment in appendices; thus the book can be read without the need for the immediate de-coding of mathematics! A comprehensive bibliography and index complete the book which has also 14 coloured photographs including "off-the-screen" pictures.
"Colour Television, The N.T.S.C. System, Principles and Practice," by P. S. Carnt, B.Sc. (Eng.), A.C.G.I., A.M.I.E.E., and G. B. Townsend, B.Sc., F.Inst.P., M.I.E.E., A.K.C., is published by Iliffe Books Ltd. for Wireless World and costs 85 s .

## Transistor Radar Simulator

RADAR simulators have not, in the past, been notable for their compactness-at least one 6 ft , 19 -in rack or its equivalent was used to house the equipment and often, for a complex installation, the space occupied was very much greater, and power consumption was such that fan-cooling was necessary.
Solartron, however, have produced a simulator which, for a six-target installation, takes up no more space than an ordinary office desk. The key to this reduction in size and power consumption, for each target unit consumes only 20W, is the use of transistors. Designed for easy servicing, all the plug-in printed-circuit boards are colour coded and fully labelled with test points and provision has been made for the addition of units to simulate all the "gadgets" available and effects seen on the most modern radars.


# Voltage or Current Operated? 

By "CATHODE RAY"

THERE has been a lot of discussion lately about how we should regard transistors. One question is whether any of the three basic circuit configurations is more fundamental than the others, and if so which. It seems to have been satisfactorily established that there can be no preference on purely theoretical grounds, but I am glad to be able to report general agreement on the proposition that for practical purposes there are advantages in regarding the common-emitter configuration as the normal one.

Being analogy-minded, and therefore inevitably looking on the transistor as a new kind of valve, I have never been able to think of any other as the normal; and that is why it makes me so cross that people allocated the primary transistor symbols$\alpha$, etc.-to the common-base configuration. They might have had some excuse in the short-lived era of the point-contact transistor, but no excuse whatsocver for persisting in the error to this day, thereby creating a wholly unnecessary difficulty and complication for every student of electronics, including generations yet unborn, unless those who made a false start on the common-base track exert the slight mental effort of getting on to the right one again. Oddly enough, I find it is the comparatively young engineers who are most apt to justify ill-conceived conventions by the plea that "it's too late to change", thereby showing themselves less progressive and mentally adaptable than their elders who altered the firmly-established "resistance" into "resistor" for the sake of terminological tidiness, even though it was less practically important than the basic transistor symbols.

And as for the crypto-Americans among us who persist in favouring what they call the "groundedbase" configuration (and even the true Britons who call it "earthed-base ") Fig. 1 should be sufficient comment.

But (to get back to the subject) I was referring to those who are busy announcing their discovery that a transistor is rather like a valve and should be taught as such. I am naturally among the most enthusiastic in welcoming them, belated though their conversion is. However, an occupational hazard of new converts is allowing enthusiasm to get the better of them. At least one of them ${ }^{1}$ might be thought to have done just that when he urged that it would be helpful to consider as the important parameters of the transistor the mutual conductance ( $g_{m}$ ) and the input admittance ( $y_{i n}$ ) and strongly challenged the common view that the transistor is current operated, in contrast to the valve, which is voltage operated. He argues that the situation is like that of a capacitor shunted by a resistor, in which the force between the plates is proportional to the current supplied but is not caused by that current. And about six years ago no less an authority than Dr. Shockley ${ }^{2}$ said " the [voltage] bias across

[^4]the emitter junction controls the electron flow into the base region. In effect, the emitter junction acts like the region between the cathode and grid in a vacuum tube."

The " common view" is expressed in a well known manual ${ }^{3}$ : "The base current ... is important because it controls the current in the emitter-collector circuit. A similar controlling function is exercised in the valve by the control-grid voltage."

So here is a contradiction: some say transistors are current operated; others, that they are voltage operated. Which are right?

The first thing is to decide what exactly is meant by "current operated" and "voltage operated".


Fig. 1. Here the base is earthed. So, with the most elementary and irrefutable logic. it could be called an earthed-base circuit. But would it not be disowned as such by those who use that term? Many who, for some reason that has never been satisfactorily explained, refer to "grounded-base" circuits, would in addition disown themselves as Americans, logical though that conclusion is. The only unconfusing term for this circuit is "common-emitter".

These descriptions were used long before transistors were thought of. So, like the lawyers when they want to settle the meanings of terms, we might look up the precedents.
When I first began to study electricity I was told that instruments for measuring current were wound with a few turns of thick wire, whereas instruments for measuring potential difference, called voltmeters, had a great many turns of fine wire. That seemed to be the only difference, and I was a good deal puzzled how it could be that instruments for measuring two fundamentally different quantities were identical in principle, differing only in degree. If one gradually varied the turns and gauge of wire, at what precise point did an ammeter turn into a voltmeter?

Such being the textbooks and lecturers of the period, it was left to me to work out for myself that the so-called voltmeters were really current meters, and that the voltage was deduced thereby from the current flowing through a known resistance. And that the only true voltmeter was the electrostatic variety.

[^5]But in common thought a moving-coil voltmeter responds to volts (the current taken by it being an unavoidable evil) and so may almost by definition be regarded as voltage operated, in contrast to ammeters and milliammeters which are current operated. The inquiring student appears pedantic for objecting that there is really no difference in principle.
The distinction, unscientific though it may be, is of even greater practical significance when we come to adapt our moving-coil instrument for a.c. The metal rectifiers used for the purpose vary widely in their resistance, both with the current flowing and the temperature and with the particular sample chosen. This being so, the rectifier resistance, or the voltage required to pass a given current through it, would be a most unpractical parameter to put first in instrument design. Certainly it is of some interest, to the extent that one wants it to be as little as possible, but its precise value is altogether unimportant. It wouldn't do at all to give a rectifiertype milliammeter higher ranges by shunting it, as one would a d.c. instrument, for the readings would then depend on the uncertain and variable rectifier resistance. Instead, one uses a current transformer.
So although the first cause in making the pointer move is undoubtedly the e.m.f. that drives current through the rectifier and meter coil, this voltage is only of minor concern to the meter designer, who for practical purposes regards the contraption as current operated. When he connects in series a sufficiently high known resistance to render the rectifier resistance negligible by comparison, then he has produced a voltmeter and only then do practical people describe it as voltage operated.

And so one might go on with relays, microphones, and many other devices. Whatever may be the first cause and whatever may be the direct cause of the perceived result, voltage operated devices are normally understood to be those having a relatively high input impedance and/or a simple relationship between result and input voltage; and correspondingly for current operated devices.

Let us now try, like a jury, to forget what every man in the street thinks he knows about the case and apply strictly judicial minds to it. In particular,
(a)

(d) a, [rom $\longrightarrow$
(b)



Fig. 2. Are these voltage operated or current operated, and why? (The coil and pointer denote a moving-coil meter.)
let us look more closely at the capacitor analogy, Fig. 2(a). To make the thing a little more practical, we can suppose the capacitor to be an electroscope or an electrostatic voltmeter, in which the force between the plates produces a visible result. Then of course we would all have to agree that this result was due to the potential difference between the plates. But might it not also be permissible to regard that p.d. in turn as due to the current through the shunt? The combination could, in fact, be scaled in milliamps. When we find a high pressure at the point where we connect the garden hose to the tap, may we not think of it as due to the current of water, in combination with the resistance of the hose? This seems to be a question of point of view rather than absolute right or wrong.
Example (b) shows a valve, in which the anode current is controlled by grid-to-cathode p.d., without appreciable current flow. This can hardly be described as other than voltage operated or controlled. Connecting a resistor between grid and cathode (c) creates essentially the same situation as in (a). Some may say it opens up a new branch circuit but makes no difference in principle to (b), others that this branch current controls the p.d. (depending on the resistance of the source) and thereby controls the anode current. Example (d) shows our ammeter. Here the deflection is produced by a magnetic field, which is caused by the current through the coil. But some may point out that the current is driven by an applied e.m.f., so as regards first causes it is voltageoperated. The same applies to the voltmeter (e) but this time there may be more who regard voltage as the operative quantity.

In all these except (b) there is a current and a voltage, and as they are directly proportional to one another there is liable to be dispute as to which is the cause. But look at (f), in which the deflection is directly caused by the current, and the current is-or can be argued to be-caused by the applied e.m.f., but is not proportional to it.

Legal cases in which the true cause has to be established are often troublesome, and the jury needs careful direction by the judge. May I suggest that the safest ,policy throughout Fig. 2 is to discard all "causes" which in principle are not essential. In (a) a current is not essential to the production of a force between the plates; they could be completely insulated and static. The same goes for (b) and (c). In (d) and (f) the current is the operative quantity; voltage could be dispensed with altogether by making the wire of a suitable metal cooled to a temperature at which it is superconductive. The rectifier could be a mechanical one with the same treatment. The only room for doubt would seem to be concerning (e), in which current is essential, but also resistance, and therefore voltage is essential for producing the current. The verdict in that case would probably rest on whether the instrument was considered as a whole or as a " movement" (by comparison, say, with the electrostatic type).

If we apply to the transistor this principle of what is essential, we can hardly avoid the conclusion that it is voltage operated. The base current, it seems to me, is an incidental and unavoidable evil, the amount of which (other things being equal) depends on the thickness of the base, the proportions of $p$ and $n$ impurities, etc. A valve would not,
presumably, cease to be voltage operated if it happened to be used with a positive grid, in which circumstances its similarity to a transistor is very close ${ }^{4}$.

But while this may be all very convincing, it seems to me quite academic. I am sure that when so many people say transistors are current operated they are not thinking of theoretical physics or deciding on first or direct or essential causes. What I believe they are thinking about can be illustrated by some characteristic curves I plotted for a fairly typical transistor I happened to have around-the OC45. Incidentally, they turned out to be very similar to the published " average" curves.

The output of a transistor is most appropriately expressed in terms of collector current, $\mathrm{I}_{c}$. In Fig. 3 this is plotted against the input or base current, $\mathrm{I}_{b}$, and also against the input voltage, $\mathrm{V}_{b}$. The collector voltage was of course kept constant.

Comparing these, we see that the $\mathrm{I}_{c} / \mathrm{I}_{b}$ curve is remarkably straight, right from the origin, whereas the $\mathrm{I}_{c} / \mathrm{V}_{b}$ curve, after a late start (not shown) is thoroughly curved all the way. It is in fact (as can be shown by plotting $\log \mathrm{I}_{c}$ against $\mathrm{V}_{b}$ ) almost exactly logarithmic. There are theoretical reasons why this should be so.

If for some special purpose we desired to make the logarithm of the transistor output proportional to the input, then we would obviously make the input the input voltage. But for nearly all practical purposes we want the output to be directly proportional to the input, and this relationship is clearly far better fulfilled by the $I_{c} / I_{b}$ curve, in which the input is current.

The effectiveness of a transistor as an amplifier is expressed by the slopes of these curves, the slope of the $\mathrm{I}_{c} / \mathrm{V}_{b}$ curve being $g_{m}$, and that of the $\mathrm{I}_{c} / \mathrm{I}_{b}$ curve, $\alpha$. The curves tell us at a glance that, right from zero, $\alpha$ is fairly constant, whereas $g_{m}$ varies widely all the way. So whatever bias voltage was applied, the output current would be a very distorted version of the input voltage.

It may be argued that such a transistor would usually be used for signals of a very small amplitude, over which even the $I_{c} / V_{b}$ curve is reasonably straight. But even if the potentialities of the transistor were restricted in that way, the amplification-indicated by the slope of the curve-would vary enormously with the voltage bias applied. And although it wotild not be difficult to decide on a bias suitable for this particular OC45 transistor, that bias would probably be quite unsuitable for another OC45 transistor. The point at which the $I_{c} / V_{b}$ curve reaches, say, 0.5 mA , varies greatly from one sample to another. This is not a feature peculiar to that type of transistor or its maker; it is common to all types and makes sold at reasonable prices.

It has been pointed out that if the $I_{r} / V_{b}$ curve is continued beyond about 0.25 V it tends to straighten out. Yes; but one of the main ideas of using transistors is to economize in current, so most of ten they are used below the part that could reasonably be described as straight.

So however the theoretical physicists look at it, in common practice transistor bias is related to current. And nearly always the input signal is applied as current. That is what I think designers have in mind when they say transistors are current operated.

Another thing I think they have in mind when
${ }^{1}$ Electronic Technology, February 1961, b. 37 (Editorial).


Fig. 3. Showing the relationship of collector current $I_{c}$ (at a constant collector voltage $-3 V$ ) to base voltage, $V_{b}$, and base current, $I_{b}$. Note the "false zero" for the $V_{b}$ scale. Transistor: OC45.
comparing transistors with valves is their low input resistance, contrasted with the almost infinite input resistance of a valve (at low frequencies). While emphasizing the close analogy between transistors and valves, Mr . Armstrong nevertheless recommends as the second most important transistor parameternot its voltage amplification factor, or even its equivalent of $r_{a}$, but its input admittance. This is the reciprocal of its impcdance, and is quite large, in contrast to the valve's which is almost nil.

Not only so, but like $g_{m}$ it is extremely non-linear, as can be deduced from Fig. 3. Using it, a curve of $\mathrm{I}_{b}$ against $\mathrm{V}_{b}$ (or vice versa) can be constructed; Fig. 4. The input admittance (or actually conductance, since no account is taken of reactance) is shown by the slope of this curve, which varies just about as much as $g_{m}$. So it too is rather an awkward thing to have to fill into design formulae.

Though I would hate to discourage anyone from teaching valves and transistors by comparison, that being what I do myself, the best policies can be spoilt by pressing them too far. To ignore the contrasts between valves and transistors is an example.

For any who may prefer figures to curves-the popular choice is, no doubt, both combined-here tabulated are the vital statistics of my OC45.*

| $\begin{gathered} 1 \\ \mathbf{V}_{b} \end{gathered}$ $(\mathrm{V})$ | $\begin{gathered} 2 \\ \mathrm{I}_{c} \\ (\mathrm{~mA}) \end{gathered}$ | $\begin{gathered} 3 \\ g_{m} \\ (\mathrm{~mA} / \mathrm{V}) \end{gathered}$ | $\begin{gathered} 4 \\ g_{i n} \\ (\mathrm{mv}) \end{gathered}$ | $\begin{gathered} 5 \\ r_{i n} \\ (k \Omega) \end{gathered}$ | $\mu$ | 7 $\alpha$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.150 | 0.18 | 7.2 | 0.25 | 4.0 | 2000 | 37 |
| 0.175 | 0.50 | 20 | 0.50 | 2.0 | 1650 | 40 |
| 0.200 | 1.4 | 56 | 1.08 | 0.93 | 850 | 48 |
| 0.225 | 3.7 | 148 | 3.0 | 0.34 | 430 | 56 |
| Ratio, max min |  | 20.6 | 12 | 12 | 4.7 | 1.5 |

* I am aware that some of these symbols are used elsewhere with different meanings, but if people choose to use for transistors the same symbols as for valves but with different meanings, responsibility for resulting confusion is entirely theirs. I adhere to the meanings that have been universally understood for the last 35 years or so. And I refuse to make the common-emitter $\alpha$ wear a' still less degenerate into a $\beta$; if you insist that all three configurations are on an equal footing, let their $\alpha s$ he $\alpha_{s}, \alpha_{b}$ and $\alpha_{c}$, the subscript ireticating which footing, let their $\alpha s$ he $\alpha_{\rho}, \alpha_{b}$ and $\alpha_{6}$, he subscript Erictish is common to input and output. The latest British Standard eiectrode is common to input and output. The latest British Standard on the subiect (BS.3363: 1961) apparently sets out to discourage the
use of $\alpha$ altogether, mentioning it only in an inconspicuous footnote use of $\alpha$ altogether, mentioning it only in an inconspicuous footnote
as a possible alternative to $-h_{f}^{\prime} \alpha^{\prime}$ is entirely ignored, and $\beta$ is to be as a possible alternative to - $h_{f} b^{\prime} \alpha^{\prime}$ is entirely ignored, and $\beta$ is to be
hfe. The only thing about this that gives me any joy is the ofticial use, at last, of the single subscript to indicate configuration.


Fig. 4. Input characteristic ( $l_{\mathrm{b}}$ against $V_{\mathrm{b}}$ ) for OC45. Again, $V_{c}=-3 V$.

Column 3 is what has been recommended as the most important transistor parameter, and that varies the most widely of the lot. Coupled with it was $g_{i n}$, column 4 (shown alternatively in 5 as resistance), and that comes next in variability. Column 6 shows the strangely overlooked $\mu$, which by comparison is tolerably constant (I had, of course, to do some $\mathrm{I}_{c} / \mathrm{V}_{c}$ measurements to find it). But far more constant is $\alpha$, column 7.

I will concede that in some transistors, especially
the high-power kinds, $\alpha$ varies more and $g_{m}$ varies less than in the OC45; on the other hand, there are some of which the opposite is true and $\alpha$ is almost perfectly constant. All this reminds one strongly of $\mu$ in valves.

Personally, then, I am not disposed to quarrel with people who call transistors either current operated or voltage operated, provided they do so in the right context. It seems to me misguided to prove by theoretical physics that the Mullard handbook and all suchlike are wrong in saying that transistors are current operated; and it would be equally wrong to quote the arguments I have just been using, against Dr. Shockley.

Readers with long memories (Mr. Clay?) $\dagger$ may recall, however, that there is one related situation in which a perfectly definite answer is forced on us. I refer to negative resistance, all of which appears on a current/voltage graph as a downwards-to-the-right slope. In spite of that, experiment reveals two distinct types of behaviour; the difference, as I showed in the February 1957 issue, is due to some negative resistance being voltage operated (os controlled) and some current operated.

It would save a lot of acrimonious breath and ink if we were always careful to observe the distinction between questions that are decided for us by Nature and those that are matters of convention or point of view.
$\dagger$ The allusion is to correspondence which appeared in this journal between April and September 1960.-Ed.

## BOOKS RECEIVED

F.M. Simplified by Milton S. Kiner. The third, completely revised edition of a non-mathematical treatise on the whole subject of frequency-modulation. The author describes the fundamentals of transmission and reception, including aerials and audio amplifiers in the first ten chapters. Several chapters are then devoted to the alignment and servicing of receivers, with reference to commercial equipment, followed by a section on the principles of f.m, transmitters and commercial transmitting equipment. A fault-finding chart is included and there is a bibliography. Pp. 376; Fig. 306. D. Van Nostrand Company Ltd., 358 Kensington High Street, London, W.14. Price 45s.

Transistor Circuits and Servicing, by B. R. A. Bettridge. (2nd edition.) Explains, in a practical manner, the nature of transistors, their applications in radio circuits and recommended methods to adopt when servicing transistor equipment. Written for the service engineer. Pp. 227; figs. 12. Iliffe Books Ltd., Dorset House, Stamford Street, London, S.E.1. Price 3s.

A First Course In Wireless, by " Decibel." The fourth, revised edition of a well-known elementary textbook of radio theory. Ranging from a chapter entitled "What is Electricity" to a description of superheterodyne technique and audio amplifiers, the book is completely nonmathematical and very readable. A chapter has been included on semiconductors. Pp. 247; Figs. 98. Sir Isaac Pitman and Sons, Ltd., Pitman House, Parker Street, Kingsway, London, W.C.2. Price 12s 6d.

Linear Graphs and Electrical Networks, by S. Seshu and M. B. Reed. An introduction to the use of linear graphs in electrical engineering network problems. The treatment is at post-graduate level, and Laplace transforms, the theory of functions and Boolean algebra are used extensively. The major part of the book is devoted
to the application of the linear graph. A comprehensive bibliography is included. Pp. 315. Addison-Wesley Publishing Company, Inc., 10-15, Chitty Street, London, W.1. Price 74s.

Industrial Electronics Apparatus by P. van der Ploeg. Concerned with reliability in industrial electronics the book discusses the electrical and mechanical design, and installation of equipment from this viewpoint. The second part of the book deals with maintenance, detailing essential equipment and proposing methods of faultfinding and repair. Data on valve operating characteristics is contained in a supplement. Pp. 116; Figs. 22; plates 33. Cleaver Hume Press Ltd., 31 Wright's Lane, London, W.8. Price 9s 6d.

Radio Waves in the Ionosphere, by K. G. Budden. A mathematical treatise on the propagation of radio waves in the ionosphere, and on their reflection from its boundaries. Intended both as a reference book for engineers and a textbook for students. It is assumed that the reader is familiar with the operators div, curl and grad., and electro-magnetic theory. Pp. 542. Cambridge University Press, Bentley House, 200, Euston Road, London, N.W.1. Price 95s.

La Modulation de Fréquence by J. Marcus. A mathematical treatise on the subject of frequency-modulation. Each chapter presents the theory of the phenomenon under discussion before going on to the more practical aspect. The more highly-mathematical calculations are contained in appendices. After having dealt with definitions and fundamentals, the author proceeds to describe the generation and detection of fre-quency-modulated signals, and devotes a chapter to the problem of noise. Multiplexing is discussed and examples are given of commercial f.m. equipment. Pp. 320; Figs. 175. Editions Eyrolles, 61 Boulevard SaintGermain, Paris, 5e, France. Price 43.65 NF (by post).

## Magnetically-Focused

# Travelling-Wave Tubes 

By J. M. WINWOOD*

use of reversed-field permanent Magnets

TRAVELLING-WAVE tubes and some other microwave valves depend for their operation on the interaction between an r.f. field and a long, straight electron beam. In most cases, because of the mutual repulsion between electrons, this beam would expand too rapidly unless constrained by immersion in a suitable magnetic field or by other means. Such a focusing field may be provided by a long solenoid, but when possible it is obviously advantageous to replace electromagnets and their power supplies with lightweight permanent magnets.
It is possible to design a uniform field magnet :o replace almost any solenoid (although there is a limit to the straightness of field obtainable with permanent magnet circuits, the errors can be made comparable with ordinary mechanical tolerances in coils) but the resultant permanent magnet will usually be very heavy and stray fields may extend over a large area.
Suppose that a certain axial field $\mathrm{H}_{0}$ is required to focus a given beam. The weight of a magnet designed to give this magnetic ficld is proportional to the cube of the length of uniform field $\mathrm{H}_{0}$ required since magnets with similar shapes but varying sizes all give the same field. However, although the field must be parallel with the axis of the electron beam,

the polarity of the magnet is immaterial. Thus, in order to decrease the weight of the focusing assembly for a given valve, it may be possible to use an assembly of several short magnets, each of which separately is capable of giving the desired field. For example, if we use a combination of two magnets each half the length of the original magnets, their weights will each be $\frac{1}{8}$ of the original. The total weight of the focusing system would then be only $\frac{1}{4}$ of the original. It will be necessary to reverse the direction of the fields of adjacent magnets so that the stray field of any magnet (which is oppositely directed to its wanted field) docs not reduce the useful field of its neighbours. The stray field of the assembly will then be much lower than that of an equivalent uniform field magnet.
One application of this principle is in periodic focusing. Clogston and Heffner ${ }^{3}$ and others ${ }^{2}$ have shown that it would be possible to replace a uniform magnetic field with a sinusoidal field having a similar r.m.s. value (and suitable period). Fig. 1 shows a typical periodic permanent magnet circuit together with its associared travelling-wave tube and Fig. 2 shows a plot of the magnetic field. The weight of the magnetic material is about 2 lb . This should be compared with about 40 lb for the equivalent uniform-field magnet.
Present low-noise travelling-wave tubes require a high magnetic field near the cathode (at least 500 and perhaps 1500 Oersteds) and it is also important that there should be no interception current in the early part of the slow-wave structure. A solenoid to give this field over the whole length of the valve may require from 0.2 to 2 kW and with the higher powers will probably require water cooling, while the equivalent uniform-field permanent magnet may weigh more than 100 lb . One effective solution for low-noise travelling-wave tubes would appear to be the com-

[^6]Fig. 1. Periodic permonent magnet circuit and (below) travelling wave tube.

Fig. 2. Plot of typical



Fig. 3. Reversing-field permanent-magnet circuit and travel-ling-wave tube.
bination of a short permanent magnet giving a suitably high uniform field in the cathode region, together with a periodic focusing system. If the field at the cathode is large, one finds that good focusing is only obtained if the peaks of the periodic field are also high. Unfortunately a criterion for satisfactory periodic focusing is that the period ( L ) is given by

$$
\mathrm{L}<\sqrt{\frac{400 \overline{\mathrm{~V}}}{\eta \mathrm{~B}^{2}}}
$$

where $V$ is the beam voltage, $B$ the peak flux density

and $\eta$ the ratio of the charge to mass of an electron, all in m.k.s. units. Because of the limitations of available magnetic material, this is not easily satisfied for the high peak fields required.

Recently, therefore, some theoretical and experimental work has been devoted to the possibility of using only a small number of abrupt reversals of field in order to reduce the weight of magnetic material in certain particular applications where periodic focusing is not possible. Such a system, with comparatively long periods, has been called reversing-field focusing. If it were possible to make very sudden reversals of magnetic field, the number and position of the reversals would be immaterial. In practice it is not possible to achieve perfectly sharp reversals, and it is found that the correct positions depend on both the amplitude of the magnetic field and on the beam voltage. This method of focusing has been found advantageous not only for low-noise travellingwave tubes, but also for high-power klystrons where periodic focusing of the beam would be possible if the position and size of the cavities did not interfere with normal periodic permanent magnets. The weight-saving factor when a reversing-field system with $n$ units of equal length replaces a unidirectional field is better than $n^{2}$. However, if the weight of the pole-pieces and r.f. circuitry is taken into account, there is little point in using more than one or two reversals.
The use of reversing field focusing has been discussed for the case of magnetically shielded cathodes by Murphy ${ }^{3}$ and the case of immersed cathodes will be the subject of a paper which will be published later ${ }^{4}$.

Systems with one reversal have been shown to work well for a range of low-noise t.w.t. amplifiers operating at frequencies covering from 3,000 to 10,000 $\mathrm{Mc} / \mathrm{s}$. An example of a typical amplifier for the $6,000 \mathrm{Mc} / \mathrm{s}$ communications band is illustrated in Figs. 3 and 4. The magnetization of the magnet system is also indicated in Fig. 4 and the axial magnetic field is plotted in Fig. 5. The direction of the field on the axis of the circuit is controlled by assemblies of soft ferro-magnetic rings (known as field straighteners) between the pole-pieces and is not dependent on the symmetry of magnetization of the magnets. Thus the performance of the travelling-

Fig 4. Magnet assembly of reversing-field circuit of Fig. 3.

Fig. 5. Plot of typical reversing-focusing field.
wave tube is not affected by the presence of small transverse stray fields from other sources. The weight of the magnet is 20 Ib , compared with about 100 lb for the equivalent uniform-field magnet.

The noise factor and gain of a t.w.t. are similar to those obtained in an equivalent solenoid, but the extra weight and fault liability of the solenoid power supply are eliminated. In addition there will be no danger of r.f. modulation induced by insufficient smoothing or poor stabilization of the power supply, or by pickup in the solenoid coils. Perhaps, however, the greatest advantage of the reversing-field system is that whereas the solenoid takes a long time to reach thermal equilibrium and may also require special cooling, particularly in enclosed equipment, the permanent magnets waste no power and remain cold so
that consistent life and performance should be obtained from the valve.

## References

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# 1,000-FT RADIO TELESCOPE 

## use of natural bowl-shaped valley

By R. J. SLATER, b.S.., A.m.I.c.E

NOW under construction at Arecibo, Puerto Rico, and expected to be completed shortly, is a $1,000-\mathrm{ft}$ diameter radio telescope. When completed, this new telescope will dwarf the $250-\mathrm{ft}$ diameter Jodrell Bank telescope and $600-\mathrm{ft}$ diameter radio telescope now being built at Sugar Grove, West Virginia. It will not however be as flexible in operation as either of these two telescopes.
When completed the telescope is to be used for investigations into the nature of the ionosphere.
The Arecibo radio telescope will have an aerial area of 18 acres, and will be able to detect a reflector only 3 ft square at a distance of 22,000 miles.
In contrast to conventional radio telescopes the aerial will be only a short distance above the ground in a large bowl-shaped valley. Instead of the parabolic antenna normally used with radio telescopes, the antenna at Arecibo will be made hemispherical so that it can scan a larger segment of the sky (up to $40^{\circ}$ ). To compen-
sate for spherical aberration a specially designed line feed is thus necessary. This will be suspended 435 ft above the wire mesh reflector. By movement of the line feed it will be possible to detect incoming waves and to direct radar signals within a cone of 40 degrees.

Levinthal Electronics Products are building the transmitter. This will permit initial operation of the telescope as a radar at $430 \mathrm{Mc} / \mathrm{s}$ with a beam-width of $\frac{1}{8}$ degree and a maximum power of $2 \frac{1}{2} \mathrm{MW}$ : Cornell University have designed the receiver. This will have two channels, a spectrum analyser and a gated radiometer for pulse integration.

Advantages of the Puerto Rican location as a site for this telescope are the natural bowl-like configuration of the valley in which it is situated, absence of radio noise in the area, and the latitude. This last is within $23 \frac{1}{2}^{\circ}$ of the equator, thus permitting planetary observations with $20^{\circ}$ of beam span.

Impression of how the $1,000-\mathrm{ft}$ Arecibo radio telescope will look on completion.


## By "DIALLIST"

## Reliability Wanted

NO ONE could agree more heartily than I with Earl Mountbatten of Burma in the plea for greater reliability in electronic apparatus which he made in his presidential address to the British Institution of Radio Engineers. If you have no need to keep an eye on production costs, a very good standard of reliability can be attained. I'm thinking of the apparatus shot up into space in exploring rockets: price there is no particular object and the gear seems to survive pretty well such rough treatment as terrific acceleration, and big temperature changes. I feel, though, that the increased freedom from breakdown is needed chiefly in the moderately priced gear which the man in the street buys in most of the world's countries to-day. Where I'd like to see greater reliability is in such things as domestic sound radio and television sets. You can't look through a radio magazine published in any country without finding descriptions of faults and fault finding in such sets.

## Shocks Are Warnings

WHAT wickedly dangerous things connections to the electric mains by two-pin plugs and sockets and lampholder adaptors are. It's an even
chance with either whether or not you connect the metal parts of any apparatus to the neutral or the phase wire. If I'd anything to do with it, I'd make it illegal to fit any but properly earthed three-pin sockets or to sell electrical goods provided with two-pin plugs or lampholder adaptors. Not long ago a man who was actually a skilled electrician was killed by a shock from his electric guitar. The unfortunate fellow had had shocks from it previously, but took no notice of them. A shock, however slight, from any piece of electrical gear is a warning: it shows that there is something wrong and action should be taken at once. If you move into a new house, it's always as well to run over the threepin sockets with a neon pole-finder. I've several times found many of those in friends' houses wrongly wired, so that switching off merely broke the neutral and left the phase socket alive.

## TV Gets Going in France

IT has been officially announced that the number of licensed television receivers in France passed the two million mark at the end of March, when $2,131,305$ were in use. Between the end of March 1960 and the same date in 1961 over 600,000 new TV sets were installed. In this country

## "WIRELESS WORLD" PUBLICATIONS


and in the United States it seems as if the saturation point has almost been reached-it can never quite be reached because of the number of new houses that become occupied. France has still a long way to go before anything of the sort happens there. It's believed that there'll be another big jump forward when the second programme with 625 -line definition gets going.

## Exploring Caves in the " Med"

WHAT an interesting time the members of the Cambridge University Underwater Exploration Group will have in the Mediterranean. Equipped with a formidable array of electronic gadgets, they have set out from this country in the 138 -ton yacht Titan:a and will spend four months on their task, which is to make a fresh set of readings in the level of this sea since the early days of the Ice Age. All the fifteen members of the expedition are experienced divers. Navigation to and from the "Med" is being done largely by means of Marconi radar and two Ferrograph echometers. There is also a portable echometer for use in mapping underwater caves. Once located, the caves are to be explored by divers, equipped with underwater intercommunication apparatus. Nearly 50 underwater caves are known and from these the team hope to collect evidences of human occupation in the old days. They will also search for specimens of organic matter, which, after testing the radioactive carbon 14, may date the time when the caves were above the surface.

## Underwater Television

NEW uses for underwater television are continually being found. One of the latest is of Australian origin. The catching of sea crayfish is an important industry off Australian coasts; but it's not always easy to find them, for they move about from reef to reef. The idea is to equip a control boat with a TV camera and to send her over successive reefs. If crayfish are there, they show up well on the screen. Once found this boat would put out a radio marker buoy, transmitting a v.h.f. signal to guide fishing boats to the scene of action.

Other jobs for underwater TV are being found in the Suez Canal. There, it will locate submerged debris, which now causes much damage to the cutting teeth of dredgers. It will also enable engineers to examine ships damaged below the water line and to direct repair operations. It is hoped that means will soon be found of fitting cameras to the keels of ships passing through the canal. On monitor screens it will then be possible to keep a constant watch ahead on their clearance of the bottom and this should prevent any possibility of their running aground.

## Further Education

HERE is a selection from the many prospectuses and syllabuses of both part-time and full-time courses we have received from colleges and further education establishments.
Twickenham Technical College.-The first of three four-week full-time courses begins on October 2 nd. It covers "Electronic Circuit Design." The second, "Transistor Theory and Applications," starts on November 6th, and the third, "Principles of Automatic Control," on January 15th. On Friday evenings from September 22nd the college is providing a 12-lecture course on printed circuit techniques and on Thursday evenings from September 28th a 23-lecture course on pulse circuit design.

South-East London T.C.-An evening course of about 25 lectures on electric circuit and field theory commences on October 17th.
Norwood T.C.-In addition to fulltime courses for C. \& G. certificates in telecommunications engineering and the P.M.G.'s certificate for marine radio officers, there are short courses of 6-12 weeks' duration in such subjects as electronic computers, transistors, parametric amplifiers and medical electronics. A six-lecture evening course on masers and parametric amplifiers starts on October 3rd.
Northern Polytechnic.-A five-year part-time day or evening course for the recently introduced Electronic Servicing Certificate is provided. The college's three-year course for its diploma in telecommunications fully meets the requirements for the graduateship examination of the Brit. I.R.E.
Radio Amateur's Exam.-Classes in preparation for the P.M.G.'s examination are again being held at the Wembley (Middx.) Evening Institute (Mondays from Sept. 18th); Allan Glen's School, Glasgow (Tuesdays from Sept. 12th) with a general radio theory class on Thursdays (from Sept. 14th); Brentford (Middx.) Evening Institute (Wednesdays from Sept. 20th) with a radio servicing course on Tuesdays and a mathematics course on Thursdays; and Ilford (Essex) Literary Institute an eight-month course on Wednesdays (from Sept. 20th) and a two-year course on Thursdays, both courses being organized by the East London R.S.G.B. Group.


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## By "FREE GRID"

## Transistorized Tintinnabulations

DURING this summer there have been many references in the press to the nuisance caused at our seaside resorts by the tiny and sometimes tinny portables which add their transistorized tintinnabulations to the already existing pandemonium caused by bawling babies and barking dogs. I cannot say this addition to normal beach noises distresses me a lot as, being blessed with a clear conscience, I never find any difficulty in taking a quiet nap on the beach while Mrs. Free Grid tans her torso.

However, one day earlier in the summer I did have a somewhat unusual experience which may be of help to our seaside authorities in giving them an idea as to how it would be possible to tackle this new nuisance. I was having my normal nap on the sands when I received a sharp dig in the ribs from Mrs. Free Grid who wanted to know why all the portables on the beach seemed to be bellowing morse at full blast.

When I had collected my senses, and my false teeth which I always remove when sleeping, I was astonished to realize that all the portables on the beach were churning out my initials, while their owners were frantically but unsuccessfully trying to recapture the B.B.C's drownedout daily drool. My initials were soon followed by the morse signal "de" (from) and then by the initials of one of the little grid leaks of the third generation. Then followed a message urgently requesting my presence at the car, which was parked on the sea front.


Junior Sparks.
the boy standing by the open bonnet of the car. It appeared that he had forgotten exactly whereabouts on the beach he had left me, and so he had displayed his initiative by connecting the rod aerial of the car radio receiver to one of the sparking plugs and using two pieces of wire connected in the primary circuit as an improvised morse key. The urgent demand for my presence arose because he needed money for icecream.

It was this incident which made me think what an excellent thing it would be if seaside corporations could equip a car with a low-power spark transmitter to trundle up and down the promenade every now and again. With a direct-coupled spark transmitter, of course, the tuning is so broad that it would break through on any of the wavelengths to which the beach sets would be tuned.

The trouble is that it would cause interference to people who were using sets in nearby houses, and the Postmaster General's minnions would then intervene. What is obviously wanted is some form of selective or directional jamming. W.W. does not dabble in politics otherwise I might be able to suggest the name of a foreign power which could advise in this matter.

## Forestalled Inventions

SPEAKING as one who has always regarded Hertz as giving the first practical demonstration of ClerkMaxwell's theory of electromagnetic waves, I was rather surprised to read recently that Edison forestalled him by several years.

In the issue of the Scientific American, dated December 25th, 1875, Edison gave a full description of his apparatus for generating and detecting the presence of e.m. waves. There is nothing very startling in that, of course, for after what Clerk-Maxwell had to say, it was obviously open to any competent person to seek experimental proof of his theory. The only part that interested me was that Edison was several years in advance of Hertz*, who is always the one mentioned whenever reference is made to the first practical demonstration based on Clerk-Maxwell's work.

It was Edison also who, in 1883, first stuck a metal plate in an electric lamp and measured the current passing across the gap between it and the filament. In one sense this constituted the invention of the diode which Fleming patented twenty-one years later. But the difference is that Edison had no idea of using it as a rectifier for the detection of wireless signals and he did not patent it, whereas Fleming had and did.

I suppose there must be many instances of that sort of thing not only in the matter of radio inventions but of others also. Thus Edison first had the idea of recording sound in 1876 and in the following year he patented the cylinder-instrument which we know as the phonograph. But Leon Scott recorded sound on his "phonautograph" twenty years earlier, in 1857, but he did not pursue the matter.

Coming to modern times, articles dealing with the experiments of Lossev (a Russian engineer) and others with what were called oscillating crystals appeared in W.W. during 1924, and the matter was not new even then. Yet nearly twenty-five years had to pass before these devices, in greatly improved form, made their bow under the name of transistors.

Many of the things which I myself invented in pre-war years, such, for instance, as radio-controlled traffic lights for emergency operation by fire engines and ambulances (2.12.37) have not yet been put into use. When they are I feel quite sure I shall not be the one to receive the credit of the "marvellous new invention" as it will be called by the lay press.

* Among other even earlier anticipations of e.m. wave phenomena (as distinct trom induction effects) may be cited the words of Joseph Henry in a communication to the Smithsonian Institution in 1842: "It the Smithsonian Institution in 1842 : "It would appear that a single spark is sufficient throughout at least a cube of 400,000 feet of capacity, and it may be further inferred that the diffusion of motion in this case is almost comparable with that of a spark from flint and steel in the case of light." But it was Hertz whose scientific work verified hypothesis.-ED.


## Lexical Ectopism

CAN anybody tell me why it is that when we went all classical by adopting the word "anode" in place of the more homely "plate," we still continued to use the plebeian word "grid" to describe the electrode which acts as the door or gateway which regulates the anode current by the degree to which it is open or shut?
Why didn't we call it a thyrode or pylode? The mundane word "grid," used to describe an electrode which is sandwiched between such lordlysounding things as an anode and a cathode has always struck me as a very strange ectopism.

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AMPLIFIER KIT Model MA-I2
 A compact high fidelity power amplifier (including auxiliary power supply) 12 watts output. Wide frequency range and low distortion. A variable sensitivity control is fitted enabling it to be used with an existing am plifier in a stereophonic system. Other applications include sound reinforcing systems, transmitter modulators, for use with tape recorders, also as a general pur pose laboratory amplifier. \&10.19.6

STEREO-HEAD BOOSTER KIT


## Model

USP-I
Hi-Fi Stereo Pre-Amplifier for low-outpu lnput 2 mV .s. Input 2 mV . to 20 mV . Output
Irom 20 mV . to $2 \mathrm{~V}, 40-20,000 \mathrm{c} / \mathrm{s}$. Also suitable as low-noise R.C.-Coupled highgain monaural
£6.17.6

STEREO CONTROL UNIT KIT Model USC-I
Incorporates incorporates all worth. while features
for high fidelity stereo and mono. Push-button seleccion, accurately matched ganged control; to $\pm 1 \mathrm{~dB}$. Negative feedback rumble and ariable low-pass filters. Printed circuit boards. Accepts inputs from most tape heads and any stereo or mono- $218,18.6$ pick-up.

## TAPE DECKS

Are available as "packaged deals" with other equipment. Customers purchasing much of their audio equipment at the same time will find our PACKAGED DEAL scheme more economical. Details un request.

[^7]

STAND



A NEW AND ATTRACTIVE CABINET in modern seyle designed to house all your Hi-Fi equipmen (including tape deck and full-sized transeription record player). The cabinet parts are veneered and pre-drilled, with edging in Panoplex plastic strip, for ease of finishing. Complete with every thing you need for assembly, including screws, hinges and even a padsaw! Left "in the white for finishing to choice.
Size $39 \frac{1}{1} \times 32 \times 21$ if in .
£17.5.0
-

## TAPE AMPLIFIER UNITS

 Models TA-IM andTA-IS


This Combined Tape-Record/Replay Amplifier is available in both monophonic and stereophonic models. Model TA-IM can be modified to the stereo version with modification kit TA-1C.
TA-IM, £18.2.6; TA-IS, £23.6.0; TA-IC, £6. 10.0


## CHEPSTOW

## EQUIPMENT CABINET KIT

Spacially designed tor' those whose floor space is at a premium. Secoreo Amplifier Tuner Stereo Amplifier and ad ditional power ampliffer where is available An upper self-power stereo amplifiers self-power stereo amplifier to ensure maximum heat dissipation. Ven. eered and left in white "lor finishing to per sonal taste. Overall dimensions
are $35 \mathrm{in}, \times 18 \mathrm{in} . \times 33 \mathrm{in}$ high are $35 \mathrm{in} . \times 18 \mathrm{in} . \times 33 \mathrm{in}$. high


HI-FI STEREO AMPLIFIER KIT Model S-88 Gives 16 w . output ( 8 per channel with 0.1 per cent. distortion channel). Is has
ganged controls metal cabinet with a golden surround and push-pull output. 20 mV . ( 4 mV . available $7 / 6$ extra).

HI-FI SPEAKER SYSTEM KIT Model SSU-I Oucted-port bass reflex cabinet, " in the white." Fre. quency response to $40-16,000 \mathrm{c} / \mathrm{s}$. Power rating 25 wates. Matched speaker units Bin. high flux
 ( 12,000 lines)
 with hyperbolic cone and 4in. Wide angle dispersion type for higher freauencies.
With legs $\& \| / 16 / 6 \ldots . . . . . . . .$.

## COTSWOLD SPEAKER SYSTEM KIT

This acoustically designed enclosure measures $26 \times 23 \times$ 15 special 12 in. bass a special
speaker with 2 in . speech coil, ellipspeech coin, elliper together with a pressure unit to cover the full frequency range o. quency range
$30-20,000 \mathrm{c} / \mathrm{s}$. Its polar distribution
makes it ideal for really Hi-Fi stereo livered complete, with speakers, cross-over livered complete, whit, level control, Tyan grille cloth unit, "eve control, "ygan grise cloth, etc. taste, all parts are precut and
drilled for ease of assembly.
\&21.19.0

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## Sin. OSCILLOSCOPE KIT



## Model O-12U

Laboratory quality at utility oscilloscope price and ease of assembly make this kit of ourstanding value. Vertical frequency response $3 \mathrm{c} / \mathrm{s}$ to $5 \mathrm{Mc} / \mathrm{s} .,+1.5 \mathrm{~dB} .-5 \mathrm{~dB}$. sensitivity 10 mV . per cm . at 1 kc. Horizontal frequency $1 \mathrm{c} / \mathrm{s}$. to over $400 \mathrm{kc} / \mathrm{s}$. ( $\pm 1 \mathrm{~dB}$. up to $200 \mathrm{ke} / \mathrm{s}$.). The Heath patented sweep dircuit functions from $10 \mathrm{c} / \mathrm{s}$ to $500 \mathrm{kc} / \mathrm{s}$. in five ranges giving five times the usual sweep of other 'scopes. In addition it has exceedingly short re-trace and rise times and electronically stabilised power supply. Included is a 48 -page $£ 36.10 .0$ inseruetional Manual.
ELECTRONIC SWITCH KIT Model (Oscilloscope Trace Doubler) S-3U


This extremely useful, low priced device will extend the use of duties orherwise only in the province of the double-beam tube. In short, at a nominal cost, the Heathkit model S.3U will give you the advantages of a double (or other multiple) beam 'scope, while retaining alf the advantages of your present single-beam instrument.
Hitherto an electronic switch of this nature, permitting the simultaneous observation of two signals on the sereen of a single-beam C.R.T oscilloscope, has cost nearly as much as the 'scope itself. 10.15 .6


## MULTIMETER KIT <br> Model MM-IU

Provides wide voltage, current, resistance and dB ranges to cover hundreds of applications. Sensitivity 20,000 ohms/volt D.C. and 5,000 ohms/volt A.C. Ranges: 0.1 .5 v . to $1,500 \mathrm{v}$. A.C. and D.C.; $150,1 \mathrm{~A}$ to $15 A \mathrm{D.C}. ; 0.2 \Omega$ to 20 MS . \& 11.18 .6
AUDIO SIGNAL GENERATOR KIT Model AG-9U

$10 \mathrm{c} / \mathrm{s}$. to $100 \mathrm{kc} / \mathrm{s}$., switch selected. Distortion less than $0.1 \%$. 10 v . sine wave output metered in volts and dB 's. \&19.19.6

## AU.DIO VALVE MILLIVOLTMETER KIT Model AV-3U

Very sensitive. High stability. 1 mV . to 300 V . A.C. $10 \mathrm{c} / \mathrm{s}$. to $400 \mathrm{kc} / \mathrm{s}$.
£13.18.6

## AUDIO WATTMETER KIT

## Model AW-IU

This popular meter is used in many recording studios and broadeasting stations as a monitor as well as for servicing purposes. Dissipation rating up to 25 w . Continuous. 50 w , intermittent. \&14.14.0

## HI-FI F.M. TUNER

Tuning range 88-108 $\mathrm{Mc} / \mathrm{s}$. Flywheel tuning. Attractive Plastic Front Panel in twosone grey with golden
trim surround and motif. Thermometer type visual tuning indicator. Pre-aligned I.F. transformers (eliminates adjustment). Three I.F. Stages. Wide-band low distortion Ratio Detector. Complete R.F. Unit, wired, tested and pre-aligned (ready for mounting to chassis). Printed circuit for I.F. Amplifiers and Ratio Detector, for ease of assembly. No alignment necessary after assembling. Builtin power supply. Outpur sockers for stereophonic adaptor (for stereo transmission when available).
TUNER UNIT Model FMT
4 U (incl. $16 / 11$ P.T.) with 10.7 Mc/s I.F. output........... Supply MLIER and 4 Owe plete with case and valves...... 11 II 0

Sold separately ......... Total $£ 14130$

## TRANSISTOR PORTABLE

 RADIO KIT Model UXR-IPresented in elegant real hide case with tasterul gold relief. 4 a 6 assembled in 4 to 6 hours, and you have a set in the top flight of transistor por. transformers, printed transformers,
7 in.
$x$ in.
printed high-flux speaker.


## 4-wave TRANSISTORISED <br> PORTABLE RADIO KIT Model RSW-I

Using 7 latest type eransistors and three diodes this highly sensitive set is specially designed for Short and Medium wavebands and $11-18 \mathrm{~m}$.). In solid leather case fitted with retractable whip with ${ }^{\text {r }}$
aerial.


## PERSONAL TRANSISTOR RADIO KIT Model UJR-I

Operated by a 4.5 v . torch battery, thls sensitive dual-wave headphone set is a fine introduction to electronics for young and old. In Polystyrene moulded plastic case which accommodates battery (and
amplifier if added).

Additional Amplifier Stage Model UJR-IS will enable the UJR-1 to work a loudspeaker under favourable conditions. 16/6 extra

## Deferred Terms

available on all orders above $\$ 10$

## VALVE VOLTMETER KIT

## Model V-7A

The world's most popular valve volemeter, with printed cireuit and । per cent. precision and laboratory performance it has 7 volary performance. It has 7 voltage ranges measuring respectively d.c. volts to ., 1 and a.c. 1,500 r.m.s. and 4,000 peak ro peak. Resistance $4,00 \mathrm{~s}$ urements from 0.1 ohm to 1,000 M ohms with internal battery. D.C. input impedance is II megohms and dB measurement has a centre-zero scale. Complete with test prods, leads and standardising battery.

R.F. PROBE KIT Model 309-CU

This complete probe kit will extend the frequency range of the V.7A Valve Volemeter to $100 \mathrm{Me} / \mathrm{s}$ and will enable useful voltage indication to be ob tained up to $300 \mathrm{Mc} / \mathrm{s}$.
£1.9.6

## POWER SUPPLY UNIT KIT Model MGP-I

Compact, general purpose unit suitable for FM Tuners, Tape Recording Amplifiers and general Laboratory use. Input $100 / 120 \mathrm{v}$. 63 A C. 200 Outpu 120 mA max. 24.16 .6

## DECADE CAPACITOR KIT

Model DC-I
Capacity values $100 \mu \mu \mathrm{~F}$ to $0.111_{\mu} \mathrm{F}$ in $100 \mu \mathrm{~F}$ steps. Precision silver-mica capacitors and minimum loss ceramic waler switches ensure $£ 6.5 .6$

## R.F. SIGNAL GENERATOR <br> Model RF-IU

Provides extended frequency coverage on six bands from $100 \mathrm{ke} / \mathrm{s}$. $100 \mathrm{Mc} / \mathrm{s}$. on fundamentals and up to $200 \mathrm{Mc} / \mathrm{s}$ on calibrated harmonics.

23in. SERVICE OSCILLOSCOPE KIT Model OS-I

Light, compaet, portable, for serviee engineers. Printed circuit board tor easy construction. We. $10 \frac{1}{2} \mathrm{lb}$. Size $\sin . x \sin \times$
£19.10.0 14íin. long.


## CAPACITANCE METER KIT Model CM-IU

This Direct-Reading Capacitance Meter is a very low priced, time-saving instrument which is so useful that is should be part of the general equipment of every electronic laboratory and production line. Easily built in a few hours. $0-10014 \mathrm{~F}, 0-1,00014 / \mathrm{F}, 0-0.01 \mu \mathrm{~F}$ $0-0.1, \mu$ F. The meter has $4 \frac{1}{i} \mathrm{in}$. scale and can be used by an unskilled operator after a few minutes' 214.15 .0 instruction.


| so usetul |
| :---: |
| $\square$ |



Covers all amateur bands from 80 to 10 metres, crystal controlled. Power input 75 wates C.W. 60 watts peak controlled carrier phone. Ousput 40 watts to aerial. Provision for V.F.O. Filters $\{32.10 .0$
minimlse T.V. interference.

## AUDIO SINE-SQUARE WAVE generator kit Model AO-IU

An inexpensive generator which covers $20 \mathrm{c} / \mathrm{s}$ to $150 \mathrm{kc} / \mathrm{s}$. in four ranges with choice of sine or square waves. The latter up to $50 \mathrm{ke} / \mathrm{s}$. Output voltage 10 v . max. and distortion less than $1 \%$. An ideal instrument for audio testing. Size $9 \frac{1}{2} \ln . x \quad 312.18 .6$

## HIGH VOLTAGE PROBE KIT

 Model HV-336Measures voltages up to 30,000 v. D.C. with negligible circuit loading. A special High Stability 1,090 megohm resistor gives a mulsiplication factor of 100 X when used with a valve voltmeter of 11 megohms inpur impedance such as the
£2.15.6
BALUN COIL UNIT KIT


Useful transmitter accessory. Will match unbalanced co-axial lines, used on most modern transmitters, to balanced lines of either 75 or $300 \Omega$ impedance. adjustment over the frequency range of 80 through 10 meters, and will handle power inputs $£ 4.9 .6$
up to 200 watts. up to 200 watts.

## Forthcoming Kits

## STABILISED POWER PACK

 Models MSP-IM and MSP-IWSpacially recommended for industrial and laboratory use, meeting the need for a reliable and versatile stabilised power pack capable of a very high performance. Input 200-250 v., $40-60 \mathrm{cls}$. A.C., fully fused. Outputs: H.T. 200-410 v. D.C. at 20-225 mA . in 3 switched ranges. Unstabilised A.C. 6.3 v . at 4.5 A ., centre-tapped. Two $3 i n$. "easy-to-read" meters for reading voltage and current simultaneously. Separate L.T. and H.T. supply cransformers. All output circuits are isolated. Size $13 \mathrm{in} . \times 8 \frac{1}{2} \mathrm{in} . \times 9 \frac{1}{2} \mathrm{in}$. MSP-IM (with meters)
£34.12.5
MSP-IW (without meters).....
ع27.17.0 V-7A.

B-IU

#  <br>  

## THE <br> "MOHICAN" GENERAL COVERAGE RECEIVER KIT Model GC-IU <br> 

This fully transistorised receiver, which includes 4 piezo-electric transfilters, is in the forefront of receiver design. It is an excellent portabie or fixed station receiver for both the Ham and the short-wave listener. To overcome the problems of alignment, etc., the R.F. "front-end " is supplied as a pre-assembled and pre-aligned unit. Designed for outstanding performance, its many features inelude a 10 transistor circuit, printed circuit board, telescopic whip antenna, tuning meter, and a large sliae-rule dial giving a total length of approximately 70 inches.
Housed in a strong steel cabinet in stoveenamelled green and powered by two 6 volt dry batteries (not supplied) mounted internally, it gives continuous frequency coverage from $550 \mathrm{Ke} / \mathrm{s}$ to $30 \mathrm{Mc} / \mathrm{s}$ in five bands; thus enabling world-wide reception. Electrical bandspread on five additional bands covers the amateur frequencies from 80 to 10 metres-each band having a scale length of approximately 8 inches. B.F.O. tuning and


## GRID-DIP METER KIT

 Model GD-IU

Functions as oscillator or absorption wave meter. With plug-in coils for continuous frequency cover- 010.9 .6
age from $1.8 \mathrm{Me} / \mathrm{s}$. to $250 \mathrm{Mc} / \mathrm{s}$.

Additional Plug-in Coils Model 341-U extend coverage down to $350 \mathrm{kc} / \mathrm{s}$. With dial correlation curves, 15/-

## TRANSISTORISED GRID-DIP METER KIT Model XGD-I

Similar to GD-IU. Fully transistorised with a frequency range of $\mathbf{2 1 0 . 8 . 6}$
1.75 to $45 \mathrm{Mc} / \mathrm{s}$.

## AMATEUR TRANSMITTER KIT

 Model DX-I00U

The world's most popular Amateur T.X. Kit

- Completely selt-contalned, compace "Ham Transmitter. 150 W. D.C. input.
- Built-in high stable VFO and all Power Supplies. TVI: Careful design has reduced TVI to a minımum by use of effectively screened frequency-generating stages and pi-tuned circuits at the input ano output the PA stage, and by II chokes and pi network fiters to all outlets from the cabinet. No ewer than 3.5 dise-ceramic by-pass capacitors help to achieve the exceptional stability and high-performance for which this Transmitter is noted.
- The KT88 high-level anode and screen modulator stage gives over 100 watts of audio from less than 1.5 $m V$. input.
2djustable drive and clamp control ensure that valves are only driven sufficiently to maintain the required output.
- Keying on CW is via the VFO and buffer amplifiter cathodes; the other RF valves are biased beyond cut-off. When zero-beating the TX with incoming signals, the exciter stages only may be run without the final amplifier being switched on.
Provision has been made for remote contro operation.,
- VFO slow-motion drive is very smooth and backlash íree. VFO or Crystal control.
Covers all Amateur bands up to
$30 \mathrm{Mc} / \mathrm{s}$. phone or CW ...............
£81.10.0
VARIABLE FREQUENCY OSCILLATOR KIT Model VF.IU


Specially designed to meet the demand for the maximum possible flexibility from an amateur Transmitter which would otherwise be subiect to certain limita tions imposed by erystal control. For all Amateur Bands luar byetres. ldeal for Heathkit DX-40U and similar transmitters ................... 211.2.0

## Deferred Terms

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All prices include free delivery in U.K.

## Please send me FREE CATALOGUE (Yes/No)..

Full details of Model(s).
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WESTINGHOUSE MICROSCATTER BRINGS YOU 4 OPERATING ADVANTAGES AT THIS HIGHER FREQUENCY

Canadian Westinghouse Company Limitedpioneers in tropospheric scatter at 5000 mc have supplied equipment for service throughout the world. Operating results substantiate FOUR basic advantages for long range multihop trunk systems.

1. SIZE - Compact radio equipment allows trailer or fixed station installation. Small antennas, 1028 feet in diameter with high gain. Close antenna

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## "STETTNER" CERAMIC DISC \& TUBULAR TRIMMERS

miniature and standard.
Sizes $7.5,10,12,16$ and 25 mm . dia. Eminently suitable for Transistor Radios and Printed Circult application. High quality and reliabilitylow prices.
"STETTNER" CERAMIC CAPACITORS
A very wide and comprehensive selec. tion of CERAMIC CAPACITORS, tubular and dise. LOW VOLTAGE ceramic Capacitors for transistorlsed

"MEUBERGER" SUB-MINIATURE Low voltage ELECTROLYTIC CAPACITORS for D.C. applications, transistor circuitry and printed circuit applications. 4.5 mm . dia. MCITORS for all hectirlic CAP ACITORS for all the above applications
plus photo-flash equipment. D.C. range plus photo-flash equipment. D.C. range from $3 v$. to 385 v . Etched foil construction, hermetically sealed in aluminium tubes, iully tropical and compact. Temperature range: standard $-20^{\circ}$ to $+70^{\circ} \mathrm{C}$, for more
stringent requirements, specii $\quad$ stringent requirements, ${ }^{5} \mathrm{p}{ }^{3} \mathrm{cii}$
models for $-40^{\circ}$ to $+85^{\circ} \mathrm{C}$.
P.Y.C. insulated or non-insulated P.V.C. insulated or non-insulated


SPECIAL TRIMMERS
Tubular-screw adjustment, mica dielectric. Wide capacitance sweep, e.g. A/R TRIMMER $2 / 20 \mathrm{pF}$ mounced on ceramic base.

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 CAPACITORShermetically sealed in aluminium tubes. CAPACITORS for discharge lighting applications.
CAPACITORS for Motor Starting. BOTH TYPES ARE SUITABLE FOR OPERATING IN TEMPERATURES OF UP TO $+90^{\circ} \mathrm{C}$ WITH PEAK OF $+100^{\circ} \mathrm{C}$.

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Single position Vacuum Oven. Temp. $0-300^{\circ} \mathrm{C}$ Vacuum range $10^{-4}$ double ended for fitting in glove box.

ine for C.R.T. complete with oven, air circulation, automatic temperature controls, etc. $\qquad$


## In Design and Production

## PH HECO

use

## MARCONI TEST EQUIPMENT



In Italy, people happily go home to their Philco radio and television receivers. For Philco realise that the continued success of their products is due to a rigorous adherence to quality standards. It follows naturally that this leading Italian company employs a wide variety of Marconi instruments. Prominent in this picture is the Wave Analyser TF 455 E , a highly selective and sensitive Analyser for the accurate evaluation of both absolute and relative levels of individual components of a complex waveform. It covers the frequency range $20 \mathrm{c} / \mathrm{s}$ to $16 \mathrm{kc} / \mathrm{s}$.

## MARCONI INSTRUMENTS

For full details of Wave Analyser TF 455E, an instriument which has many uses in testing audio equipment, write for Leaflet G193. Please mention any other fields of electronic measurement in which you are interested.

## THE PHILCO ITALIANA LABORATORIES, MILAN

Marconi test equipment, including the Wave Analyser TF 455 E (at left), being used to test the distortion of the low-frequency amplifier of a transistored receiver undergoing development.

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23/25 Station Square, Harrogate. Telephone: 67455

[^8]

AGENTS THROUGHOUT THE WORLD


The award for Outstanding Engineering Achievement presented by the American National Academy of Television Arts and Sciences to the English Electric Valve Company Limited for their work in developing the $4 \frac{1}{2}$ inch Image Orthicon.
With this presentation comes the distinction that it is the first occasion that the award has been presented anywhere outside the United States of America.

## 'ENGLISII

 ELECTRIC" IMAGE ORTHICONSUsed by broadcasting stations throughout the world to provide better picture quality than ever previously attained
$3-\mathrm{in}$. and $4 \frac{1}{2}$-in. tubes for Studio, Outside Broadcast and Medical applications.


## seven-range meter, including V, mV, $\mu \mathrm{A}$, made for Elliott's at short notice

This seven-range meter, using Ernest Turner Model 605 was calibrated with special ranges by Anders at short notice for Elliott Brothers Ltd for the specialpurpose test gear shown above. All the meters in this complex installation were supplied by Anders, who have the pleasure of carrying out similar work for a number of famous manufacturers. Anders are indebted to Elliott Brothers for kind permission to illustrate this equipment.

The Anders Instrument Centre commands the largest stocks of meters in the country, unique calibrating facilities, and detailed knowledge of metering problems. Most standard meters are supplied immediately. Non-standard meters of all kinds, shapes and sizes, for special voltage and current ranges, are accurately calibrated, tested and normally ready within 10-14 days. Makes include Avo, Crompton Parkinson, EAC, Elliott, Pullin, Tayylor, Turner, Weir, Weston. Types include moving coil, moving iron, thermocouples, electrostatic, dynamometers, from $1 \frac{1}{2}^{\prime \prime}$ to large switchboard instruments, and complete range of accessories. Please write or 'phone for details of the Anders meter service.

# ADDESS 

## ELECTRONICS LIMITED

103 Hampstead Road, London NWı. Tel: EUSton 1639 Contractors to GPO and Government Departments. Ministry of Aviation approved.

## COMPONENT'S REVIEW

## TUNNEL DIODES

## now in JEDEC T0-18 Cases

STC, having introduced Tunnel Diodes to Europe, now carries the design of these devices a stage further by encapsulating them in JEDEC TO-18 cases. The diodes are available to industry immediately.

Tunnel Diodes are finding many applications in digital computers, counting circuits and in high-frequency low-noise amplifiers. These new devices are destined to carry semiconductor performance into the kilomegacycle region.

|  | JK <br> 9B | JK <br> 10B | JK <br> 11B | JK <br> 198 | JK <br> 20B | JK <br> 21B |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Peak <br> Current | mA <br> (nom) | 1.0 | $5 \cdot 0$ | $15 \cdot 0$ | 1.0 | $5 \cdot 0$ | $15 \cdot 0$ |
| Current <br> Ratio | (typ) | 4 | 4 | 4 | 6 | 7 | 8 |
| Junction <br> Capacitance | pF <br> (typ) | 25 | 50 | 125 | 10 | 30 | 90 |
| Resistive cut-off <br> Frequency Mc/s (typ) | 540 | 810 | 810 | 1200 | 1050 | 980 |  |



BIAS VOLTAGE (mV)
TYPICAL CHARACTERISTIC FOR A JK10B TUNNEL DIODE
Full details of these devices may be obtained from STC Transistor Division, Footscray, Sidcup, Kent.

## STANTELUM CAPAGITORS

 sealed tantalum capacitors, stantelum, are manufactured in four main groups:
HIGH TEMPERATURE FOIL TYPE
This is a range of tantalum capacitors for operation up to $125^{\circ} \mathrm{C}$ and the devices are manufactured to withstand vibration conditions far in excess of those specified in RCS 134B

> | Temperature range | -40 to $+125^{\circ} \mathrm{C}$ |
| :---: | :---: |
| Voltage range | 6 to 100 V d.c. |

Capacitance range
Polarized types 0.4 to $200 \mu \mathrm{~F}$ Non-polarized types 0.2 to $100 \mu \mathrm{~F}$

## STANDARD FOIL TYPE

First in the Stantelum range, this type has been incorporated into numerous communications and industrial equipments since its introduction in 1954. The range is Type Approved to RCS 134B

> | Temperature range | -40 to $+85^{\circ} \mathrm{C}$ |
| :---: | :---: |
| Voltage range | 6 to 150 V d. |

Capacitance range

Polarized types 0.3 to $200 \mu \mathrm{~F}$ Non-polarized types 0.15 to $100 \mu \mathrm{~F}$

## MINIATURE FOIL TYPE

Miniature Stantelum capacitors are a further development of the standard foil range. They have a space factor proportionate to their rated working voltage resulting in components of the smallest physical size. Available with axial or radial terminal wires

$$
\begin{array}{c|c}
\text { Temperature range } & -25 \text { to }+85^{\circ} \mathrm{C} \\
\text { Voltage range } & 3 \text { to } 25 \mathrm{~d} . \mathrm{c} . \\
\text { Capacitance range } & 1.5 \text { to } 16 \mu \mathrm{~F} \\
\text { Polarized types }
\end{array}
$$

## SOLID TANTALUM

Solid tantalum capacitors give up to three times capacitance, for a given rated voltage, as compared with the foil type capacitors. The range has been designed in line with MIL Specification C-26655-2

| Temperature range | $\begin{array}{c}-55 \text { to }+125^{\circ} \mathrm{C} \text { (with voltage derating. } \\ \text { Voltage range } \\ \text { Reto technical data sheets for details). } \\ \text { Capacitance range } \\ \text { Co } 35 \mathrm{~V} \text { d.c. } \\ \text { Polarized types. Sintered slug and solid electrolyte } \\ \text { construction }\end{array}$ |
| :---: | :---: |
| cor full details of these capacitors, ask for Technical. Data |  |
| For fieets from STC Capacitor Division, Brixham Road, Paiguton |  | Devon.

## miniature SELENIUM REGTIFIERS

The existing range of Miniature Selenium Rectifier Assemblies manufactured by the STC Rectifier Division has been extended. The previous range of miniature rectifiers included the "M" type and the "Q" and "MQ" Unistor. The term "Unistor" has now been dropped and the range widened to comprise the types below:

| Type | Description | Remarks |
| :---: | :---: | :---: |
| M | Single plate in aluminium case. | Half-wave device fitted to axial leads (Plate types 1 or 3 ). |
| T | One plate or two plates in aluminium case. | Half-wave device fitted to axial leads (Plate types 1, 3, 6, 8 or 9 ). |
| Q | Up to five plates in series in moulded nylon case. |  |
| MQ | As for $Q$ but hermetically sealed and tropicalised. |  |
| P | Up to five plates in moulded rectangular plastic case shaped for automatic insertion. | Available in halfwave, doubler, push, pull or bridge configuration, with multiple leads (Plate types 1, 3, 6, 8 or 9 ). |
| R | Is a skeleton form of $P$ for use in restricted space. |  |
| L | Cylindrical case in two sizes for up to ten or up to twenty plates. |  |

These SenTerCel Selenium Rectifiers are designed for use in electronic circuits calling for a diode of goed reverse/forward resistance ratio and closely controlled characteristics. When used in place of thermionic valves SenTerCel Miniature Rectifiers virtually eliminate problems of heat dissipation and a.c. hum, and save the cost of provision of heater power, valve bases and associated wiring. Being of small size they are easily accommodated in circuits and are suitable for most applications including modulators and demodulators, discriminators, logical circuits, limiting diodes, asymmetrical resistors, etc.


Full details are contained in Advance Information booklets "Miniature Selenium Rectifiers" and "Applications of Miniature Selenium Rectifiers", available from STC Rectifier Division, Edinburgh Way, Harlow, Essex.

## HIGH FREQUENCY CRYSTAL FILTERS

## 90 dB discrimination in 1 cubic inch

These are rugged, hermetically sealed panclimatic units designed primarily for AM and FM mobile radio working on 50,25 and $12.5 \mathrm{kc} / \mathrm{s}$ with an intermediate frequency of $10.7 \mathrm{Mc} / \mathrm{s}$. No circuit adjustments are necessary if terminations are within the stated tolerances. Brief details of characteristics are given below. For full information, apply to STC Quartz Crystal Division for Data Sheets.


445-LQU-901A
Pass Band Ripple: $\quad 2 \mathrm{~dB}$ maximum
Stop Band Discrimination:
70 dB minimum $\pm 35 \mathrm{kc} / \mathrm{s}$ 90 dB minimum $\pm 50 \mathrm{kc} / \mathrm{s}$ maintained over at least $\pm 300 \mathrm{kc} / \mathrm{s}$

## 445-LQU-901B

Pass Band Ripple: $\quad 2 \mathrm{~dB}$ maximum
Stop Band Discrimination: 70 dB minimum
$\pm 17.5 \mathrm{kc} / \mathrm{s}$
90 dB minimum $\pm 25 \mathrm{kc} / \mathrm{s}$ maintained over at least $\pm 300 \mathrm{kc} / \mathrm{s}$

## 445-LQU-909A

Pass Band Ripple: $\quad 1 \mathrm{~dB}$ maximum
Stop Band Discrimination: 60 dB minimum $\pm 50 \mathrm{kc} / \mathrm{s}$ maintained over at least $\pm 300 \mathrm{kc} / \mathrm{s}$

## 445-LQU-909B

Pass Band Ripple:
1 dB maximum
Stop Band Discrimination: 60 dB minimum $\pm 25 \mathrm{kc} / \mathrm{s}$ maintained over at least $\pm 300 \mathrm{kc} / \mathrm{s}$

A new publication, MQ/106, listing the standard ranges of STC crystals, is available from STC Quartz Crystal Division, Temple Fields, Harlow, Essex.

STC Microwave oscillators include:
$V$ Type Coaxial Line Oscillators and H -wave Oscillators with excellent frequency stability, a high degree of modulation linearity and low working voltages. No forced air cooling is required.
O Type (Y Codes) Backward Wave Oscillators with a very wide electronic frequency coverage.
Z Type Reflex Klystrons with a wide electronic tuning range and a high degree of modulation linearity.

Brochure MS/113, "STC Microwave Tubes", is available from STC Valve Division, Footscray, Sidcup, Kent.

## MIGROWAVE OSGILLATORS




DIMENSIONS, WEIGHTS AND RATINGS



The Mullard BYY15 Silicon Power Rectifier offers:

* Direct rectification of the mains
* High reliability factors
* Space savings
* PLUS lower costs

For the direct rectification of 250 V mains, with full voltage tolerance, the Mullard BYY15, a $20 \mathrm{~A}, 400 \mathrm{~V}$ silicon power rectifier, offers high performance and reliability at a really economical price.
It can be used in series or parallel combinations for output currents of more than 20 A and still show an appreciable saving over rectifiers with higher current ratings. From a 250 V supply a single phase bridge of four BYY15's gives an output current of 40A and a three phase bridge of six BYY15's gives 60A.

For full data on the BYY15, please write to the address below quoting reference M359.

## Mullard

MULLARD LIMITED Semiconductor Division Mullard House Torrington Place London WC1 Telephone Langham 6633


| Q Melers | $\begin{aligned} & \text { Type } \\ & 260 \text { AP } \\ & 190 \text { AP } \\ & 280 \text { AP } \end{aligned}$ | Freq. Range 50 KC to 50 MC 20 to 260 MC 210 to 610 MC | a Finge 10 to 625 5 to 1200. 10 to 25,000 | Tuning Cap. Aanga 30 to 460 uut 7.5 to 100 utf 4.0 to 25 uut | Q Accuracy <br> $50 \%$ to 30 MC <br> $7 \%$ to 100 MC <br> $20 \%$ to 610 MC |  | $\begin{aligned} & \text { Price } \\ & \text { £ } 370 \\ & \text { £ } 390 \\ & £ 950 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| O Comparators | $\begin{aligned} & \text { Type } \\ & 265 \text { A } \end{aligned}$ | Freq. Range 200 KC to 70 MC | 0 Range 30 to 500 | L Range 0.15 mh to 15 mh | C Range <br> $5 \mu \mu$ to $01 \mu \mu^{f}$ | R Range $500 \Omega$ to $20 \mathrm{M} \Omega$ | $\begin{aligned} & \text { Price } \\ & £ 318 \end{aligned}$ |
| FM-AM Signal Generalors | $\begin{aligned} & \text { Type } \\ & 202 \mathrm{E} \\ & 202 \mathrm{G} \\ & 225 \mathrm{AP} \end{aligned}$ | Freq. Range 54 to 216 MC 195 to 270 MC 10 to 500 MC | Output Range <br> $0.1 \mu \mathrm{~V}$ to 0.2 V <br> $0.1 \mu \mathrm{~V}$ to 0.2 V <br> $0.1 \mu \mathrm{~V}$ to 0.1 V | FM Mod, <br> 0 Ia 240 KC <br> 0 to 240 KC <br> 0 to 60 KC | AM Mod 0 to 50\% 0 to $100 \%$ 0 to $30 \%$ |  | $\begin{aligned} & \text { Price } \\ & £ 450 \\ & £ 440^{\prime} \\ & £ 478 \end{aligned}$ |
| Sweep Signal Generalors | $\begin{aligned} & \text { Type } \\ & 240 \text { AP } \end{aligned}$ | Freq. Range 4.5 to 120 MC | Output Range <br> $1 \mu \vee$ to $0.3 \vee$ Sweep <br> $1 \mu \mathrm{H}$ to $0.1 \vee \mathrm{VW} \& A M$ | Sweep Range $\pm 1 \%$ to $\pm 30 \%$ of conter freq. | AM Mod. $30 \%$ | Markers crystal and pip. | $\begin{aligned} & \text { Prlce } \\ & £ 728 \end{aligned}$ |
| Transistor Test Sel | $\begin{aligned} & \text { Type } \\ & 275 \mathrm{~A} \end{aligned}$ | $\alpha$-Range <br> 0.100 to 0.9999 | $\beta$-Range <br> 7 to 200 | $\begin{aligned} & \mathbf{H}_{\mathbf{i b}} \text { Range } \\ & 0.30 \text { to } 3000 \Omega \end{aligned}$ | \% |  | $\begin{aligned} & \text { Price } \\ & £ 374 \end{aligned}$ |
| RX Meters | $\begin{aligned} & \text { Type } \\ & 250 \mathrm{~A} \end{aligned}$ | Freq. Range 500 KC to 250 MC | R Range $15 \Omega$ to $100000 \Omega$ | C Range <br> 0 to 20 muf | L Range <br> $0.001 \mu \mathrm{~h}$ to 100 mh |  | $\begin{aligned} & \text { Price } \\ & £ 610 \end{aligned}$ |
| Signal Generator Calibrators | $\begin{aligned} & \text { Type } \\ & 245 \mathrm{C} \\ & 245 \mathrm{D} \end{aligned}$ | Freq. Range 500 KC to 1000 MC 500 KC to 1000 MC | Calibrated Input $0.025,0.05,0.1 \mathrm{~V}$ $0.025,0.05,0.1 \mathrm{~V}$ | Calibrated Output <br> 5,10 or $20 \mu \mathrm{~V}$ <br> $0.5,1.0$ or $2.0 \mu \mathrm{NV}$ | $\begin{aligned} & \% \text { AM Range } \\ & 10-100 \% \\ & 10-100 \% \end{aligned}$ |  | $\begin{aligned} & \text { Price } \\ & \text { £ } 158 \\ & \text { 154 } \end{aligned}$ |
| Univerters | $\begin{aligned} & \text { Type } \\ & 207 \mathrm{EP} \\ & 207 \mathrm{GP} \\ & 203 \mathrm{~B} \end{aligned}$ | Freq. Range <br> 100 KC to 5 MC <br> 100 KC to 55 MC <br> 100 KC to 25 MC | Output Range <br> $1 \mu \vee$ to 0.1 V <br> $1 \mu \mathrm{~V}$ to 0.1 V <br> $1 \mu \mathrm{~V}$ to $0.1 \vee$ | FM Mod. <br> 0 to 240 KC <br> 0 to 240 KC <br> 0 to 15 MC | AMB Mod. <br> 0 to 50\% <br> 0 to $100 \%$ <br> $30 \%$ | Accessory to $\begin{aligned} & 202 \mathrm{E} \\ & 202 \mathrm{G} \\ & 240 \mathrm{AP} \end{aligned}$ | Price <br> 1172 <br> £ 208 <br> £ 168 |

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A standard form of amplifier with a wide frequency response, and the additional facility of x 10 sensitivity when needed over a limited bandwidth.

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A-MP Taper Blocks, used in conjunction with A-MP Taper Pins, form the most practical method of providing from 10 connections upwards in the smallest possible space. The housings are of nylon for positive dielectric performance and mechanical strength. The blocks are made in basic units of $10,20,30$ and 60 cavities, and any combination of taper pin receptacles is possible in each block. They are designed for stacking to provide any desired capacity and thus afford the design engineer a remarkable degree of design freedom.
May we send you our new catalogue on Taper Technique?




Facing the fact nothing in series production is made regardless of ultimate cost, every manufactured article is a compromise. What matters, is "how much of one?"
There are better tape recorders than the new Brenell Mark 5 type M, but not many and not much. This new machine of ours is basically the well-established and highly-reputed Mark 5, but incorporates certain refinements and facilities which many an enthusiast will welcome. The fact that it is not a radical departure either in specification or functional styling, results from our policy of making a very good thing . . . and making it in such a way that by development even higher standards of performance and dependability may be offered.
88 gns. buys much more than the features listed below. It buys integrity and craftsmanship in design, component manufacture and individual assembly. The kind of quality these represent, is so very close to perfection yet so comparatively inexpensive that one would need more affluence than critical concern in order to fault it.
A demonstration will show " the finest compromise in the world "to be a supportable and worthwhile claim. And if your demands or price inclination are more modest, the original Mark 5, at 64 gns., continues to be available.

Separate recording and replay heads and amplifiers. The replay amplifier may be used for tape monitoring during recording: the tape passes across the replay head a fraction of a second after recording.

## Ifrenell

MARK 5: 64 GNS. MARK 5 STEREO: $\mathbf{\text { C99.12.0 MARK } 5 \text { DECK: }}$ 28 GNS. 3 STAR 58 GNS. ( $\ddagger$ track model ovailable). 3 STAR STEREO: 89 GNS. (additional $\frac{1}{4}$ track replay focilities E12 extra)

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Fully ceramic construction.
Longer life expectancy.
Higher seal temperature ratings.
Plug-in replacement for
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## MEDIUM POWER

## TETRODES



SELECTION FROM EIMAC RANGE

| TYPE | ANODE DISSIPATION (Watts) | FREQUENCY FOR MAX. RATINGS (Mc/s) | BRIEF DESCRIPTION |
| :---: | :---: | :---: | :---: |
| $\begin{aligned} & 4 \times 150 \mathrm{~A} \\ & 4 \times 150 \mathrm{D} \end{aligned}$ | $\begin{aligned} & 250 \\ & 250 \end{aligned}$ | $\begin{gathered} 150 \\ 150 \\ 500 \text { (C.W.) } \end{gathered}$ | 26.5 v . heater version of $4 \times 150 \mathrm{~A}$. |
| 4X150G | 250 | 1,500 (pulse) | U.H.F. version of 4X150A |
| 4X250B | 250 | 500 | Improved $4 \times 150 \mathrm{~A}$, partly cerámic construction. |
| 4C×250B | 250 | 500 | Improved 4X250B, fully ceramic. |
| $4 \mathrm{C} \times 250 \mathrm{~F}$ | 250 | 500 | 26.5 v . heater version of 4 CX 250 B (Modern 4XI50D). |
| 4CX250K | 250 | 500 (C.W.) <br> 1,500 (pulse) | U.H.F. version 4CX250B (Modern 4XI50G) |
| 4 CX 250 M | 250 | 500 (C.W.) <br> 1,500 (pulse) | 26.5 v . heater version of 4 CX 250 K . |
| 4 CX 300 A | 300 | 500 | Rugged tube, stacked ceramic construction. |
| 4CNI5A | 15 | 500 | Pulse version 4CX300A; smaller, lighter. |
| 4C×125C | 125 | 500 | 4CX300A with different cooler system. |
| 4W3008. | 300 | 500 | Water cooled version 4×250B. |

SOME NEW TYPES

| Y249 | 250 | 150 | Rugged 4X150D. |
| :--- | :--- | :--- | :--- |
| Y252 | 250 | 500 | Rugged 4CX250B. |
| Y253 | 300 | 500 | Rugged 4W300B. |


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The top model of its class, designed for the professional user. A recorder with quality features which will attract the interest of radio, television, and motion-picture studios, as well as the disc-recording industry. Tape speeds $7 \frac{1}{2}$ and 15 i.p.s.
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## meters

## DC Microvoltmèter; type GM 6020

Imprit.
Measuring rangei, $100 \mu \mathrm{~V}$ (fis.d.)
10 V inull steps
Input impedanceg I $\mathrm{M} \Omega( \pm 1.5 \%)$
in parallel with
$-20 \mu \mu \mathrm{~F}$
Imput II
10 mV (f.s.d.) 1000 V in 11 steps $100 \mathrm{M} \Omega( \pm 1.5 \%)$ in parallel with $10 \mu \mu \mathrm{~F}$

Overall aceuracy with respectito fall scale: $3 \%$ Pre-deflection $i<5 \mu \mathrm{~V}$
Drift: $<1 \mu \mathrm{~V}$ per hour after 1 hour of warming.up
Antomatic polarity indication doubles the effective scale length with respect to centre-zero instruments. DC currents may be measured directly with this instrument due to the high accuracy of the inpat resistance.
Measuring range; $100 \mu \mu \mathrm{~A}$ (f.s.d.) $-10 \mu \mathrm{~A}$. Aceuracy: $<3.5 \%$

## Broadband Millivoltmeter, type. GM 6012

Prequency range: $2 \mathrm{c} / \mathrm{s} \cdot 1 \mathrm{Mc} / \mathrm{s}$
Measuring ranges 1 mV (f.s.d.) 300 V in 12 steps dB seale: .80 dB up to $+52 \mathrm{~dB}(0 \mathrm{~dB}=1 \mathrm{~mW}$ into $600 \Omega)$.
Input impedances $4 \mathrm{M} \Omega$ in parallel with $20 \mu \mu \mathrm{~F}$ (up to 3 V ) $10 \mathrm{M} \Omega$ in parallel with $10 \mu \mu \mathrm{~F}$ (in the other ranges).
Overall aceuracy with respect to full scales
${ }^{\prime}$ within $\pm 2,5 \%, 5 \mathrm{c} / \mathrm{s} \quad 100 \mathrm{kc} / \mathrm{s}$
within $\pm 5 \% ; 2 \mathrm{c} / \mathrm{s} \cdot .1 \mathrm{Mc} / \mathrm{s}$
Pre-deflection: $<100 \mu \mathrm{~V}$
High Frequency Millivolimeter, \&ype GM 6014

Without
pre-attenuator
Frequencȳ Fange: $1 \mathrm{kc} / \mathrm{s} \cdot 30 \mathrm{Mc} / \mathrm{s}$
Measuring ranges 1 mV (f.s.d.).
300 mV in 6 steps • 30 V in 6 steps
dB scale:
Damping at 1, ké/s
$1 \mathrm{Me} / \mathrm{s}:$
$30 \mathrm{Me} / \mathrm{s}$ :
Me/s $-700 \mathrm{k} \Omega$
Input capacitancè: $7 \mu \mu \mathrm{~F}$
$-2 \mathrm{M} \Omega$
Pre-deflection: Compensated by electrical zero setting
Variations of the frequency characteristics:
$<5 \%$ over the whole range, with respect to the response at the frequency of the calibration voltages.
Ocerall accuracy: < $3 \%$ with respect to full sciale"añd with reference to the frequency characteristic.

## With

pre-attenuator' $10 \mathrm{kc} / \mathrm{s} \cdot 30 \mathrm{Mc} / \mathrm{s}$ 100 mV (f.s.d.) 40 dB up $10+32 \mathrm{~dB}$ $50 \mathrm{M} \Omega$ $10 \mathrm{M} \Omega$ $2 \mathrm{M} \Omega$ $2 \mu \mu \mathrm{~F}$

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## Compact

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A two-speaker model complete with treble volume control. Cabinet size $23 \frac{1}{2} \times 14 \times$ 12 in .
Weight 37lb. complete Impedance 15 ohms. Max. input 15 watts £29/10/- complete, tax free.

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A four-speaker system complete with mid-range and treble volume
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Cabinet size $35 \times 24 \times 12 \mathrm{in}$. Weight 65 lb . complete. Impedance 15 ohms. Max. input 15 watts. £49/10/- complete, tax free.


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HEATERS:
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REPEATABILITY: EXPOSURE:

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INSTANT RESET:
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From .2 to 500 seconds.
From .5 to 230 volts AC or DC 2 to 6 watts.
Fully compensated from
$-65^{\circ} \mathrm{C}$. to $+125^{\circ} \mathrm{C}$.
Precision Types to $\pm 1 \%$.
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Types suitable for up to
$20 \mathrm{~g} .2,000 \mathrm{c} / \mathrm{s}$.
Special Types can repeat d
oletion of previous cycle.
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Weight $\frac{2}{3}$ to $\ \frac{1}{2}$ ozs.
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PORTABLE TRANSISTOR
A.C.
$V$
$O$
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$T$
$M$
$E$
$T$
$E$
$R$


Measures $50 \mu \mathrm{~V}$ to 500 V . on 12 ranges.
Response $\pm 3 \mathrm{~dB}$ from $6 \mathrm{c} / \mathrm{s}$. to $250 \mathrm{kc} / \mathrm{s}$. High input impedance and low noise level.
Can be used as an amplifier with gain up to 80 dB .
Type TM2B
LEVELL ELECTRONICS LTD. 10-12 ST. ALBANS RD., BARNET HERTS.


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Write for free descriptive leaflet.

## GEVASONOR

MAGNETIC TAPE

[^9]
## "SIMPLEX" SOUND HEADS

## STANDARD $\frac{1}{2}$ TRACK MONAURAL

$R / P$
Gap .0002. . 55 Inductance at I.Kc. 7.5 MV. Output at I Kc. Fully Modulated Tape.

## TWO NEW HEADS FOR TRANSISTOR OPERATED EQUIPMENT

## TYPE: HI-LO RECORD PLAY $\frac{1}{2}$-TRACK

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Standard "Simplex" mounting and physical dimensions.
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Triple gap Erase Head working on a completely original principle designed for extremely efficient operation from a low voltage D.C. source, i.e., dry battery $4-6 \mathrm{v}$.
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[^10]

## Brief Technical Data

Operating carrier frequency 3,000 c.p.s. $\pm 5 \%$
Minimum Input signal 50 mV R.M.S.
Input. Impedance । Megohm.
Input amplifier bandwidth -3 db at 2,500 and 3,500 c.p.s.

Effective limiter range $\pm 10 \mathrm{~dB}$
Meter scaling-"Peak wow" 0 to $\pm 1 \%$ (centre
" wero). "
R.M.S

Crossover frequency 20 c.p.s.
Flutter " meter response-3db at crossover.
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Wow meter response _IdB at 0.5
C.R.O. output frequency response level down to zero frequency -3 dB at 200 e ep. s .
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## Common-Emitter Amplifier



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## ARTICLES

IN THE SEPTEMBER ISSUE INCLUDE:

Symbolic Logic
Elementary Boolean algebra is explained simply and its application to the design of computer circuits is discussed. Examples are given of how the states of a number of flip-flops may be represented. It is shown that algebraic simplification of the equations is reflected in circuit simplification.

Transistor Current Gain at U.H.F.
This article describes how a coaxial-line system and a twin-channel comparator are used to determine amplitude and phase variations of transistor current gain. The results in the frequency range 300 to 800 $\mathrm{Mc} / \mathrm{s}$ are then compared with values obtained by a bridge method.

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one $9 \times 5$ in．speaker ．．．．．．．．．．． 25 gns．
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Transistor Travelling Superhet＂Trabant T 6＂Technical Data：Power supply 2 flat batteries 4.5 volts－Working voltage 9 volts max．Power consump－ tion ca． 12.5 mA at 8 volts without modulation－Semi－ conductor
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2 transistors，

- Receiving
2 $\underset{\text { ranges }}{\text { germanium diodes }}$ short， －Receiving ranges short， tuning planetary drive with tuning planetary drive with them variable－Intermediate frequency 460 kilocycles－AVC acting on the first intermediate frequency transistor，additional attenuating diode in parallel with the first intermediate fre－ quency circuit－LF final stage $\geqq 300 \mathrm{~mW}$－Loudspeaker permanent dynamic oval speaker $\ldots$ VA－Aerials ferrite aerial for medium and long wave，tele－ scopic aerial for short wave－Housing unbreakable wooden housing coated with coloured material－Dimensions $10 \frac{1}{8} \mathrm{in} . ~ \times$ 7 tin．$\times 3 \frac{5}{⿱ 亠 䒑}$
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| BRIEF SPECIFICATION |  |
| :---: | :---: |
| RATIMGS | Heater Voltage (Volts) $5 \pm 5 \%$ <br> Meater Current (nominal) (Ampa) 5 <br> Absolute maximum PIV surpe fating (kV) 20 <br> Muimum Mean Cathode Current (Amps) 3 |
| MOUMTIMG POSITIOM | Base Down (Vertical) |
| MAXIMUM DIMENSIOMS | Overall Length 248 mm Diameter 51 nam Seated helch 240 mm |

If you want to know more about this valve and discuss its application to your own equipment-write to us

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## 11 <br> Bellina-Lee"

 COAXIAL PLUGS \& SOCKETSSafe-tough-and fitting all standard input sockets of British television sets, this well-known co-axial plug fully meets the growing requirement for domestic equipment which is intrinsically safe, i.e., completely isolated from supply mains.
All exposed portions of the body are shrouded in black nylon which, besides being an excellent insulator, possesses great mechanical strength. This connector will support the full weight of a grown man without breaking.

Specification:

## B.S. 3041 :1958.

Cable loading:
Coaxial, $\frac{1}{1}$ in. to $\frac{3}{16}$ in. overall dia.; inner conductor 0.048 in . max. dia.
U.K. Patents: 679410,695439.
$\begin{array}{ll}\text { L734/P/AI } & \text { Free Plug } \\ \text { L734/J/AI } & \text { Free Socket }\end{array}$
"Belling-Lee" coaxial connectors are designed to provide the most efficient general purpose terminations possible for solid dielectric or semi-air-spaced cables between $\frac{1^{\prime \prime}}{8}$ and $\frac{5}{16}$ " outside diameter.

L604/S/Cd Fixed Socket L734/S Fixed Socket (Flush Mtg.) L603 Insulated Fixed Socket
L617 Bulkhead Adaptor
Ll42! Bulkhead Socket
L616 Line Coupling

These are the connectors on which the RECMF standards and subsequently BS plugs and sockets were based.

Telephone: Enfield 5393 - Telegrams: Radiobel, Enfield

## "BELLING-LEE" NOTES

No. 32 of a Series

## Some mechanical aspects of

 design: Part 5.Having indicated the more important aspects of contact design, we come to the insulator on which they are mounted. In a simple connector this may consist of a plate of suitable material, but more intricate components call for complex shapes which, if production quantities warrant it, are conveniently obtained by moulding techniques.

Confining ourselves to the vast range of materials which are covered by the omnibus title of "plastics," these may be broadly classified in two main categories, the thermo-plastics, and those which are thermo-setting. The former can always be softened by heating and can then be reshaped, but the latter, after initial moulding and curing, do not become plastic when re-heated; they may be distorted, and ultimately they blister, char, and undergo a radical change in composition and properties. Thermoplastic materials are also damaged by excessive heating, of course.

The temperature at which thermoplastics soften is relatively low (mostly well below $150^{\circ} \mathrm{C}$ ), and this does impose some limitation on the range of applications to which they can be put. Apart from overall changes of configuration which they experience at elevated temperatures, metal inserts may become displaced in the process of soldering unless a certain amount of care is exercised. Some types even suffer a change of shape at ordinary room temperatures under very light pressures which may be no more than their own weight. This is called "cold flow," and pitch gives a striking demonstration of the effect; obviously such materials are mechanically unstable and useless for making precision parts.

Apart from the characteristic limitation however, there are a number of thermo-plastic materials which possess excellent electrical properties, and, due to this and the comparative ease with which they can be moulded (relatively low pressures as well as temperatures are involved), they have achieved widespread use as electrical insulators for moderate temperature work. The most important of these are cellulose acetate, polystyrene, polyethylene, poly-vinyl chloride, nylon, and now polypropylene. Thermo-setting materials require higher moulding temperatures and pressures, and have higher working temperatures, and greater mechanical rigidity, but electrical characteristics which are less good than the best of the thermo-plastics, being markedly inferior at very high frequencies although many of them make excellent insulators for medium and low frequency applications.
(To he continued)
Advertisement of
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Written 18th July, 1961

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 THE IUSICUnfair to flautists! If you stifle the input with a poor microphone, you trifle with the output from the speaker. Do the right thing by the performer and the composer, by the tape recorder and by your ear. Use the right microphone. Use an Acos microphone. An important new one has recently been added to the range.

MIC 45



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| Brald | Bonding, Impregnating or Coating Material | Temperature Category | Dielectric Strength |
| :---: | :---: | :---: | :---: |
| Terylene | Varnish (Oi! Based) | $\stackrel{120 \mathrm{C}}{\mathrm{Class} \mathrm{E}}$ | 3.000 V . |
| Cotton or Rayon | Varnish (Oll Based) | $\begin{gathered} 105 \mathrm{C} \\ \text { Class A } \end{gathered}$ | $\begin{aligned} & 1,500 \mathrm{~V} \text {. or } \\ & 3.000 \mathrm{~V} \text {. } \end{aligned}$ |
| Glass <br> Braid | Varnish (Oil Baserl) | 120 C | $\begin{aligned} & i, 500 \mathrm{~V} \text {. or } \\ & 3,000 \mathrm{~V} \text {. } \end{aligned}$ |
| G'ass | P V.C. | ${ }_{\text {Class B }}^{130 \mathrm{C}}$ | 5.000 V . |
| Glass | Silicone Resin | $\begin{aligned} & 250 \mathrm{C} \\ & \text { Ciass H } \\ & \hline \end{aligned}$ | 800 V . |
| Glass | Nong (Heat treated) | 450 C | 600 V . |
| Giass | Identification Oye | $\begin{gathered} 450 \mathrm{C} \\ \text { (Colous5 } \\ \text { lade } 180 \mathrm{C} \text { ) } \end{gathered}$ | 600 V . |

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Ask for a leaflet describing the HF156 and the additional facilities for vehicle-borne operation and for power supply from lead/acid accumulators or dry batteries.

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# Aspects of design 

## SERIES REGULATOR

VALVES IN STABILISED POWER SUPPLIES

Fig. 1 illustrates the circuit of a typical Stabilised Power Supply employing a series regulator valve $V_{1}$, triode connected, a simple pentode shunt amplifier $V_{2}$ and a gas discharge tube $V_{3}$ as a voltage reference. A fraction of the output voltage, determined by the setting of VR1, is compared with the voltage at $\mathrm{V}_{3}$ and the difference, amplified by $V_{2}$ controls the bias and hence the impedance of the valve $V_{1}$. Thus the series valve $V_{1}$ must accommodate variations of input volts, output volts and output current by changes of "anode to cathode " and "grid to cathode" volts, and these voltage excursions must be made subject to the following limitations:
(a) $V_{1}$ must not pass positive grid current.
(b) The rated voltages and dissipations must not be exceeded.
The design specification of a stabilised power supply should include a statement of the following:

1. The required maximum output voltage $\mathrm{V}_{\max }$
2. The required maximum output current $l_{\max }$
3. The input mains voltage variations to be accommodated
4. The regulation characteristic of the input rectifier circuit which will include a value of ripple voltage and the probable spread of output voltage due to production tolerances in rectifier and circuit components.
From this specification the working point of $\mathrm{V}_{1}$ is determined so that the anode to cathode voltage is as low as possible consistent with conditions ( 2 ) and (a) above. This ensures that the anode voltage and the effects of input voltage variations are at a minimum.


FIG.I

Start of positive grid current in a thermionic valve usually occurs at a grid potential between -1 V and 0 , and $V_{1}$ must therefore be capable of passing $\mathrm{I}_{\text {max }}$ throughout its life at a bias greater than -1.0 V . A limit is thus set on the minimum anode to cathode voltage of $V_{1}$ which is determined by constructing an "end of life limit" curve on the $I_{3} / V_{3}$ characteristic. In the absence of other information this can be approximated by a reduction of the anode current by $35 \%$ at all parts on the published $\mathrm{I}_{\mathrm{I}} / \mathrm{V}_{\mathrm{B}}$ curve for $\mathrm{V}_{\mathrm{g}}=-1 \mathrm{~V}$. This is shown by the curve $A B$ on Fig. 2 which gives the characteristics of a typical series regulator valve. The intersection of this curve with $I_{\text {max }}$ shows the minimum anode to cathode voltage of $\mathrm{V}_{1}$. Added to $\mathrm{V}_{\mathrm{max}_{\mathrm{s}}}$, this figure gives the output required for a low limit rectifier at the trough of the ripple cycle when the mains input is at a minimum. Then from the specification (4) for the rectifier circuit, the locus of the change of rectifier output volts with low limit rectifier at low mains volts is calculated and is shown plotted as curve CD in Fig. 2. The intersection of curve $C D$ with the voltage axis at $C$ shows the low limit of input volts, and from this the nominal and maximum mains input volts are calculated.

The rectifier output locus for a high limit rectifier at high mains volts is drawn as curve EF in Fig. 2, intersecting $\mathrm{I}_{\text {max }}$ at point $F$ which must lie to the left of point $G$, the intersection of $I_{\text {max }}$ with the maximum dissipation line. FG represents the permissible range of output voltage at $I_{\text {max }}$ before the maximum dissipation is exceeded. The corresponding range at any lower current can be obtained by drawing the same high limit locus through the point of intersection of the required current and maximum dissipation lines.

The lowest output current obtainable from the supply is a function of the maximum bias of $V_{1}$ and is determined by the

Associated Electrical Industries Ltd
Radio and Electronic Components Divlsion Technical Service Department Tol: TEMple Bar 8040 Grams: Assocelect London
intersection of the GH locus with the relevant $I_{a} / V_{B}$ characteristics. This figure is that of a high current or long grid base limit valve which, in the absence of other information, can be approximated from the corresponding published curve by a shift in anode volts of about $-15 \%$.
The maximum bias of $\mathrm{V}_{1}$ is either the maximum permitted by the voltage ratings of $\mathrm{V}_{1}$ or the maximum available from the output of $\mathrm{V}_{2}$. The latter value is set by the conditions that (1) $V_{2}$ shall not operate below the knee of its $I_{8} / V_{a}$ characteristic, and (2) it shall not run with positive grid current flow. Violation of either of these conditions results in serious loss of amplifier

gain. Condition (1) is only of importance when the volts across $\mathrm{V}_{2}$ are less than 100 V . Condition (2) depends to some extent on the value of $R_{L}$ and a large value of this resistor reduces the likelihood of positive grid current flow. On the other hand, too large a value may mean that $\mathrm{V}_{2}$ operates near its cut-off and the effects of negative grid current in $\mathrm{V}_{1}$ are greater. The anode current of $V_{2}$ should be substantially greater than the maximum negative grid current of $\mathrm{V}_{1}$.

## EXAMPLE

Given (1) Maximum output voltage 250 V
(2) Maximum output current 120 mA
3) Mains variation $\pm 10 \%$
(4) Rectifier circuit having an output impedance ( $r_{s}$ ) of $500 \Omega \pm 10 \%$ and a ripple voltage of 5 volts peak at 120 mA . (This can be only a tentative specification at this stage because the input volts are not yet determined).
Using an S11E12 as the series valve:
Maximum anode watts (triode connected)
30 W
Max. screen grid voltage 300 V
Max. control grid volts
Minimum anode to cathode volts (see curve AB ) 96 V
Minimum rectifier output (allowing 5 V peak ripple) 101 V
Maximum volts drop in rectifiera t $120 \mathrm{~mA}\left(=I_{\max } \mathrm{r}_{\mathrm{s}} \times 1.1\right) 66 \mathrm{~V}$
Minimum input volts $=66+101+250 \quad 417 \mathrm{~V}$
Maximum input volts
510 V
Nominal input volts 464 V
Nominal volts across $\left.\mathrm{V}_{1}\right\}$ (see locus JK) 154 V
Nominal bias volts on $\left.\mathrm{V}_{1}\right\}$
17 V
Minimum volts drop across rectifier at 120 mA
( $\mathrm{I}_{\text {max }} \mathrm{r}_{\mathrm{s}} \times 0.9$ )
54 V
Maximum rectifier output at $120 \mathrm{~mA} \quad 456 \mathrm{~V}$
Maximum volts across series valve
206 V
Therefore output voltage may be reduced 44 volts before 30 W are dissipated.

At 10 mA a high limit valve would require a bias of -80 V which is well within the requirements for maximum bias of $V_{1}$.
A reasomable anode current for $\mathrm{V}_{2}$ would be .5 mA giving an anode load of $270 \mathrm{k} \Omega$.

## NEW TRIODE TETRODE FOR <br> MAZDA 30FL13

The 30FL13 consists of a high slope tetrode with frame grid construction and a general purpose triode for use in television sync. separator circuits. The short grid base and high slope of the tetrode enable good pulse limiting to be obtained with the anode load resistance directly connected to the HT line and a fairly high screen voltage.

The triode has identical characteristics to the 6/30L2

$$
\begin{array}{llllr}
\text { Heater current (amps) } & \text {. } & \text {. } & \mathrm{J}_{\mathrm{h}} & 0.3 \\
\text { Heater voltage (volts) } & \text {., } & \ddots & \mathbf{V}_{\mathrm{h}} & 10.0
\end{array}
$$

## TENTATIVE RATINGS AND DATA

| mum Design Centre | ings | $\begin{gathered} \text { Triode } \\ 1.5 \end{gathered}$ | Tetrode |
| :---: | :---: | :---: | :---: |
| Anode Dissipation (watts) .. $\mathrm{pa}_{\mathrm{a}}($ max $)$ |  |  |  |
| Screen Grid Dissipation (watts) | $\mathrm{Pa}_{2}($ max $)$ |  | 0.5 |
| Anode Voltage (volts) | $\mathrm{V}_{3}(\mathrm{max})$ | 250 | 250 |
| Screen Grid Voltage (volts) | $\mathrm{V}_{\mathrm{E} 2 \text { (max }}$ ) |  | 250 |
| Heater to Cathode |  |  |  |
| , |  |  |  |

Inter-Electrode Capacitances $f(\mathrm{pF})$

|  |  | Triode | Tetrode |
| :---: | :---: | :---: | :---: |
| Input | $\mathrm{c}_{\text {f }}$ | 2.3 | 10 |
| Output | Cout | 2.0 | 2.6 |
| Control Grid to Anode | $\mathrm{C}_{\mathrm{g}-\mathrm{s}}$ | 2.4 | 0.04 |
| Grid Triode to Grid 1 Tetrode | $\mathrm{C}_{\mathrm{gt} \text { t-gl }}$ |  |  |
| Anode Triode to Anode Tetrode | $\mathrm{c}_{\mathrm{a}-\mathrm{aq}}$ |  |  |
| Grid Triode to Anode Tetrode | $\mathrm{c}_{\mathrm{kt}} \mathrm{s}^{\text {q }}$ |  |  |
| Anode Triode to Grid 1 Tetrode | $\mathrm{c}_{\text {st-gl }}$ |  |  |

## TETRODE CHARACTERISTICS



## TRIODE CHARACTERISTICS

Anode Yoltage (volts)
Anode Current (mA)
Mutual Conductance ( $\mathrm{m} \mathrm{A} / \mathrm{V}$ )
Amplification Factor
Mounting position: Unrestric
Base: B9A (Noval).
Connections:


Maximum Dimensions (mm)

| Overall Length | .. | .. | .. | .. | 56 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Seated Height | .. | .. | .. | . | 49 |
| Diameter | .. | .. | .. | . | .. |
| 22.2 |  |  |  |  |  |

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102 and 103

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| :--- |
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900 ft 5 5 in . Std. Play
$16 /-$ 1,200ft. 5 5in. Long Play 19/6 1,800 tit. $5_{1}^{3}$ in. Dble. Play $37 /-$ 1,200tt. 7in. Std. Play 21/$1,800 \mathrm{ft}$. 7in. Long Play $28 / 6$ 2,400ft. 7in. Dble. Play 47/3 in . D.P. message tape 400 ft . with spare spool $10 / \mathrm{F}$ Many other types available including "Scotch,", "EMI," " Triton," " Synand Accessories. RE-ENTRANT LOUD HAILERS


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This armplifer is built to the very higheat technical standards and presented atrictly $t^{0}$ Mwo of the pew triode-pentodes, type ECL86, oomplete Mullard valve line-up including two of the new triode-pentodes, type ECL86, in each channel. Two specially designed output stages for ultra linear operation.
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AS ADDIO SPECLALISTS WE CONFIDENTLY RECOMMEND THIS DESIGN it is a MUST to the serious minded sound enthusiast.
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$650+J 4500$ ohms. SECONDAR Impedance $650+\mathrm{J} 4500$ ohms. SECONDARY
(Rotor) 1 -phase. Max. coupling voltage 57.3. (Rotor) 1 -phase. Max. coupling voltage 57.3 .
Phase lead $6^{\circ}$ Output impedance 700 ohms d.c.
Length overall $2 \frac{7}{7}$ in. Width 1 ti in. Spindle dia. $\frac{10}{6}$ in Weight 4.2 oz . Rotor inertia .014 amps in. ${ }^{3}$-Max frictional torque .45 oz . in. Max. electrical error $\pm 7 \mathrm{ft}$ Manufactured to Bu of Ord Spec: commercia equivalent type 11 C 2 A 1 .

## Type CT4

$£ 6$

en Dins DRAG CUP MOTOR Type HM2/3/D
20 volts, 2 -phase, $400 \mathrm{c} / \mathrm{s}$, 4 -pole. Incorporates $530-1$ ratio gearbox terminating in poindle. Torque at rotor $7.5 \mathrm{gm} . \mathrm{cm}$. Moment of inertia $3.2 \mathrm{gm} . \mathrm{cm}^{2}$ : Starting $7.5 \mathrm{gm}, \mathrm{cm}$. Morment of inertia 3.2 gm . cm . Impedance n5 200 ohms . Max torque demand $100 \mathrm{gm} . \mathrm{cm}$. Length overall 2 tin. Width (at flange) 100 gm . Weight 2 oz .

MINIATURE CONTROL MOTOR Type IIM50C
input $13 / 26$ volts $400 \mathrm{c} / \mathrm{s}$. Output 6,700 \&5 .p.m. at 26 vols. Min. stall torque 42 gm . cm . Stall current $204-250 \mathrm{~mA}$. Max. input Widh 1 Plain shaft spindle tin. dia Stainless steel encased. Low loss connector block. New.
 COLD CATHODE TRIGGER TUBES Sub. miniature cold cathode valve developed by Ericsson primarily or computer work. Anode-cathode running voltage of 95 to 140 at 4.5 mA , and at 290 anode volts require a trigger current of only 250 microamps to cause the anode to take over the discharge. Typica ionization time: 90 microseconds. Will withstand up to 310 volts
with zero trigger voltage without self-igniting. Complete with full with zero trigger voltage without self-igniting. Complete with ful performance data in original packs of 100 at the special price of $\mathbf{E 5 , 0} 0$ Minimum quantity supplied: 6 for 10/- Post paid.

Post paid.

## ELECTRIC

## ACTUATORS

Special offer of aircraf quality, precision engineered rotary actuators by leading British manufacturers. In new or first-class used condition. For 24 volt operation.
TYPE 2
Split field, series wound, reversible motor fitted with electro-magnetic brake. Max. load $50 / 60 \mathrm{lb}$./in. Output $0.02 \mathrm{h.p}$. at 13,000 r.p.m Reduction gear ratio 2,857 to 1 . Length 7 in. Weight 2 tib. Fitted with adjustable limit switches.

75/ - Post paid.
TYPE 3

ration of 3-positionof angular settings determines in which actuator gives wide variety 50 lb . in. Output 0.017 h.p. at 17,000 r.p.m. Full range travel: 140 deg. in 2 seconds Weight 3.25 ib

75/- Post paid.
TYPE 5
Two-pole,split series wound motor. Fitted with doubleplate friction clutch. Speed of motor 11,000 r.p.m.reduced through epicyclic and worm gears to 60 deg rotation of right-angled drive shaft in 3 sec.
Consumption 3 amps.


## - BARGAIN OFFERS

VCR139 (Cossor 23D equivalent) $2 \frac{1}{2}$ in. cathode ray tube 15/Postage $2 / 6$
Mains suppressor in diecast sealed case, 2 for 5/-. Postage $2 /$ Double pole knife changeover switch on porcelain base, 2 for $4 /$ Postage $1 /$-.
Pyrex aerial insulators, four 3in. OR one 7in., 6/-, Postage $1 / 6$ Neons, ten 115 volt for $19 /-$. Postage $2 / 6$. Siz 80 volts for $6 /$. Postase $1 / 6$
Bulgin type " M " microswitches, 4 for $10 /$-. Postage $1 / 6$
Metal rectifiers: selenium $6-12$ volt $1 \frac{1}{2}$ amp., $9 / 6$. $2 \frac{1}{2} \mathrm{amp} ., 9 / 6$ Metal recti
4 amp . $16 / 6$.
4 amp., $16 / 6$. Charging transformers: Pri
at 4 amps., $18 / 6$. Postage $3 /-$
STC Miniature Silicon Diodes, input 50 v . peak inverse; output 15 v. 0.5 amp . D.C., 4 for $10 / \mathrm{F}$. Post paid.

## ELECTRONIC IGNITION ANALYSER

Versatile, portable equipment specially designed for the critical analysis of aero-engine ignition systems. Displays entire performance of ignition system on a cathode ray screen while engine is running-simultaneously showing each plug firing in a side by side comparison. (Reveals excessive carbon formation, faulty condenser, leaking cables, incorrect plug or contact breaker gap, worn cams, etc. Ten-step loading switch absorbs energy from system and thus accentuates test to show-up deterioration in coil primary, secondary winding, condenser, cables, etc. Straightforward connection to system. Power supply can be switched to either $230 / 250$ volts A.C. mains, or 6,12 or 24 volts D.C. In attractive metal case $9 \times 133 \times 173$ in. deep. Complete with circuit, instructions and good and faulty trace drawings. Guaranteed serviceable.
£15.0.0 $\qquad$


## APNI TRANSDUCER

Consists of magnet and coil which is attached to an aluminium diaphragm suspended freely and perforated to prevent air damping. A and perforated to prevent air day over diaphragm to form 2-gang over diaphragm to form
capacitor having swing of $10-50$ p. f . Widely used in wobbulator circuits, Wide
etc.

## INVERTORS

28 volt DC to 115 v .3 phase $400 \mathrm{c} / \mathrm{s}$ AC. Type 102A Output 625 VA . Brand new and complete with type $34(5 \mathrm{UC} / 5820)$ voltage and frequency control unit. $\$ 15.0 .0$ Carriage $10 / \mathrm{F}$ 28 VOLT DC to 115 v . 1 phase AC Self contained motor generator unit with complementary carbon pile voltage regulator, contactor and associated rectifier in separate compartment on same base. Continuously rated for $25 / 28$ volts D.C.
input with 360 VA output at 115 volts single phase A.C. at 1,600 input with 360 VA output at 115 volts single phase A.C. at 1,600 cycles with a power factor of 1.0 . Fan cooled with end plate for
blast or internal cooling as required. Type 200. Ref. 5UB/5083. blast or internal coolin
In first class condition.
£4.10.0 Carriage 7/6.
200/220 Volts D.C. to 200/250v. 1 phase $50 \mathrm{c} / \mathrm{s}$ AC.
Output 260 watts. New, in sound-proof cabinet
£9.0.0 Carriage $10 /$-.
24 volt DC to 26 v .1 phase $400 \mathrm{c} / \mathrm{s}$ AC.
Output 6VA. Size $2 \frac{1}{6} \mathrm{in}$. dia. 4in. long $1 \frac{1}{2} \mathrm{in}$. high pedestal base Instrument quality. AS NEW. $27 / 6$ Carriage paid.

28 volt DC to 115 volts 1 phase $400 \mathrm{c} / \mathrm{s}$ AC.
Output 50VA. Size $7 \times 4 \times 5 \mathrm{in}$. high. In black crackle case on antivibration mounted pedestal base containing condenser filter. Fan cooled.

As new. 24.10 .0 Carriage $5 /$ -
PRESSURE INDUCTANCE
TRANSDUCER
£2.10.0
By J. Langham Thomp-
son Ltd., covering range
Post paid. $0-500 \mathrm{lb}$. sq . in.
Machined aluminium block contains integral diaphragm, standard BSP connection, and bleed hole. Diaphragm movement determines gap between wire-wound inductance in sintered housing and remote gap between wire-wound inductance insintered housing and remote



## SYNCHRONOUS

 CLOCK MOTORS $\begin{array}{ll}\text { Postage and } \\ \text { packing } 1 / 6 . & 8 / 6\end{array}$Brand new, standard, 200/250 volts, 50 cycles, a.c. mains operated synchronous motors by Sangamo Weston. Fitted with siandard clock drive spindle.

## HI-FI STICK

 MIKE Type 39-1 Acros directional, highly sensitive. Response substantially flat to $10 \mathrm{kc} / \mathrm{s}$. Load resistance $5 \mathrm{M} \Omega$.New, Boxed
w, Boxed Post paid. $35 /=$


## TELEVISION

 OSCILLOSCOPERelease of a small quan.ity of the latest version of the well known APN-4 Indicator Unit from the American Loran Airborn radio navigation system. This provides a system. opportunity to golden opportunity servicing and development tool as described in Wireless World. Steel, double-deck, chassis with double-deck, chassis with fully screened 5CPl tube in the centre, all highsistors, separate tag boards and layout diagrams for individual sections etc. Modern circuit technique centred around one type of valve ( 14 uf etc. Modern circuit technique centred around one type of valve (147), and R.C.A. $100 \mathrm{kc} / \mathrm{s}$ Crystal. Brand new with W.W. Circuit and R.C.A. 100
for conversion.
$25 \mathrm{c} / \mathrm{s}$ Tuning Fork Drive 60'AMPLIFIER

Carriage
Modern light-alloy cased. Drive unit type 114 containing a robust 8 in. induction sustained 25 c's tuning fork with attendant induction pick-ups and waverorm amplitier
comprising 2
DF50, diode and 6 L 6 output. 5 U 4 G rectifier and VS110 stabiliser in power supply derived from highpow supple der - arily highby standard mains type Hieh grade components throughout. Easily removed, flexibly mounted tuning fork assembly energised by 6.3 volts A.C. only. Case size: $8 \frac{1}{2} \times 7 \frac{1}{2} \times 10 \frac{1}{2}$

## ANTENNA BEAM ROTATING MOTOR

Powerful British series-wound split field 24 -volt motor with a $600-1$ picyclic reduction gear turning a $\frac{z}{3}$ in. long, bin. diameter splined drive at $12-15 \mathrm{r} . \mathrm{p} . \mathrm{m}$. Removal of the easily detachable ( 24 voli) magnetic brake housed in a separate rear casing permits operation from either A.C. or D.C. at any voltage between 6 and 30 with corresponding variable speed. Limit switches operate after approximately 3 turns in either direction, but these can be shorted out for continuous running. Designed for external use, easily waterproofed. Consump tion 4-6 amps. 55/- plus 7/6


Brand New. 30/- Post free.

## eld 24 -volt motor with a $600-1$ n. long, tin. diameter splined he easily detachable (24 volt) rear casing permits operation between 6 and 30 with corres- n operate after approsimately asily waterprout for continuous

 50/- carriage.REMOTE INDICATOR
Remote indication to within $1^{\circ}$ on precision instrument type fush fitting black crackle indicator with 3 in . dial calibrated in $2^{\circ}$ steps plus the four cardinals. Simple D.C. wiring ( $6-30$ volt) from specially wound potentiometer in sealed die-cast housing with $\frac{1}{3}$ in. drilled spindle transmits accurate signal of horizontal
or vertical bearing.

## LOW VOLTAGE PRECISION RELAY

Actuates heavy-duty, silver contact, 7/6 2-pole changeover switch rated at 25 amps. and mounted on low loss

Post \&
Packing 2/base. Input 24 volts 5 watts. Changeover occurs at $16-17$ volts and reverse changeover when voltage drops by changeover when voltage drops by
 DES 1 to withstand 200 vibrations per second with unimpaired performance. Size: $2 \frac{3}{2} \times 2 \times 1 \mathrm{~d}$. Weight ozs. Dust cover protected. New in original
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PRECISION POTENTIOMETER
Magnificent ball-bearing mounted, $25 \mathrm{k}, 10$ watt, precision wirewound potentiometer by Colvern. Brand new in original carton with wound potentiometer by Coivern. Brand new in original carton with test certiacate and
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 POCKET PORTABLE Completely portable-NO EXTERNAL AERIALOR EARTH REQUIRED. This is an amazing little receiver with built-in aerial and small enough to be held in the palm of the hand. Medium wave reception at wonderful volume. No fiddley tuning! plied with drilled and colour coded components. Easily assembled with the aid ow the easy-tofollow assembly in-
structions provided. structions provided
 (45 necessary components, including transistors, wiring wire and even solder ONLY $32 / 6$ plus $1 / 6$ P. \&,$P$. Battery $3 /$ extra. Ardente type deaf-aid earpiece complete with cord and plugs extra at 12/6. Parts price list and Easy Lay-out Plans 2 /- post free. Callers welcome to hear this set demonstrated at any of our branches. Our reputation is your guarantee.

## METER IMPORT!

20,000 OHMS PER VOLT!!
 RANGES: A.C. VOLTAGE : $10,50,100,500$ and ohms per volt). D.C. VOLTAGE : 5. $25,50,250,500$ : S-25, 50,
and $2.5 \mathbf{k}^{2}$
20, 20,000 ohms per volt). 50 micro-amps., $0-$ 50 micro-a 2 mps ., 0 -
$2.5 \mathrm{~m} / \mathrm{a}, 0-250 \mathrm{~m} / \mathrm{a}$., $2.5 \mathrm{~m} / \mathrm{a}, 0,0-250 \mathrm{~m} / \mathrm{a}$,
RESISTANCE:
$0-6 \mathrm{k}$. O-6 meg. ( 300 ohm and meg. 30 k . at centre and scale).
CAPACITANCE: 10 Actual size $4 \frac{1}{2} \times 3 \frac{1}{4} \times \operatorname{lin}$, pf. to . 001 mid., DECIBELS: -20 to +22 db . mid . 0.1 mid . A fully guaranteed pocket size meter, knife edge pointer, top quality, supplied complete with test prods and full opera- E . ting instructions at 6 ONLY Plus $2 / 6$ P. \& $P$. Bona-fide trade enquiries invited. Optional extra, attractive carrying case $13 / 6$ only. Leaflet available.

## INCLUSIVE OFFER

STEREO AMPLIFIER fitted in ATTRACTIVE
TWO TONE REXINE TWO TONE REXIN
GARRYING CASE
4 watts per chan-
nel. Both speaker speaker
units are detach.
able fas able (as ted) volume/on off, ume/on off,
and treble erol:. A.C con240 v . Cabinet for B.S. R Stereo
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price $13 \frac{1}{2}$ Gns. plus $7 / 6$ P.\& P. Limited quantity only. B.S.R. UA 14 STEREO AUTOCHANGER available at $£ 8 / 19 / 6$ extra.
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## THE "CITIZEN"

Introducing our new Sensitive 5 -Stage (4 transistor plus diode) pocket transistor receiver-for full Medium Wave recoption

Completely
$\star$ Completely self-contained-no external aeriel or earth required.

- Genuine 2hn. High Flux P.M. Speaker.
${ }^{\star}$ Pish-Pull output.
\& Socket provided transistors.
Socket provided lor personal listening.
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$\star$ Volume Control with on/ofi switth-condenser tuning, * Attractive Red polystyrene cabinet measures $5 \ddagger \times 3 \times 1$ inin., chrome handle, attractive dlal.
Suitabie crystal deaf-aid type miniature ear-piece fitted with milnature fack plug at 0 NLT $7 / 6$ extra, if required. All parts arailable separately-itemsed list and full assembly

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## THE "WAVEMASTER" 7-TRANSISTOR

## LUXURY PORTABLE

## 400 MILLIWATTS OUTPUT

To build yourself, Medium and Long waves-Push-Pull Superhet A.V.C. Perifect Car Radio reception. Size $10 \mathrm{in} . \times 6 \frac{7}{4} \mathrm{in} . x$ $4 \frac{1}{2}$. at base tapering to 4 in . at top. Very attractive two-tone grey Vynide covered cabinet with black and gold printed escutcheon plate, cream and gold knobs, handle and cabinet fittings. * Weight-complete with long-life $7 \frac{1}{2}$-volt battery $\left.-4 \frac{1}{2} \right\rvert\, \mathrm{b}, ~ \star \quad$ Mazda high-grade transistors throughout. $\star$ High-Flux 7in. $x 4 i n$. Elliptical Speaker. $\star$ Slow motion tuning. $\star$ Co-axial socket at rear for direct connection to Car Radio Aerial. 太 Improved reception by use of seven-section plated telescopic aerial disappearing into Cabinet when closed, 34in. above Cabinet when fully extended.


## All required

components
solder, etc., anding full instructions, solder, etc., and battery at apecinal inclusive
price of price of
Plus $2 / 6 \mathrm{p}$ \& p. ONEY 95/-
Yes NINETY-FIVE SHILUNGS Yes NINETY-FIVE SHILUNGS
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Construction simplified by Bakelite chassis board with the following components already mounted: I.F. Transformers (3). Oscillator Coil, Trimmer, Bank, Output Transformer, Interstage Transformer, Aerial Brackets and Earth Bar. SPECIAL INCLUSIVE PRICE for all required components, fult assembly instructions-nothing more to buy-is $£ 10 / 19 / 6$ plus $3 / 6$ P. \& P. Alignment service available. Full assembly instructions and individually priced parts list, all of which are available separately, $2 / 6$, post f́ree.

SUPER I-VALVE SHORT-WAVE RADIO


World-wide coverage at most reasonable cost.
Covers $40-100$ Covers 40-100 metres with the coil supplied, Can be extended
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THE R.C. $3 / 4$ WATT AMPLIFIER Compare the advantages. Treble bass AND middle conAND midde con-
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stove enamelled steel stove enamelled steel
chassis measuring only chassis measuring only
$8 \mathrm{in}, \mathrm{x} 4 \mathrm{in}, \times 1 \frac{1}{4} \mathrm{in}$. Four en
8in. $x$ in. $x$ lin. graved cream knobs are included in the price
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## RADIO JACK (25)

Covers local medium wave stations variably tuned. Compact self contained unit requiring only connection to aerial (no power supplies required) for first-class reception when used in conjunction with your tape recorder or high gain amplifier. All necessary parts available at a special inclusive price of only $19 / 6$. P \& P. $1 / 6$.

## NEW! "POPULAR FOUR IMPROVED APPEARANCE AND PERFORMANCE

 ished walnut finish, cream trim, attractive horizontal dial (as illustrated). Quality 5in, P.M. speaker. Specially wound high gain supersensitive Denco coils. Medium and Long Wavebands. Excellent Continental reception! bands. Excellent Continental reception!
Overall dimensions: $12 \mathrm{in}, x 6 \mathrm{in}, \times \sin$. A.C. $200 / 250 \mathrm{v}$. Simple construction with guaran$200 / 250 \mathrm{v}$. Simple construction with guaran-
teed results. Easy to follow practical and teed results. Easy to follow practical and
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HI-FI SHOWROOM AT TOTTENHAM COURT ROAD FOR DEMONSTRATIONS OF THE LATEST HI-FIDELITY EQUIPMENT BY ALL LEADING MANUFACTURERS i.e., Leak, Quad, Armstrong, Dulci, Ferrograph, Reflectograph, Vortexion, Tannoy, Linear, Wharfedale, Grundig, Goodmans, W.B., Rogers, Garrard, Lenco, B.T.H., Pamphonic, Simon, Brenell, Collaro, Telefunken, Fi-Cord, etc., etc. A full range of high quality cabinets to suit all purposes is on show, i.e. |" RECORD HOUSING" "W.B." "A.D." etc. Enquire about our interesting part-exchange scheme for personal callers. H.P. Available.

## RECORD PLAYERS

 Full range at usual competitive prices. Motereng his. Aacities SINGLE RECORD UNIT. Very latest type. Heavy $8 \frac{3}{4} \mathrm{in}$. dia. table, low flutter performance $200 / 250 \mathrm{v}$. With tap at 80 operating amplifer valve filament if required. Complete with matching pick-up with mount and rest. Brand new and fully guaranteed. ONLY 89/6, plus 3/6 P. \& P. Pickup available separately, complete with mount and rest $25 /$-, plus $1 / 6$ P. \& $P$.

JUST ARRIVED! 4-SPEED BATTERY OPERATED VERSION OF ABOVE 6 volt operation complete with pick-up $£ 5 / 9 / 6$ plus P. \& P. 3/6. TRANSISTOR AMPLIFIER now available for use with the above battery player. Compact size, 500 milliwats output, printed circuit construction, tone and volume controls. Supplied complete with 8 in. $\times 2$ in. 20 ohms matching quality speake
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LATEST GARRARD MODEL 210. Four-speed manual or automatic. 10 in . and 12 in . records of same speed can be mixed in any order, wired for stereo, attractive white colour scheme. Price $10 \frac{1}{2}$ gns., plus $3 / 6$ P. \& P.
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Not repeatable, limited quantity.

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FOUR STATION PRE-SET SUPERFOUR STATION PRE-SET SUPERHET chassis. Two controls only, volume on/off, and simple 4 station rotary selection switch. Set to Light,
Home and Third programme, also Home and Third programme, also Light programme on long waves.
Frame aerial included also 5in. quality speaker mounted on chassis. Overall measurement 9 in. $\times 6$ tin. $\times$ $5 \frac{1}{2}$ in. high. Only $£ 4 / 17 / 6$ plus $5 /-$ p. \& p.

FRUSTRATED EXPORT. Not repeatable! L., M. and S.W. SUPERHET RECBEIVER. Manufactured by McCarthy for export At present for operation on 6 volts. but conversion details supplied free


Valve line-up: 6K8G, $6 K 7 \mathrm{G}, 6 \mathrm{Q} 7 \mathrm{C}$ 6F6G, $6 \times 5 \mathrm{G}$ and 6 volt 4 pin nonsynchronous vibrator. 8 in . P.M. Speaker, 4 watts outpue. P.U. socket Ext. L.S. socket, etc. Tone control,
Fitted in polished wood cabinet, Fitted in polished wood cabinet, size $21 \frac{3}{3} \mathrm{in} . \times 10 \frac{1}{2} \mathrm{in} . \times 10 \frac{1}{2} \mathrm{in}$. These cabinets are slightly soled owing to storage, but each is guaranteed un-
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A.M. RADIOGRAM CHASSIS Manufacturers' surplus. Brand new and fully guaranteed. Long, Medium and Short Waves. ECH81, EF89 EBC81, EL84, EZ80, siow motion tuning, tone control, ferrite rod aerial. Provision for gram, extension speaker, and tape play-back. Chassis size $l l i n$. deep by $8 \frac{1}{2}$ in. wide.


Dial engraved on attrattive brown and gold front panel size $16 \frac{1}{2} \mathrm{in} . \times 9 \mathrm{in}$. which forms escutcheon for easy at $\varepsilon 8 / 19 / 6$ plus $5 /-\mathrm{p}$. \& p. H.P. avail able.

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Our working model of this amazing organ for home construction may be heard and seen at our Hi-fi Showroom in Tottenham Court Road, W.I For the benefit of constructor's all components, keyboards, chokes, etc are available ready made. Full constructional details are available in book form at 15/- plus 1/6 p. and p. We shall be happy to forward a complete price list on receipt of a stamp Please address all organ enquiries for the attention of Mr. L. Roche

NEM TAPE RECORDER CONSTRUCTORS
LATEST COLLARO STUDIO TAPE TRANSCRIPTOR. Latest type incorporating Record, Interlock, Lever, Button, 3 motors, 3 speeds, P. \& P. Usual H. P. facilities P. \& P. Usual H.P. facilities.

## NEW! TAPE RECORDER AM-

 PLIFIER TYPE 83II-V. Subassembled - anyone can build! Printed Circuit, all components mounted and dip soldered. Already tested. Each lead cut to length.All that is required to complete the tape recorder is for a few components to be mounted in the cabinet and the free ends of the leads soldered to terminals which are clearly marked
 Everything supplied, all you need is solder iron, pliers and screwdriver Valve line-up. EFS6, ECC $832 \times$ ELB4 EZ81 and EM84 magic eye. Monitoring facilities, ourput socker for feedin to high quality amplifier can be used as "straight" amplifier for record reproduction EQUALISING ON TWO SPEEDS OUTSTANDING VALUE AT $£ 11 / I I /$ plus $2 / 6$ p. \& p. including all necessary instructions

ATTRACTIVE TWO-TONE PORTABLE CARRYING CASE. Suitable for above amplifier and Collaro Studio deck. Fitted with 9 in, $\times 5$ in Sitable for above amplifier and Collaro Studio deck. Fitted with in. $x$ Sin.
High Flux P.M. speaker for high quality reproduction. Inclusive price E5/5/-. Plus $5 /-$ P. \& P.

## CRYSTAL MICROPHONE.

Lapel-type. Complete with clip and screened lead. Brand new, 17/6. Pius 6d. P. \& P. (as illustrated)
MIC 45-1. Acos latest flat pistol-grip Crysta microphone Attractive black and gold finish. OUR PRICE $29 / 6$ plus 1- P \& P. ACOS MIC 39-1. Crystal stick microphone List price 6 gns . Our price $39 / 6$ plus $1 / 6$ P. \& P. MIC 40. General-purpose crystal microphone with desk stand Our price 22/6 only plus $1 / 6$ P. \& P. M.C.24. Imported rystal, attractive streamlined polished metal case in corporates muting switch. List price 64/-. OUR PRICE 32/6 only. 1/-P. \& P


TELEPHONE PICK-UP COIL. Designed to feed into the micro phone input of either a tape recorder or any high gain amplifier. Easil attached to telephone by rubber suction attachment. The coil is electro statically shielded to minimise hum pick-up. When positioned on tele phone model is more than adequate for a fully modulated tape record ing. Brand new complete with 5 fr . shielded cable. ONLY 14/-. P. \& P. 1/6


MAGNETIC RECORDING TAPE SPECIAL! An enthusiast's "must." Brand new (NOT SUB-STANDARD) High grade Acetate Base 5 in .600 ft . $16 /-, 5 \mathrm{in}$. 900 ft . $18 / 6,5 \frac{1}{2} \mathrm{in}$. $1,200 \mathrm{ft}$. 23/6, 7in. 1,200ft. 25/-, 7in. $1,800 \mathrm{ft}$. 35/-. Extra quality Mylar Dupont, 3in. 300ft. 13/., Sin. 1.200ft. 37/6. 7 in . $1,800 \mathrm{ft}$. $44 / \mathrm{-}, 7 \mathrm{in}$. $2,400 \mathrm{ft}$. $60 /$. Each on plastic spool. All Post free. Trade enquiries invited.
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As new guaranteed perfect, by leading manufacturers, $5 \mathrm{in} .9 / 6 ; 6 \frac{1}{2} \mathrm{in}$. $10 / 6$ : $7 \mathrm{in} . \times 4 \mathrm{in} .10 / 6 ; 8 \mathrm{in} .13 / 6$; also 10 in with O/P transformer ( 5,000 ohms) 17/6. All 3 ohm speech coil, also 8 in available, in attractive cloth covered cabinet, ideal for extension speaker 22/6. Each item plus 1/6 P. \& P. Large selection of Brand New Speakers. Full list on request.
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Bulld a high quallty recorder in the $£ 70$ class for only

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 Can bo assembled in $\frac{1}{2}$ nour.
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太 3 SPEEDS 太 FREQUENCY RESPONSE $60-11,000$ C.p.s. $\star$ SWITCHED 4 WATTS $\star$ MAGIC EYE RECORDNG LEVEL INDICATOR * 3 MOTPUS Fast rewind $\star$ TAPE MEASURING AND CALIRRATING DEVICE $\star$ TAKES
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EFFECIVE AUTOMATIC ERASURE.
EFFECTIVE AUTOMATIC ERASURE.
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HF1012, 10 watts, 15 ohm (or 3 ohm) speech coil. Where a really good quality speaker at a low price is required, we highly recommend this uuit with an amazing performance. $84 / 10 / 9$. Please state whether 3 ohm or 15 ohm required BASS REFLEX CABINET, Specially designed for above speaker. Acoustically lined and ported. Polished Walnut
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27/9 ( $\begin{aligned} & \text { Listed } \\ & 45 /-)\end{aligned}$
$39 / 6$ (Listed $\left.\begin{array}{l}\text { Gns. }\end{array}\right)$
Limited number.
10,000 ohms per
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THE SKY FOUR T.R.F. RECEVVER


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receiver with selen lum rectither, for nclusion la cablinet nut veneered type. it employs valves
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Type Biyl. An all-dry battery eliminator. Size $5 \frac{1}{x} 4 \frac{x}{} 2 \mathrm{n}$. approx. Completely replaces batteries supply $1.4 \vee$. and 90 v. Where A.C. mains $200.250 \%$. nd 00 . diagrata $39 / 9$ or ready for use $46 / 9$.
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 Ing Choke, Double Electrolytic Condenser, Aluminium Chassis and Circuit.

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A complete kit of parts to conatruct a good qualty $3+3$ watt (total 6 watt) stereo amplifier providing really me-nke reproduction. sultable for use with all stereo
pick-up heads at present avallable. Ganged volume and tone controls. Preset balance control. Outputs for matched $2-3$ ohm speakers. For $200-250 \mathrm{v}$. A.C. mains. Astonisblag value.
R.S.C. STEREO/TEN HIGH QUALITY AMPLIFIER KIT

Vaives E Z81, ECC
 83, ECC83, EL84, bass and treble controls .giving, "cut'
and ".boost."
Sen sittvity 50 mv .
watts hlgh walts high quality
output on each
channel. Can be used as straight 10 trolk: Stereo/Monangal switch, ganged ance. Gutputs for 3 ohm epeakers, and bal point wiring diagrams and inptructions. Illustration full wirimg detalls nad priced parts

GNS.

ACOS Hap 69 Hi-Fi Crystal Cartridgen. (Turnover type with Gapphire stylus.) Standard replacerreent for Garrard
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All parts to construct a very compact. highly senzitive amplifler suitable for any type of single or autochange player. Size $12 \times 2\} \times 212 \mathrm{in}$. Chassis is malne transiorme
isolated. For $200-250$ y. A.C. mains. Out$\begin{array}{lll}\text { put for } 2-3 \text { ohm speaker. } \\ \text { control with mains switch. } & \text { Volume and tone } & 39 / 6\end{array}$

## SELENIUM RECTIFIERS

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VARLEY ${ }^{2}$ V 14 A. ${ }^{\text {H. }}$ ACCUMULATORS. New
 JASON F.M. TUNER Type FMT1. All parts including Dial, Punched Chassis and Valves.
Power supply required 180 v .25 mA and 6.3 v . 1.5 a EX GOVT. SMOOTHING CHOKES 60 mA 10 h .400 omms 311 80 mA 20 h .900 ohms
100 mA
5 h .100 ohms 100 mA 10 h .100 ohms $\mathrm{B} / \mathrm{I}$ 150 mA 10 b. 100 ohms
${ }^{120 \mathrm{~mA} 12 \mathrm{~h} .100 \mathrm{ohms}} 10119$
200 mA 8-10 h. 100 ohms $11 / 9$

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## HEAVY DUTY KIT BATTERY GHARGER KITS

 $6 / 12 \mathrm{v}$. variable charge rate up to 6 amps. Consisting of Mains Trans., F.W. (Bridge) Selenium Rectifier, 0-7 amp. meter. Variable Charge Selector. Fuses, fuse-holders, panels, plugs and circuit. Only 39/6. Post $4 / 6$.CHARGER
TRANSFORMER8
$\begin{array}{lll}200-230.250 & \text { v. } & 50 \mathrm{c} / \mathrm{s} \\ 0-0.15 & \text { v. } & 14 \\ \text { a }\end{array}$
 $\begin{array}{lllll}0-8-15 & \text { v. } 3 & 3 & \text { a. } & 16 / 9 \\ 0-8.15 & \text { r. } & 5 & \text { a. } & 19 / 9\end{array}$


Consisting of Mains Transformer, F.W. Bridge, Metal Rectifier, well ventilated steel case. Fuses, fuse-holders, grommets, panels
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6 v . or 12 v .2 amps.
6 v. or 12 v. 2 amps.
(inclusive of ammeter) $8 / 12$ v. 4 amps.
6 v. or 12 v. 4 amps., with and ammeter

ASSEMBLED CHARGER
6 v. or 12 v. 2 amps. Fitted Ammeter and selector plug for 6 v . or 12 v . Louvred metal case, finished tractive hammer blue. Ready for use with mains and output leads. Double Fused $\begin{array}{ll}\text { Only } & 49 / 9 \\ \text { Carr. 3/8. } & 49\end{array}$

## ASSEMRLED 6 v . or 12 v



Fitted Ammeter and variable charge selector. Also selector plug for 6 v . or 12 v . charging. Double fused. Well ventilated steel case with blue hammer finish. Ready $\begin{array}{ll}\text { manse wind } \\ \text { mad }\end{array} \quad 69 / 9$ output leads. Carr. 5\%. or Deposit $13 / 3$ and 5 monthly payments of $13 / 3$.
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$0-50$ micro-amp. Diameerer $2 \neq 1 \mathrm{in}$ appros. scaled $0-100$ Flush mountling, 29/6.

EX GOVT. MAINS TRANSFORMERS Prumary 0-110-200-230-250 v. 275-0-275 \%. $100 \mathrm{~mA}, 6.3$ 7 2.
7
nout $200-250$

Primary $200-240$ \%. Sec. 3,500
50 watis, $0-110 / 120-230 / 250$ v.
D.C. SUPFLI ETTS. Suftable for electric trains. Consist rect. (F.W. Bridge): 2 fuseholders, 2 fuese, change direetion - witch, variahle speed regulator, partially driled steel case and circuit. Verg limited number, $33 / 9$

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VALVES! Full range at renily competitive prices.

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Well ventilated, black cracsle finished, undrified cover Size $14 \times 10 \times 88$ in, high, IDEAL FOR BATTERYCEARUSED FOR AMPLIFIER. Only $9 / 9$, plus $2 / 9$ post. RELAYS. Carpenter Type Polarised, 2 I 9,500 turns at
1,685 ohms, $13 / \theta$. Ministure type G.E.C. 670 M1092
bealed mire ends 4 c/overs platinum, $12 / 9$. 1,685 ohms. $13 / 0$. Ministure type $12 / 9$.
sealert wire ends 4 c/overs platinum, $12 / 9$.

## R.S.C. A10 ULTRA LINEAR 30 WATT AMPLIFIER


gram, etc. can be simultaneously applied for mixing purposes. AT OUIPOL SOCEET OF 300 v. 20 mA , and 6.3 ₹ 1.5 A . FOn A ONLY 11 Or Factory built using latest EL34 output valves and with 12 Carr. 10/-11g/IS. months guarantec. 14 GNS. TERMS CN ASSEMBLED UNaTS. Protective Cover 19/g. Type 807 output valves are naed whin High Quality Sectionally feedback of 20 D.B. in main hop, CERTIFIEL PERFORMANCE FIGURES ARE EQUAL TO MOST EXPENSIVE UNITS AVALLABLE. Frequency responke + 3 D.B. $30-20,000 \mathrm{c} / \mathrm{s}$. Tone Controls $\pm 12$ D.B. at 50 e/cs. $\pm 12$ D.B. to -6 D.B. at 12,000 c/es, hum and
noise 70 D.B. dowa. Good quality retiable components used. Chassis finish blue hammer. Overall size $12 \times 9 \times 9$ in. approx. Power consumption 150 watte. For A.C
 DDEAL FOR USE WITR MUSICAL INSTRUMENTS, SUCH AS STRING BASS, ELECTRONIC ORGAN, GUITAR, etc. FOR DANCE BANDS, GARRISON THEATRES, etc. etc. We can supply Microphones, Speakers,
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FULL RANGE OF LINEAR HIGH FIDELITY AMPLIFIERS ALWAYS IN STOCK For $200-250$ v. 00 c.p.s. A.C. mains. Overall size only $111 \times 2 \frac{1}{2} \times 2 \downarrow \mathrm{in}$. Fitted Vol. and Tone Control with mains switch. Designed for use with any kind of single player or record
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A highly sensitive $4+$ valve quallty amplifier for the home, small club, etc. Only 50 millfidelity pick-up heals in addition to all other types of plek-ups and practically all makes Separate Bass and Treble controla are provided. These give full long playing record equalisation. Hum-level is negligible being 71 D.B. of 300 v .26 mA . and L.T. of 6.3 F .1 .5 a. is avallable for the supply of a Railo Feeder Unit or Tape Deck pre-amplifier. Por A.C. mains input of 200-250 F . $50 \mathrm{c} / \mathrm{s}$. Output for 2 - F ohm speaker. Chansis in not alive. Kit is complete in every detail and includes fully puached chassis (with baseplate) with the blue avd Tnstructions. Exceptlonal value at only 94:15/-

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P.M. SPEAKERS. 2-3 ohms 2inn. Perdlo 21/9. 5in. Gcodmans $17 / 9.7 \times 4 \mathrm{in} . \mathrm{R} . \mathrm{A}$ Elifpticel 19/9. 6in. Rola 18/9. 8in. Rola 19/9. 8in. Goodmans $25 / 9$. $8 \times 6 \mathrm{in}$. Elac 12in. R.A. 29/11. 121n. R.A. 3 or 15 ohms, 10 watts, 12,000 lines, $59 / 6$.

## TWEETERS, 4 in . Plessy, 3 ohms 18/9. R.A. 10 ohms $25 / 9$

R.S.C. TRANSFORMERS Fulls Guaranteed. MAINS TRANSFORMERS. Primarles 200-250-25 FULEY SHROUDED. UPRIGHT MOUFTING. 250-0-250 ₹. $60 \mathrm{mA}$. , 6.3 ₹. 2 a., 5 ₹. 2 a. 21-3-3in.

 | $300-0-300$ ₹. 100 mA , |
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| $350-0.350$ | $350-0.350 \mathrm{v} .150 \mathrm{~mA}$.



TOP BHROUDED DROP-THROUGH TYPE 260-0-260 ४. 70 mA., 6.3 ₹. 2 a, b v. 2 a $250-0-250$ ₹. 100 mA , $350-0-350$ v. 80 mA. . $50-0-250 \mathrm{~F} .100 \mathrm{~mA} .6 .3 \mathrm{~F} .1$ a B \% 2 a.... $\begin{array}{lll}300-0-300 & \text { v. } 100 \mathrm{~mA} ., 6.3 & 130 \mathrm{~mA} . \\ 3.3 & 4 \text { a., } 5 \text { v. } 3 \text { a }\end{array}$ suitable for Mullard 510 Amplifier.
$50-0-350$
v .10 mA . $\mathrm{f.3}$ v. 4 a., 5 v. 3 a $350-0-350$ v. 150 mA . 6.3 v. 4 a., os v. 3 a FILAMENT TRANSFORMERS

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LINEAR L45 MINTATURE 4/5 W. QUALITY AMPLIFIER. Suitable for uee with any record playing unit and most onntrols For $4 . \mathrm{C}$ mains input of $200-250$ y. $50 \mathrm{c}, \mathrm{p}, 8$ Ou put for $2 / 3$ ohm speaker. Three miniature mullard ralven Size only $6 \times 5 \times 5$ in. hlgh. Chassls folly lenlated from
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Interleaved \& impregnated OUTPUT TRANSFORMERS Midget Battery Pedtode 66: 1 for 3\$4, etc... $3 / 9$
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B,000 to $30 . . . . . . . . .4 / 6$ Standard Pentode 5,0000
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Push pull 10.12 watte to match 6 vo to $3.5-8$ or 15 is
Puah pull EL84 to 3 or 15010.12 watta
Push pull Dltra Linenr for Mnllard 510 ............
Push pull
15-18
watte, sectlonally wound.
KTh6, etc.. for 3 or iso
Push pull 20 watt bjgh-quality nectionally wound
$6 \mathrm{~L} 8, \mathrm{KT66}$, etc., or 4 or $15 \Omega$ fully shrouded.
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120:1 High quality. clamped
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$250 \mathrm{~mA}, 5$ H., $100 \mathrm{a} \quad 11 / 9$
$150 \mathrm{~mA} .7-10 \mathrm{H} ., 250 \mathrm{n}$
$100 \mathrm{~mA}, 10$ H., 200 g
$8 / 9$
100 mA .10 H $200 \mathrm{~g} \quad 8 / 9 \quad 1 \mathrm{mmp}, 10 \mathrm{H} ., 400 \mathrm{D} 4 / 11$
PARMEKO MAINS TRANSFORMERS Fully hy
$500 \cdot 0-500$ v. 120 uA., 6.3 v. 4 \&., 5 v. 3 \&............. 31/8
LINEAR TAPE PRE-AMPLIFIER Type LP/1, Ywitched negative feedback equalisation. Positions for Record fin., 3 inn., 7 in. and Playback. EM 84 . Recordidg level
Indicator. Deaigred primarily as the lind between Collaro Indicator. Desigreed primarily as the lings between Coilaro
Tape Tranacriptor and high adelity amplifer but suitable almost any Tape Deck. 9 GNS Bend 8.A.E. for leaflet

## LINEAR PRE-AMP/TREMOLO UNIT

Sultable for use with any Gultar Ainplifier. Controis
Volume Volurne, Frequency, Amplitude and switches. Valves: EF88 and EF80. Inputs for Guitar Pick-up or Mike, and
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## HIGH FIDELITY 12-14 WATT AMPLIFIER TYPE A11

## PUSH-PULL

 ULTRA LINEAR OUTPUT"BUILT-IN" TONE CONTROL PRE-AMP STAGES

Two input sockets with arsocla of " malke" and gram. as in valves: ECC83, ECCOs
EL84, FL84, 5 Y 8 . High Quality sectionally wound outpit transformer specially designed or Uiltra Linear operation and reliable small condensers of current manufacture. INDIVIDUAL, CONTROLS FOR BASS AND TREBLE " LIt" and "Cut." Frequency response $\pm 8 \mathrm{D} . \mathrm{B}, 30-30,000 \mathrm{c} / \mathrm{cs}$. Bix negative feedback hops. Hums level $60 \mathrm{D} . \mathrm{B}$. down. ONLY 23 millivolts INPUT required for FULI OUTPUT. Buitable for une with all makes and types of pick-ups and microphones. Comparable with the very best designs.
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ONLE 8 GIS. $10 \%$ f reqnired louvred metal cover with 2 carrying handles can be aupplied for 18/9. TE for illustrated leaflet detalling ready-to-assemble Cabinete. speakers. Microphones, etc. dit terins.

## R.S.C. PORTABLE GUITAR AMPLIFIERS



JUNIOR 5 WATT. HIgh Quality Output. Separate Bass and Treble "cut" and "" boost" controls.
Bensitivity 15 mvv . High Flux 8 in. Vspeaker. Input sockets for Radio/Tape or Grara Pick-up and Mike Instrument Mck-up. Handsotne strongly made cabinet (size approx. $14 \times 14 \times 7 \mathrm{in}$.). Finiabed in 8.19 .6 Carr. 7/8. Or Depoait $£ 1$ and nine 28. 19.0 monthly payments $£ 1$.

SENIOR 10 WTTS EIgh-Fidelity Push-Pulloutput. Beparate Baas and Treble "cut" and boot controis, Twin separately controlled Guitar and String bass Guitar and String Bass cen be used at the rarne time. Two Loudspeakers are incorporated: $12 i u$.
P.M. for Bask notes and $17 \times$ din. elliptical for
 $34 / 9$ and 9 monthly payments $34 / 9$. Both models for $200-250 \mathrm{~V}$. A.C. maina.
COLLARO CONQUEST 4-SPEED AUTO-CEANLatest model for $200 \cdot 250 \mathrm{v}$. A.C. mains, $£ 6 / 19 / 6$ Carr. ${ }^{4 / 6 \text {. }}$ MONARCB AUTO-CHANGERS.
 UAB. 4 speed T/O Pick-up with sapphire stylus
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any of the above supplied with T/O stereo/mon-
aural bead for el extra.
COLLARO JUNIOR. $4 \cdot$ epeed Single Players with

LOUDSPEAKER IN POLISHED WALNUT FINISHED CABINET. Gauss 12,000 lines. Speech coil, 3 ohms or 15 ohms. Obly $94 / 19 / 6$.
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18in. 20 WATT 15,000 line $1 / \mathrm{speakers} 15$ ohms in Cablnet finished
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E.S.C. STANDARD EQUIPMENT CABINET. Designed to house a variety of equipment such as Tape or Record Player Unit, Amplifler and Tuned Unit. Size aud appearance as per Reffex Cabinet below. There two cabinets, can be aliguen to form a complote high fidelity assembly at a
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R.8.C. STANDARD BASS REFLEX CABINET for 121 n Loudspeakers, acoustically libed and pirted. Size 201n. $x$ $\begin{array}{lll}14 i \mathrm{in} . \times 13 \mathrm{in} \text {. Beautiful walnut veneer linlsh. } & \text { Eapecially } \\ \text { recommended } \\ \text { for use with }\end{array}$ recommended for use with Speaker below, $25 / 19 / 6$.
Set of four legs an be supplied for $29 / 6$ per set.


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(15 ohms) consistligg of a
blgh quality 12 in. apeaker of orthodor design eupport fing a mmail elliptical speaker ready wired whith choke
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COMPLETE WITH INSTRUCTIONS, LEADS AND batteries (List $\mathbf{6} 19 / 10 /$-)
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NO EXTERNAL AERIAL OR EARTH 3-TRANSISTOR and 2-DIODES PERSONAL POCKET RADIO with 5 stages giving clear reception on medium wave, amateur top band and shipping. FULL STATION SEPARATION Only first-grade components used
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Free Instructions and Price
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- A sensitive superhet with 150 mW push-pull output on $2 \frac{1}{2} i n$. speaker. Uses 6 first-grade Mullard transistors and printed circuit. Moulded cabinet. Red, Blue or Cream
- All parts sold separately. Send for list. Mustrated Building Plans $1 / 6$ plus post. ALL PARTS REQUIRED $£ 8.19 .6$
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## 750 mW

4-TRANSISTOR
PUSH-PULL AMPLIFIER
(over I watt peak output)
Uses OC7I/OC8ID 2 -OC81.

* $\pm 3 \mathrm{~dB} 70 \mathrm{c} / \mathrm{s}$ to $12 \mathrm{ke} / \mathrm{s}$.
- Overall size $3 \times 2 \frac{2}{4} \times \frac{3}{4} \mathrm{in}$.
- Built on printed circuit.

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Size $5 \frac{1}{4} \times 3 \times 1 \frac{3}{4}$ in


MULLARD and EDISWAN
Matched Sets of

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| 1-OC44 | ONLY |
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|  |  |
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| 6 Ediswan | tors and |
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| $1-\times 8103$ | I |
| 2 - $\mathrm{XClOI}^{1}$ | PER SET |
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WE STOCK THE LARG EST RANGE OF MINIATURE AND SUB-MINIATURE COMPONENTS FOR THE HOME CONSTRUCTOR IN THE COUNTRY AT VALUE FOR MONEY PRICES. LET US HAVE YOUR ENQUIRIES.


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$$
\begin{array}{|l|l}
\hline \mathbf{2 0 , 0 0 0} & \leqslant \begin{array}{l}
\text { Size } 4 \frac{1}{2} \times 3 \frac{1}{4} \times \\
\text { Ohms Volt ! } \\
\text { Over } 20 \text { Scales }
\end{array} \\
\hline
\end{array}
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Price, inclusive of Test
Prods. Battery and
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g.p
3 A new design for Hi fi to feed quality
valve or transistor $\quad$ Fully lllustrated valve or transisto

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Heavy 8izin. metal zurntable. Low fluter performance, $200 / 250 \quad \mathrm{~V}$. shaded motor perlormance, 80 , for amplifier valve filament with tap at 80 v . for amplifier val
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A Pair of midget $465 \mathrm{kc} / \mathrm{s}$ !.F. eransformers, plus LW and MW coils PRICE $10 /$ per sec. P. \& P. $1 / 9$.
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108 K 10-inch. New and boxed. 75 K 10-inch. New and boxed.
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120 and 121 .
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MAINS POWER SUPPLY UNITS． Potted and sealed transformer and choke by famous maker．Mounted on metal chassis $6 \frac{1}{2} \times$ $7 \frac{1}{2}$ in．，complete with $5 Z 4$ ．rectifier valve
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Contacts $2 \frac{1}{2}$ amp． 230 volt， 24 hour phase，$\ddagger$ hour divi sions，allow setting for one make and one break to be made every 24 hours，complete with key．Used but guaranteed perfect． Price 27／6 each．P．\＆ P．2／－．

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PACKARD BELL BRAND NEW RELAYS 2 pole C／O． 6 vole 80 ohms． $7 / 6$ each．P．\＆P． 6 d ． MINIATURE RELAYS 250 ohms．Two makes．For operation on 4．5－9 velt．Idea！for makes．For operation Weight iust over 1 oz． Price 12／6 each．
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Used but perfect Complete with two way calling system
（buzzer）． （buzzer），interna battery．All ready or simple two－wir
E3／2／6 each or 66 the pair．P．\＆P． $3 / 6$ each handset．
DESK TELEPHONE SETS，similar to G．P．O extension telephones．Each complete with automatic dial，internal bell and long connection core and junction box．Used but in perfect working order．Price $2 / 17 / 6$ each．P．\＆P． 3／6．

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 PHONES．Used but in good condition Price $12 / 6$ ．P．\＆P． $1 / 6$ ．NEW BALANCED ARMATURE HEAD－ PHONES．TYPE DLR5．Guaranteed perfect．Price $12 / 6$ each．P．\＆P．2／－．

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5 amp．D．C．M．I． 2 tin in．fl．rnd．
$7 \frac{1}{2}$ amp．D．C．M．I． $3 \frac{1}{2}$ in．proj．rnd
$7 \frac{1}{2}$ amp．D．C．M．I． 3 tin．proj rnd．．．．．．．．
9 amp．D．C．Hot Wire W．R． $2 \frac{1}{2}$ in，tl．rnd．
15 amp ．D．C．M．C． 2 in ．rnd．．．．．．．．．．．．．．．．
Voltmeters
20 v．D．C．M．C． 2 in ．fi．sq．．．．．．．．．．．．．．．．．．．． 1016
30 v．M．I．3in．proj，rnd．．．．
300 v．A．C．M．I． $2 \frac{1}{i n}$ in．fl．rnd．
400 v．A．C．M．I． $4 \frac{i}{2 n}$ ．Fnd．．．．
$90-180 \mathrm{v}$ ．A．C．M．I． $4 \frac{1}{2}$ in．fl．iran
Milliammeters
1 mA．M．C． 2 itin．fl．rnd．．
200 mA ．M．C． 2 tin．fl．rnd
500 mA ．M．C． $2 \frac{1}{2} \mathrm{in}$ ．fl．rnd
Miniature latest type moving coil $0-5$ milli－ amp meter，I $\frac{1}{2}$ in． diameter，flush fit－ ting，complete with fixing clip．Price 17／6．P．\＆P．I／－．
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Miniature latest type moving COIL MICROAMP METER，F．S．D． 300 microamp，flush mouncing，square rim lisin．$x$ $1 \frac{3}{4}$ in．，round dial $1 \frac{1}{4}$ in．Ideal as field strength meter or output level recorder or tuning meter．Price 26／－．P．\＆P．1／－
LATEST TYPE ERNEST TURNER． $0-200$ volt A．C．RECTIFIED M．C．METER． Flush mounting，round，3in．scale．Prıce 37／6． P．\＆P． $1 / 6$ ．

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 RANGE VOLTMETER． 5 \＆ 100 volt D．C．3in．scale，F．S．D．ImA． Brand new in carrying case with Test Prods and Leads．Price 27／6． P．\＆P． $2 / 6$.
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From 5,675 to 8,650 in steps of $25 \mathrm{Kc} / \mathrm{s}$, and from $5,706.66$ to $8,400 \mathrm{in}$ steps of $33.3 \mathrm{Kc} / \mathrm{s}$. All types $5 /$ - each. Also in 1,600 , $1,605,1,610,1,615,1,620,1,625,1,630 \mathrm{Kc} / \mathrm{s}$ at $7 / 6$ each.

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500 Kc (10X Type) 7/6. 100 Kc RCA 3 Pin (with socket) $17 / 6$. $1,000 \mathrm{Kc}(\mathrm{HC} 6-U) 17 / 6.5 \mathrm{Mc} / \mathrm{s} 5 / \mathrm{c}$

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Complete with original Calibration Charts, Crystal and Valves In soiled condition but guaranteed perfect working order. A gift at $£ 10$.

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Made by Sangamo Weston. Brand new. Type S.145. Size 3in. $x$ $2 \frac{3}{3} \mathrm{in}$. 850 ohms resistance. 4 Scales operated by lever, "Set Zero," " $0-3$," " $0-30$," " $0-300$." Easily coupled to rotary range switch by cord or lever. Complete with suggested circuits, a gift at 20/-. Easily adjusted to 24-0-25 Microamps.
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An excellent $T / X$ at a give-away price. Coverage $2-18 \mathrm{Mc} / \mathrm{s}$. 21 and $28 \mathrm{Mc} / \mathrm{s}$ easily added. Autotune mechanism allows selection of any one of eleven (pre-selected) frequencies. Built in $200 \mathrm{~K} / \mathrm{C}$ Crystal calibrator checks the typical Collins Super Stable V.F.O Uses standard valves including P.P.811's modulating the 813 final. Size only $23 i n$. wide, 16 in . deep, 12 in . high. Requires power supply of 1,000 to $1,250 \mathrm{v} .250 \mathrm{M} / \mathrm{A}$ (for $100-200 \mathrm{w}$. input). 400 $225 \mathrm{M} / \mathrm{A}$ and L.T. for heaters and autotune mechanism. Supolied complete with valves, calibration charts, circuit and full technical details including 21 and $28 \mathrm{Mc} / \mathrm{s}$ conversion and power supply information. Definitely no snags (except TVI).
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An excellent basis for a 2 meter Converter. See February S.W Mag. Complete with yalves and Jones plug and socket. Pric 15/- post paid. Extras if required, 7,580 Crystal 5/-. I.F. Trans. as specified (unconverted), $2 / 6$.
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Type (1). Input 12 v . Output 300 v . or 250 v . or 200 v . at 30 w . A complete kit of parts incorporating high-grade toroid transformers, silicon (Bridge) rectifiers, New Market V30/10P Transistors Full audio and R/F filtering to V.H.F. operating frequency 400 c . Eificiency $85 \%$. All component parts mount on heatsink which is supplied completely drilled. Size $5 \times 4 \times 3 \mathrm{in}$. H. Price £5/15/Type (2). As above but outpur 45 w . Uses OC35 Transistors. Price £6/17/6.

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[^15]
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V., 12 V. and 3 v. dry battery. Range over 10 miles. Full instructions and circuit supplied. These units have been "demobbed" by removal of the "Send Receive" switch. A replacement switch with fitting instructions is supplied. We offer this fine unit with all accessories as listed above at the ridiculous price of $30 /$ - or two for $57 / 6$. We will supply an extra 46 set, complete with valves (but no accessories) as a source of spares for only $7 / 6$ extra. Extra set of valves $4 /-$. Batteries are available a $22 / 6$ per set. A low-priced Transistorised Kit of Parts for operation of above from 6 v . or 12 v. D.C. will soon be available.

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Type (1). Complete Assembly as used in the AR.88. Price $8 / 6$ Type (2). Wearite Heavy Duty 3 Bank Switches, each Bank 2 Poles 6 Ways. Price 7/6.

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The Sherill M.6. A superb compass originally designed for armoured cars. Complete with Manual and Deviation Corection Card. Further details on request. Cost over £40. Price £3/15/-

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Contact cooled bridge type. Output 250 v. $120 \mathrm{M} / \mathrm{A}$. Price $5 / 6$. Transformer for same with 6.3.v. 3A winding. Price $8 / 6$.

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Type (1). Venner 14-day clockwork Time Switches. One Make and One Break every 24 hours. Complete with key, 1 amp. contacts Price 27/6.
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Miniature silicon power diodes at new low prices. Made by one of England's greatest manufacturers. $250 \mathrm{M} / \mathrm{A}$ D/C output Typ (1) 400 P.I.V. Price 3/6. Type (2) 600 P.I.V. Price 5/6. Type (3) 800 P.I.V. Price $7 / 6$.

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The transmitter portion of the 1986. Unusable in its present
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If you have ever written to us you will receive a copy of our comprehensive list within a few days, if not, then please let us have your name and address.

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 10 watt $\}$ Wre-WOUND RESISKOR 15 watt $\}$
12,500 ohms $-50,000$ ohms. 10 w
WIRE WOUND POTS. 3 w. Pre-set Min. T.V. type, Knurled slotted knob.
 Ditto il w. Garbon Track, CONTROL $10 \Omega$ SPEAKER O/P TRANSFORMERS. Miniature 3V4, etc., 4/6. Heavy Push-Pull 10 watts 15/6. Push-pull 20 w. 6 k. P. P.P. $30 /$. L.F. CHOKEs. 10 H 80 mAA .46 . $10 \mathrm{H} ~ 68 \mathrm{~mA} .5-10 \mathrm{~B} 85$ mA. $10 / 6$. $10 \mathrm{H} 120 \mathrm{~mA} .12 / 6$. 10 H 150 mA . 14

## MTANDARD TRANSFORMERS $200 ; 00-250,80 \mathrm{~mA}$., 6.3 tapped 4 V .4 a. Rectifier 6.3 <br> or 4 v. 2 a. Ditto $350-0-350$ <br> MINIATURE $220 \mathrm{v} .20 \mathrm{~mA}, 6.3 \mathrm{v} .1 \mathrm{a}$ <br> MIDGET, $220 \mathrm{v} .45 \mathrm{~mA}, 6.3 \mathrm{~V} .2 \mathrm{a}$. <br> STANDARD, $250-0-250,65 \mathrm{~mA}$., 6.3 v 3.5 <br> GEATER TRANS., 6.3 v. 14 a., 76 ; $\ldots . .4$ amps. GENERAL PURPOSE LOW VOLTAGE. Output 3 6. $8,9,10,12,15,18,24$ and 30 v . at 2 A . AOTO. TRANS. $150 \mathrm{~V}, 10,70$ AUTO TRANS. 500 w., $0,115,120,200,230,250,250$ <br> ALADDDN FORMERS and cores, Ina. 8d. itin. 10d.

 2.3in. FORMERS 5937 or 8 and Cans 151 or $1 V 2$. SOLON. Midget solde ring Tron, 220140 v. 25 w ., 24/MANS DROPPERS. $3 \times 1 / \mathrm{in}$. Adf. Sliders .3 amp .
 LINE CoRD.
per foot, 2 -way, $1 /-$ per foot,
3 -way
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CRYSTAL MIKE INSERT by Acos $8 / 6$ | Precision engineered. Size onls 1 itn. dia. $\times$ tin. |
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I.F. TRANSFORMERS $7 / 6$ pair
$465 \mathrm{ke} / \mathrm{s}$, slug tuning miniature can $11 \times \times$ in . High CRYSTAL DIODE G.E.C. $2 /$-, GEX 34 4/-. 40 Circults 3/H.R. HEADPHONES. 4,000 obms, brand new, 15/- pair SWITCH CLEANER. Fluld, squirt spout. $4 / 3 \mathrm{tin}$. TWIN GANG CONDENSERS. 500 , PR Miniature, 1 gin. 91 -: Midget $7 / 6$ with trimmers $9 /-$ Single 50 or 80 pfis 100 pf., 160 pf., $5 / 6$. Solid dielectric $100,300,500$ pf., $3 / 6$. VALVE HOLDERS. EASO, 6d. B12A, CRT, 1/3. Eng.
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THE HI-GAIN BAND 3 PRE-AMP Cascode circuit using Valve ECC84. 17db gain. Kit $29 / 6$ less power; power pack. Plans only 6d.
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BULLD IT YOURSELF using 4-SPEED BSR MONARCE READY BULLT 3W, AMPLIFIER, HANDSOME PORTABLE CASE. HIGH FLUX 6 in . LOUDSPEAKER Total Price
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"F P W pocket six transistor kit, all parts, printed circuit and cabinet, $£ 8 / 15 /$.
Weyrad Printed Circuit Components in 8 tock
$485 \mathrm{Kc} / \mathrm{s}$. SIGNAL GENERATOR. Total cost $15 / \%$. Uses B.F. S. Unit ZA 30038 ready mide. POCKET SLZE $2 \& \times 4 \neq \times$ lin. slight modifications required, intl instructions supplied.
Battery $7 / 6$ extra 69 v. $+1, ~ \mathrm{v}$. Details 8 .

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Long spindile. Guaranteed
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${ }_{\text {5 K }} \mathrm{K}$. ohms up to 2 Meg.
No switch $3 /$-. D.P. SW. $4 / 6$
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 FERRODYNAMIGS "BRAND FIVE $5 \ln .600$ feet.5 in. 800 feet.
Sin. B00 feet...... 18/6 SuLAR DUPONT
7in. 1,200 feet $\because 235{ }^{2}$. Double Play

Spare Reels Min. 1/6; 4in 5 in.

RECTIFERS. RM1 5/-; RM2 6/-; RH3 8/-; RM4 16/RMS $20 \mid-;$ FC31 $2 \% / 6 ; 14 A 861 \geqslant / 6 ; 14 A 100$ 21/-
MINIATURE CONTACT COOLED RECTIFIERS $50 \mathrm{~mA} .7 / 6 ; 60 \mathrm{~mA} .8 / 6 ; 85 \mathrm{~mA}$. $9 / 6 ; 200 \mathrm{~mA}$. $21 /$ -
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Circuit and component book, using four 6 AMG $2 / 6$. Complete zit FMT1 with Jason Calibrated dial and 4 valves, $£ 6 / 5 /-$, or with New Jason Cabinet FMT2, £2
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 $2,500 \mathrm{Y}, 3 / 6 ; 0.001$ nifd., $2,000 \mathrm{~F}, 1 / 9 ; 500 \mathrm{pt}, 20 \mathrm{kV} .9 / 6$ CERAMIC CONDS. 500 v. 0.3 pif. to 0.01 mifl., 9 di .
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 $1 / 3.250$ pf.. $1 / 6$. 600 pt., 750 pt., 1/9. Phillips, $1 /$-e
NEW ELECTROLYTICS. FAMOUS MAKES

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161450 v .
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$237 / 25$
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# Wilkinsons 



MINIATURE RELAYS

| Siemens High | Speed Sealed |  |
| :---: | :---: | :---: |
| $2.2 \Omega+2.2 \Omega$ | H96A | $15 / 6$ |
| $50 \Omega \Omega+500 \Omega$ | H9GD | $22 / 6$ |
| $1700 \Omega+1700 \Omega$ | H96E | $25 /-$ |
| Siemens High | Speed Open |  |
| $100 \Omega+100 \Omega$ | H85N | $15 /-$ |
| $1000 \Omega+1000 \Omega$ | H95A | $17 / 6$ |

RELAYS P.O. TYPE 3000 Built to your own specification Keen Prices Quick Delivery
Contacts up to 8-Changeover KEY SWITCHES
Various P.O. types ex stock.



Comprehensive range available from stock

## MAGNETIC COUNTERS

Counting to 9999. 2-6 v. D.C., $15 /$ - each, post $1 / 6$. $75-120$ v. D.C., $15 /$ - each, post $1 / 6$. HIGH SPEED TYPE No. 100 c .,
$100-120$ v. D.C. $35 / \mathrm{m}$, post $1 / 6$.

ROTARY CONVERTER. Input 24 v. D.C. Output 220 V. A.C. 250 watts. Pedestal type with D.P. Ironclad switch. BRAND NEW, £17/10/-, carr. 15/BATTERIES. Portable Lead Acid type, 6 volts 125 ampere hours. In metal case $16 \mathrm{in} . \times 8 \mathrm{in} . \times 1 \mathrm{lin}$. (Two will make an ideal power supply for our 12 -volt Rotary Converters). Uncharged $86 / 10 /$ - each, carriage 15/24 volts 85 amperes, $\$ 14$ each, carriage $15 /-$.
NIFE BATTERIEs. Nickel Cadmium, 6 volts 75 amps. Crated and connected. Brand new $£ 7 / 10 /-$, carr. $15 /$. Special inter-crate connector supplied free with two batteries
WESTALITE BATTERY GHARGERS. Made by Westinghouse (type BC14-6/40). Input $200 / 250 \mathrm{v}$. A.C. will charge 6 -volt or 12 -volt batteries at $0 / 40$ amps. Coarse control switch with eight positions and fine at $0 / 40$ amps. Coarse control switch with eight positions and fine ammeter. Fused A.C. and D.C., grey enamel finish, dimensions ammeter. Fused A.C. and D.C., grey e
$24 \mathrm{in} . \times 14 \mathrm{in} . \times 13 \mathrm{in}$. 845 each. Carriage $20 /$ -

15 AMP. BATTERY CHARGER (Westinghouse Type B.C.3) will charge three lead acid cells at 15 amps. Input $200 / 250$ volts, 50 cycles A.C. Charging current is regulated by four-position switch and variable resistance for fine control. Fitted with $0 / 20$ ammeter, rotary on/of switch and rewirable
fuses. This first-class instrument at the bargain price of $\& / 5$, carriage $15 /$ TELEPHONE SET TYPE "A." Ringing and speaking both ways on a four-core cable. Carries the voice loudly and clearly over any distance. Two handsets are supplied as ulus. and the Suitable 4-core PVC cable 10d. per yd. Price 75/- set post $3 / 6$. TELEPHONE SET TYPE "K." The most compact telephone set available as the $4 \frac{1}{2}$. flat battery and buzzer is built-in to the hand instrument. Ringing and speaking both ways on twin wire. Instrument is complete with 5ft. flex. Easily hangs on he wall. Set of two instruments, $£ 5 / 10 /-$, post $3 / 6$. Two cor lex 3d. yard.
LOUDSPEAKER BARGAINS. AXIOM 150 dual cone 12in,, 15 watts 15 ohms. Fully dust proof, $27 / 19 / 6$, carr. $7 / 6$. ELAC 5 in. round, 3 ohms. $11 / 6$, post $1 / 6$ PYE 10in. Portable. 3 ohms. Built into wooden carrying case and complete with 45 ft . waterproof flex and jack plug, $50 / \mathrm{-}$, carr. $7 / 6$.
FANS INDUSTRIAL TYPE. $230 / 240$ volt A.C. Capacitor Motor, 16 in blades, adjustable louvres, filter. Ideal for paint shop. £20, carr. 25/-. AIR BLOWER powered by a 230 v. A.C. motor, $15 i n$ fan. Volume o free air at max. r.p.m. is $1,250 \mathrm{cu}$. ft. per min. At maximum efficiency $900 \mathrm{cu} . \mathrm{ft}$. per min. Brand new $\mathbf{2 5}$, carriage $30 /$.
CERAMIC WAFER SWITCHE8. Full list available.
1 Bank 1 pole 3-way ... 4/6 each 2 Bank 2 pole 4-way... 10/6 each 1 Bank 1 pole 5-way ... 5/6 each 3 Bank 1 pole 11-way... 18/- each $\begin{array}{lll}1 & \text { Bank } 2 \text { pole } 2 \text {-way } . . .5 / 6 \text { each } 3 \text { Bank } 6 \text { pole } & 2 \text {-way... } 7 / 6 \text { each } \\ 2 \text { Bank } 1 \text { pole 11-way ... 12/6 each } 3 \text { Bank } 4 \text { pole } 3 \text {-way.. } 7 / 6 \text { each }\end{array}$ 2 Bank 1 pole 11 -way ... 12/6 each 3 Bank 4 pole 3 -way... $7 / 6$ each
2 Bank 1 pole 12-way ... $7 / 6$ each 4 Bank 2 pole 4 -way... 18/6 each 2 Bank 1 pole 12 -way .... 7/6 each 4 Bank 2 pole 4 -way... $18 / 6$ each Others, incl. Paxolin types, 1 Bank $3 / 6,2$ Bank $5 /-, 3$ Bank $6 / 6$, post $1 /-$ HEADPHONES. High resistance $4000 \Omega$ with cords $17 / 6$, post $1 / 6$.

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230/240 volts, 50 cycles, 1,420 r.p.m. $\frac{1}{2}$ in shaft on Standard foot mounting or with sin. shaft, resilient mounting. Either type, \&5/10/-, carriage $10 /$.

VACUUM PUMP AND COMPRESSOR.
Edwards type IV, $\frac{1}{2} \mathrm{in}$. shaft, complete with fywheel, couplings, oil filter and union flywheel, couplin
$\mathrm{E} 6 / 10 /-$, post $3 / 8$.

## M

r.s.D.

100 Microamp 50 Microamp 250 Microamp 500 Microamp
1 Milliamp 2 Milliamp 30 Milliamp 100 Milliamp 1 Ampere 3 Ampere 5 Ampere 10 Ampere 20 Volts 30 Volts 40 Volts 500 Microamp 1 Milliamp 5 Milliamp 10 Milliamp 20 Volts 30 Volts 40 Volts 15 Amps 3 Amps 5 Amps 30-0-30 Amps 50-0-50 Amps 25 Amps D.C ${ }_{50}$ Amps A.C.

GUARANTEED
 Type
MCFR MC/FR $\mathrm{MC} / \mathrm{PR}$ $\mathrm{MC} / \mathrm{FR}$ $\mathrm{MC} / \mathrm{FR}$ $\mathrm{MC} / \mathrm{FR}$
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$\mathrm{MC} / \mathrm{FR}$ $\mathrm{MC} / \mathrm{FS}$ $\mathrm{MI} / \mathrm{FR}$
$\mathrm{MI} / \mathrm{FR}$ MI/F or PR MI/FR
 WEE MEGGER. 500 volt. In leather cartying case s $17 / 10 / 0$, post $3 /$ FREQUENCY METERS. $45-55$ cycles per second, 230 volts, $6 i n$ dia. Flush Round. Brand new in maker's box. $810 / 10 /$-, post $3 / 6$.

$$
\begin{aligned}
& \text { Round. Brand new in maker's box. } 210 / 10 \text {-, post } 3 / 6 \text {. } \\
& \text { METER REGTIFIERS } 1 \text { M.A., } 5 \text { M.A, F.W. bridge, } 8 / 6 \text {, post }
\end{aligned}
$$

AMMETER. $0-3$ amps. D.C., by Turner, MC/FR, 6 in. $90 /-$, post $2 / 6$. MICROAMMETER. 250 F.S.D. $3 \frac{1}{2} \mathrm{in}$. F.R. Sangamo Mod. S37. Scaled for valve vol tmeter. Circuit available free, $55 /-$. post $1 / 6$.
UNI-PIVOT GALVANOMETER, by Cambridge Instruments, $50-0-50$ micro amps, dia. 4 in . Knife pointer, mirror scale. Complete with leather carrying case. Ideal for laboratory use, $£ 10$, carriage $3 /-$
PORTABLE VOLTMETER. $0-100$ volts A.C.ID.C., accuracy within $2 \%$ 8 in. mirror scale, knife pointer, in polished case. A precision moving iron nstrument at a very low price, $£ 4 / 19 / 6$, post $3 / 6$
PORTABLE AMMETER. $0-3$ amp. A.C./D.C. 3 in. scale in case $35 /-$, post $2 / 6$ AVO TEST BRIDGES. $220 / 240$ volt A.C. Measure capacities from 5 pf to 50 mfd . and resistances from 5 ohms to 50 megohms. Valve volt-meter range 0.1 to 15 volts and condensers leakage test, $£ 9 / 19 / 6$, post $3 /-$ RACK8-POST OFFIGE STANDARD. Oft. high with U-channel sides
drilled for 19 in. panels, heavy angle base. drilled for 19 in . panels, heavy angle base.

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RESISTORS EX STOCK IN QUANTITY. WIRE WOUND, HIGH STABILITY CARBON, ETC. BEST MAKES AT LOWEST PRICES ALSO POTENTIOMETERS AVAILABLE


WONDERFUL VALUE ONLY 15/6. Post $1 /$-. Weighs only two ounces. 7,000 r.p.m. Reversing switch. Free length of polythene drive.

## ATTENTION ALL MANUFACTURER8.

ONE HOLE FIXING SWITCHES. Singlepole double-throw 3 amp., 250 volts A.C. 1/6 each. 12/- doz., $£ 37 / 10 /-$ per 1,000 . Ask for quotation for 5,000 or upwards. 100,000 available from stock now!
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CATHODE-RAY TUBES. VCR 139A, $2 t i n$. diam., $30 /-$, post $3 /-$
BARTLETT ELECTRIC DRYING OVENS. Internal dimensions $20 \mathrm{in} . \times$ $20 \mathrm{in} . \times 20 \mathrm{in}$. 230 volt A.C. with adjustable thermostat giving automatic Remperatures up to $160^{\circ}$ shown on built-in gauge

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Kita comprise-six 2部. dia. Tubular Bicel Bections of 6 it length, top-section aud base Prckets, Guys and Fittings. Y00 can purchase this normally expensive MAST for a fraction of lta cost. Please add $\begin{aligned} & \text { able) wooden carrying case }\end{aligned}$ able) wooden carrying case. larly suitable to take aerials for Tx., Rx.
F.M. F.M. and TV (especially orerseas. Exyta plied at $17 / 6$ per bection £8.10.0 only U.S.A. Type 45ft. TELECOM. AERIAL MAST. (7 sections, 6it. Bin. $x$ 2tin., guys etc.). This entirely complete set in carrying case $12 \frac{1}{2}$ Gns. Carr. 17/6. Or 2 sets for $£ 25$. Carr. extra. British Manufacture only.
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World Famous TELLPHONES "F " TYPE in Attractive Case

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## finest quality brass. Non-rusting. Base

 diameter 2 in. Complete with hand-winding winch for easy, rapid extension; and cablewire bracing stays. One of the best masts ever produced.Winds down to $9 f$ t.

## NEW! MINIATURE PANEL METERS "S"METER MODEL SR.2P. Standard "Hamn "' Signal strength indicator. Calibrated

Precigion bullt clear plastic miniature pane, meters. Featurlag d'arsonval movements, jewelled bearing, kilvered dials with black numerals and pointers. Accuracy $2 \%$ of full scale. $1.21 / 32 \mathrm{in}$. square fronts, 1 lin. overall front to back. Require 1 tin. diameter round hole in panel. All have clear plastic fronts with zero aljustment screw in" units from 0.9 with scale terminating in +10 to +30 db calibrations. Additional amateurs for conversion of any Commanication Recelvers with AvC action to give
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VO METER MODEL VR, 18 . Calibrated and damped In accordance with standard VU Meter Practlce. Upper scale reads -20 to $+3 V U$. Lower scale reads $0.100 \%$ modulation. Uses precision carbon film multiplier resistor and full wave recti民er, 42/6. Model MR.250, 0 to 500 цA. 32/6.
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All Models Individually Boxed and Fully Guaranteed. P. \& P. $2 / 6$ each


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## A.R. 88D RECEIVERS

Frequency coverage $550 \mathrm{kc} / \mathrm{s}$ to $32 \mathrm{Mc} / \mathrm{s}$ supplied fully reconditioned and in perfect working

LAPEL MICROPHONE 178 Precision engineered Crystal Mic-rophone-for lapel or hand use. Only I $\frac{1}{2}$ in. dla. Exceptionally sensicive. Chrome-plated case and $17 / 6$. P. \& P. I/-


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10,000 O.P.V. on BOTH A.C. and D.C Ranges: D.C. Voltage: $0-6-30-120-600-1,200 \mathrm{v}$. (10,000 o.p.v.)
A.C. Voltage: $0-6-30-120-600-1,200 \mathrm{v}$. ( 10,000 o.p.v.).
D.C. Current: $0-120 \mu \mathrm{~A}, 0-12-300 \mathrm{~mA}$. Resistance: $0-20 \mathrm{~K}, 0-2 \mathrm{Meg}$. ( 150 ohm, 15K at centre scale). Capacitance: 0.005 to $0.15 \mu \mathrm{~F}$ (at A.C. 6 v.). Decibels: -20 to $\pm 63 \mathrm{db}$ ( 600 ohms I mW ., odbm $=0.775$ v.).
Accuracy: D.C. voltage and current $\pm 2 \%$ .s. A.C. Voltage $\pm 4 \%$ f.s. Resistance $\pm 3 \%$ of total scale length
Size $4 \frac{1}{2} \mathrm{in}, \times 3 \mathrm{in} . \times \mathrm{lin}$. Complete with test 55/1916.

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Here is value in transistor transformers consisting of one Driver Transormer and one Output Transformer pair for miniature ransistor portables Driver Model LT44: Primary: 20k. Secondary: 1k. Centre Tapped. Ratio: 5 : 1 Output Model LT700: Primary: 1.2 K . Centre Tapped. Output: 3.2 ohms. Ratio: 20 : ONLY 9/6 per pair. P. \& P. I/6.

SLIM RADIO PLUG AND SOCKET P.3I Two way, black bakelite, solder terminal plug. SOCKET standard JACK ing, neat finish $5 / 6$ pe
 reproduction of the finest quatity. Supplied free is a small transformer unit with cord and plug which steps
impedance up to $4,000 \Omega$. Only $15 /-$. P. \& P. 2/6.

RH-20 RADIO HEADPHONES Hi-impedance-2,000 ohms-general use headset. Black and vory plastic cased electro-magnetic unics with adjustable Meadivand listening for all types ofapplica tions. Individually packed, with flexible cord attached. 14/6,
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> NEW DYNAMIO
MICROPHONE MICROPHONE
Model DM-175. Bean. Model DM-175. Beau-
tifully designed and titulractively finished Lightweight, complete with stand Output imp. 1 K . ohm. freq. respons $150-9,000$ c.p.s.

$\pm 3 \mathrm{db}$. Sensitivity $\pm 73 \mathrm{db}$. Ideal for almost all applica | tions. |  |
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| F. | 29/6. |

P. 217 A. MINIATURE 2 $\frac{1}{2}$ IN. SPEAKER A miniature $\mathrm{Hi}-\mathrm{Fi}$ speaker that out-performs all others. Designed to meet oday's requirements for transistor, miniature and sub-miniature applications. Size: $2 \frac{1}{2}$ in. square $x$ lin deep.
Voice coil impedance: $\theta$ ohms. Freq range: 150 $5,000 \mathrm{c} / \mathrm{s}$. Power: 200 MW


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New lightweight portable megaphone. Features removable micro phone for remote operation. Extreme battery economy despite high sound volume output. Features pistol grip switch, lightweight spun aluminium horn. Weight only 4 lb . $\& 14 / 10 \%$ Post paid.
SUB-MINIATURE
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MODEL RA.II

## TRANSISTOR TAPE RECORDER

Size only $6 \mathrm{in} . \times 8 \frac{1}{4} \mathrm{in} . \times 2 \frac{3}{4} \mathrm{in}$. and weighs a mere $2 \frac{1}{2} \mathrm{lb}$. Fully transistorised complete with mike, earphone, built-in speaker and amplifier. Powered by economy. Records and plays for over one hour on standard 3in. reel. (34 minutes each track.) The RA.! I is a precision miniature cape recorder which slips easily into a brief case or handbag. P.M. speaker and amplifier. Engineered for ease of operation. All controls are accessible on front panel. The magnificent two-cone plascic and meral case farures a carrying handle and snap open top for fast, easy tape loading. Complete with batteries, tape and accessories.

| $\begin{aligned} & \text { "AGOSY" RECORD } 19 / 6 \\ & \text { PLAYER CABINET } \end{aligned}$ |
| :---: |
| Exceptional offer. A lightweight portable player Cabinet in Rust or Cream. Famous manufacturer. Size $14 \frac{1}{2} \times 11 \frac{1}{2} \times 6$ in. Takes our single player; 2 control Amplifier; 5in. Speaker. Post, Paciking and Insurance 5/6. |

## TAPE RECORDER AMPLIFIER <br> Compact welldesigned 5 -valve Input for Microphone, Radio and Gram. Size $8 \frac{1}{3} \times 3^{\circ} \times 4{ }^{2} \mathrm{in}$ and Gram. Sila <br> Extras: Dial plate including sockets and superimpose 

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Ex-manufacturer's salvage, "Money Back Guarantee."
5,6 and 8 Bin . round and $7 \times 4$ 4in. elliptical and others.
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## MINIATURE SPEAKERS 16/9

New, $2 \frac{1}{2}$ and 3 in . P. \& P. $1 /$-.
ELLIPTICAL SPEAK
New, slot type. $8 \times 3$ in. and $7 \times 4$ in.
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only 12/6


12 v. (special
atispor for $200 \mid$
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tra). Automatic solder feed including reel solder and spare parts. It is a tool for electronic soldering or car wiring. Revolutionary in design. Cannot burn. for wise. posts 316 .

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114 6/9. 879 9/9. 873 8/9. EDISWAN
$X C 121$ and $\mathrm{XB} 1138 / 9$ each. POST FREE
COMPLETE 17in. TELEVISION £11. 10.0
An excellent ex-Rental Table model. Famous manufacturer. Tuned ITA/ $B B C$. Guaranteed 12 months. Terms available. Personal collection advised. Special delivery rate by
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* Acos mic. 39/I. Crystal stick microphone for use as a hand, desk or floor stand unit. Listed at 3 gns . OUR PRICE 30/6. Table Stand $7 / 6$ extra. Floor stand adaptor, $12 / 6$ extra.
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 FOR D.C. \& A.C. APPLICATIONSEngineered to prectsion standards, this high-grade instrument os mado available at the lowest usually assoclated with luxury instruments. This "SCOPE" will appeal particularly to Service Engineers and Amateura. A high gain, extremely stable differential Y-Amplifler ( $30 \mathrm{mV} / \mathrm{C} . \mathrm{M}$. ). Provides ample sensivity with A.C. or Dor measurement inputs. Especialty suitable for measurement tenance of D.C. levels is of paramount importance. Pueh-Pull X amplifier; Flyback suppression; Internal Tinee base Ecan Waveform avallable for external use; pulse/output available for checking cxternal X $1 / \mathrm{P}$ and CRT. Brightness Modvlation. A.C. mains $200 / 250 \mathrm{~F}, \mathrm{S15/15/-plus}$ P. \& P. $7 / 6$ or $30 /$ deposit, plue P. \& P. $7 / 6$ and 12 monthly payments of $26 / 6$.
FULL 12 MONTHS GUARANTEE INCLODNE VALVES AND TUBE.

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A.C. MAINS $200 / 250$ volts. Provides:OPERATION, for FM/TV alignment linear frequency sweep up to $12 \mathrm{Mc} / \mathrm{s}$. From $400 \mathrm{Kc} / \mathrm{s}-80 \mathrm{Mc} \mathrm{Mc}$. CAPACITANCE MEASUREMENT. Two ranges provided $0-60 \mathrm{pf}$. and $0-120 \mathrm{pf}$. SPECIAL FACIL-
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Will tune to all Band I and Band III stations. BRAND NEW by famous manufacturer. Complete with P.C.C. 84 and P.C.F. 80 vitives (in series). IF. 16-19 or 33-38. Also can be modified as an aerial converter (instructions supplied).
Complete with knobs.
32/6
Plus $3 / 6$ P. \& P.


## HEATER TRANSFORMER <br> To suit the above, $200-250$ v. $8 /-$ plue $1 / 6 \mathrm{P}$. \& $\mathbf{P}$

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4 -speed plays 10 records 12 in . 10 in . or 7 in , at 16,33 , 45 or 78 r.p.m. Intermixes 71 n ., 10 in . and 1 lin. records of the same speed. Has manual play position; colour brown. Dimenkions: 12引n. $\times 10$ in. Space required with Ful-Fi turnover crysial head. $£ 6 / 19 / 6$. Plus $5 /-$ F. \& P.

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\section*{EMI \\ Interesting vacancies have occurred in the Calibration Department of the Feltham Laboratories of EMI Electronics Lid. for the following: \\ ENGINEER \\ to carry out the maintenance, modification and calibration of test gear equipment to A.I.D. standard. Candidates should have at least two years' experience of this work and also hold qualifications up to H.N.C. (Electrical Engineering) standard. \\ TECHNICAL ASSISTANT \\ to assist an Engineer in the carrying out of the work detailed above. Experience in the servicing of test gear, either in the Armed Services or industry is essential. An O.N.C. (Electrical Engineering) would be a distinct advantage. \\ Initial salaries will be determined by qualifications and experience and it is Company practice to review salaries annually on the basis of ability and potential. \\ Applicants should write, giving full details and quoting Ref. Aa/8/x, to: \\ Personnel Manager, \\ EMI ELECTRONICS LTD., HAYES, MIDDLESEX.}

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We are looking for men with enthusiasm and initiative to join our development team 1. FACTORY TEST GEAR DEVELOPMENT ENGINEER

The man appointed will be engaged on varied work, applications ranging from L.F. to U.H.F. While H.N.C. with 3 years' experience in the Radio and T.V. field would be desirable a man with a good technical background coupled with experience would be considered. Preferred age group 25 to 35 .

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For this appointment T.V. experience preferably on the Tuner and R.F. side is essential.
The work will initially be on printed circuit T.V. tuners, but opportunity exists for a young Engineer of ability to continue his studies and broaden his scope. Preferred age under 28.

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This is a Senior appointment and age is of secondary importance.
These appointments offer the opportunity to work for a Company who have been pioneers in the development of electronic equipment.
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Letters of applicarion which should be accompanied by tabulated details of education, experience and present salary, will be treated in strict confidence and should be addressed to:-

Personnel Officer
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FLEETS LANE,
POOLE, DORSET.

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Vacancies for radio technicians aged 19 or over at Airports and Radio Stations throughout the United Kingdom maintaining radio communication and electronic navigational aids.
A fundamental knowledge of radio with some practical experjence required for entry. Training given on the equipment in use.

Salary according to age and station, approx. \(£ 810\) at age 25 , rising to \(£ 930\).
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Facilities to study for higher qualifications giving good prospects of pensionable posts and promotion to Telecommunications Technical Officer Grades with salary maximums \(£ 988\),
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Apply for further details to Ministry of Aviation (EST/5a), Room 755, The Adelphi, John Adam Street, London, W.C.2, or any employment exchange quoting order No. Westminster 3552).

VACANCIES FOR RESEARCE AND DEVELOPMENT CRAFTSMEN IN GOVERNMENT SERVICE electrical (1) Radio mechanics for the maintenance and instatlation of \({ }_{\text {ration }}^{\text {radio comm }}\)
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- telegine
- maintenance or
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A thorough basic knowledge of elecoronics and the ability to maintain equipment is essential. Industrial experience in an allied industry would be an advantage.
Salaries are in the range of \(£ 891-£ 1560\) p.a.


Applications must be made in writing to: The Personnel Manager, ABC Television Ltd., Broom Road, Teddington, Middlesex.

\title{

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Candidates, between 20 and 30 years of age and single must be able to transmit and receive morse at \(20 \mathrm{w} . \mathrm{p} . \mathrm{m}\). (plain language or code) and be capable of elementary maintenance of wireless transmitting and receiving equipment
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\begin{abstract}
Windscale and Calder Works, and Chapelcross Works require experienced men with knowledge of electronic equipment and/or industrial instrumentation for fault diagnosis, repair and calibration of a wide range of instruments used in nuclear reactors, radiation laboratories and chemical plant. This interesting work involves the maintenance of instruments using pulse techniques, wide band low noise amplifiers, pulse amplitude analysers, counting circuits, television and industrial instruments used for the measurement of pressure, temperature and flow.
\end{abstract}

Men with Services, Industrial or Commercial background of radar, radio, television, industrial or aircraft instruments are invited to write for further information. Training Courses in Specialised Techniques are provided for successful applicants having suitable Instrumentation background.

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Applications to:
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The Head of the Department of Physics.

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have the following staff vacancies in the design and development department of their West London works:
ELECTRONIC ENGINEER with experience in the design of transistor line transmission equipment and filter networks.
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JUNIOR DRAUGHTSMAN to work with the above team.
These vacancies are permanent and pensionable, and occur in a rapidly expanding company.
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Salaries will be in accordance with qualifications and experience.

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ONE ESTIMATOR FOUR TEST ENGINEERS
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Full-time One Year Course in Radio and Television. College course in basic principles for prospective servicing engineers.
Next course commences 5th Seprember 1961
This course is recognised by the Radio Trades Examination Board (R.T.E.B.) for the new Servicing Certificate examinations.

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A. Radio and Television Servicing.
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For details, write to:

\section*{The Principal, p11 \\ THE PEMBRIDGE COLLEGE OF ELECTRONICS}

34 a Hereford Road, London, W. 2

\section*{ENGINEERING AUTHORS}

One of the leading Companies in the electronics field located in the Home Counties, wishes to strengthen the Group responsible for preparing technical publications and maintenance manuals of their products. Vacancies exist for Senior Authors in the Radar, Data Processing, Microwave Communications, High Power Transmitter and Television Studio fields. These are senior appointments on the Company's permanent staff. Salaries will be attractive and will normally be in the range \(£ 1,100\) to £1,400 p.a.
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1. Staff to maintain the electronic equipment of our computers. We require both Junior and fully qualified engineers. Applicants for junior posts should have G.C.E. "A" level in Physics and Mathematics and an active interest in electronics.
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For all posts full training will be given and there are excellent prospects for advancement.
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New term commences 25th September. 1961
Prospectus free on application to Secretary.

\section*{ASSISTANT ENGINEER GRADE I (RADIO)}

Required by TANGANYIKA GOVERNMENT, Police Department, on contract for one tour of \(21 / 27\) months, commencing salary (including Overseas Allowance) \(£ 1,287\) a year in scale rising to \(£ 1,671\) a year. Gratuity \(25 \%\) of total salary drawn. Outfit allowance £45. Free passages. Liberal leave on full salary.
Candidates, under 40 years of age, must have a wide experience of installation, running and maintenance of medium and low powered H.F. and V.H.F. equipment together with ancillary apparatus. Experience of telephone and teleprinter practice, erection of lattice and other masts and installation and maintenance of generating plant an advantage.
Apply to CROWN AGENTS, 4 Millbank, London, S.W.1., for application form and further particulars, stating age, name, brief details of qualifications and experience and quoting reference \(\mathrm{M} 2 \mathrm{~A} / 51288 \mathrm{WF}\).

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Successful candidate will be required to take up appointment as soon as possible.

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Please witte to
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The Computing Division of Elliott Brothers is engaged upon the design and prototype construction of a new high speed digital computer.

A number of vacancies for Technical Assistants exist on this project, giving opportunitics to gain experience of high speed circuit and logical design techniques.

Applicants should have already completed at least second year O.N.C. (Elec.), Inter Applicants should have aready completed at ieast second year O.N.C. (Elec.), pursue their studies on a day release basis with a view to obtaining a final qualification

Please write initially to the Personnel Manager (Ref.: 610),
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\section*{INDEPENDENT TELEVISION AUTHORITY}

The Independent Television Authority has vacancies for Engineers at its Transmitting Stations. The work calls for a high degree of skill and knowledge of electronics and consists of the operation and maintenance of television transmitters and ancillary equipment. Applicants need not be experienced as training will be given to suitable candidates who have the necessary basic knowledge. Shift work is required, but the normal hours of working are between \(8 \mathrm{a} . \mathrm{m}\). and midnight.
The Authority is a growing organisation which plans a number of new Transmitting Stations. These will demand qualified staff, and it is the Authority's policy, where possible, to promote its own staff to fill the higher grade vacancies.

Spare-time study is encouraged by reimbursing the cost of approved courses; and full-time study courses at no cost to the employee are available to selected engineers within the Authority.

Conditions of service are excellent and include a contributory pension scheme and a generous house purchase assistance scheme which is available after a qualifying period of service. Transfer allowances are paid on transfer from one station to another, and consideration is given in some cases for certain removal allowances to be paid to married men on first appointment.
The Authority would welcome applications from young men who have a good basic knowledge of electricity, electronics, radio or radar; and preliminary interviews can be arranged in various parts of the country. Starting salaries would be offered between \(£ 780\) and \(£ 1,270\), and those who possess a degree in engineering or equivalent qualification such as Higher National Certificate, could be considered, after a period of experience with the Authority for a grade with a maximum of \(£ 1,425\) per annum. Thereafter promotion is by merit, and the higher grades carry salaries in excess of \(£ 2,000\) per annum. Applications should be submitted to the Personnel Officer, I.T.A., 62, Brompton Road, London, S.W.3, giving age, qualifications, and experience, and quoting ref. number WW/E/36.

\section*{THE AUSTIN MOTOR COMPANY LIMITED require ELECTRONIC ENGINEERS}

A for: Maintenance of Electronic Data Processing Equipment. Both Valve and Transistor Techniques as well as Magnetic Drums and cores are involved with a variety of input and output equipment.
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\section*{ALSO}

B for: Evolution and Engineering of control systems. These long-term projects embrace advanced relay logic, static switching and data transmission.
Whilst academic qualifications are desirable, the prime requirements for these posts are inventiveness, a flair for logical design and proven ability to convert ideas into sound engineering.
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50-0-50 \\
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[^0]:    * Roval Radar Establishment.
    $\dagger$ Physical Society Exhibition-January, 1961.
    $\ddagger$ U.K. Patent Application No. $42094 / 60$.

[^1]:    P 7.S.M.P.T.E, Vol. 69, No. 12, p. 868, A New Video-Tape Recording System, by Norikazu Sawazaki, Motoi Yagi, Masahiro Iwasaki, Genya Inada and 「akuma Tamaoki.

[^2]:    *Lecturer, South Shields Marine and Technical College.

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[^4]:    ${ }^{1}$ H. L. Armstrong, Electronic Technology, June 1961, p. 229.

    * Proc. I.E.E., January 1956, p. 35.

[^5]:    ${ }^{1}$ Mullard Reference Manual of Transistor Circuits, p.13.

[^6]:    * Mullard Research Laboratories, Redhill.

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