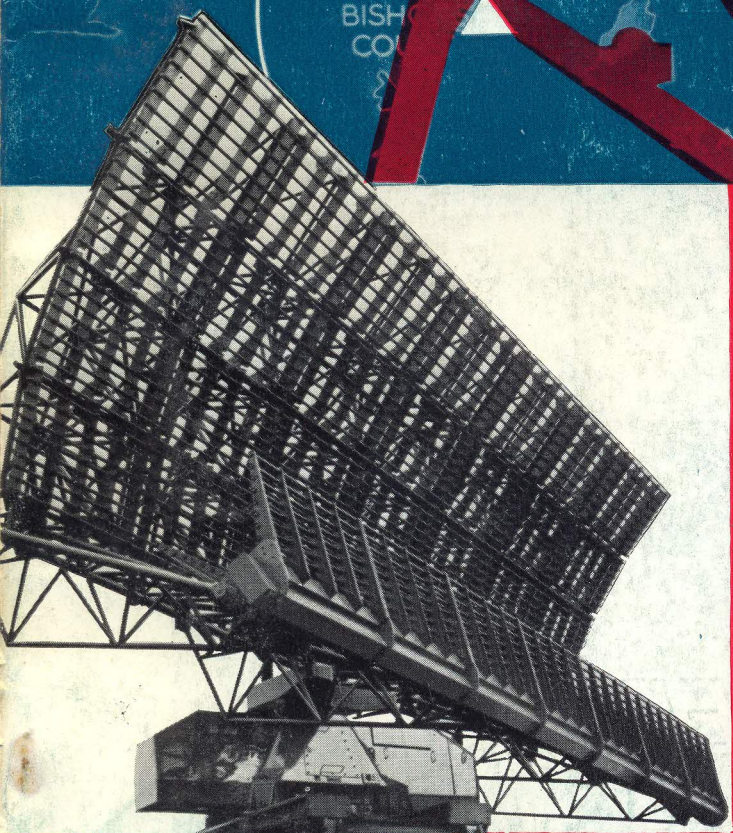


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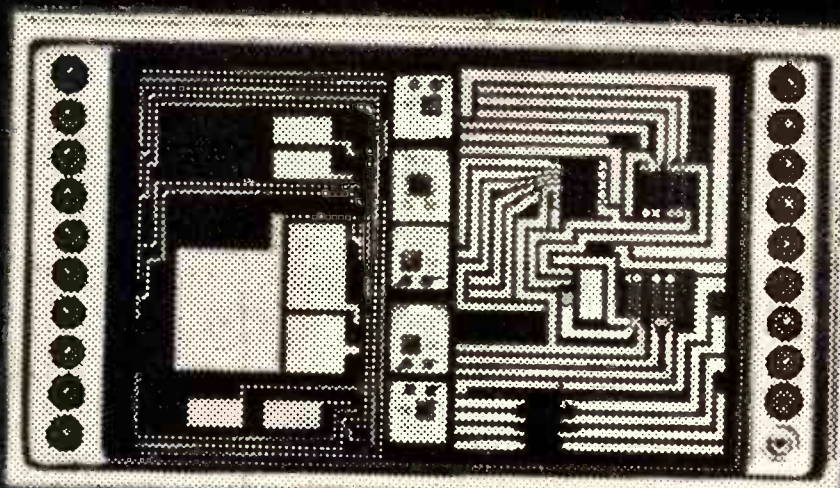
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ELECTRONICS, TELEVISION, RADIO, AUDIO

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## Who Designs Systems — and How Well?

APPOINTMENTS and situations-vacant advertisements, some in large display panels, are making us aware of a new breed of specialist called a systems engineer. Sometimes he is given a specific “discipline”—telephone, computer, avionics—but often just as a “systems engineer.” From the blurb in the advertisement it appears that the wanted engineer is mainly an electronics man, although he is not to be concerned with the detailed design of specific pieces of equipment. He apparently has to build up existing pieces of equipment or known techniques into systems primarily for the transmission, processing and presentation of information. On his work may depend the safety of human lives—as for example in the new National Air Traffic Control Scheme described in this issue, and a plane’s automatic landing system—or the operation of vast industrial plants.

Where do these systems engineers come from? How are they trained and how do they get their experience? These questions ought to be examined, as it does not appear that there is any established machinery for training them. One might go so far as to say that they are virtually amateurs, picking up expertise as they go along.

An important aspect of systems engineers’ work is reliability. In electronics and communications we tend to think of reliability mainly in terms of immunity from breaking down of components or equipment, and of circuit designs having good safety factors, etc. These things are all necessary of course in the individual parts of systems, but are not enough in themselves to ensure system reliability.

For example, a system can fail even though all the electronics are working perfectly. In an information processing system a situation could arise where more digits are being fed into a store than it will actually hold: the capacity of the store is exceeded and there is consequently a loss of accuracy or a complete breakdown.

Redundancy, therefore, plays a vital rôle in achieving reliability in the design of systems, as indeed is the case with animal nervous systems so that part of the “hardware” can be damaged and yet the overall system carries on. An example of a system achieving reliability through redundancy is the automatic landing system being designed for the Trident and other aircraft. This is a triplicated system with a majority vote scheme for ensuring correct operation. If two out of the three autopilots give the same output it can be assumed that that output is the correct one. If only two autopilots were installed, and they gave different outputs, how would one know which was correct?

Redundancy design techniques are a complex of economics, logic, statistics (including probability theory), information theory, etc., and the systems engineer, while being at heart an electronics man, must, it would seem, be a “generalist” rather than a “specialist.”

**VOL 71 NO 9**  
**SEPTEMBER 1965**



# A Simple Transistor F.M. Tuner

## DESIGN USING A PULSE DISCRIMINATOR AND AN LC-TUNED LOCAL OSCILLATOR

By J. C. HOPKINS,\* B.Sc., Grad.I.E.E., A.Inst.P

**F**OLLOWING the publication of the "Wireless World F.M. Tuner" (July 1964) some interest seems to have been aroused again in the pulse counting type of receiver. P. J. Baxandall<sup>1</sup> has also pointed out that a simplified version using an LC-tuned local oscillator, and employing valves, had been designed and built by him some years ago. The following is a description of a transistor tuner designed along similar lines.

### R.F. and mixer stages

These are shown in Fig. 1. The aerial is coupled *via* a coaxial cable to the emitter of  $Tr_1$  which acts as a common-base amplifier. The operating current of the stage is set at about 0.7 mA and this yields an input impedance which approximately matches the input cable. Since this impedance is somewhat inductive at 90 Mc/s, it can be rendered resistive by simply adding the tuning capacitor  $C_2$ .

The r.f. stage is capacitively coupled to the base of  $Tr_2$  which acts as a self-oscillating mixer. As suggested by Baxandall, a 45 Mc/s local oscillator frequency was tried, the second harmonic of this beating with the signal to produce the required i.f. (at about 200 kc/s.). However this was found to produce a high level of second harmonic signal at the aerial terminals and so it was decided to employ a 30 Mc/s oscillator and tolerate the lower value of conversion gain produced. As a result, the gain of the r.f. stage slightly more than compensates for the loss incurred in the mixer! Nevertheless an overall sensitivity of the order of 100  $\mu$ V is achieved.

The oscillator configuration employed is a modified Clapp type, the transistor operating in common-base mode so far as this action is concerned. The base is connected to earth *via*  $L_3$  and  $C_7$  which is broadly series resonant near 30 Mc/s. This reduces the fundamental component of the local oscillator signal fed back over the r.f. stage. A rejector circuit ( $L_2, C_6$ ) for 60 Mc/s is also included. At the same time, these components are chosen so that at 90 Mc/s they balance the capacitive part of the input impedance of  $Tr_2$ , thus assisting the signal transfer from the r.f. stage. The oscillator frequency is stabilized against ambient temperature changes by using a resistive biasing network which renders the change in collector current with temperature quite small and the final compensation is achieved by giving the capacitor  $C_{11}$  a negative temperature coefficient. This is achieved by the parallel combination of a high-stability capacitor with a ceramic type having a coefficient of  $-750$  p.p.m. per  $^{\circ}$ C.

Intermediate frequency signals are taken at low impedance from the emitter of  $Tr_2$  *via*  $R_{10}$  and the low pass filter  $L_5, C_{16}, L_6$ . The latter gives a fairly level response up to about 350 kc/s but attenuates at higher frequencies quite sharply, the mutual inductance of the two windings series resonating at about 2 Mc/s with  $C_{16}$ . This gives good rejection of the adjacent f.m. channels which produce beat frequencies in a region where the gain of the i.f. amplifier is still significant. It was found that a standard 470 kc/s i.f. transformer could be used to produce this filter, the usual winding inductances (without

\*Bristol College of Science and Technology.

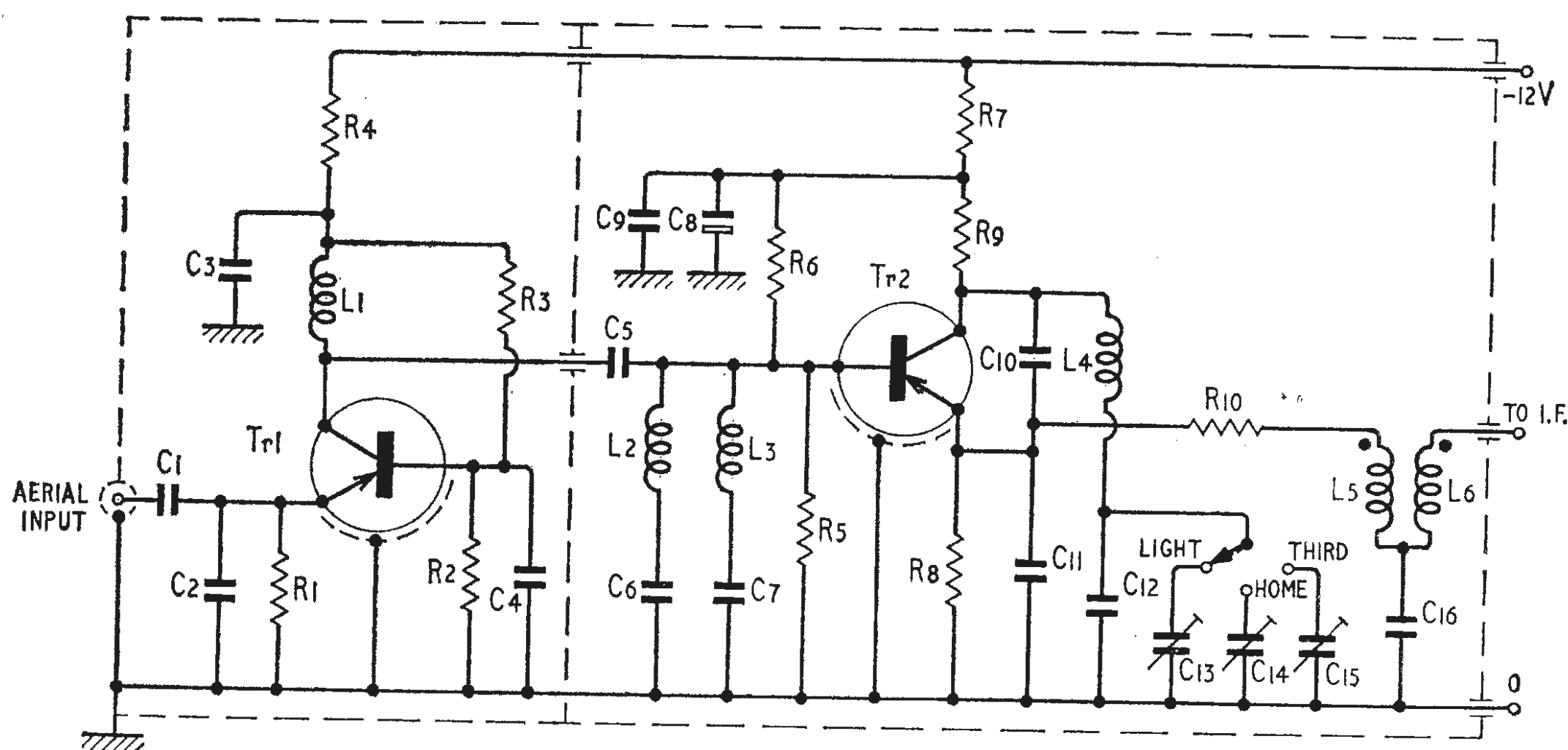
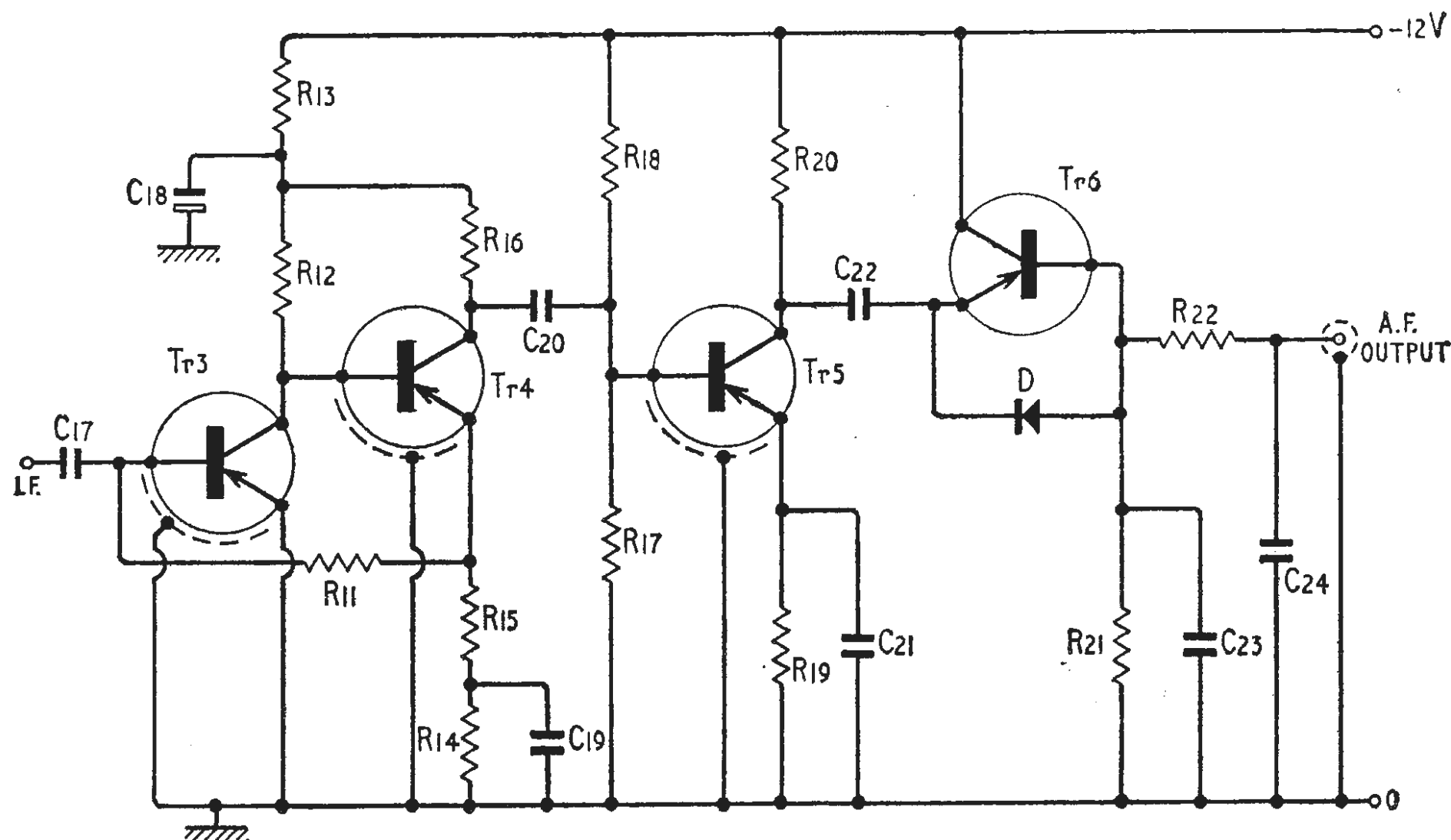


Fig. 1. R.F. and mixer stages.



Fig. 2. I.F. and discriminator stages.



the normal tuning capacitors) and the coupling between windings being quite suitable for the job in hand.

### I.F. and discriminator sections

These are shown in Fig. 2.  $Tr_3$  and  $Tr_4$  form a directly coupled pair with feedback both at d.c. (to achieve

temperature stabilization) and at signal frequency where it usefully levels the frequency response and reduces gain changes produced by the different samples of OC171.

$Tr_5$  acts as final amplifier stage and is over-driven to produce a limiting action. A rectangular wave of approximately 11V pk-pk appears at the collector, the limiting

### LIST OF COMPONENTS

#### Resistors

$R_1$	1k $\Omega$	$R_{12}$	10k $\Omega$
$R_2$	1k $\Omega$	$R_{13}$	1k $\Omega$
$R_3$	10k $\Omega$	$R_{14}$	680 $\Omega$
$R_4$	1k $\Omega$	$R_{15}$	100 $\Omega$
$R_5$	3.9k $\Omega$	$R_{16}$	6.8k $\Omega$
$R_6$	10k $\Omega$	$R_{17}$	3.3k $\Omega$
$R_7$	1k $\Omega$	$R_{18}$	27k $\Omega$
$R_8$	2.2k $\Omega$	$R_{19}$	470 $\Omega$
$R_9$	2.2k $\Omega$	$R_{20}$	2.7k $\Omega$
$R_{10}$	2.2k $\Omega$	$R_{21}$	3.9k $\Omega$
$R_{11}$	39k $\Omega$	$R_{22}$	15k $\Omega$ ( $\pm 5\%$ )

All resistors  $\frac{1}{2}$  W,  $\pm 10\%$ , carbon, unless otherwise stated.

#### Capacitors

$C_1$	0.001 $\mu$ F, disc ceramic.
$C_2$	4.7pF $\pm 10\%$ , ceramic.
$C_3$	0.001 $\mu$ F, disc ceramic.
$C_4$	0.001 $\mu$ F, disc ceramic.
$C_5$	3.3pF $\pm 10\%$ , ceramic.
$C_6$	10pF $\pm 1\%$ , silvered mica.
$C_7$	25pF $\pm 1\%$ , silvered mica.
$C_8$	10 $\mu$ F, 15V sub-miniature electrolytic.
$C_9$	0.001 $\mu$ F, disc ceramic.
$C_{10}$	220pF $\pm 1\%$ , silvered mica.
$C_{11}$	218pF: 68 pF $\pm 1\%$ , silvered mica, in parallel with 150pF $\pm 10\%$ , ceramic.
$C_{12}$	68pF $\pm 1\%$ , silvered mica.
$C_{13}$	3-30pF concentric trimmer.
$C_{14}$	
$C_{15}$	
$C_{16}$	624pF: 68pF in parallel with 556pF, both $\pm 1\%$ , silvered mica.
$C_{17}$	0.01 $\mu$ F $\pm 20\%$ , 250V polyester.
$C_{18}$	1 $\mu$ F, 15V sub-miniature electrolyte
$C_{19}$	0.1 $\mu$ F $\pm 20\%$ , 250V polyester.
$C_{20}$	0.01 $\mu$ F $\pm 20\%$ , 250V polyester.
$C_{21}$	0.1 $\mu$ F $\pm 20\%$ , 250V polyester.
$C_{22}$	68pF $\pm 1\%$ , silvered mica.
$C_{23}$	2700pF $\pm 1\%$ , silvered mica.
$C_{24}$	3600pF $\pm 1\%$ , silvered mica.

#### Inductors

- $L_1$  6 turns 22 swg (enamel)  $\frac{1}{2}$ in dia., spaced to about  $\frac{1}{2}$ in long (self supporting).
- $L_2$  13 turns 26 swg (enamel), close wound on 1W carbon resistor of high value ( $\frac{7}{8}$ in dia.).
- $L_3$  19 turns 26 swg (enamel), close wound as for  $L_2$ .
- $L_4$  8 turns 18 swg (enamel)  $\frac{1}{2}$ in dia. close wound (self supporting).
- $L_5, L_6$  Standard 470 kc/s i.f. transformer (Radiospares) with dust cores removed.

Connect "start" ends of windings together.

#### Switch

Single pole, 3-way wafer switch (Radiospares).

#### Semiconductor devices

- $Tr_1$ - $Tr_5$  OC171.
- $Tr_6$  OC41.
- D OA10.

#### Notes

- (a) Total consumption: about 8mA at 12V.
- (b) The supply voltage should preferably be held to about  $12 \pm 1$ V. This could most conveniently be derived from the mains and roughly stabilised with a Zener diode to achieve the value required.
- (c)  $R_{14}$  (nominally 680 $\Omega$ ) may require adjustment with some transistor pairs ( $Tr_3, Tr_4$ ). A value should be chosen which sets the collector voltage of  $Tr_4$  at between 5 and 7V negative w.r.t. earth.
- (d) A modification of the discriminator circuit values will enable the tuner to feed about 1V a.f. into loads of 1M $\Omega$  or greater. This is done by adopting the following component values:—
  - $R_{21}$  39k $\Omega$ ,  $\frac{1}{2}$ W,  $\pm 10\%$  carbon.
  - $R_{22}$  150k $\Omega$ ,  $\frac{1}{2}$ W,  $\pm 5\%$  carbon.
  - $C_{23}$  270pF,  $\pm 1\%$  silvered mica.
  - $C_{24}$  330pF,  $\pm 1\%$  silvered mica.
 The modification is useful for feeding some valve power amplifiers without the need for an intermediate pre amplifier.



action being sufficiently good up to 350 kc/s to achieve excellent discriminator action.

The discriminator itself is a transistor pump<sup>2</sup>. This is a modified version of the familiar diode pump which gives improved linearity at the higher output levels. The audio output is finally taken *via*  $R_{22}$  and  $C_{24}$  which provide the required de-emphasis characteristic. An audio output of about 100 mV (r.m.s.) for a deviation of  $\pm 75$  kc/s, can be delivered into loads of 100 k $\Omega$  or greater. Where this is done with a coaxial cable, care should be taken to see that the length does not exceed about 10ft.

### Construction

This is not unduly critical but the whole must of course be enclosed in a screened aluminium box and the r.f., mixer and i.f. sections screened from each other.

The discriminator and i.f. stages are assembled on an insulating board using conventional wiring techniques. (A printed wiring board would probably also be suitable). The r.f. and mixer stages are most conveniently assembled on paxolin insulated tag strips screwed to the aluminium housing, the most suitable place for the low-pass filter seems to be within the mixer compartment, the normal screening can of the i.f. transformer being removed and the coil former mounted directly on the chassis.

### Setting up

**Aerial.**—The tuner should preferably be fed from a dipole aerial proportioned for Band II operation. This should yield an adequate signal for correct operation for

field strengths down to 250  $\mu$ V/m, if care is taken with the aerial installation. In areas of very low field strength a multi-element array will be necessary.

**Oscillator.**—The main adjustment required is that of setting the local oscillator frequency. This is most conveniently done by feeding in 90 Mc/s signals from a signal generator (say about 500  $\mu$ V r.m.s.) into the aerial terminals and adjusting the self supporting coil  $L_4$  until the whole range can be tuned with the trimmers  $C_{13}$ ,  $C_{14}$ ,  $C_{15}$ .  $L_1$  should also be adjusted to peak at about mid-band, i.e. 94 Mc/s. Final oscillator frequency adjustment can easily be done on a signal, if a high-resistance voltmeter is arranged to read the mean d.c. signal appearing at the a.f. output socket. The appropriate trimmer is first adjusted to give a low intermediate frequency—as indicated by a “null” reading on the voltmeter—and then the oscillator frequency is moved to one side of this setting, to produce a voltmeter reading of 0.4 V. This will give a mean i.f. of about 180 kc/s.

### Acknowledgement

I wish to thank Professor S. H. Ayliffe for permission to publish this article and for the use of the facilities of his department.

### REFERENCES

1. “Transistor FM Tuner” : P. J. Baxandall (Correspondence) *Wireless World*, September 1964, p. 460.
2. “Elements of Transistor Pulse Circuits” : T. D. Towers, *Wireless World*, August 1964, p. 403.

## Books Received

**Topology and Matrices in the Solution of Networks**, by F. E. Rogers. An initial detailed explanation of the rudiments of topology is used as a basis for introduction to the matrix concept. The combined principles are extended progressively to the solution of network equations and then applied to fundamental theorems and four-terminal networks. Worked examples, given at the end of each chapter, link theory with practical application. Pp. 204; Figs. 100. Price 45s. Iliffe Books Ltd., Dorset House, Stamford Street, London, S.E.1.

**Dynamic Circuit Theory**, by H. K. Messerle. Written as an introductory course on electromechanical energy conversion and electromechanical systems, the book uses dynamic circuit theory as a basis for the formulation of the principles of electrodynamics. Particular attention is given to the derivation and analysis of lumped parameters and their use for representation of electromechanical devices. Double storage transducers, commutator machines, two- and three-phase machines, and multiphase systems are dealt with in detail. Worked examples are included. Pp. 657; nearly 330 Figs. Price £5. Pergamon Press Ltd., 4 & 5 Fitzroy Square, London, W.1.

**The Invention of the Traveling-wave Tube**, by Rudolf Kompfner. An interesting, lucid account of the research by the author which led to the invention of the travelling-wave tube. Parts of the text which recount particularly difficult stages of the work are tempered with humour and will act as a stimulant to others engaged in the arduous field of research. Pp. 30; Figs. 18. Price 10s 8d. W. Heffer & Sons Ltd., 3-4 Petty Curry, Cambridge.

**Handbook of Electron Tube and Vacuum Techniques**, by F. Rosebury. A new version of the Tube Laboratory Manual produced by the Research Laboratory of Electronics at the Massachusetts Institute of Technology. The introductory sections deal with procedures and techniques in the manufacture of thermionic valves and other evacuated devices.

The rest of the book contains a glossary of terms comprising a detailed and comprehensive compilation of definitions, materials, processes, etc., presented in graphical and tabulated form together with explanatory diagrams. Pp. 597; Figs. 154. Price £6 12s. Addison-Wesley Publishing Company, Inc., 10-15 Chitty Street, London, W.1.

**The Electron in Electronics—Modern Scientific Concepts for Electronic Engineers**, by M. G. Scroggie. Couched in the inimitable style for which the author is so well known, the book fulfils the need of students and engineers requiring a lucid explanation of the physics of the electron in modern electronics. Energy levels, work functions and valency bonds are dealt with in the introductory chapters which lead to the quantum theory and photons. The controversy of electromagnetic radiation—wave theory versus photon theory—is discussed in detail and includes the effects of polarization, diffraction and interference. Continued expansion of the text then covers semiconductors and aspects of atomic theory such as magnetogyric ratio, electron spin, nuclear spin and magnetic resonance. The final chapter is devoted to relativity. Throughout the text, the standard of mathematics and general physics does not exceed G.C.E. “A” level. Pp. 276; Figs. 132. Price 45s. Iliffe Books Ltd., Dorset House, Stamford Street, London, S.E.1.

**Principles of Transistor Circuits (Third Edition)**, by S. W. Amos. First published in 1959, the contents have been expanded in successive editions to deal with later developments of the transistor. In this edition the general arrangement of the subject matter of the book remains the same—the physics of semi-conductors, design of transistors, receivers, oscillators and generators. Additions to the text include d.c. stabilization of amplifiers by direct coupled feedback, phase shift and Wien-bridge oscillators, blocking oscillators and transistor sawtooth generators. Two appendices give details of the manufacture of transistors and an explanation of transistor parameters. Pp. 293; Figs. 172. Price 35s (stiff cover), 25s (limp cover). Iliffe Books Ltd.



## A Way of Speeding Up the Application of New Techniques to Medical Practice

# Medical Instrumentation

By VLADIMIR K. ZWORYKIN<sup>\*</sup>, Ph.D., D.Sc.

**As an introduction to the two forthcoming conferences on medical electronics, in Tokyo (29th August) and Brighton (28th September), Dr. V. K. Zworykin, who is an international leader in this field, gives his views on a problem which concerns him greatly—the excessive delay that occurs between the introduction of new instrumentation techniques and their application to medical practice. Recently Dr. Zworykin, who is 76, was awarded the I.E.E.'s Faraday Medal for his notable scientific and industrial achievements, including the invention of the iconoscope, and his work in medical electronics.**

**F**OR many years I have advocated the establishment of a chain of specialized institutions devoted to the advancement of medical instrumentation throughout the world, linked by our International Institute for Medical Electronics and Biological Engineering in Paris. While institutions of this nature have existed for a long time in several of the Eastern countries, in particular the U.S.S.R. and Czechoslovakia, I have found it relatively difficult, until recently, to develop the enthusiasm needed for their launching in the West and in the United States in particular. However, there are many signs that the climate is becoming more favourable for such ventures. Many influential voices have been added to my own, urging the creation of Institutes of Medical Electronics and Biological Engineering in various localities. This makes it desirable that we should examine what the structure and the functions of such an Institute might properly be. While my suggestions are necessarily tinged by my experience in the United States, the basic problems and conditions are sufficiently similar in other countries to make such an examination of general interest.

Our past experience with various national interdisciplinary professional societies, as well as with the International Federation of Medical Electronics and Biological Engineering, has emphasized the benefits to be derived from closer contact between the medical and engineering professions. The co-operation promoted by these groups has already proved exceedingly fruitful. At the same time it has thrown into clear relief a gap in the application of engineering knowledge to medical problems.

This gap exists primarily in the development of new devices for large-scale use in clinical practice. It may

be attributed to the long period of testing and evaluation which, in medicine, must intervene between the construction of an engineering model and the large-scale distribution of the final device. The resulting expense and delay in marketing, which finds no counterpart in other branches of industry, discourages private enterprise from ventures in the development of medical instrumentation. A primary objective of the Institute should be, I submit, to remove this impediment. In this manner the flow of promising ideas in the field of medical electronics and biological engineering, greatly augmented in the past years through interdisciplinary co-operation, would be directed most effectively to the advancement of medical practice and, with it, to the improvement of general health and well-being. The orientation of the Institute would thus be primarily practical, since the practical application of engineering methods in medicine has, so far, tended to lag far behind their application in scientific research in the life sciences.

It should be recognized that, in principle, any new group could undertake the launching of an Institute of the type here considered. However, it is vital for its success that it should benefit from close association, from the very beginning, with organizations in the field of medical electronics and biological engineering which have been built up in the past decade. This imposes, in my opinion, a special responsibility for this undertaking on those of us who have been intimately associated with the development of the above organizations.

With this preface, what might the structure and functions of the Institute be?

Let us first consider the structure of the Institute, which would be a non-profit organization. The control of the Institute would rest in the hands of a board of directors, consisting of persons deeply convinced of the importance of the mission of the Institute and ready to maintain a financially sound basis for its operations. It would be supported by a group of eminent technical advisers drawn from the engineering and medical professions. The board would appoint a Director of the Institute who, with his secretarial assistants, would constitute the initial permanent staff of the Institute. The Director, in addition to his other duties, would be charged with establishing rosters of specialists in the medical and engineering fields who could be drawn upon to carry through technical projects in their area of competence which have been undertaken by the Institute. These specialists might be persons retired from industrial and other organizations with a prescribed retirement age who are eager to contribute their skills to the humanitarian purposes served by the Institute. While placement on the roster would not imply remuneration of any kind, travelling and *per diem* expenses incurred in the service of the Institute would be reimbursed. The establishment of the rosters may be regarded as a device for circumventing the large initial expenditure inherent in setting up a well-rounded paid professional staff and, at

<sup>\*</sup>Vice-President and Technical Consultant, Radio Corporation of America.



the same time, utilizing an important available source of talent.

The activities of the Institute might include:—

1. Keeping informed concerning problems and ideas encountered in international medical practice and research and submitting them to members of the roster for evaluation with respect to importance and feasibility of further development.

2. Arranging for follow-up activity if the evaluation recommends further work; this could be carried on within the Institute or with the aid of outside organizations, always with the collaboration of the originator of the problem and of members of the evaluating panel.

3. Carrying on such evaluation and follow-up activities for other organizations under contract.

4. Application for grants for the construction of working models and further development by an appropriate organization if this appears justified.

5. Organization of working groups from the Institute roster to supervise work carried forward under such grants and to arrange for the publication of the results in the technical journals.

6. Making arrangements for patent protection and negotiating licensing agreements under patent rights acquired by the Institute, if, under the conditions prevailing in the country, this were consistent with obtaining support from other sources.

7. Seeking financial support for the Institute from industry, foundations, and other sources, making use of professional assistance as needed.

We can envisage the function and growth of the Institute taking the following course. To begin with, the staff would make known, through appropriate professional channels, that it was available for consultation on medical engineering problems encountering obstacles of a technical, financial or some other nature. The consultation might result in a referral to a commercial or scientific organization with interests in the same field or experience in solving problems of a similar nature, or it might point out published work with a bearing on the subject. Just by serving as a focus at which medical and engineering scientists would be together, the Institute would frequently provide the starting point for collaborative investigations. If a specific project required financing, the staff might put the applicant in touch with possible sources of support after a favourable evaluation of the project by members of the advisory panel.

The Institute would not concern itself with basic research investigations which are already well supported by other agencies, but would deal primarily with the design and application of medical instrumentation. In due time, as engineering designs perfected and tested with the assistance of the Institute became widely accepted in hospitals, the demand for them would increase to a level sufficient to yield a financial return to the electronic and mechanical industries which had made the original collaborative effort. As the Institute became more widely known and a greater range of problems was presented to it, the need for laboratory facilities would become evident. Thus, in response to demand, it might gradually develop into a larger-scale research institute of medical electronics and biological engineering. The necessary "*in vivo*" experiments, which initially would be carried out in co-operating hospitals and other institutions, might then be transferred to its own facilities. Thus the Institute might grow, from relatively modest beginnings, into an establishment fully equivalent to the extensive institutes for medical instrumentation set up in Russia and other countries of Eastern Europe.

I estimate that an Institute of the type here contem-

plated might be launched, under the conditions prevailing in the United States, with an initial annual budget of \$100,000 or less. This would just suffice to pay the Director and his assistants and provide the minimal office space and equipment required. Its growth would be determined by its recognized usefulness to industry and the medical and engineering professions. The favourable response I have received so far assures me that the growth of the Institute would be rapid and that it would come to provide an important service to the patient, the physician, and the research scientist alike.

We should lose no time in calling such Institutes into being. They would do much to close the gap between theoretical understanding and practical utilization in the application of engineering knowledge to medicine.

## Chartered Engineers

THE granting of a Royal Charter to the Council of Engineering Institutions, formerly known as the Engineering Institutions Joint Council, has brought a step nearer the day when the titled "chartered engineer" (C.Eng.), without reference to a particular discipline, will be used by members of the 13 constituent institutions.\* To this end it is proposed to introduce a common Part I examination which will benefit "cross-fertilization" between the different disciplines. It will not be easy to reconcile the varying requirements of the different institutions, each representing a specialized branch of science and technology.

In the Rules of the C.E.I. it is specified that there shall be "an examination in the principles of engineering which shall be set by the Council . . . and shall be of a standard at least equivalent to that of a degree in engineering currently awarded by a university. The Council will accept certain qualifications as exemption from this examination.

The Institution of Electronic & Radio Engineers has issued a policy statement regarding the proposed common examination. "It has been clear," it says, "from the outset that this will preclude the degree of specialization which characterizes engineering studies today, particularly in the universities, where departments, chairs, and new courses in electronics have slowly but steadily appeared since the war."

It is pointed out that through the proposed regulations governing the examination the C.E.I. "will exert a powerful influence on the structure and content of courses of study in colleges of technology and even the universities. Proposals which are in sharp contrast with accepted practice in engineering education deserve for that very reason, more thorough and prolonged discussion."

The I.E.R.E. warns against the possibility of the Council foundering "on the uncharted rocks of educational policy, many of which are not yet discernible," and adds "A liberal conception of the specialist requirements of the individual engineering professions is most necessary if we are to avoid the mistakes of the past in restricting development of new technologies."

The proposed Pt. I syllabus comprises papers in the following subjects:—mathematics, properties of materials, principles of electrical engineering, applied mathematics, fluid mechanics and thermodynamics.

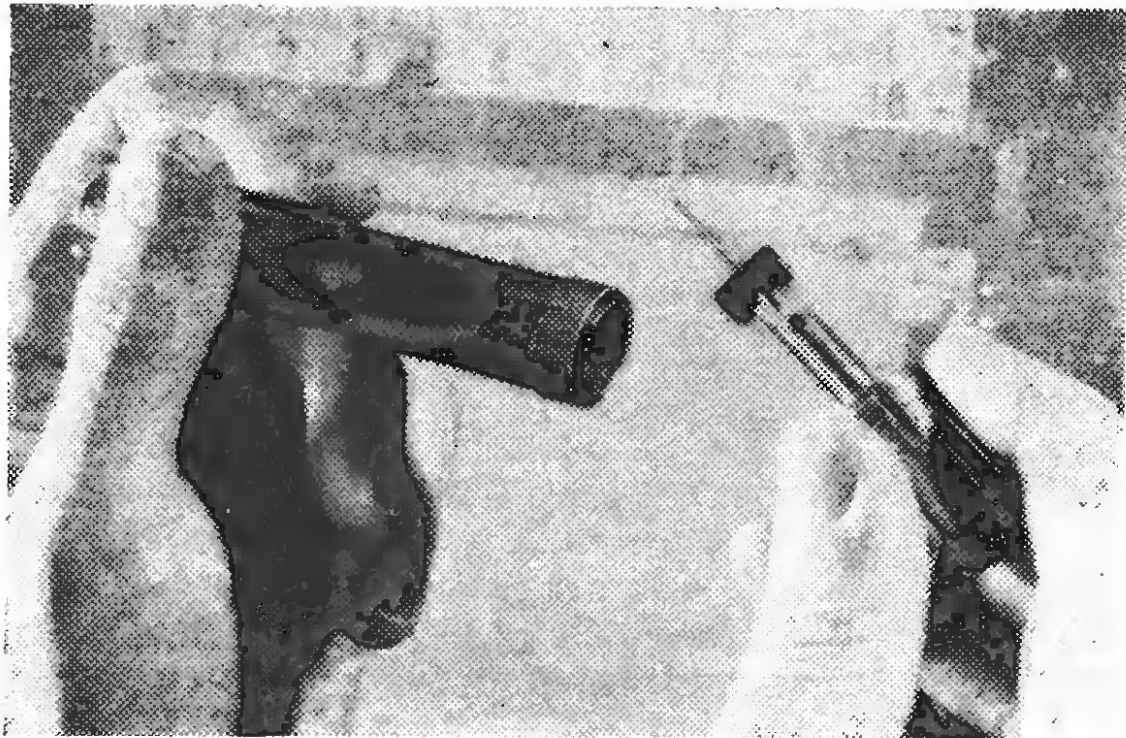
While giving support to the principle of a common examination the I.E.R.E. feels that it cannot agree that this demands a Part I exam with no optional papers. It therefore proposes an examination based on a core of four compulsory papers of a broader basic coverage (such as mathematics, engineering science, principles of both mechanical and electrical engineering) plus at least one optional paper to cater for the requirements of individual institutions.

\*Royal Aeronautical Society; Institution of Chemical Engineers; Institution of Civil Engineers; Institution of Electrical Engineers; Institution of Electronic and Radio Engineers; Institution of Gas Engineers; Institute of Marine Engineers; Institution of Mechanical Engineers; Institution of Mining Engineers; Institution of Mining and Metallurgy; Institution of Municipal Engineers; Institution of Production Engineers; and Institution of Structural Engineers.



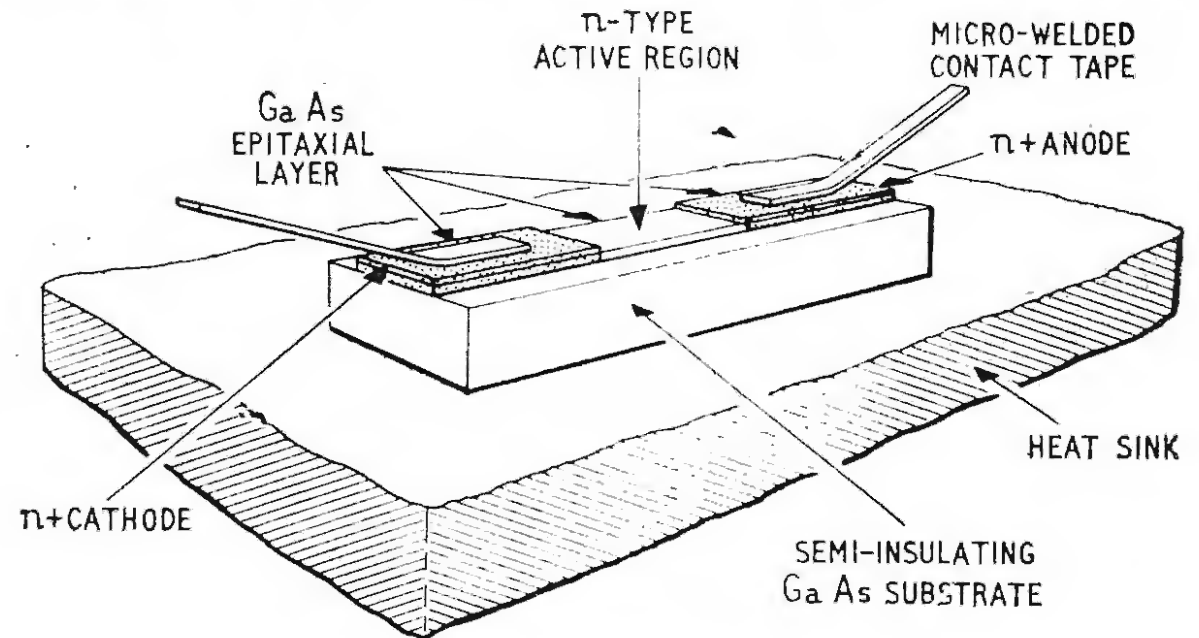
# EPITAXIAL GUNN-EFFECT DEVICE

AN epitaxial version of the Gunn-effect device has been developed as an experimental microwave oscillator by Standard Telecommunication Laboratories (see "The Gunn-Effect," *Wireless World*, August 1965, p. 416). It has a volume of 0.1 in<sup>3</sup> and is said to produce several milliwatts of power at 1 Gc/s. S.T.L. explain that the epitaxial construction enables the frequency and the threshold power



of the device to be determined independently of the resistivity of the active region or the mechanical and thermal properties.

On a substrate of semi-insulating gallium arsenide about 100  $\mu$ m thick is grown a 15  $\mu$ m layer of gallium arsenide whose properties are optimum for the active region of the device. The effective cross-sectional area for the current path is determined by removing part of this layer to form a narrow track 100  $\mu$ m wide. The anode and cathode are formed by converting two parts of the track to n+ regions,



leaving a gap of the original n-type material between them, the length of which determines the self-oscillating frequency. The semi-insulating substrate is bonded to a heat sink and electrical connections to the anode and cathode are made by micro-welding tapes to metal contacts on the top surface of the n+ regions.

The shape of the substrate controls the mechanical and thermal properties of the device. The electrical properties, determined by the dimensions of the epitaxial n-type track, can be varied independently of the shape of the substrate. It is stated that the configuration is suitable for mass production, using precision masking techniques similar to those employed in the manufacture of semiconductor integrated circuits.

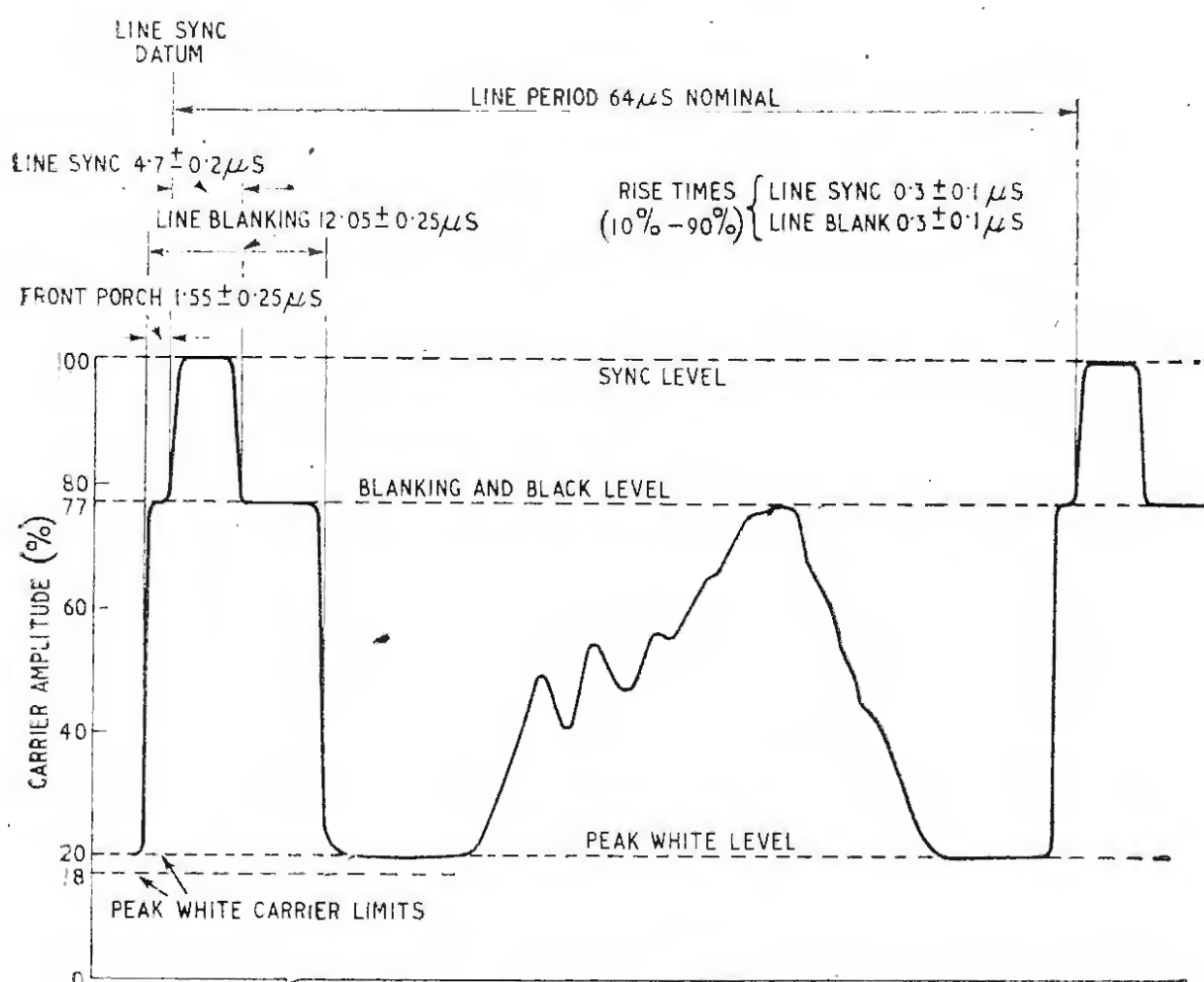
S.T.L. are also looking into the idea of three-terminal Gunn-effect devices in which domain formation can be influenced by the potential of an isolated gate electrode similar to that in a metal oxide semiconductor transistor—the cathode and anode being in the positions of the source and drain of the M.O.S.T. respectively.

## 625-LINE TELEVISION WAVEFORM

LATEST change to the B.B.C.'s 625-line vision signal waveform is the addition of a test signal for use in automatic test equipment at unattended transmitting stations. This signal is inserted on lines 17 and 330, and consists of a 12.5  $\mu$ s bar, a sine-squared pulse (half-amplitude duration 0.2  $\mu$ s) and a five-step staircase. The first four steps of the

staircase have a duration of 5.3  $\mu$ s and the final step a duration of approximately 4.0  $\mu$ s, all steps being of equal height.

The B.B.C. has also published tolerances on the figures in the 625-line vision and sound signal specification, and for the benefit of readers who may not possess up-to-date information we give here the current specification together with the idealized carrier amplitude waveform.



Channel bandwidth	.. .. .	8 Mc/s
Spacing between unmodulated sound and vision carriers	.. .. .	6 Mc/s $\pm$ 1,000 c/s
Vision modulation	.. .. .	a.m. negative
Upper sideband	.. .. .	5.5 Mc/s
Lower sideband	.. .. .	1.25 Mc/s
Synchronizing level	.. .. .	100%
Blanking level	.. .. .	76% $\pm$ 1%
Difference between black level and blanking level	.. .. .	0%
Peak white level	.. .. .	19% $\pm$ 1%
Sound modulation	.. .. .	f.m.
Peak deviation	.. .. .	50 kc/s
Pre-emphasis	.. .. .	50 $\mu$ s
Ratio of peak vision carrier power to sound power	.. .. .	5 : 1
Lines per picture	.. .. .	625
Interlace	.. .. .	2 : 1
Field frequency	.. .. .	50 c/s
Line frequency	.. .. .	15,625 $\pm$ 0.15 c/s
Approximate gamma of picture signal	.. .. .	0.5
Nominal video bandwidth	.. .. .	5.5 Mc/s
Aspect ratio	.. .. .	4 : 3

Transmissions are normally asynchronous, i.e. the sync signals are derived from a stable oscillator and are not locked to the mains.



# Electronics for "Mediator"

Comprehensive air traffic control scheme designed to cope with the rapidly increasing density and speed of air traffic over the United Kingdom

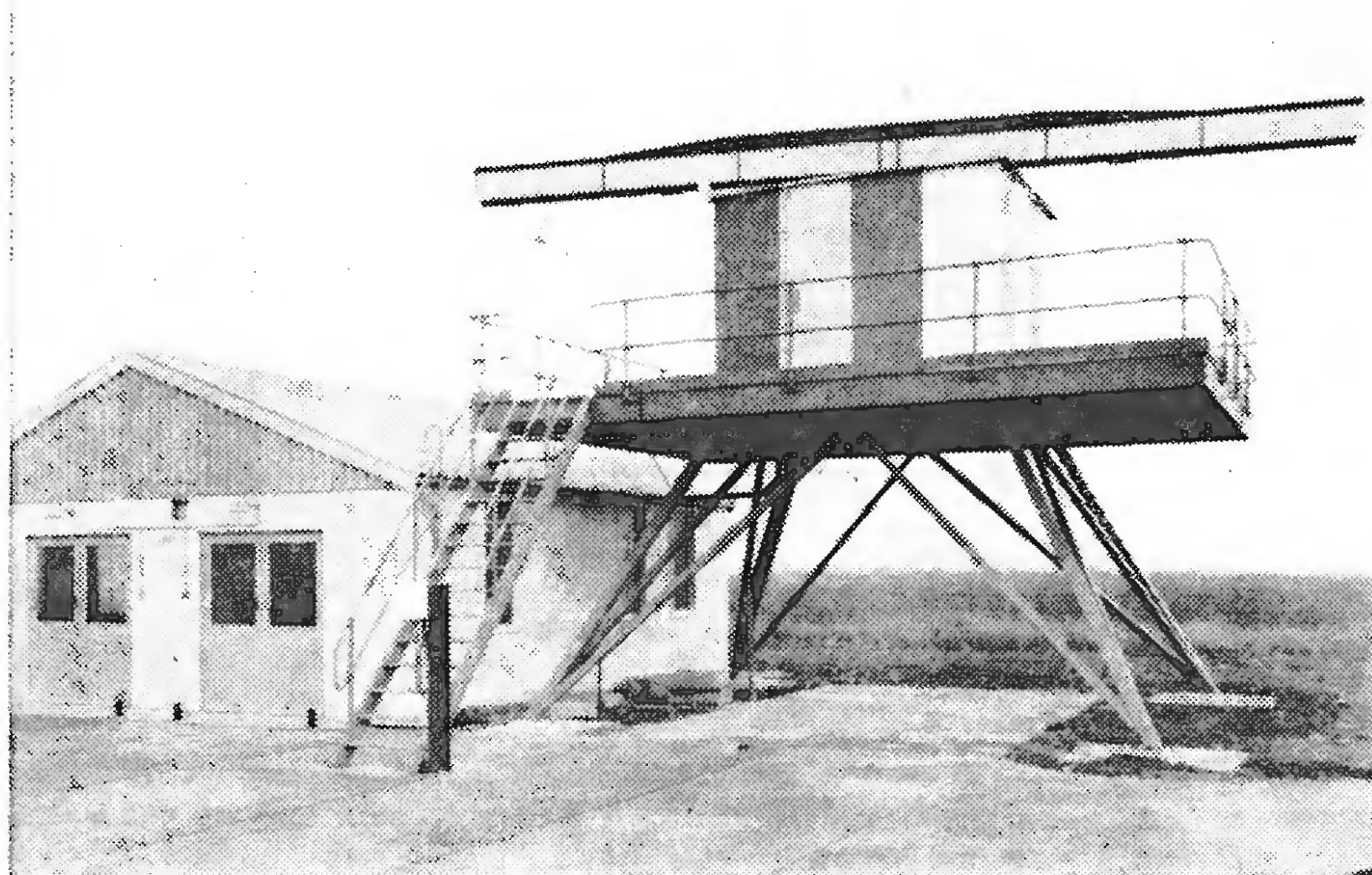
**E**XTENDED radar coverage and automatic data processing are the two electronic cornerstones of a comprehensive air traffic control scheme now gradually being introduced in the U.K. under the code name "Mediator". The radar surveillance will eventually cover the whole of the U.K. Flight Information Region below 57°N, from a height of 5,000 ft upwards. It is being provided initially by primary radar stations, but these will gradually be supplemented by co-located secondary radars which will assist in identifying aircraft and provide accurate information on their heights. The automatic data processing equipment, based on electronic digital computers, will not only reduce the controllers' normal work-load by maintaining an up-to-date store of information on the intention and progress of all aircraft, performing automatically all the necessary analysis and correlation of different information sources, but will also make possible the rapid prediction of conflicting flight paths.

## Government N.A.T.C.S.

The new scheme is being put into operation by the National Air Traffic Control Services. This is a Government body which was formed in 1962 for the express purpose of setting up a comprehensive a.t.c. system and which is responsible to both the Ministry of Aviation (for civil aircraft control) and the Ministry of Defence (for military aircraft control). "Mediator" is comprehensive because it will serve all users of British airspace—airlines, charter companies, military aviation, research and development flying, private business users

and so on, right down to gliding clubs. The impetus for the scheme has come from the rapidly increasing density and speed of air traffic. From 1957 to 1964, for example, civil air transport movements in the U.K. airspace increased by nearly 50%, while the top speed of civil aircraft rose during this period from about 300 knots to about 600 knots. This has demanded a corresponding increase in the information handling capacity of the air traffic control loop (information gathering—decision making—transmission of instructions), an increase which could not be provided by the existing facilities nor by a straightforward multiplication of the existing equipment and personnel.

Hitherto air traffic control has been based on the so-called "procedural" method (in which pilots report their positions to controllers by R/T), while radar has served mainly in a monitoring or backing-up role. With the increasing density and speed of air traffic, the information gathering part of procedural control is now beginning to show limitations (e.g., errors can occur in reading aircraft instruments and in air/ground voice communication). These limitations restrict the volume of air traffic that can be handled because the standards of separation between aircraft have to be sufficiently large to allow for the errors in time and space that can occur. This is a particularly serious problem in and around the London Terminal Area. Radar, however, which requires no co-operation from the pilot, is inherently faster and more accurate as a means of position finding, and is consequently beginning to assume a more important role in control operations—especially now that secondary radar is being adopted more widely. Be-



*Cossor SSR.5G secondary surveillance radar installation at London Airport. Interrogator/responders and servo equipment are housed in the building.*



cause of this, aircraft separation standards for radar control are smaller than for procedural control. These, then, are the basic reasons why the existing a.t.c. radar coverage is being extended in the new scheme.

There are similar reasons for the introduction of

automatic data processing in place of conventional a.t.c. methods of handling information. Here the main problem is to process the increasing volume of information at sufficiently high speed to allow effective control. Each controller can cope with only a limited number of air-

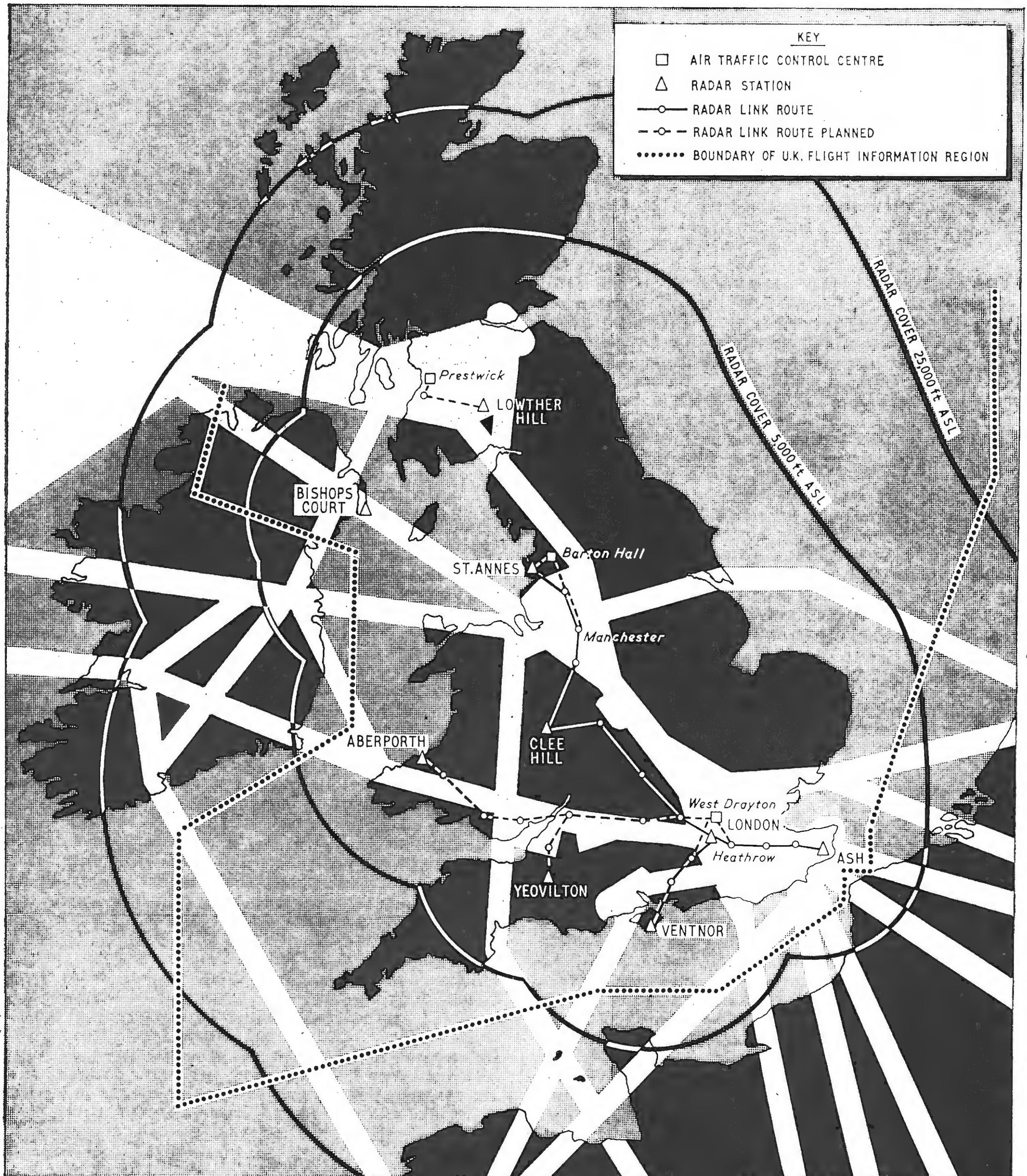


Fig. 1. Radar network to be completed by 1969, showing main airways and other controlled airspace, new air traffic control centres, and radar coverage at 5,000 ft and 25,000 ft. The boundary of the U.K. Flight Information Region is indicated.



craft. Under the present method of working an increase in air traffic calls for an increase in the number of controllers—but this means that more time must be spent in communicating between controllers. Furthermore, the increase in traffic density results in control problems of greater complexity, which take correspondingly longer to solve by human mental processes. The use of automatic data processing equipment will enable these delays to be reduced considerably, so that they no longer present a serious time lag in the control of high speed aircraft; it will also facilitate predictive operations such as calculating times of arrivals and possible conflicts between flight paths.

In the new scheme the airspace of the U.K. Flight Information Region, Fig. 1, will be divided up horizontally by the existing airways (which are defined by radio navigational aids and mainly used by airlines) and vertically into the following sections: upper airspace (above 25,000 ft), middle airspace (above 5,000 ft and below 25,000 ft), controlled airspace (the airways part of the middle airspace in which positive control is exercised) and lower airspace (below 5,000 ft). The degree of control exercised will vary throughout this total airspace in a complex pattern determined by the forecasted increase of aircraft movements in the horizontal and vertical divisions, and will range from a minimum of control in the upper airspace in the north of Scotland to maximum control in the controlled airspace above the London Flight Information Region. Two types of information will be required from all aircraft moving through this total airspace. The first is flight plan data—a statement of intention which must be filed by every aircraft entering the system and which is subsequently fed into the data processing equipment by keyboards. The second is flight progress data—mainly the output of the primary and secondary radars, giving aircraft identification, position and height—which is fed directly into the data processing system (in the later stages of the project without human intervention).

### Progressive introduction of the scheme

How far has the new scheme progressed? The radar network is the most advanced part. New primary radars at London and Manchester serve the controlled airspace, and the cover they now provide will be greatly extended by the progressive introduction into service of new radars at Ash (Kent), St. Annes (Lancs), Clee Hill (Shropshire), Ventnor (I.o.W.) and Lowther Hill (Lanarks) and by the addition of existing radars at Yeovilton (Somerset) and Aberporth (Cardigan). Ash and St. Annes should be operational this September, Clee Hill and Ventnor before the end of this year and Lowther Hill in 1967, and Yeovilton and Aberporth will be added to the system in 1968. All radar stations have been, or are being, linked to the air traffic control centres they serve by wide-band microwave links. Secondary surveillance radar (s.s.r.) is being progressively added to all the radar stations—the installation at London is complete and others are in progress at Ash and Ventnor.

All primary radars mentioned are Marconi S264A equipments, with the exception of Aberporth (Marconi S300) and Clee Hill (Plessey DASR-1). London, Ash and Ventnor s.s.r.s. are Cossor SSR5G equipments. Radio link equipment connecting St. Annes, Ash, Ventnor and Clee Hill to their air traffic control centres is of Marconi manufacture.

For the upper airspace, new equipment is being installed at joint civil/military a.t.c. radar units at Bishops

Court (N. Ireland), Sopley (Hants), Boulmer (Northumberland) and Hack Green (Cheshire), while two new military radar units at Lindholme (Yorks) and Watton (Norfolk) will be fully operational by July 1966. The middle airspace will be served by the units at Lindholme and Watton, and also by a new unit at North Luffenham (Rutland), which will provide general radar surveillance in the Vale of York, East Anglia and the Midlands. Information from the London, Ash and Ventnor radars will also be used to give an improved radar control service to aircraft flying in the London Flight Information Region, crossing the airways and in the London Terminal Area.

### Data processing and display

As for the information processing and display operations, these will be divided between three air traffic control centres: a Scottish centre at Prestwick airport, a Northern centre at Barton Hall (Preston) and a Southern centre at West Drayton, near London (Heathrow) Airport. The Scottish centre, controlling all airspace north of 57° N and the middle airspace north of the Clyde-Forth valley, will use raw radar information and no automatic data processing. The Northern joint centre, dealing with the middle and controlled airspace in the north-west area, will not have automatic data processing equipment installed but will be able to make use of information processed at West Drayton. The Southern centre, which will be responsible for all the rest of the controlled and middle airspace and for all the upper airspace south of 57° N, will be the largest of all three centres and will house the automatic data processing equipment for the whole scheme. The building at West Drayton has been completed, the procedural control element of the existing S.A.T.C.C. at Heathrow is being transferred into it and the first stage of electronic information handling is expected to be working in 1966.

Fig. 2 shows in broad outline the equipment to be installed at the West Drayton S.A.T.C.C. Positional information from remote primary and secondary radar stations is received via 7-Gc/s broad-band radio links and from the local radars at London (Heathrow) Airport via G.P.O. coaxial cables. Signals available at the radio link terminal are primary and secondary video, trigger pulses and aerial turning information. These signals are distributed to various destinations—to raw radar displays on controllers' consoles in the operations room, to extraction equipment and to secondary radar decoding equipment. In the extraction equipment the analogue positional information is converted into digital form, and is then fed into the radar data processing equipment where it is converted into Cartesian coordinates and stored.

The function of the radar data processing equipment is to maintain track records of all aircraft (these being continuously up-dated by fresh positional information), to detect possible track conflicts (by prediction of future radar responses) and to read out this track information for marking of raw radar and synthetic radar displays. The secondary radar decoding equipment provides aircraft identity and position information for the extraction equipment and also gives identity and height read-outs at controllers' consoles and s.s.r. marking of raw radar displays.

In procedural control the principal document for recording aircraft information—identification, destination, estimated time of arrival, etc.—is the flight progress strip. Information needed by controllers is taken





# SWITCHED THYRISTOR VOLTAGE REGULATOR

By F. BUTLER, O.B.E., B.Sc., M.I.E.E., M.I.E.R.E.

THE most efficient way of producing a constant load-voltage from an unregulated d.c. source is to use a switched thyristor as a control element between source and load. When it is conducting, the voltage drop across it is between 1 and 1.5 V, and with a load current up to 10 A the loss will not exceed 15 W. When blocked (non-conducting), the energy loss in the thyristor is zero.

Two switching modes are possible. In one, the average switching rate is held constant but the proportion of the total time during which the switch remains closed is variable. The method is commonly described as time-ratio control and it may be exercised manually or automatically. A second method of control is to switch on the thyristor and then turn it off after a fixed period of time. In this case regulation is effected by varying the repetition frequency of the fixed-duration pulses. The second method is rather simpler to engineer and its only disadvantage is that on light load the pulse recurrence frequency may fall so low that filtering becomes difficult. In practice this effect is only troublesome in variable-voltage supplies which are required to operate at maximum load current with a very low output voltage setting.

## Thyristor turn-off methods

A controlled rectifier can be turned on by a low-level short-duration positive pulse into the gate electrode. The problem is to turn it off. Six or seven methods of doing this have been proposed, most of them having some objectionable features, notably cost or complexity. All involve the same basic principle, which is to charge up a capacitor to a high voltage and then to discharge it through the thyristor in a direction opposite to that of the normal load current. The controlled rectifier will block if the load current is reduced to zero for about 60 microseconds or if a reverse voltage can be maintained across it for at least 20 microseconds.

One of the simplest and most reliable turn-off circuits was suggested by R. E. Morgan of the (American) G.E. Company. It is shown in Fig. 1. In the steady state,

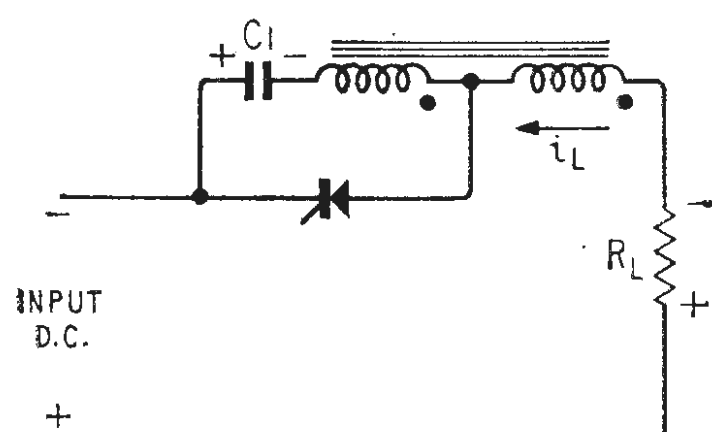


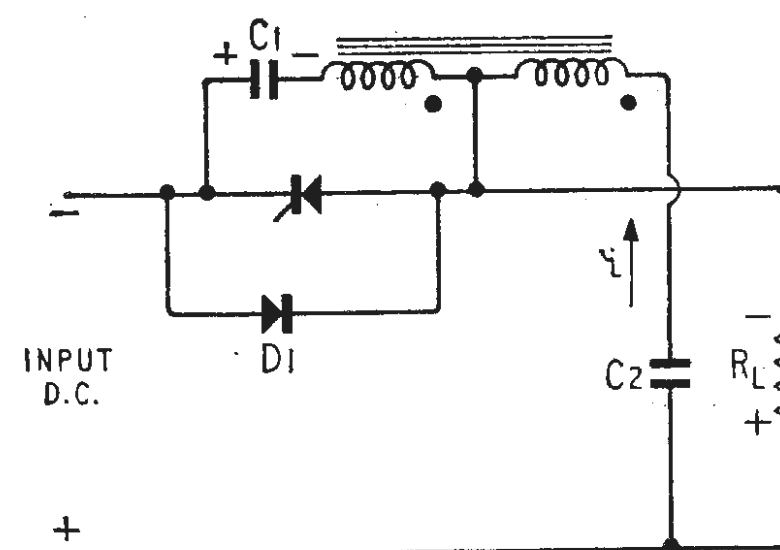
Fig. 1. Thyristor turn-off circuit due to R. E. Morgan.

before the thyristor is turned on, the capacitor  $C_1$  becomes charged up to the input direct voltage, with a polarity opposite to that shown on the diagram. There is no flux in the auto-transformer core, no voltage across either of its windings and the load voltage is zero. On firing the controlled rectifier, a current shown as  $i_L$ , passes through one winding of the transformer and

through the load. The induced voltage in the other winding charges up the capacitor with the polarity shown, which is opposite in sense to the initial charge. At first the charging current into the capacitor is such as to produce an ampere-turn balance with the current in the primary or load section of the winding. The core remains unsaturated. When the capacitor becomes fully charged the current into it sinks to zero but load current continues to flow in the primary winding. In consequence the core material (nickel-iron or permalloy), becomes saturated and both winding impedances become very small. In effect the capacitor is then connected directly across the thyristor but with a polarity in the correct sense to turn it off.

The circuit has some good features. For example, an increase of load current will cause more complete magnetic saturation of the core of the transformer and also the capacitor becomes charged to a higher peak voltage.

Fig. 2. Modified version of the Morgan circuit.



Both effects co-operate to give a more positive and abrupt turn-off of the thyristor. The turn-off mechanism is inoperative on no load and a dummy load must be used to cope with this condition. A second, more minor disadvantage is that the turn-off pulse characteristics tend to vary with the load current.

The writer has found that a modified version of Morgan's circuit can be made to give reliable turn-off under a wide range of load conditions, provided only that, as is also necessary with Fig. 1, the input voltage is considerably higher than the required maximum load voltage. It need hardly be remarked that this does not imply a reduced conversion efficiency in either circuit. The new arrangement is shown in Fig. 2. One feature is that the auto-transformer has been taken out of the main load circuit. When the thyristor is turned on by means of a positive gate pulse the forward voltage drop across it sinks to about 1 V and load current flows in  $R_L$ . At the same time a current pulse is passed by  $C_2$ , which is initially uncharged. This current pulse in the primary winding of the transformer induces a high voltage in the other winding, charging up  $C_1$  with the polarity shown. This is in the correct sense to turn off the thyristor as in the Morgan circuit. The diode  $D_1$  is not strictly necessary but it serves two useful purposes. Provided that it is of the fast recovery type (low hole-storage time), it protects the thyristor from exposure to high peak inverse voltages. It also serves to discharge  $C_1$  in the shortest possible time. Clearly the action of this turn-off circuit is independent of the magnitude of the





ments. The construction and mode of operation of the unijunction device have been described by the writer in an earlier paper.\* Briefly, it forms a relaxation oscillator which produces a saw-tooth waveform across a capacitor which is periodically discharged to produce a short duration pulse for firing the thyristor. The repetition rate can be varied by changing the capacitor size or by varying the charging current.

In Fig. 3, the charging current is determined by an output voltage sensing arrangement of two transistors Tr1 and Tr2; the transistors (high gain low power p-n-p types) form a differential amplifier. The base of one of them is supplied with a constant reference voltage from a 5.6 V Zener diode. The base of the other is taken to the slider of a potentiometer connected across the output terminals of the power supply. A rise of output voltage increases the base current of Tr2 and causes a greater voltage drop across the common emitter resistance. This in turn reduces the collector current of Tr1 which constitutes the capacitor charging current. The reduced charging current lowers the recurrence frequency of the firing pulse train and restores the output to its original voltage.

At full load the p.r.f. is about 3 kc/s. Load current pulses of this frequency are easily filtered with moderate values of inductance and shunt capacitance. The remaining component, not so far discussed, is a 100-ohm 10 W resistor, permanently connected across the output terminals. It ensures positive turn-off of the thyristor under external no-load conditions.

### Performance

The percentage voltage regulation depends mainly on the gain of the error-signal amplifier. With high gain transistors Tr1, Tr2 the regulation against load current changes is within 1 or 2 per cent from zero to full load.

\* "Controlled Rectifiers in Stabilized Power Supplies," by F. Butler, *Wireless World*, October 1963, p. 480.

The precise figure depends on the output voltage setting. Against supply voltage changes the performance is even better. An input voltage change of 100 per cent has an almost imperceptible effect on the output voltage. The 20 V Zener diode which regulates the working voltage of the unijunction transistor contributes to this result.

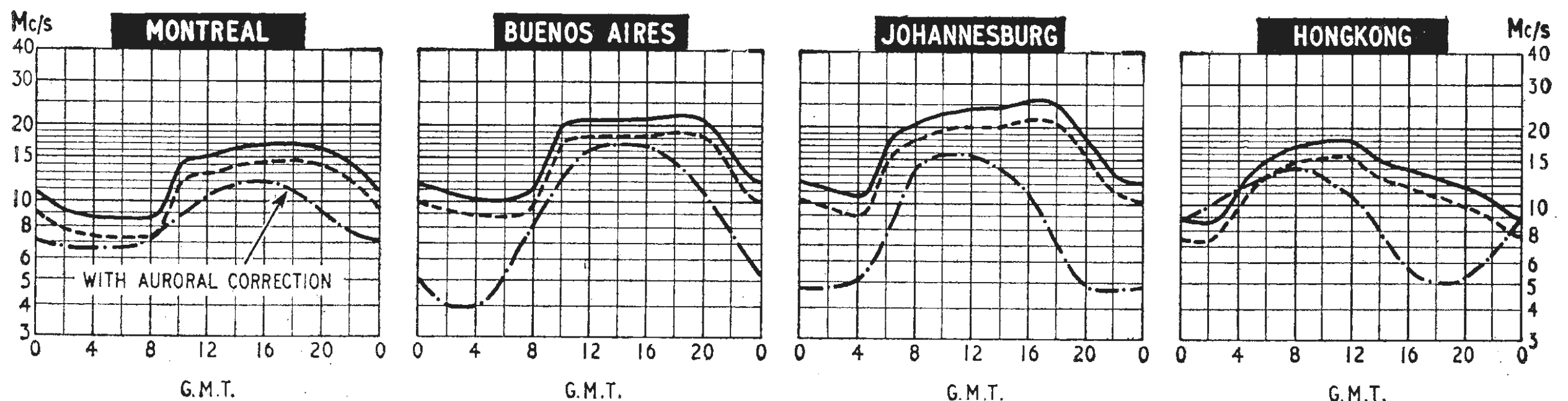
The response time to step changes of load current is set mainly by the time constant of the main filter circuit. It cannot be less than the reciprocal of the low-pass cut-off frequency. In other words, the better the filtering the longer is the response time. Preferably, all the smoothing should be accomplished in a single stage and by using a high firing-pulse frequency this amount of filtering will be found satisfactory and the transient response is good enough for most applications.

Circuit losses are quite small. If p.n.p. silicon transistors are used for Tr1 and Tr2 the equipment will work well over the temperature range -20 to at least 80°C.

A fast-acting fuse in the input circuit will give acceptable protection against overloads though it would fail to safeguard a transistor regulator. Still better protection, almost instantaneous in action, can be given by shunting a transistor or silicon controlled switch across the charging capacitor of the unijunction oscillator and arranging for the voltage drop across a sensing resistor, under overload conditions, to bias the shunt element into conduction, thus inhibiting firing pulses.

The only real disadvantage of power supplies of this type springs from the very perfection of the thyristor as an electronic switch. It can be turned on and off in a matter of microseconds and these switching transients are quite difficult to suppress, reminding one of the difficulties at one time experienced with vibrator power supplies. The effect is most troublesome if the regulator is used to supply radio receivers, low-level digital circuits or high-gain broad band amplifiers. However the most useful applications of thyristor stabilized supplies are in the high voltage, high power field where efficiency and reliability are of much greater consequence than a noise-free output.

## H. F. PREDICTIONS — SEPTEMBER



The MUFs are beginning to show the effect of the slowly rising Ionospheric Index. The predicted Index has risen from 12 in June to 22 for this month. Comparisons with the predictions for previous years show that the MUFs are about 1 Mc/s higher than in 1964 or 1963, and comparable with those of 1962.

The prediction curves show the median standard MUF, optimum traffic frequency and the lowest usable frequency (LUF) for reception in this country. Unlike the standard MUF, the LUF is closely dependent upon such factors as

transmitter power, aerials, and the type of modulation. The LUF curves shown are those drawn by Cable and Wireless Ltd. for commercial telegraphy and assume the use of transmitter power of several kilowatts and rhombic type aerials.



## Subscription Television

THE Postmaster General, the Rt. Hon. Anthony Wedgwood Benn, has announced that the Government intends to continue with the subscription television experiment despite the withdrawal of all but one company from the pilot scheme.

Last year the P.M.G. announced the names of five organizations which were offered licences to enable them to participate in the experiment—the licence to be valid for three years from the date of commencement of service. Subsequently, licences were issued to three, Pay-TV Ltd., Choiceview Ltd. and Telemeter Programmes Ltd. Of these three only Pay-TV intends to continue and the areas in which it is licensed to operate are Sheffield and London (initially the Boroughs of Westminster and Southwark). Programmes are to be the responsibility of the operator and will be fed via relay networks to subscribers who will pay for viewing time by means of coin boxes fitted to their receivers.

The decision regarding the introduction of a permanent service will depend upon the analysis of results based upon economic and social factors involved. For example, one of the many factors to be considered is that of the effect on cinema attendances, and the Board of Trade is being consulted to arrange for protection of the legitimate interests of cinema exhibitors in the areas in which the pilot scheme will operate.

## I.T.U. Plenipotentiary Conference

MORE than 500 delegates from most of the 127 member countries will be participating in the Plenipotentiary Conference of the International Telecommunication Union (I.T.U.) which opens in Montreux, Switzerland, on September 14th.

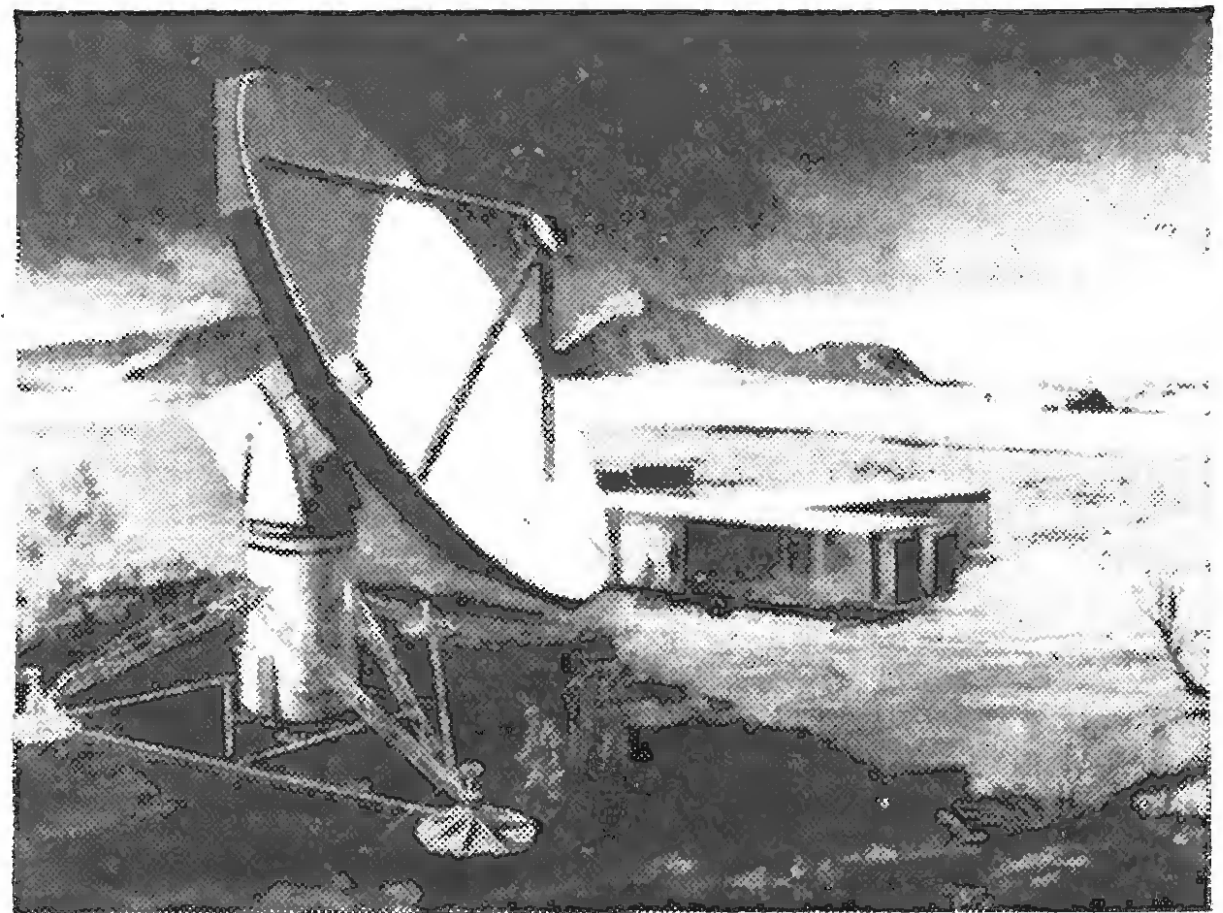
The Plenipotentiary Conference is the I.T.U.'s supreme authority although this year's conference, which takes place in the Union's centenary year, is only the ninth to be held. The founding conference met in Paris in May 1865 and succeeding conferences took place in Vienna in 1868, Rome 1871, St. Petersburg 1875, Madrid 1932, Atlantic City 1947, Buenos Aires 1952 and Geneva 1959.

The main purpose of the Plenipotentiary Conference is to revise the I.T.U. Convention—the Union's basic charter.

The U.K. delegation will be led by W. A. Wolverson, C.B., deputy director of the G.P.O.

**Broadcast Receiving Licences.**—During the first six months of this year the number of combined television and sound receiving licences in the U.K. increased by 203,321 bringing the total to 13,358,003. Sound-only licences fell by 92,959 to 2,766,874; this figure includes 638,642 for sets in cars representing an increase of 22,342. On August 1st, the combined television and sound licence fee was increased from £4 to £5 and the sound-only licence from £1 to £1 5s.

**Confederation of British Industry.**—The Federation of British Industries (F.B.I.), the National Association of British Manufacturers (N.A.B.M.) and the British Employers' Confederation (B.E.C.) have amalgamated to form the C.B.I. which was established by a supplementary Royal Charter effective on July 30th. The charter supersedes the original charter granted to the F.B.I. All communications should now be addressed to the Confederation of British Industry, 21 Tothill Street, London, S.W.1 (Tel.: WHitehall 6711).



**Mobile ground station links** for satellite communications are being designed and built by the communications division of Hughes Aircraft Company to enable existing and future satellites to be linked in a worldwide communications network. Each mobile station consists of three power units, three equipment vans and a 40ft diameter paraboloid as shown in the illustration. Four voice and five teleprinter messages can be received, amplified and transmitted simultaneously via synchronous or medium altitude active satellites.

The first I.E.E./I.E.R.E. joint meetings of the 1965/6 session will be held on September 29th. The Institutions' Computer Groups are holding a one-day conference on airborne computers at the School of Hygiene & Tropical Medicine, Keppel St., London, W.C.1, from 10.30 a.m. In the evening at 6.0 at the I.E.R.E., 9, Bedford Square, W.C.1, the Medical Electronics Group have arranged a meeting at which Dr. P. E. McGuff will present a paper on "Treatment of Experimental Animal and Human Malignant Tumours by Laser Radiation." Tickets obtainable from the I.E.R.E., are required for both meetings.

**European A.T.C.**—A computer-controlled system for the identification and tracking of civil aircraft is to be installed at the Eurocontrol Experimental Centre at Bretigny, France. The prime contractor is Elliott-Automation and the work will be carried out in conjunction with Standard Elektrik Lorenz (W. Germany), Ateliers de Construction Electronique de Charleroi (Belgium) and Cossor Electronics. The new A.T.C. scheme for the U.K. described elsewhere in this issue may well form part of the overall Eurocontrol in the not-too-distant future. By July 1st next year it will be compulsory for aircraft to carry transponders for use with the secondary radar system.

**Radio Interference in America.**—Authority to prohibit the production of electronic or electrical devices which might cause radio interference has been requested by the Federal Communications Commission, but the Electronic Industries Association has asked the Senate Communications Subcommittee to delay legislation until the F.C.C. and representatives from industry can discuss alternative methods of solving radiation-interference problems.

**Frequency Tolerance of Aircraft Transmitters.**—The I.T.U. Radio Regulations (Geneva) 1959 require that, as from January 1st, 1966, the carrier frequencies of all aircraft transmitters operating in the band 118 to 136 Mc/s be maintained to within 50 parts in a million of the selected channel. However, an analysis made by the Ministry of Aviation reveals that the number of transmitters operating outside the stipulated tolerance is insignificant and equipment with a frequency tolerance of 100 parts in a million may remain in use until further notice. Should a particular type or types of equipment consistently fail to meet the I.T.U. requirements, remedial action will be called for.

**Guide to Electronic Equipment.**—The Industrial Control and Electronics Division of B.E.A.M.A. has issued the first edition of a "Guide to the Specification and Purchase of Electronic Equipment for Industrial Systems." In the past, lack of general specifications for industrial electronics equipment has sometimes resulted in the use of specifications which may be inappropriate or unnecessarily costly. The guide will assist both customers and manufacturers by specifying standard types of equipment to meet the requirements for various applications and discusses other factors which need to be considered by both contracting parties. Priced at one guinea, the guide is available from the British Electrical & Allied Manufacturers' Association, 8 Leicester Street, Leicester Square, London, W.C.2.

**Requirements for R.F. Connectors.**—Part 1 of the International Electrotechnical Commission Publication 169, "Radio-frequency connectors," has recently been issued. Relating to connectors for r.f. transmission lines for use with electronic equipment, the publication establishes uniform requirements for electrical, climatic and mechanical properties, test methods, interchangeability and compatibility of connectors and connectors with cables. Price £3 from British Standards Institution, Sales Branch, 2 Park Street, London, W.1.

**U.K. Kompass,** a detailed register of British industry, is available in three volumes (£15 15s the set) from Kompass Register Ltd., R.A.C. House, Lansdowne Road, Croydon, Surrey. Two volumes list suppliers of more than 33,000 products manufactured in the U.K. The third volume details the location, products, share capital, directors, number of employees and other information of over 24,000 manufacturing companies.

**Sound and Vibration Research.**—The Science Research Council has made a grant of £228,200 to the University of Southampton towards the cost of research in sound and vibration under the direction of Professor E. J. Richards, director of the Institute of Sound and Vibration Research. Part of the grant relates to the provision of acoustic chambers and an audiology laboratory.

The Hungarian Society for Optics, Acoustics and Film-techniques is organizing a second conference on **Magnetic Recording** to be held in Budapest between October 11th and 15th, 1966. Papers on the subjects of static magnetic memories and recording on moving magnetic media are invited for inclusion in the conference programme. Further details can be obtained from the society—Optikai, Akusztikai és Filmtechnikai Egyesület, V, Szabadság tér 17, Budapest.

**R.T.E.B.**—The Radio Trades Examination Board this year celebrates its 21st anniversary. During the 21 years it has examined over 22,000 candidates for its certificates in radio and television servicing.

The series of articles, **Elements of Transistor Pulse Circuits**, by T. D. Towers, which appeared in *Wireless World* during 1964, has been used as a basis for a book of the same title published by Iliffe Books Ltd., price 35s.

**Two Years in Space.**—July 26th marked the second year in space of Syncom II, the world's first synchronous communications satellite. Hughes Aircraft Company who designed and built the satellite report that Syncom II stationed above the Indian Ocean has received and transmitted voice and teleprinter messages for an average of 13 hours a day. It has been in use for a total of 9,508 hours and has travelled more than 119 million miles in orbit.

**Ghana's television service,** comprising three transmitting stations at Accra, Kumasi and Sekondi-Takoradi, was officially opened by President Nkrumah on July 31st. The three stations, which serve approximately one quarter of the country, have central studios in the capital. The service, which operates in Band I on 625 lines (7 Mc/s channels) with f.m. sound, was a "turnkey" project of the Marconi Company. Ghana's external sound services have been extended by the installation of two Marconi 250-kW h.f. transmitters at Ejura where there are also six 10-kW h.f. transmitters for internal sound broadcasting.

American production of **colour TV receivers** in April this year was nearly double that of April 1964. The figures are 179,321 compared to 92,318, an increase of 94%. Although April output was down on the March figure of 205,577 the total production for the first four months of this year was 682,178 compared to 378,545 for the same period last year, an increase of 78%.

**Air Defence for Three NATO Countries.**—To control the air defences of Belgium, the Netherlands and West Germany the individual governments have selected the Tactical Air Weapons Control System (T.A.W.C.S.) designed by the Hughes Aircraft Company of Fullerton, California. In order to obtain NATO council approval for modernization of their air defence control system, the three countries formed an international planning group. The system provides the countries with not only collective air defence but also individual facilities for the rapid detection, identification and tracking of potential enemy air threats. Ground installation equipment supplied with the system includes communications, electronic displays, computers and data processing units.

**New Colour Film from C.O.I.**—Aspects of the technology of microelectronics are dealt with in the film "Thin-film Microcircuits" released by the Central Office of Information. The progress of a circuit is followed in this Mullard film from the design stage to the finished product, together with a description of evaluation and final testing. Running time 15 minutes; available on free loan from Central Film Library, Government Building, Bromyard Avenue, Acton, London, W.3.

**1966 I.E.A. Exhibition.**—The next International Instruments, Electronics and Automation Exhibition will be held at Olympia from May 23rd to 28th, 1966. Bookings are 15 per cent up on the 1964 exhibition in which 148 exhibitors out of 729 came from overseas.

**German Radio Show Stamp.**—30 million copies of a special stamp are to be printed featuring the German Radio Show which will be held in Stuttgart from August 27th to September 5th. The design depicts the Stuttgart TV tower surrounded by symbolic radiations.

The ninth B.R.E.M.A. exhibition of **cabinet styling accessories** will be held at the Hotel Russell, London, W.C.1, from September 28th-30th. It will be open each day from 2 to 6 p.m. and admittance is by invitation or business card. There will be 48 exhibitors.

The **Council of Engineering Institutions**, formerly the Engineering Institutions Joint Council, has moved to 2 Little Smith Street, Westminster, London, S.W.1. (Tel. SULLivan 3912-4.)



# PERSONALITIES

**G. D. Speake**, M.A. (Cantab), A.M.I.E.E., appointed Director of Research for the Marconi Company, has since 1962 been chief of research at the Great Baddow Research Laboratories



G. D. Speake

and Development manager for the Radar Division. Mr. Speake, who is 45, took his degree in physics at St. Catharine's College, Cambridge. He joined the Marconi Company in 1950 and was engaged in radar systems research until 1954 when he was appointed chief of the vacuum physics section of the Research Division. Two years later he became chief of the microwave physics section. Before joining Marconi, Mr. Speake was a Flight Lieutenant in the Technical Branch of the R.A.F. and later, instrument manager at the Plastics Division of I.C.I.

Following the acquisition by Marconi Instruments of W. H. Sanders (Electronics) Ltd., **Professor H. M. Barlow**, F.R.S., and **Dr. E. Eastwood**, C.B.E., have been appointed to Sanders' board. Dr. Barlow is Pender Professor of Electrical Engineering at University College, London, where, except for war service, he has been on the academic staff since 1925. During the early part of the war he worked on the development of radar at the Telecommunications Research Establishment and in 1943 was appointed superintendent of the Radio Department at the Royal Aircraft Establishment, Farnborough. Dr. Eastwood joined the English Electric Group at the Nelson Research Laboratory, Stafford, in 1946, where he was in charge of radiation studies. Two years later he was appointed deputy chief of research with Marconi's at Chelmsford, and subsequently became Director of Research. Dr. Eastwood has been primarily engaged in research in the field of molecular constitution and in the application of radar techniques to the investigation of celestial noise and the detection of meteors.

**Harold Peterson**, who has been in Australia since 1960 as managing director of both British Automatic Telephone & Electric Co. Ltd., and Communication Systems of Australia Pty. Ltd., as well as a director of other Australasian companies, has been appointed chief executive of the Plessey Company's South African Region. Plessey's interests in the region include the Instrument Manufacturing Corp. of South Africa which produces the Tellurometer radar surveying instrument. Mr. Peterson, who is 46, began his career with the G.P.O., was in Royal Signals throughout the war, then with Cable & Wireless for eight years before joining A.T. & E. which is now part of Plessey.

**F. W. Stoneham**, M.B.E., Ph.D., B.Sc.(Eng.), A.M.I.E.E., who recently joined Creed & Company (makers of teleprinting and data processing equipment) as managing director has also been appointed a director of ITT Europe Inc. Dr. Stoneham is a graduate of University College Nottingham and was in the Royal Corps of Signals from 1939 until 1954 when he retired with the rank of Lt. Colonel. He was then with Smiths Aircraft Instruments until 1959 when he joined Ultra as chief engineer. He was managing director of Ultra Electronics when he left in May this year.

**Geoffrey F. Meakes**, who has been with the Racal Organization in the U.K. since 1951 and was responsible for a large part of the development of the famous Racal RA.17 communications receiver, has become chief engineer of Racal Communications Inc., of Silver Spring, Maryland, U.S.A. He was intimately associated with setting up Racal Communications Inc., and Racal (Canada), Ltd.

**W. R. Parkinson**, founder of the original Radio Gramophone Development Company has retired. When the R.G.D. factory at Bridgnorth became A. T. & E. (Bridgnorth) Ltd. he became technical director and he is here shown (left) being presented with a pair of binoculars by E. J. Bartlett, manager of A. T. & E. (Bridgnorth)



**Dudley Seward**, O.B.E., managing director of Rank-Bush Murphy for the past four years, has been appointed general manager of the consumer products division of Standard Telephones & Cables in succession to **Gibson B. Kennedy**, who is returning to the United States. In his new position, Mr. Seward is responsible for the K.B., R.G.D., Regentone, Ace and Argosy brands of domestic sound and television equipment manufactured at Footscray (where he has his headquarters), Hastings and Rhyl. Mr. Seward, who was at one time managing director of Texas Instruments Ltd., is a member of the P.M.G.'s Television Advisory Committee.



D. Seward

**E. C. J. Jezierski** has been appointed chief engineer of Radio Communications Co., of Crewkerne, Somerset. Previously he was research director with Derritron Research Development Ltd., where he was concerned with the design of telecommunications, telemetry and missile control equipment.





**Air Cdre. Lionel H. Greenman**, C.B.E., who has been senior air staff officer, R.A.F. Signals Command since May last year, has been transferred to technical operations at the Maintenance Command H.Q. Air Cdre. Greenman, who is 50, was a Post Office engineer before joining the R.A.F.V.R. in 1936. In 1943 he went to America and became deputy director of technical requirements with the R.A.F. Mission in Washington. For two years from 1959 he was commanding No. 30 Maintenance Unit, R.A.F. Sealand, Cheshire. He is succeeded as senior air staff officer at Signals Command by **Air Cdre. John Goodman**, M.I.E.R.E., who joined the R.A.F. in 1932 as an aircraft apprentice at No. 1 Electrical and Wireless School, Cranwell. During and since the war he has served at various bases at

home and overseas and at the Air Ministry. In 1962 he took command of the Radio Engineering Unit at R.A.F. Henlow and since 1963 has been commandant of the Central Signals Establishment.

**J. R. Humphreys** has become general manager of A. C. Cossor's Industrial Products Group. He will be responsible for the operations of the Cossor Instrument Co., Cossor Communications Co., Best Electrics and Cossor Valve Co. He succeeds **J. F. Eldredge**, who, after spending over three years at Cossor, is returning to Raytheon in the United States. Mr. Humphreys was, until recently, divisional manager of the Telecommunications Division of Elliott Bros. (London) Ltd., prior to which he



J. R. Humphreys

was for a number of years chief engineer of Pye Telecommunications.

## "The Indefatigable Dr. Eccles"

### 90TH BIRTHDAY OF A LAST CENTURY PIONEER

A NAME to conjure with in the more elevated radio-technical circles during the first quarter of the present century was that of Dr. W. H. Eccles, F.R.S., who recently celebrated his 90th birthday. His name recurred constantly in *Wireless World* during its early years.

William Henry Eccles was born at Ulveston, Lancs., on 23rd August, 1875. It would hardly be too much to say he became the first of the radio physicists, though he has to his credit many contributions to the technology of the art. He came near to being a founder member of the world's first wireless company, the Wireless Telegraph and Signal Co., eventually to become the Marconi Co., which he joined in 1899—during Queen Victoria's reign! That was a year after the firm started at the Chelmsford works. Armed with an Honours B.Sc. in physics, gained the year before from the Royal College of Science, he started work on the design of oscillation transformers or "jiggers," as they were called, for the new tuned sets that were just coming in. He also started a study of the coherer, the only detector of the period, which led to a better understanding of the action of that temperamental device. Then, after a short spell as editorial assistant on *The Electrician*, he changed over to teaching electrical engineering, physics and mathematics. Whenever opportunity offered he did radio research.

What was probably Dr. Eccles's most significant work was on a subject at the very heart of our affairs—on radio wave propagation. In 1911 he published a Royal Society paper explaining and expanding the theory put forward by Oliver Heaviside some ten years earlier and since then largely forgotten or ignored. Heaviside had tentatively said "there may possibly be a sufficiently

conducting layer in the upper air. . . ." Eccles now suggested that the ionizing effect of sunlight might account for observed differences between day-time and night-time transmissions. The subject, which was treated in greater detail later, aroused quite violent controversy but, by the end of 1912, when some support for his ideas came from observations made during a partial solar eclipse, the Eccles theory was widely accepted and solid foundations were laid for subsequent work by Appleton and others.

It would hardly be too fanciful to put forward Dr. Eccles as the grandfather of the transistor. In 1909 he demonstrated oscillating crystal detector circuits and developed the general theory "that under certain conditions a rectifying detector could become a generator of oscillations and conversely a generator of oscillations could be used as a rectifier."

One of his minor contributions was the proposal in 1919 of what has since become the universal valve nomenclature—diode, triode, heptode, etc. *Wireless World* may well blush with shame for having stigmatized that proposal of "the indefatigable Dr. Eccles" as being "too academic" for general acceptance. He was often ahead of his times.

When, just after the first World War, the project for a British "Imperial Chain" of long-wave stations was revived Dr. Eccles was appointed vice-chairman under Lord Milner of a Government committee to plan the details. Before the scheme came to fruition the "short-wave bombshell" was exploded but the long-wave Rugby station eventually started operation.

During his distinguished career he occupied many important posts and has accumulated an impressive list of honorifics. He is Past-President of the

Physical Society; of the Institute of Physics; of the Institution of Electrical Engineers; of the Radio Society of Great Britain and *President d'Honneur* of the International Radio Scientific Union (U.R.S.I.) of which he was a member almost from its beginnings.

Dr. Eccles recently talked about some of his little-known activities during the first World War. In 1915 he was invited to advise the War Office on radio matters and devised a short-wave transmitter with valves in push-pull capable of oscillating at the then unheard-of high frequency of 60 Mc/s. Sets to this design were tried by the French army for short-distance work, but the signals were heard as far away as Syria. That was the first indication that short waves had possibilities for long-distance working. At about the same time he devised a valve-maintained tuning fork for frequency control.

In 1917, when Professor of Electrical Engineering and Applied Physics at the City and Guilds Institute, he was appointed to the anti-submarine committee and the college laboratory was taken over by the Admiralty. Many applications of valves to underwater signalling and detection were developed.

After 1924, when Dr. Eccles suffered a severe illness, he was forced to confine his activities to private consultancy. He now lives in retirement on the South Coast. Happily, his health is now remarkably good except for failing eyesight and his memory exceptionally clear. In boyhood he spent some months in a Quaker community near the birthplace of Michael Faraday (whom he greatly admires) and there absorbed the faith to which he has since adhered. By reason of his beliefs, he has been reluctant to patent his inventions.

H. F. S.



# Demonstration of Oscillatory Action

By T. PALMER,\* B.A., Grad.I.E.E., Assoc.I.E.R.E.

**I**N a previous article<sup>1</sup>, a description was given of a method for demonstrating the phase difference of currents flowing in a parallel arrangement of L, C and R. The signal source was an oscillator with a frequency of 5 cycles per minute and phase difference was demonstrated by the pointer movements of moving-coil centre-zero

meters. By using a double-beam cathode ray oscilloscope and an a.f. signal generator our demonstrations can be extended to display oscillatory action.

\* Acton Technical College.

<sup>1</sup> "Demonstrating A.C. Theory," by T. Palmer, *Wireless World*, October 1963, p. 515.

Parallel resonance can be demonstrated by the circuit of Fig. 1. Suitable values are 30mH for the coil and 0.5 $\mu$ F for the capacitor. The A2 trace of the oscilloscope displays the generator voltage, and the A1 trace displays the voltage across the tuned circuit. By varying the frequency of the signal generator above and below the resonant frequency the effect of resonance can be displayed. At resonance the two traces are in phase and the voltage across the tuned circuit has maximum amplitude.

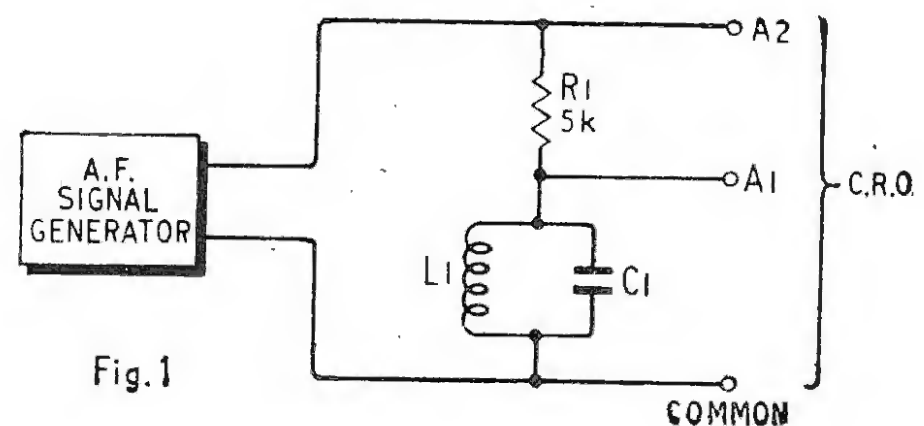
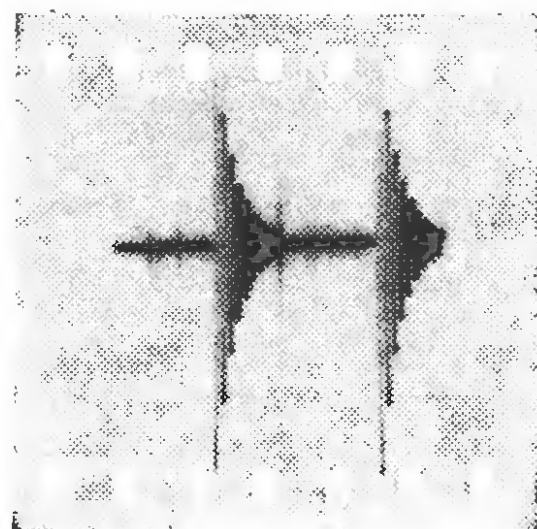


Fig. 1

We now take the circuit of Fig. 1 and modify it to that of Fig. 2. A change-over switch, S1, is operated by a



A

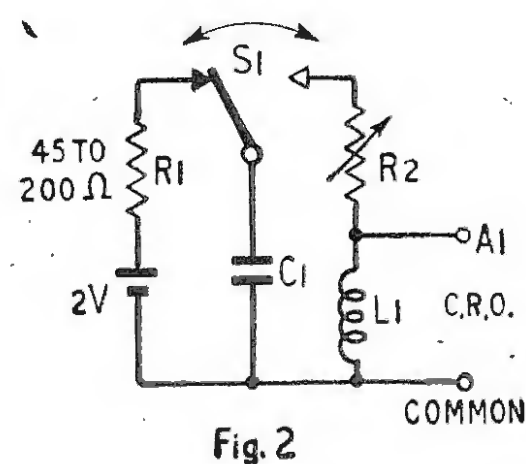
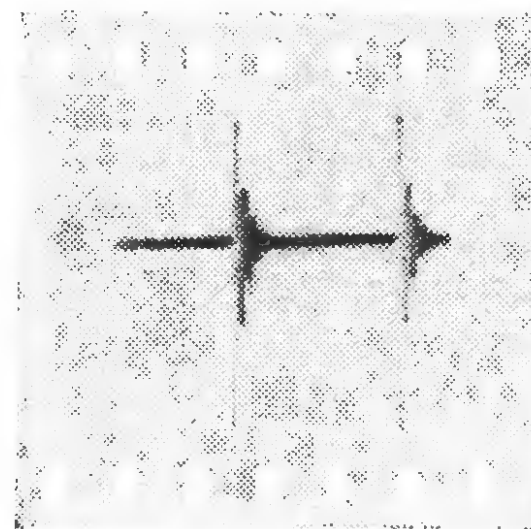


Fig. 2

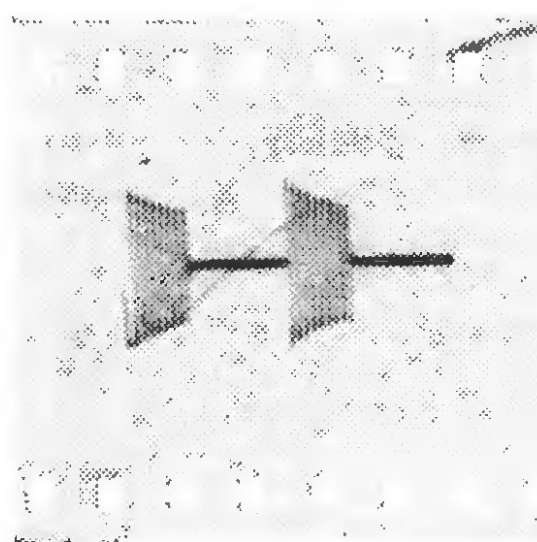
Carpenter relay working at 50c/s. In one position of the switch, a 2-volt accumulator charges C1 through R1; in the other position, C1 discharges through L1 and R2, a variable resistor of 0-50 $\Omega$ . The waveform of the voltage across the coil is shown in Oscillogram A, with R2=0 $\Omega$ . With R2=30 $\Omega$ , the waveform is as shown in Oscillogram B. Having shown this waveform we reduce R2 to zero.



B

In Fig. 3, the coil L1 is connected in the input of a very simple transistor amplifier which has a coil, L2, of 30mH in the collector circuit. First, this coil is remote from L1, and, when the amplifier is switched on, there is no difference in Oscillogram A. However, as the

collector coil L2 is advanced towards L1, the trace on the scope is seen to die away either more rapidly (as if the resistance R2 in Fig. 2 had been increased—negative feedback) or less rapidly (positive feedback). Whether we have the first effect or the second depends, of course, on



C

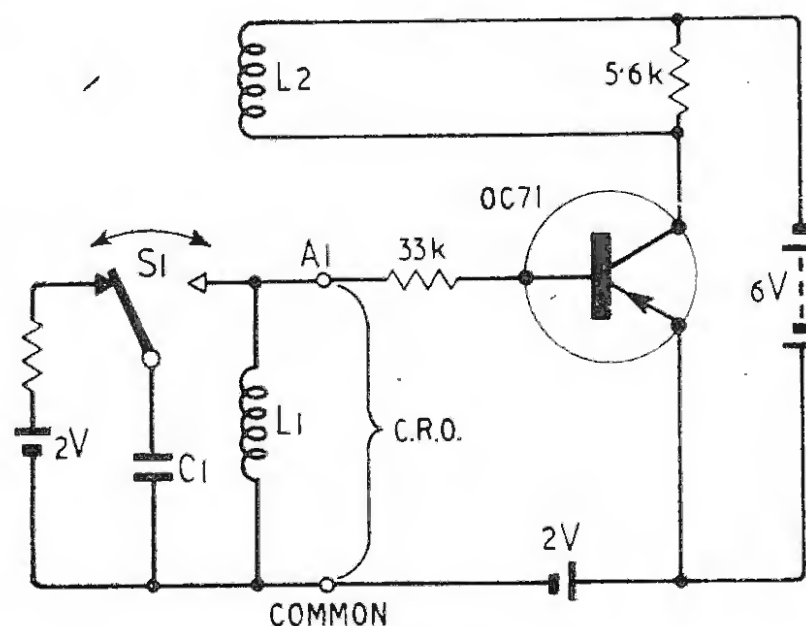
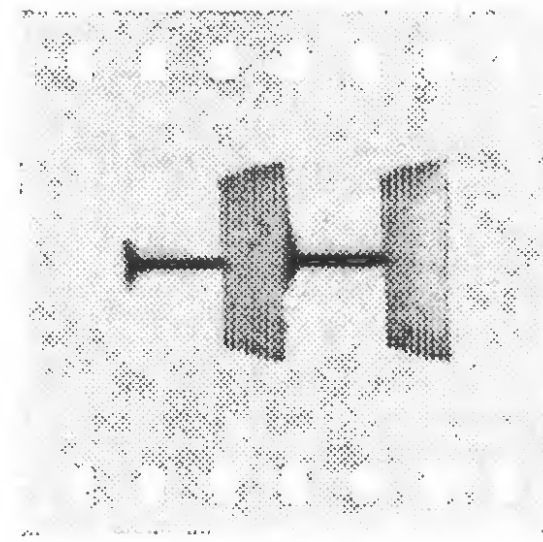


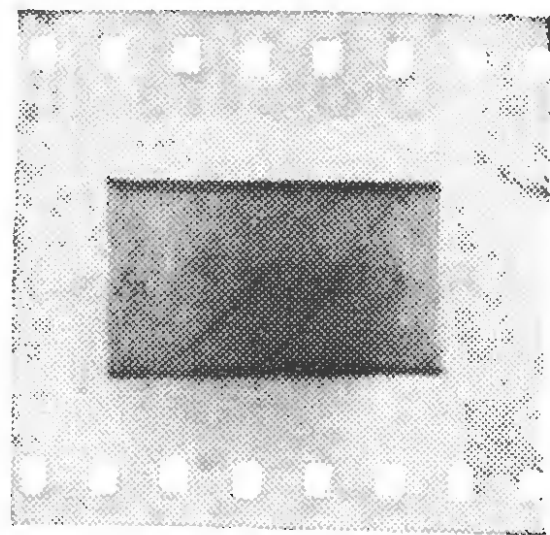
Fig. 3



D

the way L2 is connected. Both effects should be shown in turn. With positive feedback, as L2 is advanced towards L1, the oscillation dies away less and less rapidly (as in Oscillogram C). With L2 still closer to L1, oscillations are seen to grow, as in Oscillogram D.

L2 is left in the position which produces increasing amplitude of oscillation, the Carpenter relay is disconnected and the coil is strapped permanently to the capacitor as shown in Fig. 4. Sustained oscillations are seen as in Oscillogram E and F (for F the time-base has been speeded up) showing that the parallel circuit of Fig. 1 has become part of an oscillator.



E

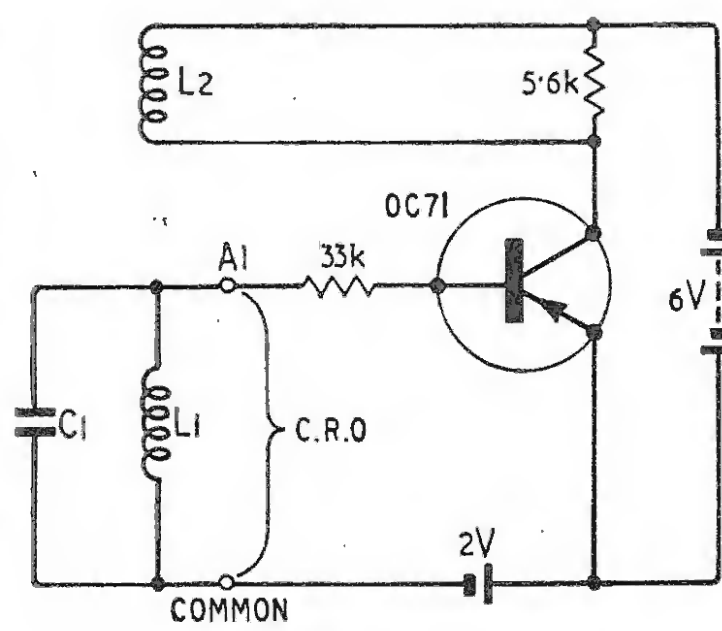
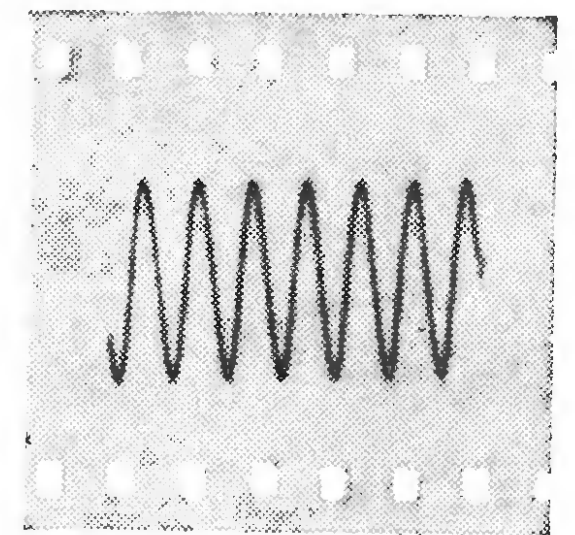


Fig. 4



F

It scarcely needs to be stressed that these demonstrations are intended only for elementary students although the last demonstration may help those who wish to study

the action of super-regenerative circuits. With conditions corresponding to those of Oscillogram D, try charging C1 from batteries of different voltages.

## September Conferences and Exhibitions

Further details are available from addresses in parentheses

- |  |                         |   |                    |
|--|-------------------------|---|--------------------|
| <b>LONDON</b><br>Sept. 13-17.<br><b>Engineering Materials &amp; Design Exhibition</b><br>(Industrial Trade Fairs, 1-19 New Oxford St., W.C.1)            | Olympia                 | <b>SWANSEA</b><br>Sept. 21-23<br><b>Physics of Semiconducting Compounds</b><br>(Inst. Phys. & Phys. Soc., 47 Belgrave Sq., London, S.W.1)                         | University College |
| Sept. 13-17<br><b>Microwave Behaviour of Ferrimagnetics &amp; Plasmas</b><br>(I.E.E., Savoy Place, W.C.2)  | Savoy Place             | <b>OVERSEAS</b><br>Sept. 4-12<br><b>Italian Radio &amp; TV Show</b><br><b>International Electronic Components Show</b><br>(A.N.I.E., via Luciano Manara 1, Milan) | Milan              |
| Sept. 20-24<br><b>Thermionic Electrical Power Generation</b><br>(I.E.E., Savoy Place, W.C.2)   | Savoy Place             | Sept. 6-9<br><b>Opto-Electronic Components &amp; Devices</b><br>(M. Coulmy, D.R.M.E., 7 rue de la Chaise, Paris, 8)   | Paris              |
| <b>BRIGHTON</b><br>Sept. 28-Oct. 1<br><b>European Medical Electronics Symposium &amp; Show</b><br>(Symposium Secretary, 4 Mill Street, London, W.1)      | Hotel Metropole         | Sept. 6-11<br><b>Electromagnetic Wave Theory</b><br>(Dr. R. Timman, c/o Technological University, Julianalaan 132, Delft)   | Delft              |
| <b>CAMBRIDGE</b><br>Sept. 1-7<br><b>British Association Meeting</b><br>(British Assoc., 3 Sanctuary Bldgs., Great Smith St., S.W.1)                      |                         | Sept. 7-11<br><b>INEL—Industrial Electronics Exhibition</b><br>(Swiss Industries Fair, Postfach, Basle 21)  | Basle              |
| <b>CRANFIELD</b><br>Sept. 20-24<br><b>Network Theory Symposium</b><br>(S. R. Deards, College of Aeronautics, Cranfield, Beds.)                           | College of Aeronautics  | Sept. 7-14<br><b>International Congress on Acoustics</b><br>(5e Congrès International d'Acoustique, 35 rue Saint-Gilles, Liège, Belgium)                          | Liège              |
| <b>LIVERPOOL</b><br>Sept. 15-17<br><b>Nuclear and Particle Physics</b><br>(Inst. Phys. & Phys. Soc., 47 Belgrave Sq., London, S.W.1)                     | The University          | Sept. 9-11<br><b>Industrial Electronics &amp; Control Instrumentation</b><br>(L. Winner, 152 W42nd St., New York 52)  | Philadelphia       |
| <b>MANCHESTER</b><br>Sept. 6-10<br><b>Materials &amp; Environmental Testing</b><br>(Inst. Mech. Engrs., Birdcage Walk, London, S.W.1)                    | Col. of Science & Tech. | Sept. 9-19<br><b>International Radio &amp; TV Salon</b><br>(F.N.I.E., 16 rue de Presles, Paris 15)  | Paris              |
| Sept. 7-9<br><b>Internal Friction in Solids</b><br>(Inst. Phys. & Phys. Soc., 47 Belgrave Sq., London, S.W.1)  | The University          | Sept. 14-Nov. 12<br><b>I.T.U. Plenipotentiary Conference</b><br>(International Telecom. Union, Place des Nations, Geneva)   | Montreux           |
| Sept. 28-Oct. 2<br><b>Electronics, Instruments &amp; Components Show &amp; Convention</b><br>(Institution of Electronics, 78 Shaw Rd., Rochdale, Lancs.) | Belle Vue               | Sept. 17-19<br><b>International Ham Convention</b><br>(L. Vervarcke, Lippenslaan 284, Knokke, Belgium)  | Knokke             |
| <b>OXFORD</b><br>Sept. 5-11<br><b>Electromagnetic Distance Measurement</b><br>(Royal Society, 6 Cornwall Terrace, London, N.W.1)                         |                         | Sept. 17-26<br><b>Firato Electronics Exhibition</b><br>(RIA, Europaplein 8, Amsterdam)  | Amsterdam          |
| <b>SOUTHAMPTON</b><br>Sept. 21-23<br><b>Applications of Microelectronics</b><br>(I.E.E. Symposium, The University, Southampton)                          | The University          | Sept. 17-Oct. 3<br><b>British Exhibition</b><br>(British Overseas Fairs, 21 Tothill St., London, S.W.1)   | Tokyo              |
|  |                         | Sept. 21-23<br><b>Conference on Magnetism</b><br>(Verein Deutscher Eisenhüttenleute, Breite Str. 27, Düsseldorf)  | Vienna             |
|  |                         | Sept. 22-24<br><b>Military Electronics Convention</b><br>(I.E.E.E., Box A, Lenox Hill Station, New York 21, N.Y.)   | Washington         |



# LETTERS TO THE EDITOR

The Editor does not necessarily endorse opinions expressed by his correspondents

## Transistor Cascade Crystal Oscillator

IN my article in the July issue there is a mis-statement in the paragraph under the heading "The Bootstrap Cascade Circuit". The offending sentence reads: "Both transistors are used in the common-base connection, though this may not be apparent from the circuit diagram." The wording should read: "Tr<sub>2</sub> is used in the common base connection while Tr<sub>1</sub> is a common collector stage which acts as the collector load impedance of Tr<sub>2</sub>".

My attention was drawn to this slip by a young reader, Mr. C. Marcus, of Ashted, Surrey, who pointed out in a well-reasoned letter that there is no alternating potential on the collector of Tr<sub>1</sub>. He went on to justify his comments by re-drawing the circuit to illustrate the a.c. conditions more clearly and finally he built circuits and obtained both sinusoidal and relaxation oscillations at will.

My description of the functions of Tr<sub>1</sub> was perhaps too brief but the point had been more fully covered in an earlier article on "Transistor Wide-Band Cascade Amplifiers" (March 1965). Some further explanation is required. If in Fig. 4 of my July article the quartz crystal, the feedback diodes and their associated capacitors are removed, we are left with two series-connected transistors and their bias networks. If an alternating signal voltage is applied to the emitter of Tr<sub>2</sub> it acts as an earthed-base amplifier. Its complex collector load is formed by Tr<sub>1</sub>, R<sub>1</sub>, R<sub>2</sub>, R<sub>5</sub> and C. If C is large, or if its reactance is low at the signal frequency, the alternating output voltage of Tr<sub>2</sub> appears at the base of Tr<sub>1</sub>, across R<sub>1</sub>. If the output is taken from the emitter of Tr<sub>1</sub>, it is at low impedance since this transistor is acting as an emitter follower. At the same time Tr<sub>1</sub> and its associated components simulate a very high-impedance collector load for Tr<sub>2</sub>, giving a large voltage gain, without calling for an excessive supply voltage. A limit to the load impedance is in fact set by R<sub>1</sub> which (with large C), is effectively in parallel with the load presented by Tr<sub>1</sub> and R<sub>5</sub> in series. High gain thus calls for a high value of R<sub>1</sub>, with proper selection of R<sub>2</sub>, R<sub>3</sub> and R<sub>4</sub> to maintain the correct operating bias. To sum up, Tr<sub>1</sub> acts simultaneously as a high-impedance load as seen from Tr<sub>2</sub> and also as an output stage of low impedance to any load connected to its emitter terminal.

Finally, I mentioned the possibility that the new crystal oscillator might be suitable for development into a high-grade frequency standard. Readers interested in this topic are referred to a recent paper by P. J. Baxandall, "Transistor Crystal Oscillators and the Design of a 1 Mc/s Oscillator Circuit of Good Frequency Stability", *Radio and Electronic Engineer* (I.E.R.E.), Vol. 29, No. 4, April 1965, p.229. It takes a new look at some well-established oscillator circuits, re-drawing them to suggest a fresh analytical approach, makes a critical comparison of the Pierce and Miller circuits and finally gives details of a new series resonance oscillator of high performance.

Although many designs for stable crystal oscillators have been published, some actually going into details like component values, nearly all have the weakness that no reasons are given for the choice of the techniques actually used. In this respect Peter Baxandall's paper is outstanding. It provides a wealth of unique information

to the designer of such equipment, for whom it is not too much to say that the paper is indispensable.

Cheltenham, Glos.

F. BUTLER

## Units

MR. GIBBS writing again on this subject at considerable length in the August issue, dismisses my first three points (April issue, p.196) as matters merely of convenience rather than principle. Is convenience not then important? Yet paradoxically he himself raises a point of convenience in conjuring up a fanciful picture of SI advocates trying to persuade semiconductor specialists to measure the volume of germanium in cubic metres. Does he really suppose that I or anyone else would spend our time campaigning for the statement of inter-electrode capacitances in farads? The SI system does not exclude the well-known set of multiples and submultiples. Incidentally, I disposed of this argument in my original article.

Mr. Gibbs is just as wrong in his closing sentence suggesting, on no evidence at all, that I wish to enforce any system of units by legislation. He must be running short of arguments to have to invent Aunt Sallies to hit out at. He also ignores my point (6), which is a matter of principle.

The first argument in his letter seems to be based on the premise that what a lot of people have done must be right. Are there no such things as enlightenment and progress?

I do not intend to waste space by arguing the essential difference between H and B, when it has been done by writers of much greater authority whose works are on record for Mr. Gibbs or others sufficiently interested.\*

Mr. Gibbs undermines his own case against electrical charge being basically one quantity, whether reckoned in e.m. or e.s. c.g.s. units, by his arguments for the identity of H and B. If he can believe that electric charge is fundamentally two quantities at the same time as believing H and B are fundamentally one quantity he can believe anything. And then he goes on "From the atomic point of view, then, a distinction between the units of B and H is a considerable inconvenience," when he has already dismissed convenience as too unimportant to discuss compared with principle! Incidentally, I have recently written a book on atomic electronics without being conscious of the inconvenience mentioned. Neither, apparently, were the physicists Bleaney and Bleaney in their very successful textbook on electricity and magnetism from the modern point of view (now in its second edition), written throughout in m.k.s.a. units.

I do seem to have based my appeal to Maxwell on an incomplete reading of the context, and am obliged by Mr. Gibbs to conclude that on this matter he has been proved wrong, as he admittedly has been with regard to his Art.501 which states that magnetic force acts on the conductor, not the current.

I am fairly sure that arguments in favour of the c.g.s.

\* E.g.: C.W.O.H., "Wireless Engineer", Feb. 1933 p. 61; Apr. 1933, p. 179 Dec. 1949, p. 383; etc.  
Sir J. J. Thomson, "Elements of Electricity and Magnetism" 5th edn., (1921), Art. 153.  
O. Heaviside, "Electromagnetic Theory," Vol. 1, Arts. 20-23.

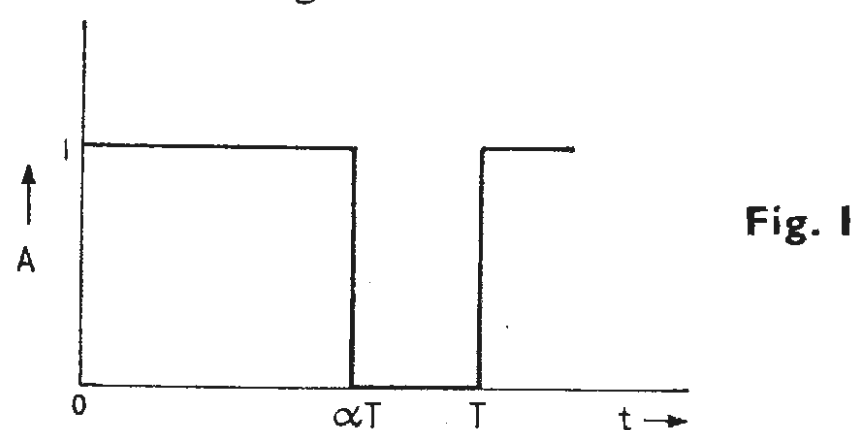
systems made now will look rather quaint to our successors in the not very remote future.

“CATHODE RAY”

## Radiation from Class D Amplifiers

IN the July issue of *Wireless World* Mr. F. Butler pointed to the problem of radiation caused by class D amplifiers. The radio frequency interference produced by the carrier and its harmonics can indeed be quite objectionable if no special precautions, such as low-pass filters or screened and twisted loudspeaker leads, are used. The design of such filters, however, is particularly difficult as the introduction of linear frequency-dependent circuits may cause non-linear distortion of a different nature than already discussed for purely inductive loads. To understand this phenomenon it is necessary to know more about the high-frequency components of p.w.m.

The rectangular waveform shown in Fig. 1, having a



variable mark-space ratio denoted by  $\alpha$ , can be represented by:

$$F(s) = \frac{1}{s} \frac{1 - e^{-\alpha s T}}{1 - e^{-s T}}$$

where  $T$  is the duration of one period. Apart from the low-frequency component which is intended to flow through the load it can be shown that the high-frequency components (first and higher order harmonics) are given by:

$$F_h(t) = \frac{1}{\pi} \sum_{n=1}^{\infty} \frac{1}{n} \left\{ \sin(n\omega t - 2n\pi\alpha) - \sin n\omega t \right\}$$

$$\text{or } F_h(t) = \sum_{n=1}^{\infty} \frac{\sin n\pi\alpha}{n} \cos(n\omega t - n\pi\alpha)$$

where  $\omega$  is the angular velocity of the p.w.m. repetition rate (first harmonic) and  $n$  is the order of each harmonic. This formula shows that each component is phase modulated and that the modulation index for each component is proportional to its order. Further the amplitude of each component is inversely proportional to  $n$ , and varies with the mark-space ratio  $\alpha$  as given in Fig. 2.

Thus, when the pulse width is modulated, simultaneous amplitude and phase modulation of each component occurs in such a fashion that the pulse width corresponds uniquely to the amplitude and phase relationship given by the formula. When this relationship is distorted by a low-pass filter having an improperly designed amplitude and phase characteristic, the pulse width at the output will be altered with respect to the p.w.m. at the input. Although generally this distortion will be non-linear (depending on the characteristics of the filter) it is of no consequence as long as the load is a purely linear element. This is because the high-frequency components contain no d.c. or l.f. component and will average out in a normal loudspeaker.

The situation is different when part of the energy at the input of the filter is reflected back into the output stage.

In the properly designed filter the prescribed relationship between the harmonics is maintained and only loss of efficiency may occur. However, if this is not the case, a superposition of two signals, only related by the filter characteristics, is presented to the highly non-linear output stage and gives rise to modulation effects. The result is not only non-linear distortion of the audio signal (depending on the transistor switch characteristics as already discussed in these pages) but also beat products between the high-frequency components themselves. This last effect is particularly objectionable, since the beat product of the harmonics of the 2nd and 3rd order then not only produces a non-linearly distorted audio signal but may again beat against the first harmonic, producing more distortion. This type of distortion is unique to the class D amplifier and cannot be compared to that produced by the more conventional classes

As transistor switches are not the ideal generators to match filters to, it is advisable that the group delay of the filter is constant over a sufficiently large range to ensure that the energy of reflected harmonics is low enough when the prescribed relationship between them is lost. This is not true for all types of loudspeaker, so one should be careful in selecting a suitable reproducer.

Much has been said in these pages on the subject of p.w.m., but it seems less known that a class D amplifier driven by a f.m. signal is equally capable of producing audio amplification. The only difference between the two methods is that f.m. differentiates the modulating signal if the modulation index is independent of the frequency of the modulating signal, whereas p.w.m. does not. In a properly designed f.m. audio amplifier the audio signal should therefore be integrated before modulation. This effect explains why, in the case of, e.g., the closed loop p.w.m. amplifier, the distortion introduced by the limited p.w.m. can be compensated by frequency modulation of the p.w.m. repetition rate—or, as Mr. K. C. Johnson put it in the May issue: “might not the feedback . . . ‘know’ that a judicious amount of f.m. can actually reduce the troublesome l.f. sidebands?” However, it will be clear that a suitable filter for f.m. is even more difficult to design than for a fixed repetition rate.

Finally, it seems surprising that the more conventional circuits for producing p.w.m. as used in telemetry, etc., have not been discussed. As so many readers are vividly interested in the subject, a fairly simple circuit is given in Fig. 3 which needs little explanation. A symmetrical driver feeds a flip flop modulator (2N1304), which in turn drives directly the symmetrical output stage. The transistors in this last stage are driven hard so that extra

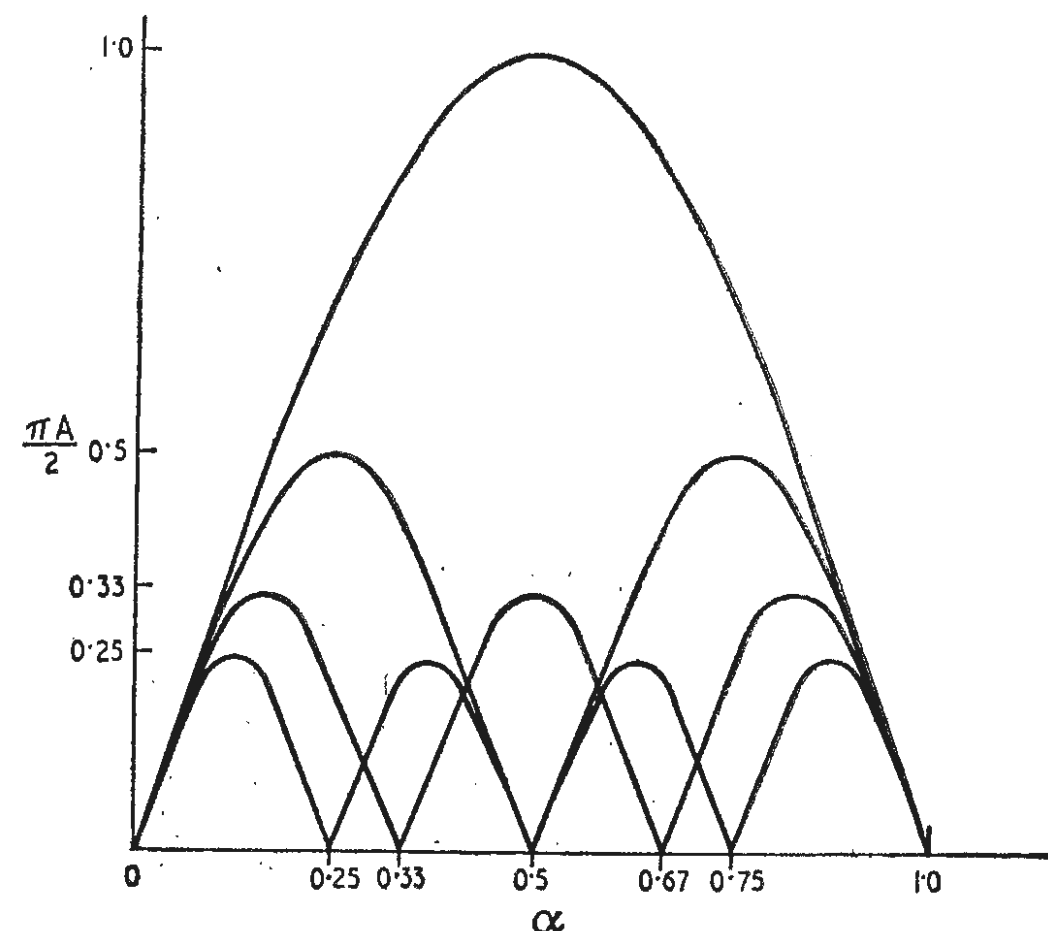


Fig. 2



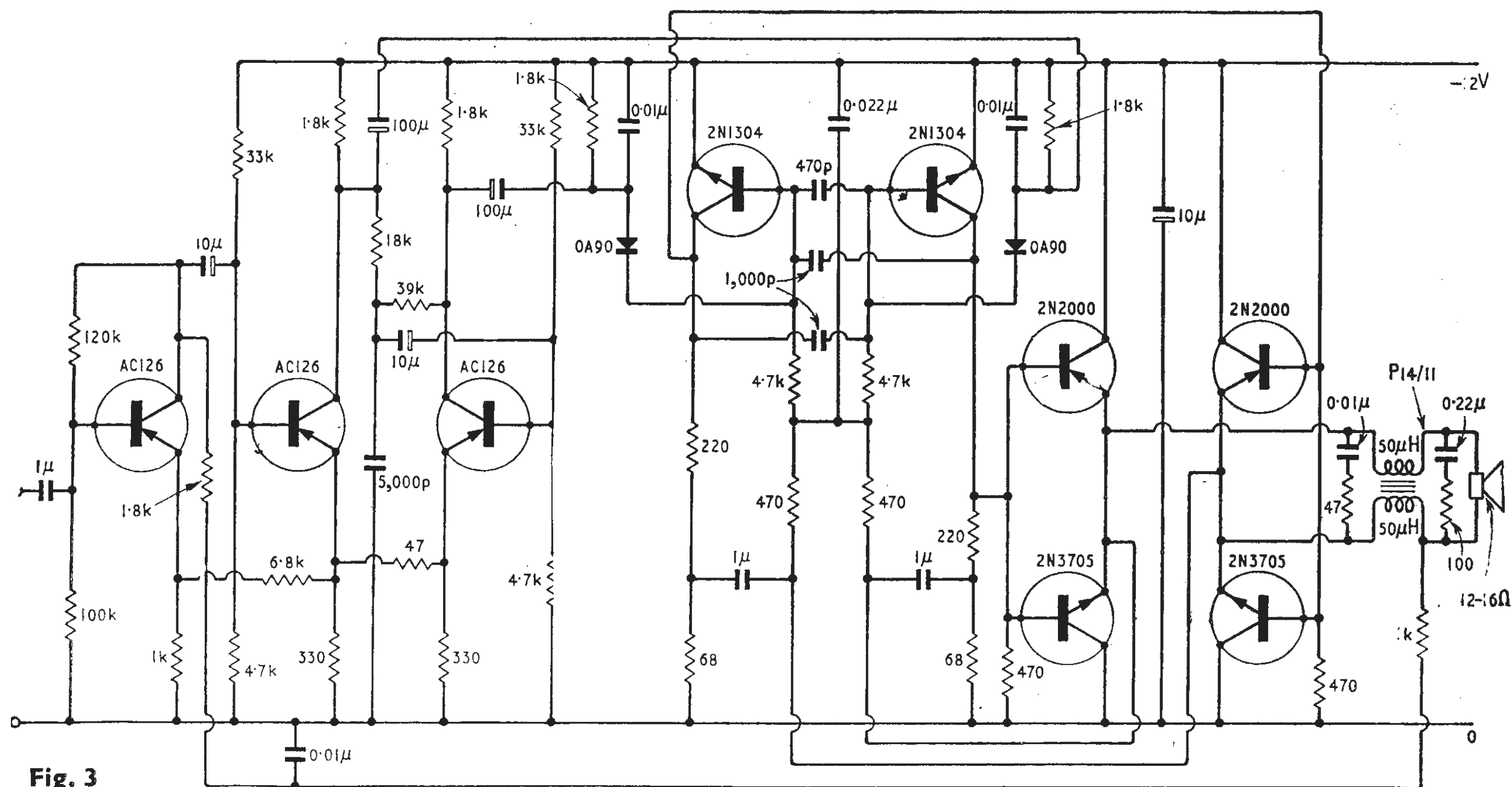


Fig. 3

diodes to provide alternative paths are not necessary. Furthermore, the simple (but by no means optimum) filter is damped to reduce the reflected energy.

Amsterdam.

D. BOSMAN

## Satellites & TV Standards

YOUR editorial in the August issue has, rightly, raised the problem of television standards and the use of synchronous satellites. May I suggest that a possible solution offers itself, if we have the courage to accept the fact that the new u.h.f. television service for the U.K. is obsolete before it has got off the launching pad?

The plan for the u.h.f. service is, by now, well known. The country is to be covered by a number of high-powered transmitters, with a number of low-powered "fill-in" stations to cater for the low-lying and badly shadowed regions. A capital expenditure of some £100 million will be involved.

It has recently been announced that a satellite housing a high-powered transmitter can be put into orbit and it is, surely, more practical (and very much cheaper) to use such a satellite to broadcast the country's television service. The satellite could be commissioned and put into orbit for, probably, less than £20 million, and maybe it could be simplified by being engineered for this exclusive use. Existing problems of co-channel and similar interference would not arise, neither would those due to propagation over the earth's surface.

The satellite signal frequencies would, of course, need to be very much higher than the u.h.f. band in order that a high-gain aerial of modest dimensions could be used at the receiver. Existing receivers need not, however, be made obsolete; a frequency converter could be fitted either as part of the aerial installation, or at the receiver.

If we used such a system it would, of course, provide "free" television programmes to a large proportion of the earth's surface. Herein lies a particularly attractive aspect of the system. We could "go-it-alone" with the reasonable assurance that viewers in other countries will wish to see these "free" programmes. It is probably too

much to hope that such a venture could be a combined European operation in its early stages.

Is it too late to re-cast the country's television service into a sophisticated system that could be far in advance of any other? It could give receiver manufacturers the "shot-in-the-arm" they so desperately need.

R. S. ROBERTS

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## FURTHER EDUCATION

THE following courses to be held at various centres during the forthcoming academic year have been selected from information received as being of particular interest to *Wireless World* readers.

**Twickenham College of Technology.**—In addition to part-time courses leading to the O.N.C. and H.N.C. with endorsements for the graduateship examinations of I.E.E. and I.E.R.E., special lecture courses are available on fundamentals of semiconductor devices, transistor circuit design, basic electronics, network analysis and basic principles of systems analysis.

Full-time and part-time post-graduate courses in electrical engineering leading to the internal M.Sc.(Eng.) degree of the University of London commence on September 27th at **West Ham College of Technology**, London, E.15. Evening courses for post-graduates include semiconductor device design, semiconductor circuit design theory and linear network theory.

Among the subjects dealt with by special evening lecture courses at **Hendon College of Technology** are an introduction to microwaves, introduction to automatic computing techniques in industrial applications, transistors and transistor circuit design, and high-fidelity sound reproduction.

The prospectus from the **Northern Polytechnic**, London, N.7, gives details of full-time and part-time degree courses together with a professional course leading to a diploma exempting students from the graduateship examination of the I.E.R.E.

**Bristol Technical College** is offering a two-year full-time course in aircraft radio and electronics as well as courses for the P.M.G.'s certificates for marine radio officers.

**Brighton Technical College.**—Part-time courses and block release courses for technicians are outlined in the Engineering Department's prospectus "A."

Post-graduate laboratory courses at **Portsmouth College of Technology** include a ten-evening course on the analysis and simulation of control systems and another on microwave measurements.

# Semiconductor Detectors for Nuclear Radiation

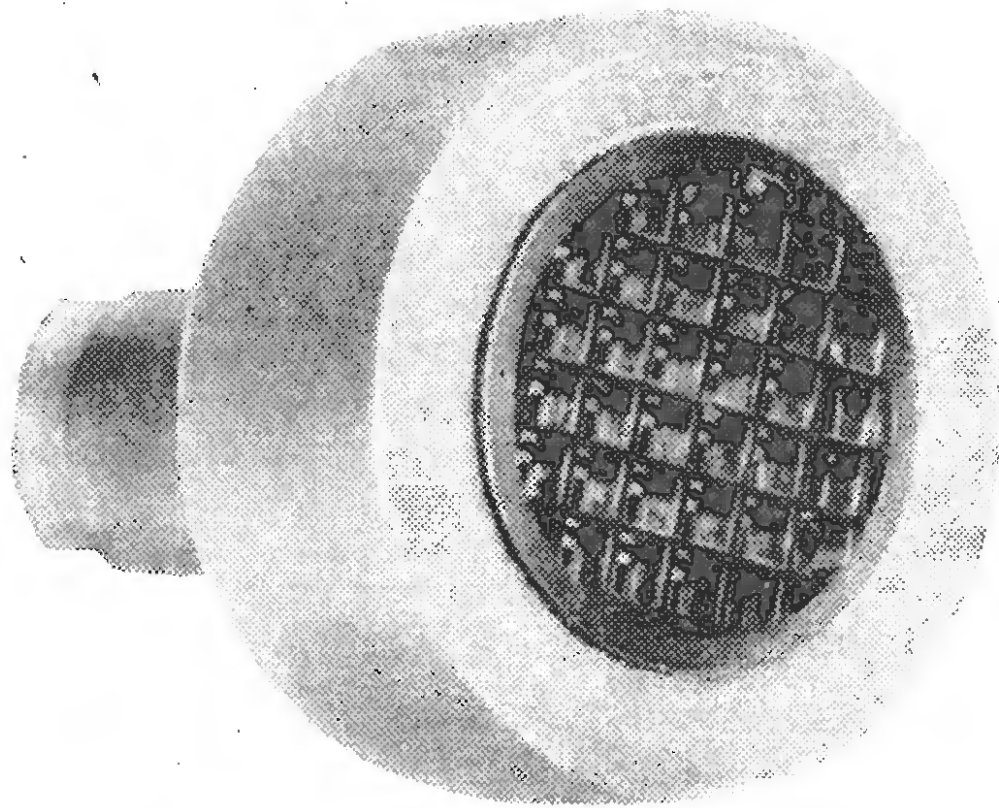
By J. B. DANCE, M.Sc.

IF  $\alpha$ ,  $\beta$  or  $\gamma$ -radiation is absorbed by matter, the energy is dissipated in the formation of ions and excited atoms. With application of a suitable electric field, the ions may be collected at the electrodes and the resulting pulse used to operate a scaler or ratemeter. In some forms of detector (ionization chambers, proportional and Geiger-Müller counters) the ions are formed in a gas, but during the past few years much effort has been expended on solid-state ionization chambers, partly because a solid absorbs energy from penetrating radiation far more effectively than a gas. A particle which will travel 1 metre in air can be absorbed by about 1 mm of silicon. Particles are absorbed in a solid in scintillation counters, but the process by which the energy of the particles is converted first into photons and then into

energy of a  $\gamma$ -ray is shared with an electron; the electron is given a high velocity and a  $\gamma$ -ray of lower energy is formed. The  $\gamma$ -ray may undergo further Compton scattering, but is more likely to escape unless the volume of the absorber is large. Radiation exceeding 1.02 MeV can cause electron-positron pair production. The positron will meet another electron and the two will be annihilated, two  $\gamma$ -rays (about 0.51 MeV) being formed.

In Compton scattering and pair production it is likely that a large fraction of the energy of the  $\gamma$ -ray will escape the absorbing material. If a  $\gamma$ -photon is absorbed by the photoelectric process, however, the whole of the energy of the photon is absorbed. Thus if a detector is used which produces output pulses of an amplitude proportional to the energy absorbed, the amplitude of these pulses will be proportional to the energy of the incident  $\gamma$ -radiation only if the absorption occurs by the photoelectric process.

The photoelectric absorption coefficient is proportional to the fifth power of the atomic number of the absorber. Thus if it is necessary to determine the energy spectrum of  $\gamma$ -photons, it is desirable that the absorbing material should have a high atomic number.



A silicon surface-barrier detector with a detachable collimator (Elliott S.R.D.I.).

photo-electrons at the cathode of a photomultiplier tube is very inefficient.

For any specific material the fraction of the total energy used in ion formation is almost independent of the initial energy of the radiation and of the type of incident particle. Thus a particle of 2 MeV energy will produce about twice as many ions as a 1 MeV particle absorbed in the same medium, but the ions formed by the 2 MeV particle will be distributed over a greater path length. In many types of detector the number of ions collected (and therefore the output pulse amplitude) is proportional to the energy absorbed from the particle. The energy required to form each ion pair in a gas varies from about 22 to 37 eV according to the nature of the gas.

The ionization produced by a charged particle is a result of the electrostatic forces between the particle and the electrons of the matter through which it is passing. The energy of  $\gamma$ -radiation is dissipated indirectly in three main ways. In the photoelectric effect the whole of the energy of a  $\gamma$ -photon is used to eject an electron from an atom; the fast electron then behaves as a  $\beta$ -particle and produces ions. In Compton scattering the

## Resolution of detectors

If a detector is being used for energy spectrometry, the output pulses will not have exactly the same amplitude even if the energy absorbed by the detector from each particle is identical. One reason for this is that the presence of noise pulses may increase or decrease the amplitude of the detector output pulses. In addition, the exact fraction of the energy of the incident particle used to create ions is determined by probability. A similar effect occurs in scintillation counters where the exact fraction of the energy used to create photons (and hence electrons at the photo-multiplier cathode) shows a statistical variation around an average value. Thus if the output pulse amplitude of any detection system is converted into an energy spectrum by means of a pulse height analyser, the spectrum for monoenergetic particles will be of the form shown in Fig. 1. In a spectrum of radiation containing a number of peaks, two of the peaks may be so close together that they cannot be distinguished from a single peak. The width of a single peak at half the

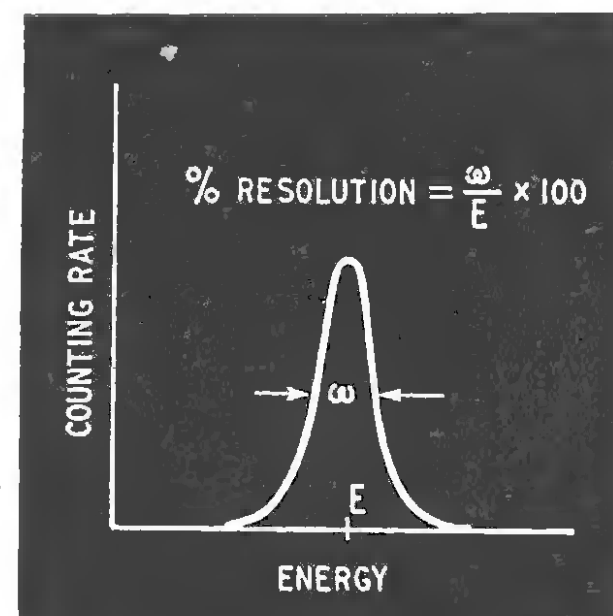


Fig. 1. A typical energy spectrum of monoenergetic radiation.



maximum height may be used as a measure of the energy resolution of the system.

## SEMICONDUCTOR DETECTORS

In order that the statistical spread of each energy peak shall be as small as possible, the material of the detector should be chosen so that as many ions as possible are formed for each MeV of energy absorbed from incident radiation. Not only will this reduce the statistical spread in the number of ions formed, but it will also increase the signal amplitude and therefore reduce the effect of any noise pulses.

Each ion pair formed in a semiconductor material requires an energy of about 2-4 eV; this is only about one tenth of that required by gaseous absorbers. It is also very much smaller than the energy required to produce one photoelectron in a scintillation counter (which varies from about 200 eV in a thallium-activated sodium iodide crystal to over 1 keV in organic phosphors). Semiconductor detectors can therefore show excellent energy resolution.

If the maximum resolution is limited by the noise level, it might be expected that semiconductor detectors would show an improvement of about ten times when compared with gas filled detectors. If, however, the statistical spread in the fraction of the energy which is used to create ions is limiting the resolution obtainable, it would be expected that the use of a semiconductor detector would improve the resolution by a factor of  $\sqrt{10}$ . In practice noise often limits the resolution, but other factors must be taken into account, particularly the noise introduced by the first stage of the amplifier used.

The number of ions formed in a semiconductor material per MeV of absorbed energy is inversely proportional to the gap in the energy band of the material used. It will be shown, however, that other factors are more important than this in the choice of the semiconductor material.

### Homogeneous detectors

Semiconductor detectors may be divided into two main types, the homogeneous detectors and the junction detectors. Homogeneous detectors consist of a piece of semiconductor material sandwiched between two electrodes. They can be used for individual particle counting only if the temperature is very low, but certain types of homogeneous detector can be used for integrated flux measurement at normal temperatures. Junction detectors can be used for counting individual particles both at room and low temperatures, but have the disadvantage that their sensitive volume is severely limited. In order to appreciate how these types of detector have been developed and why they have certain limitations, it is necessary to consider the properties of the semiconductor materials used.

The material to be used in a solid-state ionization chamber designed for counting individual particles must have a fairly low specific conductivity, or statistical fluctuations in the steady current passing between the electrodes (i.e. noise) will provide pulses of the same order of amplitude as the pulses caused by the radiation being detected. As in a gas-filled detector, the number of charge carriers present in unit volume of the material in the absence of radiation must be relatively small, although it is desirable that their mobility shall be large in order to obtain short pulse rise times for fast counting. This requirement seems to indicate that a high-purity semiconductor material with a fairly large energy gap

should be chosen so that the number of thermally generated charge carriers will be comparatively small.

A second requirement is that the mean free carrier lifetime should be reasonably high. Impurity atoms, dislocations, etc., in the crystal lattice form local energy bands within the forbidden region. These bands act as traps at which free charges may be temporarily or permanently held, since the probability of recombination with a charge of the opposite sign is fairly small at these trap levels. The trap density should be low (as in a gas-filled detector) or a partial loss of the signals will occur together with a change in the properties of the material as the electron population of the traps is altered ("polarization"). The energy resolution will then be impaired.

It is most unfortunate that materials which have the required energy band gaps have carrier lifetimes which are too low. The energy gaps of germanium and silicon are not large enough to enable a homogeneous block of either of these materials to be used as a detector at room temperature, although the trap density is low. Gallium arsenide has a suitable energy gap, but the carrier lifetimes in this material are too low; in addition it can show oscillations at high field strengths. Diamond was one of the first materials used in a solid-state detector, but apart from the prohibitive price of large crystals of this material, it has a number of other disadvantages including high trap density. Considerable effort is being made to find new materials which will be suitable for homogeneous detectors, but even if such materials are found, it is likely that there will be considerable difficulties attached to the fabrication of single crystals of the materials of the required uniformity.

**Flux measuring detectors.**—Integrating instruments do not provide a separate pulse as each particle strikes the detector, but are merely used to give an indication of the particle flux at the detector. In this type of instrument traps which lengthen the response time may not matter, since it is only necessary to measure the mean current passing through the detector.

Semiconductor flux detectors take the form of a crystal of the semiconductor material between two electrodes. As the radiation flux (often gamma) increases, the resistance of the crystal decreases. Cadmium sulphide is commonly used in flux detectors, but other group II-VI compounds can be used, such as cadmium selenide and telluride. Sometimes insulators (polythene, p.t.f.e. etc.) are used for dosimetry, since they have a density of approximately unity; however, they are not as sensitive as cadmium sulphide.

**Charge amplification.**—Cadmium sulphide and selenide are materials of large energy gaps and high trap densities. However, the traps may be used to obtain a charge amplification of perhaps 10,000. If ions are formed by a particle of nuclear radiation striking a cadmium sulphide crystal, the electrons are quickly swept to the anode, but many of the holes are trapped. If suitable electrodes are employed, the field due to the trapped holes will cause electrons to enter the crystal from the cathode. A small proportion of these electrons will neutralise trapped holes, but most of them will pass to the anode. Further electrons will be injected from the cathode until eventually all of the trapped holes will be neutralized.

If the time for an electron to pass across the crystal is  $t_p$  and  $\tau$  is the mean lifetime of an electron, the total charge which passes through the crystal per incident particle will be  $n\tau/t_p$  where  $n$  is the charge formed by an incident particle. The ratio  $\tau/t_p$  may be called the amplification of the device. A high gain will be obtained

if  $\tau$  is fairly large and if  $t_p$  is kept small by choosing a thin crystal with a high electron mobility. In practice the electron lifetimes are modified by crystal imperfections which act as electron traps. A high concentration of such traps will reduce the sensitivity and increase the response time. The crystals are fine needles about 1 cm long with indium electrodes attached to them. They are sealed in a glass tube. The most suitable crystals must be selected from a batch which have been grown from the vapour phase.

Cadmium sulphide and selenide detectors are available with sensitivities of 0.1 to 50  $\mu\text{A rad}^{-1}\text{hr}^{-1}$ ; generally the cadmium sulphide types are the more sensitive. A linear response over many orders of magnitude up to at least  $10^8 \text{ rad hr}^{-1}$  can be obtained. These detectors have the advantages that they are small and cheap (less than £5) and the associated instrumentation could hardly be simpler. It is only necessary to connect a cadmium sulphide detector in series with a moving coil microammeter and a battery to make an inexpensive portable  $\gamma$ -ray monitor. These detectors are not damaged by high radiation intensities.

One of the main disadvantages of the cadmium sulphide detector is the long response time for moderate radiation intensities ( $\sim 1$  sec.). When a cadmium sulphide detector is placed in a radiation field of moderate intensity, the current passing increases fairly slowly to a maximum value in a time which is of the same order as the lifetime of the trapped carriers. A similar slow decrease occurs when the detector is removed from the field. The response time is short at high intensities (where the traps are quickly filled), but it is generally so large at intensities of the order of the recommended human tolerance levels that it seems doubtful whether these detectors in their present form will be useful for health monitoring at low intensities.

The response time of a cadmium sulphide cell which has been kept away from radiation for some time is greater than that of a cell which has been irradiated during the previous few hours. In order to avoid this effect, some cadmium sulphide cells incorporate a radioisotope in the semiconductor material so that some of the deeper traps are kept filled. Such crystals pass a small current even in the absence of an external field and this current must be "backed off" in the instrument.

It has been found that cadmium sulphide detectors giving current gain can produce single pulses of several volts amplitude when they absorb  $\alpha$ -particles<sup>(2)</sup>. Although the energy resolution and maximum counting rate are very limited, such low cost  $\alpha$ -counting systems may be useful when a large number of the detectors are required.

## Junction detectors

In a p-n junction holes from the p-type semiconductor initially diffuse across the junction into the n-type and electrons from the n-type diffuse into the p-type. Equilibrium is established when the potential developed across the junction by this carrier diffusion prevents further diffusion from taking place. The junction potential repels free charges away from the junction. The junction region contains no free charge carriers and is therefore referred to as the depletion region. The application of a negative bias potential to the p-type material will increase the depth of the depletion layer (and hence decrease the junction capacitance) by drawing mobile charges further from the junction.

Although the number of free charge carriers in a homogeneous sample of silicon is too great for it to be employed as a solid-state ionisation chamber at room temperature,

silicon p-n junctions can be made in which the depletion region is used as the active part of a solid-state detector at room temperature.

Silicon junction detectors are the most commonly used form of semiconductor detector. The depth of the depletion layer is, however, severely limited and is dependent on the applied reverse bias potential. Germanium junction detectors must be cooled to liquid nitrogen temperatures.

**Depletion depth.**—The depth of the sensitive depletion region of a junction detector is controlled by the applied bias voltage; optimum bias voltages range from a few volts to over a kilovolt. The depletion depth,  $d$ , is given by the following approximate equations:—

$$d \approx 5 \sqrt{\rho V} \times 10^{-5} \text{ cm in n-type silicon}$$

$$\text{and } d \approx 3 \sqrt{\rho V} \times 10^{-5} \text{ cm in p-type silicon}$$

where  $\rho$  = specific resistance of the silicon used in ohm cm, and  $V$  = the applied bias voltage.

The depletion depth required to stop a charged particle depends on the type of particle and its energy. For example, a 5.5 MeV  $\alpha$ -particle requires a depletion depth of about 25  $\mu\text{m}$  in silicon for complete absorption, whereas a  $\beta$ -particle of about 56 keV or a proton of about 1.4 MeV will penetrate to a similar depth. A depth of about 0.2 mm of silicon is required to stop a 0.21 MeV electron or a 5 MeV proton; this depth can be obtained by the use of a n-type silicon of resistivity  $3.6 \times 10^3$  ohm cm at a bias of about 46V.

A germanium depletion region of a certain depth will stop particles of about twice the energy of those just absorbed by a silicon depletion region of the same depth.

The charge collection time,  $\tau$ , in a thick detector is given by the approximate equation<sup>(3)</sup>:—

$$\tau = \frac{W^2}{\mu V}$$

where  $W$  is the depletion depth of the detector,  $\mu$  the carrier mobility, and  $V$  the applied bias voltage. As  $\tau$  is proportional to  $W^2$ , it is desirable to keep  $W$  as small as possible consistent with the absorption of the particle. It is also desirable to make  $W$  only slightly greater than the particle range if there is an appreciable gamma background. On the other hand, it is desirable that  $W$  should be large for very high resolution spectroscopy, since the junction capacitance will then be small.

An excessive bias voltage will result in increased noise owing to the greater current flowing. At small bias voltages inefficient charge collection will also result in increased noise. An increase in the bias voltage will have the advantage that the charge carrier transit time will be reduced. The electric field strength at all points in the semiconductor material must be considerably less than that at which avalanche breakdown occurs in silicon (about  $6 \times 10^5 \text{ V cm}^{-1}$ ). A graphical method for determining the optimum detector operating conditions has been published<sup>(4)</sup>.

## Junction detector construction

*Silicon surface barrier junction detectors* are made from n-type silicon, a p-type layer being formed at one face by spontaneous oxidation. A gold film of about 20 to 50  $\mu\text{g cm}^{-2}$  is evaporated onto the oxidized face to form one electrode and an aluminium or magnesium alloy electrode is formed by evaporation on the back surface of the silicon. The depletion region extends from the



gold electrode inwards to a depth which depends on the applied bias, but which is normally less than 1 mm. This type of detector is fairly easy to make in the laboratory, but the percentage of really good detectors which will withstand a high bias and produce little noise is not usually very high.

*Silicon diffused junction detectors* are manufactured by allowing an element such as phosphorus or boron to diffuse into one side of a silicon slab (normally p-type) at a temperature of perhaps 900°C in an inert atmosphere. An aluminium film is simultaneously allowed to diffuse into the slab from the other side. One disadvantage of the diffused junction detector is that the high temperatures employed in its manufacture may lead to a reduction in the carrier lifetimes; surface barrier detectors are not raised above room temperature during manufacture and therefore do not suffer from this effect. Generally the diffused junction types are somewhat more robust and for this reason are likely to be more suitable for some purposes.

*Lithium-drifted junction detectors* can be made with depletion regions of 1 to 2 cm by employing a principle discovered by Pell<sup>(5)</sup>. Initially lithium is allowed to diffuse into one face of a silicon slab under very carefully controlled conditions. Lithium is a donor in silicon and the Li<sup>+</sup> ions rapidly diffuse into interstitial sites in the lattice. They are then caused to drift at a lower temperature under the influence of an electric field. This results in a deep depletion region being formed. The lithium ions tend to pair off with boron impurity atoms present in the silicon so that the specific resistance of the semiconductor material and hence the depletion depth is greatly increased. The amount of drifted lithium automatically adjusts itself to compensate for the presence of the acceptor ions to an accuracy of up to 0.001%. Lithium drifted germanium detectors can be made in a similar way.

Lithium-drifted silicon surface barrier detectors have been prepared with window thicknesses of less than 10<sup>-4</sup> cm and depletion depths of a few mm.

## JUNCTION DETECTOR APPLICATIONS

**α-counting and spectrometry.**—Silicon junction detectors are replacing scintillation counters for many α-monitoring purposes, especially where a probe of small size is required. The low background count of the semiconductor detector enables it to be employed to measure the activity of very weak α-sources; background counting rates of less than 0.15 counts per hour have been reported<sup>(6)</sup>.

Silicon surface barrier and diffused junction detectors are ideal for α-particle spectrometry. α-particles of normal energies are completely absorbed in the narrow depletion region. The thin window of the detector combined with the small amount of energy required to form an ion pair in silicon enables very high resolution to be obtained. It is necessary to place the specimen and the detector in a vacuum if the best possible energy resolution is required, since α-particles lose an appreciable part of their energy in air.

The high resolution offered by silicon junction detectors in α-spectrometry almost always enables the emitting radioisotope to be identified. Indeed, the element no. 103, lawrencium, was first identified in this way although only a few counts per hour could be recorded. The high energy resolution obtainable with a semiconductor α-spectrometer is well illustrated by the americium-241 spectrum shown in Fig. 2.

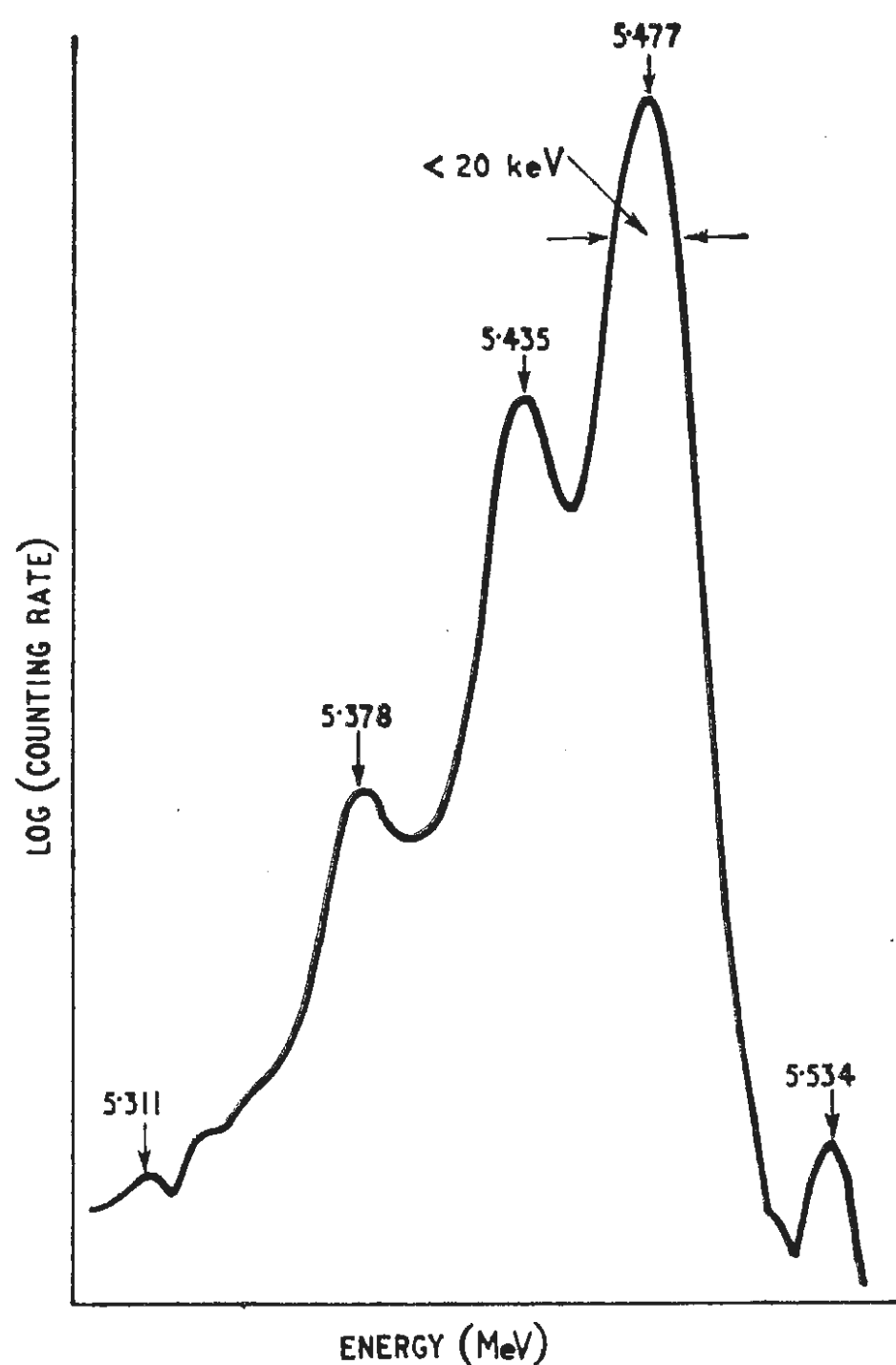


Fig. 2. The α-spectrum of americium 241. The excellent energy resolution is obtained by cooling a detector with a depletion depth of about 1mm.

If air containing α-emitting dust is drawn through a filter paper, the amount of each α-emitter present can be estimated from the energy spectrum of the material on the filter paper; when other types of detector are employed, it may be necessary to wait one or two days for the natural radioactive materials in the air to decay. An automatic α assay equipment which includes a 2 cm dia. solid-state detector has been designed for monitoring the activity of filter papers from the personal air samplers worn by people employed in active areas.

**β-counting and spectrometry.**—A junction detector can be used for β-counting if the depth of the depletion region is sufficient to absorb enough energy from each particle (10-15 keV) to produce a pulse which exceeds the level of the noise pulses. Semiconductor detectors are not very suitable for the counting of very low-energy β-radiation at room temperature. The small size of the detectors, however, renders them especially attractive for certain medical applications, especially in cancer work.

For β-spectrometry it is necessary that almost all of the particles shall be absorbed within the depletion region. High resistivity detectors should be employed at a fairly high applied bias for β-spectroscopy in order to obtain a suitable depletion depth. Lithium-drifted silicon detectors should normally be used for β-energies exceeding about 500 keV. They can be made with depletion regions deep enough to absorb β-particles with energies up to about 8 MeV and may be used at room temperature or, for better resolution, at liquid nitrogen temperature.

The detectors offer better resolution than scintillation β-detectors but have the disadvantage that they require a low-noise amplifier. Except at low energies a semiconductor detector is very suitable for use in magnetic

$\beta$  spectrometer instead of a Geiger-Müller or scintillation detector.

**$\gamma$ -counting and spectrometry.**—Solid state detectors are not efficient  $\gamma$ -detectors, since their volume is small and the atomic number of the semiconductor material is low. They are much more satisfactory for the counting of fairly low energy  $\gamma$ -rays or of X-rays than high energy  $\gamma$ -rays, since a much greater fraction of the former cause ionization in the crystal. Scintillation detectors employing a thallium-activated sodium iodide crystal are more efficient  $\gamma$ -ray detectors than any semiconductor device available at the present time, since the size of the crystal can be fairly large, its density is high and the iodine (of the sodium iodide) has a high atomic number.

Silicon junction detectors are available for the measurement of  $\gamma$ -radiation dose rate. They are small, rugged and stable devices, the typical sensitivity being  $10^6$  to  $10^8$  counts per rad. In medicine lithium-drifted silicon devices are used to measure the doses given in cobalt therapy. Owing to their low  $\gamma$ -efficiency, semiconductor detectors are more useful for measuring medium to moderately high levels of  $\gamma$ -radiation than very low levels.

For  $\gamma$ -spectroscopy lithium-drifted germanium devices offer resolutions exceeding those of other types of detector at energies greater than about 300 keV. At lower  $\gamma$ -ray energies the quartz crystal spectrometer offers greater resolution at smaller efficiencies. Lithium-drifted silicon detectors can be used for low-energy  $\gamma$ - and X-ray spectroscopy (preferably at liquid air temperatures), but germanium (atomic number 32) doped with gallium or zinc has a much greater photoelectric absorption coefficient than silicon (atomic number 14).

Lithium-drifted germanium detectors must not only be used at low temperatures, but they must also be stored at low temperatures. RCA state that their lithium-drifted germanium diodes should be stored at or below  $-20^\circ\text{C}$  and that storage at liquid nitrogen temperatures should prolong their life indefinitely. Storage at room temperature may cause failure within three months.

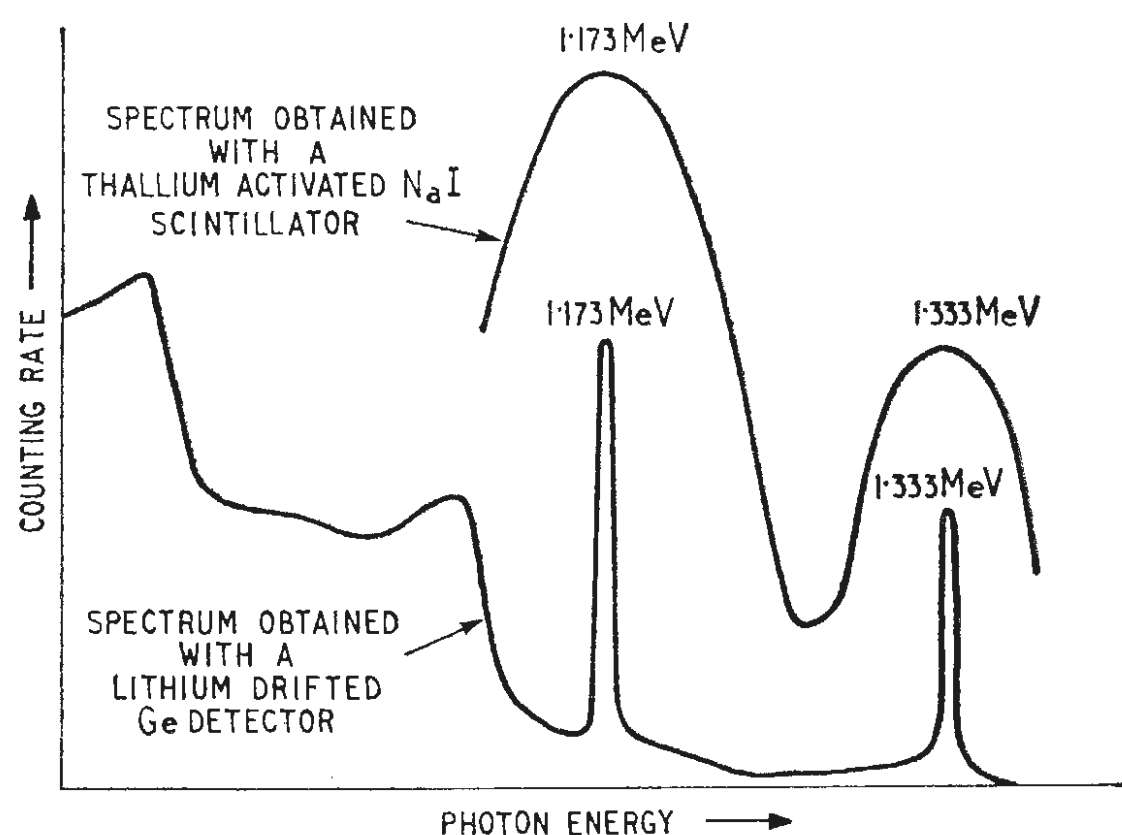


Fig. 3. Cobalt-60  $\gamma$ -spectra showing resolution of lithium-drifted Ge detector compared with that of a normal spectrometer.

Lithium ions are quite mobile in a germanium lattice at room temperature and the compensated depletion region will be partly lost after the device has been at normal temperatures for a few hours. This is almost unavoidable during shipment, but the compensated region can be regenerated by bolting the device to a heat sink and applying a reverse bias of about 150V in series with a  $1\text{ k}\Omega$

current-limiting resistor. The time for which this potential should be applied depends on the length of time for which the device has been at room temperature. After one week at room temperature the reverse current should be passed for about three hours. No reconditioning should be required for detectors which have been stored at temperatures below  $-40^\circ\text{C}$ .

Lithium-drifted germanium detectors offer very high  $\gamma$ -resolution, since the formation of an ion pair in this material requires an energy absorption of only 2.8 eV and the atomic number is great enough for the probability of absorption by the photoelectric effect to be appreciable. The resolution can be better than 10 keV at energies of up to about 6 MeV. The high resolution of the detector for the two  $\gamma$ -ray energies of cobalt-60 is shown in Fig. 3, together with the type of spectrum obtained from a typical scintillation spectrometer employing a thallium-activated sodium iodide crystal.

**Neutron detection.**—When neutrons pass through matter they produce very few ions, since with no charge and a high mass they do not react with electrons appreciably. Neutrons are detected by allowing them to react with certain nuclei so that ionising radiation is formed which can then be detected in the usual way.

Fast neutrons are often detected by allowing them to strike protons in a hydrogenous material. The recoiling protons are detected by the ionization they produce. Both thermal and fast neutrons can be detected by allowing them to interact with the nuclei of boron-10, when  $\alpha$ -particles are produced, or with lithium-6, when protons are formed. Ionizing particles are also formed when uranium undergoes neutron-initiated fission.

Semiconductor detectors can easily be converted into neutron detectors by placing a thin plastic cap (which contains many hydrogen atoms) or a thin neutron conversion foil containing one of the elements mentioned in the previous paragraph in front of the windows of the detector.

Neutron spectrometers can be made by placing two matched semiconductor detectors on each side of a neutron conversion foil. The total energy of the particles formed when a neutron reacts with the foil is absorbed by the detectors and the incident neutron energy may be calculated from the output pulse size.

**Other particles.**—Semiconductor detectors can be employed for counting other types of ionizing particles such as protons, deuterons, tritons, fission fragments, etc. If suitable depletion depths are used, the energy spectrum of the particles may be obtained. Generally a lithium-drifted device should be used if a depletion depth exceeding 0.6 mm is required.

## SPECIAL TYPES OF DETECTOR

Special types of semiconductor detector are available, but they will not be discussed in detail, since they are likely to be of interest only to the specialist. A fully depleted transmission detector may be used to measure the energy lost by a particle per cm of its path and in combination with a thicker detector provides information which often enables an unknown particle to be identified. Special types of detector are available for work on the polarization (spin) of particles formed in nuclear reactions. Another special detector, the "nuclear triode" provides two coincident output pulses which provide information on the energy of the particle and its position from one end of the detector.

Detectors can be designed which provide internal am-



plification by transistor action<sup>(8)</sup>, but unfortunately this does not yield an improved signal to noise ratio. If a detector could be designed which would give an amplification similar to the gas amplification of a proportional counter, it would almost certainly have a bright future.

A phosphor has been used in contact with a photodiode<sup>(9)</sup>. Although this system is much smaller than the conventional scintillation counter, the energy resolution is inferior owing to the noise produced by the photodiode. Nevertheless, the energy required to produce an ion pair is about 70 eV which is less than required for a conventional scintillation counter.

### RADIATION DAMAGE

Gas-filled detectors are not permanently damaged by very high radiation levels, but the atoms of semiconductor detectors can be displaced in the lattice by the energy of the radiation and this results in the so-called Frenkel defects<sup>(10)</sup>. The effect of impurity atoms created under neutron bombardment may also affect the detector properties. Lithium-drifted devices are about one hundred times more sensitive to radiation damage than other types of junction detector. The latter are likely to be affected by about  $10^{10}$   $\alpha$ -particles per  $\text{cm}^2$ ,  $10^{15}$   $\beta$ -particles per  $\text{cm}^2$ ,  $10^{12}$  fast neutrons per  $\text{cm}^2$  or  $10^8$  rad of  $\gamma$ -radiation. This limits the application of junction detectors in reactor instrumentation and in the van Allen belts. However, the amount of radiation damage to a semiconductor detector may be estimated from the electrical properties of the device and used as a measure of the integrated radiation dose received.

### INSTRUMENTATION

Although a particle of ionizing radiation will produce more ions in a semiconductor material than in a gas filled detector, semiconductor counters lack the gas amplification which occurs in proportional and Geiger-Müller detectors. The output pulses from semiconductor detectors are therefore relatively small and low-noise pre-amplifiers are required.

Let one ion pair be formed in a semiconductor material for each  $w$  electron volts of energy absorbed. The charge of an electron is about  $1.6 \times 10^{-19}$  coulomb and therefore the charge collected at each electrode of a detector (assuming no losses) when  $E$  MeV of energy are absorbed will be:—

$$Q = \frac{10^6 E}{w} \times 1.6 \times 10^{-19} = \frac{1.6 E}{w} \times 10^{-13} \text{ coulomb} \dots (1)$$

The change in the voltage across the detector,  $\delta V$ , will therefore be given by the equation:—

$$\delta V = \frac{Q}{C} = \frac{1.6 E}{w C} \times 10^{-13} \text{ V} \dots (2)$$

where  $C$  is the capacitance of the detector plus stray capacitance. For silicon  $w=3.5$  eV and, if  $C$  is 50pF,  $V$  can be calculated from (2) to be 0.9 mV when a particle of 1 MeV energy is completely absorbed in the depletion region. The pulse rise time can be as small as 10 ns but when the detector is connected to its pre-amplifier, stray capacitance is likely to increase the pulse rise time to about 100 ns. A normal low-noise amplifier of the type used for proportional counting with a gain of 80 to 90 dB may be employed for simple counting.

It can be seen from (2) that the amplitude of the voltage pulse produced by a semiconductor detector is dependent on the capacitance of the device and on the associated stray capacitance. Changes in capacitance will occur

when the voltage across the detector is altered to change the depletion depth, when this voltage drifts slightly or when a change in the cathode temperature of the first valve of the pre-amplifier causes an alteration of the space charge in the valve. Any of these changes will cause a semiconductor particle energy spectrometer to drift during operation if the output voltage from the device is amplified in the normal way.

Equation (1) shows that the charge collected at the electrodes of a semiconductor detector is independent of the capacity of the device. The difficulty mentioned in the previous paragraph can therefore be avoided if a charge-sensitive pre-amplifier is used which produces an output voltage pulse of an amplitude proportional to the charge fed to the input of the amplifier.

The basic circuit of a charge-sensitive pre-amplifier is shown in Fig. 4. Capacitive feedback occurs *via*  $C_f$  and the effective input capacitance therefore becomes  $C_f(1 + A)$  where  $A$  is the loop gain of the system (com-

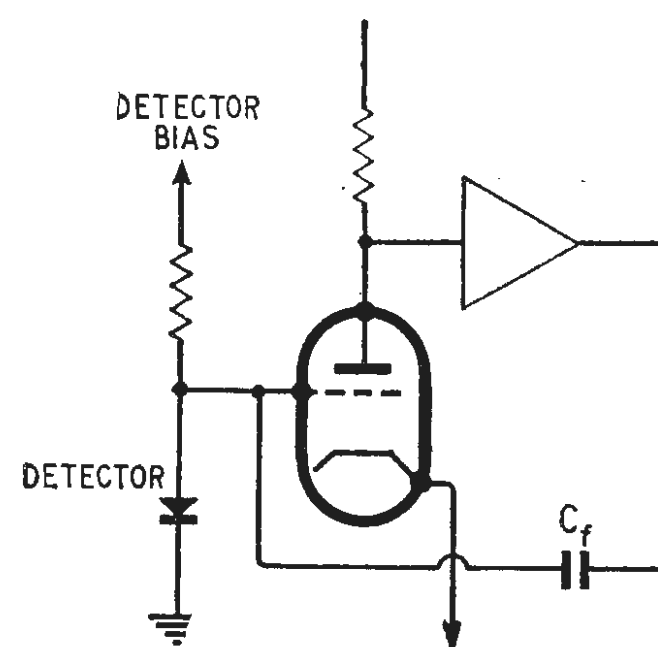


Fig. 4. Basic arrangement of a charge-sensitive pre-amplifier.

pare with the Miller effect in a valve). If  $A$  is very large, the output voltage,  $V_o$ , is given by the equation:—

$$V_o = \frac{Q}{C_f}$$

Thus the output voltage is independent of the diode and stray input capacitance. The large effective input capacity produced by the feedback renders any change in the diode or stray input capacitance negligible.

Apart from the elimination of drift, the use of a charge-sensitive pre-amplifier for energy spectroscopy enables the effect of variations of the detector bias on the spectrum to be observed without taking into account the change in the detector capacitance. The use of a charge-sensitive preamplifier results in the same signal to noise ratio that would be obtained with a similar voltage-sensitive amplifier. The feedback capacitor,  $C_f$ , has a typical value of 5 pF, in which case the output voltage will be about 9 mV per MeV, of absorbed energy.

The complete circuit of an Elliott charge-sensitive pre-amplifier is shown in Fig. 5. A cascode input stage is employed to minimize noise while providing a high gain. The input stage is completely screened and this helps to ensure that feedback occurs only *via*  $C_f$ . If square waves of voltage  $V$  are injected into the test pulse input, charges of  $V/C_s$  (where  $C_s$  is the 2.5 pF series capacitor shown) will be injected into the first stage of the amplifier and will produce a peak in the spectrum which is useful for checking the calibration and resolution.

Other designs for charge-sensitive valve pre-amplifiers can be found in ref. 12. Valve amplifiers provide a lower noise than transistor amplifiers<sup>(13)</sup> if the detector capacitance is less than about 500 pF, since the grid current

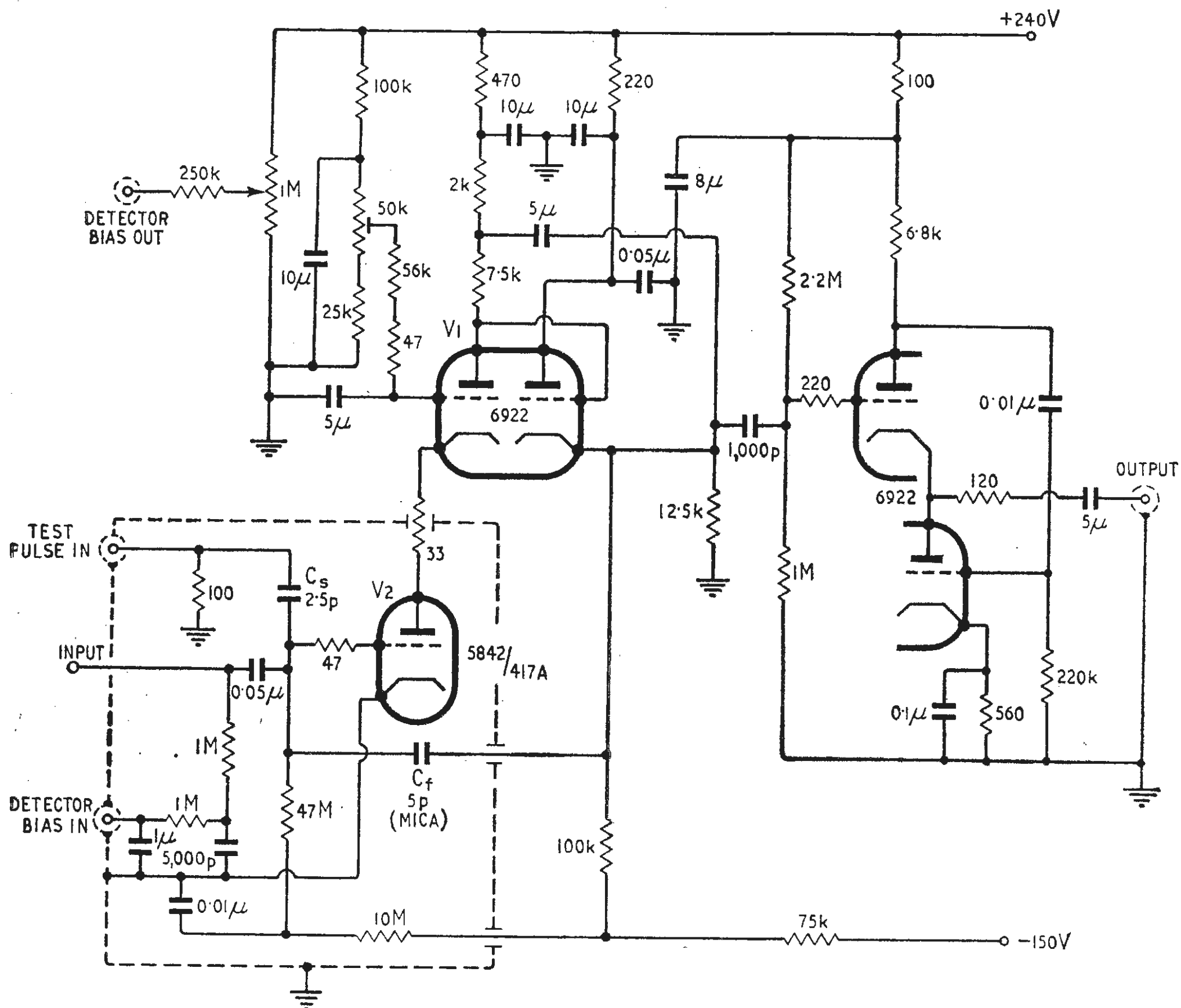


Fig. 5. A charge sensitive pre-amplifier.

of most valves is less than the base current of most transistors.

Due to the large effective input capacitance of charge-sensitive pre-amplifiers they are unsuitable for fast counting, particularly in coincidence work.

### Conclusion

Semiconductor detectors have been widely used in nuclear physics laboratories, but are now commonly used elsewhere when small, lightweight and rugged detectors are required which provide a low background counting rate. They can be used for the high resolution spectroscopy of particles which do not have very low absorption coefficients in semiconductors, although they must be cooled for the best results. It seems unlikely that they will completely replace the normal Geiger-Müller tube for simple radiochemical work since they require more complicated instrumentation, and most semiconductor junction detectors are at present more expensive than common Geiger-Müller tubes.

It has only been possible to discuss some of the major points of interest in this survey of semiconductor detectors. Readers requiring further information are referred to ref. 2. Commercially available equipment is surveyed in ref. 13.

**Acknowledgements**—The writer is indebted to Elliott Bros. Ltd., Mullard Ltd., R.C.A. (Gt. Britain) Ltd., Simtec Ltd. of Canada, 20th Century Electronics Ltd., and to the librarians of A.E.R.E., Harwell for information they have kindly provided.

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# NEWS FROM INDUSTRY

## Anglo-French Collaboration

WHETHER the Concorde supersonic airliner gets off the ground or not one thing is certain, the collaboration in technical know-how since its inception has improved the bonds between the British and French industrialists, especially in the electronics field. In past months several Anglo-French links have been announced and in recent weeks two more have come to light.

### Aircraft Navigational Equipment.—

Ferranti Ltd. and SAGEM (Societe d'Applications Generales d'Electricite et de Mecanique), of Paris, have entered into an agreement whereby the two companies will pool their knowledge and experience in the design and development of aircraft navigation equipment. This agreement has already borne fruit in the award of a contract to Ferranti for an attitude reference system and ground test equipment for the European Satellite Launch Vehicle (Eldo). The gyroscopes and accelerometers for the system will be made by SAGEM. In addition, Sud Aviation (joint constructor with the British Aircraft Corporation of the Concorde), have decided to equip the Concorde with an inertial navigation system developed and manufactured jointly by SAGEM and Ferranti.

**Computers.** — The two British giants English-Electric-Leo-Marconi Computers and International Computers & Tabulators have put forward a proposal for a joint Anglo-French project for a large computer to the Minister of Technology, Mr. Frank Cousins. A proposal for an identical project has been submitted to the French Government by CITEC (Compagnie pour l'Informatique et les Techniques Electroniques de Contrôle). CITEC is a jointly owned subsidiary company of C.S.F. (Compagnie Generale de Telegraphie sans Fil) and C.G.E. (Compagnie Generale d'Electricite). It was formed last year to develop and produce industrial, scientific and military computers.

The companies concerned have made it clear that without Government support, the proposals will never see the light of day.

Another plan under discussion is the formation of a European consortium including I.C.T. and E.E.L.M. from Britain, CITEC from France, Telefunken from Germany and Ericsson from Sweden.

**Plessey Automation Group.**—Following the major reorganization of Plessey, which came into effect on 1st July this year, the company's automation group is to be located at Poole in Dorset. The automation group will eventually comprise four divisions covering the principal activities of data handling, data

processing, traffic management and automation accessories. Mr. H. E. C. Nash who joined Plessey as a consultant last January from Elliott-Automation is the group's director.

**Bristol to Exeter Microwave Phone Link.**—Standard Telephones and Cables Ltd. have received a contract from the Post Office for an extension to the London-West Country radio network being installed by them. The links between London and Bristol and between Bristol and Cardiff are under construction and next year work will begin on the Bristol-Plymouth-Goonhilly leg, of which the new Bristol-Exeter project forms a part. Two r.f. channels will be used (using the aerials already planned) for the extension.

**Microwave Associates Ltd.**, of Luton, have received a contract from the B.B.C. that calls for portable solid state television link equipment operating in the 7 Gc/s band. This equipment is to be used by the B.B.C. for outside broadcast purposes. Either monochrome or colour signals can be transmitted. Microwave Associates have also received contracts from the B.B.C. for point-to-point links and for special ultra light-weight battery operated survey and path test equipment.

**Cossor Electronics Ltd.** have formed a marine division to market the wide range of marine products manufactured within the Raytheon organization, of which Cossor is a subsidiary. From 1st October, the new division will operate from Shelley House, Noble Street, London, E.C.2. Included in the present range of products are Cossor v.h.f. transceivers, Raytheon 3 and 10 cm radars and Loran navigational equipment. Mr. S. D. Coode-Bate is divisional manager.

**H.C.D. Research Ltd.** established four years ago to make precision crystal oscillators, frequency standards and associated equipment, recently formed a subsidiary company to handle their growing semiconductor business. The new company, called Semikron Rectifiers and Electronics Ltd., operates from the parent's headquarters at 77 Gloucester Road, Croydon, Surrey (Tel.: THORnton Heath 7485). Last month we made reference to the new company Semikron, but inadvertently transposed the names of the parent and subsidiary. We apologise for any misunderstanding that may have arisen.

**Abbey Electronics and Automation Ltd.**, have, through the acquisition of a new 5,000 sq ft factory, doubled the size of their manufacturing premises at Delamare Road, Cheshunt, Herts. (Tel.: Waltham Cross 25106.)

**English Electric's** £200,000 computer centre at Huyton, Lancs., was formally opened on 16th July by the Prime Minister, the Rt. Hon. Harold Wilson.

**Mullard Applications.**—The applications staff of the Mullard Research Laboratories, Redhill, Surrey, have been moved to the company's Central Application Laboratory, New Road, Mitcham, Surrey. (Tel.: Mitcham 3471, Telex 23709.)

**Plessey Radar Ltd.** are supplying, under a contract worth £40,000, three air traffic control radar installations to the Bulgarian Government. They will be located at Sofia, Varna and Burgas and will provide air surveillance for civil aviation over Bulgaria.

**Tektronix U.K. Ltd.** have, since the 1st July this year, been operating a repair centre for the maintenance and recalibration of their oscilloscopes and ancillary instruments. Information on this service can be obtained from the field support department, Beaverton House, Harpenden, Herts. (Tel.: Harpenden 61251, Telex 25559.)

**The British Radio Corporation**, who now market HMV, Marconiphone and Ultra radio and television sets, are moving to 284 Southbury Road, Enfield, Middx. (Tel.: HOWard 2477.) Ultra's former premises at Eastcote, Middx., and the headquarters of the sales division of His Master's Voice and Marconiphone at Cavendish Place, London, W.1, are being vacated.

**Texas Instruments** have acquired a 6,000 sq ft warehouse and office site at 12 Wellcroft Road, Slough, Bucks. (Tel.: Slough 28578, Telex 84363.) From this address the company's supplies division will operate a same-day service for the supply of small orders for T.I. devices.

**C. & N. (Electrical) Ltd.**, of The Green, Gosport, Hants., offer industry and research an enquiry service in the field of sequential control, data processing and logic circuitry. (Tel.: Gosport 80221, Telex 8621.)

**Control Logic** of Boston, U.S.A., who manufacture a wide range of digital logic circuit modules, are to have their products marketed in the United Kingdom and Western Europe by Electro Mechanisms Ltd., of 218-221 Bedford Avenue, Slough, Bucks. (Tel.: Slough 27242.)

**Mial S.P.A.**, of Milan, manufacturers of capacitors, have appointed Waycom Ltd., of Capacity House, Rothsay Street, Tower Bridge Road, London, S.E.1, (Tel.: HOP 2615) sole U.K. distributors.

**U.K. Solenoid Ltd.**—Since the formation of Chilton-Solenoid (U.K.) Ltd. three years ago, there has been some confusion owing to the similarity in name with Chilton Electric Products Ltd., both of Hungerford, Berks. In future, the former company is to trade under the name U.K. Solenoid Ltd.

**Pye H.D.T. Ltd.**—To form one body within the Pye organization to look after their closed circuit television interests, the industrial division of Pye Telecommunications Ltd. has been combined with the original Pye H.D.T. Company. The initials stand for High Definition Television.

# Experimental Thyristor Control Circuits

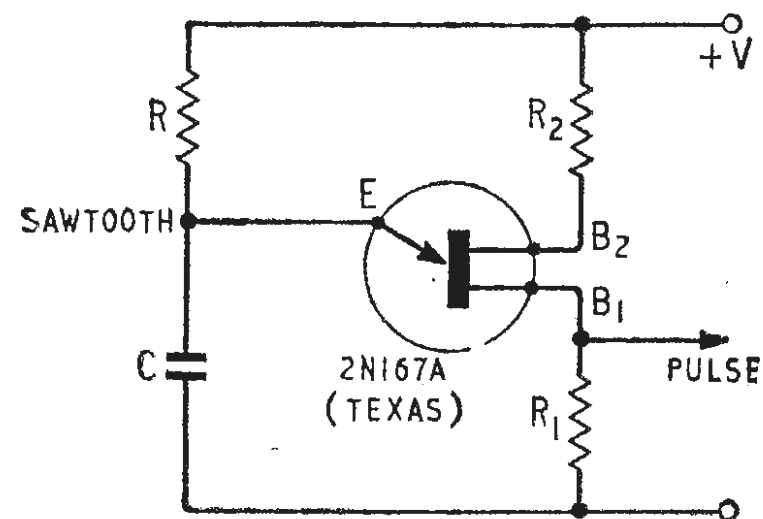
By N. M. MORRIS,\* B.Sc., A.M.I.E.E., A.M.I.E.R.E.

Conclusion of a two-part article presenting a range of thyristor control circuits for use by students and experimenters. The article starts with pulse circuits using unijunction transistors and Shockley diodes then goes on to applications of the control circuits in closed-loop regulators.

## UNIUNCTION TRANSISTOR

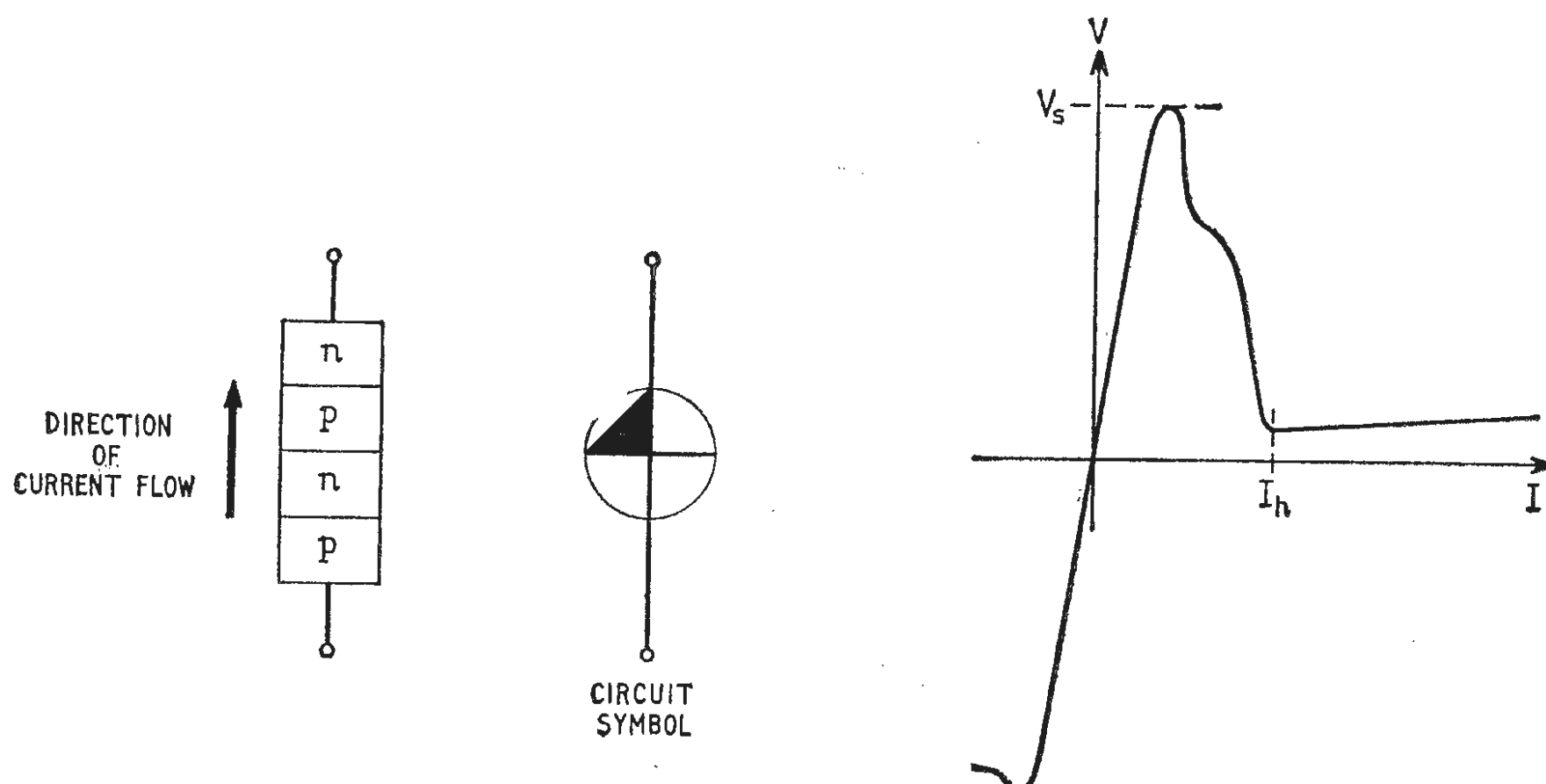
THE unijunction transistor is a convenient device for pulse generation in thyristor circuits. The device comprises a bar of n-type material with two ohmic contacts and one p-n junction. The two ohmic contacts are known as base-one ( $B_1$ ) and base-two ( $B_2$ ) respectively and the p-type material is known as the emitter (E). The circuit employed to produce pulses is shown. While the p-n junction is reverse-biased the voltage across the capacitor rises exponentially, giving a sawtooth waveform at the emitter. When the capacitor voltage reaches a value known as the peak-point voltage, the p-n junction becomes forward-biased and the capacitor discharges through  $R_1$ . This  $R_1$  has a low value, resulting in a pulse output; after the capacitor has discharged the p-n junction returns to a blocking state and it is again possible to charge the capacitor. A pulse of 10 to 20 microseconds duration at an amplitude of about 5 volts is produced and the pulse repetition rate is about  $0.8 RC$  seconds. \*The actual values depend on the unijunction transistor and components used. Typical values with a 2N1671A (Texas Instruments) unijunction transistor are:  $V_s$ , 22 volts;  $C$ ,  $0.1 \mu F$ ;  $R$ , 10 to 100 k $\Omega$ ;  $R_1$ , 22  $\Omega$ ;  $R_2$ , 100  $\Omega$  (required to give temperature stability).

\*North Staffordshire College of Technology.



The pulse repetition rate is controlled by the methods outlined for the two-transistor pulse generator circuit above, i.e. by shunt or series control of capacitor charging current. Small modifications to the values of circuit components are necessary, but the principle is unchanged. The output pulse may be connected directly to the gate of the thyristor or through an RC network as shown above. The unijunction circuit may be used directly to replace the two-transistor pulse generator section of the pre-amplifier described last month, p. 399, by connecting the unijunction emitter to the point marked A.

## FOUR-LAYER (SHOCKLEY) DIODES



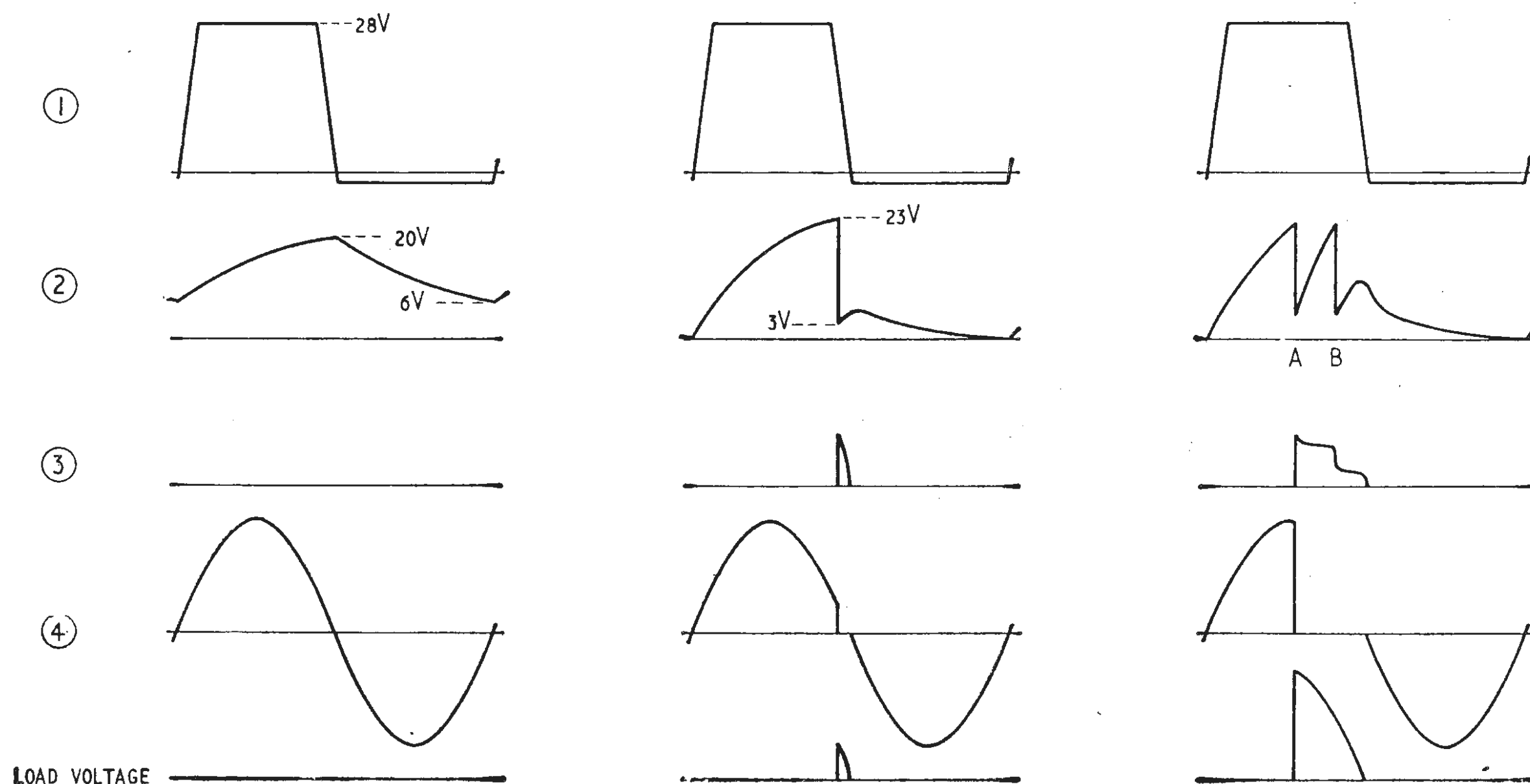
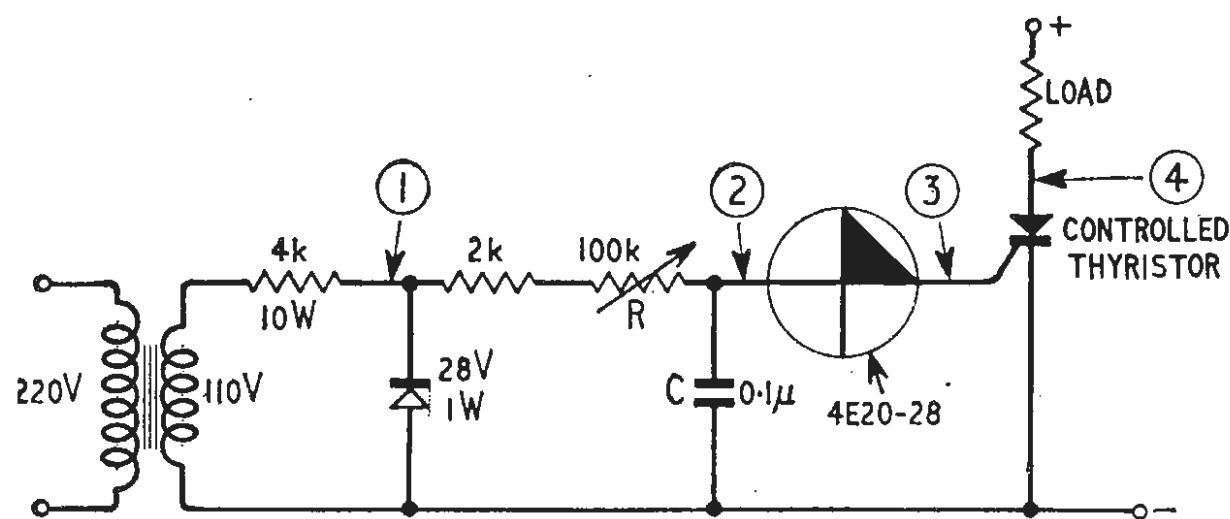
THE Shockley diode is a p-n-p-n device which is triggered from a forward blocking state to a conducting condition when the voltage across it exceeds the switching voltage, shown here as  $V_s$  ( $I_h$  is holding current). The current at the switching voltage is typically a few hundred microamperes. In the conducting state the dynamic resistance is a few ohms and the device can deliver a peak current of the order of one ampere for about ten microseconds.



## GATE CONTROL CIRCUIT USING A SHOCKLEY DIODE

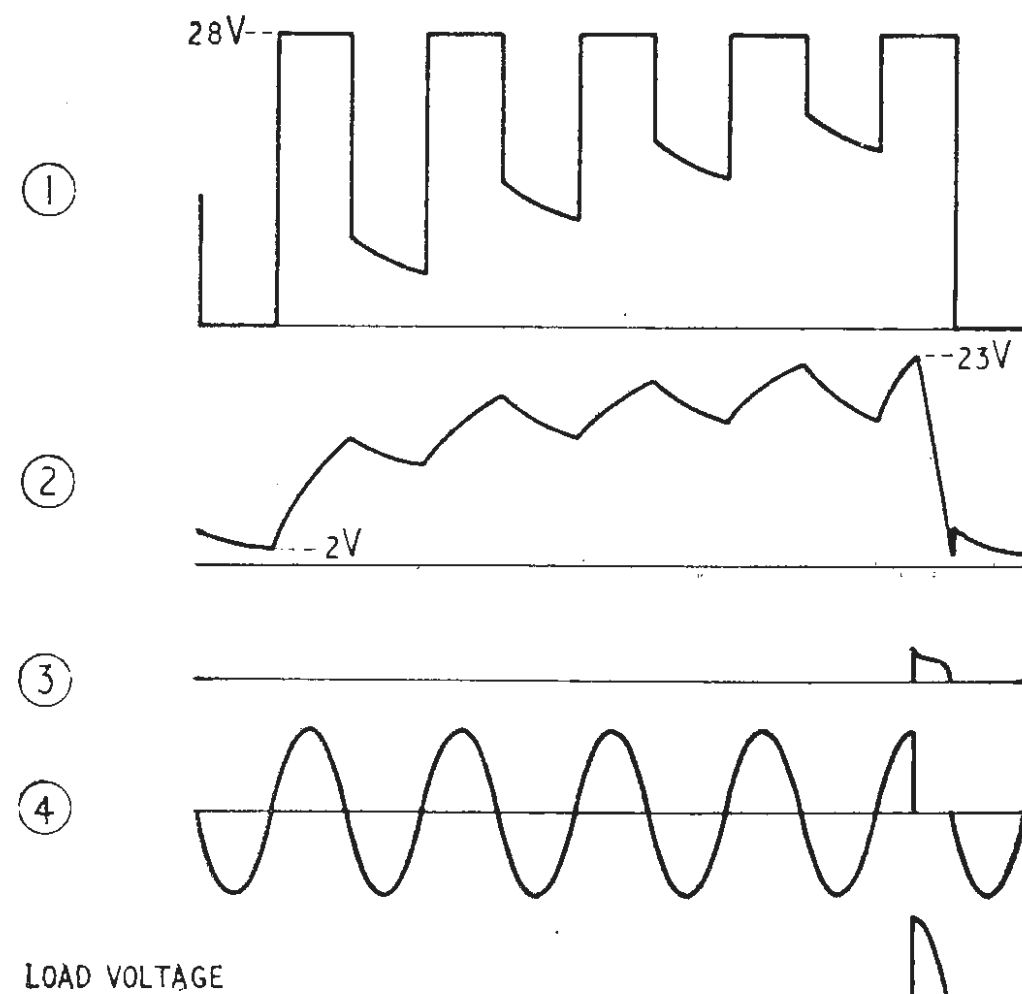
THE gate control circuit shown here is fed from a Zener diode limiting circuit providing a clipped positive voltage of 28 V, which is in excess of diode switching voltage. A suitable diode is the Brush-Clevite Type 4E20-28. The negative voltage applied to the circuit is limited to about  $1\frac{1}{2}$  V. If the charging time-constant RC is very

large, the peak voltage across the capacitor in the positive half-cycle may not be sufficient to break down the diode. Relevant voltage waveform for one such value of RC is shown on the left-hand column of waveform diagrams. Reduction of R to about  $70\text{ k}\Omega$  results in stable firing in the last  $10^\circ$  of each positive half-cycle; waveforms for this condition are shown in the middle column. Further reduction in R results in earlier firing at A (righthand column) giving an increased voltage across the load. At this point the capacitor voltage suddenly falls to a value which cannot sustain the diode holding current and the device reverts to a blocking state. This allows the capacitor voltage to build up again in the positive half-cycle, switching the diode on again at B. By adjustment of R it is possible to control the thyristor conduction over practically the whole of the positive half-cycle.

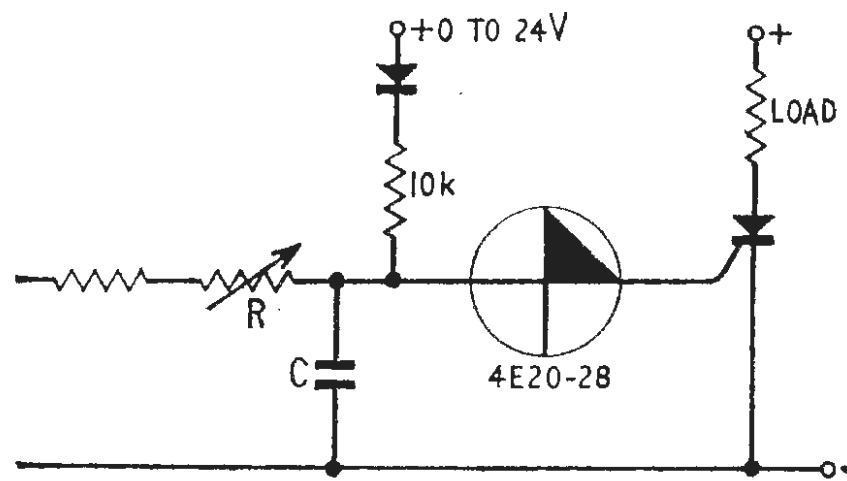


## TIME-DELAYED FIRING USING A SHOCKLEY DIODE

THE introduction of a diode between the transformer and the  $4\text{ k}\Omega$  resistor in the previous gate control circuit allows firing to be delayed. Without the diode in circuit the capacitor can discharge through R and the Zener diode in the negative half-cycle of the supply voltage. With the diode in circuit the leakage resistance is very high and the voltage across the capacitor is retained. If the charging time-constant is large, the thyristor is not switched on in the first positive half-cycle and the potential across the capacitor stays substantially at this value during the negative half-cycle. In succeeding half-cycles the capacitor voltage is "pumped up" until it reaches the switching voltage of the Shockley diode, when the capacitor is discharged and the thyristor is turned on. Reduction of R reduces the time taken to reach the switching voltage, the maximum value of R being set by the condition that the charge and discharge time constants are nearly the same. Waveforms for this mode of operation are shown here.



## CONTROL OF SHOCKLEY CIRCUIT USING A VOLTAGE INPUT

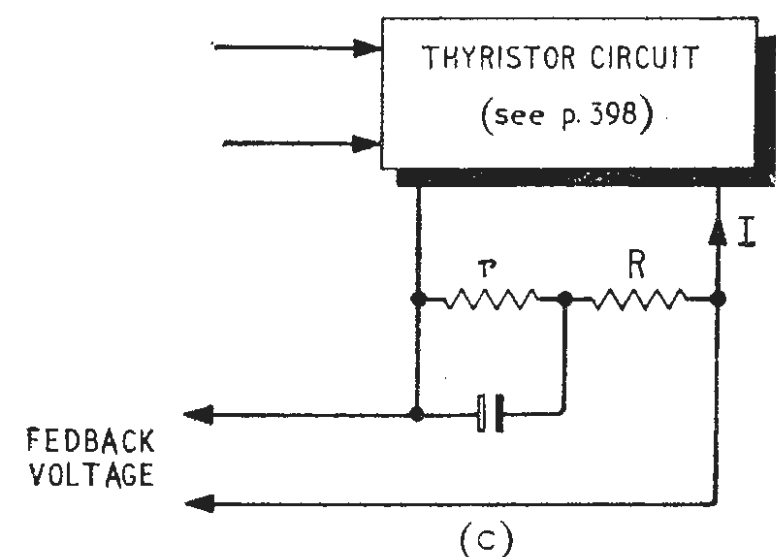
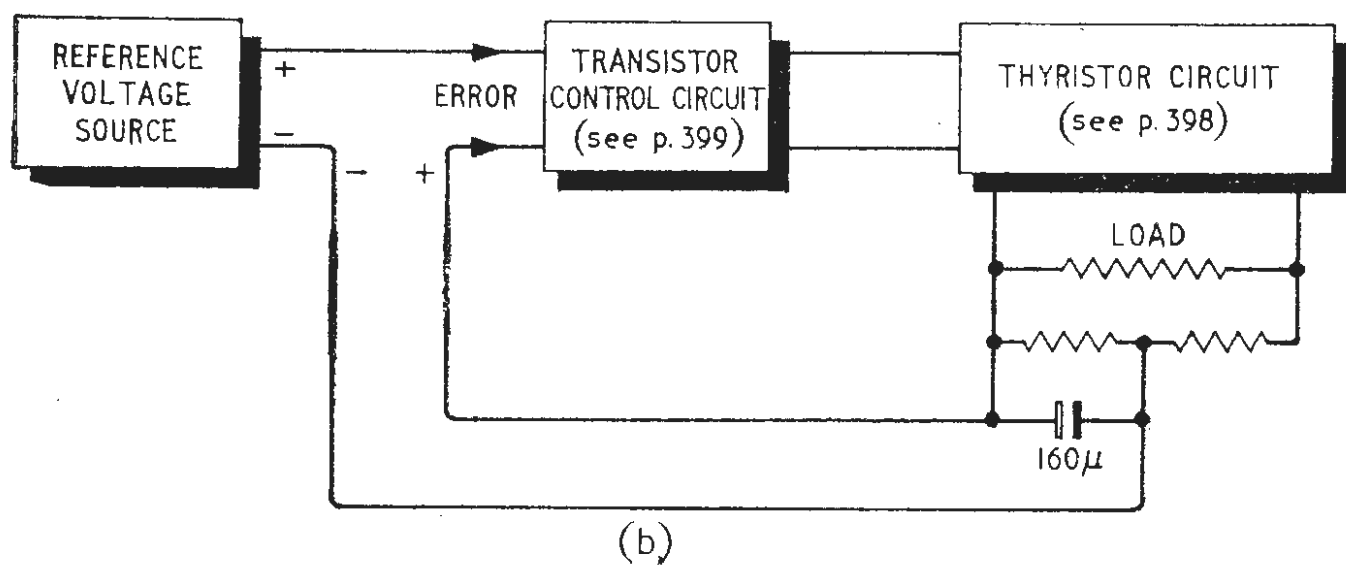
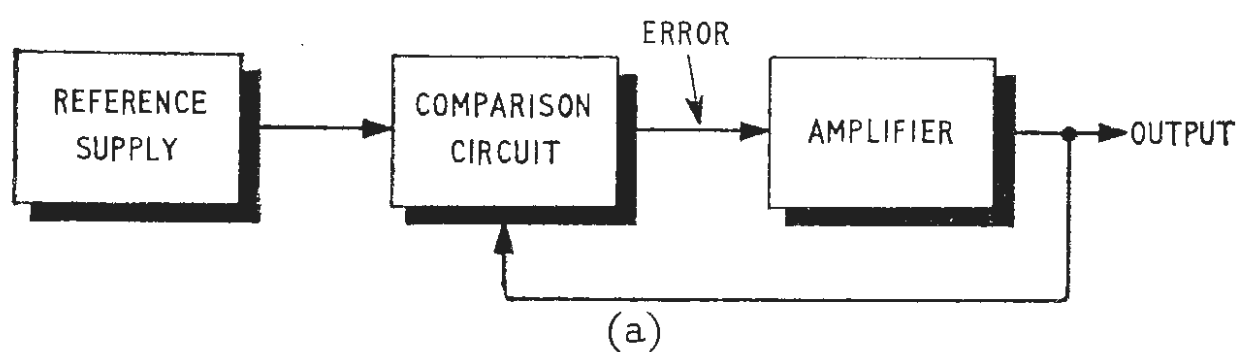


IF the gate control circuit is modified as shown here, the additional potential allows the Shockley diode switching voltage to be reached earlier. Time delayed firing again is obtained by the insertion of a diode in the 110-V supply. Variable resistor  $R$  is adjusted to the point where the thyristor just fires. Increasing the externally applied voltage from 0 to 20 V gives full control of firing pulses over the whole positive half-cycle. The external control voltage can conveniently be obtained from the d.c. amplifier given last month (bottom of p. 399).

## APPLICATION TO CLOSED-LOOP REGULATORS

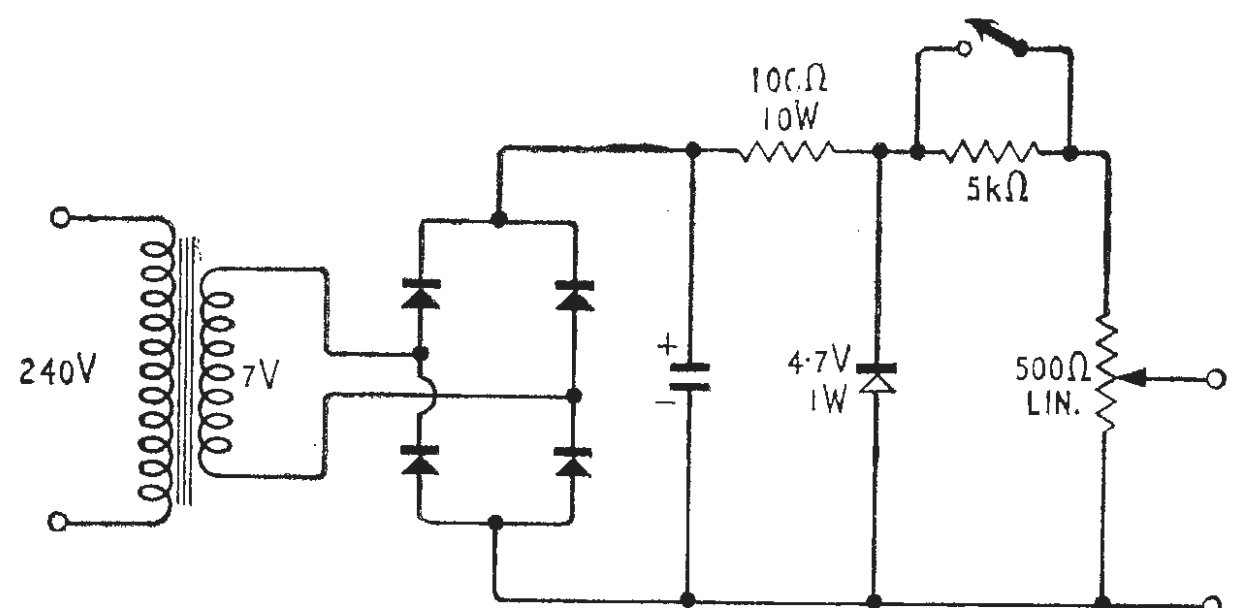
THE basic requirements of a closed-loop regulating system are shown at (a). The output, or a signal proportional to it, is compared with a reference voltage and the difference between the two (the error) is amplified to give the output. The higher the gain the lower the error, the limit of gain being set by overall stability, which is dictated by the time lags present in the regulator. A simple voltage regulator is shown at (b). The reference

voltage circuit is given next in this article; the transistor control circuit given on p. 399 last month (pre-amplifier); and the thyristor circuit was given on p. 398 last month ("Full wave power control"). The only time lag of any significance in the system is the RC smoothing network in the voltage signal feedback path. Since there is only one lag involved, the regulator is inherently stable and the amplifier gain may be increased to its maximum value. By feeding back the voltage developed across a low resistor  $r$ , as shown in (c), the current in the load resistor  $R$  can be maintained constant. For accurate control  $r$  should be as small as possible, consistent with the fact that the potential developed across it should be much greater than the allowable error.



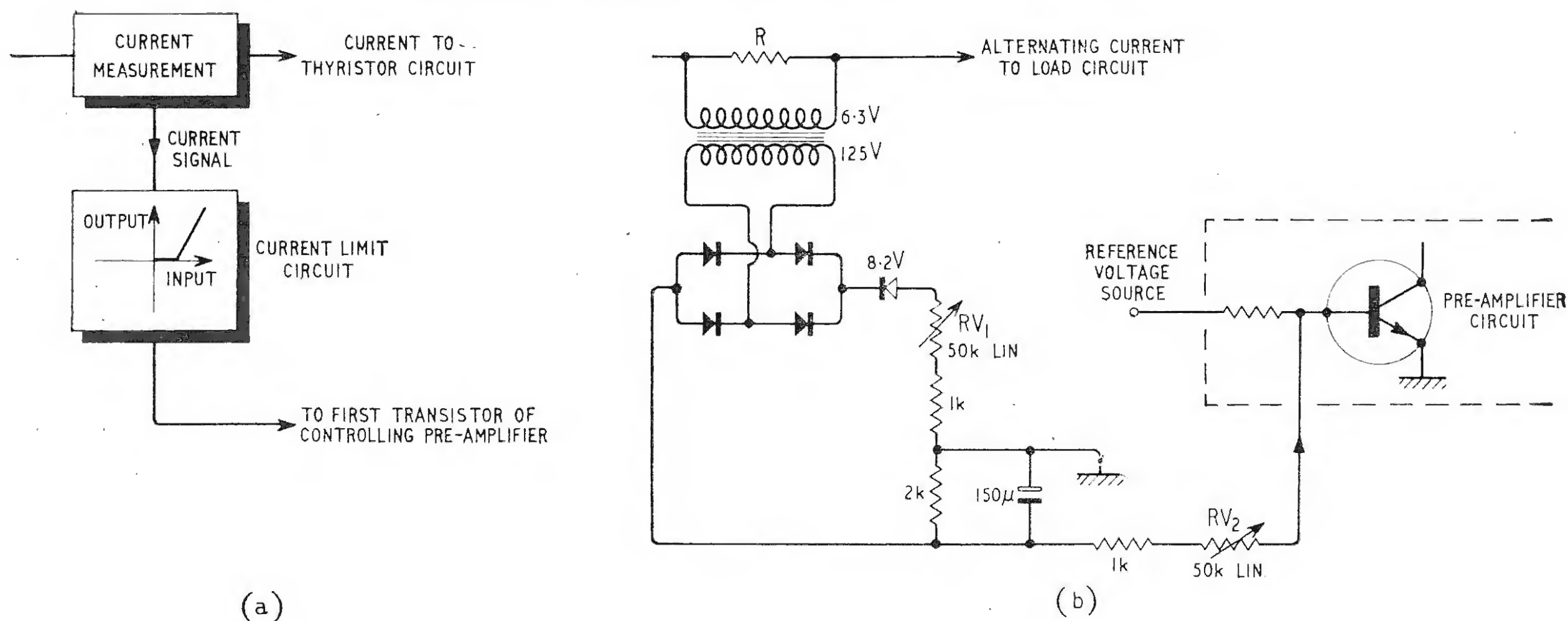
## REFERENCE VOLTAGE SOURCE

THE reference voltage source in a closed-loop control system can conveniently be obtained from a single-phase, full-wave rectifier with capacitor smoothing, followed by a Zener diode to stabilize the voltage across the reference potentiometer. If the output of the accompanying circuit is connected directly to the input of the pre-amplifier above the 5 k $\Omega$  resistor must be connected into the circuit to limit the maximum excursion of the reference voltage. When it is used in a feedback regulator circuit to be described later the 5 k $\Omega$  resistor is short-circuited.





## CURRENT LIMITATION IN THYRISTOR CIRCUITS



IN order to keep the average dissipation in the thyristor within specified values, even in experimental circuits, it is desirable to provide some method of current limitation. The basic principles are shown here at (a). The current is measured and a signal proportional to it is fed into a circuit which gives zero output for a given range of input signals; beyond this point the output increases with input. The knee of the characteristic is arranged to coincide with the current limit setting. The output of this circuit is applied as negative feedback to input of the controlling pre-amplifier (p. 399 last month), so reducing the overall gain of the regulator. This has the effect of reducing the pulse

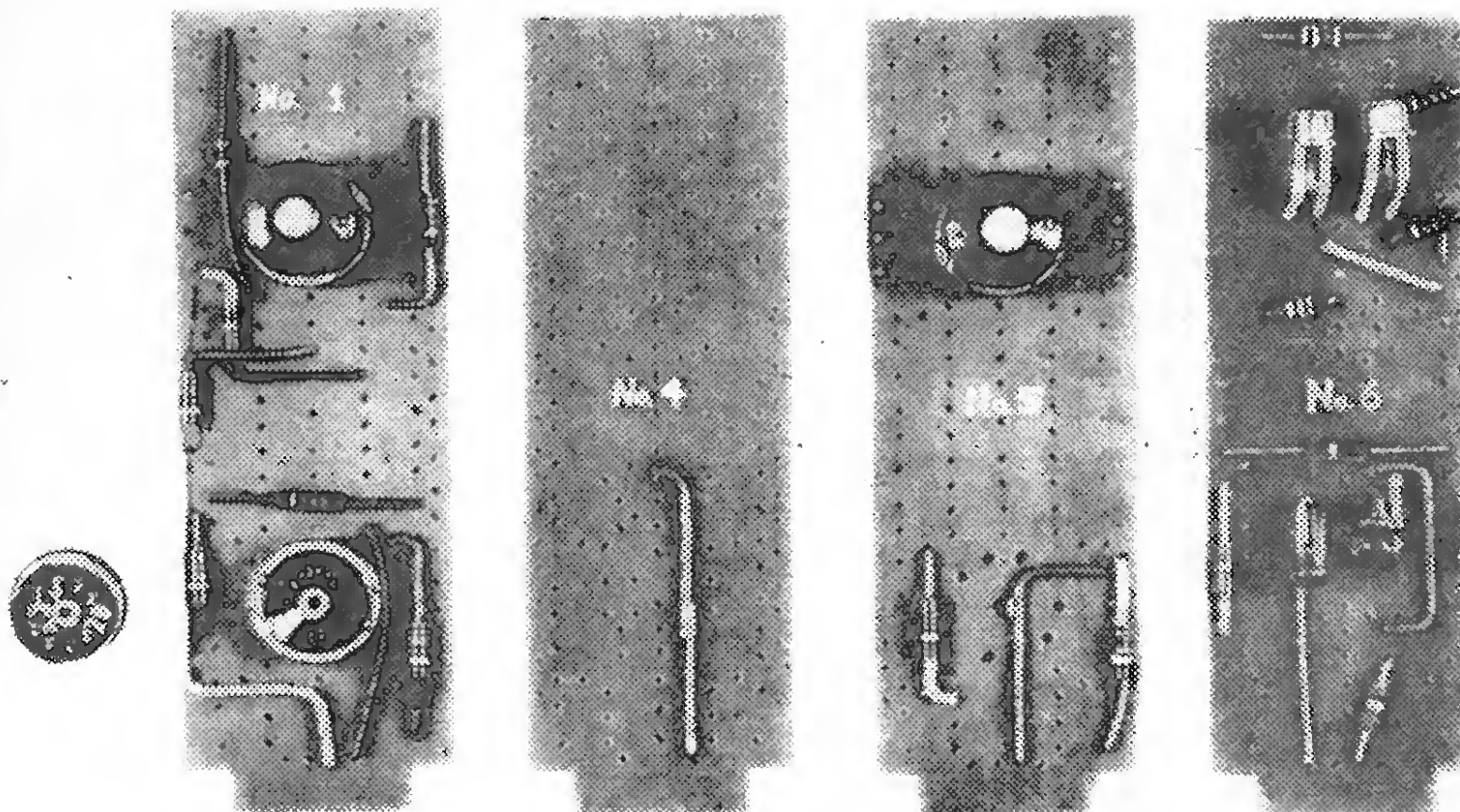
repetition rate to the thyristor; hence the load current falls to the required value. It is generally convenient to measure the load current on the a.c. side of the supply by inserting a resistor in series with the load current (b). The r.m.s. voltage across this resistor,  $R$ , should be about  $1\frac{1}{2}$  V at the value of current to be limited. A heater transformer has been found suitable for this application, the non-linear characteristic being obtained by the Zener diode—resistance network. For minimum current limiting effect  $RV_1$  and  $RV_2$  should be set at their maximum values. If they are reduced to zero the current in the thyristor circuit is limited to a very low value.

## CONSTRUCTION OF EXPERIMENTAL CIRCUITS

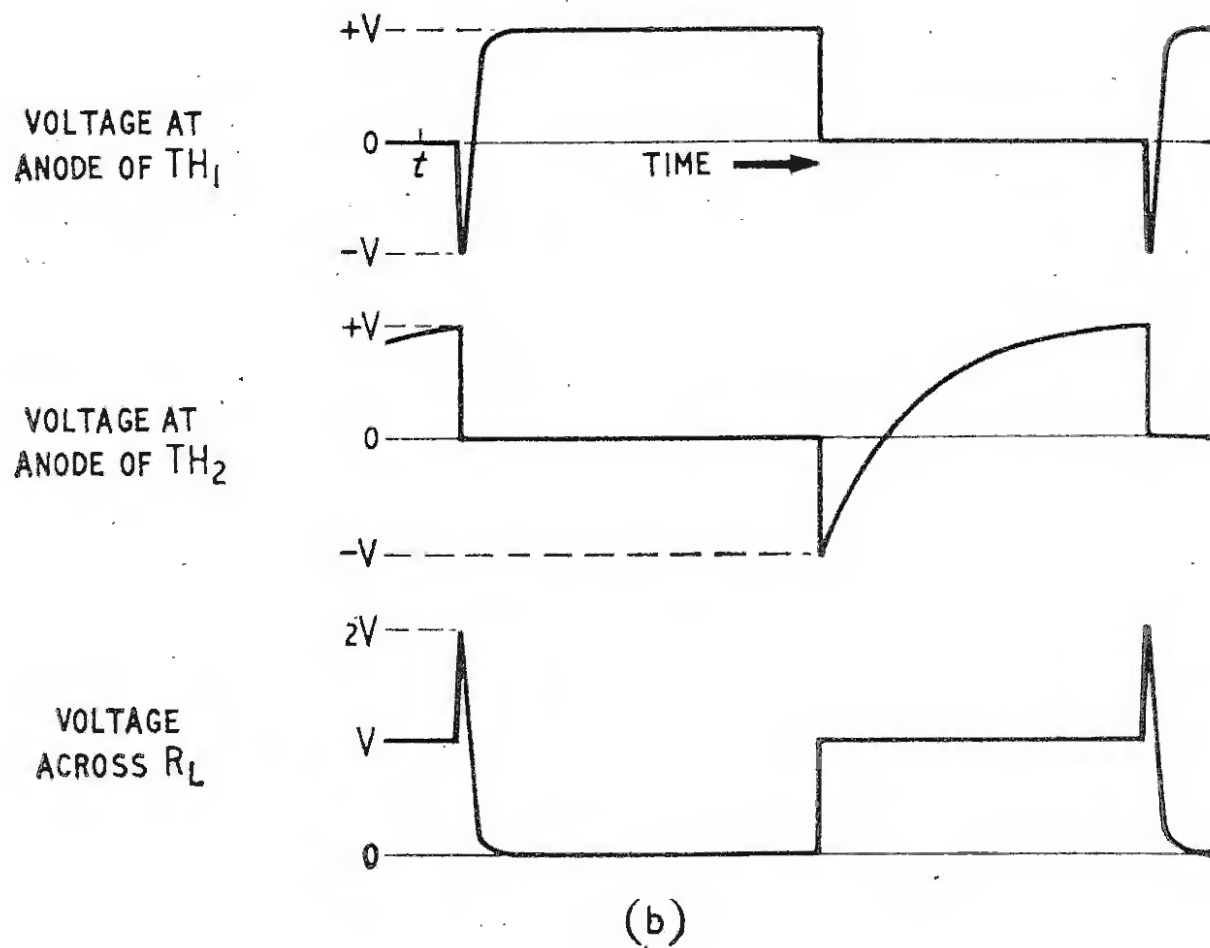
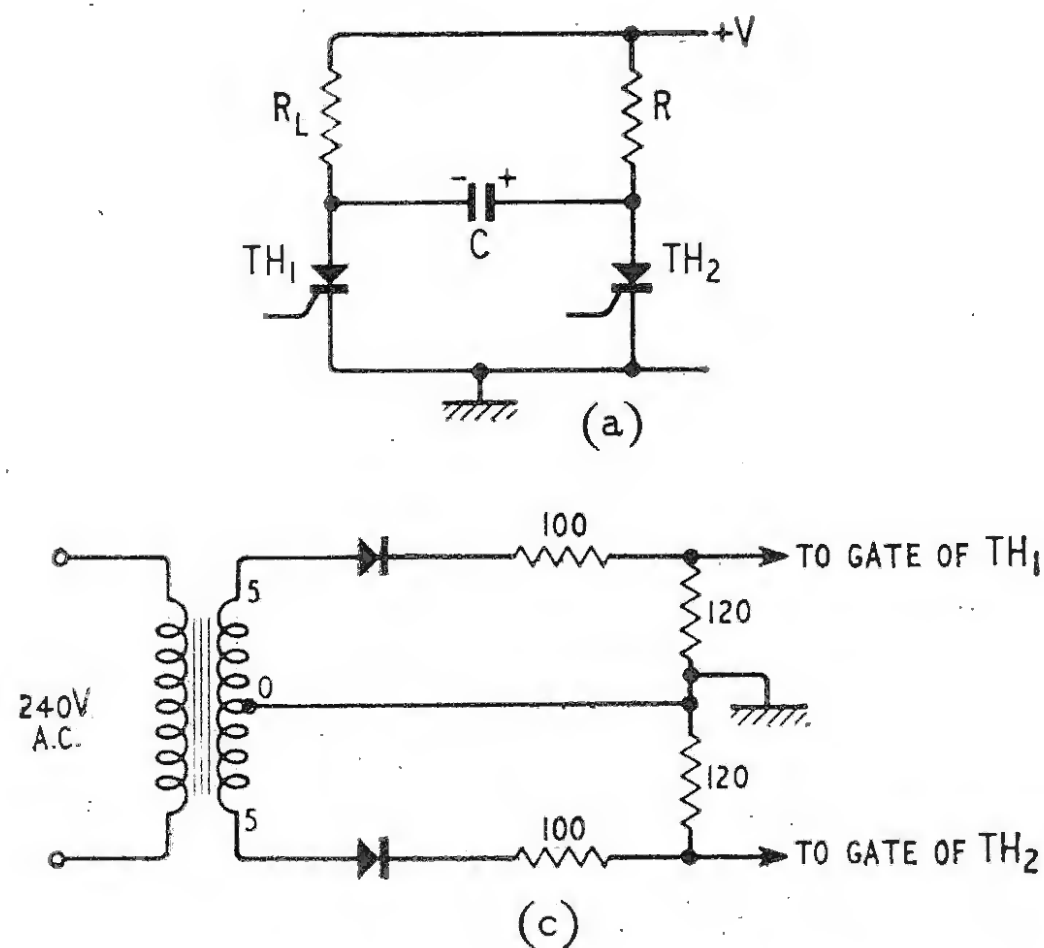
THE circuits outlined in this article have been used by the author in conjunction with thyristors with ratings between 4 A, 25 p.i.v. and 10 A, 400 p.i.v. Many other methods of control are available including electromagnetic methods, blocking oscillators and Schmitt circuits, and references to the design of these are given on page 454.<sup>(2) (3) (4)</sup>

For convenience of storage and interconnection of circuits, printed circuit boards were used. A selection of these is shown in the photographs. No. 1 (left) is the two-transistor pulse generator; No. 4 (second from left) is the Shockley diode; No. 5 (third from left) is the unijunction transistor circuit; and No. 6 is a circuit comprising the first two sections of the controlling pre-amplifier. The transistor and Unijunction transistor pulse generator circuits were built up using boards with valve bases on

them for convenience of removal of transistors for other experiments. One transistor is shown removed from its holder.



## THYRISTORS IN DIRECT CURRENT CIRCUITS



TO switch off a direct current it is necessary to reduce the thyristor current to a value below its holding value so that it can assume its blocking state. Various methods have been devised to do this, most of them involving charging or discharging a capacitor, since it may be regarded as a load or source of practically zero resistance at the time of switching. One simple circuit is shown here at (a).

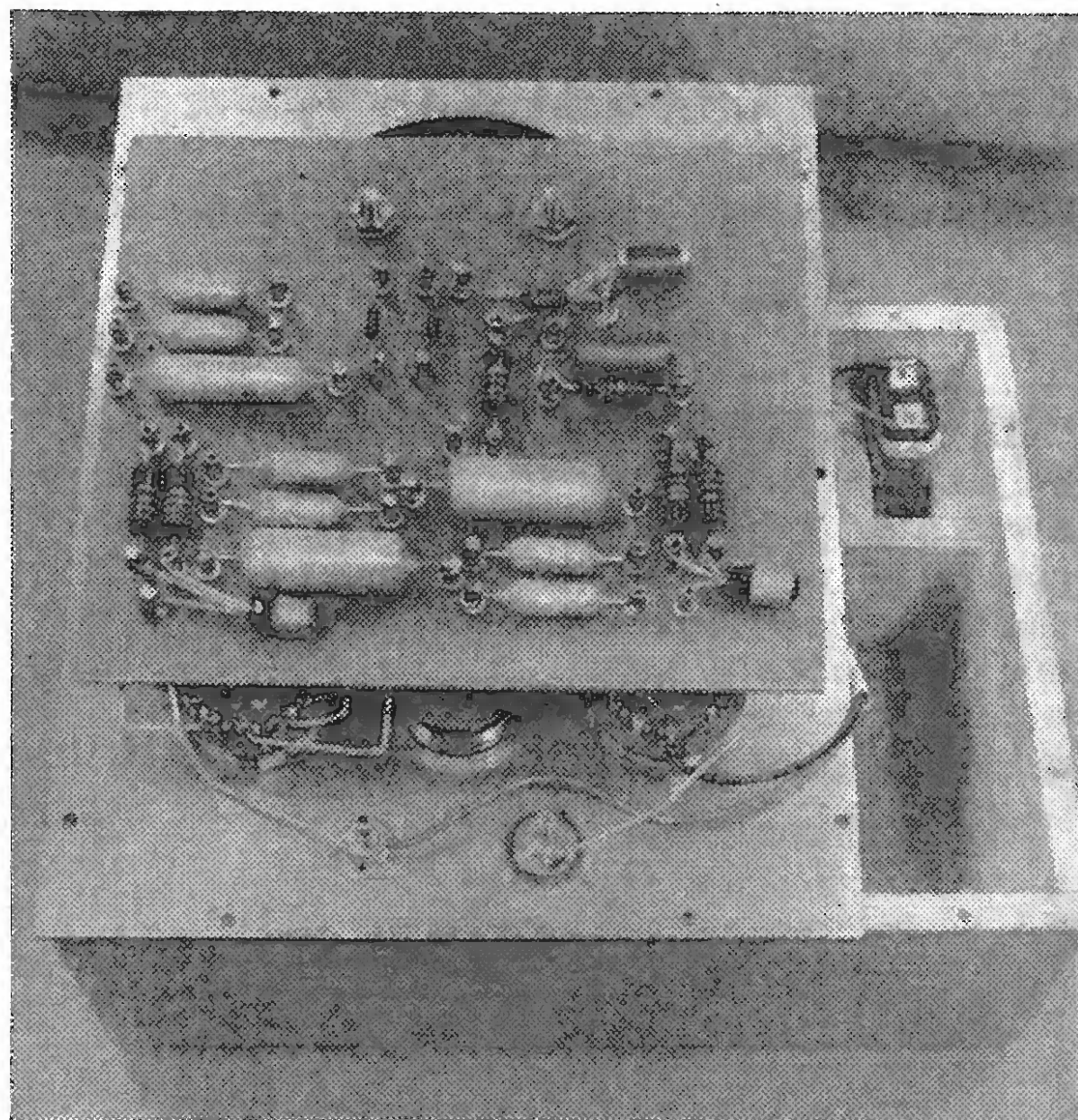
Suppose  $TH_1$  is conducting at time  $t$  as shown in (b). The polarity of the potential across the capacitor is shown in (a); if  $TH_2$  is switched on a little later, the positive terminal of the capacitor is connected to earth, making the anode of  $TH_1$  instantaneously  $-V$  volts relative to earth. This thyristor is now reverse biased, and provided forward current does not flow for a time equal to the turn-off time of the device (typically  $25 \mu s$ ), the thyristor will assume its forward blocking condition. With most commercially available thyristors this condition can be satisfied if the product  $R_L C$  is greater than 30, where  $C$  is in microfarads. To switch the load current on, a signal is applied to the gate of  $TH_1$  which turns  $TH_2$  off by the process outlined above. Resistance  $R$  does not have any effect on the switch-off of load current, but the minimum time between switching operations is set by the time taken for the capacitor to charge up to  $V$  volts. Resistance  $R$  can be selected on the basis that the minimum time between switching operations should be greater than  $5RC$  seconds, where  $C$  is in farads. In diagram (a),  $V=30$  volts,  $R_L=15\Omega$ ,  $R=660\Omega$ ,  $C=3 \mu F$ . In practical cases the load usually has some inductance and it is necessary to shunt  $R_L$  with a diode to allow the load current to decay slowly when the thyristor is turned off.

To allow inspection of the switching waveforms on a c.r.o. the two thyristors must be switched alternately. A simple circuit to perform this operation is shown at (c).

### REFERENCES

1. "Firing Requirements for Silicon Controlled Rectifiers," by T. J. Jarratt. *Mullard Technical Communications*, Vol. 6, No. 55, March 1962.

2. "Transistorized SCR Firing Circuits," by T. J. Jarratt. *Mullard Technical Communications*, Vol. 7, No. 65, June 1963.
3. "Simple Electromagnetic Methods of Pulse Generation," by R. F. Burbridge and M. James. *Proc. I.E.E.*, Vol. 112, No. 2, February 1965.
4. "Silicon Controlled Rectifier Manual." General Electric Co. of New York.
5. "Controlled Rectifiers in Stabilized Power Supplies," by F. Butler. *Wireless World*, October 1963.



First prize in the Junior Section of the annual Constructors' Competition organized by the Welwyn Garden City Group of the R.S.G.B. was won by Trevor Baker, aged 16, with this version of the capacitance meter described in *Wireless World* in April 1964. He used Formica bonded to the non-copper side of a piece of printed-circuit board for the front panel; the copper being connected to the low-potential terminal to provide a hand-capacitance screen. Trevor Baker planned and produced a printed circuit board on which to mount the components.



# Electronic Laboratory Instrument Practice

## 9.—AUDIO AMPLIFIER MEASUREMENTS

By T. D. TOWERS,\* M.B.E., A.M.I.E.E., A.M.I.E.R.E.

UNDER the impact of British Standard 3860 : 1965 and the recommendations of the American Institute of High Fidelity Manufacturers (I.H.F.M.), audio amplifier measurements now begin to follow a common pattern. Where American and British practice differ, the British standard is followed in this article.

### Output power

The measurement—like the design—of an audio amplifier must start with the output end. The first consideration is “*rated output power*,” i.e. the power the manufacturer or designer claims can be delivered continuously by the amplifier to a stated load resistance at 1 kc/s without the harmonic distortion rising above a specified limit. Typical distortion limits are 10% for “entertainment” applications, 1% for average high-fidelity and 0.1% for very high fidelity. To verify the rated output of an amplifier a 1 kc/s sinewave is fed through it at a level sufficient to produce the rated output power in a non-inductive load as specified by the manufacturer, and, after not less than 30 seconds, the harmonic distortion is measured by one of the methods described later in this article.

Another output characteristic of the amplifier, not to be confused with the rated output power, is the “*maximum output power*.” This is the power output at 1 kc/s that can be obtained when the level is raised until the output total harmonic distortion equals the limit used by the manufacturer for specifying the rated output power. Naturally the maximum should not be less than the rated power.

In the U.S.A., the term “continuous output power” is used synonymously with the British “maximum output power” to describe the greatest single-frequency power that can be obtained from an amplifier for not less than 30 seconds without exceeding its rated total harmonic distortion. Other terms formerly used for the same concept have been “sine-wave power,” “r.m.s. power” or “steady state power.”

Manufacturers have always tried to find more valid (or more customer-attractive?) methods of rating the power available from an amplifier than the continuous output power. The British Standard does not recognize these, but American practice is sometimes to specify a “music power output.” This is the greatest single-frequency power that can be obtained from an amplifier without exceeding its rated distortion where the measurement is made immediately after the sudden application of a signal and during a time interval so short that supply voltages within the amplifier have not changed from their no-signal values.

Another concept sometimes used (and beloved of advertising staff!) is the “peak power” rating. This can be taken as twice the corresponding single-frequency rating. For example, by the specific term “peak power rating” is usually meant twice the rated output power

defined earlier; similarly the “peak music power output” is twice the “music power output.”

As described in the last article (No. 8) of this series, the output power can be measured on an audio power meter or calculated from the r.m.s. voltage across the load resistance. In the latter case, a true r.m.s. reading meter should be used, and it is prudent to inspect the output waveshape with an oscilloscope to ensure that it is reasonably sinusoidal.

On the load resistance, the British Standard merely provides that it should not vary from its nominal value by more than 5% while dissipating any power up to the amplifier rating. The American I.H.F.M. recommends that it should be capable of dissipating the full output of the amplifier while maintaining its resistance within 1% of the rated value, but also that it will not have more than 10% reactive component at any frequency up to 5 times the highest test frequency.

The 1 kc/s input test signal to the amplifier should be sinusoidal and accurate in frequency to  $\pm 2\%$ . It should be low distortion relative to the amplifier distortion being measured, the B.S.I. recommendation being that the r.m.s. total of all components other than the fundamental should not be more than 1/5th of the expected harmonic distortion in the amplifier. This need for a pure test signal is sometimes overlooked, particularly in measuring high-quality, low-distortion amplifiers. I have known cases of apparently high amplifier distortion traced back to the generator. Conversely, I have known of high-distortion amplifiers measuring low because the generator and amplifier distortions balanced each other out.

In discussing output power we have tacitly assumed we are dealing with power amplifiers. For pre-amplifiers we are concerned with rated and maximum output voltages, but the same principles apply. The manufacturer specifies a rated output voltage which the pre-amplifier can supply at 1 kc/s without exceeding a stated limit of harmonic distortion. The maximum output voltage is the actual voltage output at this stated distortion limit.

### Harmonic distortion (single tone)

In commercial amplifiers it is customary to consider the available output power in relation to the total harmonic distortion at that power.

The simplest (and fastest) method of measuring harmonic distortion is to use a commercial *distortion-factor meter* (also known as an harmonic-distortion meter or total-distortion meter). The basic arrangement of a distortion-factor meter is illustrated in Fig. 63(a). A single frequency sinewave from the a.f. generator (usually 1 kc/s) is applied to the amplifier under test. This signal should be as free of distortion as possible, and to this end a tuned filter is often interposed after the signal

\*Newmarket Transistors Ltd.

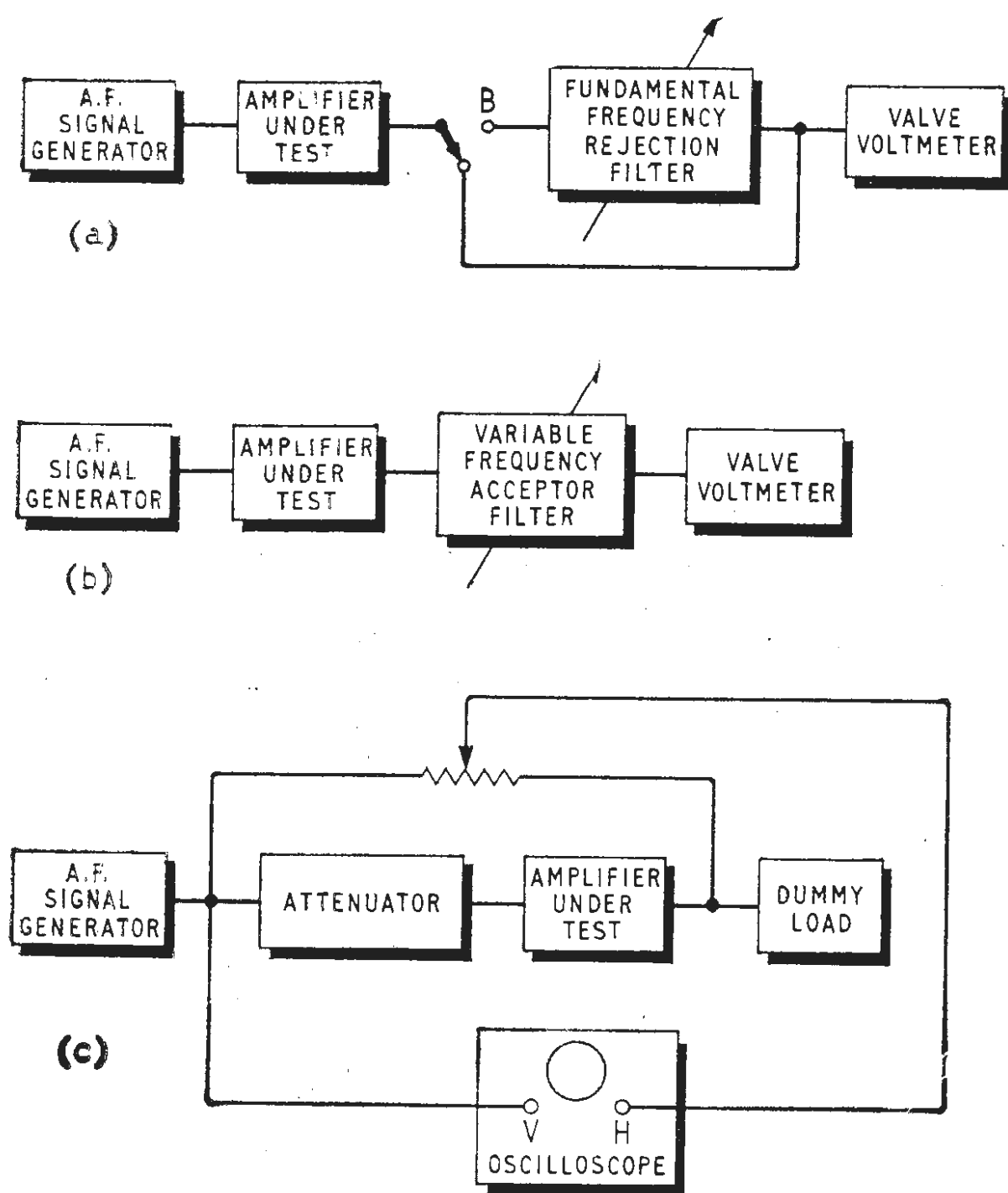


Fig. 63. Basic arrangements for different methods of measuring audio amplifier harmonic distortion: (a) distortion-factor meter; (b) wave-analyser; (c) "balance"-method.

generator. With the switch in position A, the amplifier output voltage (comprising fundamental and harmonic components) is measured on the valve voltmeter. The switch is then transferred to position B and the funda-

mental frequency rejection filter is tuned for minimum output voltage. The ratio of this minimum voltage (which represents harmonic components) to the first voltage (which represented fundamental plus harmonics) is computed to give the distortion percentage.

While distortion-factor meters are adequate for measuring total harmonic distortion, more refined testing requires that each harmonic in an amplifier output should be assessed separately. The "wave analyser" is the instrument normally used for separate measurement of each of a series of harmonics. Fig. 63(b) shows in diagram form the basic arrangement of the wave analyser. In this case the output signal from the amplifier is passed through a variable frequency acceptor filter which is tuned in turn to the fundamental and each successive harmonic. By this means it is possible to read off the comparative voltage of each frequency and compute the percentage of 2nd, 3rd etc. harmonics present individually in the amplifier output.

A third method sometimes used to measure harmonic distortion whose accuracy is much less affected by distortion in the input signal to the amplifier under test is shown in Fig. 63(c). This "balance-method" consists of balancing the fundamental of the amplifier output signal against the input signal at the vertical input of an oscilloscope. If no harmonic distortion were introduced by the amplifier, the vertical signal at the scope input would be zero, i.e. a horizontal line. Harmonics introduced by the amplifier gave rise to a vertical deflection trace which can be calibrated to give a direct visual indication of each harmonic. (The circuit shown assumes that phase inversion occurs across the amplifier.)

Commercial distortion measuring equipment can be expensive, but it is possible to build your own distortion factor meter reasonably easily. Fig. 64 gives a suggested three-transistor circuit with a Wien-bridge network to suppress the fundamental, and leave only the harmonics,

(continued on page 457)

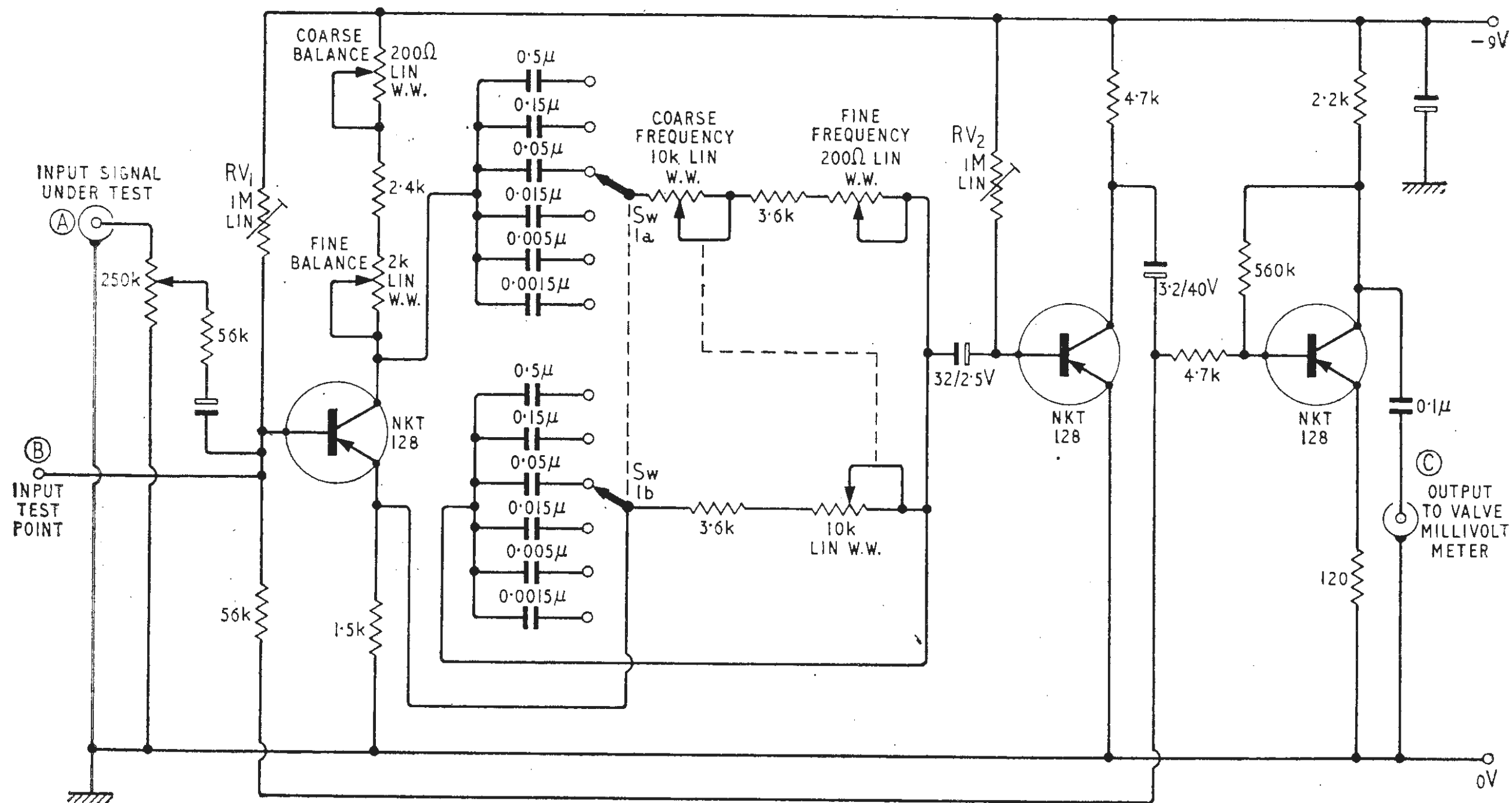


Fig. 64. Suggested circuit for transistor distortion-factor (total-distortion) meter covering 20-20,000 c/s.



of the signal under examination. With a 1 kc/s signal from the amplifier applied to the input point (A) the balance and frequency controls are adjusted for minimum reading on the valve voltmeter at the output point (C). The amplifier test signal is then changed to 2.5 kc/s (well beyond the second harmonic of 1 kc/s) and the level adjusted with the 250 k $\Omega$  input potentiometer until the output voltage reaches a convenient reference level,  $V_o$  (e.g. 1 V r.m.s.). The voltage  $V_b$ , at the base of the first transistor is also noted. The amplifier test frequency is returned to 1 kc/s and the input level adjusted (if necessary) to give the same base voltage,  $V_b$ . The balance and frequency controls are re-nulled and the resultant voltage,  $V_p$ , at the output measured. The percentage total distortion is then given by  $(V_D/V_o) \times 100\%$ . With a 1 V reference, a 10 mV reading represents  $(10/1000) \times 100 = 1\%$  total distortion.

## Sensitivity

The sensitivity of an audio amplifier is nowadays (following the British Standard) often specified in terms of a "sensitivity voltage," i.e. the e.m.f. applied in series with the stated source resistance, to the input terminals in order to obtain the rated output power or voltage. Note that for a sensitivity voltage specification you must define the source impedance and the rated output power. Sensitivity voltage is measured as shown in Fig. 65(a), where  $V_s$  is the e.m.f. from a voltage (low impedance) source which, when applied *via* the specified source

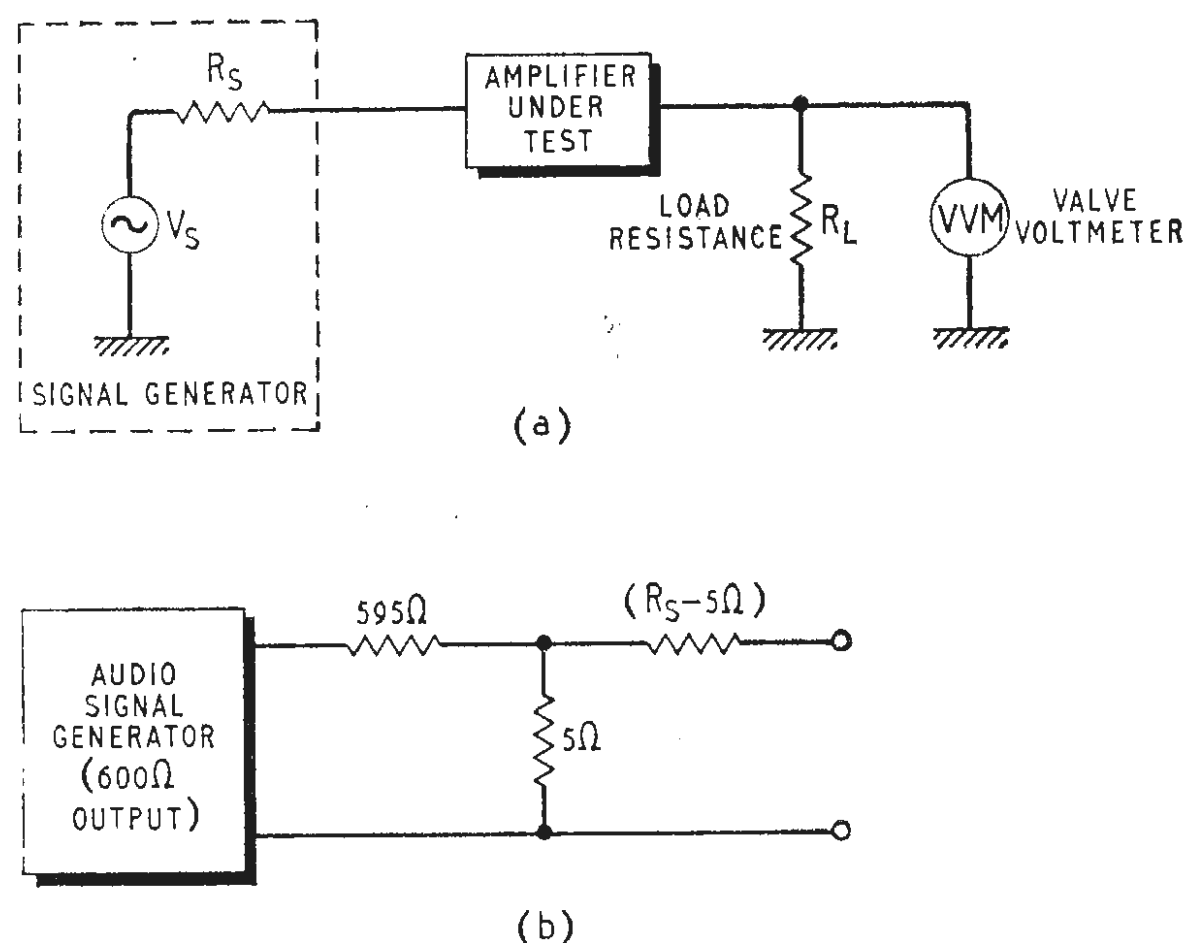


Fig. 65. Sensitivity voltage measurement:— (a) general arrangement; (b) simulating a source resistance  $R_s$  with a standard 600 $\Omega$  audio generator.

resistance  $R_s$  to the amplifier, gives the rated power output as measured by the valve voltmeter across the specified load,  $R_L$ . A practical arrangement to provide the correct generator drive is shown in Fig. 65(b). It should be noted that the sensitivity voltage is *not* the voltage at the input of the amplifier, but is the voltage applied to a source resistance in series with the amplifier input. Even some experienced engineers are confused on this point.

## Gain

A concept related to sensitivity is amplifier gain. The British Standard recommends the use of "transducer"

gain,  $G$ , with defined source and load resistances. This is measured with the same arrangement as for sensitivity in Fig. 65. The source e.m.f., fed into the amplifier via the defined source resistance  $R_s$ , is adjusted to a value  $V_s$  for which the output voltage  $V_o$  across the load resistance  $R_L$  gives an output power one tenth (10 dB down) of the amplifier's rated output power. The maximum available power from the source (obtained only if the amplifier input resistance exactly equals the source resistance) is  $P_s = V_s^2/4R_s$ , and the power in the load is  $P_o = V_o^2/R_L$ . The transducer gain  $G$  (in dB) =  $10 \log_{10}(P_o/P_s)$ . Once again, note that the gain defined here is not the ratio of output power to amplifier actual input power.

The gain of a pre-amplifier is measured in the same way. A source of e.m.f. fed through a specified source resistance is adjusted until the pre-amplifier output voltage, measured on a high impedance meter, is 0.707 (i.e. 12 dB down) of rated output voltage. The transducer gain is then calculated as before.

It scarcely needs pointing out that in all amplifier measurements unless specifically stated otherwise, any volume control should be set for maximum gain.

## Frequency-amplitude response measurements

Frequency response measurements rank with distortion measurements in assessing amplifier fidelity. They fall into two main categories, referred to as (a) "power bandwidth" and (b) "bandwidth."

*Power bandwidth* is the curve of maximum output power (for the defined total distortion) versus frequency, plotted with logarithmic scales on both axes. The British Standard recommends that measurements should be made up to 5 kc/s. The lowest value of maximum output power on this curve is of interest because it is used in the measurement of bandwidth discussed below. The measurement of the power bandwidth response reduces itself to measuring the maximum output power as described earlier over a range of frequencies instead of at the normal 1 kc/s reference frequency.

*Bandwidth* relates to the variation of amplifier sensitivity with frequency. For this measurement, the amplifier controls are first set "flat"—i.e. gain control at maximum and tone controls or filters set for most uniform frequency response. A 1 kc/s sinusoidal signal is then applied to the input and adjusted in amplitude to a specified output power, which must not be more than the minimum noted on the power/frequency curve referred to above. (American practice here is to set a 1 kc/s output power at least 10 dB down on the rated output power and not less than 20 dB above residual noise.) The input signal frequency is then varied in steps above and below 1 kc/s over the frequency range of interest and the change in sensitivity voltage (i.e. e.m.f. into source resistance into amplifier) necessary to keep the output constant is measured in decibels. This change in decibels (reversed in sign) is plotted on a linear vertical scale against frequency on a logarithmic scale. The "bandwidth" is often popularly specified as the lower and upper limit frequencies where the sensitivity has dropped by a certain amount—frequently 3 dB—from the 1 kc/s value.

Typical 3 dB bandwidth specifications are

- (a) Telephone 300-3500 c/s; (b) Radio receivers etc. 100-4500 c/s; and (c) "Average" hi-fi 20-20,000 c/s.

Frequency response tests can be carried out using conventional good-quality signal generators and valve voltmeters, but the plotting of results is time-consuming.

Commercial equipment is available in the form of strip chart recorders, which can produce a pen record in a few minutes and wobblers which display an instantaneous scope trace of the frequency response.

### Intermodulation or two-tone distortion

With a single frequency tone, non-linearity in an audio amplifier gives rise to harmonic distortion discussed earlier. When two separate single-tone audio frequencies are fed simultaneously through the amplifier, a new kind of distortion, "intermodulation distortion," arises from the non-linearity. The a.f. components interact and give rise to sum and difference frequencies as well as the two fundamental test frequencies and their harmonics. For example, in an amplifier with intermodulation distortion, the feeding of 100 c/s and 5,000 c/s input signal will produce significant outputs not only at the two test frequencies but also at 4,900 and 5,100 c/s. Such distortion is the more objectionable in that it introduces frequencies not harmonically related to the test frequencies. Until the issue of B.S. 3860:1965 several different methods of measuring intermodulation distortion were used, but the preferred method is now the "high-low" frequency one. In this a small high-frequency signal (about 5,000 c/s) is applied to the amplifier together with a large low frequency one (about 100 c/s) of four times the amplitude. The intermodulation distortion percentage in the output can be arrived at by filtering out the two test frequencies and computing the residual r.m.s. signal as a fraction of the full r.m.s. output. This gives the total intermodulation distortion, but a wave analyser can also be used, as with harmonic distortion, to evaluate the separate frequency components of the total.

Commercial intermodulation distortion test sets are available, but anyone interested in doing a few intermodulation tests can set up the arrangement in Fig. 66 with instruments available in most laboratories. Fig. 66(a) shows frequencies of 100 and 5,000 c/s with a 4 : 1 amplitude ratio being fed into the amplifier via a balanced bridge which prevents intermodulation distortion at the input. The bridge transformer is a high-quality 1 : 1 audio isolating transformer and the four 680 Ω resistors must be carefully equalized to isolate the two signal generators. The amplifier output is fed

through a high-pass filter to reject the low frequency. Fig. 66(b) shows an RC filter circuit used by the author for 100 c/s rejection. The residual modulated 5,000 c/s signal is fed to the scope vertical amplifier and its time base synchronized direct from the 5,000 c/s generator. The scope trace is shown in Fig. 66(c) with the method of computing the percentage intermodulation distortion.

### Crossover distortion

With the recent popularity of transistor amplifiers "crossover distortion" has been much bandied about. I have heard some claim that it is a form of intermodulation distortion, but one should be clear on this point—it arises with a single frequency signal and is a form of harmonic distortion. A sinewave input as Fig. 67(a) becomes transformed to the waveshape at Fig. 67(b). Why it is called "crossover" distortion should be clear from the little plateau in crossing over the zero axis. In most forms of harmonic distortion the higher harmonic distortion components are usually relatively small, but with cross-over significant components can sometimes be found out to the fifth and higher harmonics. This should be remembered when using a wave analyser as it is possible to overlook these higher harmonics.

### Hum

Hum in an amplifier output is usually measured with a voltmeter or power meter isolated from the amplifier output by a low-pass filter passing only up to the fourth harmonic of the power supply frequency, i.e. to 200 c/s in the United Kingdom. The meter should preferably be true r.m.s. reading. (A wave analyser may also be used, and the hum voltage computed from the square root of the sum of the squares of the component voltages.) The hum level of the amplifier is specified in decibels relative to the rated output of the amplifier when the input is terminated with a standard value resistor (which should be a low-noise high-stability resistor screened to prevent stray hum pick-up). The standard resistor is usually made equal to the source resistance of the input transducer for which the amplifier is designed.

The r.m.s. meter plus low-pass filter method of measuring hum can lead to erroneous readings because it does not discriminate against noise in the low-frequency

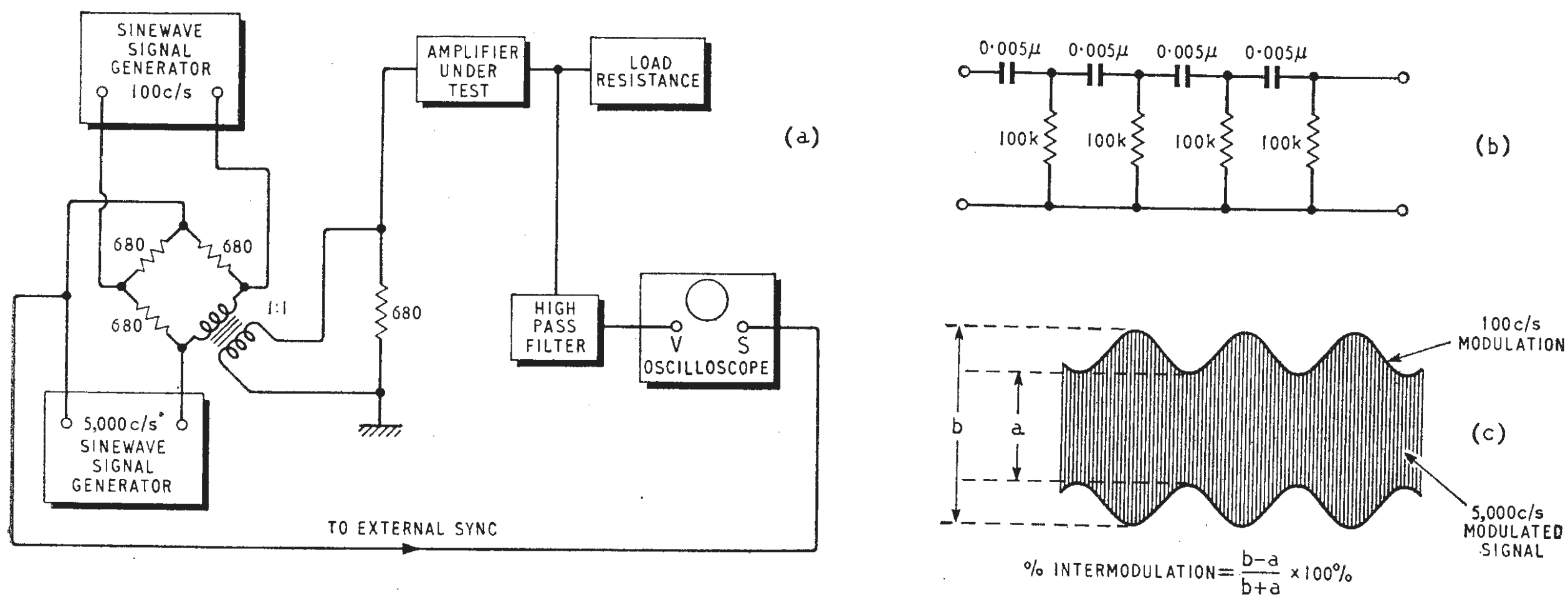


Fig. 66. One experimental arrangement for measuring intermodulation distortion:— (a) general block diagram; (b) RC high-pass filter for 100 c/s rejection; (c) intermodulation distortion computed from 100 c/s modulation depth on 5,000 c/s.



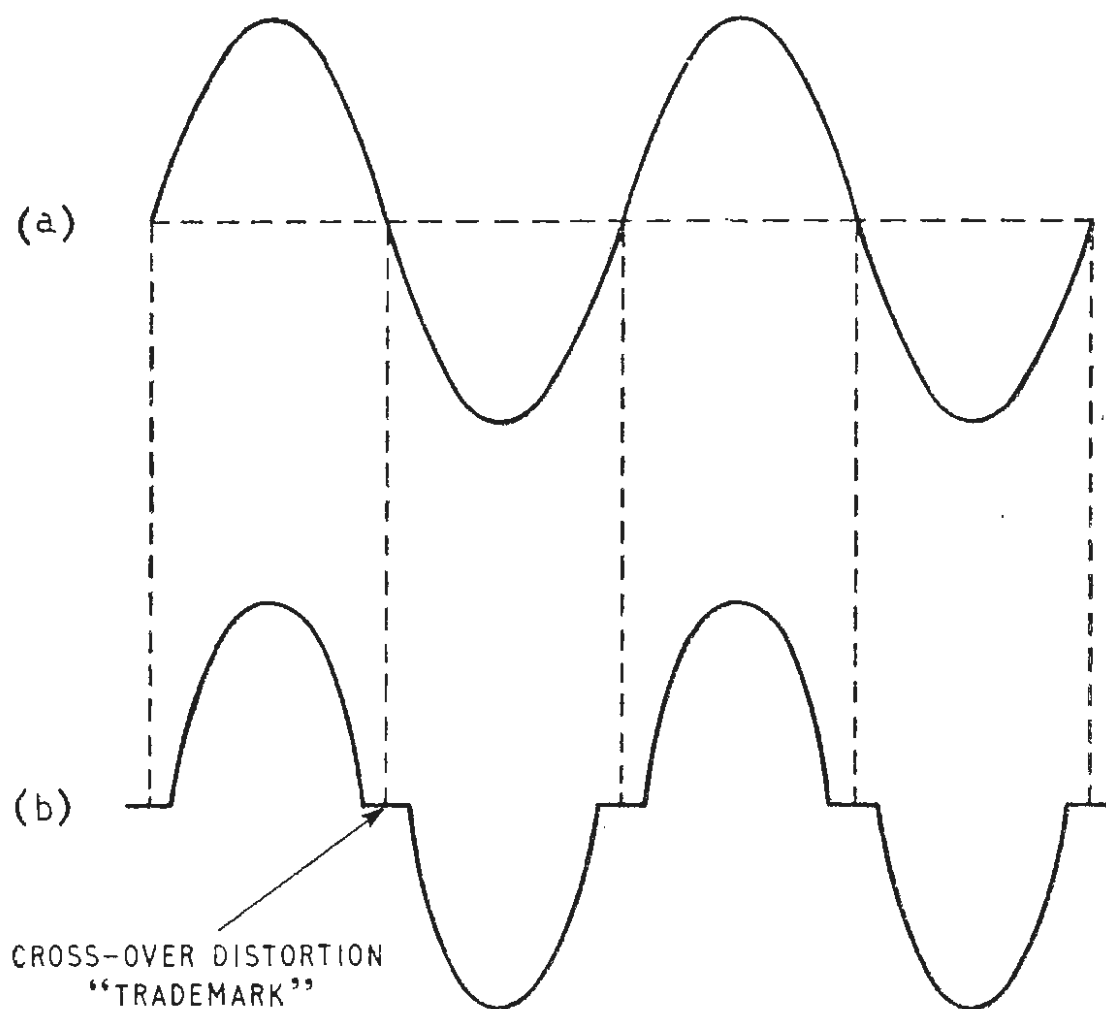


Fig. 67. "Crossover" distortion waveforms:— (a) input sinewave; (b) output waveform with significant crossover distortion.

passband of the filter. For this reason it is usual to inspect the hum voltage on a scope at the same time to ensure no significant noise signals.

## Noise

Apart from hum, noise in an amplifier system may show up as hissing, crackling, popping, etc. It is usual to treat "noise" as not including hum, and such noise output may be measured with an r.m.s. voltmeter or power meter isolated from the amplifier output by a high-pass filter that effectively removes hum components. As with hum measurements, the input should be terminated with a specified resistance.

The simple high-pass filter method treats all noises in the spectrum in the filter passband equally, but owing to the selective hearing of the human ear, a better indication of the noise assessment of an amplifier is obtained by using a selective high-pass filter which still blocks hum voltage but accentuates noise at the frequencies where they have the most effect on the normal listener. This gives rise to a "weighted noise output voltage" instead of a simple noise output voltage, but, except for the filter design, measurement methods are the same as for unweighted noise.

The noise output power (r.m.s. voltage into load resistance) expressed in decibels down relative to the rated output power is one index of the noise performance of the amplifier. Another index sometimes used is the "equivalent noise input voltage". This is the input voltage at 1 kc/s in series with the stated source resistance that would produce an r.m.s. output voltage across, or power in, the stated load resistance equal to that produced by amplifier noise. To measure the equivalent noise input voltage a 1 kc/s sinewave test signal voltage,  $V_s$ , is applied to the amplifier input *via* the specified source resistance, to produce an output voltage,  $V_o$ , across the load resistance  $R_L$ , such that the output power is less than the rated output power of the amplifier. The test signal is then removed and the input terminated by a screened resistor (usually equal to the source resistance). Under these conditions, an r.m.s. noise output voltage  $V_N$  is read. The equivalent noise input voltage is then equal to  $(V_s \times V_N)/V_o$ .

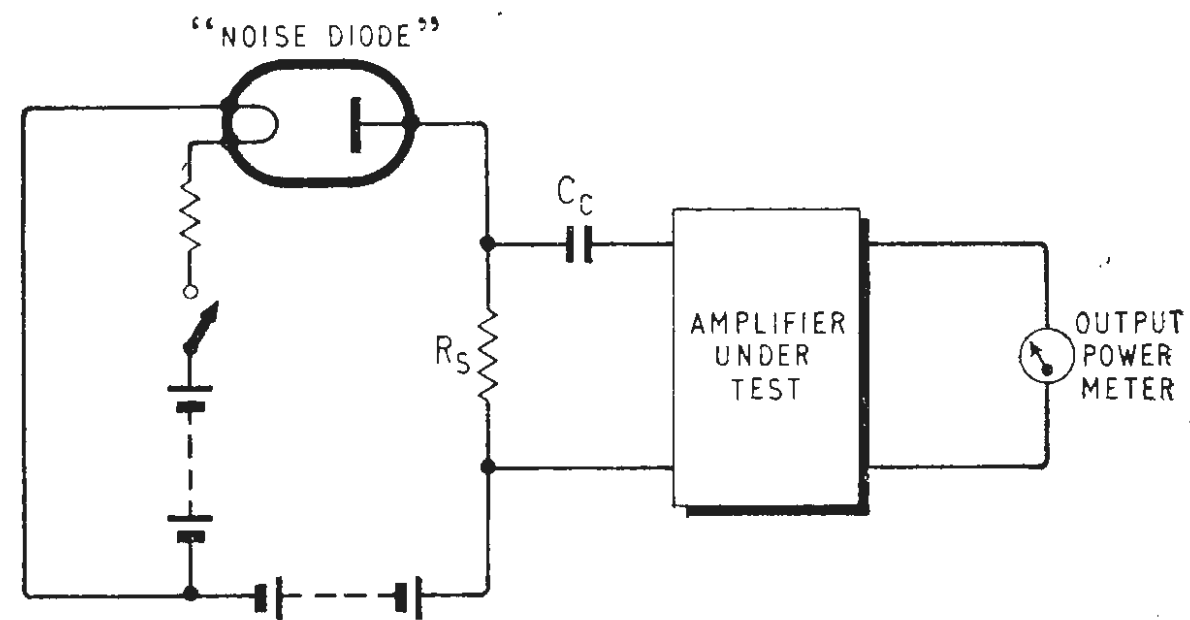


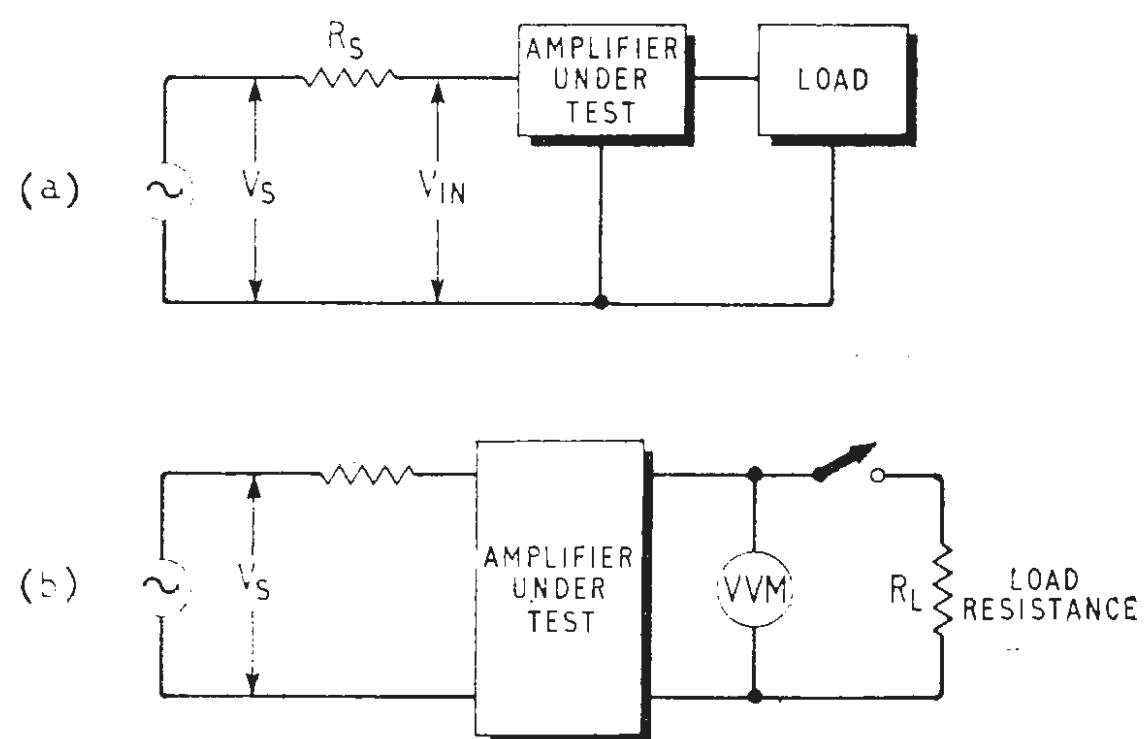
Fig. 68. Noise figure measurement circuit.

Another way of specifying the noise performance of an amplifier is by means of its "noise factor". This is the ratio of the total r.m.s. noise output voltage to that part of it which is due to the thermal noise of the source circuit treated as a passive network at 290°K over the frequency range of the amplifier. The noise factor,  $N$ , can be measured using a noise generator (generally a saturated thermionic diode) and an output meter arranged as shown in Fig. 68. The resistor  $R_s$  should be within 5% of the specified amplifier source resistance, and the coupling capacitor  $C_c$  should be not less than  $3300/R_s$  microfarads (where  $R_s$  is in ohms). The noise output is first measured with the diode filament cold. The filament current is then increased until the noise output power is increased by a convenient factor  $P$  (usually  $\times 2$ ) and the diode current  $I_D$  (amps) is measured. If the resistor  $R_s$  is at 290°K (normal room temperature), the noise factor  $N$  expressed as a numerical ratio is given by  $N = 20I_D R_s (P - 1)$ . Often  $N$  is expressed in decibels rather than as a pure ratio.

## Impedances

The *input impedance* of an amplifier is the impedance looking *into* the amplifier input. It is difficult to measure because in many cases the impedance being measured can depend upon the source impedance presented to the amplifier input by the measuring circuit. An impedance bridge may be used, but it is essential to see that it presents the proper source impedance to the amplifier input. So far as the input resistance is concerned a simple method of measuring this is shown in Fig. 69(a). A sinewave voltage input  $V_s$  at the test frequency (usually 1 kc/s) is applied *via* a specified source resistance  $R_s$  to give an output below the rated output power. The source open circuit voltage  $V_s$  being known, the voltage

Fig. 69. Measuring input and output resistances of any audio amplifier:— (a) input resistance; (b) output resistance.



$V_{IN}$  at the amplifier is also noted, and the input resistance computed from  $R_{IN} = R_S \cdot V_{IN} / (V_S - V_{IN})$ .

Amplifier output impedance too can be measured with an audio-frequency impedance bridge, but in the absence of such an instrument the arrangement shown in Fig. 69(b) can be used for measuring output resistance. A 1 kc/s source being applied to the input, the output voltage,  $V_{O'}$ , with no load attached, and  $V_O$  with the specified amplifier load  $R_L$  are measured. Then the amplifier output impedance,  $R_{OUT}$ , is given by

$$R_{OUT} = R_L (V_{O'} - V_O) / V_O$$

Connected with the amplifier output resistance is its "damping factor", i.e. the ratio of the specified load resistance to the output impedance (assumed to be resistive) of the amplifier at a stated frequency. The damping factor is usually measured at 50 c/s. A 50 c/s signal is applied to the input to produce one quarter of the rated output power in the specified output load resistance. Let  $V_O$  be the output voltage for this. Now remove the output load, keeping the input signal constant, and let the measured open circuit output voltage be  $V_i$ . Then the damping factor,  $F_D$ , is given by

$$F_D = V_O / (V_i - V_O)$$

## Stability

An important thing to check, especially in professional audio amplifiers, is the stability margin and whether the amplifier behaves satisfactorily towards both ends of the frequency response. The stability test prescribed by B.S.3860:1965 is to operate the amplifier without a load but with a capacitor connected across the output terminals. Where the amplifier is claimed to be unconditionally stable, the capacitor load is varied by steps of  $0.01 \mu\text{F}$  from  $0.01$  to  $0.1 \mu\text{F}$ , and by steps of  $0.1 \mu\text{F}$  from  $0.1$  to  $1 \mu\text{F}$  for a nominal  $15 \Omega$  load. For other stated loads these values should be adjusted inversely as the load resistance. Where no claims of stability are made, the capacitor should be such that its reactance at 200 kc/s is equal to the nominal load impedance, e.g.  $0.05 \mu\text{F}$  for a 15 ohm load. The actual test of stability when the amplifier is capacitor-terminated is to inspect the output voltage in an oscilloscope to ensure no spurious oscillations, first with no input to the amplifier and then with a signal varying from 10 c/s to 70 c/s in frequency and an amplitude equal to the sensitivity voltage (see earlier) at 1000 c/s.

One popular method of amplifier stability assessment is "square-wave testing" in which a suitable square wave is applied to the input, and the output inspected on an oscilloscope screen. To reproduce faithfully a square wave of frequency  $f$  the amplifier must be capable of passing frequencies down to  $f/10$  and up to  $10f$ . A little thought is therefore required in selecting the square wave repetition frequency. For example, 1 kc/s is suitable for a general test on an amplifier with a bandwidth from below 100 c/s to above 10 kc/s. A square wave can be regarded as made up of an infinite number of odd harmonic related sinewaves, and therefore an amplifier being tested with square waves is being checked simultaneously at a number of frequencies. Some experience is necessary to interpret the significance of output distortion of a square wave, but as a rough generalization rounded leading edges indicate poor high-frequency response, upward tilt of the wave tops, excessive l.f. response or bass boost and downward tilt or "droop" poor low-frequency response. If the output has spikes, "ringing", or damped oscillations on the wave tops, the amplifier may have excessive high-frequency response, excessive amplification in some band of frequencies or instability.

## Precautions

In all audio amplifier measurements it is important, especially in low-level measurements (such as hum or noise) to ensure that the measurement technique does not give rise to spurious effects such as hum introduced by a ground loop formed between the instrument and the amplifier.

In all distortion measurements always measure the distortion of the signal generator itself to verify it is not less than five times down on the amplifier distortion.

Always check the calibration of any instruments before making exact measurements. Some things, like the accuracy of the frequency setting of your generator, are seldom questioned, but a few weeks before writing these words the author found the explanation for some curiously inconsistent amplifier response results in a standard commercial signal generator that gravely showed 9 kc/s on its setting dial while it delivered a steady 6 kc/s from its output terminals!

Finally if you have occasion to carry out any substantial tests in audio amplifiers, buy a copy of B.S.3860:1965 and consider its recommendations very carefully. In this also you will find described a number of other tests sometimes carried out on such amplifiers which could not be covered in this article.

## Commercial Literature

A 52-page catalogue containing electrical and mechanical design information on the "valves and cathode ray tubes for industry" manufactured by the M-O Valve Company, of Chelmsford, has been forwarded to us.

9WW 321 for further details.

"Simplification of Biasing Circuits using Transistors BCY42 and BCY43" is the title of an application note available from the Semiconductor Division of Standard Telephones and Cables Ltd., Footscray, Kent. The transistors mentioned are low level silicon epitaxial planar types with a two-to-one spread in gain, at a collector current of 1 mA.

9WW 322 for further details.

"SESCO Semiconducteurs."—This 44-page catalogue contains details of many hundreds of semiconductors ranging from signal diodes and rectifiers to thyristors and u.h.f. transistors. Also included are thin film circuits, microwave diodes, photosensitive devices and ring modulators. Copies of this catalogue are obtainable from SESCO's (Société Européenne des Semiconducteurs) U.K. representatives M.C.P. Electronics Ltd., Station Wharf Works, Alperton, Wembley, Middx.

9WW 323 for further details.

"Magnetic Recording Heads" for computers, data recorders, simulators and magnetic drum information storage units are described in a new series of data sheets issued by Gresham Lion Electronics Ltd. Binders containing these data sheets (A4) are available from the company's magnetic recording head department, Lion Works, Hanworth Trading Estate, Feltham, Middx. Eleven types of head for digital and analogue applications with up to 33 tracks per inch are included.

9WW 324 for further details.

The "Brimar Valve and Cathode Ray Tube Manual, Number 10" is now available, price 7s 6d, from the Brimar publicity department of Thorn-AEI Radio Valves and Tubes Ltd., of 155 Charing Cross Road, London, W.C.2. Industrial cathode-ray tubes and industrial switching transistors have been added for the first time to this publication, which contains 416 pages and gives design data on 629 different valves and c.r.t.'s. An equivalents list containing over 1,200 commercial and CV types is included.



## SELF-CONTAINED TELEPHONE SCRAMBLER

THE picture shows a portable voice scrambler recently introduced in America to combat the invasion of telephone privacy by line tapping—a subject of growing concern in the U.S.A. and not unheard of in Britain. The transistor battery-powered device is self-contained and requires no electrical connections to the telephone handset, the scrambled speech being transmitted acoustically to and inductively from the handset. A conversation is only possible when two correspondents have identically coded scramblers. Names of people and firms owning scramblers, and the codes used, are kept secret by the manufacturers. Weighing 26 oz, and containing a power pack of mercury cells with a life of 100 hours, the portable scramblers are manufactured and supplied by the Delcon Division of Hewlett-Packard, Palo Alto, Calif., at a price of \$550 per pair.

In the U.K. the Delcon scrambler has not been approved by the Post Office for use with the public telephone system (under the official telephone regulations legal action can be taken against people using unauthorized attachments or accessories) but, of course, no such restriction applies to private telephone systems. The Post Office has, however, approved a British transistor scrambler equipment, the Secraphone



made by T.M.C., which requires electrical connections from the subscriber's instrument to a small unit (6in × 4in × 10in) and two switches on the instrument.

## NEW THIN FILM MATERIAL

BETA TANTALUM is the name given to a recently discovered variant of the metal tantalum which may prove useful as a resistive material in integrated circuits. Discovered by workers in Bell Telephone Laboratories and Western Electronic Engineering Research Centre, U.S.A., the new material has a higher resistivity and a lower temperature coefficient of resistance than ordinary tantalum, and it becomes a superconductor at a much lower temperature (0.5°K instead of about 3.3°K). Like normal tantalum, it could be used to make thin-film capacitors because it readily forms oxides and can be anodized by the usual techniques.

So far, beta tantalum has been produced only in film form. Most of the experimental data has been collected from films produced by cathode sputtering, although the material has also been observed in films made by evaporation and chemical vapour deposition processes. When the films are formed in a sputtering system containing argon at a pressure of  $10 \times 10^{-3}$  to  $30 \times 10^{-3}$  torr, beta tantalum is frequently

observed when the total pressure of other gases in the vacuum system is less than  $1 \times 10^{-5}$  torr.

Beta tantalum formed by sputtering has a resistivity ranging from 180 to 220  $\mu\Omega$  cm, and a temperature coefficient ranging from  $-100$  to  $+100$  p.p.m./°C. In contrast, normal sputtered tantalum films have a resistivity in the range of 24 to 50  $\mu\Omega$  cm and a temperature coefficient in the range of  $+500$  to  $+1800$  p.p.m./°C.

The new material has a more complicated crystal structure than normal tantalum, but converts to normal tantalum when heated in a vacuum to about 750°C.

## SOLID-STATE IMAGE SENSING PLATE FOR CAMERA

THE National Aeronautics and Space Administration of the U.S.A. are experimenting with a small television camera which uses a solid-state image sensing panel in place of the conventional electron-beam pick-up tube. Presumably they plan to use it in observation spacecraft instead of vidicon cameras (which were installed in Mariner IV to take pictures of the planet Mars and in the Ranger series to photograph the moon). The image sensing plate is a mosaic of 2,500 phototransistors, measuring 0.5 in × 0.5 in, and has an image resolving power of 100 lines per inch of plate. The mosaic is an integrated-circuit 50 × 50 configuration, formed by 50 transistor collector structures running the length of the plate, each having diffused into it 50 individual base-emitter structures with 50 deposited metal conductors for the emitters running across the plate at right angles to the collector strips. The collector strips are diffusion isolated from each other.

Integrated-circuit structures are also used to provide the panel scanning circuits. A video output signal is obtained by sequential switching of a bias voltage to the phototransistor electrodes. The complete camera, which measures 6 in × 4 in × 2½ in and uses a standard 16-mm lens, has been developed for N.A.S.A. by Westinghouse.

## RESONANCE RECTIFICATION

THE phenomenon of "resonance rectification" occurs when an alternating potential is applied to a probe situated in a plasma. A direct current flows in the probe which reaches a maximum value as the frequency of the applied potential is varied through the plasma frequency. The phenomenon is being studied at the Radio & Space Research Station of the U.K. Science Research Council and is referred to in the annual report entitled *Radio Research 1964* (H.M.S.O.).

Theories have been proposed to explain the effect but none so far seem very satisfactory and some rely on the assumption of an unrealistic plasma sheath. An approach has been made which does not require the sheath postulate and a solution has been obtained for the frequency variation of the rectified current and admittance using a spherical probe. It was demonstrated that the direct current reached a maximum when the frequency had a value about two-thirds of the plasma frequency. Initial results using a Skylark rocket with a 2½ in disc probe showed little evidence of a resonance. Later experiments carried out with a spherical probe of 1 in dia. carried 3 ft in front of the payload, showed that the probe behaved roughly as expected, although the magnitude of the current peak and its width did not appear to be as predicted. A sample record showed a peak at 2 Mc/s. Many of the experimental facts about this phenomenon are still confusing and the results of the experiments are still being worked out in detail.



# NEW PRODUCTS

## equipment systems components

### Military H.F. Transceiver

THE multi-purpose A13 radio set developed by Plessey in conjunction with the Signals Research and Development Establishment of the M.o.A. for military applications is now in full production and has been officially accepted by the British Armed Forces. Many accessories are available for the A13 making the



one-man pack, in its simplest form, into a mobile radio station.

Phase modulation is employed and is said to improve the equipment's range over that of amplitude modulated transceivers for a given power consumption. In fact, Plessey's claim an improvement of up to 30% in ground wave coverage is obtained for the same power consumption. Provisions are, however, made for a.m. working to enable the A13 to be used in current military systems. Provisions are also made for c.w. working and speeds of up to 25 w.p.m. are possible.

Simple free-running tuning is one of

the main features of this transistor transceiver, which covers 2 to 8 Mc/s and offers a choice of 2,400 (2.5 kc/s) channels. Calibration markers are provided at 100 kc/s and 10 kc/s intervals. The transceiver is powered by a 12-volt nickel-cadmium battery that can be quickly recharged from either a vehicle's

supply or from an ancillary hand generator. Output power of the transceiver is 1.5 watts, giving a working range in open country of five miles. With a transmit-receive ratio of one to nine the basic transceiver has an operational life of 8 hours per charging.

An r.f. power amplifier may be added to the simple one-man pack (as shown in the photograph) to increase the power output to 16 watts. Although this power amplifier has its own 12-volt battery, the operational life of the A13 is then reduced to 6 hours per charging, with a transmit-receive ratio of one to nine. The normal working range using the amplifier and a standard 8ft whip aerial

is 15 miles. Several other types of aerial are available, including two 150ft lengths of braid for long-distance working.

The basic unit is built on modular lines, making extensive use of printed circuit boards to simplify servicing.

Using another of the optional items, the harness adaptor unit, the A 13 will provide reliable vehicle communication. When installed, the equipment is powered from the vehicle's supply, via a regulator unit, another optional item. This provides a stabilized 14.4 volts from a nominal 24-volt source.

9WW 301 for further details

### TAPE/DISC UNIT

SUITABLE for use with most types of ancillary equipment for producing background music, is the new tape/disc unit Type G/CD2 from the Coventry Shop Equipment Company, of 66 Canterbury Street, Coventry, Warks.

A Planet half-track,  $3\frac{3}{4}$  in/sec tape deck is employed and—using 7-in spools with 2,400 ft of tape—offers four hours of non-repeat playing time. Automatic track reversal is provided, but no recording or fast wind facilities are included.

The associated disc deck is a Garrard Type 3,000 LM. Either a Ronette TX88 or one of the Decca Deram mono cartridges is fitted as standard.

A transistor power supply unit, to feed the tape head pre-amplifier and the relays, is also included in the



G/CD2, which measures  $20 \times 16 \times 13\frac{1}{2}$  in. Weight is approximately 40 lb.

The price ex works is £145. Ancillary equipment, including a range of Leak amplifiers in strong wooden cases, can also be supplied.

Several other items of equipment for producing background music, including one which has an integrated f.m. tuner, are available from the Coventry Shop Equipment Company.

9WW 302 for further details



## Hall Effect Devices

TWO field probes and two multipliers using Hall Effect techniques are being manufactured by the Electronics Group of Associated Electrical Industries Ltd., of Carholme Road, Lincoln. The semiconductor material selected for these devices is indium arsenide which offers stable performance over a wide temperature range and has good power efficiency characteristics.

The field probes comprise a thin semiconductor plate mounted on a beryllia backing which has a high electrical resistivity and a high thermal conductivity—equivalent to that of aluminium. Input and output resistance of the two devices is between 4 and 20 ohms, hence the effective output induction area is negligible, thus ensuring minimal a.c. pick-up from external sources. Power dissipation of up to 500 mW (200 mW for the smaller unit) can be tolerated, and with a field of 10 kilogauss, the Hall output is approximately 2.5 volts. Temperature coefficient for the two devices (designated field probe Mk. II and miniature

field probe Mk. III) is 0.1% per degree Centigrade (between 20°-60° C).

A semiconductor magnetic circuit combination, which accepts two inputs in the form of electrical currents (preferably from relatively high impedance sources), is used in the multipliers to obtain an output voltage proportional to their product at a level suitable for amplification by either valves or transistors. Two standard types of multiplier are available differing only in the nature of their coil windings; the Type A being suitable for valve circuits and Type C for transistor applications. Both types are potted in resin, and are fitted with an International Octal valve base.

In addition to their use in analogue computers and for power measurement, these multipliers can also be used in modulation and frequency changing circuits; producing a minimum of unwanted harmonics. Other possible uses are as linear or square law detectors, for frequency analysis and in d.c. to a.c. converters.

9WW 303 for further details

## SPEAKER ENCLOSURE

SPECIALLY designed for high fidelity enthusiasts with space problems is the "Minette" enclosure from Richard Allan Radio Ltd., of Bradford Road, Gomersal, Nr. Leeds, Yorks. This speaker unit is unconventional in as much as the duralumin front panel of the enclosure forms an integral part of the bass unit by supporting the cone assembly.

The bass unit is five inches in diameter and its cone is suspended on a flexible Neoprene surround, which is glued to the front panel and, in free air, resonates at 40 c/s. The magnet assembly of the speaker is attached to the front panel by four pillars and is claimed to overcome the normal chassis resonances. A ceramic magnet is used and provides a flux density of 14,000 gauss on a one-inch diameter pole and a total flux of 56,000 Maxwells.

The tweeter in this enclosure is a specially developed version of the 460T unit and has a flux density of 6,000 gauss on a 9/16-in pole, the cone being mounted on a Cambric suspension.

A five-element cross-over network is employed and brings the tweeter in at approximately 5 kc/s. The complete unit is said to have a flat response from 80 c/s to 12 kc/s, although the overall frequency response is quoted as 45 c/s to 20 kc/s. Continuous r.m.s. power rating is 6 watts and music power rating

is 10 watts. The overall dimensions of the "Minette," which costs £17 10s 6d, are 11½ × 7 × 6¼ in. Weight is 11 lb.

To meet the needs of the home constructor, it is hoped to market the front



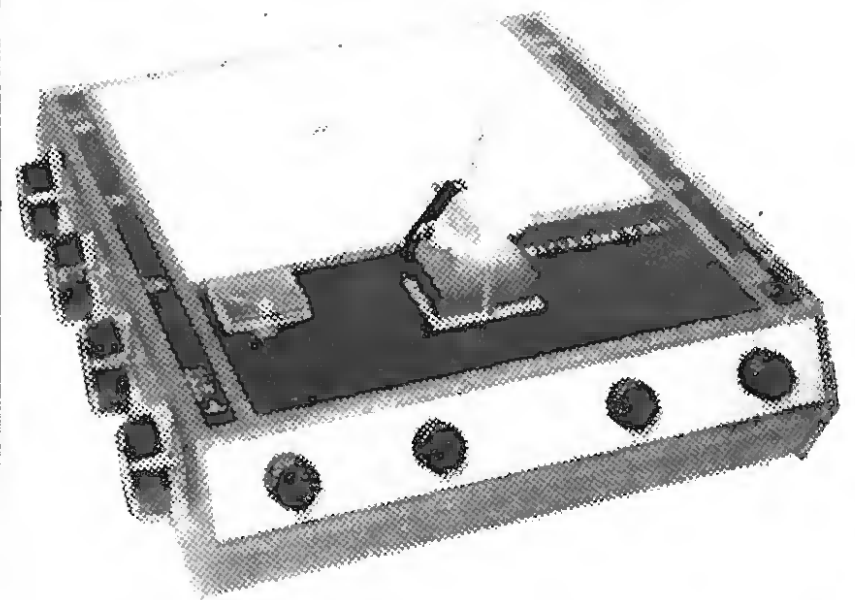
panel assembly, complete with speakers, but without the cabinet. The price has not yet been fixed, but it is understood it will be a little over half the complete price.

9WW 304 for further details

## R.F. BRIDGE

USING transformers to obtain accurate voltage and current ratios, to compare an unknown capacitance and conductance with internal standards, the new wide-range bridge by Wayne Kerr offers 0.1% accuracy for capacitance and conductance measurement between 100 kc/s and 1 Mc/s. This instrument, designated B201, can also be operated, but with reducing accuracy, up to 5 Mc/s. Capacitance range is 0.0001 pF to 0.1 μF and the conductance range is 0.001 μmho to 1 mho. Internal modulation is at 1 kc/s.

A neutral terminal is provided on the connection block that allows three ter-



minal measurements to be made if required. At present only 100 kc/s and 1 Mc/s source and detector units are available for the B201, but dummy units may be inserted to permit external equipment to be connected for measurements over the range 100 kc/s to 5 Mc/s. The B201 measures 5 × 12 × 12 in and weighs 12 lb.

The address of the Wayne Kerr Laboratories is Sycamore Grove, New Malden, Surrey.

9WW 305 for further details

## R.F. Phase Measuring Instrument

OPERATING in the 15 to 100 Mc/s range, the Teltronics Type PD 200 phase measuring instrument allows accurate phase shift measurement. Basically, the phase detector comprises a dual channel amplifier, which is used to detect by nulling the relative zero phase and amplitude of two input signals. The voltage standing wave ratio is 1.1:1 and gain adjustment is variable from +5 dB to -15 dB; input voltage range is from 250 mV r.m.s. to 500 V d.c.

A series of similar instruments operating up to 2 Gc/s made by the American company Teltronics are also available in the United Kingdom through Microwave Systems Ltd., of 9-10 River Front, Enfield, Middx. The U.K. price of the Model PD 200 is £319.

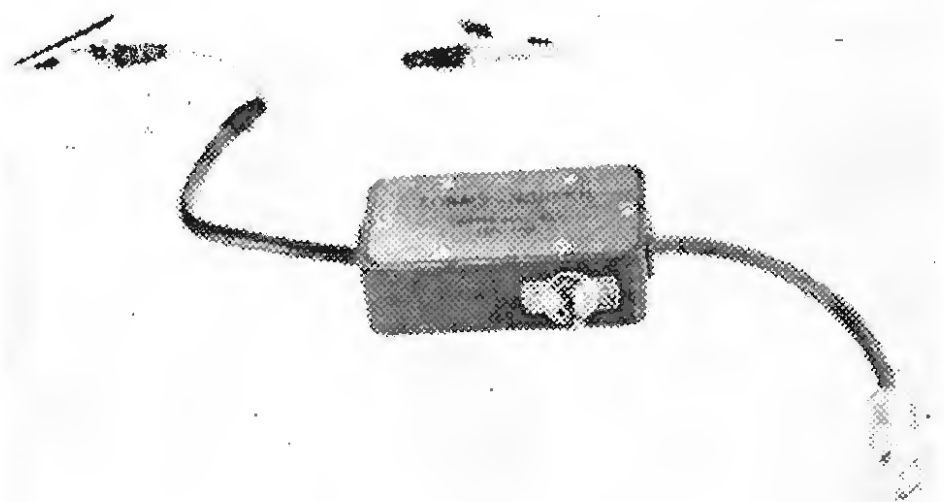
9WW 306 for further details



## Impedance Converter

AN impedance converter that allows low impedance test equipment to be used without loading the apparatus under test is being manufactured by Adams-Norcken Ltd., of Swindon. It comprises a unity-gain amplifier with an input impedance of  $8\text{ M}\Omega$  in parallel with  $1\text{ pF}$  and an output impedance of  $200\Omega$  in series with  $50\ \mu\text{F}$ . Bandwidth is from  $10\text{ c/s}$  to  $3\text{ Mc/s}$  and the dynamic range is 4 volts peak-to-peak.

Designated EPO-1, the emitter follower is claimed to have a linearity of better than 1.0%. Other specification details include a noise figure of  $20\ \mu\text{V}$  p-to-p when measured with an impedance of  $100\text{k}\Omega$ , and less than 0.25% har-



monic distortion when measured at 1 volt at  $10\text{kc/s}$ . Two Mallory Type TM175 cells are used to power the probe giving a working life of 80 hours in continuous operation.

As can be seen from the photograph, the probe is quite small and as standard, is fitted with a double screened BNC plug. Different connector and lead arrangements are available to order.

An encapsulated version for either wiring into equipment or for plug-in applications is available. This is known as the EPO-2 and is housed in a  $\frac{3}{4}$ -in diameter  $\times 1\frac{1}{2}$ -in long aluminium can. Neither batteries nor coupling capacitors are fitted to this unit, which is available with either solder pins for direct connection, Pins for printed circuit board connection, or with valve base pins.

Both of these units are marketed by Kynmore Engineering Co. Ltd., of 19 Buckingham Street, London, W.C.2. The EPO-1 probe costs £18 10s the encapsulated version EPO-2, whatever the pin arrangement, costs £8 12s.

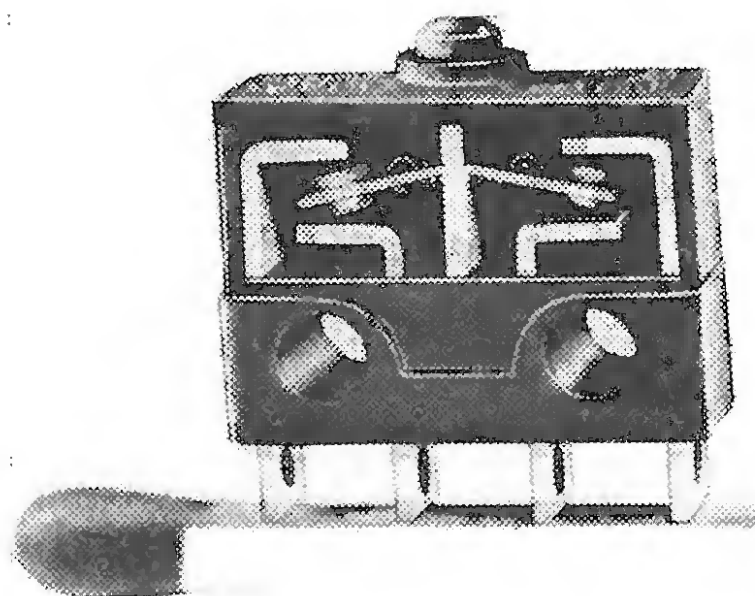
9WW 307 for further details

## SUB-MINIATURE MICRO-SWITCH

THE new micro-switch from Plessey, designated Type 18, is particularly suitable for applications where reliability in a small space is of vital importance, such as in aircraft and satellite projects. Although the dimensions of the Type 18 are only  $0.35 \times 0.2 \times 0.51$  in, it has a contact rating of 8 amps at either 250 volts a.c. or 30 volts d.c.

This micro-switch is manufactured under licence from the Licon Division of Illinois Tool Works Incorporated, U.S.A., by the Plessey Components Group at New Lane, Havant, Hants. A "butterfly" snap-action mechanism is employed to obtain a good changeover; mechanical life is in excess of  $10^6$  operations. Good vibration and shock resistance characteristics are claimed for the changeover mechanism. In fact Plessey tests at frequencies from  $10\text{ c/s}$  to  $2,000\text{ c/s}$  show no contact chatter at 25 g, even with the actuator depressed to within 0.0025 in of trip. Non-stressed ebrillium copper blades and stainless steel coil springs are used in the switching mechanism. The contacts are diffused gold plated.

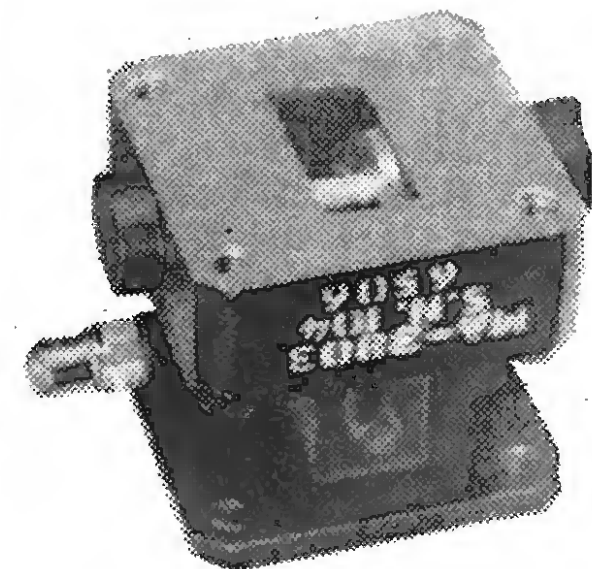
The case and cover (cut away to show the "butterfly" action in the photograph, which includes a match for comparison-purposes) are moulded in diallyl



phthalate. The Type 18 may be ganged if more than one circuit is required to be switched from the same actuator. Pre-travel plunger movement is 0.050 in and up to 0.10 in overtravel is permissible.

These switches are available from the Electro-mechanical Division, Plessey-UK Ltd., New Lane, Havant, Hants.

9WW 308 for further details



## X-Band TR-Limiter

BETTER receiver protection than that given by a TR tube alone, is claimed for the new TR-Limiter Type MA 3803 from Microwave Associates Ltd., of Cradock Road, Luton, Beds. In addition to a TR tube, this device contains a varactor diode, the action of which largely eliminates spike leakage (0.05 ergs) and, the makers claim, removes the major cause for crystal deterioration or burnout.

Compared with the normal TR tube, this unit has a similar insertion loss characteristic (0.8 dB) and has comparable dimensions ( $1.55 \times 1.64 \times 1.64$ ). Other specification details include a centre frequency in the range  $8.5$  to  $9.6\text{ Gc/s}$  with a bandwidth of  $\pm 100\text{ Mc/s}$ , an average power of 20 watts (peak 10 kW), recovery time of  $2\ \mu\text{sec}$ , v.s.w.r. of 1.3, noise ratio of 1.15, and a temperature range of  $-55^\circ\text{C}$  to  $+85^\circ\text{C}$ .

No additional power other than the "keep alive" electrode supply is needed and the protection claimed—particularly when a radar system is quiescent—is such that the device eliminates the need for a mechanical shutter.

9WW 309 for further details

## Low-loss Core Material

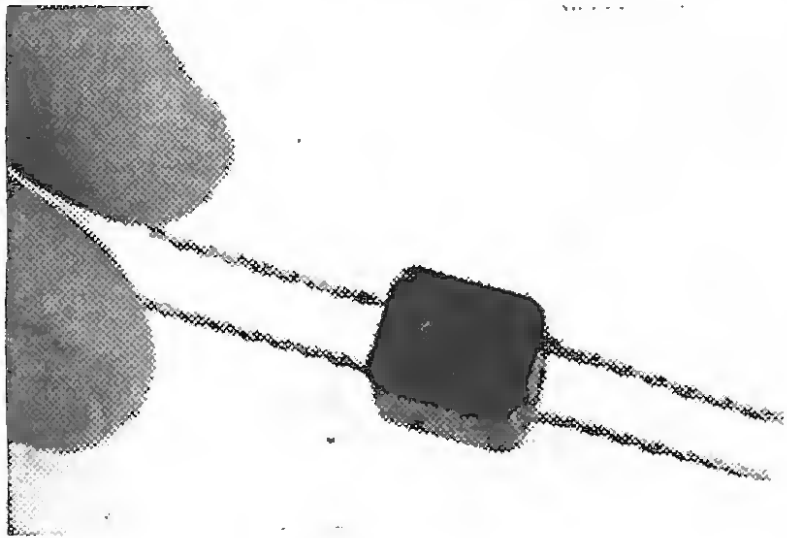
A NEW soft magnetic alloy core material, called Satmumetal and made by Telcon Metals, is characterized by low losses (about one quarter of those of silicon iron over the whole operating range of flux density up to 13,000 gauss) and a low magnetizing force requirement—again about one quarter of that for silicon iron. The magnetization curve extends beyond that of normal Mumetal to a flux density of 15,000 gauss. Permeability, varying with magnetizing force, ranges from an initial 40,000 to a maximum 250,000. Coercive force is 0.025 oersteds and remanence is 7,000 gauss. The new material, which at present is only in pilot production, is available in the form of 0.004-in thick tape of varying widths, for winding into toroidal cores.

9WW 310 for further details



## Compact Silicon Bridge Rectifier

MEASURING only 12×10×7 mm, the new silicon bridge rectifier offered by Mullard's has an input rating of 42 volts r.m.s. and will provide a rectified output of up to 50 volts at 0.5 amps. This encapsulated device has been designed for



use in the power supply sections of mains-operated radiograms, record players and tape recorders. The peak surge current for this bridge rectifier assembly, designated BY122, is 25 amps. 9WW 311 for further details

## Neon Indicators

THE number of high-intensity "Bright-life" neon indicators made by West Hyde Developments Ltd., of 30 High Street, Northwood, Middx., has been considerably increased and now includes units designed for  $\frac{3}{8}$ - and  $\frac{1}{2}$ -in hole mounting.

Those requiring  $\frac{3}{8}$ -in panel holes are made from polypropylene and the larger units are moulded in polycarbonate, a material which gives higher light transmission. Both types of material incidentally give sufficient glow from the rear to warn that equipment is live.

Three styles are available in each type of material with either clear, amber or red glow. The styles being dome, top-hat and square cap. Mounting is by means of a spring clip used to secure the indicator from the rear. Four other items complete the range: a neon, a neon with dropping resistor, a base with lead-out wires, and a neon with dropping resistor on a base.

Models are available to operate in the following ranges: 95 to 150, 160 to 260, and 270 to 500 volts a.c. or d.c. The average life of these indicators is quoted as 25,000 hours. Either six- or thirty-inch leads can be supplied.

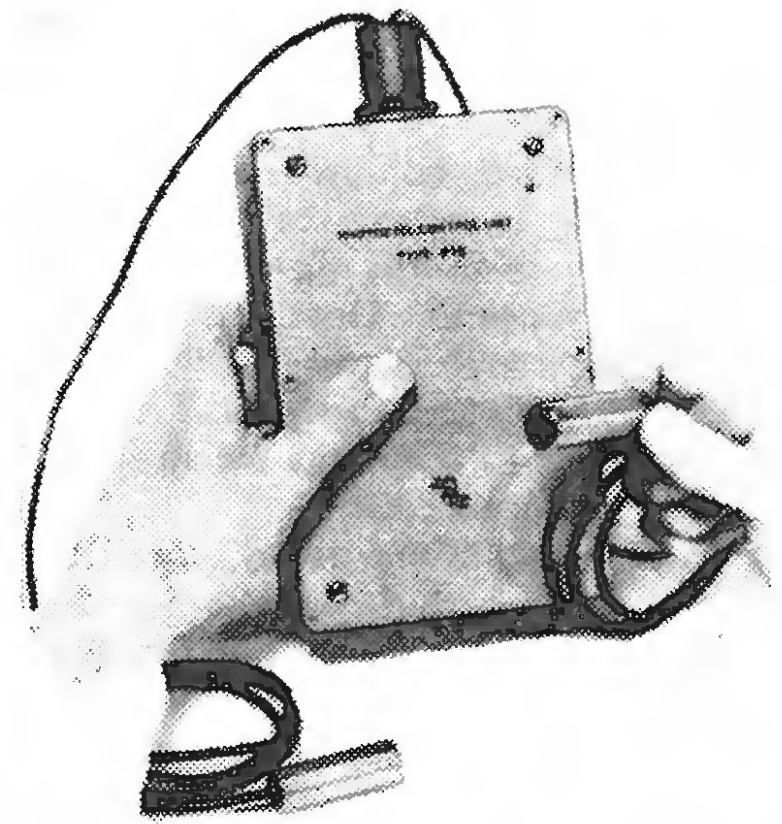
9WW 312 for further details

## PHOTO-ELECTRIC EQUIPMENT

ABLE to detect objects as thin as  $\frac{1}{16}$  in over distances of four feet, the new P 15 equipment being made by the industrial systems division of Electronic Machine Control Ltd. should find many applications in industry. As the illustration shows the equipment is quite small through the use of transistors.

The output of the unit when used in straightforward industrial applications, such as batchcounting, is sufficient to drive any counter directly without intermediate relays. However, for controlling external devices requiring relatively high currents—up to five amps, non-inductive—a changeover relay is provided in the standard equipment. A time delay can be incorporated if required.

This equipment is suitable for direct or reflected-light applications. Mounting clamps are available which allow the transmitting and receiving heads to be



adjusted to give the correct angle of incidence for any reflected light arrangement. The P 15 will operate from any 110 V or 200-250 V a.c. supply.

The ex works price of the P 15 is £22 10s and the company's address is Willow Lane, Mitcham, Surrey. 9WW 313 for further details

## Interpolated Data and Speech Transmission

APPARATUS that allows privately leased (two-pair) telephone lines to be used for the transmission of data while the lines are in use for the transmission of speech is being manufactured by the Integrated Electronics Systems Division of Standard Telephones and Cables Ltd., of Enfield, Middx.

According to tests undertaken by the Standard Telecommunication Laboratories, only 32% of the total transmission time of two-pair circuits is used in average speech communications. Most of the wastage (50% of the time) is due, of course, to the fact that only one direction is used at a time. The remaining

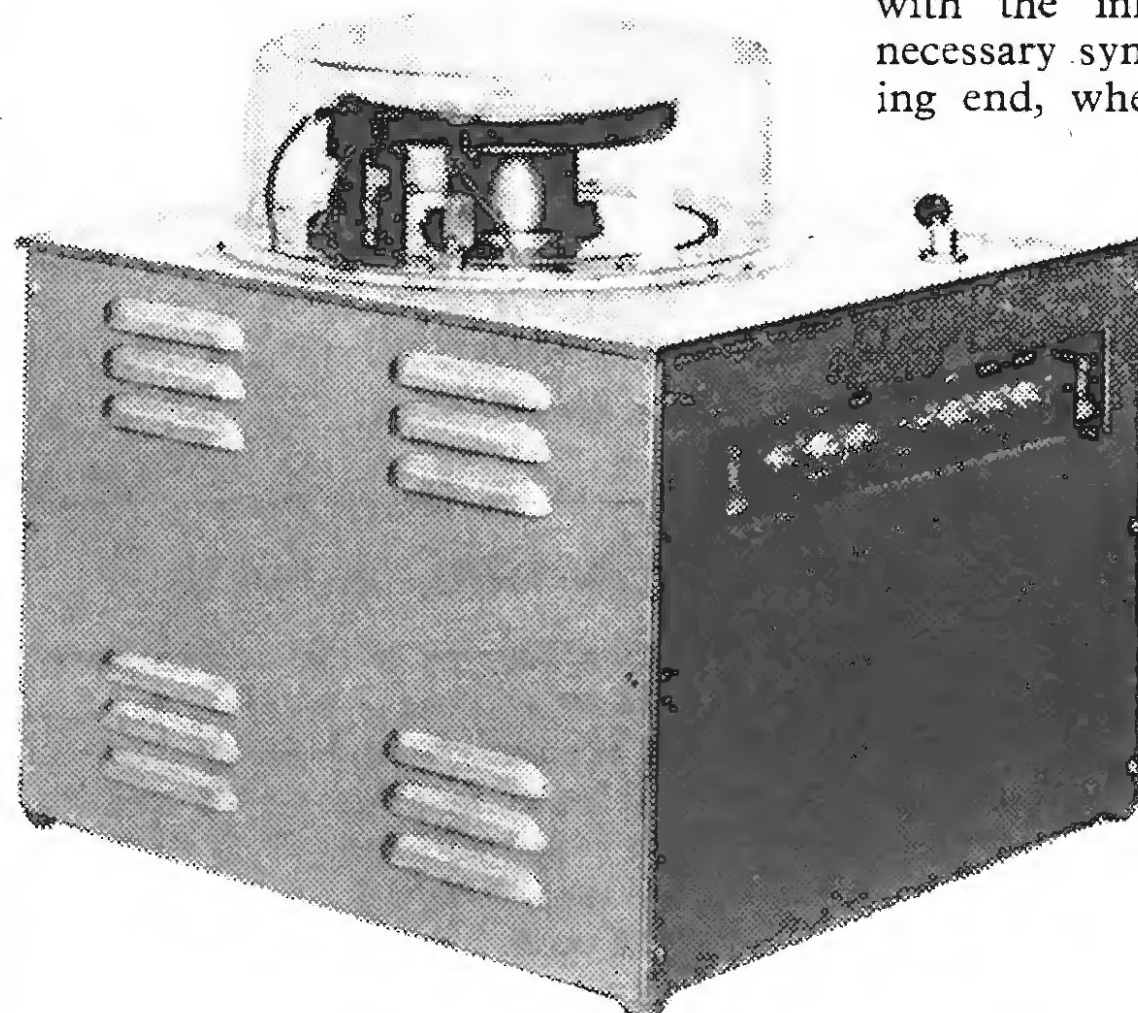
18% has been shown to be through gaps and pauses in conversation.

All but a few per cent of this unused time is utilized by the IDAST (Interpolated Data And Speech Transmission) system for the transmission of data. A circuit transmission efficiency of approximately 96% is quoted.

In order to be able to observe and act upon the quiet periods, the input speech is delayed, up to a maximum of 1/5 second, while pulses are generated for marking the beginning and end of the forthcoming speech period. In addition to this function, the generated pulses are used to switch either the data or speech on to the outgoing line. A tone is sent with the information to provide the necessary synchronization at the receiving end, where the incoming signal is

applied to parallel switch units, which head data and speech channels. This tone, which is transmitted only when speech is being sent, opens the speech channel and isolates the data channel. It can also be used to generate command signals for the data receiving equipment should this facility be required. A bandpass filter subsequently removes the tone from the speech.

9WW 314 for further details





## Closed-circuit TV Over Telephone Lines

A VIDEO intercommunication system that utilizes standard two-pair telephone lines is being offered by the Multitone Electric Company. This system, developed in conjunction with Visual Engineers Ltd., employs Grundig line amplifiers to make up for the limitations of telephone lines.

Two line amplifiers are required for a simple camera and monitor installation for distances of up to 2,500 metres. At the transmitting end, the associated line amplifier converts the asymmetrical video signal to a symmetrical one and also amplifies parts of the video signal to compensate for distortion and exponential cable losses. At the receiving end, a line amplifier is used to return the symmetrical signal to an asymmetrical one and also to further compensate for cable losses and correct any distortions.

The actual amplifiers in the Multitone system are designed to compensate for cable losses of up to 10 Mc/s, mak-

ing the system suitable for high-definition applications. Without the use of repeaters, Multitone claim that satisfactory pictures of moving subjects can be obtained over distances of 2,500 metres, and that a complete system can be remotely switched, through an automatic cross-bar telephone exchange, to allow any camera to be connected to any monitor in a private telephone circuit. With the use of repeaters, distances may be doubled.

The Multitone Sinus audio intercommunications equipment, which allows "hands-free conversation" and has been on the market for some time, has been integrated with the video system to allow a number of people to talk at the same time whilst watching a single picture.

The approximate prices of the various units are: monitors £250, camera heads (less lenses) £250, control units £250 and line amplifiers £200.

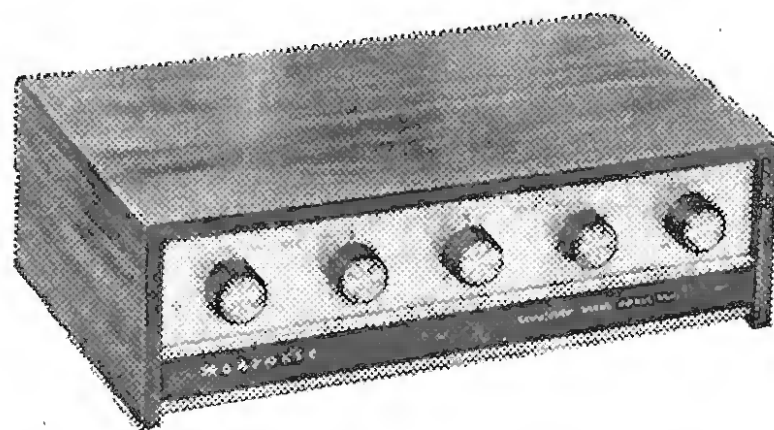
9WW 315 for further details

## Audio Mixer Unit

DESIGNED for use with a wide variety of amplifiers, tape recorders and other signal sources such as dynamic and crystal microphones and radio tuners, is the Heathkit Model TM-1 mixer unit. Two high sensitivity and high impedance channels and two of lower sensitivity and input impedance are provided on this transistor mixer. Each channel has its own, continuously variable, level control and when not in use is automatically earthed when the input plug is removed. A master volume control is provided.

The sensitivities, for an output of 200 mV r.m.s. are as follows: Channel 1, 1.5 mV with 1 M $\Omega$  input impedance and 4.5 mV with a nominal 2.5 M $\Omega$  input impedance (in the "XTAL" pickup position); Channel 2, 1.5 mV at 1 M $\Omega$ ; and Channels 3 & 4, 180 mV at 250 k $\Omega$ .

At full output frequency response is within  $\pm 3$  dB from 15 c/s to 30 kc/s and the distortion is less than 0.2%.



A music/speech switch, which in the speech position attenuates frequencies below 150 c/s, is fitted and has been found to be of benefit in public address applications where low frequencies often cause "boom" to occur. The power consumption at line voltage—9 volts d.c.—is approximately 6 mA. Dimensions are  $3\frac{3}{4} \times 11\frac{1}{8} \times 7\frac{1}{2}$  in and weight is 4 $\frac{1}{2}$  lb.

In kit form the price of the Model TM-1 is £11 16s 6d. Assembled and tested, it is available from Daystrom Ltd., of Gloucester, priced £16 17s 6d.

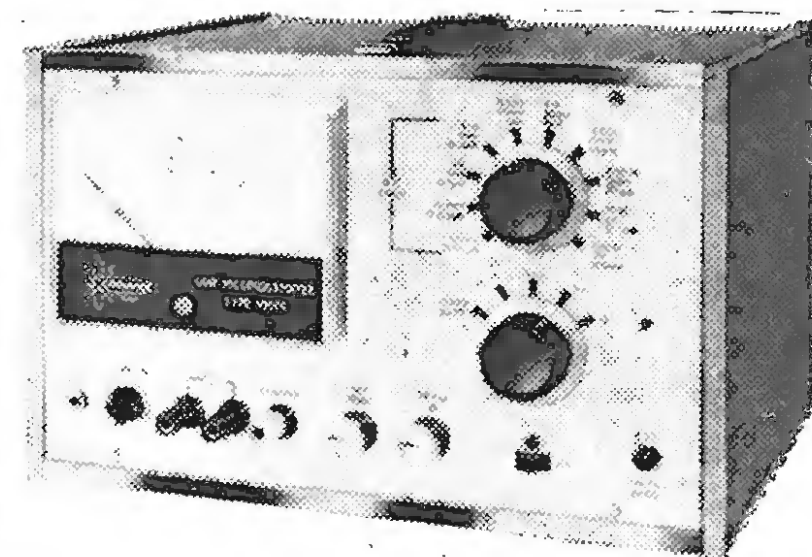
9WW 316 for further details

### INFORMATION SERVICE FOR PROFESSIONAL READERS

To expedite requests for further information on products appearing in the editorial and advertisement pages of *Wireless World* each month, a sheet of reader service cards is included in this issue. The cards will be found between advertisement pages 16 and 19.

We invite readers to make use of these cards for all inquiries dealing with specific products. Many editorial items and all advertisements are coded with a number, prefixed by 9WW, and it is then necessary only to enter the number(s) on the card.

Postage is free in the U.K. but cards must be stamped if posted overseas. This service will enable professional readers to obtain the additional information they require quickly and easily.



## U.H.F. MILLIVOLTMETER

A VERSATILE battery-operated millivoltmeter is announced by Advance Electronics Ltd., of Roebuck Road, Hainault, Ilford, Essex. This instrument, designated VM79, has six a.c. ranges covering 10 mV to 3 V f.s.d. and is suitable for use from 100 kc/s to 1 Gc/s.

Ten ranges are provided for d.c. measurement from 10 nA to 300  $\mu$ A f.s.d. Resistance measurements (1 $\Omega$  to 10 M $\Omega$ ) can be made on most types of circuitry with this instrument as the polarizing voltage is only 4 volts.

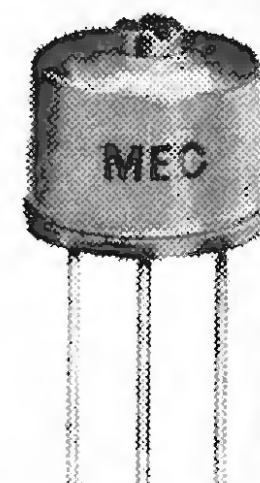
Readings are indicated on a four-inch meter which has separate scales for each facility. Accuracies quoted are as follows: a.c. voltage is  $\pm 3\%$  of reading with a v.s.w.r. of 1;  $\pm 2\%$  f.s.d. for d.c. voltage measurements;  $\pm 3\%$  f.s.d. for direct current measurements; and  $\pm 6\%$  (at mid scale) for resistance measurements. Among the accessories is a 50 $\Omega$  coaxial T probe (PL60) which will provide a v.s.w.r. of better than 1.2 (unbalanced input) over the frequency range 100 kc/s to 1 Gc/s.

A d.c. output suitable to drive an x-y recorder is provided on this instrument which measures  $7\frac{1}{2} \times 11\frac{1}{8} \times 9\frac{1}{2}$  in and weighs 10 $\frac{1}{2}$  lb. The price of the VM79 is £180.

9WW 317 for further details

## Potentiometer in TO-5 Case

SINGLE-TURN top adjustment is provided on the new Model T20P trimming potentiometer from Miniature Electronic Components Ltd., of Copse Road, St. John's, Woking, Surrey. Housed in a case with identical dimensions to the TO-5 transistor can, this device has  $\frac{1}{2}$  watt rating at 70°C. Resistance values of 50, 100, 200, 500 ohms, 1, 2, 5 and 10 k $\Omega$  are available for T20P. Temperature range is from  $-55^\circ\text{C}$  to  $+150^\circ\text{C}$ .



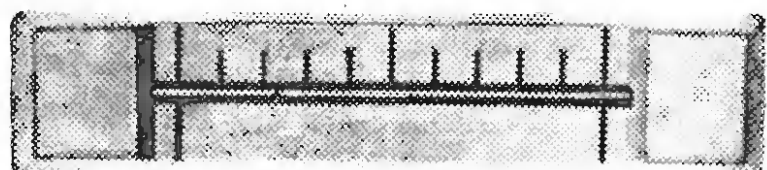
9WW 318 for further details



## Elapsed Time Indicator

A RANGE of small electrochemical ampere-hour meters, made by Curtis Instruments (U.S.A.), is now available from Miniature Electronic Components Ltd., of Copse Road, St. John's, Woking, Surrey. The basic model is the 150, which is less than 2 in long and the four versions available allow panel, printed board or socket (polarized or non-polarized) mounting.

A glass capillary tube (0.015 in dia. which allows the device to be used in any attitude due to the high surface tension of mercury) contains two columns of mercury separated by a gap of electrolyte—an aqueous solution of a soluble iodide salt and mercuric iodide. Nickel wire is used for the two electrodes. When a potential is applied across the electrodes, mercury at the anode is transferred to the cathode and as a result the gap moves from cathode to anode. The rate at which the gap



moves is, of course, proportional to the current-time integral and for a constant current the gap displacement is directly proportional to elapsed time.

For elapsed time measurement a series ballast resistor is used to determine the current which should not exceed 5 mA. A ballast resistor of 20-30 times the cell resistance (which is around a few hundred ohms) will swamp the positive temperature coefficient of the cell and reduce dependence on attitude. For a current of about 1  $\mu$ A the elapsed time is 10,000 hours and for 5 mA the corresponding time is 2.08 hours. The accuracy is  $\pm 2\%$ . With a swamp resistor, a current limiting resistor and a shunt Zener diode, the cell may be used with "rough" d.c. or a.c. Temperature range is  $-20^{\circ}\text{C}$  to  $+90^{\circ}\text{C}$ .

The coulometer may, of course, be used as a general purpose integrator and remote readout is possible by capacitive coupling or by optical means.

9WW 319 for further details

## "Press-Fit" Terminal

DESIGNED to save chassis area, the new feed-through from Sealectro Ltd. needs only 0.125 in diameter circular area on the chassis, but provides a minimum clearance above and below the chassis of 0.090 in. The body of this one-piece terminal, designated FT-SM-16L24, is of p.t.f.e.

The company's address is Walton Road, Farlington, Portsmouth, Hants.

9WW 320 for further details

WIRELESS WORLD, SEPTEMBER 1965



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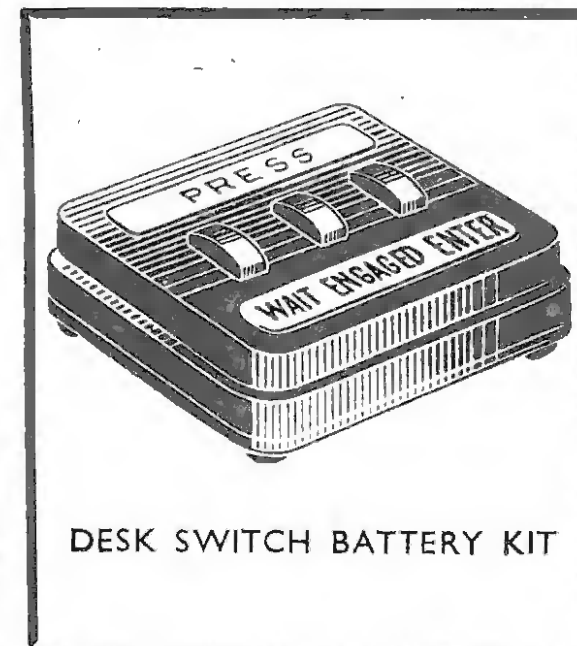
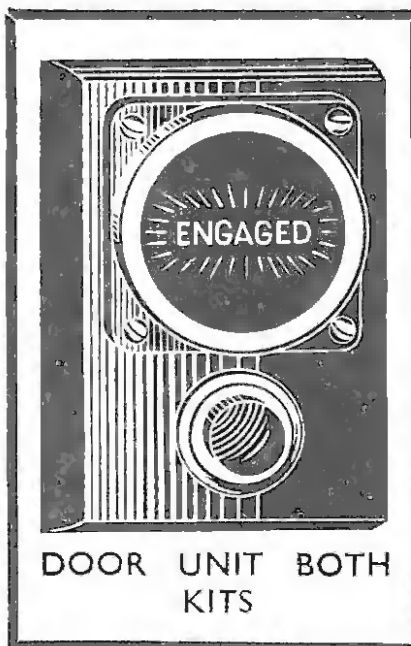
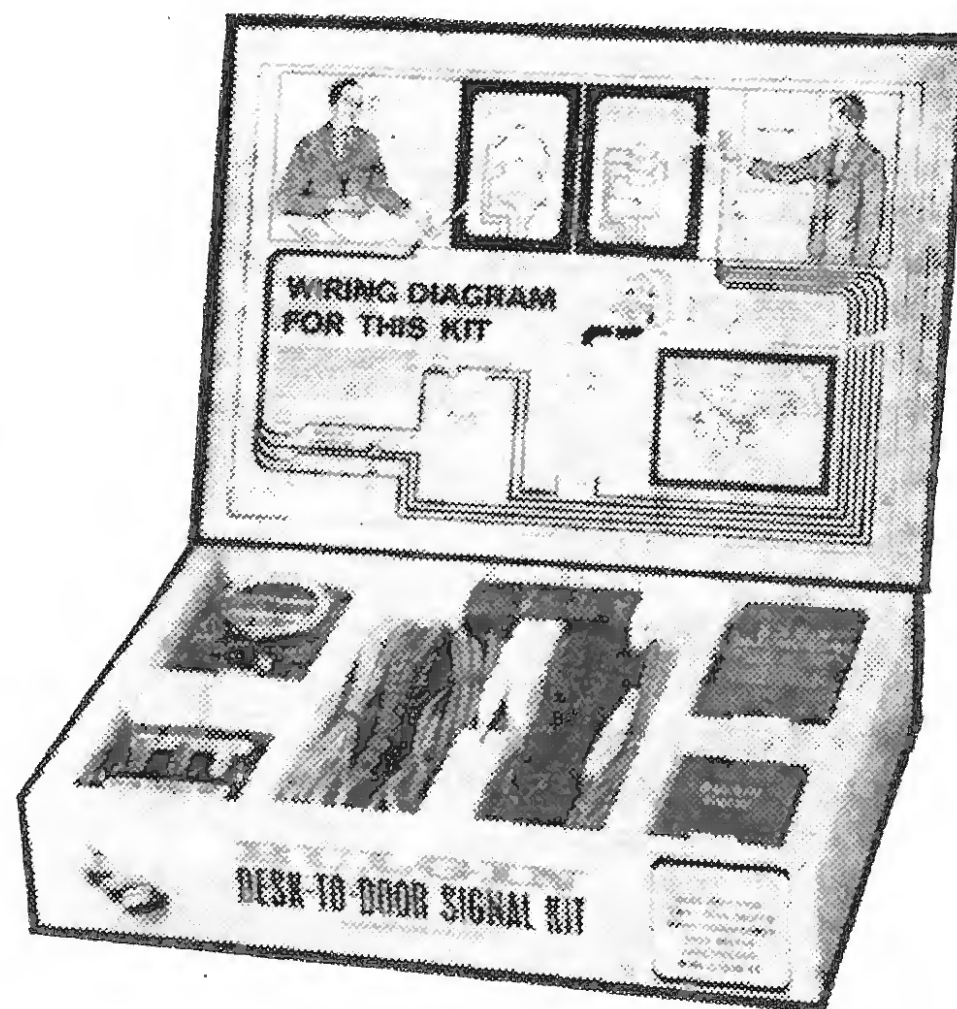
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WW-122 FOR FURTHER DETAILS.

## A Touch of the Auld Lang Synes

**B**ITTER experience teaches us that we can expect absolutely nothing of a day which starts with getting up in the morning. Armed with this philosophy one can, I find, accept the diurnal ration of slings and arrows of outrageous fortune with a fair percentage of stoicism. But, patently, some days are worse than others, and when a peremptory demand for me to attend upon the person of the Editor (no less) was delivered by express carrier pigeon, it became clear that no good could come of this one. Day, I mean, not pigeon.

To those who have had the good fortune never to have crossed the path of an Editor I should perhaps explain that it is a built-in characteristic of the race that they never demand audience in order to impart good news. The personal confrontation is traditionally reserved for matters of plague and pestilence, and so the sackcloth suit was the only possible choice of garments for the day.

Thus, in the fullness of time, after an initial interrogation at the portals of Dorset House, I was led, by a disdainful commercial equivalent of Jeeves, past cells crammed with galley-slaves until at length we hove to at the outer bastions of the *sanctum sanctorum*. Here I was received by the Editor's ravishing secretary.

Taking a compass bearing on entering the room I struck out for the hinterland and in due course came into sight of a massive desk supporting numerous telephones, with one of which the Editor was heavily entangled. He was, it seemed, at violent variance with a chap by the name of Caxton—a printer, I fancy—and as I made obeisance in the obligatory kneeling posture he slammed down the receiver and, snatching a sjambok, took off down the runway towards the doors without even a parting kick at what must have been, in the circumstances, a provocative target.

I mention all this in some detail to explain how I came to be browsing through vintage volumes of *W.W.* Being thus left *in vacuo* in a highly trepid state I approached the bookshelves which line the room from floor to ceiling, more in the hope of finding spirituous refreshment concealed behind the tomes than of imbibing mental refreshment from their contents\*. But no; all were apparently genuine, and thus it was that I found myself in company with the 1913-14 volume of *W.W.*, with nothing better to do than to read it.

Fascinating stuff. In those far off days I found that *W.W.* ran to 108 pages for 3d and that a wireless operator's uniform, complete with gold lace and gold buttons, could have been mine for 60s. Editorially, there were the familiar erudite articles, leavened with features like "Across Bolivia with a Portable set"; but would you expect to find poems? And not only did the readers get the muse for their thruppence, but, believe it or not, a cliff-hanger serial as well.

Yes, a genuine cliff-hanger. Technically slanted, of course. The hero was Charles, a vicar's son, who had invented a wireless-controlled airship complete with death-ray guns. Charles' other hobby was a girl-friend, the Squire's daughter (occasionally referred to in the narrative as Charles' lover, but not, it is to be trusted, in the modern connotation. Not in the vicarage, surely?). Gwen (that's the girl friend, familiarly known to Charles as "chicko") is

\* Judging from his description I think he must have found it.—ED.

described as "a bright intelligent girl, secretly a member of the Fabian Society." A member of that institution she might have been (and after all, every silver lining has its dark cloud), but the "bright and intelligent" bit is suspect, since she persuades Charles to let her have a go at the controls and promptly graunches the prototype airship straight into the potting shed.

Other *dramatis personae* include Doss and Suk (sic) a brace of unwashed pedlars, described as being "for ever on the prowl," and M. Dupont and Herr Buelner who are—guess what? That's right; secret agents for a foreign power.

I can't tell you all the ramifications of the plot, except to say that in the end Gwen atones by taking over the control tower and knocking out the entire invading German air force by radio control, deputising for Charles who had inconsiderately contracted a nervous breakdown at the critical hour when England had need of him. True love wins through and in the final scene we find Charles and Gwen abandoning radio control and going over to manual as they walk down the aisle together.

And when you come to think of it, and considering that World War I hadn't started, that story wasn't at all a bad forecast of what was to happen in 1940, if you substitute radar control for radio.

Letters to the Editor were mostly in the form of queries to which a reply was given, and some of these were pretty terse. One hapless correspondent, identified by the initials H. L. N., had his letter held up as a horrible example to others, and was told, *inter alia*, "... You ask too much . . . a full answer would approximate to the size and value of a text-book . . . . You are infinitely too vague . . . . Half your troubles would be removed if you would take the advice we have repeated over and over again—USE A WAVEMETER . . . . You have no possible right to use gas pipes as an earth and if you persist we run the risk of never hearing from you again . . . ."

Which just shows what a superman an Editor must be. We weaker vessels would have encouraged the impossible H.L.N. to make his earth connection on to as many gas pipes as he could find . . . . "Excellent results are obtained by perforating the main in one or two places and soldering the lead into position with the aid of a blow torch . . . ." But not the Editor. He knows that H. L. N. is the bed of nails which an inscrutable Providence has given him to lie upon, and accordingly he goes to the utmost lengths to keep the points sharpened. Of such stuff are demi-gods made.

To those Doubting Thomases who think that I have been making this up I extend my forgiveness and commend them to the library of the British Museum. And in browsing through the volumes, look also at the technical articles therein, and you may, like me, come to the conclusion that the old-timers were not nearly so far back into the Flintstone era as we are prone to think. But perhaps more of that another time.

Oh yes—just for the record—it eventually transpired that the Editor (the 1965 edition, I mean, not the 1913 one) hadn't wanted me at all, but had merely demanded to see a certain adjectival vector diagram which was in course of preparation for an article.



# ANOTHER STEP FORWARD

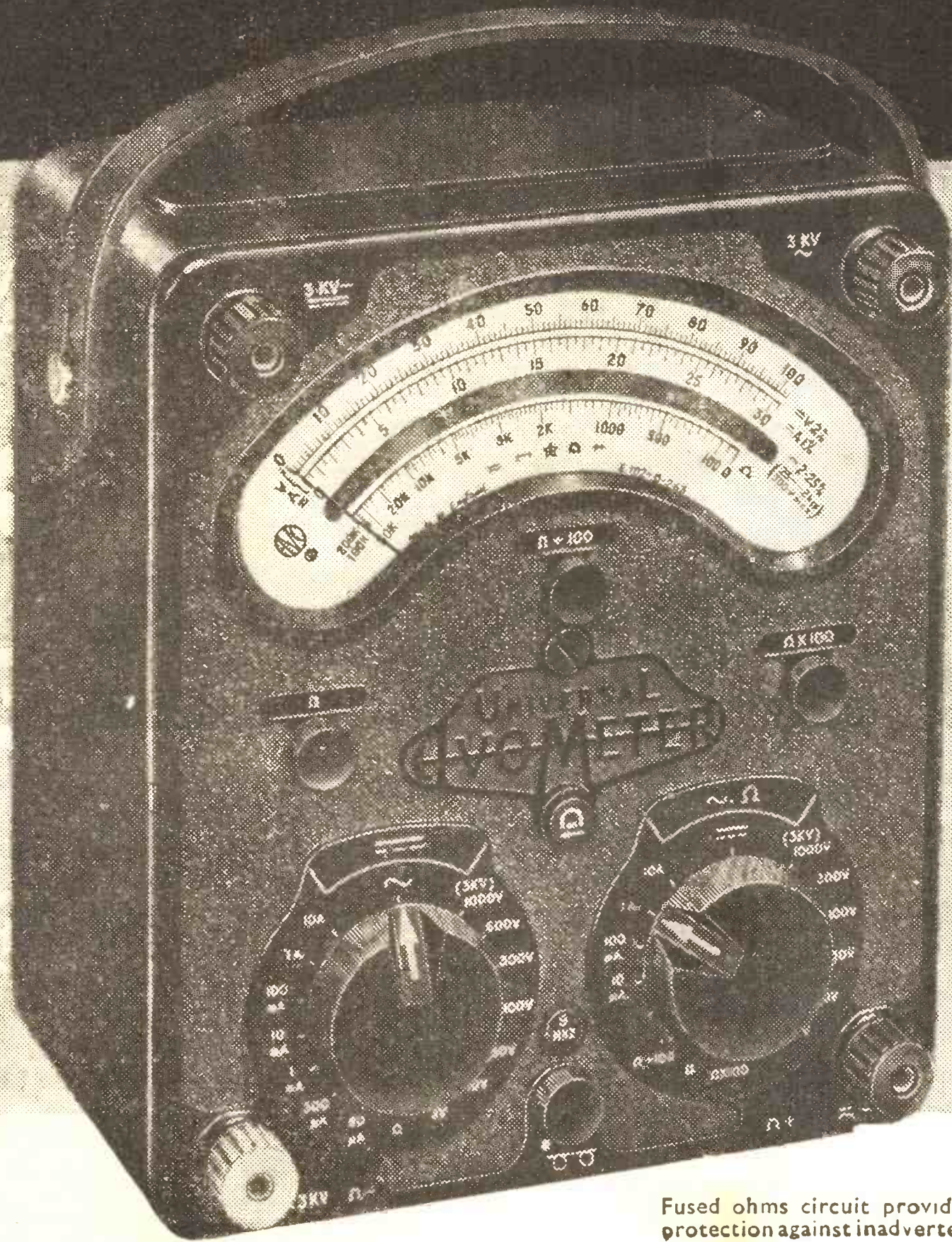
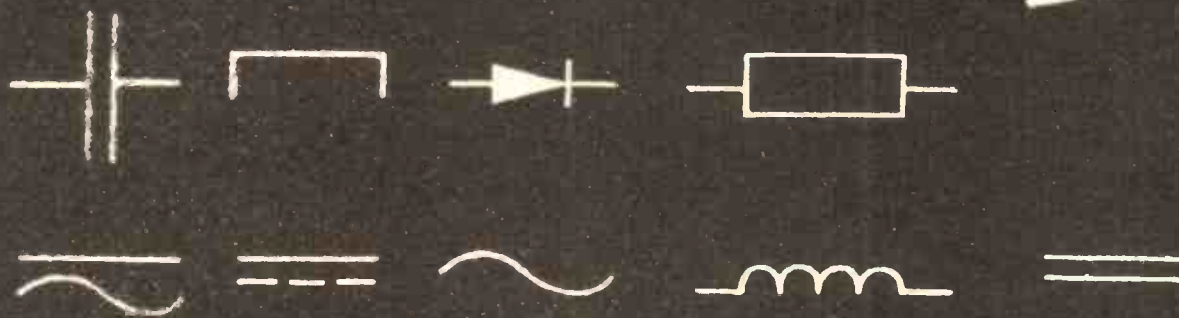
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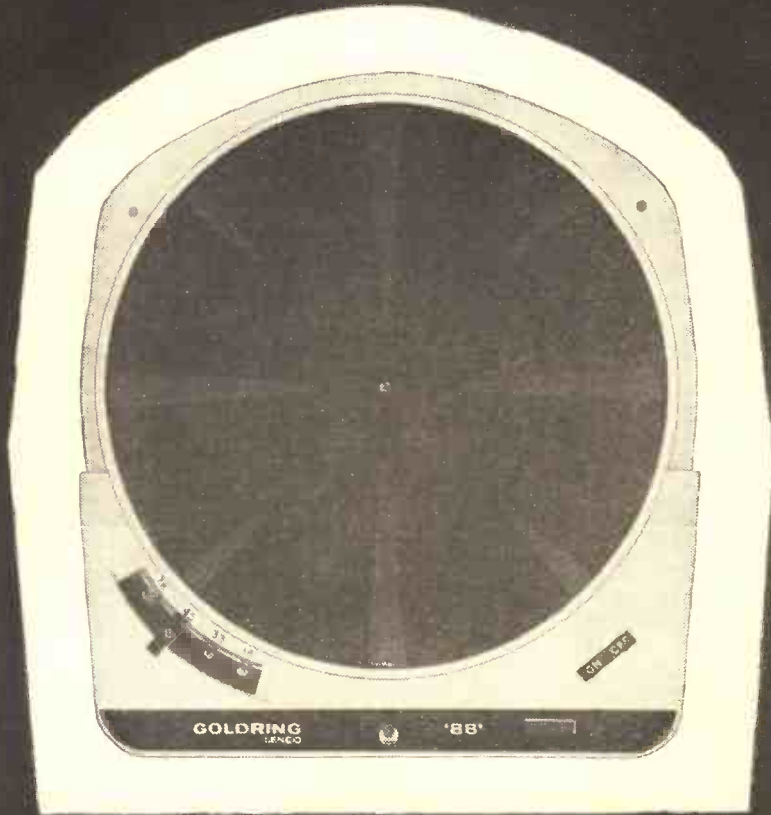
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# The shapes of sound



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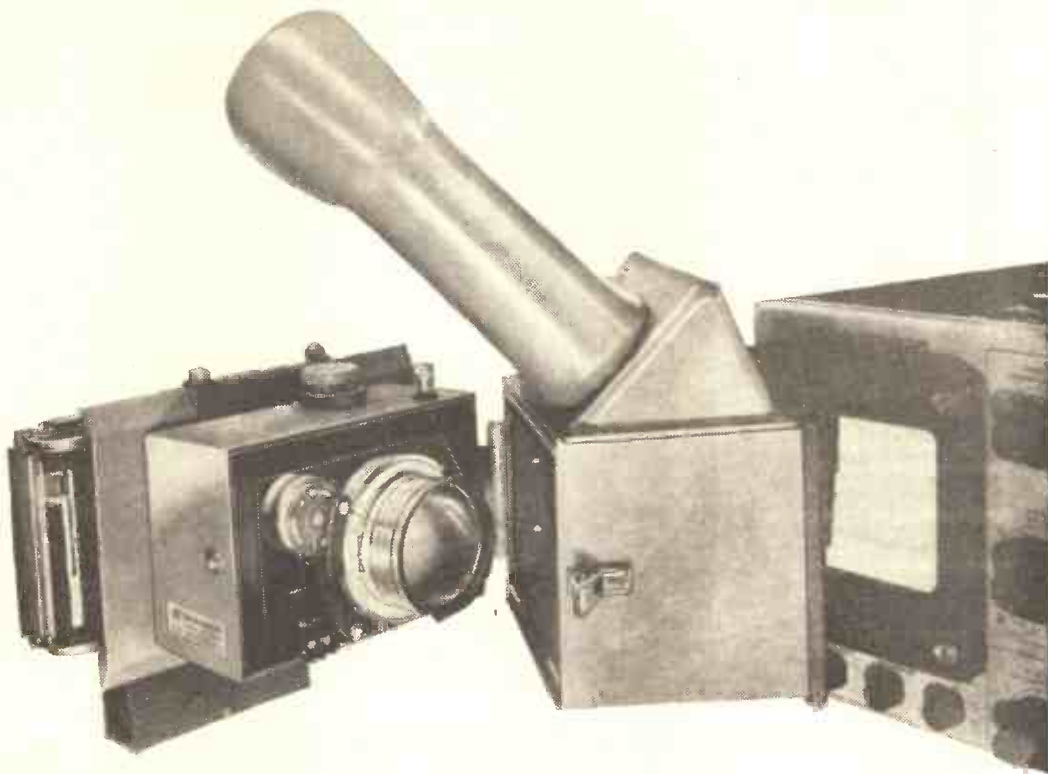


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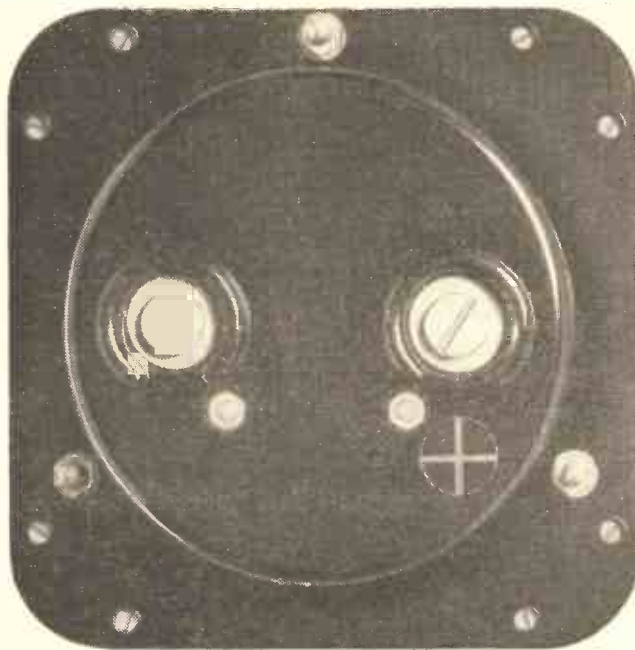
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- Smart new hammered grey finish.

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### THE NEW FULL RANGE HIGH FIDELITY LOUDSPEAKERS



**AXIOM 201**  
12 inch-15 watt-15 ohms  
Frequency range: 30-16,000 c/s  
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12 inch-20 watt-15 ohms  
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**TRIAXIOM 1220c**  
12 inch-20 watt-15 ohms  
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**AUDIOM 51 BASS**  
12 inch-15 watt-15 ohms  
**PRICE £9.12.5.**



**AUDIOM 61 BASS**  
12 inch-20 watt-15 ohms  
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... and Marconi Instruments use it at every stage of panel layout and design. *Handleability* is seldom specified, but ergonomics is a very special study at St. Albans.

Look at any instrument in the new '2000 Series'. That light grey panel colour was not chosen—it was *formulated* to give maximum legibility to lettering. Combined controls are linked to give integrated readings, and link lines have explanatory legends clearly engraved. All controls are positioned for logical sequences of operation, colour-coded and conveniently spaced. Bar knobs are used for switches and milled knobs for variable controls—both types designed and made in the factory because those precise shapes and sizes were found to be *best* for each purpose.

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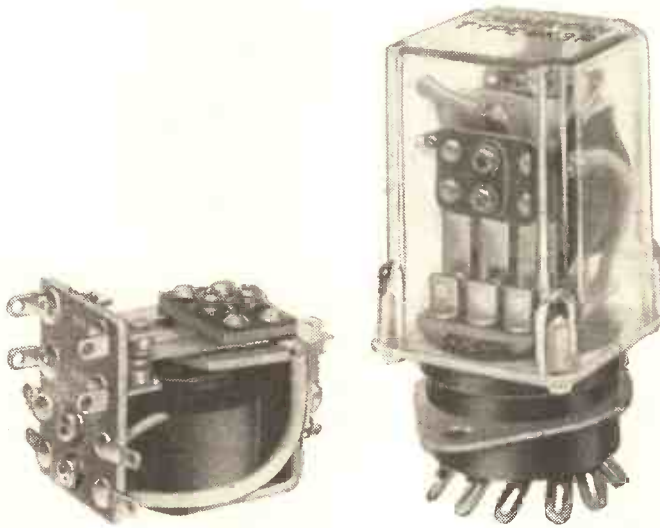
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### 5in. Flat-face GENERAL PURPOSE OSCILLOSCOPE Model 10-12U

An outstanding oscilloscope

"Y" sensitivity 10 mV, r.m.s. per cm. at 1 kc/s. bandwidth 3 c/s.-4.5 Mc/s. Frequency compensated input attenuator X1, X10, X100. T/B. 10 c/s.-500 kc/s. in 5 steps. Two extra switch selected pre-set sweep frequencies in T/B. range. T/B. output approx. 10 v. peak to peak. Built-in IV calibrator. Facility for "Z" axis modulation. Electronically stabilised power supply. Power req. 200-250 v. A.C., 40-60 c/s. 80 watts. Fused. Front panel silver and charcoal grey. Cabinet, charcoal grey, size 8 $\frac{1}{2}$  × 14 × 17in. deep. Net weight 23lb. 56-page construction and operation manual.

Kit.....£35.17.6 Assembled £45.15.0

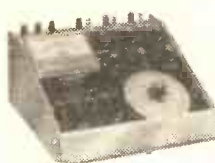


### Transistorised REGULATED POWER SUPPLY Model IP-20U

Tremendous value! 0.5-50 volts D.C. output at up to 1.5 A. Voltage or current monitored on easy-to-read meter. Adjustable current limiter.

Relay protected against overload. Less than 150 microvolts ripple. Regulation less than  $\pm 15$  millivolts. Output impedance less than 0.1 ohm. Compact 9 $\frac{1}{2}$ in. × 6 $\frac{1}{2}$ in. × 11in. Weight 11lb. net. Full details on request.

Kit.....£35.8.0 Assembled £47.8.0



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Unmatched for quality and performance at the price.

Provides a complete d.c. analysis of PNP and NPN transistors and diodes. D.C. gain (Beta, Alpha) is read direct on calibrated scales. Four lever switches facilitate fast, easy, test selection. Internal batteries for tests up to 9 v. Provision for connection to ext. power supply for higher

voltage and current tests. Modern functional styling. Size 5 $\frac{1}{2}$ in. high × 10 $\frac{1}{2}$ in. deep × 10 $\frac{1}{2}$ in. wide.

Kit.....£24.18.0 Assembled £35.10.0

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Modern styling. Extra features. The ideal VVM for the Electronic Engineer. 6in. Ernest Turner 200 $\mu$ A. meter with multi-coloured scales. Unique gimbal bracket allows bench, shelf or wall mounting. Measures A.C. (r.m.s.), D.C. volts 0-1.5, 5, 15, 50, 500, 1,500. Resistance range 0.1 to 1,000M $\Omega$  with int. battery. Vernier-action zero and ohms adjustment. Roller-tinned printed circuit. High input resistance (11M $\Omega$ ). Comprehensive assembly and operation manual. Size 5 × 12 $\frac{1}{4}$  × 4 $\frac{1}{4}$ in. Complete with test prod and leads.

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H.V. and R.F. Probes available as optional extras.

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### "STARMAKER" P.A. AMPLIFIER Model PA-1

A multi-purpose, high output, compact unit, suitable for vocal and instrumental groups, guitars, electronic organs etc. 4 inputs for guitars, microphones, record players. Has many features found only in expensive equipment, i.e. 50 watt Amplifier, two heavy duty speakers, "Magic Eye" volume indicator, variable tremolo, modern elegant cabinet.

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9 watts per channel. Within its power rating this amplifier is the finest available, regardless of price. Features include: Inputs for stereo/mono; Gram, Radio and Tape; sensitivity to meet the requirements of any pick-up; push-button selection; variable filter for optimum performance; excellently styled in two-tone grey perspex panel with golden surround and matching knobs. Suitable for cabinet mounting or as a free-standing unit. Size 13 $\frac{1}{2}$ in. × 4 $\frac{1}{4}$ in. × 12 $\frac{1}{2}$ in. deep.

Kit.....£28.9.6 Assembled £38.9.6.

## MODELS FOR THE MUSIC LOVER AND FOR FAMILY ENTERTAINMENT

### "OXFORD" LUXURY TRANSISTOR PORTABLE Model UXR-2

This superb transistor radio is the ideal domestic or personal portable Medium and Long Wave receiver. Solid leather case and handle. Easy-to-read tuning scale. Extra large loudspeaker. Push button L, MW and tone. 10 semi-conductors (7 transistors plus 3 diodes). Sockets for personal earphone, tape recorder, car aerial. Internal 9-volt battery (not supplied), lasts for months. Latest printed circuit techniques.

Comprehensive, easy-to-follow, fully illustrated Instruction Manual.

Kit.....£14.18.0 incl. P. Tax.

Assembly can be arranged on your behalf.



### A WELL DESIGNED F.M. TUNER Model FM-4U

Tuning range 88-108 Mc/s. Flywheel tuning. Attractive Plastic Front Panel in two-tone grey with golden trim surround and motif. Thermometer type visual tuning indicator. Pre-aligned. I.F. transformers. Three I.F. stages, Wide-band low distortion Ratio Detector. R.F. Unit, wired, tested and pre-aligned. Printed circuit for I.F. Amplifiers and Ratio Detector. Built-in power supply. Output sockets for stereophonic adaptor (for stereo transmission when available).

TUNER UNIT Model FMT-4U with 10.7 Mc/s. I.F. output, £2/15/- (inc. P.T.). I.F. AMPLIFIER and power supply Model FMA-4U complete with case and valves, £13/13/- Sold separately.

Kit Total ..... £16.8.0

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**TRANSISTOR MIXER**  
Model TM-1

"A must for the tape enthusiast"

Four channels with individual, continuously variable controls, plus a master volume control allows model to be used for recording from a wide variety of sources. e.g. dynamic and crystal microphones, radio tuners, record players, etc.

- ★ 7 transistor circuit and internal 9 v. battery (not supplied) allows unit to be used "in the field" as well as in the home, studio, etc.
- ★ Printed circuit board ensures consistent performance, easiest possible construction.
- ★ Professional, modern, compact, low silhouette styling.
- ★ Beautiful walnut veneered, fully finished cabinet.
- ★ Attractive anodised aluminium front panel.
- ★ Size: 11 1/2 in. x 7 1/2 in. x 3 1/2 in. high.

KIT £11.16.6 Assembled £16.17.6

Full specification leaflet sent on request.

The Outstanding  
**20+20 WATT TRANSISTOR**  
**STEREO AMPLIFIER**  
Model AA-22U



This "International Class" amplifier offers you a realism and beauty of music never before obtainable at such a competitive price.

- ★ Professional, elegant, compact, slim-line styling.
- ★ The best of American transistor techniques in a British amplifier.
- ★ Beautiful walnut veneered, fully finished cabinet will harmonise with domestic furnishing schemes.
- ★ 5 stereo inputs (five on each channel) accommodate pick-up, radio tuner, tape and two other sources.
- ★ 20 transistor 10 diode circuit.
- ★ Dimensions: 15 1/2 in. wide x 3 3/4 in. high x 12 1/4 in. deep.

Kit £43.18.0 Assembled £68.16.0

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COMPARE ANY HEATHKIT MODEL FOR PRICE, PERFORMANCE, QUALITY

**6 W HI-FI STEREO AMPLIFIER**  
KIT Model S-33H

An inexpensive stereo-mono amplifier with the high sensitivity necessary for lightweight miniature ceramic pick-ups (e.g. Decca Deram). De Luxe version of the S-33 with attractive two-tone grey Perspex panel.

Kit £15.17.6 Assembled £21.7.6

**5 W HI-FI MONO AMPLIFIER**  
KIT Model MA-5

A low-priced general purpose Hi-Fidelity amplifier based on the popular S-33 for those who do not require a stereophonic system. Separate bass and treble controls. Gram and Radio inputs. Suitable for most crystal pick-ups. A printed circuit simplifies construction.

Kit £10.19.6 Assembled £15.10.0

**HI-FI MONO POWER AMPLIFIER**  
KIT Model MA-12

A compact Hi-Fidelity power amplifier (including auxiliary power supply). 12 watts output. Wide frequency range and low distortion. A variable sensitivity control is fitted enabling it to be used with an existing amplifier in a stereophonic system. Other applications include sound reinforcement systems, transmitter modulators, for use with tape recorders, also as a general purpose laboratory amplifier.

Kit £11.18.0 Assembled £15.18.0

**STEREO CONTROL UNIT KIT**  
Model USC-1

Incorporates all worthwhile features for Hi-Fidelity stereo and mono. Push-button selection, accurately matched ganged controls to ±1 dB. Negative feedback rumble and variable low-pass filters. Printed circuit boards. Accepts inputs from most tape-heads and any stereo or mono pick-up.

Kit £19.10.0 Assembled £26.10.0

**HEATHKIT-THOMAS (Transistorized) ELECTRONIC ORGAN KIT**  
Model GD-232BE

Can be built with no knowledge of electronics. Bench £14.10.0 (Surcharge extra)



**HI-FI EQUIPMENT CABINETS**

A range of equipment cabinets is now available. Designed for maximum operating convenience or for where room space is an over-riding consideration, this range includes easy-to-build kits or ready-assembled cabinets in the white for finish to own requirements.

- "MALVERN" (illustrated) Kit. £18.1.0 (inc. P.T.)  
Assembled (left in the white) £23.6.0
- "GLOUCESTER" Mk. 1 for Tape Deck or Record Player  
Kit £17.3.6 (inc. P.T.) Assembled £22.8.6
- "GLOUCESTER" Mk. 2 for Tape Deck and Record Player  
Kit £18.10.0 (inc. P.T.) Assembled £23.15.0
- "CHEPSTOW" for Record Player or Tape Deck.  
Kit £11.12.6 (inc. P.T.) Assembled £16.17.6

**How to install Hi-Fi in YOUR home**

If you are planning to install a Hi-Fi system in your home, and are uncertain of the type of equipment to use, our widely experienced technical staff will with pleasure put forward recommendations. All you have to do is state the type of installation contemplated, the price you are prepared to pay and give details of existing equipment you wish to include, if possible.

**6 W STEREO AMPLIFIER KIT**  
Model S-33

A versatile high-quality self-contained STEREO Amplifier with adequate output for a living room. 3 watts per channel: 0.3% distortion at 2.5 w/channel; 20 dB N.F.B., inputs for Radio (or Tape) and Gram, Stereo or Monaural; Ganged controls. Sensitivity 200 mV.

Kit £13.7.6 Assembled £18.18.0

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**MONO CONTROL UNIT KIT**  
Model UMC-1

Ideal for use with MA-12 or similar amplifier. Output 0.25 v. Send for full details.

Kit £8.12.6

Assembled £13.12.6

**HI-FI SPEAKER SYSTEM KIT**  
Model SSU-1

Ducted-port bass reflex cabinet "in the white." Frequency response is 40-16,000 c/s. Power rating 10 watts. Matched speaker units 8in. high flux (12,000 lines) with hyperbolic cone and 4in. wide angle dispersion type for higher frequencies.

Kit (with legs) £12.12.0 (Less legs) £11.17.6 (inc. P.T.)

**"COTSWOLD" SPEAKER SYSTEM KIT**

This acoustically designed enclosure measures 26 x 23 x 14 1/4 in. and houses a special 12in. base speaker with 2in. speech coil, elliptical middle speaker together with a pressure unit to cover the full frequency range of 30-20,000 c/s. Its polar-distribution makes it ideal for really Hi-Fi Stereo. Delivered complete with speakers, cross-over unit, level control, grille cloth, etc. Left in the white for finish to personal taste, all parts are pre-cut and drilled for ease of assembly.

Kit £25.12.0

Assembled £33.17.0

**"COTSWOLD M.F.S." SPEAKER SYSTEM KIT**

This model, based on the standard Cotswold, measures only 36in. high, 16 1/2 in. wide by 14in. deep. Particularly recommended to those who require the best results in small rooms.

Kit £25.12.0

Assembled £33.17.0

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## HARMONIC DISTORTION METER. Model IM-12U

Harmonic distortion measurements no longer need complex, costly equipment!

- ★ Simple to use! High quality! Low cost!
- ★ 20 c/s. to 20,000 c/s in three ranges.
- ★ Distortion is read directly on a 4½in. meter.
- ★ An ideal companion for our Audio Generator Model AG-9U.



- ★ Meter scales calibrated in V.r.m.s., % distortion and dB.
- ★ Measures noise levels down to -60dB.
- ★ Quality components for precision measurement.
- ★ Saves £6s over comparable units.

### MULTIMETER KIT Model MM-1U

Provides wide voltage, current, resistance and dB ranges to cover hundreds of applications. Sensitivity 20,000 ohms/volt D.C. and 5,000 ohms/volt A.C. Ranges: 0.15 v. to 1,500 v. A.C. and D.C.; 0.150μA. to 15 A. D.C. Measures resistance from 0.2Ω to 20MΩ. 4½in. 50μA meter. A polarity reversing switch eliminates transferring test leads when alternately measuring + and - voltages.



Kit £12.18.0

Assembled £18.11.6

### OSCILLOSCOPE TRACE DOUBLER KIT Model S-3U



This device will extend the use of your single-beam oscilloscope and, at a nominal cost, will give you the advantages of a double (or other multiple) beam scope.

Kit £12.18.0

Assembled £18.10.0

### R.F. SIGNAL GENERATOR KIT Model RF-1U



Provides extended frequency coverage on six bands from 100 kc/s, to 100 Mc/s on fundamentals and up to 200 Mc/s on calibrated harmonics.

Kit £13.8.0

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### DECADE RESISTANCE BOX KIT Model DR-1U.

Range 1-99,999Ω in 1Ω steps. Ceramic switches throughout. Current rating from 500 mA. to 5 mA. according to decades in circuit. Polished wooden cabinet supplied complete.

Kit £10.8.0

Assembled £14.8.0

### RESISTANCE-CAPACITANCE BRIDGE KIT Model C-3U



Measures capacitance 10pF. to 1,000μF. Power factor and resistance 100Ω to 5M ohms. Test voltages 5-450 v. Safety switch provided.

Kit £10.10.0 Assembled £16

### AUDIO SIGNAL GENERATOR KIT Model AG-9U



10 c/s. to 100 kc/s., switch selected. Distortion less than 0.1%. 10 v. sine wave output metered in volts and dB's.

Kit £22.10.0

Assembled £30.10.0

Will give fast, accurate noise and distortion measurement in amplifiers, receivers, transmission lines, speakers, etc. Measurements are read directly on large meter. High input impedance. Freq. 20 cycles to 20,000 cycles. Distortion: 1, 3, 10, 30, 100% f.s.d. Voltmeter: 0, 1, 3, 10, 30 volts f.s.d. Dimensions: 13in. x 8½in. x 7in. deep, weight 11lb.

Kit £24.15.0 Assembled £34.0.0

### A.M./F.M. TUNER KIT

Tuning range 88-108 Mc/s. (FM) 16-50, 200-550, 900-2,000 m. Flywheel tuning. Attractive Perspex front panel in two-tone grey with golden trim. Thermometer type tuning indicator, pre-aligned I.F. transformers. Switched wide and narrow A.M. bandwidths.



TUNING HEART Model AFM-T1 £4/13/6 (inc. P.T.) I.F. AMPLIFIER and Power Unit Model AFM-A1. Complete with metal cabinet and valves £22/11/6. Sold separately.

Kit Total £27.5.0

### DUAL-WAVE TRANSISTOR PORTABLE RADIO KIT Model UXR-1

Presented in elegant real hide case with tasteful gold relief. Can be assembled in 4 to 6 hours and you have a set in the top flight of transistor portables. Pre-aligned I.F. transformers, printed circuit and a 7in. x 4in. high flux speaker.



Covers both Long and Medium waves. Dimensions 9½in. x 7½in. x 3½in.

Kit £12.11.0 (inc. P.T.)

### Money-back Guarantee

Daystrom Limited unconditionally guarantee that each Heathkit model assembled in accordance with our easy-to-understand instruction manual must meet our published specifications for performance or the purchase price will be cheerfully refunded.

### ELECTRONIC WORKSHOP KIT Model EW-1

20 exciting experiments can be made with this one kit. Transistor Radios, Intercom. Sets, Burglar Alarm, etc. A 72-page illustrated manual is included. Ideal for the junior experimenter. Kit £7.13.6 (inc. P.T.)

TAPE DECKS are available as "packaged deals" with other equipment. Details on request.

### 4½in. VALVE VOLTMETER KIT Model V-7A

The world's most popular valve voltmeter with printed circuit and 1 per cent precision resistors to ensure consistent laboratory performance. It has 7 voltage ranges measuring respectively D.C. volts to 1,500 and A.C. to 1,500 r.m.s. and 4,000 peak to peak. Resistance measurements from 0.1 ohm to 1,000 megohms with internal battery. D.C. input resistance is 11 megohms and dB measurement has a centre-zero scale. Complete with test prod, leads and standardising battery. Power requirements, 200-250 v. 40-60. c/s. A.C. 10 watts.



H.V. and R.F. Probes available as optional extras.

Kit £13.18.6

Assembled £19.18.6

### POWER SUPPLY UNIT KIT Model MGP-1

Compact, general purpose unit suitable for F.M. Tuners, Tape Recording Amplifiers and general laboratory use. Input 100/120 v., 200/250 v., 40-60 c/s. Output 6.3 v., 2.5 A. A.C.; 200, 250, 270 v., 120 mA. max. D.C.



Kit £5.2.6

Assembled £6.12.6

### DECADE CAPACITOR KIT Model DC-1

Capacity values 100μF to 0.111μF. in 100μF steps. Precision silver-mica capacitors and minimum loss ceramic wafer switches ensure high accuracy.

Kit £7.5.0.

Assembled £10.8.0

### 2¼in. SERVICE OSCILLOSCOPE KIT Model OS-1

Light, compact, portable for service engineers. Printed circuit board for easy construction. Time base 15 c/s. to 150 kc/s. in four ranges and 50 c/s. sine wave sweep. Flyback suppression on all ranges. Internal, external and 50 c/s sync. Size 5 x 8 x 14½in. long. Weight 10½lb.



Kit £22.18.0

Assembled £30.8.0

### CAPACITANCE METER KIT Model CM-1U

This Direct-Reading Capacitance Meter is a very low priced, time-saving instrument which is so useful that it should be part of the general equipment of every electronic laboratory and production line. Easily built in a few hours. 0-100μF., 0-1,000μF., 0-0.01μF., 0-0.1μF. The meter has 4½in. scale and can be used by an unskilled operator after a few minutes' instruction.



Kit £15.15.0

Assembled £21.14.0

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**AMATEUR TRANSMITTER KIT**

**Model DX-40U**



Covers all amateur bands from 80 to 10 metres, crystal controlled. Power input 75 watts C.W. 60 watts peak controlled carrier phone. Output 40 watts to aerial. Provision for VFO. Filters minimise T.V. interference. Modulator and power supplies are built-in. Single knob band switching is combined with a pi-network output circuit for complete operating convenience. A high-grade moving-coil meter indicates the final grid or anode current. Provision is made for the use of 3 crystals with access through a trap-door in the back of the cabinet. A 4-position switch selects the appropriate crystal or a jack for external VFO which can be used instead of the crystal(s).

Kit ... £33.19.0 Assembled ... £45.8.0

**SINGLE SIDEBAND ADAPTER KIT**

**Model SB-10U**



May be used with most A.M. transmitters with certain provisions. Allows full use of existing equipment for SSB facilities. Band coverage: 80, 40, 20, 15, 10 m. Unwanted sideband suppression; better than 30 dB. Carrier suppression: better than 40 dB. Power requirements: 300 v. D.C. 85 mA. (average) 30 mA. (standby). 140 mA (transmit), 6.3 v. A.C., 3.5 A. Meter: 2½in. Scale edge reading, 200µA movement, indicates carrier null and relative power output. Cabinet 11in. high x 8in. wide x 14½in. deep.

Kit ... £39.5.0 Assembled ... £54.18.0

**AUDIO SINE-SQUARE WAVE**

**GENERATOR KIT. Model AO-1U**

Covers 20 c/s. to 150 kc/s. in four ranges with choice of sine or square waves. The latter up to 10 kc/s. Output 10 v. max. and distortion less than 1%. Ideal for audio testing. Size 9½ x 6½ x 5in.

Kit ... £14.15.0 Assembled ... £21.5.0

**GRID-DIP METER KIT. Model GD-1U**

Functions as oscillator or absorption wavemeter. With plug-in coils for continuous frequency coverage from 1.8Mc/s. to 230 Mc/s.

Kit...£10.19.6 Assembled...£13.19.6

Additional Plug-in Coils Model 341-U extend coverage down to 350 kc/s. With dial correlation curves, 17/6.

**TRANSISTOR INTERCOM KITS**

**Models XI-1U and XIR-1U**

Ideal for home or business use. Up to five remote stations can be operated with each Master. The Master unit can call any one, any combination, or all five Remote stations and any Remote station can call the Master. A private call to any Remote station cannot be interrupted or overheard by any other while a conversation is in progress. Any Remote station can talk to any one or all others provided the Master is manned. These kits have been designed for easy construction and high performance. The mahogany veneered wooden cabinets are supplied completely assembled and finished. The Master unit has a 4-transistor amplifier and is operated by an internal 9 v. battery as are the Remote units. Batteries are not included with the Kits.

**Model XI-1U (Master)**

Kit ... £10.19.6 Assembled ... £16.19.6

**Model XIR-1U (Remote)**

Kit ... £4.7.6. Assembled ... £5.16.0

**"MOHICAN" GENERAL COVERAGE RECEIVER KIT**

**Model GC-1U**

This fully transistorised receiver which includes 4 piezo-electric transistors, is in the forefront of receiver design. It is an excellent portable or fixed station receiver. The R.F. "front-end" is supplied as a pre-assembled and pre-aligned unit. Its many features include a 10-transistor circuit, printed circuit board, telescopic whip antenna, tuning meter, and a large slide-rule dial giving a total length of approximately 70 inches. Housed in a steel cabinet and powered by two 6 volt dry batteries (not supplied), mounted internally, it gives frequency coverage from 580 kc/s. to 30 Mc/s. in five bands; thus enabling world-wide reception. Electrical bandwidth covers the amateur bands from 80 to 10 metres—each band having a scale length of approximately 8 inches. BFO tuning and Zener diode stabiliser. Size 6½ x 12in. x 10in.



Please write for specification leaflet.

Kit ... £37.17.6 Asmbld. ... £45.17.6

**STABILISED POWER PACK Models MSP-1M and MSP-1W**

Specially recommended for industrial and laboratory use, meeting the need for a reliable and versatile stabilised power pack capable of a very high performance. Input 200-250 v. 40-60 c/s., A.C., fully fused. Outputs: H.T. 200-410 v. D.C. at 0-225 mA. in 3 switched ranges. Unstabilised A.C., 6.3 v. at 4.5 A. centre-tapped. Two 3in. "easy-to-read" meters for reading voltage and current simultaneously. Separate L.T. and H.T. supply transformers. All output circuits are isolated. Size 13in. x 8½in. x 9½in.



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**Model DX-100U**



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**Amateur TX Kit**

- Completely self-contained. 150 w. D.C. input.
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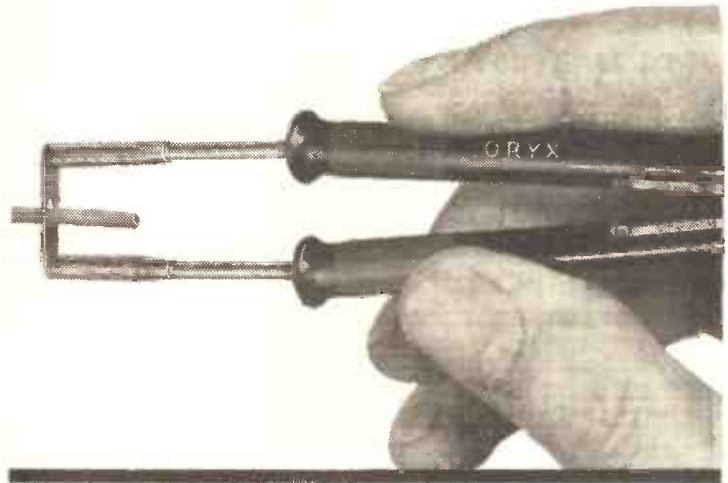
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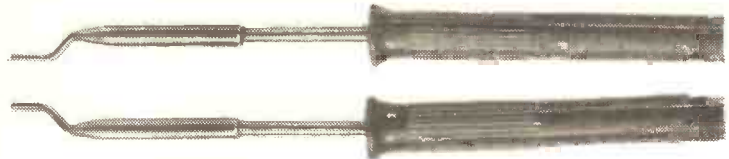
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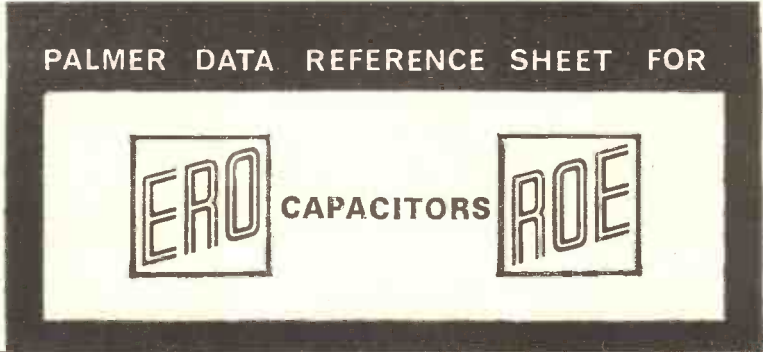


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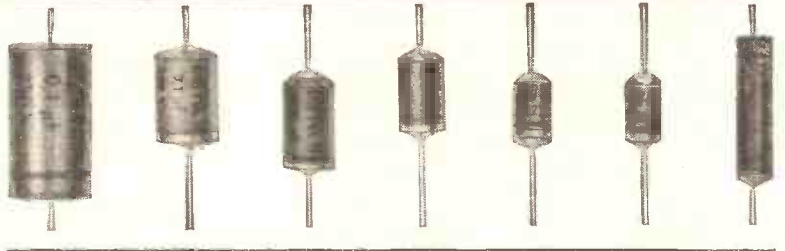
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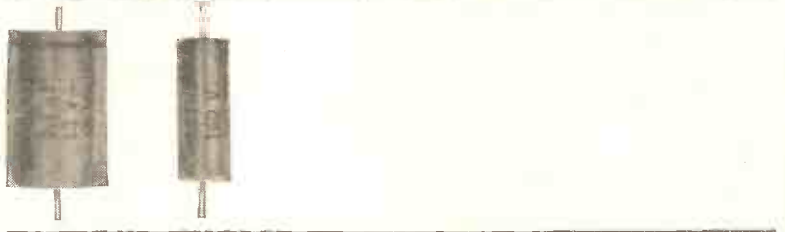
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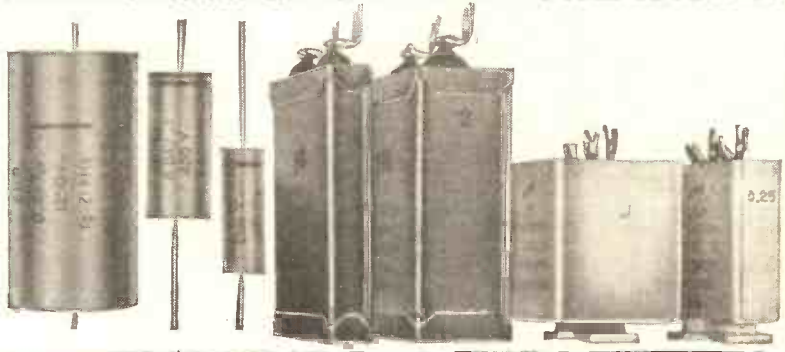
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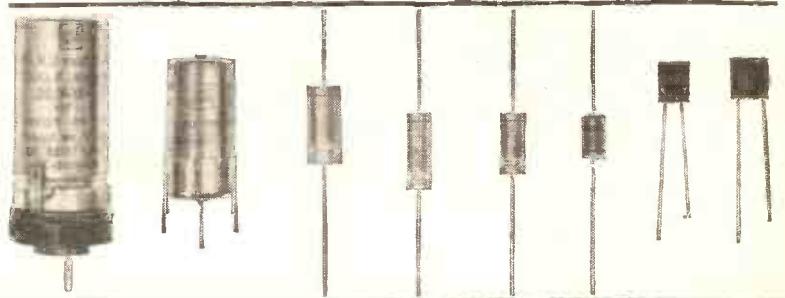
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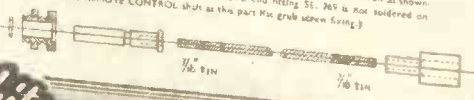
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**S.S. White**  
**FLEXIBLE**  
**REMOTE**  
**CONTROL**  
**OUTFIT**

**INSTRUCTIONS**

1. Determine the overall length of REMOTE CONTROL assembly required.
2. Select the end fittings and calculate the length of REMOTE CONTROL shaft to make the assembly.
3. Cut the REMOTE CONTROL shaft with the special shaft cutter supplied in the outfit to ensure a clean cut.
4. Tin 7/16" of each end of the REMOTE CONTROL shaft by heating the ends in a flame to above the normal soldering temperature, and then dipping in the special tinning compound supplied, agitating until the shaft is inward and then wipe with a clean rag. Do NOT use Spirits of Salts. Further supplies of tinning compound are available.
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# Wireless World

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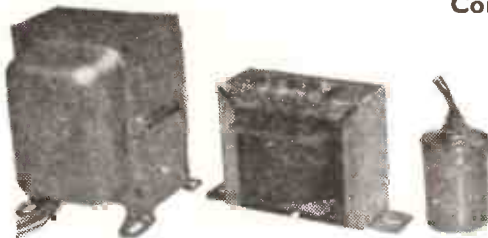
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Transformers

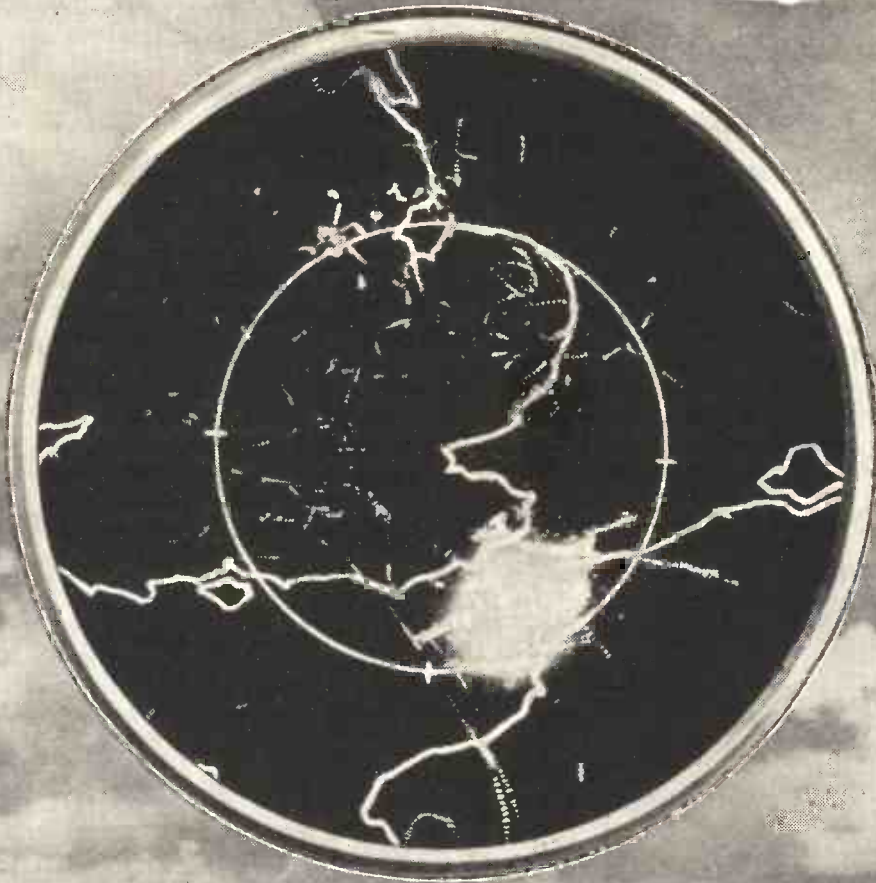
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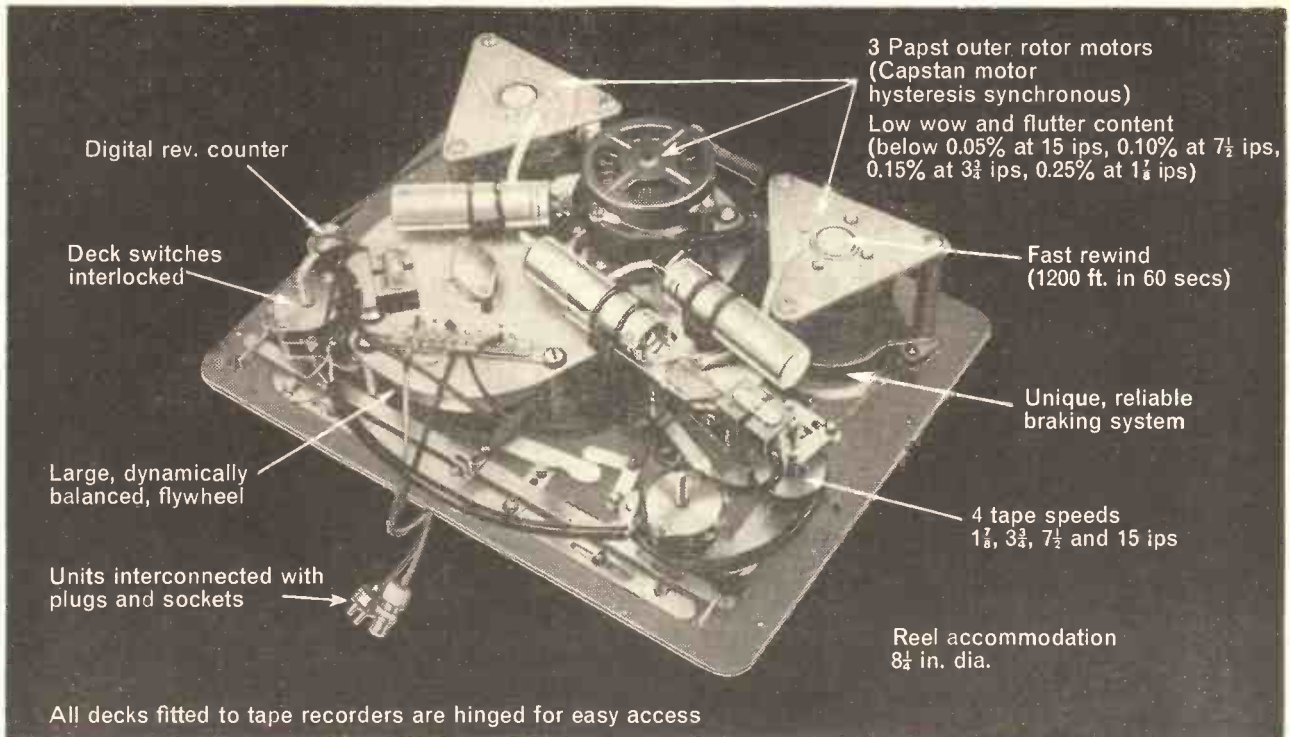
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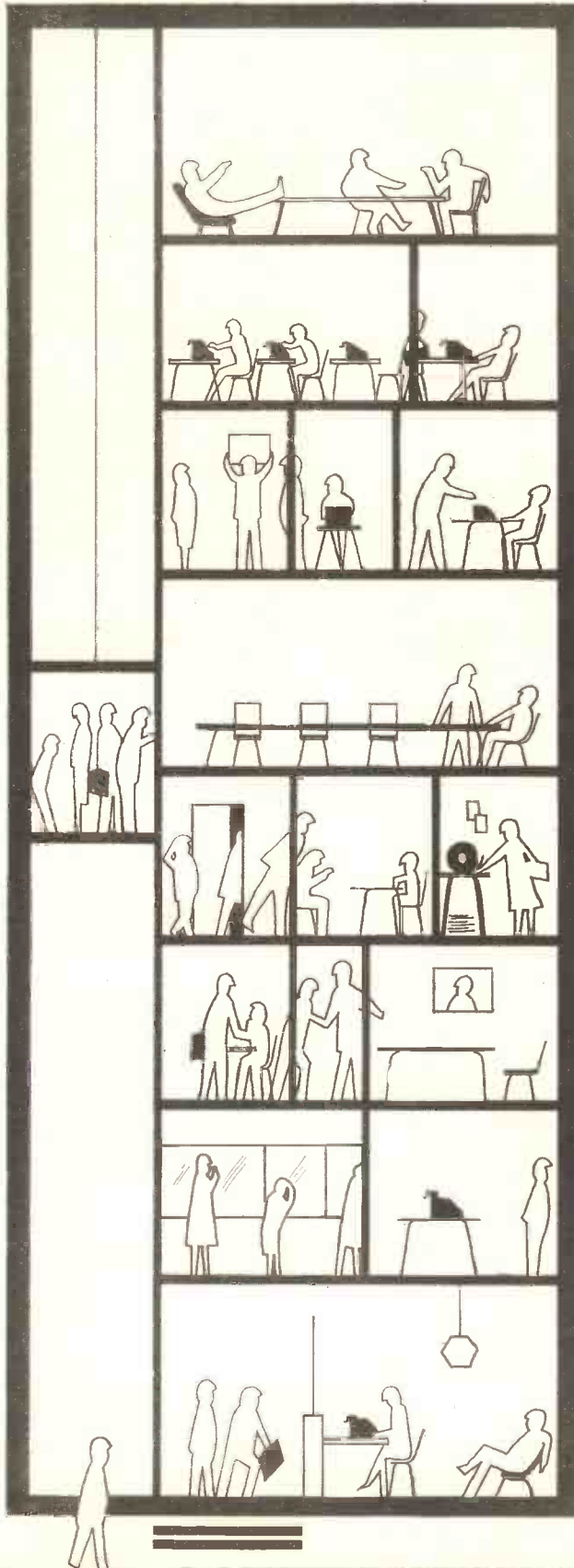
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# 6Mc/s UNIVERSAL COUNTER -TIMERS

Types TM51B  
and TM51C



High sensitivity of 35mV at frequencies up to 300kc/s.  
Low input noise to minimise error on period measurement.  
Large characters, display storage and wide viewing angle.

The in-line display is on five long-life neon numerical indicating tubes controlled by a latching circuit which holds the display stationary whilst a count is in progress and automatically resets the display at the completion of a count. This feature dispenses with the need for hold controls or display blanking and ensures a high sampling rate down to very low frequencies.

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Provision is made for an external frequency standard to be used in place of the internal 1Mc/s crystal oscillator. Pulse outputs are available on the front panel at decade divisions of either the internal 1Mc/s oscillator or the input trigger frequency, thus the instrument may be used as a frequency divider up to 1Mc/s.

## SPECIFICATION

### FREQUENCY RANGES

1c/s to at least 6Mc/s measured on 3 ranges with gate times of 10ms, 100ms and 1 second  
Accuracy:  $\pm 1$  count  $\pm$  crystal error.

### TIME RANGES

$3\mu$ s to 27.77 hours measured on 7 ranges in units of 1 $\mu$ s, 10 $\mu$ s, 100 $\mu$ s . . . 1 second.  
Accuracy:  $\pm 1$  count  $\pm$  crystal error  $\pm$  trigger error.

### PERIOD AVERAGE RANGES

$10^1, 10^2, \dots, 10^7$  input periods measured in units of 1 $\mu$ s on 5 ranges.  
Accuracy:  $\pm 1$  count  $\pm$  crystal error  $\pm$  trigger error/number of periods.

### 1Mc/s CRYSTAL ERROR

TM51B:  $\pm 0.001\%$  at 20°C after 1 minute. Ageing 2 parts in  $10^6$  per week.  
 $\pm 0.003\%$  from -10°C to +45°C after 1 minute.

TM51C:  $\pm 0.0001\%$  at 20°C after 20 minutes. Ageing 3 parts in  $10^7$  per month.  
 $\pm 0.0003\%$  from -10°C to +45°C after 20 minutes.

### TRIGGER ERROR

Any trigger circuit operated by a sinusoidal signal of amplitude S in the presence of noise N is subject to a trigger error of  $\pm 0.3N/S$ .

The input trigger circuit has an equivalent input noise of less than 300 $\mu$ V r.m.s. thus for 100mV r.m.s. input the trigger error is  $\pm 0.1\%$ .

### TRIGGER INPUT SENSITIVITY

35mV r.m.s. on sine waves from 0 to 300kc/s decreasing to 100mV at 3Mc/s and 300mV at 6Mc/s.

### TRIGGER INPUT IMPEDANCE

100 kilohms in parallel with 10pF.

### TRIGGER LEVEL

The trigger level is continuously variable from -750mV to +750mV.

### TEMPERATURE RANGE

-10°C to +45°C.

### POWER SUPPLY

100/125V or 200/250V, 45/65 c/s, 25 VA.

### SIZE AND WEIGHT

6 $\frac{1}{2}$ in. high x 10 $\frac{1}{4}$ in. wide x 9in. deep. 11 lbs.

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PORTABLE INSTRUMENTS

TM51B £275.

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Material	Typical uses	Min. thickness regularly rolled in inches	*Category
Mumetal	High frequency uses, bobbin cores for memory devices	0.0005 0.00012	RM RM
Radiometal 50	Special cores for pulse transformers	0.0005	RM
H.C.R. Alloy	High frequency pulse transformers	0.0005	RM
Permendur		0.0005	RM
Steels:			
Telmar A1S1.302	Diaphragms	0.002	RM
A1S1.316L		0.001	S
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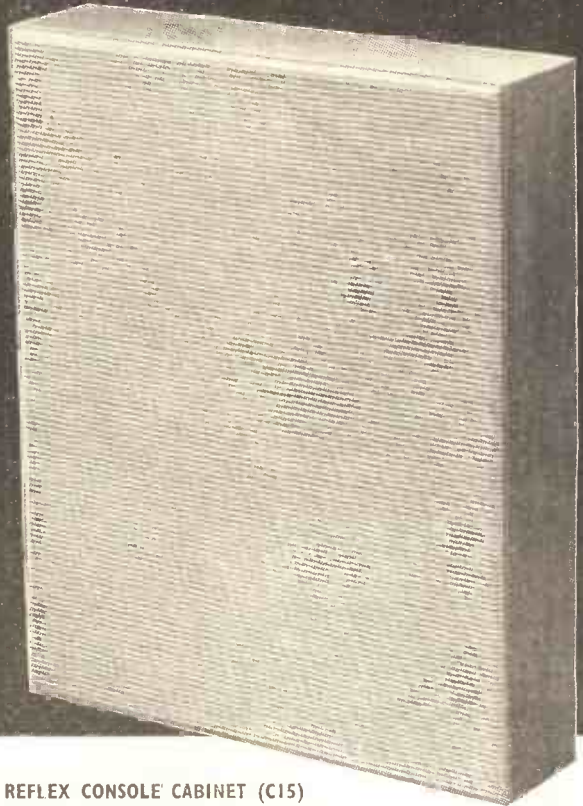
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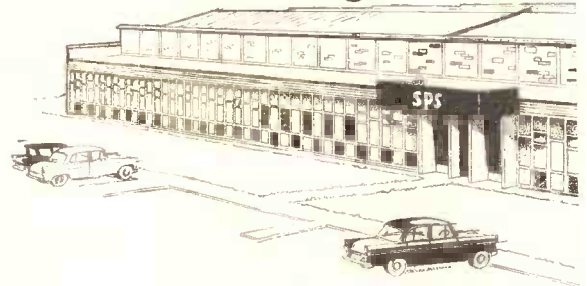
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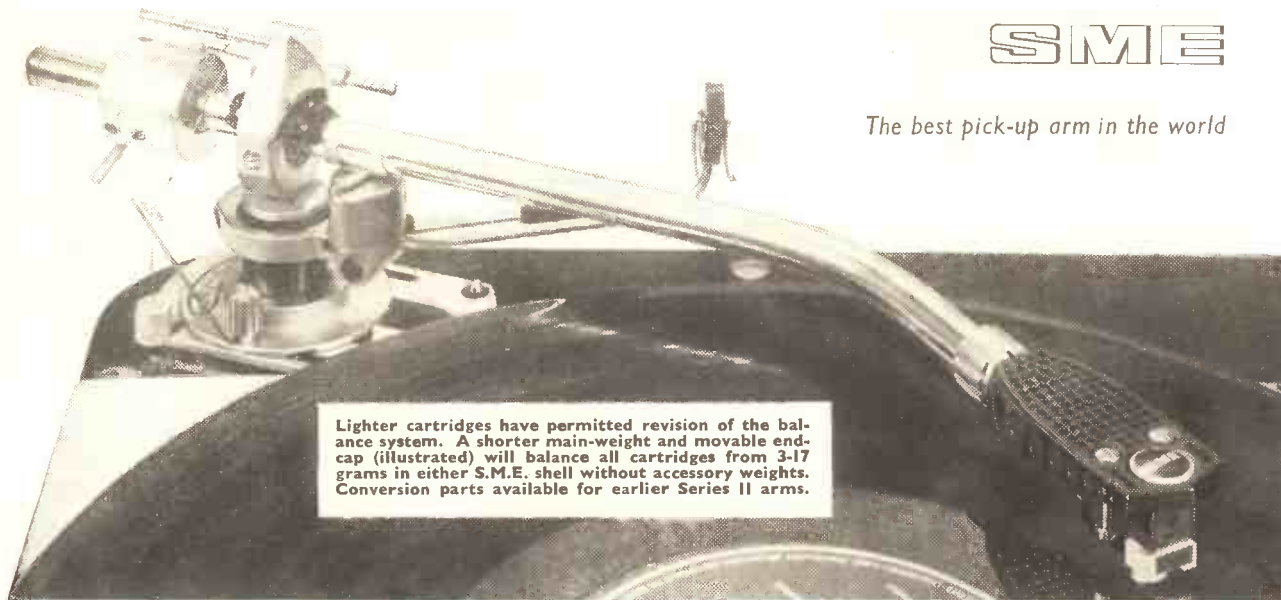
Data on all AF types available from: (NT ☉)

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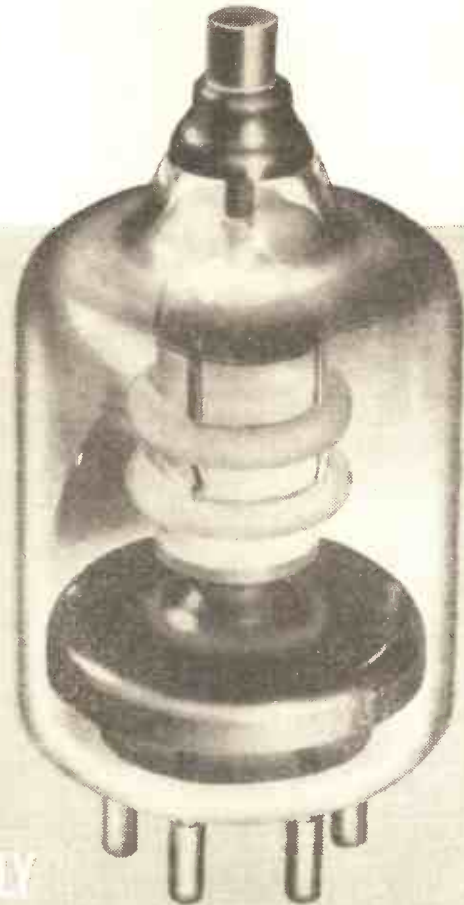
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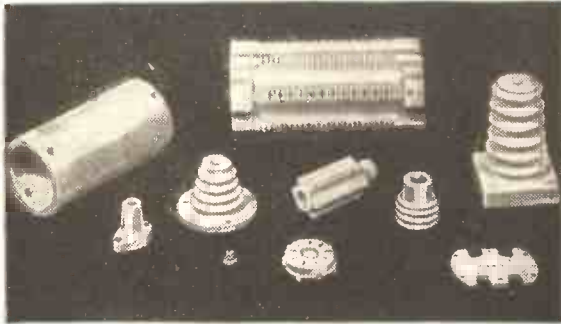
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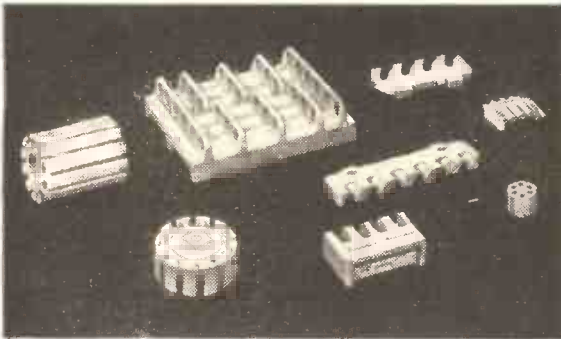
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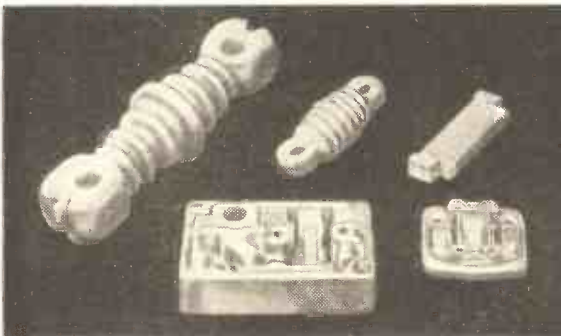
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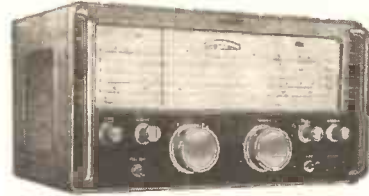
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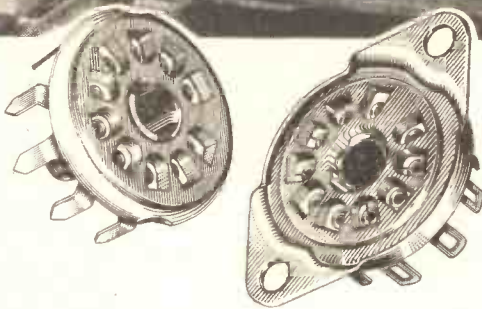


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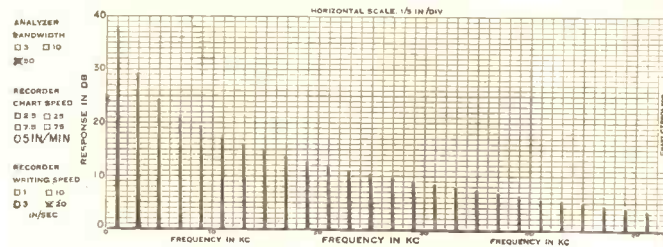
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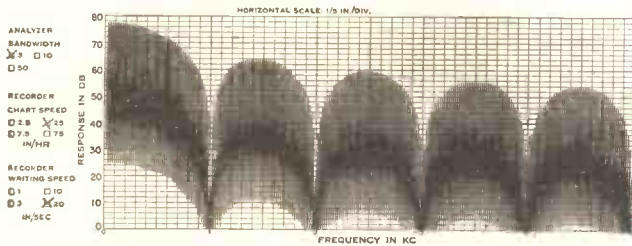
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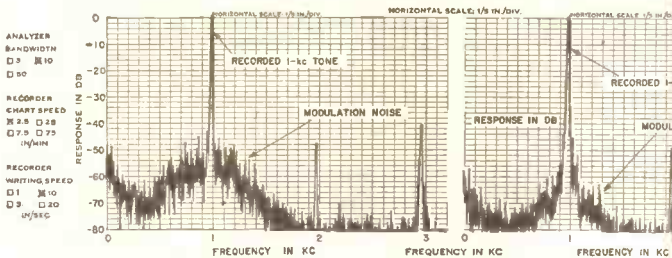
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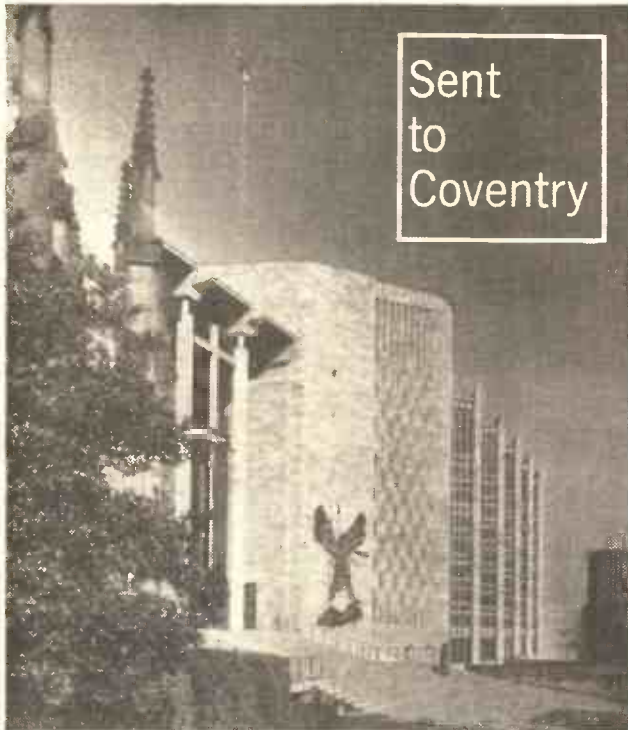
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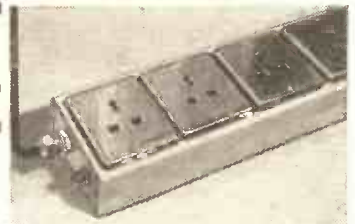
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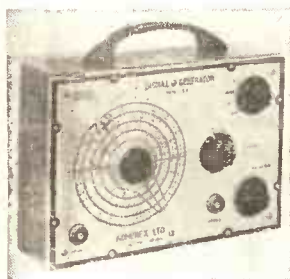
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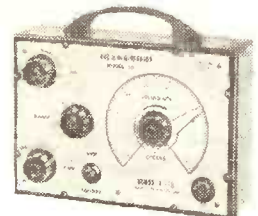
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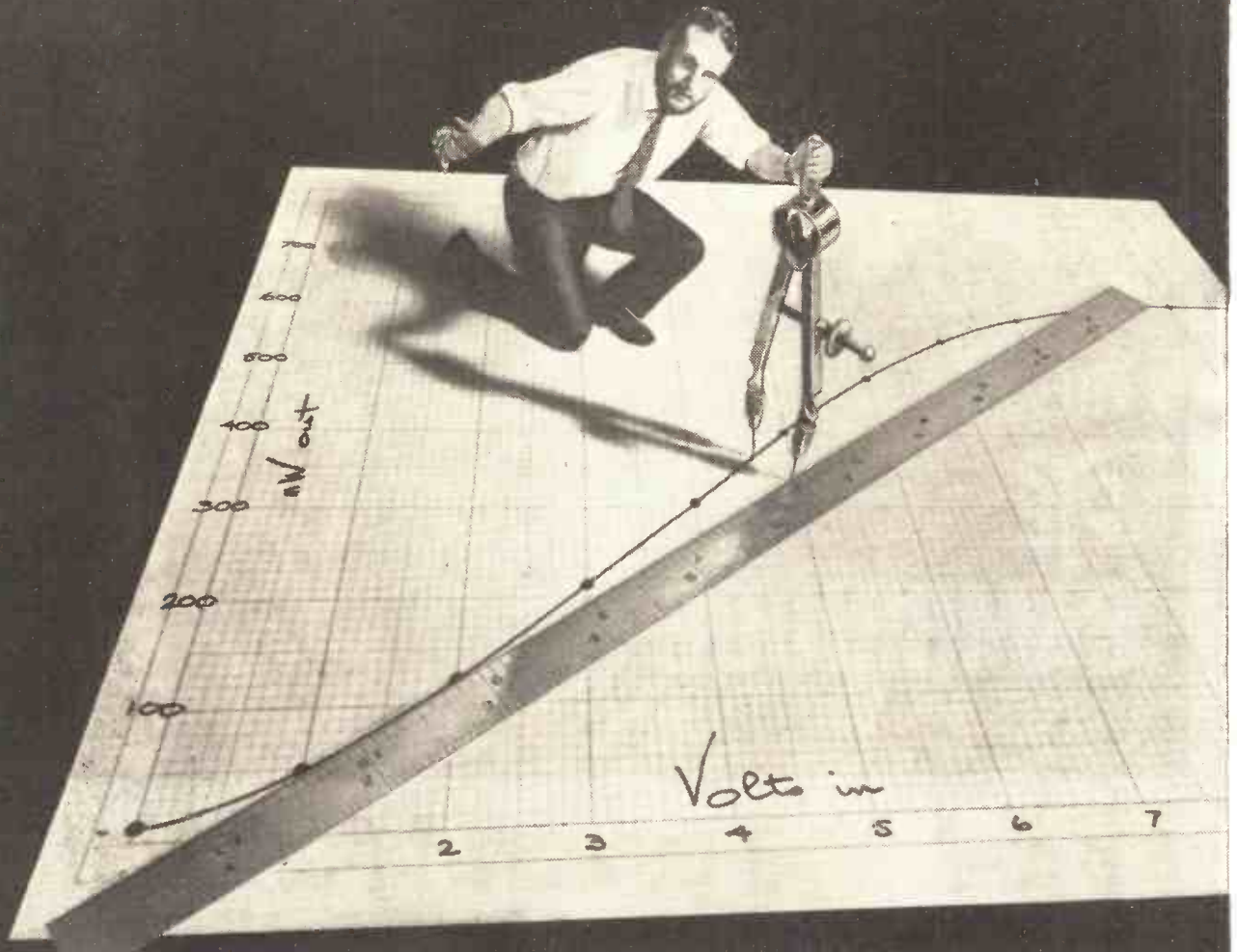
AUDIO  
GENERATOR  
MODEL 63

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WW-045 FOR FURTHER DETAILS.



# HOW DO YOU MEASURE NON-LINEARITY?



Harmonic analysis and measurements of distortion factor, noise, and inter-modulation distortion are described in a new Marconi Instruments publication.

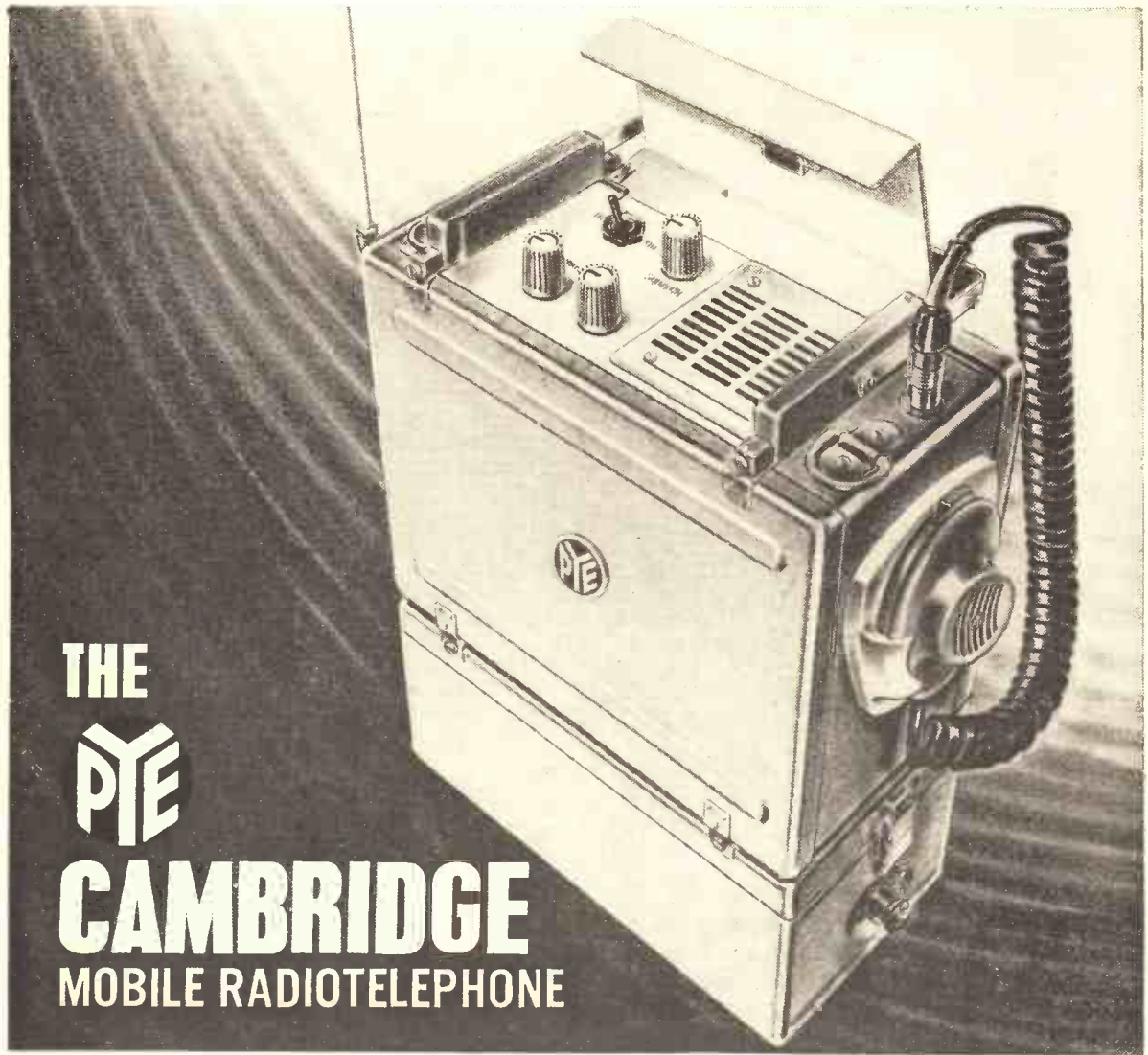
**If you work with a.f. amplifiers or transmission networks, please ask for your complimentary copy**

A GOOD NAME FOR GOOD MEASURE



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TC293



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WHARFEDALE SOUND

stereo/mono

# the Dovedale

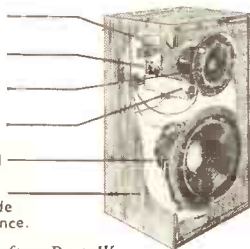
● WHARFEDALE SOUND

**WW**  
WHARFEDALE

The DOVEDALE is a restyled and improved version of the famous Wharfedale W 2. Research has proved that an enclosure of 2 cu. feet like the Dovedale is tunable and with a bass unit of very low resonance can produce 25 c/s easily and clearly. Hand built and finished in the Wharfedale tradition the Dovedale is possibly the most sensitive speaker available with this performance. To achieve these outstanding results it was necessary to develop the Flexiprene surround, producing a bass unit with a resonance of 20 c/s. Units—WLS/12 bass units with a 2" pole diameter having a flux density of 13,000 oersteds plus the well known Super 5 mid and treble

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- Crossover network  $\frac{1}{4}$  section 1 kc/s.
- Special Wharfedale 5" Tweeter unit with ceramic magnet.
- Tuning port.
- 12" bass unit with flexiprene roll surround and ceramic magnet.
- Cabinet of high density man made timber for reduced panel resonance.



Frequency range 25 c/s—17,000 c/s.  
Impedance 10/15 ohms output.  
Power Handling Capacity 15 watts (30 watts peak)  
Size 24" x 14" x 12" Weight 37 lb.

Finish zebirano, mahogany, walnut or teak veneers.

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Free technical folder on the Dovedale from Dept. W

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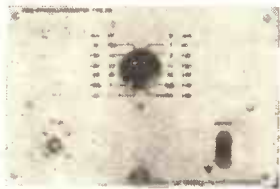




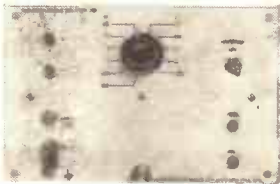
Meter Unit Type 70 with  
Wideband Millivoltmeter Type 701.

# 3 NEW UNITS join the range of plug-in instruments built to THE DYMAR SYSTEM

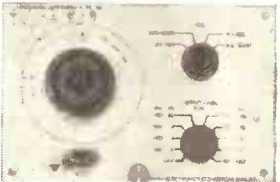
Introduced only in February, our range of high-grade laboratory instruments, using plug-in techniques, has met with an immediate and enthusiastic reception. Three new instruments now available begin the planned extension of the Dymar range and have all the in-built virtues of the original plug-ins. The basis of the system is the Type 70 Meter Unit (also available for 19" rack mounting) which provides a precision 5" meter movement and comprehensive, well regulated power supply facilities. The meter unit will accept any one of the range of plug-in instruments, giving maximum flexibility and instrument variation at greatly reduced cost.



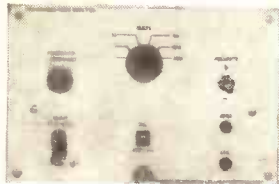
Wideband Millivoltmeter Type 701.  
Frequency: 10 c/s—4 Mc/s  
Sensitivity: 1mV—300 V f.s.d.  
Accuracy: 2% Price: £40



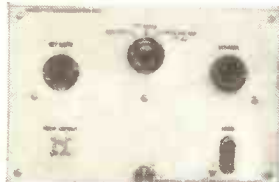
D.C. Microvoltmeter Type 721.  
Sensitivity: 100  $\mu$ V—300 V f.s.d.  
Impedance: 100 M $\Omega$   
Accuracy: 3% Price: £56



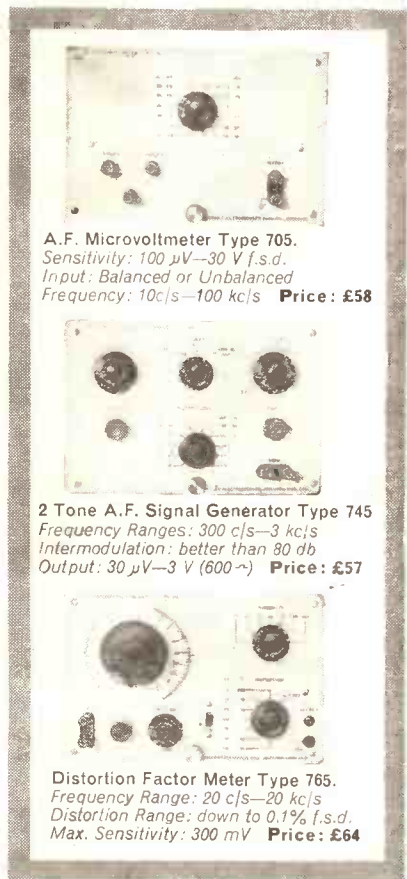
A.F. Signal Generator Type 741.  
Frequency Range: 30 c/s—300 kc/s  
Frequency Stability: 0.1%  
Output: 100  $\mu$ V—10 V (600 $\sim$ ) Price: £36



D.C. Kilovoltmeter Type 722.  
Sensitivity: 1V—30 kV f.s.d.  
Impedance: 3000 M $\Omega$   
Accuracy: 3% Price: £35



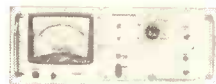
Noise Factor Meter Type 761.  
Frequency: 1 Mc/s—220 Mc/s  
Impedance: 50 or 75 $\Omega$   
Noise Factor: up to 15 db Price: £37



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Meter Unit Type 70R  
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OCTOBER 30th

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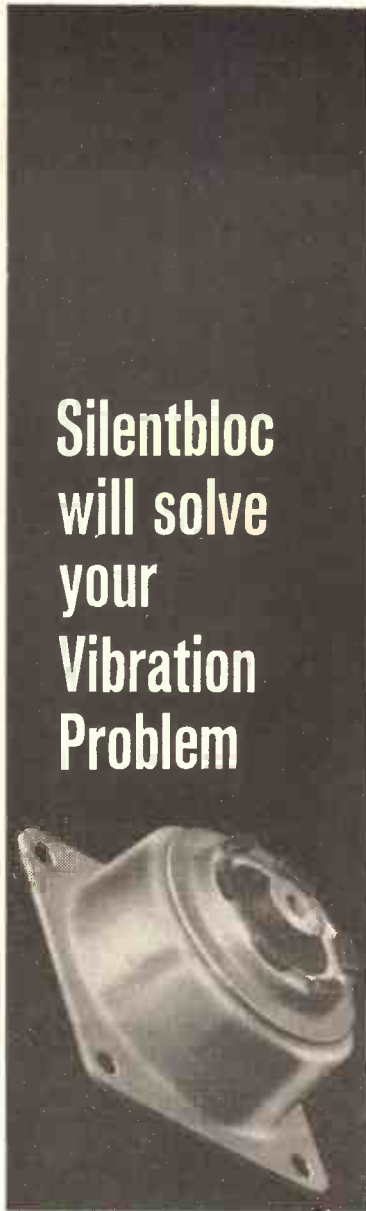
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Full information can be obtained from:

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*Silentbloc products are also manufactured by Silentbloc (Australia) Pty. Ltd., Melbourne*

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Broadway S/503

# THIS VACWELL THERMAL COMPRESSION BONDER TYPE PR56

This semi-automatic unit is designed for high speed bonding of contact wires to dice and post of the header and is ideal for integrated circuits, thin films and transistor interconnections. Leads are nailhead or scissor bonded to substrates, wedge bonded to header making for example: a complete two-bonded transistor in one operation.

It has an automatic wire feed and a stitch bonding circuit, allowing the operator to make any number of substrate connections in unlimited sequence.

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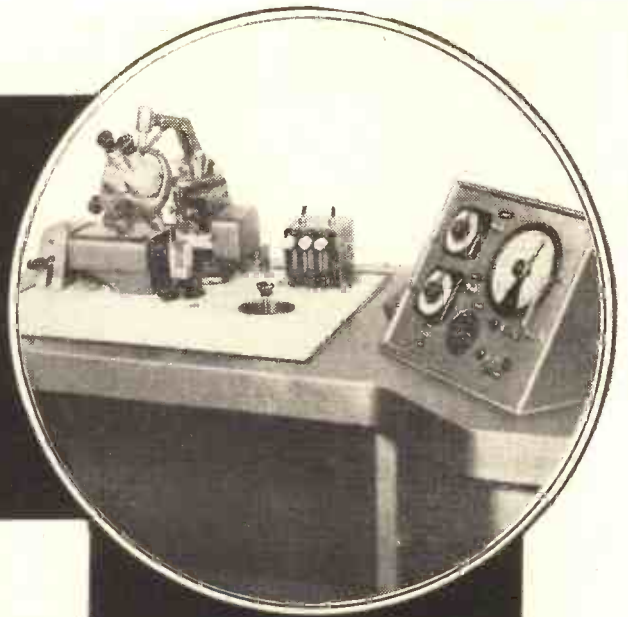


## VACWELL ENGINEERING COMPANY LIMITED

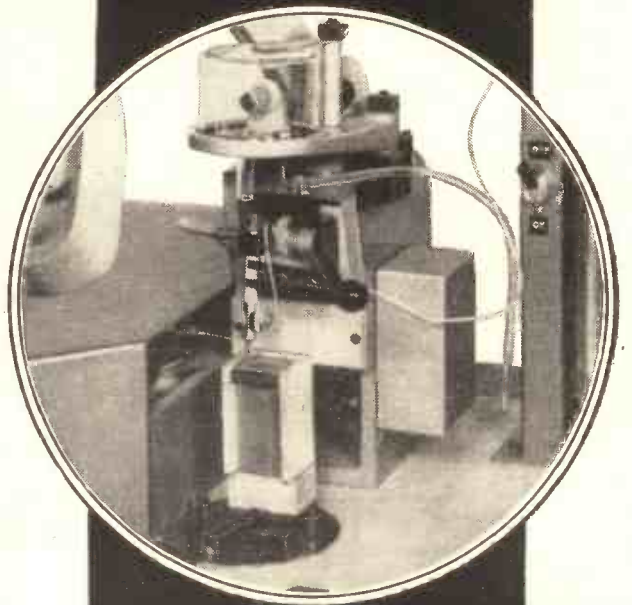
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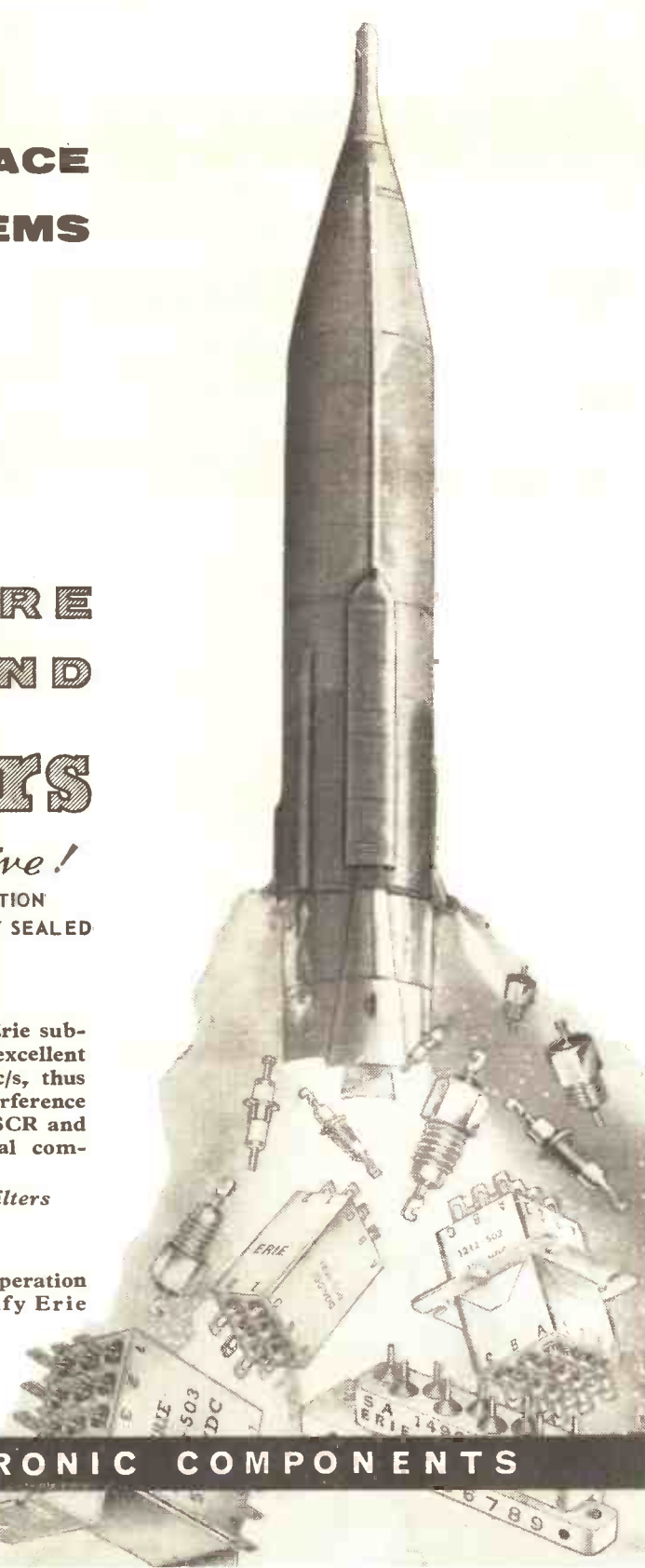
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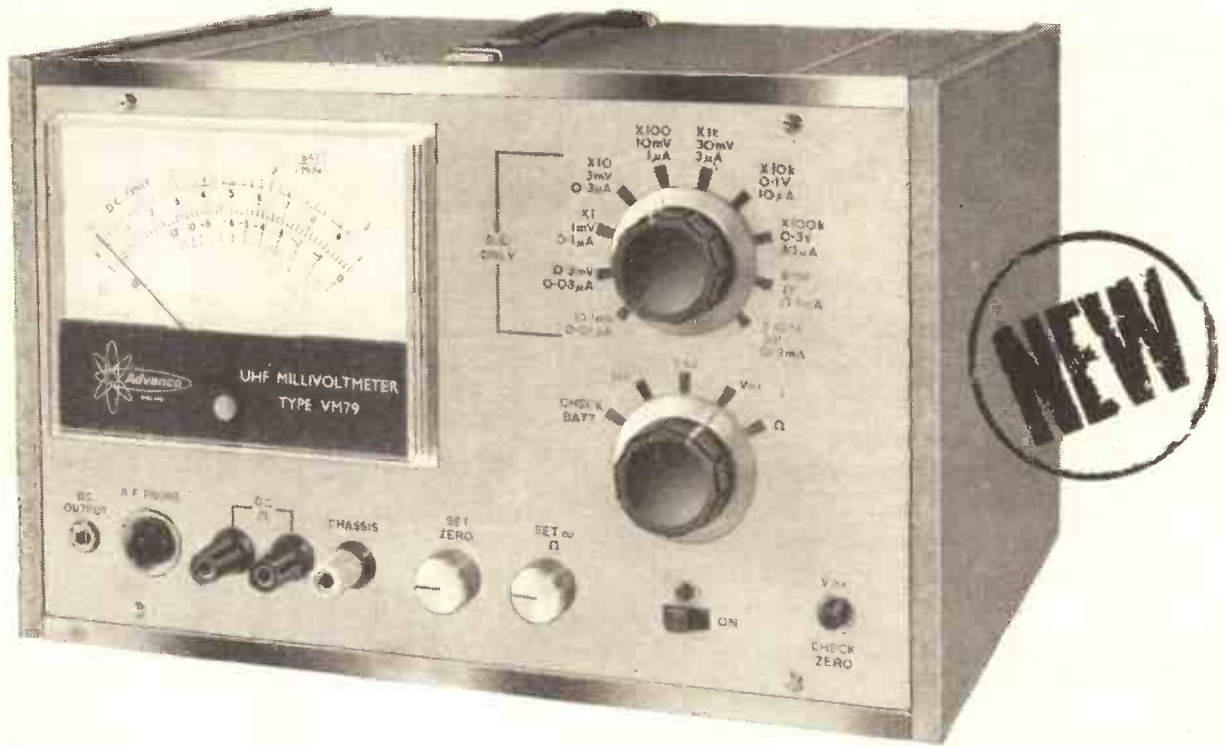
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ANTEX have solved the problem of providing miniature soldering irons with really 'heavy-duty' heat capacity — by introducing their new 18 watts model G240.

G240... a precision soldering iron possessing all the well-known advantages of ANTEX miniaturisation — yet capable of providing an intensified heat capacity.

G240's extra speed and precision opens up many new and exciting production possibilities in small-part soldering.

The G240 is available now with a choice of four different 'Ferraclad' long-life interchangeable bits\*. The G240 coupled with the standard ANTEX range means there is an ANTEX iron exactly right for your requirements!



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'Ferraclad' long-  
life bits.*

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# Q A FOR T R

## Electrosil triple rated glass-tin-oxide resistors receive qualification approval to DEF5115-1 multiple rated pattern RFG-5

In establishing a concept of multiple rating, R.C.S.C. have pointed the way to economy. This means that one type of resistor can perform three roles of operation, according to the stability required. These are equivalent to the semi-precision oxide of DEF 5114A, the grade one carbon of DEF 5112A, and the general purpose oxide of DEF 5114A. All three types can now be replaced by one resistor—Pattern RFG5 of DEF5115-1, stocks and expenditure are thus greatly reduced and the discrete component situation vastly simplified. DEF5115-1 also include Pattern RFG2, which covers general purpose metal oxide only. Needless to say the Electrosil TR range has also received approval to this Pattern.

Electrosil Type	DEF5115-1 Reference	Ratings (Watts 70°C)	Approved Range
TR4	RFG5-F	$\frac{1}{16}, \frac{1}{8}, \frac{1}{4}$	51 ohms-47K
TR5	RFG5-E	$\frac{1}{8}, \frac{1}{4}, \frac{1}{2}$	20 ohms-470K
TR6	RFG5-D	$\frac{1}{4}, \frac{1}{2}, 1$	20 ohms-1 meg

Pattern RFG5 includes 1%, 2% and 5% selection tolerances, and is therefore the only pattern in DEF 5115-1 available to 1% selection tolerances.

*Industry too, can benefit from the Triple-rating concept. Ask Electrosil today for full details; a leaflet is being prepared listing the relevant Nato stock numbers.*



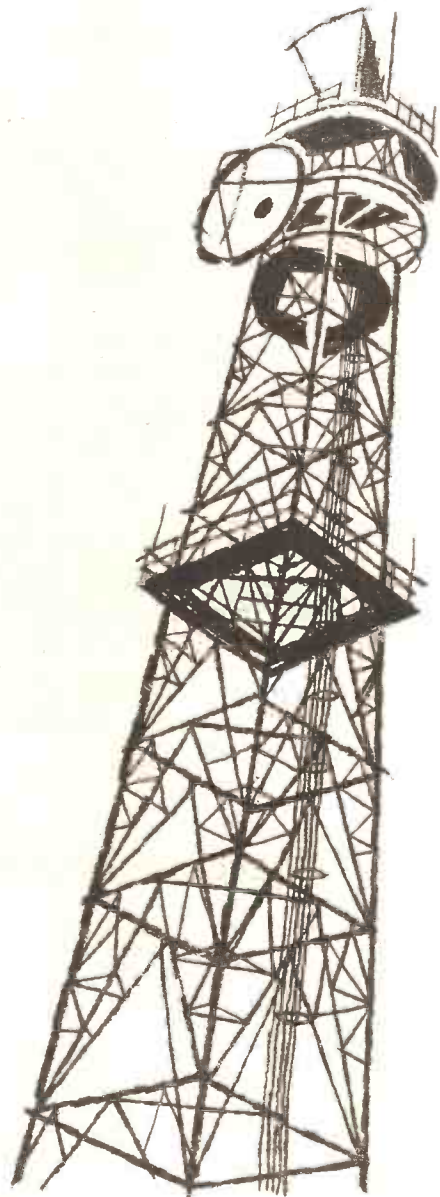
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PALLION SUNDERLAND CO. DURHAM  
Tel: Sunderland 71557 Telex 53273

**Triple Rating means Triple Economy**



# ferrite circulators for communications

- Designed for microwave links.
- Frequency Ranges:
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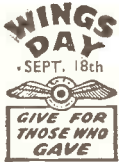
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DS/T138

## The vital role of reliable communication



When reliability is of the first importance—as with ambulance or patrol car work—BCC equipment is chosen time and time again. The BCC 81 mobile VHF transmitter-receiver is so compact that the whole unit can be fitted under the dashboard of almost any vehicle, without taking up valuable passenger space, thereby adding prestige and efficiency. Transistors are used throughout the receiver and power supply unit and in all but the final stages of the transmitter; current consumption is low—equal to only one instrument panel lamp on 'receive'; no standby facility is necessary as quick heating valves are used in the transmitter. With six channels in any frequency range between 37 and 174 Mc/s and 6 watt A.M. output, the advanced design of the BCC 81 makes it quite unbeatable in its class.

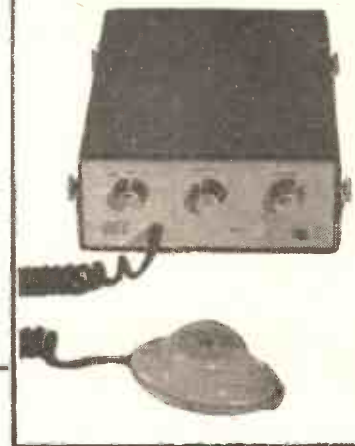


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**BCC 81**



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# BSR C1 CERAMIC cartridge

FOR PROFESSIONAL QUALITY

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## Technical Data

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Sensitivity at 1 Kc/s using Decca SXL 2057 record — 1 cm/sec. . . . .	0.110 volts ± 2 db
Stylus pressure . . . . .	2-3 grammes
Equivalent capacity . . . . .	600 pF
Loading . . . . .	2 MΩ 100 pF
Channel difference . . . . .	less than 3 db
Channel separation at 1 Kc/s . . . . .	20 db.

C1ST3 **£2 . 6 . 5** incl. tax. Stereo cartridge with double tipped sapphire stylus.  
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UA15 SS 3B fitted with C1ST3 **£10 . 18 . 11** incl. tax.  
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## UA15 SS 3B 4 speed Automatic Record Changer

Tubular, low mass pick-up arm for featherweight pressure. Large turntable for stability. Manual play facilities. Wow and flutter lowest ever. The ultimate in quality performance and dependability.

Send for details of the complete range of BSR equipment and address of your nearest BSR stockist.



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or order straight away, working out total area of material required and referring to table below, which is for four-sided chassis in 16 s.w.g. aluminium.

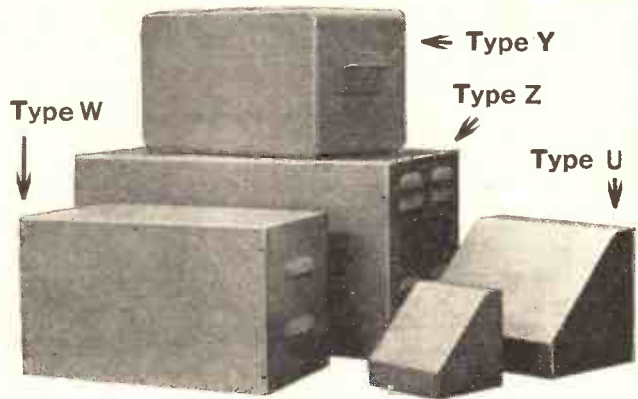
48 sq. in.	4/3	176 sq. in.	9/-	304 sq. in.	13/6
80 sq. in.	5/6	208 sq. in.	10/-	336 sq. in.	14/9
112 sq. in.	6/6	240 sq. in.	11/3	368 sq. in.	15/9
144 sq. in.	7/9	272 sq. in.	12/6	and pro rata.	

P. & P. 2/6      P. & P. 2/9      P. & P. 3/-  
Discounts for quantities. More than 20 sizes kept in stock for callers.

**FLANGES** (1/2 in., 3/4 in.), 6d. per bend.

**STRENGTHENED CORNERS** 1/- each corner.

**PANELS:** Any size up to 3ft. at 5/3 sq. ft. 16 s.w.g.; (18 s.w.g. 4/6). Plus post and-packing



## CASES

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Type U has removable bottom or back. Type W removable front, Type Y all-screwed construction, Type Z removable back and front.

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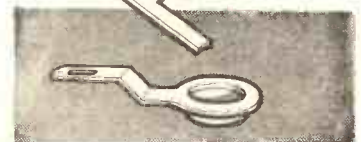
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TELEPHONE ASTON Cross 2218 (4 lines)

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**RACAL** Announce a NEW Decade Divider Unit  
 Frequency Measurement of the  
 SA.535 counter/timer is  
 extended to 15 mc/s



**Racal SA.548  
 Decade Divider Unit**  
 Extends frequency range  
 to at least 15 Mc/s  
 Trigger level offset up to  $\pm 300V$   
 All-semiconductor  
**U.K. Price £70**  
**Delivery ex stock**

**Racal SA.535  
 Universal Counter/Timer**

- Frequency Measurement to 1.2 Mc/s
- All-semiconductor
- Print-out facilities
- Time, Period and Frequency measurement
- Compact and Portable
- Six-digit in-line or vertical display

**U.K. Price £195**  
**Delivery ex stock**

The frequency range of the Racal SA.535 counter may now be extended from 1.2 Mc/s to 15 Mc/s, using the new SA.548 Decade Divider Unit. Trigger levels can also be offset up to  $\pm 300V$  facilitating discrimination against unwanted signals. The SA.548 is mains-operated and forms a plinth upon which the SA535 stands.



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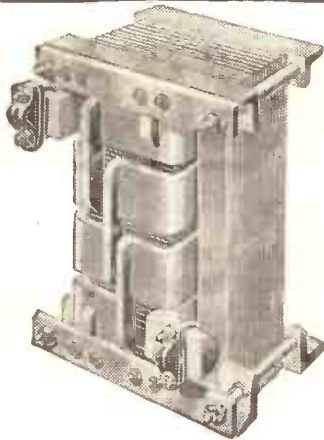
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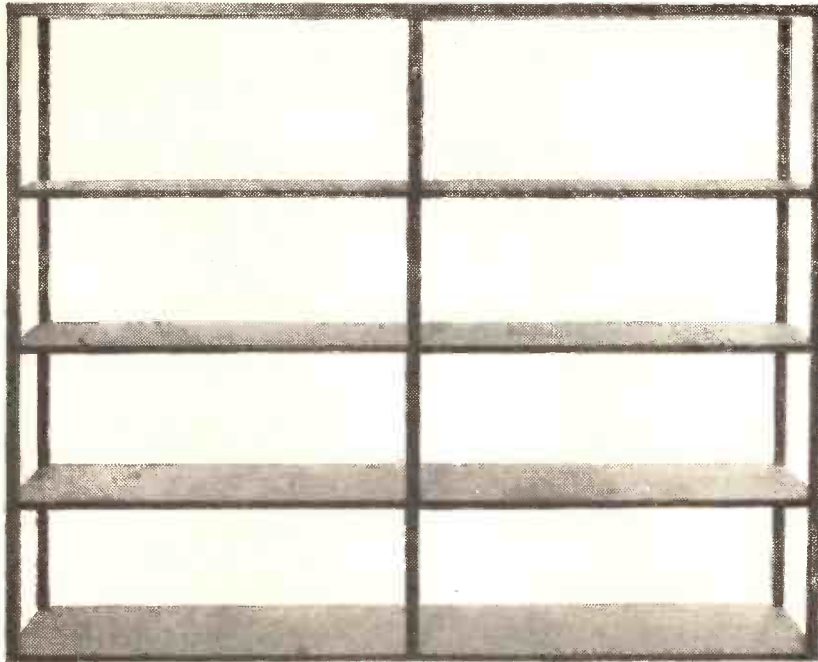
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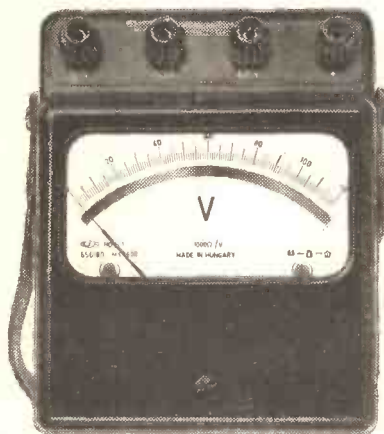
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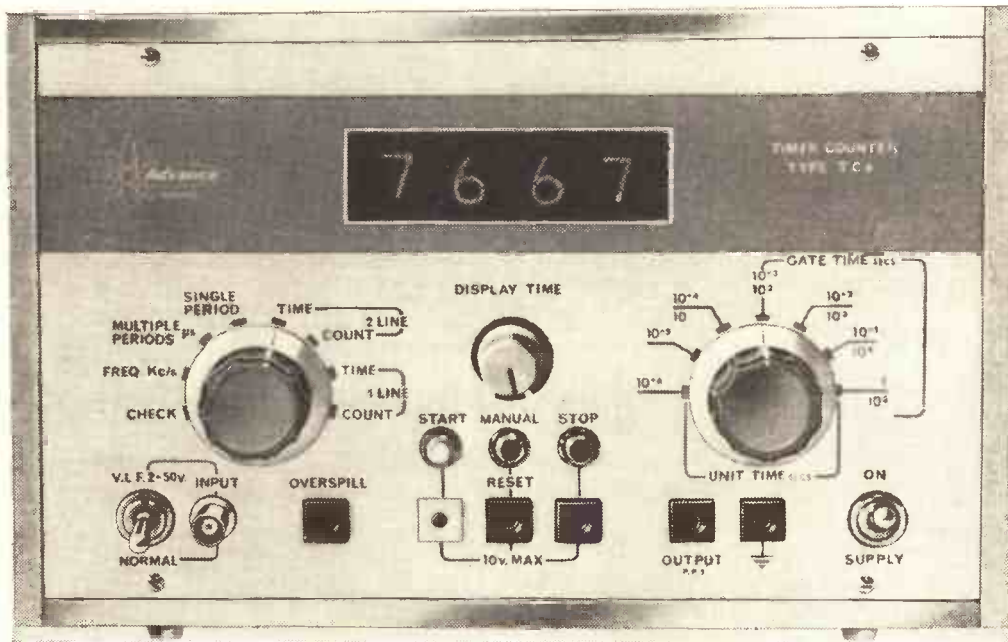
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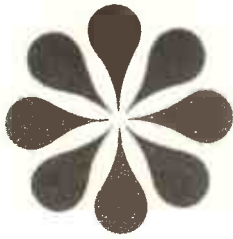
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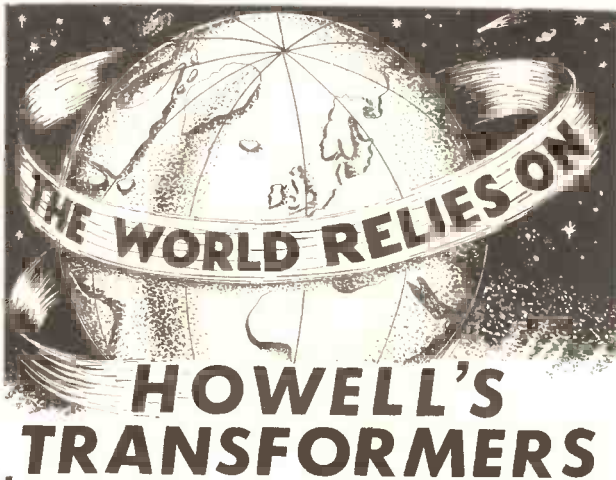
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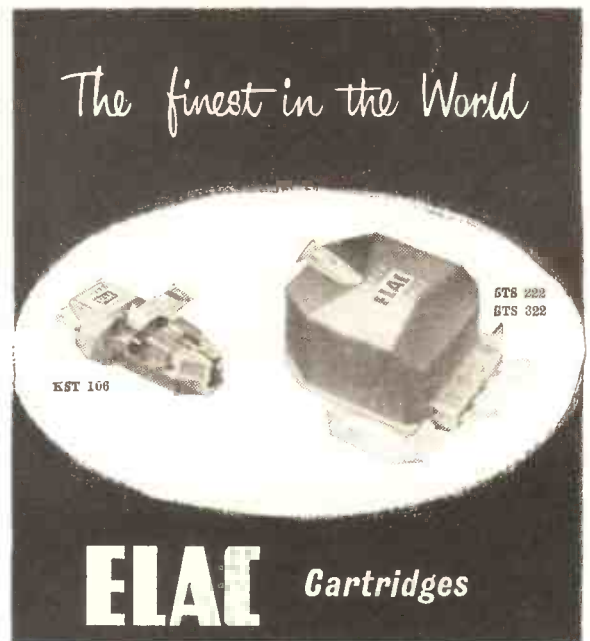
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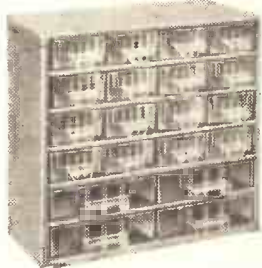


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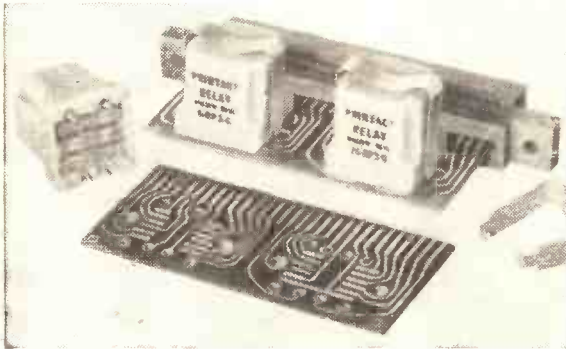
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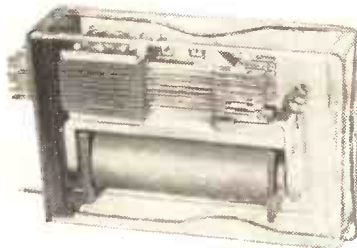
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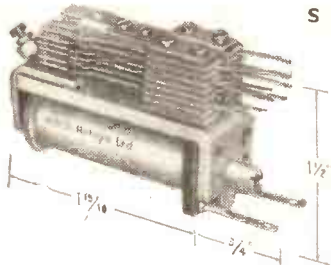
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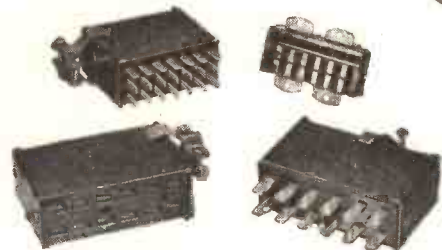
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Voltage 3 to 20  
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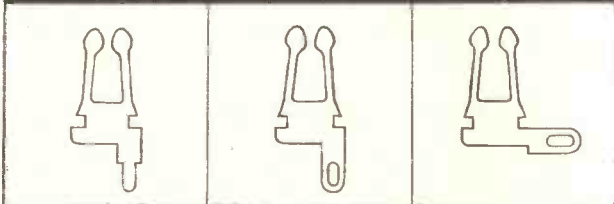
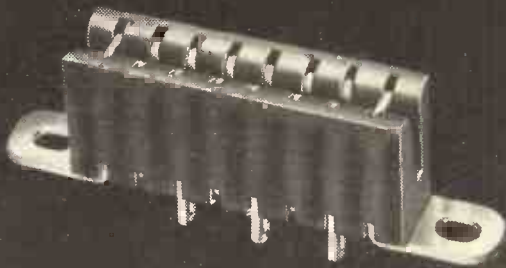
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35

These inexpensive edge connectors feature polypropylene mouldings and brass or phosphor bronze contacts with a standard tinned finish. Silver plate, gold flash, or gold plate finishes are available to special order. .100" contact pitches provide a maximum of 40 positions whilst the .150" contact pitch range provides for a maximum of 26 positions. Contact tail variations (shown above) include solder slot tails projecting either vertically downwards or at 90° to the moulding, or tails for direct mounting to a "mother" printed circuit board. Mounting brackets provide "closed" or "open-ended" connectors or include contacts for direct earthing from the mating P.C. Board.

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Working voltage: 500 Volts D.C. or A.C. Peak (.150" pitch)  
350 Volts D.C. or A.C. Peak (.100" pitch)

Current capacity: 5 amps max. per contact

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Sales offices: Wembley and Sale.



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# AMPLIFIERS

It is always possible to improve any amplifier specification given the time. The present range of standard power amplifiers detailed below were introduced in 1962, but small improvements have been incorporated since. The design is basic to all the 'Series 3' amplifiers. The 15 watt amplifier uses automatic bias of the output valves and the 25 watt version uses a fixed bias condition. The 'Series 3' is one of the most flexible and sophisticated amplifiers available today.

A new control unit, the SC22, will be available shortly. This pre-amplifier has been designed to work from anticipated new pick-up cartridges having an output of the order of 2 mV. The necessary improvement in the signal to noise ratio to make this possible has been achieved by the use of a planar epitaxial transistor in the input stage, operating in a feedback pair equalisation circuit with a low noise valve. The SC22 is capable of driving any power amplifier of up to 2 volts input sensitivity, from 2 mV input to the pre-amplifier. It is a very flexible unit having all facilities including switchable steep rumble and treble filters, loudness compensation and tape monitoring.

**Power Amplifier (Series 3)**

MA 15	Power amplifier	15 watts output	£26 10 0
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SC22	Stereo Control Unit	£35 0 0
SC22.P	" " " mains powered	£40 0 0

Leaflets are available on request for 'Series 3' Amplifier. SC22 leaflet will be available shortly.

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## XLR/EP AUDIO CONNECTORS

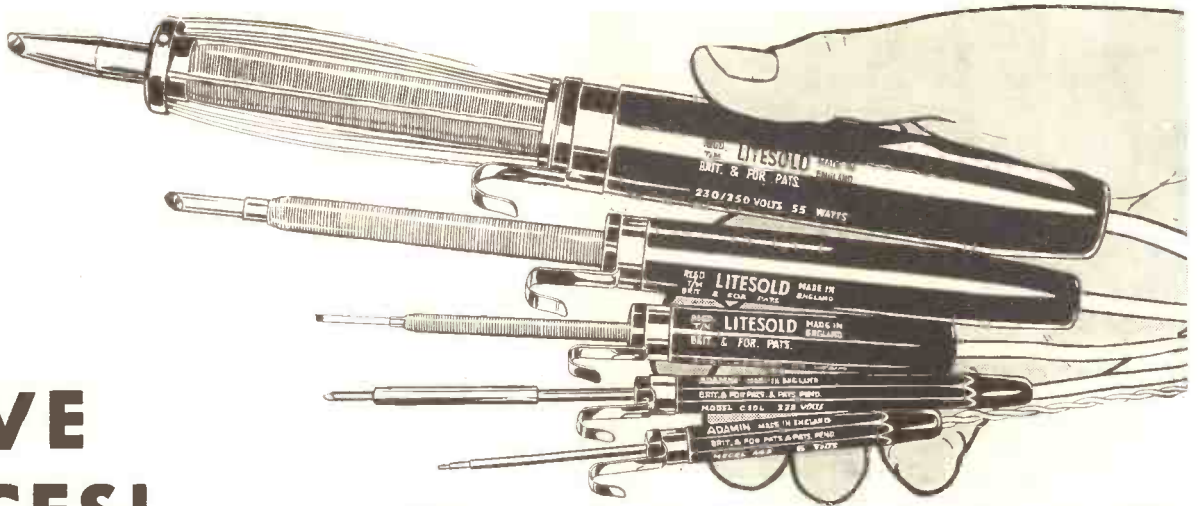
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Standing waves within the enclosure are eliminated by the generous use of B.A.F. wadding. Patents applied for.

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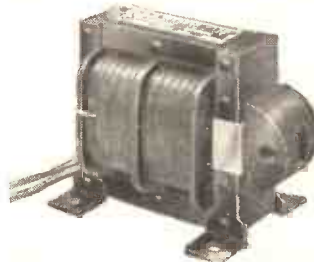
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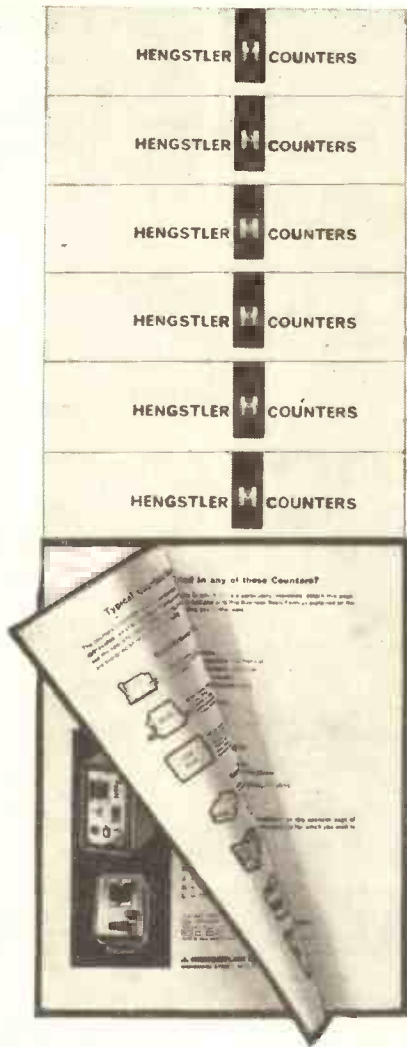
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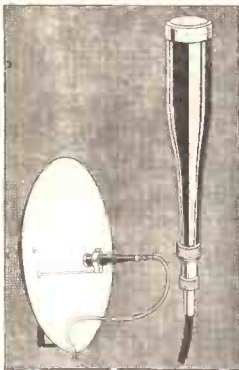
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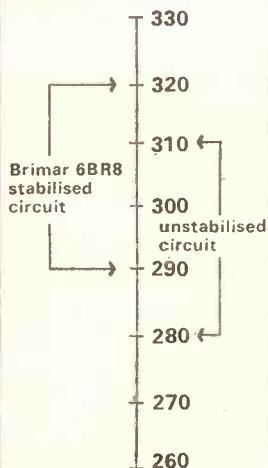


IN A NOVEL  
AUDIO AMPLIFIER  
PHASE SPLITTER CIRCUIT

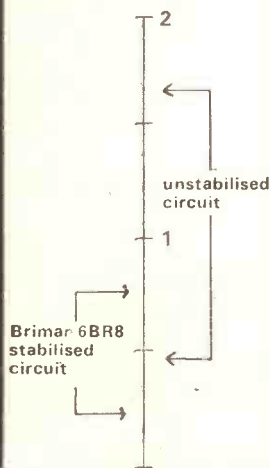
**Gain 313 at 0.41%  $D_{tot}$**   
for 8v. r.m.s. output  
using d.c. feedback  
stabilisation

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Marconi self-tuning H.F system—  
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# breakthrough

## MST 30kW transmitter type H1200

An h.f linear amplifier transmitter for high-grade telecommunications.  
Frequency range: 4-27.5 Mc/s.  
Output power: 30 kW p.e.p, 20 kW c.w.  
Meets all CCIR Recommendations.

### saves 80% floor space

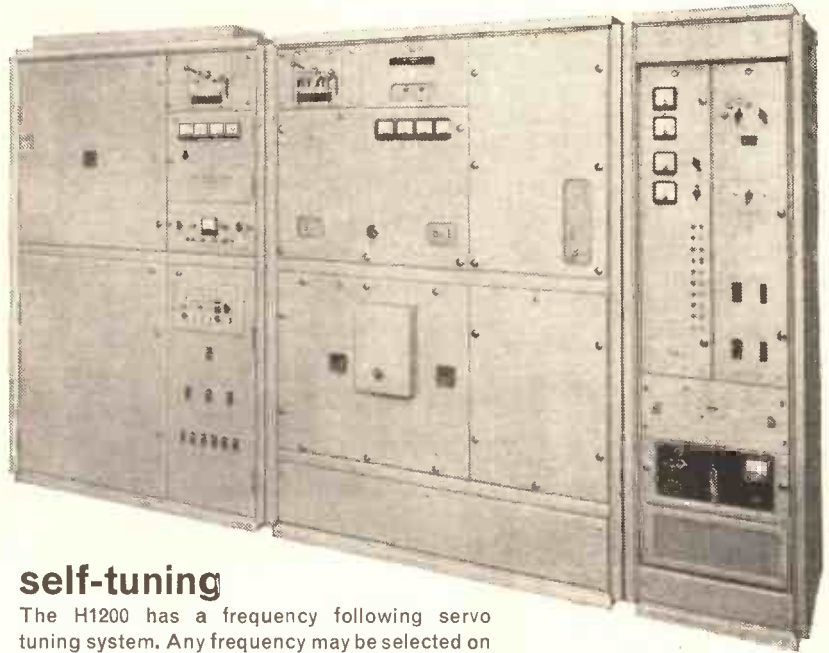
Transmitters can be mounted side by side and back to back or against a wall. Floor-ducts are eliminated and all power supply components are built-in. These features lead to smaller, simpler, cheaper buildings or more services in existing buildings.

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MST reliability allows continuous unattended operation with extended or remote control, saving maintenance and operating staff. Any fault in the servo control circuits can quickly be located with simple test routines. Transistors and printed wiring give these circuits maximum reliability.



### self-tuning

The H1200 has a frequency following servo tuning system. Any frequency may be selected on the synthesizer decade dials in the associated MST drive equipment; the unattended transmitter automatically tunes itself in an average time of twenty seconds. Final stage tuning and loading servos continuously ensure automatic compensation for changes in aerial feeder impedance caused by weather conditions. Self-tuning gives *one-man* control of an entire transmitting station.

## Marconi telecommunications systems

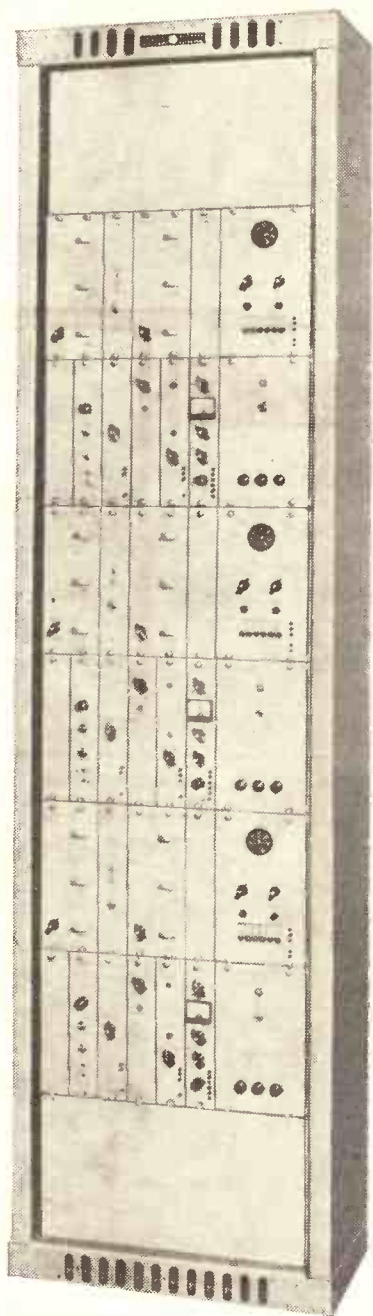
The Marconi Company Limited, Communications Division, Chelmsford, Essex, England

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LTD/HRI



# Marconi SELF-TUNING h.f. receivers



Three double-diversity  
H2002 receivers

The H2002 Series of MST receivers for high grade point-to-point h.f. communication services.  
H2002 double diversity f.s.k.  
H2102 double diversity i.s.b. or s.s.b.  
H2112 single path i.s.b. or s.s.b.

**NO OSCILLATORS**  
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**NO TUNING SCALES**

The new range of MST transistorized receivers uses synthesizers to provide accurate selection of 250,000 frequencies.

Elimination of manual tuning by a unique self-tuning system (using servo controlled varactor diodes) allows centralized extended control.

Exceptionally good frequency stability renders a.f.c. unnecessary on stable transmissions.

One-man control of an entire receiving station.

60% space saved by much smaller equipment and back-to-back and side-by-side installation.

RECEIVER



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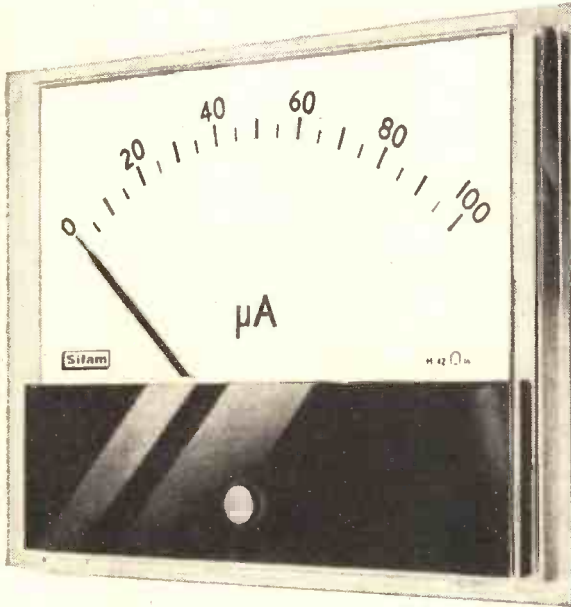
## Marconi telecommunications systems

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LTD/H55

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# no shadow of doubt...



## why Sifam 'CLARITY' instruments are specified, so often



The elimination of any solid surround to Sifam 'CLARITY' instruments eliminates top shadow, especially when instruments are mounted above eye level. This feature also provides greater readability, thereby minimising the risk of human error in recording readings.

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## INSTRUMENTS

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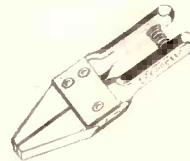
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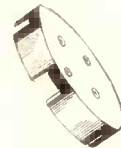
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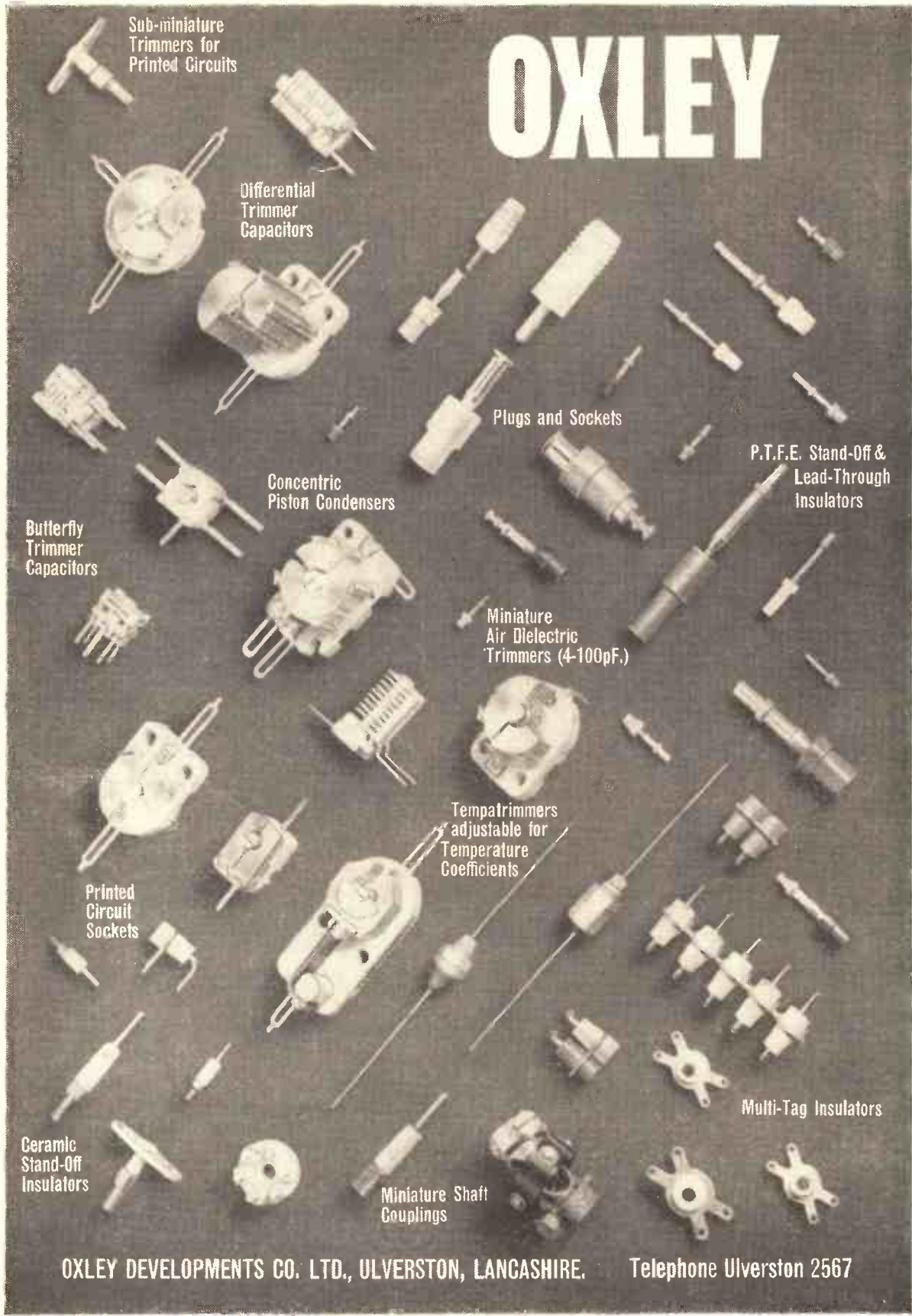
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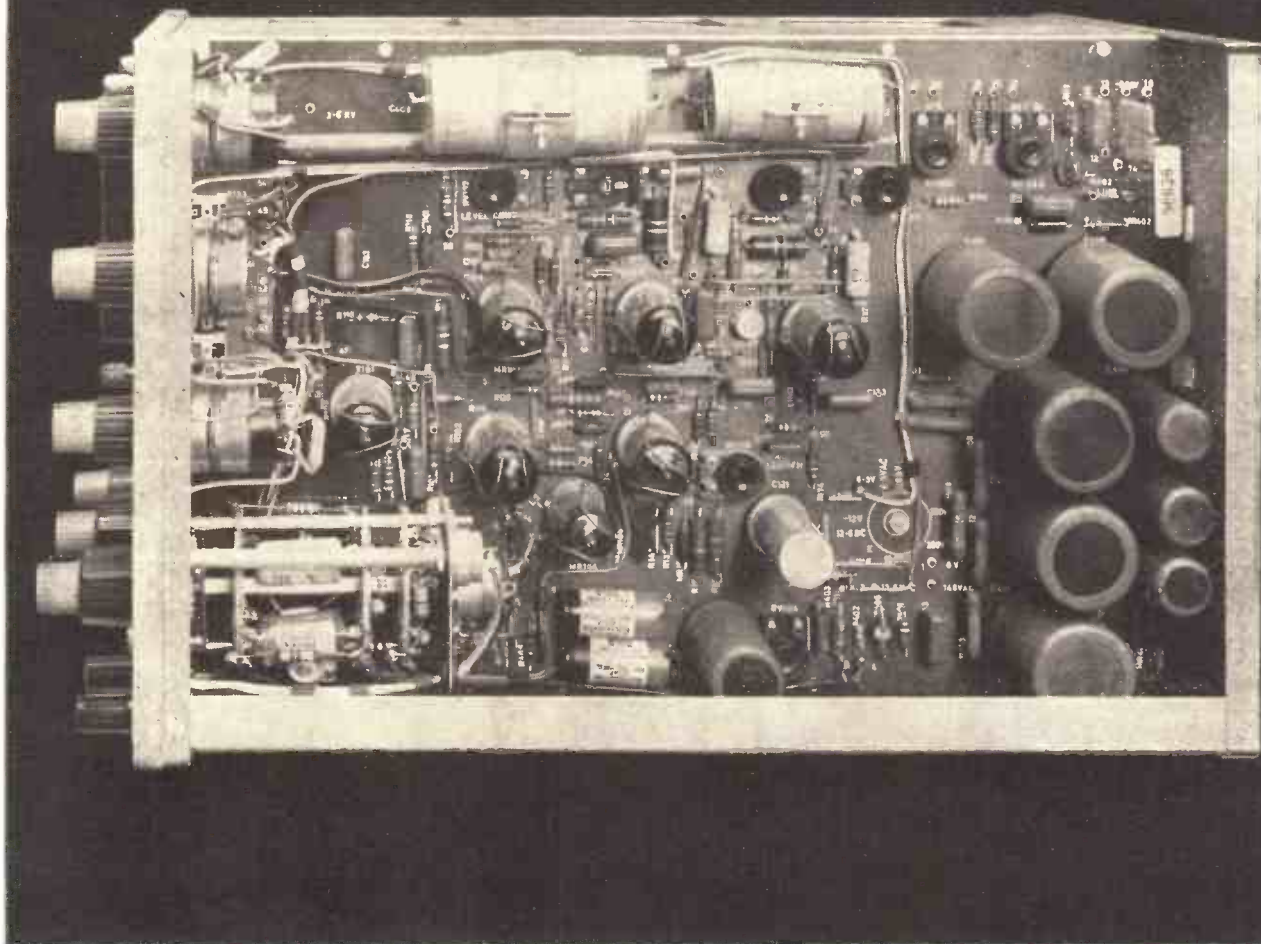
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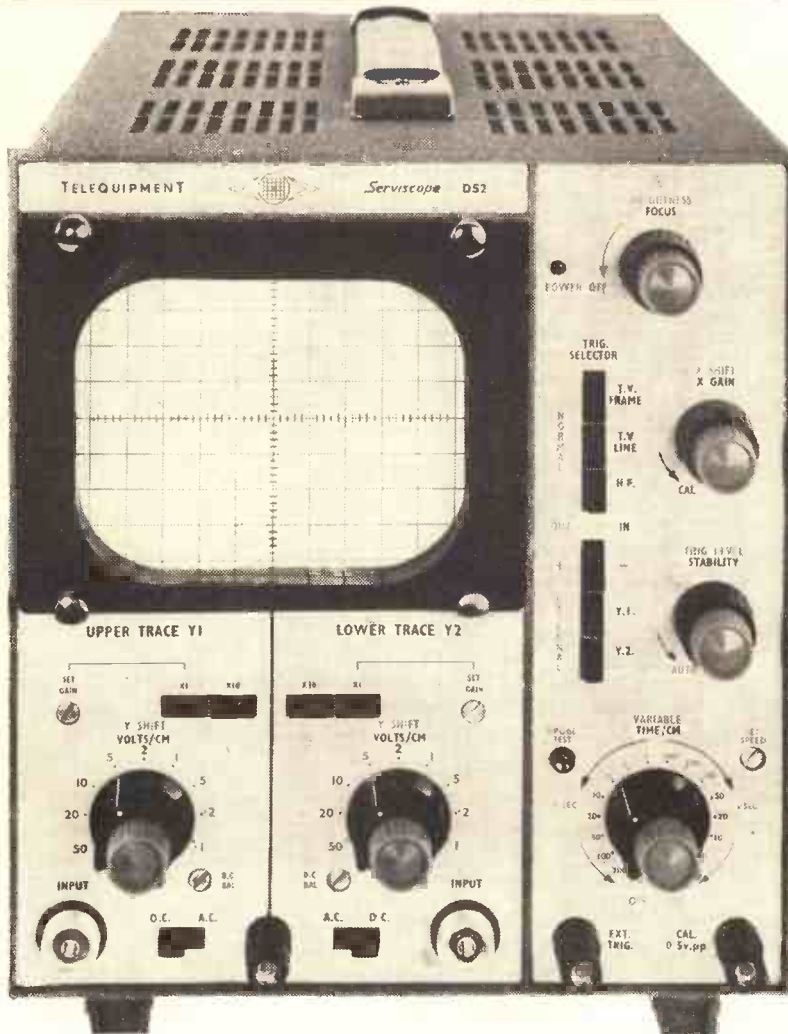
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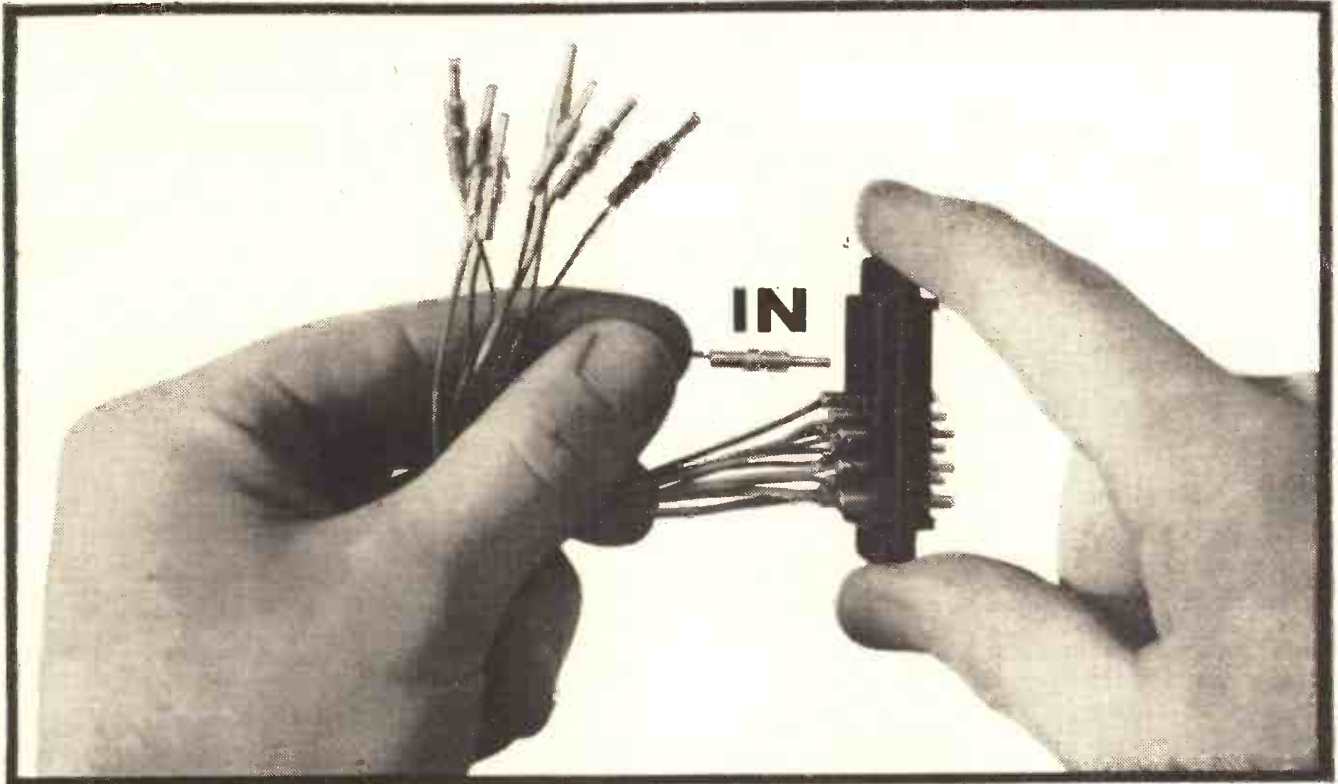
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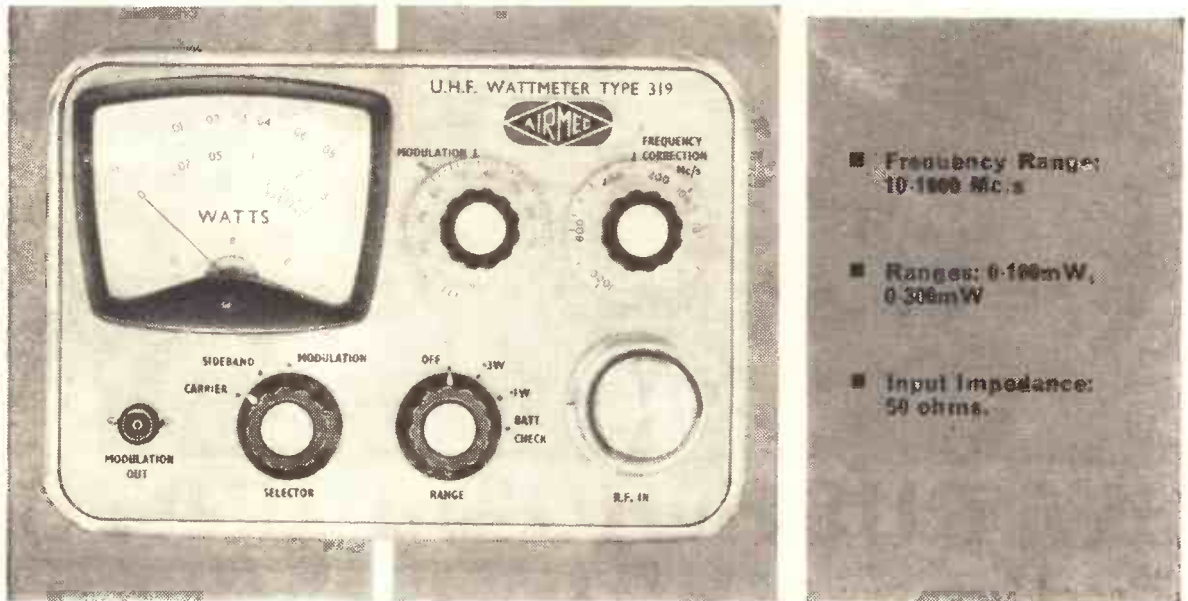


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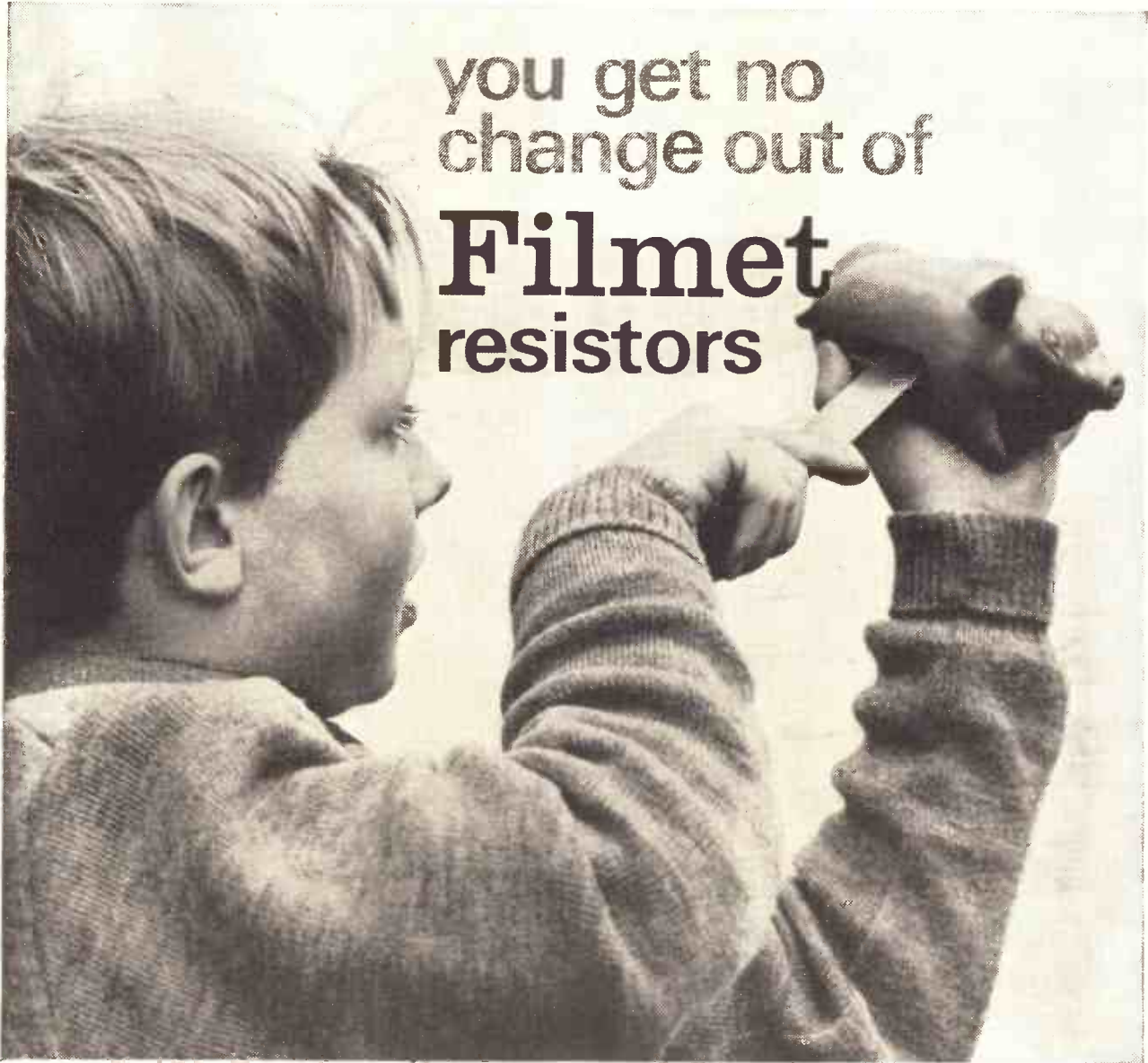
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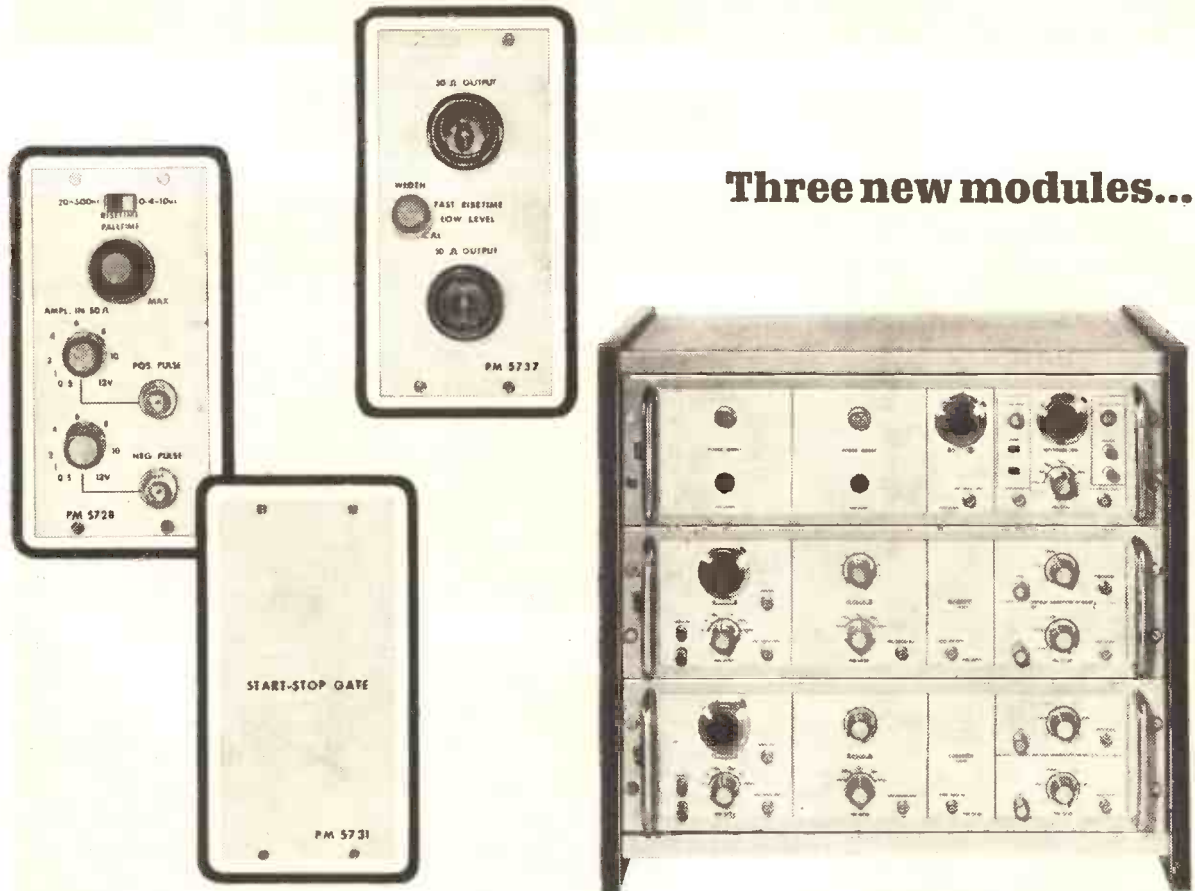
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## Three new modules...

### added to Philips modular pulse generator PM5720-40

Two new output modules and a new gate module have been added to the modular pulse generator PM 5720-40. The power output module PM 5728 provides pulses with a maximum amplitude of 12 V into a load of 50  $\Omega$  or higher at 100% duty cycle. Lower loads can be connected at reduced duty cycles. Simultaneous positive and negative pulses are available. Rise and fall time are linearly variable from 20 ns (typical value 15 ns) to 10  $\mu$ s.

The fast rise time unit PM 5737 provides two identical pulses of 1 V into 50  $\Omega$ . The twin outputs can be utilised for

reflection and similar measurements, one output being applied to an oscilloscope and the other to the network being studied. No power is wasted in resistive tee connectors. The twin outputs also provide a simple method of obtaining double pulses, one pulse is obtained direct from one output, the second from a simple open-circuited cable acting as a delay line. In this way repetition rates of up to 200 Mc/s can be simulated.

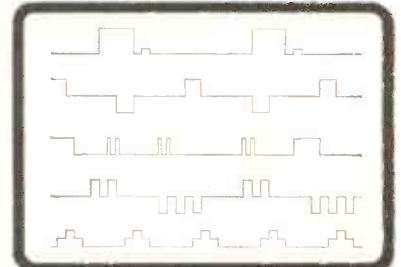
The gate unit PM 5731 performs an AND-function, the gate-open time of which can be defined by a start and a stop pulse. This

unit is particularly useful to provide more complex pulse programmes.

Additional modules are under continuous development and these three new modules are additional to the already existing units; together they make up a system which can be programmed to provide almost any required pulse or pulse sequence on one or several channels.

A survey of the available output units and some examples of pulses which can be obtained are given below.

Output units	PM 5727	PM 5728	PM 5737
Rise time	7 ns	15 ns . . . 10 $\mu$ s	0.3 ns
Fall time	7 ns	15 ns . . . 10 $\mu$ s	1.5 ns
Amplitude into 50 $\Omega$	max. 5 V	max. 12 V	1 V
Attenuation	1000x	24x	---
Main characteristics	Fast rise time Bandwidth of step attenuators 300 Mc/s	High amplitude; Variable rise and fall time	Very fast rise/fall time



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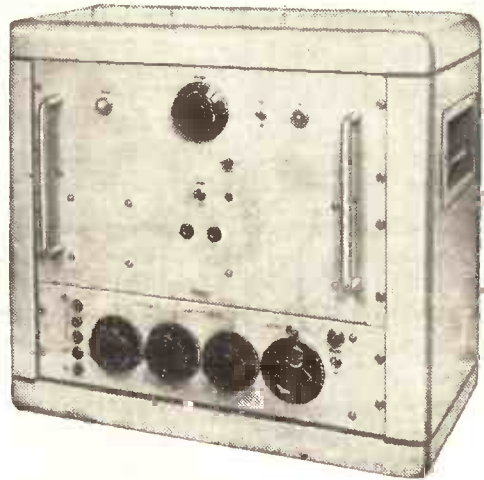
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# **Vortexion** quality equipment

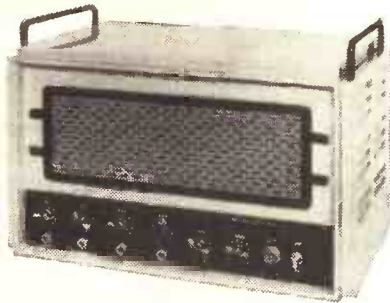
The 120/200 watt Amplifier can deliver its full power at any frequency in the range of 30 to 20,000 c.p.s. for which the response is accurate within 1 db with less than 0.2% distortion at 1,000 c.p.s. Noise level - 90 db. It can be used to drive mechanical devices, i.e., synchronous capstan or projector motors, etc., for which the power is over 140 watts on continuous sine wave. A floating series parallel output is provided for 100-120v. or 200-250v., and additional matching transformers for other impedances are available. The input is for 1 mW. 600 ohms.

## 120/200 WATT AMPLIFIER



## 30/50 WATT AMPLIFIER

The Vortexion 30/50 watt Amplifier can deliver 50 watts of speech and music or over 30 watts of continuous sine wave and the main amplifier has a response of 30 to 20,000 cps within 1 db at 0.1% distortion and outputs for 4, 7.5, 15 ohm and 100 volt line. Models are available with two, three or four mixed inputs which may be low impedance balanced line microphones, P.U. or Guitar inputs.



## ELECTRONIC MIXER AMPLIFIER

This high fidelity 10/15 watt Ultra Linear Amplifier has a built-in mixer and Baxandall tone controls. The standard model has 4 inputs, two for balanced 30 ohm microphones, one for pick-up C.C.I.R. compensated and one for tape or radio input. Alternative or additional inputs are available to special order. A feed direct out from the mixer is standard and output impedance of 4-8-16 ohms or 100 volt line are to choice. All inputs and outputs are at the rear and it has been designed for cool continuous operation either on 19 x 7in. rack panel form or in standard ventilated steel case.

Size 18 x 7½ x 9¼ in. deep.

Price of standard model £49.

The 12-way electronic mixer has facilities for mixing 12 balanced line microphones. Each of the 12 lines has its own potted mumetal shielded microphone transformer and input valve, each control is hermetically sealed. Muting switches are normally fitted on each channel and the unit is fed from its own mumetal shielded mains transformer and metal rectifier.

Also 3-way mixers and Peak Programme Meters.  
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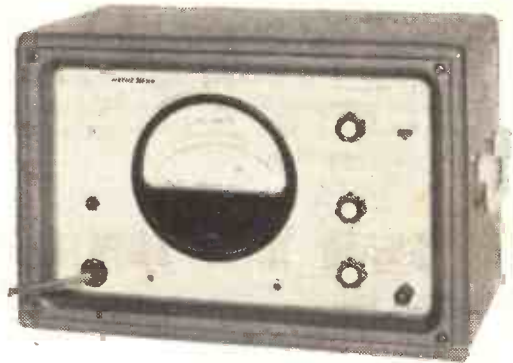
The Wayne Kerr M121 AF Voltmeter has open, linear scales for the accurate measurement of voltages with negligible loading on the source. The mirror-scale movements are individually calibrated in r.m.s. values and in dB relative to 1mW in 600 ohms. Exceptional linearity and stability have been achieved by including the rectifying elements in a current-feedback loop. The h.t. supply for all stages is fully stabilised, eliminating any undesired effects of mains fluctuations. A cathode-follower output stage is included to permit feed-through amplification of up to 60dB.

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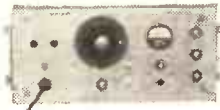
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1 mV to 10V (transformer): 600 $\Omega$  and 100k $\Omega$ ,  
balanced or unbalanced  
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High selectivity plus simple operation

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## WAYNE KERR



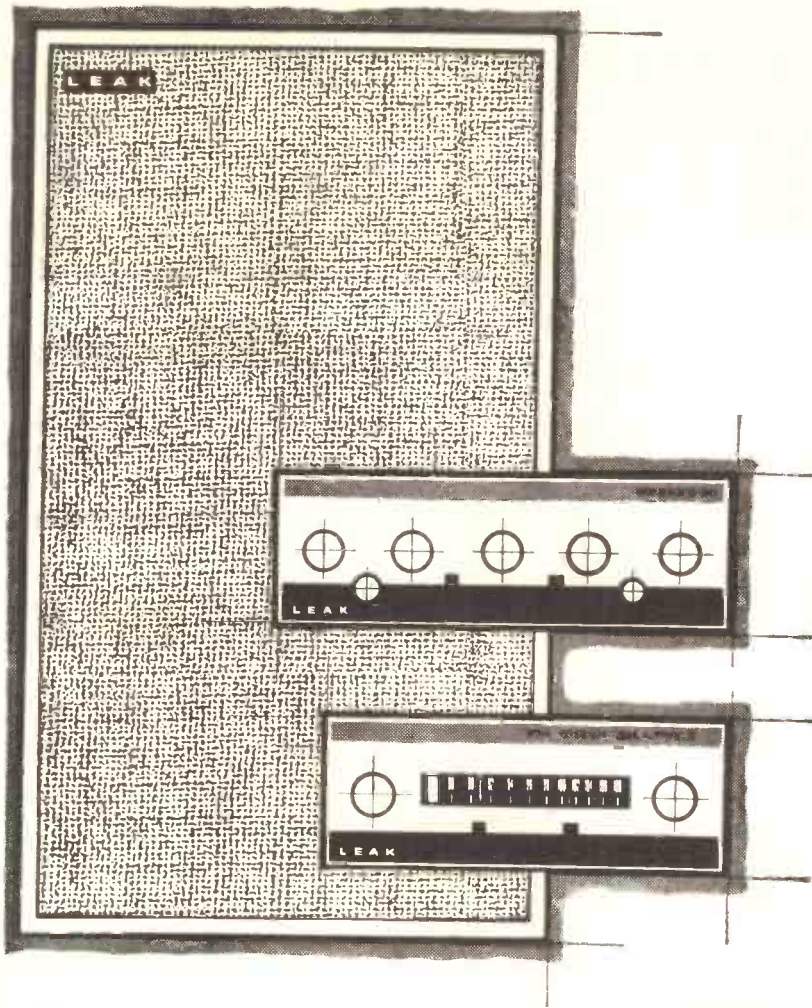
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Until you have built and used this set which is smaller than a matchbox, you will never know how exciting the British-designed Micro-6 is. Its range and power will amaze you as station after station pours in; you will find yourself able to enjoy radio where other sets often cannot be used at all. The two self-contained batteries will give 70 hours or more working life. Bandspread tuning over the higher frequency end of the M.W. Band enables Luxembourg to be tuned in with the ease and power of a local station. By now more than 20,000 Micro-6 sets have been built with outstanding success by constructors all over the world ranging from advanced electronic engineers to beginners. So start yours today.

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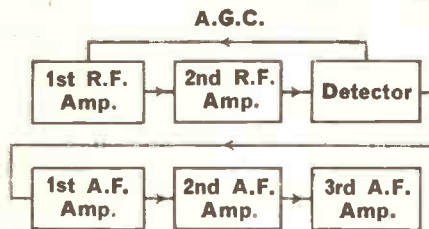
This Sinclair Amplifier is smaller than a 3d. piece! It has a frequency response from 30 to 50,000 c/s  $\pm 1$ dB and a gain of 60dB (1,000,000 times). The instructions supplied with each set of parts show how it can be used in a variety of ways which include a hi-fi amplifier which will even drive a loudspeaker, a broadband RF amplifier, an FM transmitter and a radio receiver, etc. It is also invaluable to modellers and experimenters. Building the micro-amp is simple.



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- MEASURES  $2'' \times 2''$



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Parts and instructions. 39/6

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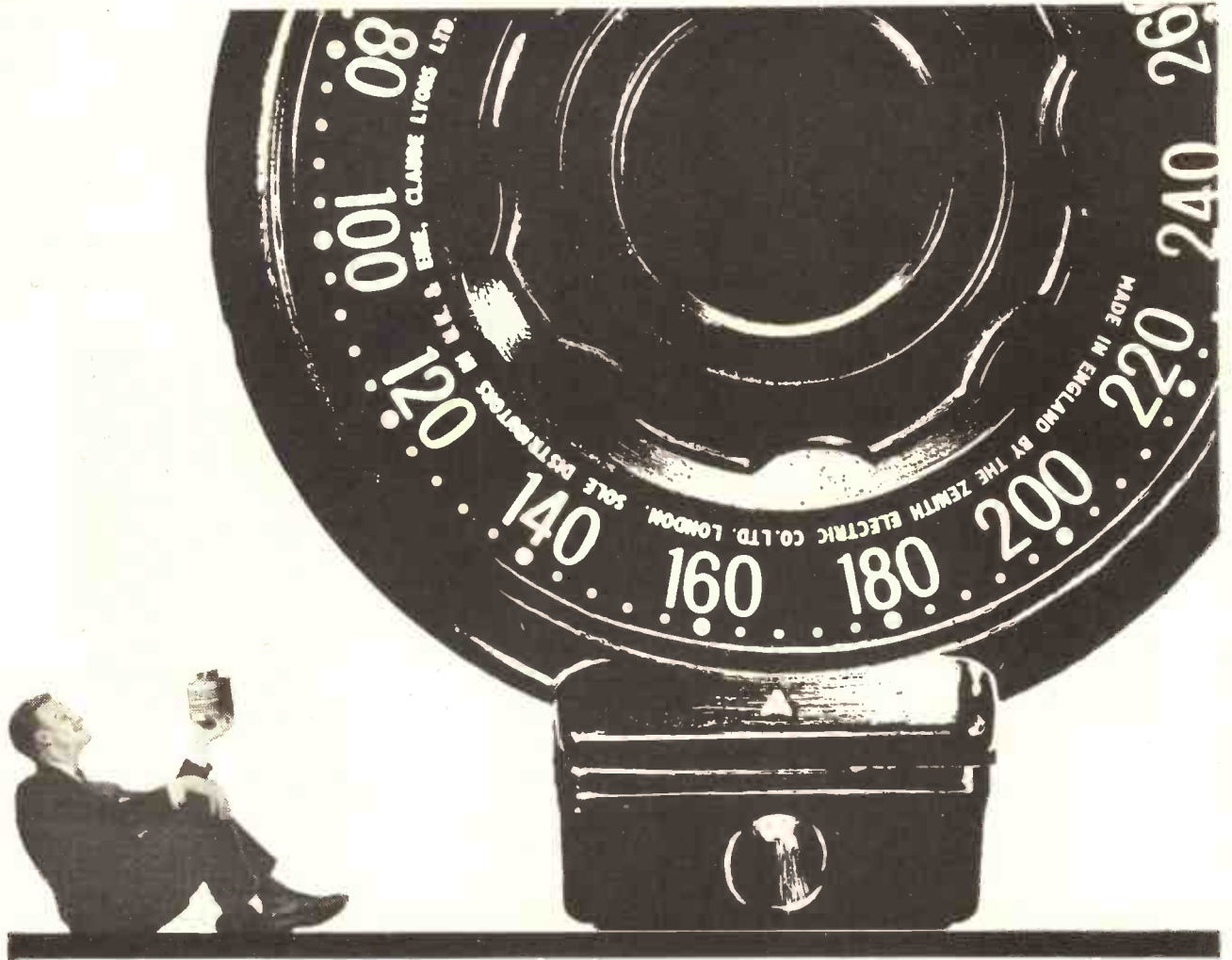
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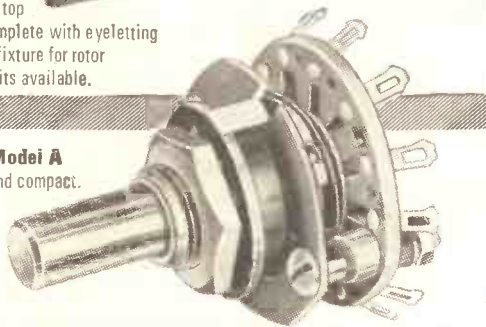
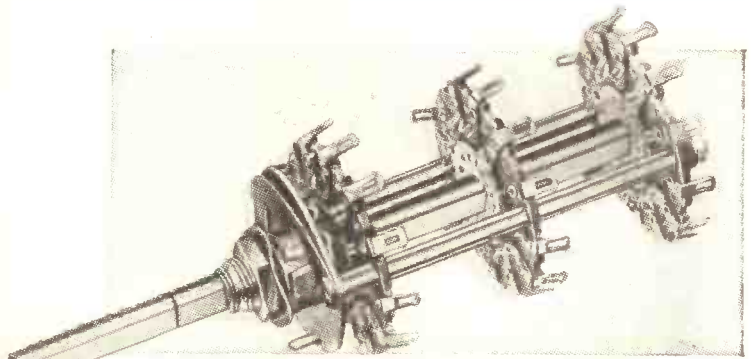
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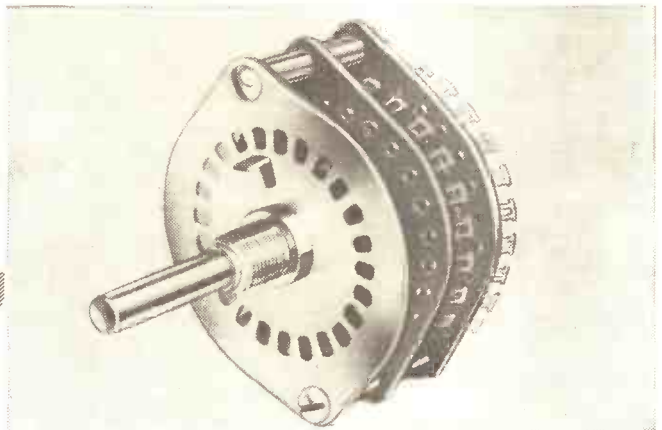
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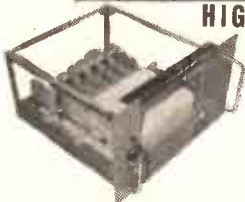
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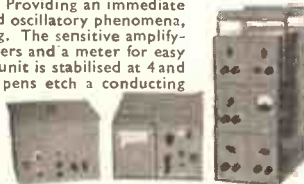
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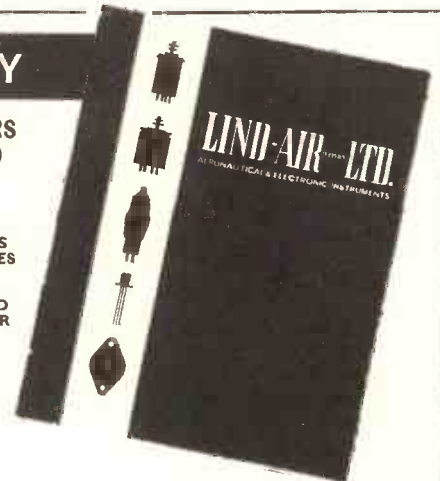
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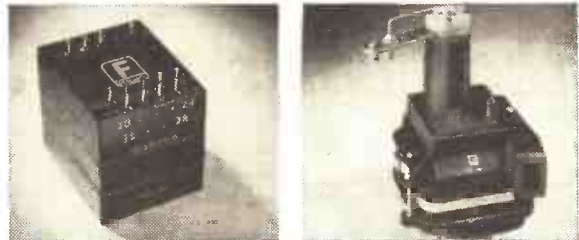
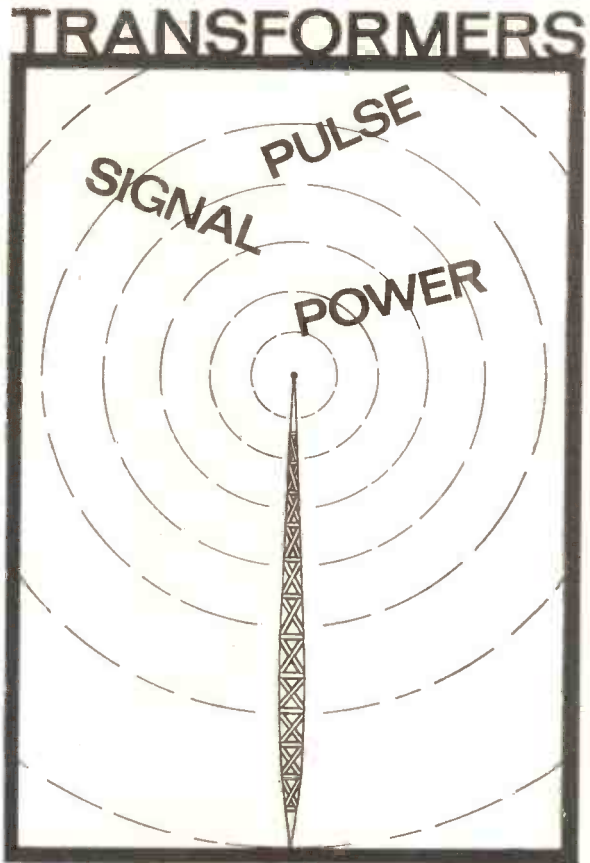
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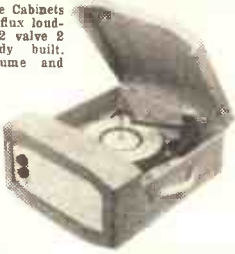
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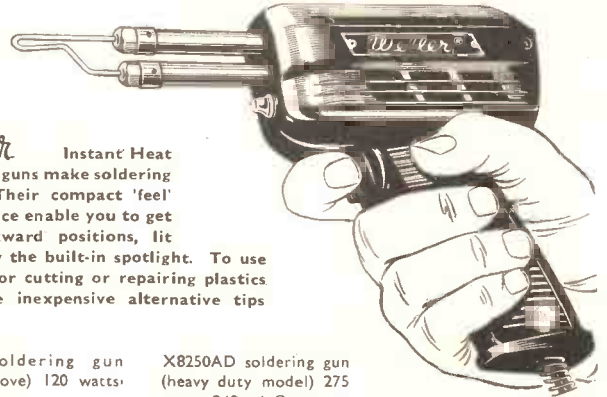
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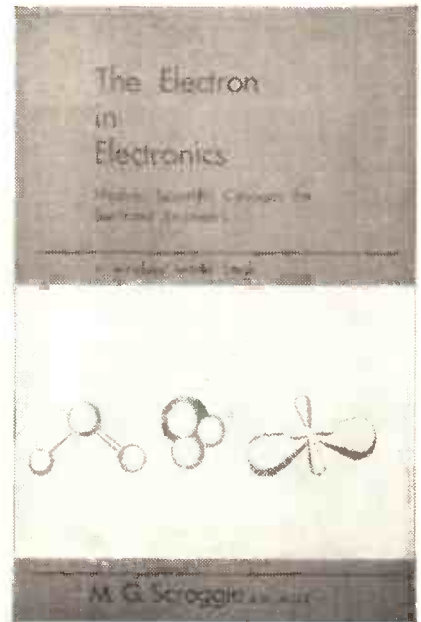
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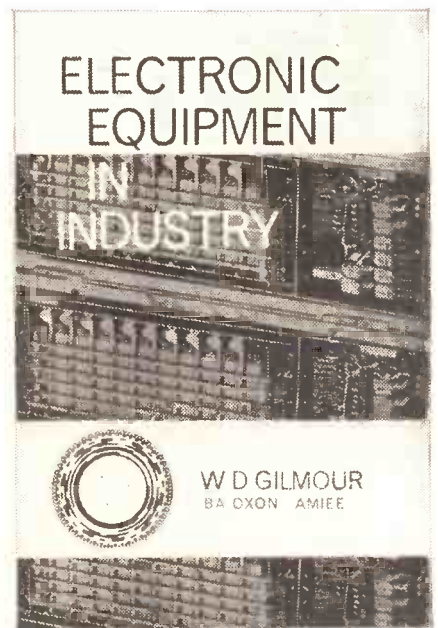
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5 1/2in. 1,200ft. 19/6	ea. for additional
7in. 1,800ft. 28/6	reels.

**SPECIAL OFFER.** 3in. Message tape 150ft. 3/9; 3



# GOVERNMENTS AGREE-

on the quality of the TEONEX range of valves. Governments all over the world have ordered TEONEX valves requiring compliance to E.V.S. or M.I.L. specifications.

Up to now, TEONEX valves have been available only for Government contracts.

In response to many enquiries, the TEONEX range, incorporating the entire working range of British-produced valves or their equivalents, has now been made available for use *outside the U.K. only.*

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Westbourne Grove Mews,  
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Suppliers of Elliott, Cambridge and Pye instruments.

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E.I.D. & G.P.O. APPROVED CONTRACTOR TO H.M. GOVT.  
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MULTIMOTOR MK. IV

**REPAIR SERVICE  
7-14 DAYS**

We specialise in repair, calibration and conversion of all types of instruments, industrial and precision grade to BSS.89.

Release notes and certificates of accuracy on request.

Telescopic Aerial Masts. Tubular Steel Copperised spray finish ring cam locking on each section provides for full or any height required. Suitable all fixings and base locations. Bottom section 1 1/2 in. dia. 20ft. (4 sections). Closed 6ft. 3in. Weight 16lb. 55/-, carr. 5/-, 34ft. (6 sections) closed 6ft. 6in. Weight 20lb. 75/-, carr. 5/-.

Auto Transformers 3 KVA. 110/250 v. mounted in steel case with external hand voltage regulator. American surplus. Brand New £12/10/-, carr. 15/-.

Siemens High Speed Relays. 50 ohm + 50 ohm type H96B 10/6 ea.; 500 ohm + 500 ohm type H96D 10/6 ea.; 1,700 ohm + 1,700 ohm type H96E 14/6 ea.

Siemens Miniature Relays. Size 1 1/2 x 1 x 1 in. Res. 700 ohm consumption 18mA on 12 volts. 2 pole 2 way contacts, contact rating up to 2 amps, 100 v. 30 watts max., 6/- ea. Heavy Duty Type 250 ohms 12-24 v. operation 48mA on 12 v. contacts at 10 amps max. 7/6 ea. Headphones Moving Coil. Finest quality with Ear Muffs for noise excluding, 12/6 ea., wired with moving coil mike, 17/6 ea. Type DLRS bal. armature, 9/6.

Blower Motors. Ideal for car heaters, etc. Ex R.A.F. equipment, 12-24 volt, D.C., 39/6, also small type high speed will work from 41-6-12 volt supply, 14/6 ea.

Small Geared Motors. Final speed 80 r.p.m. Working voltage 6-12 v. Overall size 4 x 2 x 2 in. 15/-, carr. 2/-.

Pressure Gauge. 2in. round Brass case 0-160lb., 9/6 ea.

Tannoy Loud Hailers. 3 watt output. Enclosed in strong wooded case, with steel protection, 27/6 ea.

Carbon Hand Mike, with replaceable insert, 7/6 ea.

Miniature Plugs and Sockets. Jones type, 8 Way, 3/6 pt., 12 Way, 4/6 pr.

Transmitter. Type BC 626 Part of TR S.C.E. 622 Range 100-156 Mc/s. complete with all valves par 332, 21/-, carr. 3/-.

Field Telephones. American type EE.8. complete in leather carrying case, £3/10/0, pr. post 5/-.

Motor Generator. Type 4B Input 28v. D.C. Output 80 v. 2000 cycle 2 kw. £12, carr. 15/-.

Aerial Change-over Relay. D.P.C.O. Heavy silver contacts, American Muff, 12/6 ea. Post Office Relays. 3000 ser. 2C0; 23; Coil Slugged 140 ohm 2C0; 2M; 1,000 ohms 2C0; Coil Slugged 500 ohm, all at 6/- ea. P. & P. 1/-.

Carpenters Type Relay 5HM52. 160 T. at 1.2 ohm; 3,000 T. at 150 ohms; 3,000 T. at 250 ohm, complete with securing springs and plug in base. 15/- ea. P. & P. 1/-.

G.E.C. type M1095 2M: 2B; 670 ohm, 7/6 ea.

Signal Generator. Type 106 covers 5.5-55 Megs complete in carrying case. Muff. Salford Insts. £5/0/0, Carr. 10/-.

Liner Actuator. Max. load 100 lb., 24 or 12 volts D.C. operation, reversing motor operates stainless steel pushrod through a built-in gearbox, travel up to 3in. £4/10/-, carr. 3/6.

Morse Key Assembly. Key with base, cover and terminals, complete with leads. 6/11.

Test Meter. 3 1/2 in. x 8 1/2 in. x 2 1/2 in. D.C. M.C. Ranges 0-500 ohms, 0-60 mA., 0-3 v., 0-1.5 volts. Ranges can be extended by additional resistances. 12/6 ea., carr. 1/6.

Desk Telephones. G.P.O. type, brand new in original cartons. 27/6, carr. 2/6.

38 Sets 6-9 Mezs. Walkie-Talkie sets complete as supplied to Forces. 21/-, carr. 3/-.

Thermostats. G.M. type Teddington 110-190° Far., 230 volts, current rating 9 amps., complete with capillary tube. New and boxed. 30/-, carr. 3/-.

5 GPI Cathode Ray Tube. New and boxed. 25/-, carr. 3/6.

807 Valves, 6/6. 832 valves 25/-, carr. 2/6. 5R4WGY. Valves 12/6 ea., post 1/6.

Terms: C.W.O.

**SPECIAL OFFER AR.88 RECEIVERS**

A.R.88.D Receiver. £25.0.0. each, carr. £1.  
A.R.88.LF Receiver £20.0.0. each, carr. £1  
All receivers air tested before dispatch.

**B. S. RADIO AND  
ELECTRICAL STORE**

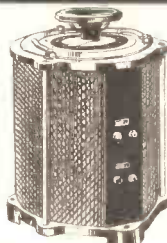
108 CHESTER STREET, BIRKENHEAD, CHESHIRE.

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VARIABLE VOLTAGE TRANSFORMERS**

**PORTABLE**



Input 230 v. A.C. Output variable 0-260 v. A.C. at 2.5 amp. Fitted in beautifully finished steel case. Complete with voltmeter, pilot lamp, fuse, switch, carrying handle, £9/17/6 P.&C.5/-.



50 AMPS.

INPUT 230 v. A.C. 50/60~  
BRAND NEW. Carriage Paid. Buy direct from the importer, keenest prices in the country. All Types (and Spares) from 1/6 to 50 amp. available from stock.

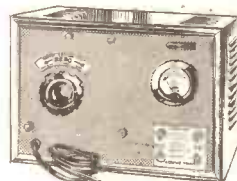
0-260 v. at 1/2 amp. ....	£3 3 0
*0-260 v. at 1 amp. ....	£4 10 0
*0-260 v. at 2.5 amps ....	£5 17 6
2.5 amps., Portable ....	£9 17 6
*0-260 v. at 4 amps. ....	£8 7 6
*0-260 v. at 5 amps. ....	£9 0 0
*0-260 v. at 8 amps. ....	£13 10 0
*0-260 v. at 10 amps. ....	£17 0 0
*0-260 v. at 12 amps. ....	£19 10 0
*0-260 v. at 20 amps. ....	£32 10 0
*0-260 v. at 37.5 amps. ....	£65 0 0
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\*These instruments are fully shrouded.



**INSULATED TERMINALS**  
available in black, red, white, yellow, blue and green. New 15/- per doz. P. & P. 1/-.

**7 AMP. A.C./D.C. VARIABLE OUTPUT  
POWER UNIT**



Input 230 v. A.C. Output continuously VARIABLE from 0 to 260 v. A.C. OR 0 to 230 v. D.C. at 7 a. Robustly constructed in metal case, complete with safety fuse, neon indicator and voltmeter. Size 17 x 12 x 7 in. Weight 36lb. Price £34/10/- Carriage 20/-.

**1 AMP. OPEN TYPE.**

(Type 1A) Compact well constructed unit designed for building into equipment. Panel or rack mounting, extending shaft. Complete with engraved voltage panel and control knob. Input 250 v. A.C. Output variable 0-260 v. Ideally suited for Manufacturers of variable voltage equipment. Price £4/17/6 post paid.

**100 WATT POWER  
RHEOSTATS (NEW)**

Ceramic construction winding embedded in Vitreous Enamel heavy duty brush assembly designed for continuous duty.

AVAILABLE FROM STOCK in the FOLLOWING 9 VALUES:  
10 ohm, 3a.; 25 ohm, 2 a.; 50 ohm, 1.4 a.; 100 ohm, 1 a.; 250 ohm, 7 a.; 500 ohm, 45 a.; 1,000 ohm, 280 mA.; 1,500 ohm, 230 mA.; 2,500 ohm, 2 a. Diameter 3 1/2 in. Shaft length 3 1/2 in. dia. 1 1/2 in. 27/6. P. & P. 1/6.

**NEW 1/2 AMP. FULL  
RANGE VARIABLE  
VOLTAGE  
TRANSFORMER**



Input 230 v. A.C. Output continuously variable from 0 to 260 v. at 1/2 amp. Size: dia. 3in., depth 3 1/2 in. including shaft, single hole fixing. Easily built into equipment. Ideal for manufacturers or Lab. use £3/3/0

**SLIDER  
RESISTANCES**



1 ohm, 12 amp., 17/6; 1.2 ohm, 14 amp. 27/6; 75 ohm, 2 amp. 37/6; 200 ohm, 1.25 amp. 37/6; 36 ohm, 6.5 to 2.8 amp., tapered winding, geared drive (less knob), 37/6. P. & P. 3/6.



**INSULATION  
TESTERS  
(NEW)**

Test to I.E.E. Spec. Rugged metal construction, suitable for bench or field work, constant speed clutch. Size L. 8in., W. 4in., H. 6in. Weight 6lb. 500 volt, 500 megohms. Price £22, carriage paid. 1,000 volts, 1,000 megohms, £28, carriage paid.

**SERVICE TRADING COMPANY**





# SERVICE TRADING CO

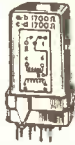
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## ULTRA VIOLET BULBS

Easy to use source of U.V. for dozens of practical and experimental uses:  
 12 volt 36 watt A.C./D.C. SBC 6/6. P. & P. 1/-.  
 12 volt 60 watt A.C./D.C. SBC 8/6. P. & P. 1/-.  
 Transformer to suit the above. Input 200-240 v. A.C., 12 volt 36 watts, 16/6; P. & P. 2/6. Input 200-240 v. A.C., 12 volt 60 watt, 22/6. P. & P. 3/6.  
 Set of 4 Colours FLUORESCENT PAINT. Red, yellow, green and cerise. In 1/2 oz. tins. Ideal for use with the above Ultra Violet Bulbs, 9/6, plus 1/6 P. & P.

## SIEMENS SEALED HIGH SPEED RELAYS

H96A, 2.2 ohm + 2.2 ohm, new.  
 H96G, 50 ohm + 50 ohm, new.  
 H96C, 145 ohm + 145 ohm, new.  
 H96D, 500 ohm + 500 ohm, new.  
 H96E, 1,700 ohm + 1,700 ohm, ex. equip., all at 12/6 each. P. & P. 1/- on each Relay.



## P.O. RELAYS, Type 3000

100 ohm, 3 c/o, 2 make, 2 break.  
 200 ohm, 6 c/o.  
 500 ohm, 1 Heavy duty c/o.  
 500 ohm, 4 Heavy duty make.  
 2,000 ohm, 4 make, 4 break.  
 16,000 ohm, 2 make, 2 break.  
 20,000 ohm, 2 Heavy duty make.  
 All at 12/6 each, plus 1/- P. & P.

## G.E.C. SEALED RELAYS

M1069 5,000 ohm, 2 c/o. M1084 180 ohm, 4 c/o.  
 M1092 670 ohm, 4 c/o. M1095 670 ohm, 2 m. 2 b.  
 M1100 670 ohm, 2 c/o. Ex new equipment.  
 All at 12/6 each plus 1/- P. & P.

**14,000 OHM SEALED RELAY.** High Speed single c/o, Platinum contacts. Super-sensitive, ideal for Transistor circuitry. Will operate on 1 milliamp 25/- P. & P. 1/-.

**20-way STRIP** containing standard Post Office telephone Jack, Sockets, overall size 11 x 3 1/2 x 1/2 in. New. Price 15/- each. P. & P. 1/6.

## SPECIAL REVERSING 24 VOLT D.C. MOTOR 2-AMPERE

Quadrant moves 90 degrees with limit switches. Ideal for opening doors, etc. Price 32/6 P. & P. 3/-.

**SOLENOID.** Overall length 3 1/2 in., stroke 1/2 in. Maximum push 8 oz. 12-24 v. D.C. operation. D.C. resistance 35 ohm. Price 8/6. P. & P. 1/6.  
**SOLENOID Heavy Duty 230 v. A.C.** Approx. 3lb. pull. 15/- P. & P. 1/6.

**SOLENOID OPERATED MAGNETIC RELAY.** Type Sc/3944, 4 Pole c/o., 10 amp. Contacts, 24 volt D.C. operation. 12/6 each. P. & P. 1/6.

## LATEST HIGH SPEED MAGNETIC COUNTERS

4 figure 10 impulses per second. Type 100D, 4.1 ohm coil, 3.6v. D.C. operation. Type 100A, 500 ohm coil, 18-24 v. D.C. operation. Type 100B, 2,300 ohm coil, 36-48 v. D.C. operation. Any type 15/- each, plus 1/6 P. & P.

**RESETTABLE HIGH SPEED COUNTER**  
 4 figure 1,000 ohm coil, 36-48 v. D.C. operation, £3/10/-, 1/6 P. & P.

## WIMSHURST ELECTROSTATIC GENERATORS



Really well constructed machine. Ideal for School and Laboratory to demonstrate the various effects associated with static energy. Will work well in any atmospheric conditions giving a spark over 3in. long in dry weather. 1 1/2 in. dia. twin plates. 2 Leyden jars. Discharge electrodes. Heavily plated fittings, mounted on solid wooden base. Outstanding value at £13/17/6. Carriage U.K. (B.R.S.) 10/-.

**ELECTRIC CHECK METER** (Sangamo Weston) 200/240 volt, A.C., 40 amp. As new 35/- plus 3/6 P. & P.

**0-4 MINUTE MECHANICAL TIME SWITCH.** 16 amp. D.P. switch, complete with knob. Will switch off any setting between 0-4 min. As new, fraction of maker's price, 10/- P. & P. 2/6.

**CRATOR.** 4 way 16 amp, 250 v. A.C. switch. 3 on, 1 off, position. Complete with knobs. 7/6. P. & P. 1/6.

**CROMPTON PARKINSON BRAND NEW 1/2 h.p. MOTORS.** 230/250 VOLT A.C. 1,400 R.P.M. Fitted with 2 1/2 x 1/2 in. SPINDLE. Price £3/5/- Carriage 8/6.

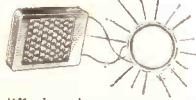
## HIGH SPEED BLOWER UNIT

200/250 volt A.C. Powerful 2-speed motor, 11,000 and 13,000 R.P.M. 17/6, plus P. & P. 2/6.

## AUTO TRANSFORMERS

Step up, step down. 110-200-220-240 v. Fully shrouded, New. 300 watt type £2/6/6 each. P. & P. 2/6. 500 watt type £3/7/6 each. P. & P. 3/9. 1,000 watt type £4/10/- each. P. & P. 6/6.

## FIRST AGAIN! TYPE 34R SILICON SOLAR CELL



Four .5 volt units series connected in high impact polystyrene case, flying lead connections. Specially designed diffusing lens system to ensure maximum light pick-up. Output—up to 2 v. at 16—20 mA. in bright sunlight. Wider spectral response, and thirty times the efficiency of selenium cells. As used to power earth satellites! 37/6, and 1/- P. & P.  
**JUST PUBLISHED "SOLAR CELL & PHOTO-CELL EXPERIMENTERS GUIDE."** Teaches the principles of light sensitive devices and their application. 26/- post paid.

**230 v. A.C. RELAY.** Type 1, 2 c/o, 2 amp. contacts, 9/6. Type 2, 2 x 15 amp. break, 2 x 2 amp. make, 1 x 2 amp. break. 11/6. Both types ex new equip. P. & P. 1/6 each.

**230 VOLT A.C. GEARED MOTORS**  
 Type D16G 5 r.p.m. 1.7lb. inch £2/9/6. P. & P. 2/6  
 Type D16G 13 r.p.m. 1.45lb. inch £2/12/6. P. & P. 2/6

**UNISELECTOR** 8 bank, 25 way, all non-bridging, full wipers, twin coil, 950 ohm. Each unused £3/2/6. P. & P. 4/6.

**MINIATURE UNISELECTOR SWITCH.** 3 banks of 11 positions, plus homing bank. 40 ohm coil. 24-36 v. operation. Ex equip. Individually tested. 22/6, plus 2/6. P. & P.

## LIGHT SENSITIVE SWITCH

Kit and parts including ORP.12 Cadmium Sulphide Photo-cell, Relay, Transistor and Circuit. Now supplied with new Siemens High Speed Relay for 6 or 12 volt operation. Price 25/-, plus 2/6. P. & P.  
**ORP.12 and Circuit 8/6, post paid.**

## A.C. MAINS MODEL

Incorporates main transformer, rectifier and special relay with 3, 5 amp. mains c/o contacts. Price inc. circuit 47/6. Plus 2/6 P. & P.

**AVO METER CALIBRATION TEST UNIT, TYPE CT155.** A modern precision instrument giving 7 standard voltages, 1 v. A.C. 2.5 v. A.C. 10 v. A.C., 25 v. A.C., 100 v. A.C. and 250 mV. A.C. Also 250 mV. D.C. from internal standard cell. Internal power supply 110-250 v. A.C. contained in portable carrying case. Size: 11 x 8 x 7 in. As new £6/10/- P. & P. 10/6.

**SEMI-AUTOMATIC "BUG" SUPER SPEED, MORSE KEY.** 7 adjustments, precision tooled, speed adjustable 10 w.p.m. to as high as desired. Weight 2 1/2 lb. £4/12/6, post paid.

**TRANSISTORISED FULLY AUTOMATIC ELECTRONIC KEYS.** 230v. A.C. or Battery operated. Incorporates built-in monitor Oscillator, Speaker, and Keying Lever. Adjustable speeds. Keying either auto., semi-auto. or hold. 4 diodes. 7 transistors. Price £16/10/-, plus 4/6 P. & P.



**TRANSISTORISED MORSE OSCILLATOR** Fitted 2 1/2 in. Moving Coil Speaker. Uses type PP3 or equiv. 9 v. battery. Complete with latest design Morse Key, 22/6, plus 1/6. P. & P.

**KEYING LEVER.** Especially designed for use with all types of electronic keys. Fully adjustable micro-switch action, no contact bounce, precision made, finely polished parts, screw down base. Price £4/4/-, post paid.

**MINIATURE IMMERSION HEATER.** 6in. x 3/4in., 240 volt, 120 watt, 6/6 plus 2/- P. & P.

1st grade	TRANSISTOR	Brand new	
OC28	17/- OC83	6/- 2N458	20/-
OC29	18/- OC139	12/- 2S019	30/-
OC41	7/- OC140	19/- SB345	7/6
OC44	6/6 OC171	9/- TK208	4/-
OC45	5/- OC200	10/6 AC107	14/6
OC71	5/- OC203	14/- AF114	11/-
OC72	7/- Get 104	6/- AF115	10/-
OC73	6/- Get 105	10/- AF116	10/-
OC75	7/- Get 573	12/6 AF117	9/6
OC76	8/- 2N706A	17/6 BC211	10/-
OC81*			

\*Available in Matched Pairs.

## DIODES

OA91 ..... 3/- IS111 ..... 4/-  
 SX781 ..... 4/- ZS10B ..... 3/-

## ZENERS 5%

All 1/2 watt 5% at 10/- each, 4.3 v., 4.7 v., 5.1 v., 5.6 v., 6.2 v., 6.8 v., 7.5 v., 8.2 v., 9.1 v., 10 v., 12 v., 15 v., 16 v., 22 v.

## HEAVY DUTY L.T. TRANSFORMER

Very conservatively rated for continuous duty. Input 110-260 volts, multi-tapped, 50 cycles, single phase. Output 28, 29, 30, 31 volts at 21 amp. Price £6/15/- Carr. 10/-.

## L.T. TRANSFORMERS

All primaries 220-240 volts.	Type	Sec Taps	Price Carr.
1	30, 32, 34, 36 v.	at 5 amps.	£2.17.6 4/-
2	30, 40, 50 v.	at 5 amps	£4.15.0 4/-
3	10, 17, 18 v.	at 10 amps	£2.17.6 4/-
4	6, 12 v.	at 20 amps	£3.12.6 5/-
5	17, 18, 20 v.	at 20 amps	£5. 2.6 5/-
6	6, 12, 20 v.	at 20 amps	£4.15.0 7/6
7	24 v.	at 10 amps	£3. 5.0 4/-

## A.C. AMMETERS

0-1, 0-5, 0-10, 0-15, 0-20 amp. F.R. 2 1/2 in. dia. All at 21/- each.

## A.C. VOLTMETERS

0-25 v., 0-50 v., 0-150 v. M.I., 2 1/2 in. Flush round all at 21/- each P. & P. extra.

0-300 v. A.C. Rect. M-Coil 2 1/2 in. 29/-  
 0-300 v. A.C. Rect. M-Coil 3 1/2 in. Type W23. 55/-

## D.C. AMMETERS

0-5 amp. D.C. M.I. 2 1/2 in. Rnd. 11/6  
 0-500 Microamp. sub-min. 1 1/2 in. dia. Scaled 0-1 milliamp 21/-

## CONDENSER

8,000 mfd., 50 v., 2 1/2 in. x 4 1/2 in. 12/6

**DELCO 12-27 VOLT D.C. SHUNT WOUND MOTOR.** 5,400 r.p.m. Torque 4in. oz. double spindle, smooth running ex-new equip. 12/6 P. & P. 2/6.

**VAN DE GRAAF ELECTRO-STATIC GENERATOR,** fitted with motor drive for 230 v. A.C. giving a potential of approx. 50,000 volts. Supplied absolutely complete, including accessories for carrying out a number of interesting experiments, and full instructions. This instrument is completely safe, and ideally-suited for School demonstrations. Price £6/6/- plus 4/- P. & P. Leaflet on request.

**Latest type SIEMENS MINIATURE RELAYS** in Transparent Case. Gold-plated spring sets. 4 c/o 700 ohm coil. 25 v. D.C. operation. Size 1 1/2 x 1 1/2 x 1 1/2 in. New in maker's packing. Price 12/6. As above 2 c/o 700 ohm coil size 3/8 x 1 1/2 x 1 1/2 in. 15/- including base.

## BUILD AN EFFICIENT STROBE UNIT FOR ONLY "37/6"

The ideal instrument for workshop, lab. or factory. This wonderful device enables you to "freeze" motion and examine moving parts as if stationary. We supply a simple circuit diagram and all electrical parts, including the NSP2 Strobe tube which will enable you to easily and quickly construct a unit for infinite variety of speeds, from 1 flash in several seconds to several thousands per minute. New, modified circuits bring price down to 37/6, plus 3/- P. & P.  
**NSP2 CV2296 STROBOTRON FLASH TUBE** made by Ferranti, brand new, I.O. base. Price 15/- P. & P. 1/-.

**SX 631 SILICON RECTIFIER.** 100 v. PIV. 750 mA. in air or 2 amp. on 2 x 2 all, heat sink, 3/6 each. P. & P. 6d., or 4 to make bridge 12/- P. & P. 1/-.

**DIALS FOR AUTOMATIC TELEPHONES,** used but good condition, 12/6 ea., plus 2/6 P. & P.

ALL MAIL ORDERS. ALSO CALLERS AT:  
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 Open till 1 p.m. Thursday and all day Saturday.

## NEW LIST OF BARGAINS

Transistor ferrite rod aerial with medium and long wave coils with circuit. 7/6.  
 Oscillator Coil and set of 3 I.F. transformers for transistor set with circuit, 12/6. Tuning Condenser to suit, air-spaced, with trimmers, 9/-.  
 Ditto, but min. 10 mm. 12/6 the set, two-gang condensers to suit 8/6 (request sub. min. circuit).  
 Midget 3in. P.M. Loudspeaker, 3 ohm. 12/6, 80 ohm 13/6.  
 Midget 208 pF + 176 pF two-gang Tuning Condenser with trimmers for transistor set. Price 9/-.  
 Push-Pull Transformer. Sub-miniature. 8/6.  
 .0005 mfd. Single Tuning Condenser. Solid dielectric 4in. spindle for transistor of Crystal set, with spindle tapped 6 BA. 2/6.  
 46 Sets (Receiver/Transmitter pack set). Unused sets complete except for crystals, 19/6. Post 3/-.  
 Battery Charger Kit, Comprises 4 amp. transformer, 5 amp. rectifier, metal case and meter to charge 6 or 12 volt batteries up to 5 amps. With variable charge rate, 19/6 each. 4/6 post & insurance.

### Waterproof Heater Wire

16 yds. length. 70 watts, self regulating temperature control. 10/-, post free.

Mains Transformer. 250-0-250 at 80 mA. 6.3 volts 5 a. (normal mains input). 12/6 each. Carr. 2/6.  
 Output Transformer. Standard pentode matching type. 3/6 each; 36/- per doz.  
 Slide Switch. Sub-miniature but appt., 2/-; 18/- doz.  
 T.C.C. or Dubilier Tubular Condensers.  
 .5 mf. 500 v. 10/- doz.  
 .25 mf. 500 v. 7/6 doz.  
 .05 mf. 500 v. 6/- doz.  
 .001 mf. 1000 v. 5/- doz.  
 .001 1000 v. 6/- doz.  
 .002 1000 v. 7/6 doz.  
 .005 1000 v. 9/- doz.  
 .02 750 v. 8/6 doz.  
 .01 1000 v. 10/- doz.

Battery Charger Rectifier. Selenium 12-15 v. 6 amp. 9/6.  
 Metal Chassis. Punched for Mullard 610 Amplifier complete with inner screening sections and stove enamelled. 8/6. P. & P. 2/9.

Unbreakable Mains Lead. Type of lead fitted to electric razors makes fine lead for test meters and any other devices where subject to continuous bending. Twin figure eight construction, soft cream P.V.C. covered. Normally costs 2/- per yard. Three fit. leads for 2/-.

Filament Transformers, 6.3 v., 1 1/2 amp., 4/6.  
 Neon Lamp—midget wire ended, ideal mains tester, etc. 2/-, Ex-Govt. 1/6.

Phillips Trimmers. 0.30 pF. 1/- each; 9/- doz.  
 Low Resistance Headphones. Ideal crystal sets, etc. 7/6, plus 2/6.

Cold Cathode Valve CV 413. Voltage regulator or trigger switch—unused but ex-equipment 2/- each.  
 Tag Panels. Ideal for construction, experimental circuits, etc. 3 of each of 12 different types, 5/- Post 1/6.

Slydlock Panel Mounting Fuses, with carrier, 5 amps. 2/- each; 15 amp. 2/6 each.

Potentiometers. Sealed type by Morganite among the best ever made, standard 1/2 spindle, 1in. long. 1 meg. 9/- doz., 2 meg. 6/- doz.  
 100K ditto 5/6 doz., 50 K 5/- doz.

MU Metal Screen for American 5 CP1, etc. 10 1/6 pair for VCR97 and other 6in. tubes, 7/- complete. Ditto for 2.3in. tube 5/- complete.

Electric Lock. 24 v. coil but rewindable to alter voltages 4/6, 48/- doz.

.1 mfd. 350 v. Small tubular metal-cased condenser made by Dubilier, 2/6 doz.

24 Volt Motor with blower attached, 12/6, plus 2/9.

115 Volt American magisips (seelys) 50/- each transmitter or receiver. Post 2/9. Pair Post Free.

Morse Practice Outfit—Comprises valve oscillator with controls in wooden box, battery operated, 12/6, Plus 2/9.

Mains from Car Battery rotary generators 12v. input 240v., output 110 mA, 40/-; 600 m.a. £5. Plus 5/- post.

H.R.O. Power Pack. Suitable for 240 or 115 volt mains give 250v. H.T. and 6.3v. i.t., new and unused, but less rectifier valve, 19/6, plus 5/- post.

A.C./D.C. Ammeter 2 1/2in. flush mounting 0-9 amps but external shunt easily removed offered at silly price, 8/6, £5 doz.

DLRS Headphones, 9/6 pair, Post 2/-.

SOULU Powered Inserts. Make excellent microphones or speaker, 5/6 each. £3 doz.

Where postage is not definitely stated add 2/- to all orders under £3. Also add 2/6 if you would like our new 100 page list of bargains.

## See in the Dark INFRA-RED BINOCULARS

These if, ed from a high voltage source will enable objects to be seen in the dark, providing the objects are in the rays of an infra-red beam. Each eye tube contains a complete optical lens system as well as the infra-red cell. These optical systems can be used as lens for T.V. cameras—light cell, etc. (details supplied). The binoculars form part of the Army night driving (Tabby) equipment. They are unused and believed to be in good working order, but sold without a guarantee. Price £21/7/6 plus 10/- carriage and insurance. Handbook 2/6.



## 750 mW TRANSISTOR AMPLIFIER

4 transistors including two in push-pull-input for crystal or magnetic microphone or pick-up—feed back loops—sensitivity 5 m/v. Price 19/6.  
 Post and ins: 2/6. 35 ohm speaker 12/6 extra.



## OUR BARGAIN OF THE YEAR



A complete kit of parts to build this 6-transistor 2 wave superhet receiver at only 39/6, plus 3/6 post and ins.

## "CORONET" Mk. IV

It fully covers the medium-wave band and that part of the long-wave band to bring in B.B.C. Light. The circuit includes a highly efficient slab aerial 2 1/2in. P.M. speaker. Overall size approximately 4 1/2 x 2 1/2 x 1 1/2in. Supplied complete with carrying case and instructions.

## AUTO CHANGER BARGAIN

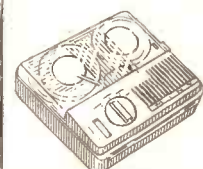
### GARRARD AUTO-SLIM RECORD CHANGER



One of the nicest record changers that this famous company make—Automatic selection of records which may be mixed—may also be played manually. Finger-tip adjustment of Stylus pressure. Fitted with mono head—but pickup wired for stereo—suitable 200/250 A.C. mains—cabinet space required 14 1/2 x 12 1/2 with 4 1/2in. above and 2 1/2in. below. DON'T MISS THIS SPECIAL SNIP, ONLY £5/15/-, (Post and ins. 6/6.)  
 Just arrived! GARRARD AT5 £6/15/- plus 6/6 post and ins.

## THIS MONTH'S SNIP

### THE "MINY" TAPE RECORDER



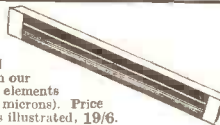
of the many tape recorders to offer at £12 or less we have at last found one we can recommend. Equally suitable for music or speech this instrument uses two motors, is completely portable and is beautifully styled and looks like a good tape recorder.

Among its many good features is a switch on the microphone to stop and start the tapes. A very useful feature for you when recording, and for your typist for note-taking, stock-taking, etc.

Other points are: twin track recording—40 mins with normal tapes, standard batteries. Although originally sold at £16/16/0, we are able this month to offer for only £7/19/6, plus 5/- Post and Insurance. Brand New and complete with microphone, batteries, tape and spools, nothing else to buy.  
 Don't miss this AMAZING offer.

## INFRA-RED HEATERS

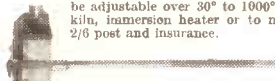
Make up one of these latest type heaters. Ideal for bathroom, etc. They are simple to make from our easy-to-follow instructions—uses silica enclosed elements designed for the correct infra-red wavelength (3 microns). Price for 750 watts element, all parts, metal casing as illustrated, 19/6, plus 2/6 post and insurance. Pull switch 3/- extra.



## THERMOSTATS

Type "A" 15 amp. for controlling room heaters, greenhouse, airing cupboard. Has spindle for pointer knob, quickly adjustable from 30-80°F. 9/6 plus 1/- post. Suitable box for wall mounting, 5/-, P. & P. 1/-.

Type "B" 15 amp. This is a 17in. long rod type made by the famous Sunvic Co. Spindle adjusts this from 50-550°F. Internal Screw alters the setting so this could be adjustable over 30° to 1000°F. Suitable for controlling furnace, oven kits, immersion heater or to make flame-start or fire alarm. 8/6 plus 2/6 post and insurance.



Type "C" is a small porcelain thermostat as fitted to electric blankets, etc. 1 1/2 amp. setting adjustable by screw through side, 3/6. P. & P. 6d.

Type "D" We call this the ice-stat as it cuts in and out at around freezing point, 3/3 amps. Has many uses, one of which would be to keep the loft pipes from freezing. It's length of our blanket wire (16 yds. 10/-) is wound around the pipes, 7/6. P. & P. 1/1

Type "E" This is a standard refrigerator thermostat. Spindle adjustments cover normal refrigerator temperature, 7/6, plus 1/- post.

## MAKING AN F.M. TUNER.

Available, at present, is a very nice cadmium-plated F.M. Tuner chassis with holes punched for coils and other components. Also a nicely printed Perspex front, and calibrated usual F.M. frequencies. Real bargain 6/6 plus 2/- or with two-gang tuning condenser 10/- plus 2/- postage.



## SPEAKER BARGAIN

12in. High fidelity loudspeaker. High flux permanent magnet type with either 3 or 15 ohm speech coil. Will handle up to 10 watts. Brand new, by famous maker.



Price 29/6 plus 3/6 post and insurance.

## Simmerstat Heater Regulator

Suitable to control elements, heater, soldering irons and boiling rings up to 2,500 watt. Complete, adjustable, normal price 65/- each, special snip price 12/6 plus 2/- postage and insurance.

## TRANSISTOR SET CASE

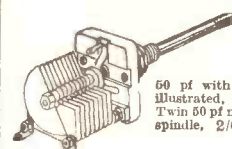
Very modern cream cabinet, size 6 1/2 x 3 x 1 1/2in. with chrome handle, tuning knob and scale. Price 4/6 plus 2/- postage.



## Fluorescent Light Kits

For pelmet lighting, etc. Kit consists of: Super silent choke; 2 chrome clips to hold tube; 2 bi-pin holders for tube and starter with a starter holder. Kit A for 80 watt tube at 27/6. Kit B for 40 watt tube at 19/6. Kit C for 2 x 2ft. 20 w. lamp 25/-, Kit D for 1 x 2ft. 20 w. lamp 18/6. Post and insurance 2/9 per Kit. Absolutely silent in operation.

## FINE TUNERS



50 pf with long spindle as illustrated, 1/6, or 12/- doz. Twin 50 pf not quite such long spindle, 2/6, or 24/- doz.

## FIVE CORE CABLE

Ideal for switching circuits, intercoms, P.A. runs, etc., each core flex copper with rubber insulation core covers overall in tough rubber or P.V.C. 9d. per yd. or 30 yds. length 15/- plus 5/- post.

## THREE UNUSUAL ITEMS

**OZONE OUTFIT**—for removing smells and generally improving any oppressive atmosphere. Kit consists of Philips ozone lamp and mains unit, only needs box. 19/6, plus 3/6 postage and insurance.

**BLACK LIGHT UNIT.** 40 watt intensity, comprises lamp, lamp holder and 40-watt choke. Only 29/6, Plus 6/6 carr. and ins.

**TIMER KIT.** Special offer of all components except metal box to make mains operated interval timer for photography etc., 12/6, Plus 2/6 post

## MAINS POWER PACK

MAINS POWER PACK designed to operate transistor sets and amplifiers. Adjustable output 6 v.-9 to 12 volts for up to 500 mA (class B working). Takes the place of any of the following batteries: P11, P13, P14, P16, P17, and others. Kit comprises: mains transformer-rectifier, smoothing and load resistor, 5,000 and 500 mfd. condensers, series diode and instructions. Real snip at only 14/6, plus 3/- post.

# ELECTRONICS (CROYDON) LIMITED

266 LONDON ROAD, WEST CROYDON, SURREY

Post orders to: Dept. WW, 43 SILVERDALE ROAD, EASTBOURNE, SUSSEX



# VALVES

Brand new, individually packed and guaranteed

AC/HL 4/6	DL94 5/9	EF53 4/6	GZ34 10/-	PL81 7/-	U18 6/-	1L05 7/-	6AK6 6/-	6L6G 6/-	12K8M 10/3	210VPT 7-pin 2/9	9004 2/6
ACP4 6/-	DL96 6/-	EF73 5/-	H63 7/-	PL82 5/-	U25 11/-	1L84 4/-	6AK7 6/-	6L6A 7/8	12Q7GT 3/3	216SG 6/-	9006 2/6
ACOPEN 5/-	DL810 8/-	EF74 4/-	HK54 22/6	PL83 6/-	U27 8/-	1N21B 5/-	6AL5 3/-	6L6M 11/-	12SA7 7/-	216SP 7/-	C.R. Tubes
AL60 5/-	DL819 15/-	EF80 5/-	HL2K 2/6	PL84 6/6	U29 4/6	1N43 4/-	6AL6W 7/-	6L7 4/-	12SC7 4/-	220PA 7/-	CV1596
AR8 5/-	EB0F 23/-	EF85 4/6	HL23 6/-	PL85 6/6	UAB080 5/8	1N70 4/-	6AM5 2/6	6L34 4/6	12SG7 3/-	220TH 4/-	(093) 65/-
AR3 8/-	EB8CC 12/-	EF96 6/6	HL23DD 6/-	PL86 6/6	UBF90 6/6	1R5 5/8	6AM6 4/-	6L20 5/9	12SH7 3/-	225DU 9/-	E4504/2B/1
ARF12 2/6	EB90C 10/-	EF99 3/9		PL87 6/6	UBF99 6/6	184 5/8	6AQ5 7/-	6N7 5/9	12SK7GT 3/3	307A 5/8	28/-
ARF24 3/6	E1148 2/6	EF91 2/9	HL41 4/-	PL88 6/6	UCB20 6/6	185 4/6	6AQ5W 9/-	6Q7G 6/-	6A8 4/-	357A 7/9	VCR97 138
ARF34 4/-	E1266 5/6	EF92 2/-	HLV2 9/-	PL89 6/6	UCB25 6/6	1T4 2/-	6AS6W 20/-	6R7 5/6	6AS7G 20/-	368A 5/-	VCR126
ARTP1 9/-	E1416 3/0	EF95 5/-	K3A 3/0	PL90 6/6	UC44 6/6	2A3 5/-	6AT6 3/6	6B7 5/6	6B7G 7/-	446A 8/-	30/-
ATP4 2/6	E1524 12/8	EF183 8/-	KT35 22/-	PL91 6/6	UC48 6/6	2C45 22/6	6AT6 3/6	6B7 5/6	6B7GT 5/8	487A 3/6	VCR138A
ATP7 9/8	E450 1/-	EF184 8/-	KT32 8/-	PL92 6/6	UC51 6/6	2C26 7/-	6AU6 7/-	6AX4 8/-	14R7 5/-	708A 3/0	40/-
AU7 55/-	E473 7/-	EHT1 300/-	KT33C 6/-	PL93 6/6	UC83 10/-	2C26 7/-	6B7 5/6	6B7GT 5/8	15D2 1/6	716B 6/0	VCR139A
B6H 15/-	EAB080 5/-	BL32 3/9	KT44 5/9	PL94 6/6	UF99 8/6	2C34 2/6	6B8G 2/-	6B8G 2/-	15E2 15/-	717A 3/0	35/-
BL63 10/-	EAC91 3/6	EL34 10/-	KT63 4/6	PL95 6/6	UL41 6/-	2C43 42/8	6BA6 4/-	6B7 5/6	19G3 10/-	724A 15/-	VCR517B
B84 8/-	EAF42 8/-	EL35 5/-	KT66 12/9	PL96 6/6	UY85 5/-	2C45 22/6	6B7 5/6	6B7GT 5/8	19G5 9/-	735A 3/0	40/-
B85 20/-	EB34 1/8	EL38 17/8	KT21 6/-	PL97 6/6	UY5 7/-	2C46 3/0	6BE6 4/3	6B7GT 5/8	19G7 5/-	803 22/8	VCR517C
B884 47/8	EB91 3/-	EL41 7/-	KT76 8/6	PL98 6/6	UY9 8/6	2C51 12/-	6B7 5/6	6B7GT 5/8	19H1 6/-	807 8/-	60/-
B2134 16/-	EB93 6/-	EL42 8/-	KT88 20/-	PL99 6/6	UY21 7/6	2D21 5/-	6B7GT 5/8	6B7GT 5/8	19M1 5/-	808 8/-	40/-
BT19 26/-	EB041 7/-	EL60 8/-	KTW61 4/6	PL00 6/6	UY41 4/-	2X2 3/-	6B7GT 5/8	6B7GT 5/8	20P4 13/-	813 6/0	30/-
BT95 25/-	EB081 7/-	EL81 8/-	KTW63 2/-	PL01 6/6	UY85 5/-	3A4 3/-	6B7GT 5/8	6B7GT 5/8	21B6 9/-	816 35/-	30/-
BT45 150/-	EBF80 5/-	EL83 6/6	KT21 6/-	PL02 6/6	Y130 4/-	3A108A 8/-	6B7GT 5/8	6B7GT 5/8	20LGGT 5/8	829A 30/-	30/-
BT89 35/-	EBF83 7/8	EL84 8/-	KT23 8/-	PL03 6/6	Y1507 5/-	20/-	6C6G 2/6	6U4GT 9/6	25V5 6/-	829B 5/0	30/-
CC3L 2/-	EBF89 6/9	EL85 8/-	LP2 10/-	PL04 6/6	Y1924 20/-	3A146J 35/-	6C5GT 6/-	6V6G 5/-	25Z4G 6/6	830B 4/-	30/-
CL33 9/-	EC82 4/-	EL91 4/6	MB100 9/-	PL05 6/6	YMP4G12 12/-	3A167M 6/-	6C6 4/-	6V6GT 7/6	25Z5 7/6	832A 45/-	30/-
CV71 3/-	EC83 12/6	EL95 5/-	MB142 12/-	PL06 6/6	YP23 3/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
CV7 6/-	EC70 4/-	EL360 20/-	MB190 5/-	PL07 6/6	YP133 9/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
CV102 1/-	EC90 4/-	EM80 6/-	MH4 5/-	PL08 6/6	YR300 6/6	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
CV103 4/-	EC91 3/-	EM81 7/8	MHLD610/-	PL09 6/6	Y805 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
CV4004 7/-	EC88 4/-	EM84 6/3	ML6 6/-	PL10 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
CV4014 7/-	EC82 5/-	EM85 9/-	N108 8/-	PL11 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
CV4015 5/-	EC83 6/-	EN31 10/-	NE17 7/-	PL12 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
CV4020 14/-	EC84 10/-	OS47 4/6	OC3 5/-	PL13 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
CV4046 40/-	EC85 6/6	BS1208 6/-	OC3 5/-	PL14 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
CV4049 6/-	EC88 9/-	EY01 5/6	OD3 5/-	PL15 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
CY31 6/6	EC091 4/-	EY86 6/8	OZ4A 5/-	PL16 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
D1 1/6	ECF82 7/-	EY91 3/-	PC04 5/-	PL17 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
D81 3/3	ECF83 8/-	EZ40 5/6	PC05 7/-	PL18 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
D81 8/-	ECF81 6/-	EZ41 6/8	PC08 12/8	PL19 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
D77 3/3	ECF83 7/6	EZ80 5/6	PCF80 6/6	PL20 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
DA30 12/6	ECL80 6/-	EZ81 3/6	PCF82 6/6	PL21 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
DAF96 6/-	ECL82 7/8	F/6057 5/-	PCF84 6/-	PL22 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
DA1 4/-	ECL83 10/-	F/6061 5/-	PCF81 9/-	PL23 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
DET5 8/-	ECL86 10/-	F/6063 4/-	PCF82 6/6	PL24 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
DET20 2/-	EF36 3/6	FW4/5006/6	PCF83 8/3	PL25 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
DET25 15/-	EF37 3/-	FW4/8008/6	PCF84 7/3	PL26 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
DF73 5/-	EF39 5/-	G1/236G 9/-	PCF85 8/6	PL27 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
DF93 3/-	EF40 8/-	G1/371K	PCF86 9/6	PL28 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
DF93 3/-	EF41 6/-	G1/371K	PCF87 9/6	PL29 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
DF96 6/-	EF42 6/-	G1/371K	PCF88 9/6	PL30 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
DK92 6/8	EF52 6/-	G50/2G 5/-	PCF89 10/6	PL31 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
DL96 5/6	EF55 5/-	G180/2M	PCF90 6/6	PL32 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
DL92 5/6	EF71 7/8	GM4 15/-	PCF81 9/-	PL33 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-
DB93 6/-	EF72 5/-	GZ32 10/-	PCF82 6/6	PL34 6/6	Y895 10/-	3B7 25/-	6C6G 3/-	6V6M 8/-	26ZGT 8/6	832 15/-	30/-

MANY OTHERS IN STOCK including Cathode Ray Tube and Special Valves.

All U.K. orders below £1 P. & P. 1/-; over £1 2/-; orders over £3 P. & P. free: C.O.D. 3/6 extra. Overseas Postage Extra at Cost.

**MARCONI COMMUNICATION RECEIVERS**  
**C.R.150.** Frequency coverage 2-60 Mc/s. in 5 bands. Two I.F.s 1st 1,600 kc/s. 2nd 465 kc/s. Image signal protecting over 40 dB up to 30 Mc/s. and 20-40 dB from 30-60 Mc/s. Self-checking calibration (built-in calibrator). Stabilisation of supply and temperature compensation. Electrical and mechanical bandspread. Metering and visual tuning indicator. Band pass from 100 kc/s. to 10 kc/s. in 5 stages. Acoustic filter associated with 100 kc/s. Bandpass position for C/W reception. Facilities for diversity reception. Excellent checked condition, £39. Mains P.S.U. by P.C.A. Radio £4/10/-, carriage 30/-.

**C.R.150/2.** Frequency coverage 1.5-22 Mc/s. in 4 bands, all other features as in C.R.150. Price £31. Carriage 30/-.

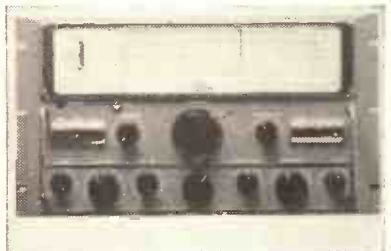
**DUMONT MODEL 241 OSCILLOSCOPE** in fully working condition £22/10/-, P. & P. 30/-.  
**"CONNECT AND FORGET, CANNOT OVERCHARGE" "ESSTRON" MARK I AUTOMATIC BATTERY CHARGER.** Initial charging rate 6-7 amps. The charging rate automatically adjusts itself to the charge in the battery. Automatic current and voltage control. Patented application of magnetic amplification to battery charging. Indicator lights show battery fully charged, receiving charge incorrectly connected or faulty cells. Mains voltage 200/250 v. Built for 6 or 12 v. batteries. Measurements 7 x 5 x 5 1/2 in. Weight 8 1/2 lb. Price £7/19/6. P.P. 3/6.

**H.R.O. SENIOR TABLE MODEL** in excellent, fully checked and tested condition together with set of 9 general coverage coils and mains P.S.U. £28. Carriage & Packing 30/-.

**ORIGINAL MAINS POWER SUPPLY FOR H.R.O. RECEIVER.** 250/115v. Brand New 65/-, P. & P. 5/-.

**2 KW ULTRASONIC GENERATOR** together with power supply unit for 200-250 v. A.C. Complete two chassis with interconnecting cables. Frequency 37 to 43 kc/s. adjusted by fine control. Peak output 2 kw, average output 500 w. Completely new with valves and manual £65 carriage paid U.K. Large selection of mains and Heavy Duty L.F. TRANSFORMERS.

**VARIOMETER** for No. 19 set, 17/6. P. & P. 3/-



**VERY HIGH CLASS COMMUNICATION RECEIVER TYPE BRT 402E.** 150 kc/s.-385 kc/s., 510 kc/s.-30 Mc/s. Fully tested £60. Carriage 30/-.

**WIRELESS SET NO. 52 (CANADIAN).** Complete station consisting of Transmitter, Receiver, supply unit for 12 v. All contained in special carrier. 1.75-16 Mc/s. in 3 bands. 813 as output valve. 45-75 w. phone and MCW, 70-100 watt CW. M.O. or crystal. Receiver includes crystal calibrator. Tx can be exactly tuned to Rx frequency. Noise limiter. Sidetone. Loudspeaker on receiver with on/off switch. All brand new with accessories. Export. Price on application.

**EVERSHED MEGGER CIRCUIT TESTER** 2 ranges. 0-1,000 ohms. 100-200,000 ohms. with test leads, leather carrying case. Tested £4/19/6. P. & P. 3/6.

**A.R.88D INSTRUCTION MANUALS** 20/-, P. & P. 2/6.

**AR88D RECEIVERS.** Fully reconditioned, £55, rebuilt models £85. Carriage paid U.K.

**NEW DHR. HIGH-RESISTANCE HEAD-PHONES.** 14/-, P. & P. 1/6.

**P. C. RADIO LTD.**  
**170, GOLDHAWK RD., W.12**  
**SHEpherd's Bush, 4946**

**ULTRA MODERN POWER SUPPLY UNIT.** Supply voltage A.C.: 105, 110, 115, 200, 205, 210, 220, 225, 230, 240, 245, 250v. Available voltages D.C.: (a) 1700-1900 v. Stabilised, adjustable approx. 1 mA (b) HT2 approx. 45 mA. (c) 260-350 v. stabilised, adjustable, approx. 45 mA. (d) 450 v. approx. 30 mA. (e) 50 v. approx. 150 mA. (f) 4.5 v. A.C., 4.5 amp. common earth. (g) 6.3 v. A.C., 4.5 amp. common earth. 5 valves, 7 silicon rectifiers, 4 Solenium HV rectifiers. Brand new £9/10/-. Carriage 12/-.

**PANEL METERS (round)**

0-50 microamps	2 1/2 in.	D.C.**	32/6
0-500 microamps	2 1/2 in.	D.C.	22/6
0-500 microamps	3 1/2 in.	D.C.	35/-
0-1mA*	3 in.	D.C.*	19/6
25-0-25mA.	2 1/2 in.	D.C.	45/-
500mA.	3 1/2 in.	A.C.	25/-
0-100mA.	3 1/2 in.	A.C.	22/6
150-0-1,500mA.	3 1/2 in.	D.C.	29/-
0-100mA.	3 1/2 in.	D.C.	32/6
0-5v.	2 1/2 in.	A.C.	22/6
0-15v.	2 1/2 in.	A.C.	17/6
0-50v.	2 1/2 in.	D.C.	22/6
0-150v.	2 1/2 in.	A.C.	24/-
0-10kV.	2 1/2 in.	D.C.	63/-

\*Extension as usually used also in H.R.O. as "8" meter.  
 \*\*Projection type.

**STABILISED POWER SUPPLY UNIT TYPE R 2001.** (EDISWAN) with 2 independent outputs. 1.0-100 v. 50 mA. metered and regulated by coarse and fine adjustments. 2. 250 v. Bias at 5 mA. Stability 0.02%. Price £18.

**THERMAL PLUS MECHANICAL CIRCUIT BREAKER FOR A.C. & D.C.** Current 1 amp. Protects against shorts (instantaneous cut out at approximately 8 amps) and against overloads: 1.8 amp. 30 seconds, 2.1 amp. 15 seconds, 2.5 amp. 8 seconds. Delayed cut off may be adjusted to different currents and times. Separate pair of contacts to indicating device. Dimensions 3 1/2 x 1 1/2 x 1 1/2 in. Price 12/6. P. & P. 2/6.

**TELEPHONE HANDSET.** Standard G.P.O. type, new 12/-, P. & P. 2/-.

**INSET MICROPHONE** for telephone handset 2/6, P. & P. 2/-.

Open 9-5.30 p.m. except Thursday 9-1 p.m.

PERSONAL CALLERS WELCOME

**O.H.M. METER**  
Nashcon  
Type V 16.  
A.C. mains operation  
200 to 250 v.  
50 c/s. 10  
ohms to 1  
Megohm (4  
ranges) and  
1 Meg. to  
10,000 Megs.  
(4 ranges)  
Weston 4in.  
mirror scale  
meter. Uses  
4 cathode-  
follower  
valves fed  
from stabil-  
ised H.T. line. With circuit, etc. A quality  
instrument at a fraction of original price.  
**BRAND NEW £8/19/6.** P. & P. 5/6. De-  
tails on request.



**PORTABLE RECEIVER TESTER**  
**MARCONI INSTRUMENTS TF-888/3**  
This instrument combines the functions of a wide range signal generator and output meter. Continuous frequency coverage of 70 Kcs to 70 Mc/s in 8 wavebands by means of a rotating coil turret. Output impedance 80 or 52 ohms or high level (500 mV) 40Ω Int. Mod. at 1,000 c/s. Two crystal checks at 500 Kcs/s and 5 Mc/s. Panel meter monitors carrier and also functions as output meter full scale 10 mV., 100mV. and 1w. Input impedances 3, 33, 150 and 600Ω. Handsome grey case, size 15½ x 7½ x 11½ high. Wt. 17½ lbs. Operates from A.C. mains 100 to 250 volts. As new, tested and guaranteed. **£39/10/-.** Carr. 10/-.

**TRANSISTORISED D.C. SUPPLY UNIT**  
Type VP II. Famous make. Bench type in handsome case 15 x 10 x 10in. Weight 18 lbs. Mains operation 200 to 250 volts 40-60 c/s. Output voltage continuously variable from 3 to 15 volts at 1 amp. (max.). Output impedance 0.01 ohms. A 10% supply variation produces less than 0.1% variation in output. Both voltage and current are independently metered. Electronic cut-out with front panel reset. **ABSOLUTELY BRAND NEW** with handbook, £21. Carr. 7/6.  
**VQ 161.** "Brick" type. Output voltage adjustable from 3 to 25 volts (1 amp. max.), by changing transformer taps and preset pots. Similar spec. to above. Not metered. Electronic cut-out. Auto reset. 3 x 4½ x 10in. Weight 8 lbs. **BRAND NEW** with handbook. **£12/10/-.** P. & P. 7/6.

**LM-14 HETERODYNE FREQUENCY METER**  
Naval version of the BC-221. 125 Kcs/s to 20 Mc/s. Undoubtedly superior to the BC-221 in construction and performance. Requires 12 or 24 v. LT and between 200 and 475 v. HT (self-stabilised). A particularly useful feature is variable RF coupling and modulation is also available. With correct individual calibration books. Unused and guaranteed. **£25.** P. & P. 7/6. Separate power unit for A.C. (if required). **£4/10/-.** P. & P. 5/-.

**GENERAL RADIO LRS HETERODYNE FREQUENCY & CALIBRATION EQUIPMENT.**  
**BRAND NEW.** **£75**



**MARCONI TF-390-G SIGNAL GENERATOR.** £7/10/-. Carr. £1.  
Four ranges: 16-32, 32-60, 50-100 and 75-150 Mc/s. A.C. mains operation. **AS NEW** in original transit cases with correct individual calibration and instruction books.

**G.E.C. RECEIVER BRT402E**  
14 valve superhet 150-385 Kcs/s, 510 Kcs/s to 30 Mc/s in six wavebands. Sensitivity, sig./noise ratio, freq. stability, etc. of the highest order. Six step variable selectivity. Xtal filter (Xtal phasing control), RF, IF and AF gain, 500 Kcs/s Xtal cal., Audio Filter, "S" meter, Ae trimmer, Variable BFO, A.C. mains operation. **EVERYTHING.** Reconditioned. **£60.** Carr. 30/-. S.A.E. for details.

**WIRELESS SET No. 76**  
A compact CW only crystal controlled transmitter. Consists of a Pierce crystal oscillator (807) and a Power Amplifier (807). Both are cathode keyed by means of a relay. Six switched crystal channels are available in the frequency range of 2 to 12 Mc/s. (Crystals not included.) Aerial current is indicated on a panel meter and two spare valves are supplied. Operates from 12 v. car battery via internal rotary transformer. RF output 9 watts. Contained in steel case 12 x 12 x 8in. Weight 30 lbs. Ideal for 80 or 40 metres or cheap enough for breakdown. Good condition and working order. Circuit included. **£3/10/-.** Carr. 10/-.

**SIGNAL GENERATOR CT-218 (FM/AM)**  
**MARCONI TF 937.** Covers 85 Kcs/s to 30 Mc/s in 8 switched ranges. Effective length of film scale is 50 ft. Output level variable in 1 dB steps from 1μV to 100 mV (75Ω). Also IV Outputs down to 0.1μV from an outlet at 7.5Ω. Int. mod. at 400 c/s, 1 Kcs/s, 1.6 Kcs/s and 3 Kcs/s. FM at frequencies above 394 Kcs/s. Variable mod. depth and deviation. Crystal calibrator 200 Kcs/s and 2 Mc/s. Monitor speaker for beat detection. Fully metered, blower cooled, Panlomatic. A.C. mains 100 to 150 and 200 to 250 volts, 45 to 100 c/s. 17 x 20½ x 17½in. Weight 117 lbs. Fully tested and guaranteed. Under 10% of original price. **£65.** Carr. 50/-.

**TELEVISION SWEEP GENERATOR**

**MARCONI TF 1104/I.**  
V.H.F. alignment oscilloscope for TV, V.H.F., IF and VF response. Crystal controlled or variable oscillator markers. Sweep width up to 10 Mc/s. Can be used as normal oscilloscope. With handbook. Details on request. **ABSOLUTELY BRAND NEW. £75.**



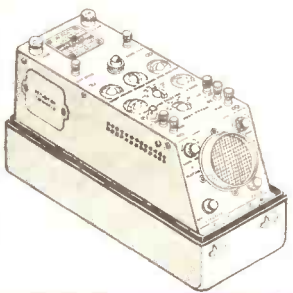
**MAGNETIC COUNTERS (Ex-G.P.O.)** 4 figures to 9,999. Coils 500Ω for 24 v. operation. Tested (no reset). 5/- each. P. & P. 1/6. **SPECIAL OFFER.** 10 for 30/-. P. & P. 5/-.

**ABSORPTION WAVEMETERS**  
**MARCONI TF-643-B.** Covers from 20 to 300 Mc/s in four plug-in coil ranges. Complete with individual calibration charts. Accuracy 1%. Indication is on a 50μA 2½in. panel meter. In original transit cases. Condition as new **£5/19/6.** Carr. 7/6.

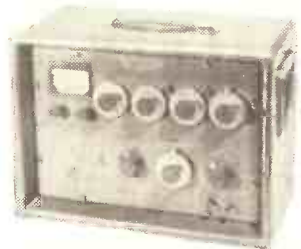
**RELAYS G.E.C. MINIATURE SEALED**  
M-1099. 670Ω 2M H/D Wire Ends ..... 7/6  
M-1052. 5,000Ω 2/CO. Plat. Wire Ends ..... 10/-  
M-1092. 670Ω 4/CO. Plat. Wire Ends ..... 12/6  
**ALL BRAND NEW AND BOXED.** Please add postage.

**MINIATURE RELAYS.** 240 v. A.C. coils. Contact assembly 2 " makes " and 1 C.O. 5 amps. Size 2 x 1½ x 1in. Unused and removed from brand new equipment. 8/6 post paid.

**HICKOCK OSCILLOSCOPE OS-8B/U**  
A high grade general purpose instrument made to exacting U.S.A. Navy specification. Detachable cover with carrying handle. Compact (13½ x 6 x 8½in.), weight 17 lbs. Green trace 3in. tube. Bandwidth "Y" amplifier D.C. to 2 Mc/s (D.C. coupled). Sensitivity 40 mV/cm. "X" amp. can be used separately, similar spec. to "Y" amp. Leads are housed in case. For A.C. mains 105 to 125 v., 50 to 1,000 c/s. **BRAND NEW,** tested and guaranteed. **£25.** Carr. 10/-. Auto transformer 15/6 extra.



**CHARLES BRITAIN (Radio) LTD.**  
**11 UPPER SAINT MARTIN'S LANE**  
**LONDON, W.C.2.** **TEMPLE Bar 0545**  
Near Leicester Sq. Station. (Opposite Thorn House)  
Shop hours: 9-6 p.m. (9-1 p.m. Thursdays). **Open all day Saturday.**



**LOW CAPACITANCE BRIDGE**  
**MARCONI TF 1342.** Range 0.002 pF to 1,111 pF. Accuracy 0.2%. Three terminal transformer ratio arm bridge allows "in situ" measurements. Internal oscillator frequency 1,000 c/s. 12 x 17 x 8½in. Weight 15½ lbs. A.C. mains 200 to 250 and 100 to 150 v. 40-100 c/s. With leads and handbook. **ABSOLUTELY BRAND NEW. £45.**

**PHASE MONITOR ME-63/U (AN/URM-67)**  
Designed to measure directly the phase angle between two applied audio frequency signals of from 20 to 20,000 c.p.s. ±1°. Direct indication on a panel meter. Input can be sinusoidal or non-sinusoidal from 2 to 30 volts peak. Of recent manufacture (1957) by Control Electronics Inc. and ex-U.S.A. Air Force. In first class condition with handbook. A complex instrument with 19 valves. **£40.** Carr. 30/-.

**MOVING COIL PHONES.** Finest quality Canadian with chamois ear-muffs and leather-covered headband. With lead and jack plug. Noise excluding and supremely comfortable. 22/6. Post 1/6. As above but complete with moving coil microphones. 25/-. Post 2/6. DLR-5 Low impedance headphones with attached throat microphone. 12/6. Post 1/6. All these items **BRAND NEW.**

**T.C.C. VISCONAL CONDENSERS.** 8 mfd. 800 v. D.C. wkg. at 71°C. CP 152 v. Size 3 x 1½ x 5in. high. **BRAND NEW (boxed), 8/6 each. DUBILIER NITROGOL.** 8 mfd. 350 v. D.C. wkg. at 71°C. Size 1½ x 1½ x 4½in. high. With fixing clips. **BRAND NEW (boxed) 5/- each. T.C.C. or DUBILIER.** 4 mfd. 600 v. wkg. CP 130T or similar. 1½ x 1½ x 4½in. high. **BRAND NEW (boxed), 4/6 each.** All post paid.

**ASSORTED CAPACITORS.** Mixed parcel of 100 all brand new, marked value quality types. Silver mica, ceramic and feed through from 1 pF to 3,000 pF. 10/-.

**STANDARD TRANSFORMERS**  
Vacuum impregnated, interleaved, E.S. screen, universal mounting. Size 4 x 3½ x 2½in. **ALL BRAND NEW.** 18/6 each. Post 2/6.  
**Type 1.** 250-0-250 v. 80 m/a. 6.3 v. 3 a. tapped at 4 v. 4 a. 6.3 v. 1 a. tapped at 4 v. and 5 v. 2 a.  
**Type 2.** As above but 350-0-350 v. 80 m/a.  
**Type 3.** 30 v. 2 a., tapped at 12, 15, 20 and 24 v. to give 3-4-5-6-8-9-10 v., etc.  
**Type 5.** 0-6-9-15 v. 4 a. Ideal for chargers.

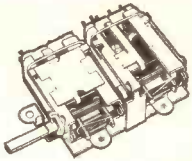
**ADVANCE CONSTANT VOLTAGE TRANSFORMERS.** Input 190-260 v. 50 c/s. A.C. mains. Output 230 v. 150 watts. **£7/10/-.** Carr. 5/-.

**OSCILLOSCOPE TRANSFORMER**  
These are replacements for the Cossor 339A 'scope. **BRAND NEW** in original packing. 79/6. P. & P. 5/6.

**SANGAMO WESTON VOLT METERS**  
561. Dual range 0-5 and 0-100 v. D.C. FSD 1 m/A. 3in. scale. Recent manufacture. Ideal for schools. Complete in super quality canvas carrying case, with test prods and leads. **BRAND NEW.** Boxed 32/6. Post 2/6.







### CYLDON A.M./F.M. PERMEABILITY TUNER FOR ALL TRANSISTOR OPERATION

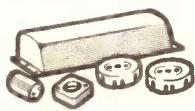
Size 2½in. × 2½in. approx. By famous manufacturer. A.M.-I.F. 470 Kc/s. F.M.-I.F. 10.7 Mc/s. A.M. coverage from 1,620 kc/s.-525Kc/s. F.M. coverage 108 Mc/s.-88 Mc/s. Circuit diagram 2/6. FREE with Tuner. 1st, 2nd, 3rd A.M.-I.F.'s 1st, 2nd, 3rd and 4th F.M.-I.F.'s V.H.F. Osc. choke A.M.-Ftrap. All the above are the R.F. end of an AM/FM receiver car radio etc. **£2.10.0**

The above items.

### BSR MONARCH UA14 With FUL-FI HEAD

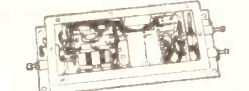
4-speed, plays 10 records, 12in., 10in. or 7in. at 16, 33, 45, or 78 r.p.m. Intermixes 7in., 10in. and 12in. records of the same speed. Has manual play position: colour, brown. Dimensions: 12½ × 10½in. Space required above baseboard 4½in., below baseboard 2½in. Fitted with Ful-Fi-turn-over crystal head, £5/19/6. P. & P. 7/6. **B.S.R. UA16**, similar to the above, £6/12/6. P. & P. 7/6. **B.S.R. GU7**, 4-speed, single player, complete with pick-up on unit plate with automatic switch £3/19/6. P. & P. 6/6.

### 40W. FLUORESCENT LIGHT KIT



Incorporating GEC Choke size 8½in. × 1½in. × 1½in., 2 bi-pin holders, starter and starter holder. **11/6** P. & P. 4/6. Similar to above: 80W. Fluorescent Light Kit incorporating GEC choke size 11½in. × 1½in. × 1½in. **17/6** P. & P. 5/6.

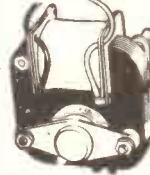
### TRANSISTOR INVERTOR



50 v. D.C. Input. Output 240 v. A.C. 40 Watts incorporating transformers, choke, condensers and 2 GET 573. In solid 16 gauge Aluminium Case size 15in. × 6in. × 2½in. by famous manufacturer. **19/6** plus 7/- P. & P. 7/6.

### AC MAINS MOTOR

Can be used for a variety of purposes, silent running, satisfactory in every way, 230/250 v. A.C. **9/6** P.&P. 3/-.



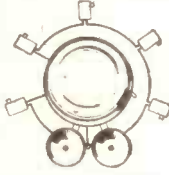
### FLUORESCENT LIGHT FITTING



Twin 40 watt 200/250 v. less tubes. **39/6** P.&P. 7/-.

### RINGO BURGLAR ALARM

A.C. Mains 200/240 volt. Fire salvage slightly tarnished. List price 7 gns. Our price complete with double gong bell, five micro switches and full instructions. **49/6** P. & P. 5/-.



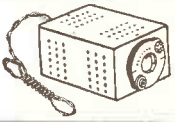
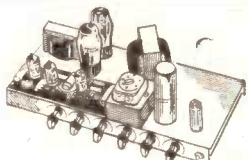
### FIRST QUALITY PVC TAPE

5½in. Scd. 850ft. ...	9/-	5in. L.P. 850ft. ...	10/6
7in. Scd. 1200ft. ...	11/6	3in. T.P. 600ft. ...	8/-
3in. L.P. 240ft. ...	4/-	5in. T.P. 1800ft. ...	20/6
5½in. L.P. 1200ft. ...	11/6	5½in. T.P. 2400ft. ...	27/6
7in. L.P. 1800ft. ...	18/6	7in. T.P. 3600ft. ...	37/6

P. & P. on each 1/6, 4 or more post free.

### 6 VALVE 15 WATT PUSH-PULL AMPLIFIER

15 × 7 × 1½in. A.C. mains 200-250 volts. 4 inputs with controls for same and bass and treble lift controls. Tapped for 3 and 15 ohm speakers. Extra H.T. and L.T. for F.M. Tuner supplies, etc., built and tested, 7 gns. plus 13/6 P. & P.



### POWER SUPPLY KIT

In metal case, size 3½in. × 2½in. × 2in. incorporating mains transformer, rectifier and condensers. 230/250 A.C. Mains. Output: 9 v. 100 mA. Price 10/6 plus 3/- P. & P.



### OSCILLOSCOPE for D.C. & A.C. Applications

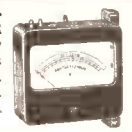
Push-pull X amplifier; Fly-back suppression; Internal Time-base Scan Wave form available for external use; pulse output available for checking TV line O/P Transformers etc. Provision for external—/P and C.R.T. Brightness Modulation. A.C. mains 200/250 v., £18/18/-, P. & P. 10/-. FULL 12 MONTHS' GUARANTEE INCLUDING VALVES AND TUBE.

### 3 to 4 WATT AMPLIFIER KIT

comprising chassis 8½in. × 2½in. × 1in. Double wound mains transformer, output transformer. Volume and tone controls, resistors, condensers, etc. 6V6 ECC81 and metal rectifier circuit 1/6 free with kit. **29/6** plus 4/6 P. & P.

**POCKET MULTI-METER.** Sizes 3½ × 2½ × 1½in. Meter size 2½ × 1½in. Sensitivity 1,000 OPV on both A.C. and D.C. A.C. and D.C. volts 0-15, 0-150, 0-1,000. D.C. current 0-150 mA. Resistance 0-100KΩ. Complete with test prods, battery and full instructions. **42/6**, plus 3/6 P. & P.

**50 MICRO-AMP. METER** Movement by world-famous manufacturer. Size 3in. × 2½in. **25/-** plus 2/- P. & P.



### FIXED FREQUENCY SIGNAL GENERATOR

Crystal control in metal case, size 10in. × 6in. × 6in. Incorporating 2 FC13 valves, mains transformer, metal rectifier, choke, indicator lamp, crystal and numerous components. Modulated and unmodulated output sockets. Originally used for I.T.V. frequencies. Brand new. **39/6** plus 7/- P. & P. A.C. Mains 200/250 volts.



**SILICON RECTIFIERS** 250 v. P.I.V. 750 milli-amps. Six for 7/6d. post paid.

## SPECIAL OFFER! "Elegant Seven" Mk. II

**POWER SUPPLY KIT** to purchasers of **Elegant Seven** parts, incorporating mains transformer, etc. A.C. mains 200-250v. Output 9v. 100mA. 7/6.

- COMBINED PORTABLE & CAR RADIO.** The Radio with the **STAR** features 4in. **SPEAKER.**
- ★ 7-transistor superhet. Output 350mW.
  - ★ Grey wooden cabinet, fitted handle with silver coloured fittings. Size 12½in. × 8½in. × 3½in.
  - ★ Horizontal tuning scale, size 11½in. × 2½in. in silver and black lettering.
  - ★ All stations clearly marked.
  - ★ Ferrite-rod internal aerial.
  - ★ I.F. Neutralisation on each stage. 460 Kc/s.
  - ★ D.C. coupled output stage with separate A.C. negative feed back.
  - ★ All components, ferrite rod and tuning assembly mounted on printed board.
  - ★ Operated from PP9 battery.
  - ★ Full comprehensive instructions and point-to-point wiring diagrams.
  - ★ Printed circuit board, back printed with all component values.
  - ★ Fully tunable over medium and long waveband.
  - ★ Car aerial socket.
  - ★ Full after-sale service.



**ONLY £4.4.0**

Plus 6/6 P. & P. Partslist and circuit diagram 2/6. Free with parts.

**RADIO AND T.V. COMPONENTS (ACTON) LTD.**  
21A, HIGH ST., ACTON, LONDON, W.3.  
Goods not despatched outside U.K. All enquiries S.A.E. Terms C.W.O.  
SHOP HOURS 9 a.m.-6 p.m. EARLY CLOSING WEDNESDAY

# Wilkinsons FOR RELAYS

## P.O. TYPE 3000 AND 600

### BUILT TO YOUR REQUIREMENTS—QUICK DELIVERY COMPETITIVE PRICES—VARIOUS CONTACTS DUST COVERS—QUOTATIONS BY RETURN



#### MINIATURE SEALED RELAYS

OVER 120 TYPES IN STOCK. SEND FOR LIST.

SIEMENS 1 C.O.		SEND FOR LIST.	
2.2Ω + 2.2Ω	H96A	18/6	
50Ω + 50Ω	H96B	19/6	
145Ω + 145Ω	H96C	19/6	
1,700Ω + 1,700Ω	H96L	22/6	
<b>G.E.C.</b>			
2,500Ω	4CO	M1008	19/6
2,500Ω	1CO	M1022	15/-
5,000Ω	2CO	M1052	17/6
5,000Ω	2m2bHD	M1095	19/6
2,500Ω	2C2K	M1417	17/6
5,000Ω	2CO	M1452	15/-
2Ω	2mHD	M1454	15/-
2,500Ω	2mHD	M1458	15/-
2,500Ω	1m1bHD	M1462	19/6
40Ω	2CO2K	M1482	15/-
180Ω	1CO	M1486	17/6
180Ω	2m2bHD	M1487	19/6
180Ω	2C2K	M1490	19/6
670Ω	2C2K	M1493	19/6
670Ω	4K	M1567	19/6
<b>S.T.C.</b>			
45Ω	1mHD	4186EB	19/6
170Ω	1mHD	4186EC	19/6
700Ω	2COMD	4190HD	19/6
2,500Ω	2CO	4184CE	19/6
2,500Ω	1mHD	4190FE	19/6
<b>ERICSSON</b>			
7,000Ω	1CO	N22242A10	25/-
260Ω	1CO	N22372AC1	15/-
5,000Ω	1CO	N22372AF1	15/-
7,500Ω	2CO	N22365AZ1	17/6
1.1Ω	4CO	N22364AA1	19/6
1.1Ω	2C2K	N22366AA1	19/6
1,500Ω	2CO2K	N22366AE1	19/6
2.4Ω	2M	N22371AA1	15/-
180Ω	2M	N22371AC1	15/-
2,000Ω	2M	N22371AB1	15/-
2.4Ω	1m1b	N22370AA1	15/-
5Ω	1m1b	N22370AB1	15/-
1,500Ω	2m2b	N22369AE1	17/6
7,500Ω	2m2b	N22369AZ1	17/6

**MINIATURE UNISELECTORS.** Plug-in type. Occupies no more space than a P.O. 3000 Relay. Siemens, No. 2200A, 3 level, 12 outlets, 50 volts, 1 bridging and 2 non-bridging wipers. Supplied complete with jack. EACH 90/-.

**WEYMOUTH RELAYS.** 24 v. D.C. 2 Make Heavy Duty 5C2007, 7/6 each.

**E.M.I. RELAYS.** Sub-miniature. 12 or 24 v. D.C. 1CO, 10/6 each.

**RELAYS.** 24 volt D.C. 4 Make, 4 Break, 10 amp. 5C31944 Dust Cover, 12/6 each.

**KEY SWITCHES** (3 position).  
P.O. 212 2C/2C Locking 6/6.  
P.O. 264 2K/2K Locking 9/-.  
4C/4C Non-Locking 13/6.  
P.O. 295 4C/6C NL/L 17/6.  
Other types available. Knobs 6d. Plates 1/-.

**SPEAKERS ELAC 5in. ROUND**  
9700 Gauss 3Ω 7/6, Post 2/6.

**TELEPHONE BULBS No. 2 Tubular.**  
6, 12 or 24 v. 1/6; 50 v. 2/-.

**RESISTORS WIREWOUND AND HIGH STABILITY CARBON** inc. Erie 109, 108 and 100, ex stock in quantity. Write or phone your requirements.

**GEARED CAPACITOR MOTORS.** 220 240 v. 50 c.v., 30 watts, 300 r.p.m., also spindle for 1,425 r.p.m. Very powerful, 75/-, post 5/-.


**MAINS MOTORS.** Capacitor 230 v. A.C. 1/40th h.p. 1,400 r.p.m., 55/-, post 4/6.

**SYNCHRONOUS MOTOR.** 200/250 volts A.C. 50 cycles with gear train driving 5 dials 1/10th hr.-10,000 hrs., 22/6, post 3/-.

**SYNCHRONOUS MOTOR.** 200/250 volts A.C. 60 r.p.m. Synclock, 25/-, post 2/-.

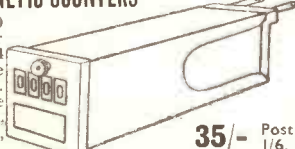
**LEDEX SOLENOID DRIVEN WAFER SWITCHES.** SIZE 5S. From 90/-, 11 Way and off, 3 to 24 Pole; also 4 Pole 12 Way and 54 Pole on/off. Commutating switch section and control wafers available.

**ONE HOLE FIXING SWITCHES**  
12/- per dozen, 75/- per 100



SINGLE-POLE Double Throw, 3 amp. 250 A.C.  
Can be used as ON/OFF or CHANGE-OVER SWITCH.

**SMALL MAGNETIC COUNTERS**



3½ x 1in., 10 counts per second with 4 figures. The following D.C. voltages are available, 6 v., 12 v., 24 v., 50 v., or 100 v.

**35/-** Post 1/6.

**VEEDER-ROOT MAGNETIC COUNTERS WITH ZERO RESET 800 COUNTS PER MINUTE. COUNTING TO 999,999. GENERAL PURPOSE TYPE.** 230 volts A.C. 65/-, Post 2/9.

**MINIATURE BUZZERS.** 12 v. with adjustable tone, 7/6.

**BUZZERS.** 230 v. A.C. Ironclad Gents P367, 50/-, post 3/6.

**HIGH NOTE BUZZERS.** 24 v. A.C./D.C. with tone adjuster, 2½ in. dia. bakelite case, 10/6, post 1/6.

**INTERCOM. TELEPHONE SET.** Ringing and speaking both ways. Supplied with buzzers, pushes, battery, etc. 75/-, Post 4/-, 4 Core Cable 8d. yard.

**WESTALITE BATTERY CHARGERS.** Input 200/250 v. A.C. will charge 6-volt or 12-volt batteries at 0/40 amps. £39/10/- each. Carriage 20/-.

**15-AMP. BATTERY CHARGER.** Will charge three lead acid cells at 15 amps. Input 200/250 volts, 50 cycles A.C. £8/10/-, Carriage 15/-.

**SELENIUM METAL RECTIFIERS F.W. BRIDGE**  
12 Volts 1 Amp. 7/6 ea. 24 Volts 1 Amp 12/6 ea.  
12 Volts 2 Amps 12/6 ea. 24 Volts 3 Amps 27/6 ea.  
12 Volts 4 Amps 17/6 ea. 24 Volts 5 Amps 35/- ea.  
12 Volts 6 Amps 20/- ea. 24 Volts 8 Amps 40/- ea.

**Mains transformers for 12 v. rectifiers.** 1 Amp. 15/-; 2 Amp. 20/-; 4 Amp. 25/-; 6 Amp. 30/-.

**TERMINAL BLOCKS.** 2-way 5C/431 or 3-way 5C/432, 6/- per doz., 50 for 16/8, 1,000 for £11.

**SATCHWELL THERMOSTATS** adjustable between 70°-190° Fahrenheit, 0-440 v. A.C., 20 amp., 11in. stem. Fitted cover 19/6, post 2/6.

**ROOM THERMOSTAT.** Adjustable between 45 and 75 deg. Fahr., 250 v. 10 amp. A.C. Ideal for greenhouses, etc., 35/-, post 2/6.


**MORSE KEYS.** Precision instrument made to inter-service specifications. Fully adjustable within fine limits. 10/6. Post 1/6.

**PRECISION SILVER MICA CAPACITORS.** 0.1 mfd. ½/10 - ca., 1% 7/6 ea., .02 mfd. 1% 5/- ea.

**BLOWER MOTORS.** 200/250 volt Capacitor Type 2,800 r.p.m. Cylindrical casing 7in. x 7in. x 7in. with open flange, each end £12/10/-.

**2in. Moving Coil Flush Round**  
Microamps 0/500 25/-  
Milliamps 0/1, 0/5 or 0/10.  
Volts 0/20, 0/30 or 0/40  
Amps 0/5, All D.C. 27/6 ea.

**2in. Moving Coil Flush Round**  
10-0-10. Milliamp, 35/-; 50 Milliamp, 35/-; 100 Milliamp, 25/-, Proj. Round 50 Microamps. Special scale, 45/-, All D.C. 100 Microamps, A.C. 85/-.



**3½in. MC Flush Round.** 2 Milliamp 200 v. both 60/-, 500 Microamp 70/-, 10 amp. 45/-.

**M.C. RECTIFIER A.C. METERS.** 3½in. FR 10 Milliamps, 70/-; 50 volts, 72/-; 100 volts 72/-; 200 volts 75/-; 1,000Ω per volt.

**FREQUENCY METERS.** 45-55 cycles per second, 230 volt, 6in. dia. Flush Round. Brand new, £10/10 -.

**VOLTMETERS** with alarm contacts 55/65 volts Moving Coil 6in. 150/-.

**PORTABLE VOLTMETERS** 150 volts D.C. MC 6½in. square by 3½in., 70/- each, post 3/6.

**PORTABLE AMMETER.** 0.3 amp. A.C./D.C. 8in. scale, 35/-, post 3/-.

**AMMETER.** 50-0-50 amp., 2in. Flush square, 17/6.

**VOLTMETER.** A.C. 0/300 2½in. Flush Round, 25/-, Postage on small meters 2/-, large 3/-.

**WEE MEGGER INSULATION TESTERS 500 VOLT SERIES 3.** BRAND NEW in leather carrying case, £18/10/-.

**MEGGER,** Series 2, ali. case, 500 volts 100 megohms, with leather case, leads, key, etc. Brand new. £37/10 -.

Few others available in good condition, £25.

**AVO TEST BRIDGES.** 200/240 volt A.C. Measures capacities from 5 pf. to 50 mfd. and resistances from 5 ohms to 50 megohms. Valve voltmeter range 0.1 to 15 volts, and condenser leakage test. Full working instructions, supplied with instrument. £9/10/0. Post 5/-.

**NEW MODEL 7 AVOMETER POWER FACTOR AND WATTAGE UNIT £7.**

A few AVOMETERS Models 7 also available £17.

**JACK PLUGS.** Cylindrical Bakelite screw-on cover, 2 con- tact, 2/6, post 6d.

P.O. 201 on headphone cord 10H/117, 3/- ea., post 1/3.

**AUTO TRANSFORMERS by S.T.C.** Totally enclosed C core type, 110-250 volts, 8 tapping, 50 cycles, size 6½in. x 5½ x 5½ 500 watts. New latest type, £4.

**POTENTIOMETERS, WIREWOUND AND CARBON** including Subminiature. Sealed and Precision types.


**MINIATURE SILVER ZINC ACCUMULATOR.** 1.5 volt, 1.5 ampere. Size 2in. x 1.13in. x 0.63in. Weight 1¼ oz. Ideal for model work, 12/6 ea., 120/- doz., post 9d.

**STROBOSCOPE FORK.** 125 cycles. P.O. No. 5 30/- ea., post 2/-.

**CABLE COUPLINGS.** Watertight 5 amp. 4 pole Brass Plugs and Sockets, 10/-, per pair, post 2/-.

**AMAZING VALUE**

**SILENT POWERFUL AC MOTOR**  
230 VOLTS  
RESILIENT MOUNTED



Fitted with thermal protecting device with Push Button reset ensures complete protection against overheating or burn-out. Ideal for lathes, drills, etc. 1440 r.p.m. ½in. shaft 1½in. long. G.E.C. make. In ¾ h.p. frame. Fully Guaranteed.

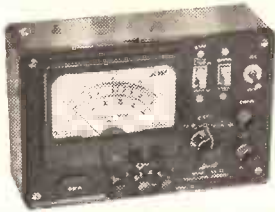
**PRICE 97/6**  
Carr. 7/6.

**SMI MINIATURE MICRO SWITCHES**  
HONEYWELL 11SM1-TN13, S.P.D.T. Size: .78in. x .250in. x .356in. 6/6 each.  
**MICRO SWITCH.** Burgess MK4BR, robust die cast casing, 8/6 ea., post 9d.

**L. WILKINSON (CROYDON) LTD.**  
LONGLEY HOUSE LONGLEY RD. CROYDON SURREY  
Phone: THO 0236 Grams: WILCO CROYDON



**TRANSISTOR TESTER  
Model AT-1**



Measures characteristics of PNP and MPN. Transistor and power diodes. Precision transistor portable instrument. 50µA meter with fitted moving coil. **£10.10.0** P. & P. 7/6

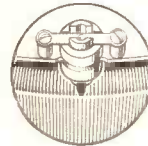
**VARIABLE VOLTAGE TRANSFORMERS**

**WORLD FAMOUS "SLIDE-TRANS" AVAILABLE ONLY FROM I.M.O.**



★ **RATED CURRENT CONSISTENT AT ALL POINTS ALONG THE WINDING.**  
Output: 0-260 v. Input: 230 v. A.C. 50/60~.  
Shrouded fully variable transformers for bench or panel mounting.

Inset shows latest type brush gear providing 1 volt variation.



1 Amp.	<b>£4.10.0</b>
2.5 Amp.	<b>£5.17.6</b>
5 Amp.	<b>£9. 0.0</b>
10 Amp.	<b>£18. 5.0</b>
20 Amp.	<b>£32.10.0</b>

Carr. & Pkg. extra

**CONSTANT VOLTAGE TRANSFORMER  
AUTOMATIC MAINS  
STABILIZER**



★ **CORRECTED WAVE**  
Modern design in 2-tone grey hammer steel case with handle. Complete with lead and plug.

Provides perfectly stabilized constant voltage for all laboratory equipment.

★ **No Moving Parts** ★ **No Maintenance.** ★ **No Attention.**

Specification:

- ★ Input: 240 v. A.C. ±20%—50 cycles.
- ★ Output: 240 v. A.C.
- ★ Accuracy: ±1%.
- ★ Capacity: 250 watts.
- ★ Size: 11 × 6½ × 6in. high.
- ★ Weight: 21 lbs. Fitted signal lamp and switch.

**£11.10.0** Carr. & Pkg. 20/-

**1,000 WATT MODEL**  
Input 240 v. A.C. ±20%.  
Output accuracy ±1%.  
Fitted signal lamp & switch, complete with plugs **£29.10.0.** Carr. and pkg. 25/-.

**PORTABLE  
VARIABLE A.C.  
POWER SUPPLY  
UNIT**

DESIGNED FOR ENGINEERS WHOSE REQUIREMENTS CALL FOR A VISUAL INDICATION OF VOLTS APPLIED.

OUTPUT: 0-260 v. 1½ amps.

INPUT: 230 v. A.C. 50/60~. Unit fitted with fuse, voltmeter, safety indicator, on-off switch and lead. Size: 8 × 5 × 5in. high.



PRICE **£8.10.0** Carr. & Pkg. 10/-

**IMMEDIATE DESPATCH**  
FULL SPARES AND SERVICE AVAILABLE

**AC/DC VALVE VOLTMETER**



Price **ONLY £35.0.0**  
C/W probes and leads—no extras.

Latest circuitry provides perfect stability and sensitivity. Professionally acknowledged.

**JUST LOOK AT THIS SPECIFICATION!**

- ★ 11 megohms per volt.
- ★ 5mV-1,500 V. A.C.
- ★ 100 mV-1,500 V. D.C.
- ★ 0.1 ohm—1,000 Megohms. PLUS

★ 1 Kc Oscillator Test Source.  
★ Complete with Test Probe with BUILT-IN A.C./D.C. switch, no fumbling or fiddling with out-of-reach knobs.

This superbly finished instrument is invaluable in Production depts. and Labs. and is presented in an attractive light grey crackle steel case with satin alloy front. Mains operated: Size and weight: 5½ × 3 × 8in. high, 5½lb.

LATEST Miniature

**WALKIE TALKIE**

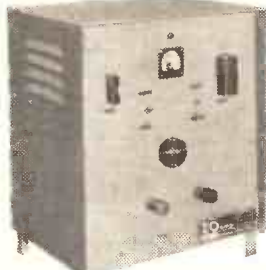
Produced to exacting specifications by leading manufacturers—E. K. Cole & Co.

This Transmitter/Receiver weighs only 5½lb. (approx.) and measures 3½ × 5½ × 9½in. A crystal controlled 4 frequency set operates from standard 'dry' battery—H.T./L.T. (i.e. Vidor L5537), 14 current series B7G valves used.

As supplied by us to Overseas Govt. Depts. SUPPLIED COMPLETE WITH VALVES & CRYSTALS  
Details & Prices of all Accessories supplied on request.

'88' Set  
Only **£10.0.0** EACH

**20 AMP. SUPPLY UNIT**



LATEST DESIGN!

HEAVY DUTY 12/24 VOLT D.C.

Spec.: Output: Adjustable up to 20 amps CONTINUOUS at 12/24 volts plus trickle. Input: 220/230/240 VAC 50 cycles. Input and Output fully fused. Neon indicator, 0-20 amp.meter. Size: 16 × 12 × 20in. high, in heavy gauge steel cabinet. Grey Hammer finish. Weight: 50 lbs. Plus 40/- Carr. & Pkg. G.B. (Inland)

ONLY **£29.10.0**

BUY DIRECT FROM MANUFACTURER

**TRANSISTORISED MEGOHMMETER**

★ **NO WINDING!**  
★ **PUSH BUTTON TO READ**  
500V.-1,000 MEGOHMS  
Portable supplied c/w batteries, probes and carrying case. Superb instrument.

ONLY **£23.10.0** Carr. & Pkg. 7/6.

Also: 500 v.-500 Megohms mains operated insulation tester. **DESIGNED FOR CONTINUOUS USE.** £26-5-0

**30 AMP. SUPPLY UNIT**

0 to 18 V.D.C. WITH SMOOTH STEPLESS VARIATION.  
Designed for CONTINUOUS use at max. loading.

★ Fitted voltmeter and ammeter.

★ Input and output fully fused.

Input Mains A.C.

Robust Construction.

2 tone grey hammer finish. Steel case.

**£49. 10. 0** Carr. & Pkg. 40/- G.B. (Inland)

Entirely suitable for plating plants, laboratory supplies, etc.

**36ft. AERIAL  
MASTS  
NEW LATEST PATTERN  
TUBULAR MASTS**

Check these vital points:

- ★ Made from 6 × 1½in. dia. Sherardized steel sections, for durability and strength.
- ★ Extra strong locating base.
- ★ Top cap with fitted pulley and halyard.
- ★ 2 sets (8) Rotproof Guy.
- ★ Rustproofed Steel Picketing Stakes.

ONLY **£13.2.6** ex works  
Carr. 17/6. Returnable wooden case 20/-.



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(ELECTRONICS) LTD.**

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(Dept. WW7), 313 Edgware Road, London, W.2.

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**RELAY UNIT.** G.P.O. 600 types 5 relays 150 ohm 1 set C/O, and 5 relays 400 ohm 2 M., 1 set C/O, in metal box 8x6x5in., £2, post 5/-.  
**BC-221 or LM 13.** Freq. meter complete with original charts in good working order. Range 125 kc/s.-20 Mc/s., £16/10/-, carr. 15/-.

**SIGNAL GENERATORS**

**TF.144G.** 230 v. A.C. 85 kc/s.-25 mc/s. In excellent condition, £16/10/- each, 25/- carr.

**TS.12AP.** Standing Wave Indicator Equipment. Complete with Amplifier and waveguide plumbing equipment, £12/10/- each, 15/- carr.

**TS.36AP** Power Meter, with accessories, used for checking radar outputs, £5 each, 10/- carr.

**DE-ICER, Controller Mk. 3.** Contains 10 relays D.P. changeover heavy duty contacts, 1 relay 4P, C/O. (235 ohms coil). Stud switch 30-way relay operated, one five-way ditto, D.C. timing motor with Chromometric governor 20-30 volts 12 R.P.M., geared to two 30-way stud switches and two Ledex solenoids, 1 delay relay, etc., sealed in steel case, size 4x5x7in., £3 each, post 5/-.

**BC640 MODULATOR UNIT.** 2x811's, mod. transformer and fil., trans. complete mod. unit fits 19in. rack 50 watts, £5/10/-, carr. £1.

**GEARED MOTORS (Reversible)**

20-30 v. D.C. 72 r.p.m., 17/6, post 2/6.

28 v. 150 r.p.m., 25/-, post 2/6.

24 v. Open gears with governor, approx. 10 r.p.m., 25/-, post 2/6.

24 v. D.C., 1.4 r.p.m., reversible with two micro switches inside gear box, silent operation, £2 each, post 5/-.

A.C. Motor 115v. 50 c/s/1300 H.P., 3000 r.p.m. Capacitor 1 mfd. 25/-, post 3/-.  
 Dalmotor SC5, 28 v. D.C. at 45 amps.; 12,000 r.p.m., output 750 w. (approx. 1 h.p.), brand new, £2/10/- each, post 7/6.

**AZIMUTH INDICATOR UNIT ID-260/GRD** 115 v. 50 c/s., complete with Azimuth Bearing Indicator and suitable for aerial direction control, 2" tube with shield suitable for modulation percentage indicator or oscilloscope and 3" speaker that can be utilised as a sidetone monitor. With all valves, in excellent condition, price £8/15/-, carriage 15/-.

**CRD6 DIRECTIONAL ANTENNA** for use with the above Instrument, £5 each, carriage £1.

**CM23 COMPARATOR SIGNAL UNIT**, £4/10/-, carriage 15/-.

**MARCONI V. LVE**

**VOLTMETERS TF428-B/1.**

Ranges: 0 to 1.5, 5, 15, 50 and 150 volts. Fitted with probe unit for RF measurements. 230 v. mains input. Brand new, £12/10/- each, carr. 10/-.

**TCS MODULATION TRANSFORMER** 20 w. Pri., 6,000 ohm C.T. Sec., 6,000 ohm, 25/- each, post 3/6.

**MICROPHONE TRANSFORMER.** Pri., 75 ohm. Sec., 125,000 ohm. 10/- each, post 2/6.

**OUTPUT TRANSFORMER.** Pri., 7,500 ohm. Sec., 500 ohm. C.T., 2.5 w. 12/6 each, post 3/-.

**POWER SUPPLY** unit for SENDER No. 36, 110-240 v. A.C. input, contains Speech amplifier. Modulator and External power supplies, 3xFW4/500 rectifiers provide H.T. for F.R. unit Speech amplifier 6C5G, Modulator 2x6C5G and 2x807 output. Size 24x16x14 inches. Housed in a fine oak case with circuit. Weight 110 lbs. As new, £6/12/6, carr. 30/-.

**CONDENSERS.** 1 mfd., 20 kv., £6/12/6 each, post 12/6 each. 0.25 mfd., 32,500 volts Wkg. £5 each, post 12/6 each. 150 mfd., 290 volts A.C. £5 each, post 12/6. 50 mfd., 330 volts A.C. 40/-, post 4/-.

10 mfd., 1,000 v. 12/6, post 2/6. 8 mfd., 1,500 volts, 17/6, post 2/-.

8 mfd., 1,200 volts, 12/6, post 3/-.

8 mfd., 600 volts, 8/6, post 2/6. 0.25 mfd., 2 kv. 4/-, post 1/6.

4 mfd., 12,500 v. D.C. working, £7/10/- each, carr. 15/-.

Vacuum condenser 50 pf. 32 kv. 30/-, post 1/6. 6 pf. 20 kv. 22/6, post 1/6.

All the above are new in cartons.

**BLOWER MOTORS.** 24 v. D.C. (small U.S.A.), 12/6, post 2/-.

**OSCILLOSCOPES,** Cossor 1035 and 1049, used condition, £30 each. Hartley type 13A, £25 each.

**INVERTERS.** Type AN3499, 28 v. D.C., 9.2 amps. input, 115 v. 400 c/s 3 phase, £5 each, post 5/-.

**TX DRIVER UNIT.** 100-156 Mc/s. Ideal for two meters, Valves 3C24, in excellent condition, fits 19in. rack, £5 each, carr. 20/-.

**CONTROL UNIT.** 230 v. A.C., output 24 v. 2 amps., 230 v. A.C. solenoid switch, 15 amps., plus relays and switches, etc., £2/10/-, carr. 12/6.

**RECEIVERS. HRO.** Used condition, less coils £10 each, carr. £1. C.52, used, freq. 1.75-16 Mc/s., £5, carr. £1.

**UNISELECTORS.** 6 bank, 25 way, 20 ohm. coil, £2 each, post 2/6; 5 bank, 25 way, 20 ohm. coil, 35/- each, post 2/6. (Ex-new equipment.)

**BOMB SELECTOR UNIT,** complete with uniselectors 3B., 25 watt, 22 ohms, magnetic counter 0-40, and 1 relay 500 ohm. 2 make, 50/- each, post 3/6.

**HEADPHONES.** DLR5, 10/- pair, 2/6 post. No. 10 headset and microphone, 15/-, post 2/6. M/C phones with chamois ear muffs and jack plug, 17/6 pair, post 2/6.

**APX6 TRANSPONDER.** Complete with UHF valves 2C42, 2C46 and 1B40, complete with special holders and condensers. 30 Valves, Blower Motor, Mechanical Counters, etc. 115 v. 400 c/s. (Suitable conversion for 1,200 Mc/s.). Price £10 each, carriage 15/-.

**AUTOMATIC PILOT UNIT Mk. 2.** This complex unit of diodes and valves, relays, magnetic clutches, motors and plug-in amplifiers, with many other items, price £7/10/-, £1 carriage.

**C.52 POWER SUPPLY** 110/230 v. A.C. or 12 v. D.C. input, £2/5/- each, Carr. 12/6.

**U.S.A. DESK MICROPHONE CRV/51018/A.** Complete with 7 yards of screened cable and universal jack (adjustable), 10/- each, post 3/-.



**POWER AND SMOOTHING UNITS.** 100-250 v., A.C. input 24 v., D.C. at 3 amps. or 12 v. twice at 3 amps., continuous rating, switched fused, etc. In metal case 19 x 7 x 7in. Smoothing two large chokes and 0-1 ma. meter scaled 0-50 volts. £7/10/- (pr.), 15/- carr.

**RESISTORS.** Variable. 3 ohm. 10 amps., 25/-, post 4/-.

**ROTARY TRANSFORMERS.** 24 v. input, 175 v. at 40 ma. output, 25/-, plus 2/- post. EICOR type, 12 v. input, 400 v. at 180 ma. output, 30/-, plus 4/- post. 12 v. input, 225 v. at 100 ma. output, 25/-, plus 3/- post. (All the above are D.C. only.)

**MICROPHONE Type T50.** Fits the palm of hand with on/off switch and lead (electro dynamic), 35/- each, plus 2/6.

**CIRCUIT BREAKER.** 150 amps. 600 v. A.C., £3 each, carr. 7/6.

**PLUGS.** Standard two-way jack plug PL55 with 6ft. lead and transformer, low to high impedance, 7/6 each, plus 1/6 post. PL68 plug and switch lead assembly, 5/- each, plus 1/6 post.

**DIPOLE AERIAL.** Complete set suitable for 60-100 Mc/s., 27/6, carr. 4/-.

**COMPRESSOR UNIT.** Aircraft cabin pressurisation unit, 28 v. D.C., with automatic switches, etc., £3/10/-, post 6/-.

**AR88 SPARES.** Set of 14 valves and headphones and 3 pilot lamps, new, original cartons, £3/10/- each, post 2/6. Set of 14 valves only, £2/10/-, post 2/-.

Vibrator unit, 6 v., 15/-, post 4/-.

Headset only, 12/6, post 2/-.

Speaker unit, R.C.A., £3/10/-, plus 5/- post.

Block condenser unit, 3x4 mfd. at 600 v., 25/- each, post 3/-.

0.01 mfd. 400 v. D.C., 4 for 12/6.

Capacitor air trimmer, 2-20 pf., box of 3, 10/-.

**1154 TRANSMITTER UNIT** less power supplies (used), £4 each, plus 15/-.

**TRANSFORMERS.** 230 to 115 v., isolation 300 va., £3 each, plus 5/-.

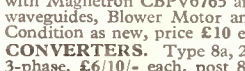
230 v. pri., 1,850-0-1,850 at 500 ma., £5 each, plus 15/- carr.

230/115 auto 300 watts, £2, post 6/-.

230 v. pri., 24 v. at 2 amp., 22/6, post 5/-.

230/115 v. pri., 275-0-275 v. at 120 ma., 6.3 v. at 4 amp., 6.3 v. at 1 amp., 25/-, post 5/-.

**RADAR RECEIVER AFG501.** Complete Unit with Blower Motor, 40 valves, Relays, Transformers, etc. Condition as new. Price £5 each, carriage 15/-.



**WHEATSTONE BRIDGE** in a beautiful

oak case, centre zero galvanometer 2.5 mA.,

4 stud switches, 0-10, 0-100 ohms, 0-inf.,

size 16x7x6in., 45/- each, 5/- post.

**RADAR TRANSMITTER AFG501.** Complete Unit in pressurised case with Magnetron CBPV6765 and Klystron 6378 and associated crystals and waveguides, Blower Motor and 12 valves. Power inputs 115 v. 400 c/s. Condition as new, price £10 each, carriage 15/-.

**CONVERTERS.** Type 8a, 24 v. D.C., 115 v. A.C. at 1.8 amps 400 cycles, 3-phase, £6/10/- each, post 8/-.

**SCANNER UNIT. AS. 596/APQ.43.** This modern piece of equipment made by a well-known American firm, normally for aircraft use, has a 30in. diameter parabolic reflector adjustable 180 deg. vertical and horizontal and is complete with standard waveguide couplings and rotary joints. Three powerful D.C. motors by Dalmotor Company, i.e. Types SC.5, SR.2 and PM.4. Three geared motors 0-6 r.p.m. and 0-150 r.p.m., also Kollsman Magslip motor type TY.971C-0460. Two solenoid contactors, small compressor unit with pressure gauge 0-30 and dehydrator unit. All the above is mounted in an aluminium casting, approx. weight 120-125 lbs. 4 Relays d.p. c/o. 24 v. 235 ohms., 4 Relays 4 p., c/o, 24 v. 235 ohms., Mechanical Counter 0-9999, 2 20K ± 0.15% Linear Potentiometer, 1,400 ohms. ± 3% Suppressors, Switches, Plugs, Sockets and assorted gears. Price £17/10/-, £2 carr. and £5 deposit for returnable container.

**MODULATOR UNIT APQ.43** mounted in a pressurised container with pulse transformer network units, 7 various relays, high voltage condensers 0.001 mfd. 10,000 v. D.C., 0.5 7,500 v. working. Valves: KU25, 3B24W, 705A(3), blower motor 27 v. .17 h.p., 7,600 r.p.m. 4.6 amps, 90 c.f.m. Omite switch 150 v. 10 amps, 8 pcs. Approx. weight 80 lbs. Price £10, carr. £1.

**APQ.43 RT UNIT** complete with Magnetron 4J50, Klystrons 2K25, WL.5846 and 18 other valves, 0-1 ma. meter, relays, etc. Weight 65 lbs. Price £15 each, carr. 17/6.

**ARN.21 or TR.9171** (Tacan Equipment), complete with valves, £25 each, carr. £1.

**TRANS./REC. WIRELESS SET** No. 31, complete sets with aerials, headphones and mikes in working order. Freq. 30/40 Mc/s. 4 channel xtal-controlled, £8/10/- each. **WIRELESS SET** No. 88. 4 channel, xtal-controlled, complete with all valves and xtals and attachments, £10 each.

**HIGH SPEED RELAYS** H96D, 500 + 500 ohm, 12/6 each, post 2/-.

**AERIAL CHANGEOVER RELAY,** Londex 24 v., 17/6 each, post 2/-.

**POWER UNIT P94A.** 24 v. D.C. input, 13 amps, 300 v. D.C. @ 300 ma., 150 v. D.C. @ 100 ma., 12 v. @ 5 amps., complete with relay, voltage regulator and radio suppressors, £3 each, carr. 12/6d., or 12 v. input, £3/10/- each.

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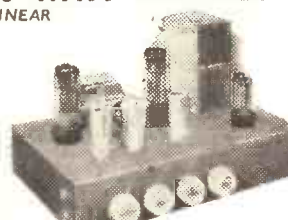
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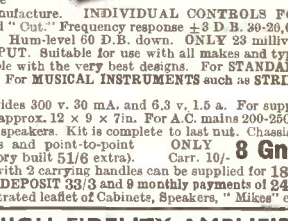
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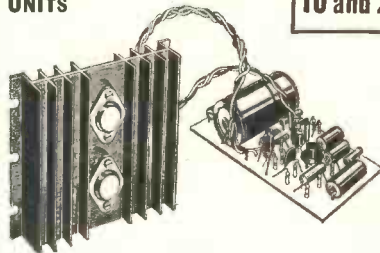


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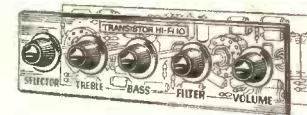
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★ **TRANSISTOR PORTABLE TEST EQUIPMENT**

All units size 6½ x 4½ x 2½ in.



- ★ RF generator, 150 kc/s to 350 mc/s in 8 ranges. RF, Mod. RF, AF outputs.
- ★ Resistance / capacitance bridge. £8.5. P.P. 2/6.
- ★ Audio generator 10 c/s—100 kc/s. 4 ranges. £16.15 P.P. 2/6

★ **VHF FM TUNER TO ASSEMBLE**



- ★ Two pre-built and aligned units plus metal work and panel.
- ★ 88 to 108 Mc/s tuning range.

★ Output 100mV. to 100 k/ohm.  
★ 6-transistor superhet, printed circuit design.  
★ Size 9½ x 3½ x 4in. ★ S/N 50dB.  
TOTAL COST TO BUILD £12.17.6 P.P. 2/6  
(All units sold separately.)

★ **2 AND 4 TRACK RECORDERS TO ASSEMBLE**

TOTAL COST TO BUILD

2-track £26 P.P. 8/6

4-track £30 P.P. 8/6

Complete range of decks, amplifiers and pre amps. in stock.



- ★ Collaro Studio decks.
- ★ 6-valve record/play amplifiers.
- ★ Sturdy portable cabinets with speaker.
- ★ Printed circuit, pre-built units.
- ★ Complete in every detail.

★ **RECORD AND PLAYBACK SYSTEM★**

LET US QUOTE FOR PARTS FOR YOUR CIRCUIT. SEND LIST FOR QUICK REPLY.

TRADE AND EXPORT ENQUIRIES INVITED.

★ **MULTI-TEST METERS (Full details in Catalogue).**

★ PT34	1 k/ohm per volt	£1 19 6
★ M1	2 " " "	£2 9 6
★ THL33	2 " " "	£3 15 0
★ EPI0K	10 " " "	£3 19 6
★ EP20K	20 " " "	£4 19 6
★ TP5S	20 " " "	£5 19 6
★ ITI-2	20 " " "	£4 9 6
★ EP30K	30 " " "	£6 10 0
★ Model 500	30 " " "	£8 17 6
★ EP50K	50 " " "	£8 15 0
★ EPI00K	100 " " "	£10 10 0

★ Model 700. Professional meter, 20 k/ohm/volt with AC/DC volts, resistance DC and AC current. Size 7½ x 5½ x 3½ in.

PRICE £17.10.0 P.P. 5/-



All types Brand New and guaranteed. (Post and packing 1/6 per meter).

SINCLAIR EQUIPMENT X10 Kit £5/19/6. X10 Built £6/19/6.  
X20 Kit £7/19/6. X20 Built £9/19/6.  
(All Sinclair designs in stock.)

**HENRY'S RADIO LTD.**  
303 EDGWARE ROAD LONDON W2  
PADdington 1008/9  
Open Mon. to Sat. 9-6. Thurs. 1 p.m.  
Open all day Saturday.





**SEW**

# PANEL METERS

MANUFACTURED BY SHINOHARA ELECTRICAL INSTRUMENTS LTD., JAPAN. FAMOUS ALL OVER THE WORLD FOR THE QUALITY, DEPENDABILITY AND ACCURACY OF THEIR INSTRUMENTS. The comprehensive range below is available ex-stock. Other ranges to special order. Special quotations for quantities.

S.A.E. FOR ILLUSTRATED LEAFLET

## CLEAR PLASTIC METERS



**Type MR.38P. 1 2 1/2 in. square fronts.**

50µA	32/6	750mA	22/6
100µA	29/6	1A D.C.	22/6
200µA	27/6	2A D.C.	22/6
500µA	25/6	5A D.C.	22/6
50-0-50µA	29/6	3V D.C.	22/6
100-0-100µA	27/6	10V D.C.	22/6
500-0-500µA	22/6	20V D.C.	22/6
1-0-1mA	22/6	60V D.C.	22/6
1mA	22/6	100V D.C.	22/6
2mA	22/6	150V D.C.	22/6
5mA	22/6	300V D.C.	22/6
10mA	22/6	600V D.C.	22/6
20mA	22/6	750 V.D.C.	22/6
50mA	22/6	15V A.C.	22/6
100mA	22/6	50V A.C.	22/6
150mA	22/6	150V D.C.	22/6
200mA	22/6	800V A.C.	22/6
300mA	22/6	600V A.C.	22/6
500mA	22/6	8 Meter 1mA	29/6

**Type MR.52P. 2 1/2 in. square fronts (Cont.)**

50mA	32/6	300V A.C.	32/6
100 mA	32/6	'S' Meter 1mA	39/6
500 mA	32/6	*1A A.C.	32/6
1A D.C.	32/6	*5A A.C.	32/6
5A D.C.	32/6	*10A A.C.	32/6
20V D.C.	32/6	*20A A.C.	32/6
300V D.C.	32/6	*30A A.C.	32/6

**Type MR.85P. 4 1/4 in. x 4 1/4 in. fronts.**

50µA	69/6	1 amp. D.C.	45/-
100µA	59/6	5 amp. D.C.	45/-
200µA	55/-	15A D.C.	45/-
500µA	49/6	30A D.C.	45/-
50-0-50µA	69/6	*1A A.C.	45/-
100-0-100µA	59/6	*5A A.C.	45/-
500-0-500µA	49/6	*10A A.C.	45/-
1-0-1mA	45/-	*20A A.C.	45/-
1mA	45/-	*30A A.C.	45/-
5mA	45/-	20V D.C.	45/-
10mA	45/-	50V D.C.	45/-
50mA	45/-	150V A.C.	45/-
100mA	45/-	300V D.C.	45/-
500mA	45/-	15V A.C.	45/-
		300V A.C.	45/-

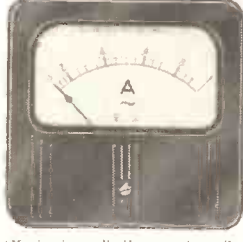
**Type MR.65P. 3 1/2 in. x 3 1/2 in. fronts.**

50µA	59/6	50A D.C.	42/6
100µA	49/6	*1A A.C.	35/-
500µA	39/6	*5A A.C.	35/-
50-0-50µA	59/6	*10A A.C.	35/-
100-0-100µA	49/6	*20A A.C.	35/-
500-0-500µA	39/6	*30A A.C.	35/-
1mA	35/-	10V D.C.	35/-
5mA	35/-	20V D.C.	35/-
10mA	35/-	50V D.C.	35/-
50mA	35/-	150V D.C.	35/-
100mA	35/-	300V D.C.	35/-
500mA	35/-	15V A.C.	35/-
		150V A.C.	35/-
		300V A.C.	35/-
		600V A.C.	35/-

## BAKELITE PANEL METERS

**Type MR.65. 3 1/2 in. square fronts.**

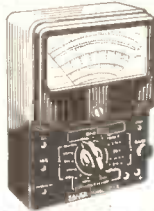
25µA	65/-	30A D.C.	29/6
50µA	42/6	50A D.C.	29/6
100µA	39/6	*1A A.C.	29/6
500µA	35/-	*5A A.C.	29/6
50-0-50µA	42/6	*10A A.C.	29/6
100-0-100µA	39/6	*30A A.C.	29/6
500-0-500µA	35/-	*50A A.C.	29/6
1-0-1mA	29/6	5V D.C.	29/6
50mV	39/6	10V D.C.	29/6
100mV	39/6	20V D.C.	29/6
1mA	29/6	50V D.C.	29/6
5mA	29/6	150V D.C.	29/6
10mA	29/6	300V D.C.	29/6
50mA	29/6	*30V A.C.	29/6
100mA	29/6	*50V A.C.	29/6
500mA	29/6	*150V A.C.	29/6
1A D.C.	29/6	*300V A.C.	29/6
5A D.C.	29/6	300V A.C.	35/-
15A D.C.	29/6	VU Meter	49/6



\*Moving iron, all others moving coil.

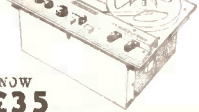
## MAGNAVOX 363 TAPE DECKS

New 3 speed tape deck, supersedes old Collaro studio deck. 2 track, £10/10/-, 4 track, £13/10/-. Carr. Paid.



**MODEL 370-E MULTIMETER**  
20,000 Ω/volt D.C. volts.  
0/1, 2.5/10/250/1,000v.  
A.C. volts 0/2.5/10/250/100/5,000v.  
D.C. Current 0/50 µA/1/10/50/250mA/1/10 amp.  
A.C. Current 0/250mA/1/10 amp. Resistance: 0/5k/500k/5 meg/50 meg.

## PROFESSIONAL 4-TRACK STEREO RECORD AND PLAYBACK TAPE DECK



Complete with 4 valve/4 transistor pre-amplifier. Will record and play back 4 track stereo and 1 track mono at 7 1/2 or 3 1/2 I.P.S. Twin meter level indicators, digital counter. Mic gain/tuner inputs. Audio output 500 MW Bias and Erase 80 kc. Response 40-18,000 C.P.S. at 7 1/2; 40-12,000 C.P.S. at 3 1/2 I.P.S. Motor 4 pole H.D. induction. Tape size up to 7in. 220/240 v. A.C. Size 15in. x 10 1/2in. x 6 1/2in. Line up: 4 - 28B173, 2 - 12A17, 1 x 12A17, 1 x 12BH7, S.A.E. FOR FULL DETAILS. PRICE £35. CARR. 15/-.

**G. W. SMITH & CO (RADIO) LTD**  
3-34 Lisle St., London, W.C.2 ALSO SEE OPPOSITE PAGE

## AVOMETERS

Supplied reconditioned, guaranteed perfect.

**MODEL D £8/19/6**  
Post & Ins. 5/-.



**TE-000. 20,000Ω/VOLT GIANT MULTIMETER.**  
6in. full view meter. 2 colour scale. 0/2.5/10/250/1,000/5,000 V. A.C. 0/25/1/2.5/10/50/250/1,000/5,000 V. D.C. 0/50µA/1/10/100/500MA/10 amp. D.C. 0/2K/200K/20 MEG OHM £13/10/- P.P. 6/-

**MODEL 500. 30,000 O.P.V. VOLT MULTIMETER**  
0/1.5/1/2.5/10/25/100/250/500/1,000 V. D.C. 0/2.5/10/25/100/250/500/1,000 V. A.C. 0/50µA/5/50/500mA. 12 amp. D.C. 0/50/K8 Meg/80 Meg Ω. £8/17/6. Post Paid.



**MODEL TE-12. 20,000 O.P.V. 0/0.6/6/30/120/600/1,200/3,000/6,000 V. D.C. 0/6/30/120/600/1,200 V. A.C. 0/60µA/6/60/600 MA. 0/6K/60K/6 Meg/60 Meg Ω. 50 PF. -2MFD. £5/19/6. P. & P. 3/6.**

**TE-58. DE LUXE 20,000Ω/VOLT MULTIMETER**  
0/6/30/120/600/1,200 V. A.C. 0/6/6/30/120/600/1,200V. D.C. 0/60µA/6/60/600 MA. D.C. 0/10K/100K/1M/10 MEG. OHM. 200PF-0.2 MFD. £5/19/6. P.P. 3/6.



**TS-76. 20,000 O.P.V. PUSH BUTTON MULTITESTER.**  
Simple operation, D.C. volts up to 1,000 v. A.C. volts up to 1,000 v. Resistance up to 10 megohm. Current up to 250 mA. Decibels -20 to +36 db. £5/5/- P. & P. 2/-.

**TE-51. NEW 20,000Ω/VOLT MULTIMETER.**  
0/6/60/120/1,200 V. A.C. 0/3/30/60/300/600/3,000 V. D.C. 0/60µA/1/2/300 MA. D.C. 0/60K/6 MEG. OHM 85/- P.P. 2/6.



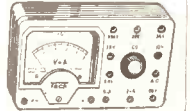
**MODEL NH201. 30,000 O.P.V. 0/25/1/10/50/250/500/1,000 v. D.C. 0/10/50/250/500 v. A.C. 0/50µA/10/250 MA. 0/5/K500K/5 Meg Ω S776. P. & P. 2/6.**

**MODEL AR-620. 20,000 O.P.V. 0/10/50/250/500/1,000 v. A.C. and D.C. 0/50µA/10/250mA. 0/10K/100K/1 Meg Ω. 250 PF - 02 MFD. 0-500 Henrys. 92/6. P. & P. 2/6.**



**MODEL ITI-2. 20,000 O.P.V. 0/5/25/250/500/2,500 v. D.C. 0/10/50/500/1,000 v. A.C. 0/50µA/25/250 mA. D.C. 0/60K/6 Meg Ω. 02.3 MFD. 78/6. P. & P. 2/6.**

**MODEL 2503. 2,000 O.P.V. 0/16/50/500/2,500 V. A.C. 0/10/50/500/2,500 V. D.C. 0/2 Meg Ω. 0/250 mA. -20 to +36 db. 49/6. P. & P. 2/6.**



**MODEL FT-1000. 1,000 O.P.V. 0/10/50/250/500/1,000 v. A.C. and D.C. 0/1/100/500 MA. D.C. 0/100 kΩ 39/6. P. & P. 1/6.**

## MODEL ZQM TRANSISTOR CHECKER

It has the fullest capacity for checking on A, B and Jco. Equally adaptable for checking diodes, etc. Spec.: A: 0.7-0.9967. B: 5-200. Ico: 0-50 microamps, 0-5 mA. Resistance for diode 200Ω -1 MEG. Supplied complete with instructions, battery and leads. £6/19/6. P. & P. 2/6.



## 9-TRANSISTOR 2 WAY RADIOS

Super quality. Range up to 5 miles. Complete with all accessories. £25 per pair. Post extra. Also available, 3-TRANSISTOR MODEL. Range up to 1 mile. Complete with all accessories. £9/17/6 per pair. Post extra. (S.A.E. for full details).



## MODEL PV-58 VALVE VOLT METER

11 meg. input. 7 D.C. volt ranges. 1.5-1500 v. A.C. volt ranges 1.5-1500 v. 4,000 Peak to Peak. Resistance 2 ohm to 1,000 megohm Decibels 10db to +60db Supplied brand new with instructions, leads and probe. £12/10/- P. & P. 3/6.



## VARIABLE VOLTAGE TRANSFORMERS

Brand New Guaranteed Fully Shrouded. Input 230 v. 50/60 c/s. Output 0-260 v.



1 amp. ....	£4/10/-	12 amp. ....	£19/10/-
2.5 amp. ....	£5/17/6	20 amp. ....	£32/10/-
5 amp. ....	£9/-	2.5 amp. portable, metal case with meter-fuses, etc.	£9/17/6
8 amp. ....	£13/10/-		
10 amp. ....	£17/-		

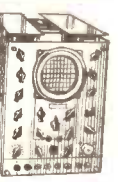
## VOLTAGE STABILIZER TRANSFORMERS

Will stabilize your mains voltage. Ideal for TV Receivers and Industrial equipment. Input 80-120 v. and 160-240 v. Constant output 110 v. or 240 v. 250 watts. Brand new guaranteed £10/10/- Carr. 7/6.



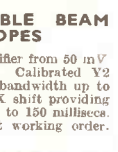
## ERSKINE TYPE I3 DOUBLE BEAM OSCILLOSCOPES

Timebase 2 c/s-750 kc/s. Separate Y1 and Y2 amplifiers. Up to 5.5 Mc/s. calib. at 100 kc/s and 1 Mc/s. 110/230 v. A.C. Guaranteed perfect £27/10/- carr. 20/-.



## COSSOR I035 DOUBLE BEAM OSCILLOSCOPES

4in. C.R.T. Calibrated Y1 Amplifier from 50 v to 50 v., bandwidth 10 Mc/s. Calibrated Y2 Amplifier from 5 v. to 500 v., bandwidth up to 100 kc/s. Directly calibrated X shift providing time measurement from 15µsec. to 150 milliseconds. Supplied in guaranteed perfect working order. £35. Carr. 20/-.



## SILICON RECTIFIERS

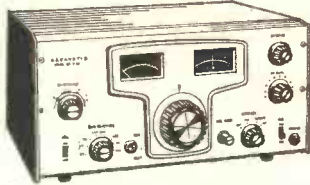
200 v. P.I.V. 200 MA. ....	2/6
400 v. P.I.V. 3 amp. ....	7/6
200 v. P.I.V. 6 amp. ....	5/6
1,000 v. P.I.V. 650 mA. ....	7/6
800 v. P.I.V. 500 mA. ....	5/6
400 v. P.I.V. 500 mA. ....	3/6
70 v. P.I.V. 1 amp. ....	3/6
150 v. P.I.V. 165 mA. ....	1/-

Discount for quantities. Post extra.

## MINE DETECTOR No. 4A

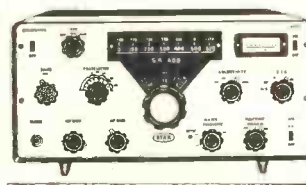
Will detect all types of metals. Fully portable. Compact with instructions, 39/6 each. Carr. 10/-. Battery 8/6 extra.





**NEW MODEL!**  
**LAFAYETTE HA-350**  
**AMATEUR RECEIVER**

10-80 metres dual conversion with mechanical filter for High Selectivity. Incorporates 12 valves, crystal controlled osc., Product detector, 100 Kc/s. crystal calib., crystal B.F.O., A.N.L., 'S' meter, etc. Supplied brand new and guaranteed. 75 GNS. S.A.E. for full details.



**STAR SR.600 AMATEUR**  
**COMMUNICATION RECEIVER**

New crystal controlled triple conversion de luxe 80-10 metre band receiver. Extremely high sensitivity, selectivity and stability. Special features include 3 I.F. stages, crystal controlled oscillator, 4-section I.C. filter, 'S' meter, V.P.O. A.N.L., 100 kc/s. crystal calibrator, etc. Supplied brand new and guaranteed. 95 GNS. S.A.E. for full details.

**LAFAYETTE HA-230 AMATEUR**  
**COMMUNICATIONS RECEIVER**

Supersedes Model HE-30. 8 valves + rectifier. Continuous coverage on 4 bands. 560 kc/s.-30 mc/s. Incorporates 1 RF and 2IF stages, Q Multiplier, B.F.O., A.N.L., 'S' meter, electrical bandspread, aerial trimmer, etc. Supplied brand new and guaranteed. 33 GNS. S.A.E. for full details. Also available in Semi-Kit form 25 GNS.

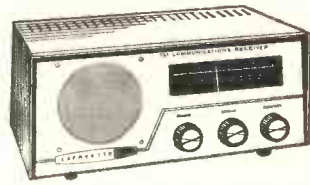
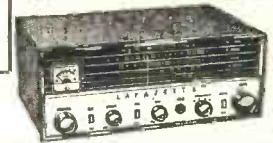


**STAR SR.40**  
**COMMUNICATION RECEIVER**  
4 Bands, 560 kc/s.-30 Mc/s. 'S' Meter-B.F.O.-A.N.L.-Bandspread Tuning-Built-in speaker. 200/250 v. A.C. Brand New. 18½ GNS., carr. 10/-.

**PART**  
**EXCHANGE**  
**WELCOMED**

**LAFAYETTE HA-63**  
**COMMUNICATION RECEIVER**

7 valves + Rectifier. 4 Bands. 560 kc/s.-31 Mc/s. 'S' Meter-B.F.O.-A.N.L.-Bandspread Tuning 200/250 v. A.C. Brand New. 24 GNS. Carr. paid.

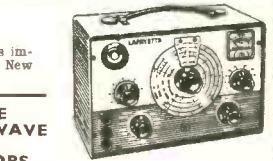


**NEW MODEL!**  
**LAFAYETTE HA-55**  
**AIRCRAFT RECEIVER**

108-136 Mc/s. High selectivity and sensitivity. Incorporates 2 RF stages including 6CW4 Navigator, 8 tubes for 11 tube performance, solid state power supply, adjustable squelch control, slide rule dial, built in 4in. speaker and front panel phone jack. 220/240 v. A.C. Supplied brand new and guaranteed. 19 GNS. Carr. 10/-.

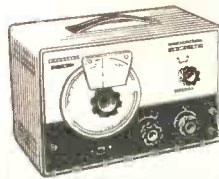
**LAFAYETTE TE-46 RESISTANCE**  
**CAPACITY ANALYSER**

2 PF-2,000 MFD. 2 ohms-200 megohms. Also, checks impedance, turns ratio, insulation 200/250 v. A.C. Brand New £15, carr. 7/6.



**TE22 SINE**  
**SQUARE WAVE**  
**GENERATORS**

Sine: 20 cps to 200 kc/s. on 4 bands. Square: 20 cps to 30 kc/s. Output impedance 5,000 ohms 200/250 v. A.C. operation. Supplied Brand New and guaranteed with instruction manual and leads. £15. Carr. 7/6.

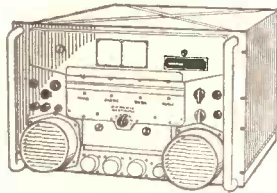


**LEADER LSG-10**  
**R.F. SIGNAL GENERATOR**

120 kc/s.-260 Mc/s. on 6 ranges. Variable R.F. and A.P. outputs. Large clear scale. Size 7½" x 10½" x 4½". 220/250 v. A.C. operation. Brand New £12, carr. 6/6.

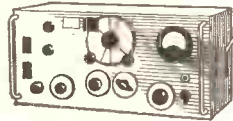
**R-278/GR RADIO**  
**RECEIVER**

U.H.F. receiver designed by Collins Radio. Provides reception of A.M. and C.W. signals on any one of 1750 channels in the frequency range of 225 to 399.9 Mc/s. and simultaneously on one fixed tuner channel in the frequency range of 238-248 Mc/s. Power requirements 115/230 v. 50/60 cps. Size 13in. x 19in. x 20in. Output 3 watts into 600 ohms. High quality modern equipment originally costing hundreds of pounds. Available in as new condition, fully tested, complete with all crystals. £60. Carr. 50/-.



**MARCONI TF 144G/4 STANDARD**  
**SIGNAL GENERATOR**

85 kc/s.-25 Mc/s. ± 1%. Output variable from 1µV to 1 volt. Internal sine wave modulation 400 cps. up to 75% depth. Operation 200/250 volts A.C. Offered in really excellent condition, like new, fully tested and guaranteed. £25, carr. 30/-.



**MODEL DA-1 TRANSISTORISED**  
**FULLY AUTOMATIC ELEC-**  
**TRONIC KEYSER**

230 V. A.C. or Battery operated. 4 diodes. £16/10/- P. & P. 4/6. Semi-Automatic Bug Keys. Precision made. Speed fully adjustable, £4/10/- P. & P. 2/6.



**G.E.C. BRT.402 RECEIVERS**

A high grade 14 valve communication receiver covering 160-385 kc/s. and 610 kc/s. to 30 Mc/s. in six bands. Special features include 2 RF stages, 'S' meter. Variable selectivity, B.F.O., A.N.L. A.G.C. 500 kc/crystal calibrator, slide rule vernier dial with logging scale. Operation for 95-130 v. and 186-250 v. A.C. Output for phones speaker or line. Offered in excellent condition, fully tested and guaranteed. £60, carr. 30/-.

**PRECISION COMBINATION**  
**VOLTMETER/AMMETER**

Two separate instruments housed in polished wood case, 6in. scales with knife edge pointers. Ranges as follows: A.C. and D.C. Volts 0-160-300-600. A.C. and D.C. Current: 0-25-50-150-200 amps. Supplied complete with shunts, leads and leather carrying case. Brand new condition. £9/19/6 each. Carr. 7/6.

**LELAND MODEL 27 BEAT**  
**FREQUENCY OSCILLATORS**

Frequency 0-30 Kc/s. on 2 ranges. Output 500Ω or 5kΩ. Operation 200/250 v. A.C. Supplied in perfect order £12/10/- Carr. 10/-.

**NOMBREX EQUIPMENT**

Transistorised Audio Generator 10-100,000 c/s. Sine or square wave. £16/15/-.  
Transistorised Signal Generator 150 kc/s.-350 Mc/s. £9/10/-.  
Transistorised resistance capacity bridge 1Ω-100 MegΩ, 1 pt-100µF. £8/5/-.  
Transistorised Induction bridge 1µH-100H, £18. Mains operated Transistor power supply unit, output 1-15 v. up to 100 mA. £6/10/-.  
All above post paid with battery.

**MAIN LONDON AGENTS FOR**  
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A.T.6 Amateur TX	£16 10 0
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**OS/3B/U OSCILLOSCOPES**

High quality Portable American Oscilloscope. 3in. crt. T/B: 3 c/s-50 Kc/s. X Amp: 0-500 Kc/s. Y Amp: 0-2 Mc/s. Power requirements 105-125 v. A.C. Supplied in brand new cond., fully tested. £25, carr. 10/- Suitable 230/115 v. Transformer 15/6.

**CTS3 SIGNAL GENERATOR**

8.9-15.6 mc/s. and 20-300 mc/s. Variable precision attenuator. A.C. mains. Supplied in perfect order less calibration chart. £12/10/- Carr. 10/-.

**REUTER TRACK TAPE**  
**HEADS**

As fitted to Collaro Mk. IV and Studio Decks. High imp. record/play back, low imp. erase. Brand new 19/6 Pair. Also Miniflux ½ track, set of 3, 29/6; Bradmatic ½ track, set of 2 92/6. Post extra.

**TS-382 F/U AUDIO OSCIL-**  
**LATOR**

High quality modern American instrument. Frequency coverage on 4 bands. 0-200 Kc/s Output impedance 1,000Ω. Output monitoring meter. 7 range output attenuator from 12 micro-volts to 12 volts. Operation 115 v. 50-1,000 CPS. Supplied as new. £40. Carr. 20/-.

**LAFAYETTE HI-FI STEREO HEAD**  
**PHONES**

★ Air cushioned headband  
★ Soft rubber ear pads  
★ Frequency response. 25 to 15,000 cycles. ★ High sensitivity. Impedance 8 ohms per phone. Supplied complete with all cables, wires, overload junction box and 3-connection plug. £2/6. P. & P. 2/6.



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First grade quality American tapes. Brand new and guaranteed. Discounts for quantities.

3in. 225ft. L.P. acetate	4/-
3in. 600ft. T.P. mylar	10/-
5in. 600ft. std. plastic	8/6
5in. 1,200ft. L.P. acetate	10/-
5in. 1,200ft. D.P. mylar	15/-
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5in. 1,800ft. D.P. mylar	22/6
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7in. 1,200ft. std. mylar	12/6
7in. 1,800ft. L.P. acetate	15/-
7in. 2,400ft. D.P. mylar	25/-
7in. 1,800ft. L.P. acetate	20/-
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Postage 2/- Over £3 post paid.

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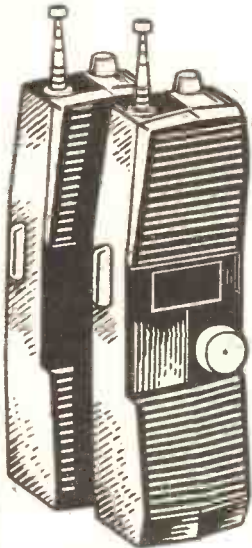
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## SUPER WALKIE TALKIES



12 TRANSISTORS  
1 DIODE  
1 THERMISTER  
**25 gns PAIR**

**MODEL HE-100.** Crystal control and Transistors and Receiver. A.M.V.C. Squelch, Push Pull Audio Output Range up to 7 miles under favourable conditions. Built-in separate speaker and mike for better modulation — gives increased range. Complete with carrying cases, batteries and telescopic aerials. Size 3in. wide, 9in. high, 2 1/2in. deep.

**9 TRANSISTOR AND 1 DIODE**

**£22.10.0** Pair

**MODEL HE-29C.** Crystal control on both Transmitter and Receiver. Push to talk operation. Earphone for personal listening. Complete with carrying cases, batteries and telescopic aerials. Size 6 1/2in. x 2 9/16in. x 1 1/8in.

**6 TRANSISTOR AND 2 DIODES**

**£17.10.0** Pair

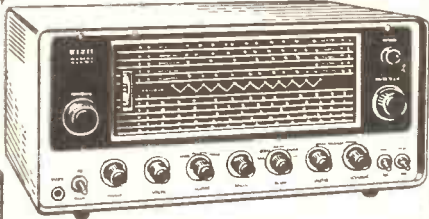
**MODEL HA-85.** Crystal control on both Transmitter and Receiver. On-off Volume control and push to talk switch. Earphone for personal listening. Complete with carrying cases, batteries and telescopic aerials. Size 6 1/2in. x 2 9/16in. x 1 1/8in.

**3 TRANSISTOR**

**£9.17.6** Pair

**MODEL HA.70A.** Crystal controlled transmitter. Super sensitive regenerative circuit. Size 5 1/2in. x 2 1/2in. x 1 1/8in. Complete with carrying cases, batteries and telescopic aerials. S.A.E. for descriptive leaflet.

## LAFAYETTE DE-LUXE COMMUNICATION RECEIVERS



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## GARRARD RECORD PLAYER BARGAINS

GARRARD AUTOSLIM Ste. eo/Mono EV26 cartridge  
**5 GNS. CARR. 6/-**

BRAND NEW WITH MAKER'S GUARANTEE.  
**BUY NOW AT THESE UNREPEATABLE PRICES!**

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**9 GNS. CARR. 5/-**

SAVE £££'s AT GEES!!!

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**NEW!**



**MOBILE 7 in. RE-ENTRANT HORN.** 8 ohm, 10 watt. Brand new. Fully guar. 5 gns.

**RE-ENTRANT LOUD HAILERS (ex Govt.)** Heavy duty 20 watts, all metal, 15 ohms. Dia. 15in., length 15in. (approx.). Brand new and boxed £10. Carr. 10/-. Ditto reconditioned £6/10/-. Carr. 10/-.

### TRANSISTORISED "BULL HORN"

Ideal for Sports meetings, building sites, etc. Range up to 200ft. Simply press trigger switch and talk. Length 11 1/2in. Weight only 2 1/2lb. Complete with batteries and instructions. **£4.15/-**. P. & P. 2/6.

**10 inch P.M. HEAVY DUTY SPEAKERS.** Complete with line trans., in all steel blue-grey double grilled cabinet, **39/6**. Carr. 5/-.



**SUPER POWER LOUD HAILER MODEL 2583.** Hearing range 1,000ft. Lightweight self-contained portable, with detachable dynamic directional type microphone with cardioid polar diaphragm. Fully transistorised power amplifier. Long battery life. Ideal for all outdoor events. Brand new and guaranteed. **PRICE 22 GNS.**

## PUBLIC ADDRESS SYSTEM



Complete system comprising Control Unit, 4 Tannoy loud hailers, microphone and headphones, etc. 12 v. D.C. operation. Low battery drain. 8 watts power output. The ideal system for mobile use, outdoor meetings, sports days, factories, garden fetes, etc. Speakers can be spaced effectively over hundreds of yards. Guaranteed Brand New in sealed cartons. Price **£10/10/-**. Carriage 15/-. Speakers available separately **39/6**. P. & P. 5/-.

**12V. D.C. TRANSISTOR AMPLIFIER MODEL T.615** 15 watts max. output. Jack plug inputs for mike and gram. 15 ohm output. Complete in silver grey hammer finish case with carrying handle. Size 9in. x 6in. 4 1/2in. **PRICE £15.**  
**MATCHING MAINS POWER SUPPLY UNIT** available. 2 0'250 v. input. 12 v. D.C. output. **PRICE 6 gns.**

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230 v. A.C. input, 50/60 cycles, continuously variable 0-280 v., current. Fully shrouded. 9 amp. £15, 5 amp. £8, 2 1/2 amp. £5/17/6.

**FIELD TELEPHONES.** Tele "F" mint condition. Complete with batteries ready to use. **£2/10/-**. P. & P. 4/-.

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5in. Std.	600ft.	8/6
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8 1/2in. Std.	1,750ft.	23/6
10in. Std.	2,400ft.	32/6
5in. L.P.	900ft.	10/-
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7in. L.P.	1,800ft.	15/-
4in. D.P.	600ft.	9/-
5in. D.P.	1,200ft.	15/-
5 1/2in. D.P.	1,800ft.	22/6
7in. D.P.	2,400ft.	25/-

TENSILISED TRIPLE PLAY	
3in.	600ft. 15/-
4in.	900ft. 17/6
5in.	1,800ft. 35/-
5 1/2in.	2,400ft. 45/-
7in.	3,600ft. 58/6

**SPARE SPOOLS**  
3in. 1/-; 3 1/2in. 1/6; 4in. 1/8; 5in. 2/-; 5 1/2in. 2/-; 7in. 2/6; 8 1/2in. 4/6; 10in. 11/-.

P. & P. 2/6 per order.  
**SPECIAL DISCOUNT FOR TAPE QUANTITIES.** Send S.A.E. for Tape List.

**B.S.R. 4 track TAPE DECKS** 5 1/2in. spools, 3 1/2 i.p.s. Brand new. Guaranteed. **£7/10/-**.

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BM3 Crystal Stick, 39/6. P. & P. 2/-.  
PA.46 Dual Imp. Dynamic 84/- P. & P. 2/6.  
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Telescopic Floor Stand, 55/- Carr. 5/-.  
Send S.A.E. for Microphone list.

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100,000 o.p.v. Model 370-N. Price **£14/14/-**.  
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4,000 o.p.v. Model H20. Price **79/6**.  
All complete with test leads, battery, instructions and fully guaranteed.

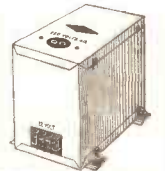
**EVERSHED & VIGNOLES.** Wee Megger 100 v., with leather carrying case, good working order, **£6/6/-**.

**EVERSHED & VIGNOLES.** Series II, 500 v. Megger in good cond. **£18/18/-**, **EVERSHED & VIGNOLES MEGGER CIRCUIT TESTER** (low reading ohm meter). 2 ranges 0-500, 100-5,000 ohms. Complete with leather case and test leads. As new **£6/6/-**.

**E. & V. BRIDGE MEGGER** 500 v., with leather case. Perfect working order, **£40**.

### NEW! DC/AC CONVERTOR.

12 v. D.C. in 230 v. 50 c/s. out. (45 watts max.) Ideal for Radio, Tape Recorders, Razors. Use in Car, Caravan or Boat. By well-known maker. Size 8in. x 4in. x 5in. Brand new. List price 104 gns. **GEE'S PRICE 45/-**. P. & P. 5/-.



### G.P.O. DESK TELEPHONES.

Black, complete with bell, handset, standard auto dial. Guaranteed sound, ex-office equipment. Bargain price **35/-**. P. & P. 5/-.



### AUTO TRANSFORMERS

Step up, step down, 110/115, 220/230 v. Fully shrouded terminal block connectors.  
150 w. 32/6 500 w. 67/6 1,250 w. 117/6  
200 w. 37/6 750 w. 77/6 1,500 w. 139/6  
300 w. 47/6 1,000 w. 90/- 1,750 w. 175/-  
Carriage 5/- on each type.

### G.P.O. STANDARD 19in. HEAVY DUTY EQUIPMENT RACKS

5ft. 6in. Angle Uprights, **£5/10/-**. Carr. 20/-  
6ft. Channel Uprights, **£7/10/-**. Carr. 20/-  
7ft. Channel Uprights, **£8**. Carr. 25/-  
All with Heavy Duty Base.

**6-IN. ALARM BELL, G.E.C. L.7502.** 3-6 v. D.C. Heavy duty all metal. **29/6**. Carr. 5/6.

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(ELECTRONICS LTD)

LONDON'S LARGEST SUPPLIERS OF  
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HOURS 9.30-6  
OPEN ALL DAY  
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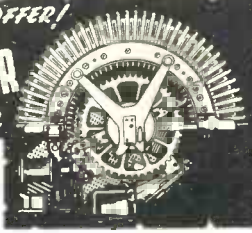
## HEAVY DUTY L.T. TRANSFORMERS ALWAYS IN STOCK ALL PRIMARIES 220-240 volts. TERMINAL BLOCK CONNECTIONS

\*Denotes Shrouded Types.

No.	Sec. Taps	Amps.	Price	Carr.
1.	25.30.35V.	40	£11 19 6	15/-
2.	25.30.35V.	20	£7 5 0	9/6
3.	25.30.35V.*	10	£4 19 6	6/6
4.	25.30.35V.*	2	£2 2 6	4/-
5.	10.17.18V.*	10	£3 2 6	4/6
6.	24V.	30	£8 10 0	9/6
6a.	24V.*	30	£9 10 0	9/6
7.	20V.	30	£6 15 0	8/6
8.	50V.	15	£7 5 0	8/6
9.	30.40.50V.*	5	£4 15 0	6/6
10.	24.36.48V.*	8	£5 5 0	6/6
11.	17.18.20V.*	20	£5 2 6	6/6
12.	6.12V.	20	£3 12 6	6/6
12a.	6.12V.*	20	£3 19 6	6/6
13.	20V.	20	£4 17 6	8/6
14.	30.32.34.36V.*	5	£2 19 6	6/-
15.	6.12V.	10	£2 5 0	5/-
15a.	6.12V.*	10	£2 12 6	6/6
16.	12V.	5	£1 12 6	4/6
16a.	12V.*	5	£1 17 6	4/6
17.	24V.*	10	£3 9 6	5/6
18.	24V.*	5	£2 5 0	4/6
19.	48.56.60V.*	1	£1 12 6	4/6
20.	12.24.36.48V.*	2	£2 5 0	4/6
21.	6.2V.*	15	£1 19 6	4/6
22.	6.3V. 5A. & 6.3V. 1A	—	15 0 0	4/6
23.	12.24V.*	1	17 6 3/6	3/6
24.	9.15V.	2	17 6 3/6	3/6
25.	6.9.15V.	4	£1 5 0	4/6
26.	12.18V.	10	£2 17 6	5/6
26a.	12.18V.*	10	£3 2 6	5/6
27.	12.18V.	20	£4 2 6	6/6
27a.	12.18V.*	20	£4 10 0	6/6
28.	48.56.60V.*	2	£2 9 6	5/6
29.	12V.	50	£6 10 0	8/6
30.	12.24.36.48V.	15	£7 5 0	9/6

## UNREPEATABLE OFFER!

### Motorised UNI-SELECTOR No. 2



8 banks 50 positions.  
Arranged to give 4 banks  
100 positions. Ex-equipment,  
in perfect  
condition.

These Selector Switches have been carefully removed from a modern PBAX (installed new in 1960). **£3/19/6** P.P. 4/6

**ALSO MODERN G.P.O. UNISELECTOR SWITCHES.**  
Alternate wiping type. 10 banks 25 positions. Two bridging; eight non-bridging wipers. 75Ω. £2/15/- P.P. 4/-.

**SIEMENS MINIATURE SELECTOR SWITCHES**  
Latest plug-in type. No. 2200C. 50Ω. 10-way, 3 bank, 3 wiper. Size 3½ x 2½ x 1½in. Complete with base. Fraction of maker's price, 69/6. P.P. 2/6.

**BRAND NEW G.P.O. 3000 TYPE RELAYS**  
2,0JΩ 5 c/o; 1,0JΩ 6 c/o; 500Ω 6 c/o; 300Ω 6 c/o.  
All at 12/6 each. P.P. 1/-; 500Ω 6 c/o, 8 lugged, 15/- P.P. 1/-; 600 Type 500Ω 4 c/o., 7/6. P.P. 1/-.

**MAGNETIC DEVICES MINIATURE RELAYS**  
Sealed type, 2,000Ω 2 c/o contacts. Size 1 x ½ x ¼in. Brand new. 10/6. P.P. 1/-.

**STC SILICON POWER RECTIFIERS RS300 SERIES**  
All type 3-amps. Wire ended. Max. P.I.V. 100 v. 5/-, 200 v. 6/-, 300V. 7/-, 400 v. 8/-, 500 v. 9/-, 600 v. 10/-, 700 v. 11/-, 800 v. 12/-, Post free. Not seconds or surplus. New and guaranteed.

**SELENIUM F.W. HIGH CURRENT BRIDGE RECTIFIERS.** Supplied brand new and guaranteed. Not to be confused with Government Surplus. All materials used are the latest design and highest grade.

**PLATE SIZE 7½in. SQUARE**

No.	Price	Carr.
No. 1.	36V. D.C., 36 amps.	£11 15 0 7/6
No. 2.	36V. D.C., 18 "	£5 17 6 7/6
No. 3.	24V. D.C., 54 "	£11 15 0 7/6
No. 4.	24V. D.C., 36 "	£5 19 6 7/6
No. 5.	24V. D.C., 18 "	£3 19 6 7/6
No. 6.	12V. D.C., 54 "	£5 17 6 7/6
No. 7.	12V. D.C., 36 "	£3 19 6 7/6
No. 8.	12V. D.C., 18 "	£1 19 6 3/6
No. 9.	12V. D.C., 12 "	£1 12 6 3/6

**PLATE SIZE 4½in. SQUARE**

No.	Price	Carr.
No. 10.	36V. D.C., 8 amps.	£2 19 6 3/6
No. 11.	24V. D.C., 8 "	£1 19 6 3/6
No. 12.	12V. D.C., 8 "	19 6 2/6

**BRAND NEW 30 AMP VANNER TIME SWITCH TYPE MD 1 BP.**

Size 5½ x 8 x 4½in. deep. 24 hr. dial. One on, one off. Beautifully finished in black bakelite case with perspex window. Packed in original cartons at fraction of maker's price. £3/19/6. P.P. 5/-.

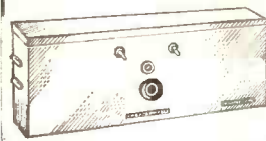
Arms for extra switch 6/- per pair

**£3-19-6**

**HEAVY CURRENT TRANSFORMERS LIMITED NUMBER ONLY**

Pri. 230 v. Sec. T 4-6-11 v. 200 a. £10/19/6. Carr. 10/-  
Pri. T 200-260 v. and 100-130 v. Sec. T 2, 28, 29, 30, 31 v. 25 a. conservatively rated £6/15/-, Carr. 10/-.  
Pri. T 210-250 v. and 105-115 v. Sec. T 27 v. 60 a. Totally enclosed new in maker's cases, £12/10/-, Carr. 10/-.  
Pri. T 210-240 v. Sec. T 17, 18, 30, 32 v. 8 a. £4/2/6. Carr. 7/6.  
Pri. T 210-225, 240 v. Sec. T 12, 18, 20, 24, 30, 36 v. 10 a. £5/5/-, Carr. 7/6.  
Pri. T 220-220, 240 v. Sec. T 50, 70, 73 v. 15 a. £6/19/6. Carr. 10/-.  
Pri. 200, 220, 240 v. Sec. T 100, 150, 155 v. 22 a. £9/19/6. Carr. 10/-.  
Pri. 240 v. Sec. T 53.5, 55.2 v. 6 a. C core £3/17/6. Carr. 6/-.

## L.T. SUPPLY UNIT TYPE S.E.1



A.C. input 200-240 v. D.C. Output tapped to give 12 or 24 volts 8 amps. continuous rating. Fitted with panel fuse. Mains on/off switch and D.C. output socket. Built in strong metal case. Size 15 x 6 x 6in. An ideal general purpose L.T. supply unit for operating relays. Contactors, battery charging, etc. £9/19/6, Carr. 7/6.

**L.T. SUPPLY UNIT TYPE S.E.2**  
A.C. input 200-240 v. D.C. output 50 volts 5 amps. Built-in metal case size 15 x 6 x 6in. Fitted with on/off switch, panel fuse, and output socket, £9/19/6, Carr. 7/6.

## BLOCK CAPACITORS

New and Guaranteed. Send for List, over 2,000 in stock.

**LATEST ARRIVALS**

Maker	Mfd.	D.C.V.	wkg.	Temp.	Price	Carr.
TCC	10	750	60°C	10/6	2/6	
TCC	10	350	60°C	6/6	2/-	
TCC	8	1,500	60°C	17/6	3/-	
TCC	8	1,000	60°C	10/6	2/6	
TCC	8	750	60°C	8/6	2/-	
TCC	8	600	60°C	7/6	2/-	
TCC	8	400	71°C	6/6	2/-	
TCC	2	2,000	60°C	12/6	2/-	
Dubilier	8	600	60°C	7/6	2/-	
Dubilier	4	800	71°C	5/6	2/-	
Dubilier	1	3,000	100°C	17/6	2/-	
Dubilier	0.5	5,000	60°C	17/6	2/-	
Dubilier 0.1+0.1	6,000	71°C	8/6	2/-		

**TELE "F" FIELD TELEPHONES**  
Generator bell ringing. Operates over a distance of several miles. Perfect condition. £3/19/6 per pair. Batteries 3/- ex. Carr. 7/6.

**SINGLE "D3" FIELD TELE CABLE**  
¼ mile drums. Unused. 45/-, Carr. 5/-.

**T.C.C. ELECTROLYTICS**  
Type CF 3240E 100 mfd. 50 v. wkg. Brand new. 15/- per dozen. P.P. 2/-, Special price for larger quantities.

**BRAND NEW D.C.M.C. INSTRUMENTS**  
2½in. round flush mounting, E. Turner. 0-50 microamps 50/-; 0-200 microamps 30/-; 0-50 milliamps 19/6; 0-10 v. 15/-; 0-20 v. 15/-; 0-200 v. 19/6. American Westinghouse 2½in. 0-150 milliamps 19/6; 0-100 milliamps 99/6; rectangular 4½ x 4½in. 0-50 microamps 99/6; 2½in. square, 0-50 microamp 49/6; 0-100 microamp 39/6; 0-500 microamp 27/6; 0-1 MA 25/-, Please add 2/- P.P. on all meters.

**HEAVY DUTY SLIDER RESISTORS**  
Zenith Double Tube Ganged Drive Log Wound. 1.3Ω 15 amps. Continuing to 55Ω 2 amps. Overall size: 22 x 9½ x 7½in. £3/19/6. Carr. 7/6.  
4Ω 8 amps. Single Tube. Enclosed, 32/6. P.P. 4/-  
300Ω 1.25 amps. S. Tube Gear Drive, 25/-, P.P. 3/-  
1Ω 12 amps. 17/6, P.P. 2/6. Ganged Twin Rheostats. 6in. dia. 200Ω 1.2 amps. each. Complete with Fixing Frame and Control Knob, 75/-, Carr. 5/- Many other types available. Let us know your requirements.

**G.P.O. HIGH SPEED COUNTERS**  
Latest Design Type 1000 4.1Ω 316 v. D.C. Type 100 a. 500Ω 18.24 v. D.C. either type 15/-, P.P. 1/6.

**A.C. ELECTRIC CHECK METERS**  
220-240 v. 40 amps. by Sangamo Weston Ltd. in perfect condition, 35/-, P.P. 4/-, Chamberlain & Hookham Ltd. 25 amp. 27/6. P.P. 4/-.

**MULTI TAPPED L.T. TRANSFORMERS**  
All Primaries 220-240 v.

Sec. Taps	Amps.	Price	Carr.
6, 9, 10, 12, 15, 20, 24, 30 v.	2	25/-	4/-
30 v. Ditto	4	39/6	4/6
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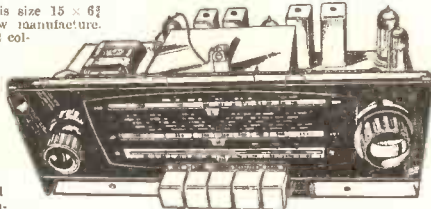
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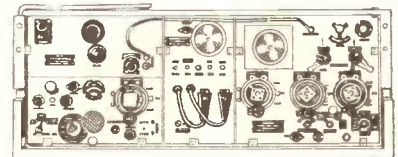
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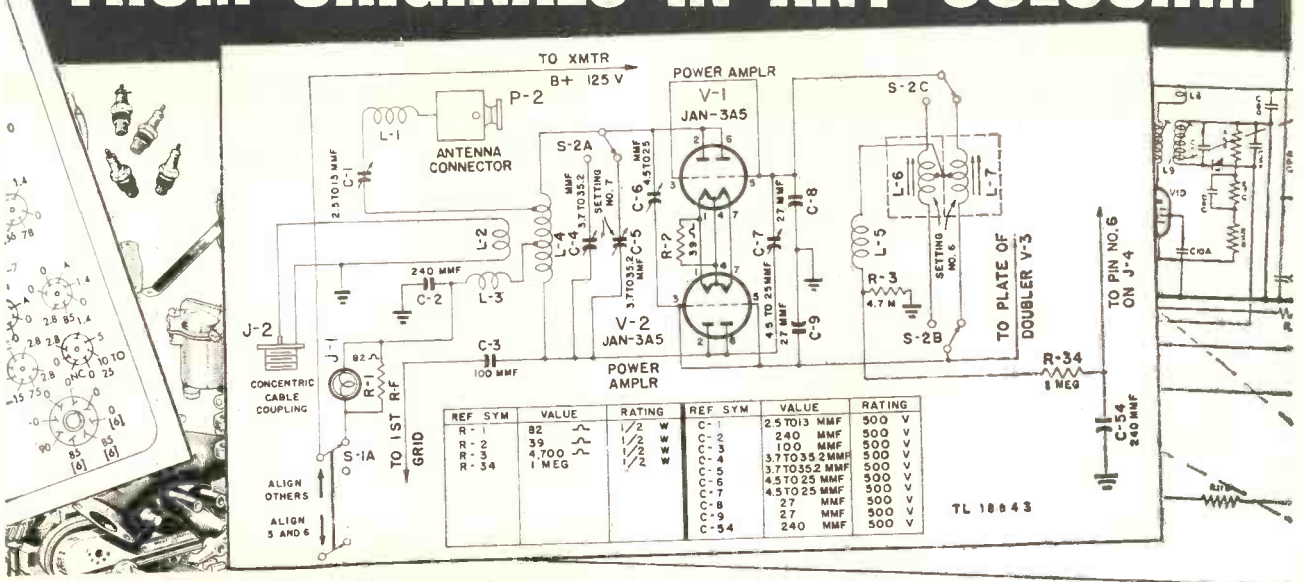
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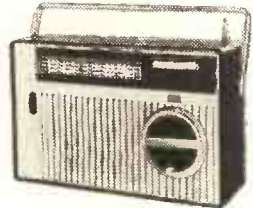
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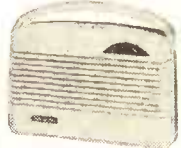
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5in. Double play, 1,200ft. Mylar base	15/-
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5in. Standard play, 600ft. P.V.C. base	8/6
5in. Triple play, 1,800ft. Mylar base	35/-
5in. Double play, 1,800ft. Mylar base	22/6
5 1/2in. Long play, 1,200ft. Acetate base	12/6
5 1/2in. Standard play, 600ft. P.V.C. base	11/6
5 1/2in. Triple play, 2,400ft. Mylar base	45/-
7in. Standard play, 1,200ft. Acetate base	10/-
7in. Standard play, 1,200ft. Mylar base	12/6
7in. Long play, 1,800ft. Mylar base	19/6
7in. Double play, 2,400ft. Mylar base	25/-
7in. Long play, 1,800ft. Acetate base	15/-
7in. Triple play, 3,600ft. Mylar base	58/6

Post 1/- extra per reel; 4 reels and over Post Free.

### TELEPHONE AMPLIFIER

Powerfully amplifies the incoming call. Fully transistorised. Pick-up suction fixed to phone. Battery-operated. Fitted with on/off switch and vol. control. Size 4 1/2 x 3 x 1 1/4in. Complete with PP3 battery. **LASKY'S PRICE 69/6** Post 2/6.

### U.H.F. TUNERS

Limited quantity only. Complete with P.C.88 and P.C.86 valves. Fully variable tuning capacitor etc. British manufacture. New and unused. Size 4 1/2in. x 5 1/2in. x 1 1/4in. We regret no circuit or data available. Knobs included.

**LASKY'S PRICE 79/6** Post 2/6.



### EXPORT MODEL TV OFFER

625 line T.V. chassis (Export Model). For 200-250 v. A.C./D.C. mains. Fitted with Band 1-III turret tuner. Fully loaded with 12 sets of coils for all CCR channels in these band P/M sound. Made by famous British manufacturer. 15 Mullard valves. Electrostatic focus and deflection. Will take 17in., 19in., 21in. or 23in. CRT. All controls fitted. Supplied new and unused with all valves. 7in. x 4in. speaker and 17in. CRT (less cabinet).

**LASKY'S PRICE £25** Carr. & packing FREE to any part of the World. (Tube sent at buyer's risk.) An allowance of £3 will be made if the CRT is not required. Circuit data included FREE.

### CRYSTAL PICK-UP CARTRIDGES

LOWEST PRICES EVER!

All Complete with Stylus L.P. and Standard. Fully guaranteed. Standard Fitting will fit most P.U. Arms and Heads. Postage 1/- extra each.

Acos G.P.59	14/-
Acos G.P.55/3	15/-
Acos G.P.65/1	17/-
Acos G.P.67/1	14/-
STEREO Acostereo 73/1, with 2 sapphires	25/-
Acostereo 73/2, with diamond LP/Stereo and sapphire	29/6
Ronette Stereo O.V. Turnover with 2 sapphires	25/-
Ronette Stereo type 105 and 106 with 2 sapphires	25/-
Ronette Stereo type 105 and 106 with diamond LP/Stereo and sapphire Std.	35/-

### AND EVEN LOWER PRICES

Save money! Some of these cartridges are cheaper than stylus C.T.1 Mono, 2 sapphires 4/11  
Collaro Type C, 2 sapphires, stereo 15/-  
Collor 801 Diamond LP, stereo 17/6  
Sonotone ST, stereo 19/10  
Sonotone 2TA, mono 15/-  
Postage 1/- extra each.

### TAPE POSITION INDICATOR

Open type—as used by most makers. With reset knob 3 DIGIT 7/6. 4 DIGIT 10/6. Post 3d. on each

## COMMUNICATION RECEIVERS



### MODEL KT 320 KIT

Supplied in sub-assemblies for easy building. Covers range from 540 Kcs to 30 Mc/s. Ham Band is provided with a scale for direct reading and can also be band spread. 9 valves. Facilities: A.N.L., A.V.C. and M.V.C. Q Multiplier also serves as B.F.O. H.F. stage and two I.F. stages ensure high sensitivity and selectivity (all coils and I.F.s are supplied pre-assembled). 2 Aerial Sockets. Stand-by position for use with a transmitter 8 meter fitted. 500-250 v. A.C. mains. Steel cabinet, grey crackle finish. Size 15 x 8 x 10in. Dial 12 x 4in. All parts new and fully guaranteed. Complete with full construction data and operating manual.

**LASKY'S PRICE 25 GNS.** POST FREE

Also available ready built and tested 33 gns. H.P. Terms Available.

### MODEL HE40

Covers medium wave band and 1.6-4.4 Mc/s., 4.5-11.0 Mc/s. 11.0-30.0 Mc/s. in switched band spread ranges. Controls B.F.O. Sensitivity, A.N.L. Receiver—Stand-by Switch, Tone Switch, 3 Meter. For 200/250 v. A.C. 4 valves and metal rectifier. Size 13 1/2 x 8 1/4 x 5 1/2in. Full instruction manual. No Kits available.

**LASKY'S PRICE 19 GNS.**

H.P. Terms £4 dep. and 11 months at £112/- Total H.P.P. £21/12/- Carr. & Pack. 10/-

### MODEL HE80

11-valves. Freq. range 540 Kcs.—30 Mc/s. and 144-146 Mc/s. Dual conversion on 2 metres, with extra R.F. stage. B.F.O. and Q-multiplier circuits. Improved A.N.L. and voltage regulated powerpack. "8" meter. Steel case 17 x 7 1/4 x 10in. For 200/250 v. A.C. mains. Brand new with full instruction manual. No kits available.

**LASKY'S PRICE 59 GNS.**

H.P. Terms £12/19/- dep. and 11 mths. at £418/- Total H.P.P. £66/17/- Carr. & Pack. FREE

## SPECIAL INTEREST ITEMS!

### ROTOCONTACT MINIATURE CLOCK/TIME SWITCH



This is a Swiss made clock only 1 1/2" in diameter by 1" deep, incorporating a pair of contacts which will close at any time preselected by the user. Fully variable 12 hour delay. The clock has a normal 24 hour spring movement with standard dial. Used by famous British manufacturer in transistor radio-alarm. Dozens of uses with all transistorised low voltage equipment. New and perfect.

**LASKY'S PRICE 21/-** Post 1/6.

### SINCLAIR SUPER MINIATURES IN STOCK

**THE MICRO-6** Miniature radio, only 1 1/2 x 1 1/8 x 1 1/4in. CAN BE BUILT FOR 59/6

**THE SLIMLINE** 2-transistor pocket radio only 2 1/4 x 1 1/4 x 1 1/4in. CAN BE BUILT FOR 49/6

**THE NEW X20** 20 watts P.W.M. amplifier and pre-amplifier. KIT PRICE £7/19/6.

AVAILABLE READY BUILT & TESTED 49/19/6.

3 pots. for vol., bass and treble, 7/6 the 3 extra. Mains power pack, if required, 24/19/6.

**THE X10** 10 watt power amplifier with integrated pre-amp. KIT PRICE £5/19/6

AVAILABLE READY BUILT & TESTED, £6/19/6.

3 pots for vol., bass and treble, 7/6 the 3 extra. Mains power pack, if required, 54/-.

207 EDGWARE ROAD, W.2.  
ELECTRONICS (FLEET ST.) LTD. 152/3 FLEET STREET, E.C.4.  
33 TOTTENHAM COURT ROAD, W.1.

PLEASE ADDRESS ALL MAIL ORDERS TO OUR HEAD OFFICE:—207 EDGWARE ROAD, W.2.

LASKY'S FOR ALL TEST GEAR & TECHNICAL ADVICE

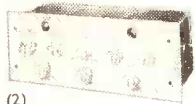
# STERN-CLYNE

Electronics Centres throughout Great Britain

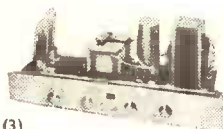
## HI-FIDELITY EQUIPMENT READY BUILT OR IN KITS OF PARTS



(1)



(2)



(3)



(5)



(6)



(8)



(9)

### (1) MULLARD "10 Plus 10" STEREO AMPLIFIER

A High Fidelity design providing up to 10 watts (per channel).  
**KIT OF PARTS £20.0.0.**  
**BUILT AND TESTED £24.0.0** (C. & I. 7/6).  
We can also supply the MAIN AMPLIFIER for operation with our DUAL CHANNEL PRE-AMPLIFIER.

**KIT OF PARTS £27.0.0**  
**BUILT AND TESTED £34.0.0** (C. & I. 10/6).

### (2) MULLARD DUAL CHANNEL PRE-AMPLIFIER

A four-valve design for both STEREO-PHONIC and MONOPHONIC operation.  
**KIT OF PARTS £12.10.0.**  
**BUILT AND TESTED £15.** (C. & I. 5/-).

### (3) THE "TWIN THREE" STEREO AMPLIFIER

Based on a recent design by MULLARD LTD. It is ideally suited for use in PORTABLE RECORD PLAYERS.

**BUILT AND TESTED £9.** (C. & I. 7/6).  
To construct a STEREO PORTABLE RECORD PLAYER we offer:  
Assembled AMPLIFIER with two 8x5in. LOUDSPEAKERS and PORTABLE CASE for £18.10.0. (C. & I. 10/-).

### (5) TUDOR AM/FM TUNER

Self powered VHF/FM long and Medium waves. FM 87.5-108.5 Mc/s. AM MW 522-1,630 Kc/s. L.W. 146-270 Kc/s. Multiplex output.  
**BUILT AND TESTED 24 Gns.** (C. & I. 7/6).

### (6) MULLARD 3-VALVE PRE-AMPLIFIER

Designed mainly for the STERN/MULLARD range of Monophonic Power Amplifiers.  
**KIT OF PARTS £10.**  
**BUILT AND TESTED £13.13.0.** (C. & I. 5/-).

### (8) MULLARD "5-10" MAIN AMPLIFIER

For use with MULLARD 2- or 3-valve pre-amplifiers with which an undistorted power output of up to 10 watts is obtained.  
**KIT OF PARTS £10.**  
**BUILT AND TESTED £13.10.0.** (C. & I. 6/6).

### (9) ABOVE INCORPORATING PARTRIDGE OUTPUT TRANSFORMER £1.6.0 extra

### (9) MULLARD "5-10RC" AMPLIFIER

The popular "5-10" complete incorporating Passive Control Unit providing up to 10 watts high quality reproduction with an input of 600 mV.

**KIT OF PARTS £12.**  
**BUILT AND TESTED £16.** (C. & I. 7/6).  
WITH PARTRIDGE OUTPUT TRANSFORMER £1.6.0 extra.

### (10) MULLARD "3-3RC"

A HIGH QUALITY AMPLIFIER DEVELOPED FROM THE VERY POPULAR 3-WATT MULLARD "3-3" DESIGN.  
**KIT OF PARTS £8.8.0.**  
**BUILT AND TESTED £11.10.0.** (C. & I. 6/6).

### (11) The "MONO-GRAM"

A small Amplifier of genuine high quality performance producing up to 3 watts undistorted output.  
**KIT OF PARTS £4.10.0**  
**BUILT AND TESTED £6.** (C. & I. 3/6).

### (12) STEREO TAPE PRE-AMPLIFIER Model STP-1

For use with current TRIVOX, BRUNELL or COLLARO "STUDIO" 1- and 2-track Stereo Decks.  
**KIT OF PARTS £22.**  
**BUILT AND TESTED £28.** (C. & I. 8/6).

### (13) MULLARD TYPE "C" TAPE PRE-AMPLIFIER

Suitable for most 1-track Mono Tape Decks.  
**KIT OF PARTS £14.**  
**BUILT AND TESTED £19.10.0** (C. & I. 7/6).

### (14) MULLARD TAPE AMPLIFIER Model HF/TR3

Based on Mullard's type "A" design and suitable for most 1-track Mono Tape Decks.  
**KIT OF PARTS £13.13.0.**  
**BUILT AND TESTED £19.** (C. & I. 7/6).

### (16) J110 POWER AMPLIFIER

Incorporates the latest diode/pentode ECC86 valves in push-pull, PARTRIDGE ultra linear output transformer, PARTRIDGE mains transformer, and smoothing choke. 10 watt output, surplus power output, surplus power available for tuner.  
**BUILT AND TESTED £12.12.0.** (C. & I. 7/6).

### (17) DOUBLE FEATURE PRE-AMPLIFIER

Inputs for microphone, crystal or magnetic pick-up, tuner unit, and in addition offers full facilities for tape recording and high fidelity replay. This unique feature means that should you wish to include tape in your hi-fi system at a later date all that is required is a suitable tape deck. Push-button switching for 3 tape speeds available.  
**BUILT AND TESTED £18.18.0.** (C. & I. 5/-).  
Prices if items 16 & 17 purchased together:  
**BUILT AND TESTED £30.9.0.** (C. & I. 10/-).



(10)



(11)



(12)



(13)



(14)



(16)



(17)

Fully descriptive leaflets available on any of the above items. **INSTRUCTION BOOKS AND DETAILED PRICE LISTS** are Supplied Free with Kits of Parts but may be purchased separately if required.

Items 1, 2 and 14, 3/- each; 6 and 13, 3/6 each; 7, 8, 9, 10, 2/- each; 11 2/6 each; 12, 5/-. All Post Free.

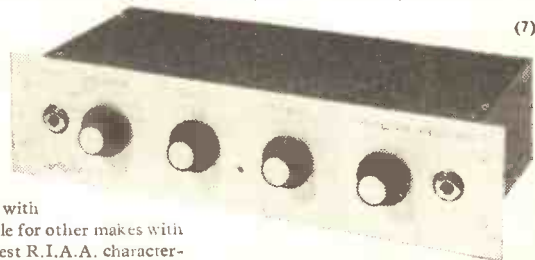
### COMBINED PRICE REDUCTION

Mullard 5-10 Main Amplifier and 2-valve Pre-amplifier.  
**KIT £15.15.0.**  
**BUILT AND TESTED £21.10.0.** (C. & I. 8/6).

Mullard 5-10 Main Amplifier and 3-valve Pre-amplifier.  
**KIT £19.10.0.**  
**BUILT AND TESTED £25.10.0.** (C. & I. 8/6).

(Above items with PARTRIDGE Transformer £1/6/- extra).

## MULLARD 2-VALVE PRE-AMPLIFIER



(7)

Employing two EF86 valves and designed to operate with the Mullard AMPLIFIERS but also perfectly suitable for other makes with input up to 250 mV. ★ Equalisation for the latest R.I.A.A. characteristics. ★ Inputs for Crystal Pickups and variable reluctance magnetic types. ★ Input (a) Direct from High imp. Tape Head. (b) From a Tape Amplifier or Pre-Amplifier. ★ Sensitive Microphone Channel. ★ Wide range BASS and TREBLE Controls. Now with brushed aluminium front panel with contrasting lettering and control knobs.

**KIT OF PARTS £6.6.0** BUILT AND TESTED **£9.10.0** (Carr. & Ins. 5/-).

**MAKE AN IDEAL COMBINATION WITH THE 2-VALVE PRE-AMPLIFIER AND OUR "5-10" MAIN AMPLIFIER**

**LEADING AGENTS FOR ALL B & O and SABA EQUIPMENT also SONY Tape Recorders**



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Electronics Centres throughout Great Britain

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We supply a complete range of Goodmans, Wharfedale, Stentorian, TSL Speaker Units and complete systems. A comprehensive leaflet is available on request, this covers specifications and prices of nearly 50 types including:—

- Celestion Model CX2012 (as illustrated) ..... £16 10 0
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  - Wharfedale W12EG 15 watts ..... £10 10 0
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## TAPE EQUIPMENT AND ACCESSORIES

### AMERICAN RECORDING TAPE

- 5in. 600ft. Std. Acetate ..... 8/6
  - 5in. 900ft. L.P. Acetate ..... 10/-
  - 5½in. 1,200ft. L.P. Acetate ..... 12/6
  - 3½in. 600ft. D.P. Polyester ..... 11/6
  - 7in. 1,200ft. Std. Polyester ..... 12/6
  - 5in. 1,200ft. D.P. Polyester ..... 15/-
  - 7in. 1,800ft. L.P. Polyester ..... 20/-
  - 5½in. 1,800ft. D.P. Polyester ..... 22/6
  - 7in. 2,400ft. D.P. Polyester ..... 25/-
- P. & P. 1/- per Reel extra, 4 or more Reels **POST FREE**.
- Fully Automatic Tape Splicer 14/6. P. & P. 1/6.
- Plastic Tape Spools 2½in. 1/-; 3in. 1/3; 4in. 2/-; 5in. 2/-; 5½in. 2/3; 7in. 2/6.
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- Any single item plus 6d. P. & P. Orders over £1 **POST FREE**.

## THE "TRAVLER" Mk. II CAR RADIO

- ★ MEDIUM AND LONG WAVES
- ★ 12 VOLT POSITIVE EARTH
- ★ PUSH BUTTON WAVE CHANGE
- ★ SIZE 7in. x 2in. x 7in.
- ★ TRANSISTORISED



ONLY  
**9 1/2 GNS.**  
P. & P. 5/-.

Ready built complete with 7 x 4in. speaker fitted to baffle, fixing brackets, filter unit all nuts and bolts and fitting instructions. Optional extras: Chromium plated weatherproof telescopic aerials. Type 1, 22in./50in. 19/6. Type 2, 2in./43in. 29/6. Type 3, 1in./50in. fully retractable and locking. Depth below wing 14in. 39/6, plus P. & P. 2/6 if purchased separately.

## RECORD PLAYER BARGAINS

- B.S.R. UA.25 4 speed Autochanger with mono cartridge ..... **£5.19.6**
- B.S.R. UA.15 4 speed Autochanger with mono cartridge ..... **£9.19.6**



### SPECIAL GARRARD OFFERS

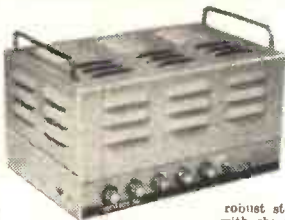
3000. 4 speed changer with Sono-tone stereo cartridge £9/19/6. LAB "A" GC8 Mono £15/15/- LAB "A" on plinth £17/17/-.

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- SRP.10 Single Player £5/9/11.
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- AT.60 with cartridge £14/1/1.
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Carriage and Insurance 5/- extra all models.

## PRESENTING THE NEW VERITONE 30 AMPLIFIER



A general purpose Amplifier of outstanding quality ideally suitable for Dance Bands, Clubs, Hotels, Factories, Indoor and Outdoor Public Address requiring a powerful, robust portable Amplifier which will provide high quality reproduction, distortion free. The Amplifier has two standard Jack Socket inputs, high gain and low gain with individual volume controls and with the master volume control the inputs may be mixed and balanced as required. The Amplifier is housed in a really robust steel case finished in smooth grey hammer finish with chrome handles and brushed aluminium front panel

with contrasting letters and knobs.

- ★ Built-in Pre-Amplifier and Control Unit
- ★ 30 watt Undistorted Output
- ★ Switched Output for 3 or 15 ohms Loudspeakers
- ★ Two Inputs, high gain and low gain with individual volume controls.
- ★ Bass and Treble Controls
- ★ Master Volume Control
- ★ Mixing Facilities

**PRICE 18 GNS.** Fully assembled and tested, carr. & ins. 10/-.  
Ventilated Cover with chrome handles as illus. 35/- ex.

## HE40 COMMUNICATION RECEIVERS

550 Kc/s-30 Mc/s. in 4 bands. **£19.19.0** Carr. 10/-.

H.P. Terms available.

Send S.A.E. for fully descriptive brochure.

## TUNER UNITS



### ARMSTRONG

- Mono Tuner Amp. 127M ..... £26 10 0
  - Stereo Tuner Amp. 127 ..... £37 10 0
  - AM/FM Tuner 223 .. £28 15 0
  - FM Tuner 224 ..... £22 10 0
- Carriage and Insurance 7/6.

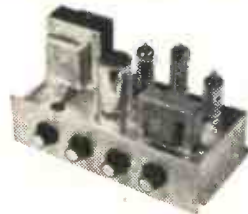
### JASON

- FMT1 FM Tuner. Kit of parts ..... £6 15 0
- FMT2 FM Tuner. Kit of Parts ..... £10 12 6
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- FMT4 Tuner ..... £20 0 4
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- Unpowered ..... £13 19 6
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- Carriage and Insurance 5/- each. Descriptive Leaflets free on request. Please state model required.

## VERITONE 300



A small versatile Gram Amplifier with an output of 3-4 watts suitable for Crystal Pickup or Radio Tuner, ideally suited for a small domestic installation on requiring good quality low output, output impedance 3 ohms, volume control, treble control, bass control and middle control. Valve line-up: EL84, EF86, EZ80. Smooth grey hammer finished chassis, size 8½ x 4 x 1½in. with brushed aluminium front panel, contrasting letters and knobs, front panel size 8½ x 2½in. Fully assembled **6 GNS.** carr. & ins. 5/-

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### "MEASUREMENTS CORPORATION" TYPE 84 "STANDARD" SIGNAL GENERATOR



Range: 300-1,000 Mc/s. Direct Calibration. Accuracy: 0.5%.

Output Level: 0.1 $\mu$ V-100 mV, continuously variable.

Infomodal Modulations—

Sine-wave—30% Max. at 400, 1,000 and 2,500 c/s.

Pulse—1 to 50 $\mu$ sec., width delay variable from 0 to 50 $\mu$ sec., p.r.f. 00 to 10,000 c/s.

Output Impedance—60 ohms.

Percentage Modulation Meter.

PRICE, in as new condition, tested before despatch and fully guaranteed. £220 0 0

Packing and carriage, 22.

### MARCONI FT934 DEVIATION TEST SET



Unbalanced "pi" type 100K $\Omega$ . Attenuator switches consisting of 21-step steel switch and wire wound resistances. Switch provides 5 time impedance steps of 4dB and intermediate 1dB steps, giving the overall range of 0 to 20dB at 1dB steps. Panel mounting, fully screened, 4in. spindle. Bored dimensions 2 3/4in. dia. x 3in. long. 10/- P.P. 2/-.

Emulsional frequency range 2.5-100 Mc/s. basic range can be extended to 500 Mc/s. by using harmonics. Deviation range, 0.5-0.25 and 0.75 kc/s. in the modulating range of 50 c/s. to 15 kc/s. Sensitivity better than 55 mV. Power supplies 100-150 and 200-250 V. A.C. Price, fully overhauled and guaranteed £25 0 0

### TRANSISTOR TESTER MODEL AT-1



For P-N-P and N-P-N Transistors.

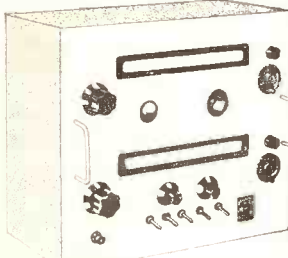
Measures I<sub>co</sub> and diode reverse current up to 50 $\mu$ A for low power transistors and up to 1 mA for power transistors. B from 2 to 500 at 1 mA. for low power and 5 mA. for power transistors. Powered by dry cells. £10/10/-, p.p. 5/6.

### UHF CRYSTAL CONTROLLED HETERODYNE FREQUENCY METERS

TS174 (T-74) 20-280 Mc/s. £140

TS175 (T-75) 80-1,000 Mc/s. £150

Mains Power Supply Unit £10/10/-



### VHF HETERODYNE PRECISION FREQUENCY METER TYPE 1B3

Total Frequency Coverage 20-1,000 Mc/s.

The instrument consists of: Crystal Controlled Oscillator (Crystal 100 kc/s  $\pm$  5 c/s.) providing spot frequencies at 25, 50 and 100 kc/s. intervals; Fine (L.F.) Oscillator continuously tuned from 5.0 to 6.25 Mc/s. in 9 bands; Coarse (H.F.) Oscillator continuously tuned from 20 to 300 Mc/s.; and associated mixer and A.F. stages. By using coarse oscillator alone quick frequency identification can be made from 20 to 1,000 Mc/s. with an accuracy of 3%. By using correct measuring procedure, i.e., by calibrating fine oscillator against crystal and beating input frequency with the former an accuracy of  $\pm$  0.2% is easily obtained. Long scales graduated in Mc/s. provide exceptional degree of discrimination. Beat detection by Magic Eye or headphones. Dimensions: 22in. x 19 1/2in. x 14in. Weight 7 1/2lb. Power requirements 115/230 v. A.C.

PRICE, new and fully guaranteed. £85 0 0

Packing and carriage £1/10/-.

### AVOMETER MODEL 7

Fully tested in perfect condition and guaranteed. £11 10 0

Set of leads £1 0 0

Packing and carriage 15/-.

### POCKET MULTIMETERS TYPE U-1

Sensitivity 1,000 $\Omega$ /V. D.C. and A.C. voltage ranges 0-10-50-200-500-1,000V. I.T.C. current ranges: 0-100-500 mA. Resistance ranges 2,000 $\Omega$ -200,000 $\Omega$ . Brand new. £22/2/- P.P. 7/6.

### VARIABLE AUTOTRANSFORMERS

230 v. A.C. input. Output adjustable from 0 to 250 v. Type O1 (Philips Skeleton Type).

i.e. without housing, 2 amps. £3 15 0 P.P. 7/6

Type B2, 2.5 A. max. £5 19 6 P.P. 7/6

Type RB5, 5 A. max. £9 0 0 P.P. 30/-

Type RB10, 10 A. max. £18 5 0 P.P. 12/6

Type RB20, 20 A. max. £32 10 0 P.P. 15/-

### POWER UNITS

TYPE 234. 19in. rack mounted fully smoothed and fused for 230 v. A.C. input. I.T. output adjustable from 380 v. to 270 v. at 80 mA. by means of primary taps and high-low switch in the secondary winding. I.T. output 0.3 v. A.C. at 4 amps. Fitted with M.I. meter to read A.C. input and D.C. output volts. Second-hand, tested, in good condition. £3 19 6

DITTO, model without meter £3 10 0

Packing and carriage 15/-.

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Unbalanced "pi" type 100K $\Omega$ . Attenuator switches consisting of 21-step steel switch and wire wound resistances. Switch provides 5 time impedance steps of 4dB and intermediate 1dB steps, giving the overall range of 0 to 20dB at 1dB steps. Panel mounting, fully screened, 4in. spindle. Bored dimensions 2 3/4in. dia. x 3in. long. 10/- P.P. 2/-.

### R.P.M. INDICATOR KIT

Radio-Altimeter Indicators with moving coil movement on 5 mA. F.S.D., easily convertible to accurate engine R.P.M. indicators. Supplied complete with parts required for conversion and detailed instructions. Suitable for 4-cylinder engines with 12 v. electrical installation. 35/- P. & P. 5/-.

### METERS

### PHILIPS FIRST-CLASS MIRROR SCALE 1 mA. D.C. M.C. METERS



Square flange 4.6in. x 4.6in. flush mounted. Scale length 4in. Body 3.8in. dia. x 1 1/4in. deep. Calibrated 0 to 1 mA. Price £65/-

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DLR5 BALANCED ARMATURE with sound powered inserts; D.C. resistance 40 $\Omega$  per insert. 10/- ea.

CHR. MOVING IRON, D.C. resistance 4,000 $\Omega$ . 15/- ea.

MOVING COIL, with moving coil microphone fitted with press-to-talk switch. D.C. resistance 10 $\Omega$  per insert. Large rubberised felt lined earcups. Very comfortable to wear. 15/- ea.

TANNOY MOVING COIL, similar to the above but fitted with heavy die-cast carbon microphone. 12/9 ea.

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Now available—3GP1 Cathode Ray Tubes as used in the P.E. oscilloscope £2/10/- P.P. 5/-.

### CATHODE RAY TUBES

VOR139A, 2 1/2in. green trace, medium persistence, 30/-

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1,500 V. E.H.T. (B12A)

4EP1, 4in. green trace, flat face, medium persistence 100/-

P.D.A.; Max. E.H.T. 4,000 V. (B12F)

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P.D.A.; max. E.H.T. 8,000 V. (B12F)

89J, 4in. double beam, blue trace, flat face, short persistence, 2,000 V. E.H.T. (special), 60/-

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5BP1, 6in. green trace, flat face, medium persistence, P.D.A.; max. E.H.T. 4,000 V. (B12D) 180/-

D113-2, 5in. green trace, medium persistence, P.D.A.; max. E.H.T. 4,000 V. (B14A) 120/-

D113-2, 5 1/2in. 1 1/2in. rectangular screen, green trace, medium persistence, E.H.T. 5,000 V. (B11A) 200/-

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APPLY to Personnel Manager:—ALBA (RADIO & TELEVISION), Ltd., Tabernacle St., London, E.C.2. [105]

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WRITTEN applications, please, to Personnel Officer, 40, Park St., W.1. [115]

### STATES OF GUERNSEY AIRPORT.

APPOINTMENT of a Radio Technician. APPLICATIONS are invited for the above appointment on the Established Staff of the States of Guernsey. Applicants must hold the City and Guilds Telecommunications Intermediate Certificate or equivalent technical qualifications and should have had previous experience in Radar and V.H.F. systems.

SALARY £735/£1,125 (£40, 4x£35, £40, £30, £40, £30, 2x£35). Commencing salary according to age and experience.

THE post is pensionable (non-contributory) and arrangements can be made for back years of service to count for pension purposes in accordance with the pensions rules.

CONTRIBUTORY Widows and Orphans Pensions Scheme (at present 3% of annual salary).

TEMPORARY housing accommodation can be provided at an economic rental and removal expenses paid.

FURTHER details of the duties and responsibilities attaching to the post may be obtained from the Airport Commandant, States Airport, Forest, Guernsey.

APPLICATIONS (stating age, qualifications, present and previous appointments, experience and the names of two referees) should be addressed to the President, Civil Service Board (W), States Office, P.O. Box No. 43, St. Peter Port, Guernsey, and must be submitted not later than 25th September, 1965. [1293]

### CIVILIAN INSTRUCTORS GRADE III:—

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WRITE for application form to C.E.P.O., Personnel Line, Caterick Camp, Yorkshire.

CLOSING date 10th September, 1965. [1284]

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WE have limited vacancies for more senior and experienced men with drive, who can lead small teams engaged on this work.

WE have also limited vacancies for persons of less experience who can be trained for such work.

APPLY to: The Personnel Manager. [131]

### A FULL-TIME technical experienced Salesman re-

quired for retail sales; write, giving details of age, previous experience, salary required, to—The Manager, Henry's Radio, Ltd., 303 Edgware Rd., London, W.2. [149]

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A vacancy exists for an additional Assistant Superintendent at Manchester. The applicants will be trained to take part in the planning and supervision of the work undertaken in both the Marine and Industrial Departments of the Service Division.

The applicant's background should be Electronic or Electrical Control in character, either in the Marine field with Radar, Radio, etc., or in Industrial Control, but ability to understand quickly the technicalities involved in unfamiliar equipment is very important.

There is a considerable amount of travelling involved about our depots and installations in progress. Applicants will be expected to have ability to organise efficiently and to deal with the considerable amount of technical problems arising in the daily routine of a Nation-wide Service Organisation; he should therefore have had many years of experience in Electrical and Electronic Maintenance and Repair work, during part of which he must have been in a supervisory capacity.

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Service Engineers required for Marine Radar, Radio and Gyro-compass and Echosounders. Applicants must have PMG and MOT Certificates and preferably reside in East London or Thames Estuary areas and Belfast. Vacancies also in other areas.

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Service Engineers required who have had experience of Electronic and Electrical Control of industrial machines and equipment. Work involves a wide range of equipment and applicants must therefore have a good technical theory background and be capable of quick assimilation of "know-how" and adaptability to provide quick and efficient service to industry. Vacancies especially in London, Manchester, Birmingham, Bristol and Belfast.

All applicants must be British born, hold a Driving Licence, be willing to travel, and should write to the address given below stating age, married or single, all qualifications and experience.

Ex-Naval C.P.O.s and P.O.s particularly welcome.

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The current vacancies for pensionable and temporary appointments include the following:—

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urgently required to fill vacancies in Ministries of Aviation, Defence, Public Building and Works, and Transport, the Diplomatic Wireless Service and Government Communications Headquarters. Vacancies in fields of (a) power, including building services, and (b) light currents and electronics.

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**SALARY (Inner London):** £1,143 (at 25)-£1,718. Promotion prospects.

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Details obtainable from Civil Service Commission.

Except where otherwise stated the above posts are pensionable.

APPLICATION FORMS are obtainable from

Secretary, Civil Service Commission, Savile Row, London, W.1.

Please quote appropriate reference.

**COMMUNICATIONS—ELECTRONIC SECURITY DEPARTMENT.** Eastcote, Ruimsip, Middx.  
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**SALARY:** S.O. £940-£1,586.  
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**OPPORTUNITIES** for permanent pensionable appointments.  
**APPLICATIONS** to: Communications-Electronic Security Department, 8, Palmer St., London, S.W.1. (15)

**ROYAL COLLEGE OF ADVANCED TECHNOLOGY,** [1287  
 Salford. Proposed University of Salford. Electronic Engineer.

**APPLICATIONS** are invited from electronic engineers for a post of Experimental Officer to join a group from the Civil and Electrical Engineering Departments developing an electronic analogue computer for use in the design and analysis of complex pipe networks. The successful applicant will be required to contribute to the current development programme, to commission and run the machine and to participate in future development work.

**APPLICANTS** should have a good working knowledge of both linear and pulse transistor circuitry, be capable of working under the minimum of supervision and be graduate members of the Institution of Electrical Engineers or hold an equivalent qualification.  
**THE salary scale** is £920-£1,340 (Bar)-£1,555 per annum.

**APPLICATIONS,** giving full details of education and experience, together with the names and addresses of two referees, should be sent to the Secretary, Royal College of Advanced Technology, Salford, S. by 20th September, 1965 quoting reference C/40. [1279

**SERVICE Technicians and Trainees** for Maintenance work on all kinds of audio equipment, required in the London area; pension scheme.—Apply: Mr. J. Vaughan, Dictograph Telephones, Ltd., Abbey House, Victoria St., London, S.W.1. Tel. Abb. 5572. [1274

**ELECTRONIC** service engineers required to service and install airborne navigational equipment at London Airport, Home Counties and overseas.—Apply: The Decca Navigator Co. Ltd., Spur Rd., Feltham, Middlesex. Tel. Feltham 4898. [1295

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**QUALIFICATIONS:** EITHER (i) G.C.E. (or equivalent) passes in English language and 3 other subjects, including 2 at A level obtained at the same examination for pure mathematics, applied mathematics, physics, chemistry; OR (ii) G.C.E. (or equivalent) pass in English language and either Higher National Diploma in electrical or mechanical engineering or applied physics, or a pass in (or exemption from) Parts 1, 2 and 3 of the Graduateship Examination of I.E.E. or I.Mech.E., or a pass in (or exemption from) Sections A and B of the I.E.R.E. Graduateship Examination under the September 1962 Syllabus and Regulations.

**SALARY (Inner London):** £740 (at 18), £1,085 (at 25 or over)—£1,575; (national) £675 (at 18), £1,010 (at 25 or over)—£1,500; salary under review; promotion prospects.  
**WRITE** to Civil Service Commission, Savile Row, London, W.1. for application form, quoting S/6202/65. Closing date 14th September, 1965. [1299

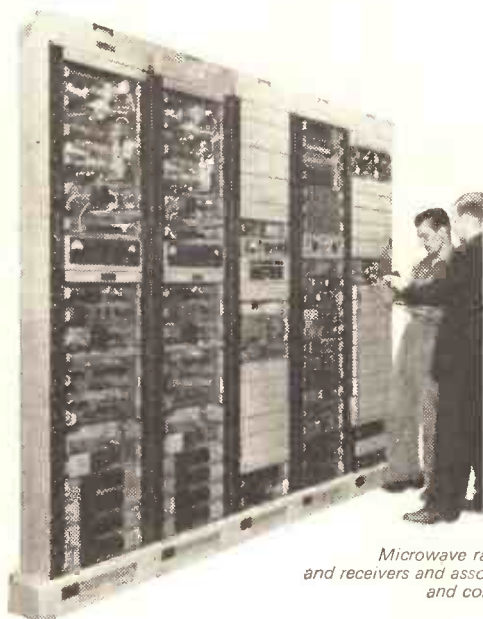
**AIRCRAFT** radio/radar engineers and mechanics with specific workshop experience in one of the following: X band radar. VHF/HP. ILS/VOR or ADF: 40-hour week pension scheme.—Apply: Managing Director, Air Transport (Charter) (C.I.), Ltd., Willow Rd., Colnbrook, Slough, Bucks. [1296

**TECHNICAL** representative required to sell American semiconductors in U.K.; previous selling experience not essential, but must have had at least five years in semiconductors; good conditions and salary to right man.—Write, giving brief details, to—Jermyn Industries, Vestry Estate, Vestry Rd., Sevenoaks, Kent. [1278

**RADIOLOGICAL PROTECTION SERVICE** (Ministry of Health and Medical Research Council), Clifton Avenue, Belmont, Sutton, Surrey, requires Technical Officer to design and construct electronic equipment used in the field of radiation measurements. Knowledge of digital circuits, pulse techniques and transistor circuitry is required. Qualifications—H.N.C. or equivalent, plus at least 7 years' appropriate experience. Salary scale £1,250-£1,813 p.a. plus London Allowance. Medical Research Council conditions of employment.

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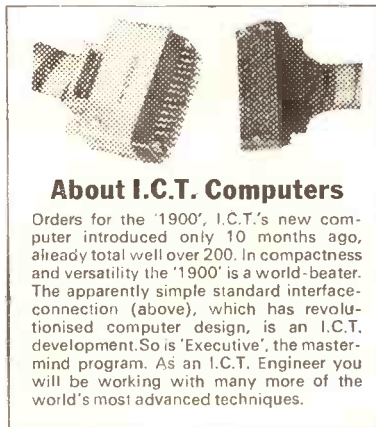
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**ELECTRONICS Senior Technician I** reqd. in the Pharmacology Department, Royal Free Hospital Medical School; experience in medical electronics an advantage; salary scale £965-£1,265, plus London Weighting; superannuation scheme, good hols.—Apply School Secretary, 8, Hunter St., London, W.C.1. [1294

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**SCIENTIFIC CIVIL SERVICE EXPERIMENTAL OFFICER CLASS, AUTUMN, 1965, RECRUITMENT.** CAREERS in science and technology are offered to men and women with qualifications in mathematics, physics, chemistry, biology, meteorology, engineering and geology as Assistant Experimental Officers and Experimental Officers, in Government Scientific Establishments.

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**SALARIES** supplemented in London area. Aid given for further education. Promotion prospects. Pensionable posts.

**APPLICATION** forms and booklet from: Civil Service Commission, Savile Row London, W.1. Please send postcard quoting S/579-580/65. Closing date 23rd September, 1965.

(FURTHER recruitment in Spring, 1966.) [1286

**TEST** engineers.—Applications are invited from test engineers with previous industrial experience of testing radio communications, receivers and transmitters; successful applicants will be offered positions on the company's permanent staff, starting salaries commensurate with qualifications and experience.—Apply in writing, giving full details, to Personnel Officer, Redifon, Ltd., Bromhill Rd., S.W.18. [124

**RADIO** and Radar technicians required for maintenance and development work at a flying unit near Barmouth, North Wales. Preference given to applicants with technical experience in H.M. forces. 5-day week. Free single accommodation. Canteen facilities, Sick benefit and superannuation schemes.—Apply Short Brothers and Harland Limited, R.A.E. Llanbedr, Merioneth. [1246

Senior Electronics Technician for Research Department in Anaesthetics. H.N.C. or equivalent required. Starting salary £1,210 with superannuation. The work is neurophysiology and sophisticated data processing techniques are used. Candidate should be interested in development of special purpose computers and advanced recording techniques. Apply to: Professor J. G. Robson, Postgraduate Medical School of London, Du Cane Road, London, W.12.



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## UNITED KINGDOM ATOMIC ENERGY AUTHORITY CHAPELCROSS WORKS

### INSTRUMENT MECHANICS

Chapelcross Works requires experienced men with knowledge of electronic equipment and/or industrial instrumentation for fault diagnosis, repair and calibration of a wide range of instruments used in nuclear reactors and radiation laboratories. This work involves maintenance of instruments using pulse techniques, wide band, low noise amplifiers, pulse amplifier analysers, counting circuits, television and industrial instruments used for measurement of pressure, temperature and flow.

Men with H.M. Services, industrial or commercial background of radar, radio, television or industrial or aircraft instruments are invited to write for further information.

**HOUSING is immediately available.**

For further details, write to:—

**Labour Manager,  
Chapelcross Works,  
ANNAN, Dumfriesshire.**

**London Borough of Richmond upon  
Thames**

**TWICKENHAM COLLEGE OF  
TECHNOLOGY, Egerton Road,  
Twickenham.**

**Principal: J. P. WOLFENDEN, M.Sc.,  
M.I.E.E.**

**Department of Electrical Engineering and  
Physics.**

**Special lecture courses commencing  
September 1965:**

**Fundamentals of Semi-conductor  
Devices**

**Basic Electronics**

**Transistor Circuit Design**

**Network Analysis and Synthesis  
Systems Analysis**

**W. R. WAINWRIGHT, B.A.  
Chief Education Officer**

**RADIO Technician** with a sound knowledge of at least three of the following types of equipment is required immediately for Meteorological Office Ocean Weather Ships: Single Side-band Transmitter, Radar (Navigational), Radar Height Finding, Echo Sounders and Radio Receivers, Automatic D.F., V.H.F. and M.F. Low-voltage Servo Recorders, Digital Telemetering Equipment.

**SALARY** scale £678-£1,104 per annum according to age, plus £120 per annum overtime allowance. Free food and accommodation provided on board ship. Applicants must be natural born British subjects.—Full details from Shore Captain, Ocean Weather Ship Base Great Harbour, Greenock. Telephone Greenock 24291. [1280]

**MEDICAL College of St. Bartholomew's Hospital, West Smithfield, E.C.1.**—Electronics technician required by Physics Department; the work is varied and includes development of a 15 MeV linear accelerator, and instrumentation for radiation dosimetry, E.S.R. spectroscopy, etc.; salary within the range £805 to £1,025 plus London Weighting.—Applications, in writing, to the Secretary of the Medical College. [1287]

**IMPERIAL COLLEGE, S.W.7.**—Electronics Development. We have an attractive position vacant in our Electronics Group; the work is concerned with application of the most modern electronics techniques to our Chemical Engineering and Technology Research. The person we shall appoint probably has an H.N.C., certainly has several years' practical workshop experience and is anxious to use his initiative. The starting salary will be over £1,000 for the right man.—Write in confidence to: Professor G. R. Hall, Department of Chemical Engineering and Chemical Technology, Imperial College, London, S.W.7. [1301]

## TESTERS

**required for interesting work on L.F.  
and H.F. Transmitters. Previous fault-  
finding experience essential.**

The positions available would be of special interest to persons employed in the fault-finding and repair of television who are keen to establish themselves in a position that offers:

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- ★ Five-day week
- ★ Good prospects of advancement
- ★ Staff status
- ★ Sick pay
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Apply: Personnel Manager

**Multitone Electric Co. Ltd.**

12-20 Underwood St., London, N.1

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No quantity too small. List on application.

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MANCHESTER, LEEDS, GLASGOW**

**WW—146 FOR FURTHER DETAILS.**

**Inner London Education Authority  
NORWOOD TECHNICAL COLLEGE  
Knights Hill, London, S.E.27**

### TELECOMMUNICATION AND ELECTRONICS DEPARTMENT

Two Lecturers required in the Department of Telecommunication & Electronics which conducts full-time courses in telecommunication, electronics, marine radio operating and radar maintenance; part-time courses additionally include radio television and electronics servicing, television technology and other specialist subjects.

Lecturers are required to conduct classes in one or more of the branches of study referred to and would be responsible for certain administrative duties.

Qualifications and/or specialist knowledge or experience appropriate to the work of the department are looked for.

Salary in accordance with Burnham Technical scale, currently in the range £1670-£1895 plus London allowance of £45 or £60, but now being reviewed.

Application forms obtainable from Principal at College and returnable within 14 days of the appearance of advertisement. Enclose self-addressed foolscap envelope.

**DECCA RADAR LIMITED.**—Test equipment technicians are required for repair and manufacture of a wide range of test equipment for use in development and production. These are staff positions with opportunity for promotion and individual initiative.—Please apply Personnel Officer, Decca Radar Limited, 9, Davis Rd., Chessington, Surrey. [1302]

**MEDICAL Research Council.**—Technician (junior grade) in electronics required to design, build and maintain research apparatus, which includes timing equipment and display apparatus; salary is determined by age on Whitley Council Scale, e.g., age 23, salary £645 plus London Weighting.—Information available from Senior Technician.—Apply Dr. O'Connor, M.R.C. Unit, Maudsley Hospital, Denmark Hill, S.E.5. [1298]

**AIRCRAFT Radio Engineer** required holding preferably Maintenance Engineers' A and B Licences, though experienced "A" man would be considered. Work covers an interesting range of radio equipment, both for complete overhaul and defects rectification. Pay would be in accordance with qualifications and experience. Please call or write to Mr. R. C. Salisbury, Rogers Aviation Limited, Cranfield Airfield, Bedford. Tel. Cranfield 481. [1292]

**ELECTRONICS Technician.** Young man required as a technician in the Department of Pharmacology to assist with research experiments on the effects of drugs in animals. Essential qualifications are an interest in and a working knowledge of electronics. Salary (M.R.C. grant) of £800 p.a. for two years in the first instance.—Applications to: Mr. N. J. G. McLaren, Department of Pharmacology, School of Pharmacy, University of London, Brunswick Sq., London, W.C.1. [1275]



**VHF TEST  
ENGINEERS**

**CAMBRIDGE WORKS LIMITED**

have vacancies in their expanding Test Organisation for men with experience of VHF Transmitters and Receivers.

Men with Service training in VHF equipment would be suitable.

Progressive rates of pay and promotion and good facilities for training are offered.

Apply: **Personnel Manager,  
Cambridge Works Limited,  
Haig Road, Cambridge.**



# SERVICE AND COMMISSIONING ENGINEERS - Croydon Area

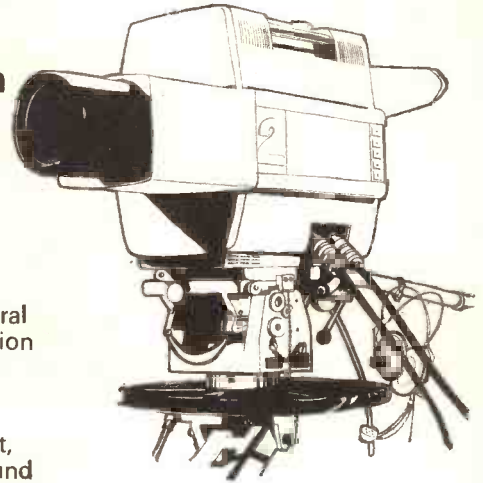
For an expanding Service Department, at Beddington Lane, Croydon, we seek the services of additional Engineers with a thorough knowledge of at least one of the following:

## Professional TV Equipment

for Studio and Industrial applications. A wide range of cameras, monitors, video recorders, together with peripheral equipment is involved. Some knowledge of colour television is desirable, but training in this field will be arranged.

## Sound Systems

Based on an extensive range of public address equipment, radio paging and inter-communication systems, background music services and professional tape recording devices.



Apply in confidence, to the Plant Personnel Officer

## PETO SCOTT ELECTRICAL INSTRUMENTS LIMITED

Addlestone Road, Weybridge, Surrey. Telephone: Weybridge 45511.



A member of the Philips Industries Group.

**E**LECTRONICS Technician required in physiological laboratory re-equipping with transistorised recording equipment. Work will consist of developing, building and servicing equipment. There are excellent opportunities for co-operative work with the Hospital Department of Physics. The person appointed will be expected to undertake some administrative responsibility in the Department. Applicants, aged 25-30, should hold an O.N.C. or equivalent qualification. Salary in the range £805 to £1,025 p.a. plus London Weighting of £45 or £55 p.a. with superannuation.—Apply, giving details of experience, to the Secretary, Guy's Hospital Medical School, London Bridge, S.E.1. [1282]

### ALIGNMENT ENGINEER

required for the alignment and test of V.H.F. and U.H.F. Radio Frequency Amplifiers. Some knowledge of this work essential but final specialised training will be given. Applications to The Personnel Manager, Belling & Lee Limited, Great Cambridge Road, Enfield, Middlesex.

**HEWLETT-PACKARD LIMITED**, Service Engineer (Electronic Instruments). A vacancy exists for a Service Engineer to work on a wide range of high quality electronic instruments. Candidates should have O.N.C., C. & G. or equivalent qualifications, or wide experience in a similar position. Good salary and prospects in a rapidly expanding organisation with an international reputation. Pension scheme and monthly staff position.—Apply in writing to: The Personnel Officer, Hewlett-Packard, Limited, Dallas Road, Bedford. [1289]

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with EASE, ACCURACY and SAFETY : 30  
with the **KILOVOLTER** : kV  
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WW-149 FOR FURTHER DETAILS.

## MINISTRY OF AVIATION

### Electrical Inspection Directorate, Bromley, Kent

**TECHNICIANS (Grade III)** age 24 or over, required mainly at Headquarters at Bromley and Woolwich, but a few vacancies also exist in other parts of the United Kingdom. The Headquarters posts include duties associated with the following types of work:—inspection and testing of electrical generating and control equipments, navigational aids and Army radar and communications equipments; testing (including environmental testing) of all types of electrical/electronic components; calibration of precision electrical measuring instruments; preparation of specifications and inspection instructions; documentation of Army telecommunications equipment involving investigation of interchangeability of components and maintenance of technical records.

Regional posts are at contractors' works and involve the implementation of inspection standards.

**QUALS.** Applicants must have served a recognised engineering apprenticeship or have had equiv. training and possess O.N.C., appropriate C. & G. Final Cert. or equiv. qualn. Appropriate experience in H.M. Forces can be considered in place of specified quals. **SALARY:** £990 (at age 26)—£1,059 (at age 28 or over on entry) rising to £1,179 for the Bromley and Woolwich posts. A little less for some of the regional posts. There are good prospects for promotion and pension. Technical College courses sponsored for suitable candidates. **APPLICATION FORMS** from Manager (PE.4257), Ministry of Labour, Professional & Executive Register, Atlantic House, Farringdon St., London, E.C.4. **CLOSING DATE** 6th September, 1965.



# ENGINEERING STAFF

The INDEPENDENT TELEVISION AUTHORITY has vacancies for ENGINEERING STAFF at its Transmitting Stations.

The work on the Stations consists of the operation and maintenance of television transmitters and ancillary equipment. This calls for a high degree of skill and knowledge of electronics, television techniques and high frequency engineering; these vacancies are for young men with good basic knowledge who can be given appropriate training. A Higher National Certificate in Electrical Engineering or similar qualification is required.

Conditions of service are excellent and include a contributory pension scheme. Shift working is involved to cover the period from 8 a.m. to midnight.

Starting salaries, depending on qualifications and experience, will be within the scale £875 to £1,145.

Applications in writing, stating age and details of experience and qualifications, and quoting Reference Number W. W. 583 should be addressed to the:—

**Personnel Officer,  
INDEPENDENT TELEVISION AUTHORITY,  
70, Brompton Road,  
London, S.W.3.**

## THE UNIVERSITY OF MANCHESTER.

APPLICATIONS are invited for appointment as Service Engineer in the Department of Chemistry to maintain and service a wide variety of spectrometers and other scientific equipment. Previous experience of service work, not necessarily on spectrometers, is essential, and candidates should preferably have H.N.C. or some similar qualification. Salary range: £870 to £1,450 per annum. The initial salary will be according to qualifications and experience. Contributory superannuation scheme. Applications should be sent not later than October 15th, 1965, to the Registrar, the University, Manchester, 13, from whom further particulars may be obtained, on quoting reference 170/65. W.W. [1301]

## BOLTON INSTITUTE OF TECHNOLOGY ELECTRICAL ENGINEERING DEPARTMENT DIPLOMAS IN ELECTRONIC ENGINEERING

Two year full-time course (entry: four appropriate "O" level passes) for the Ordinary Diploma.

Two year full-time course (entry: appropriate "A" level and "O" level passes) for the Advanced Diploma.

Successful completion of the courses gives valuable exemptions from the examination requirements of the British Institution of Radio Engineers and of the Institution of Electrical Engineers.

Further particulars from:

Head of Department of Electrical Engineering,  
Bolton Institute of Technology,  
Manchester Road, Bolton.



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● FREE SPECIMEN COPY ON REQUEST

7 TUDOR STREET, LONDON, E.C.4. FLE. 1455

WW-150 FOR FURTHER DETAILS.

## UNIVERSITY OF BELFAST

Applications are invited for the post of Senior Experimental Officer in charge of the Electron Microscopy Laboratory with effect from 1st October, 1965. In addition to administrative and maintenance duties the successful applicant will be required to assist in the training of research workers in the techniques of electron microscopy. A knowledge of the techniques of specimen preparation is also desirable. The salary scale is £1,400 x £60—£1,640 (merit bar) x £65—£2,160. Further details may be obtained from the Deputy Secretary to the Academic Council, and applications should reach him by 31st August, 1965.

## MINISTRY OF AVIATION

Royal Aircraft Establishment, Bedford

require a **TECHNICIAN**, age 24 or over, to be responsible for workshop training of electronic craft apprentices during their first two years. A wide experience of electronics, including the use of test gear required. An interest in young people and the ability to demonstrate equipment is desirable. **QUALS.** Applicants must have served a recognised engineering apprenticeship or have had equiv. training and possess an O.N.C., appropriate C. & G. Final Cert. or equiv. qualn. Appropriate experience in H.M. Forces can be considered in place of specified qualifications.

**SALARY:** £945 (at age 26)—£1,009 (at age 28 or over on entry) rising to £1,129 p.a. The salary is at present under review. Good prospects for promotion and pension. Technical College courses sponsored for suitable candidates. **APPLICATION FORMS** from The Manager (PE.4258), Ministry of Labour, Professional & Executive Register, Atlantic House, Farringdon St., London, E.C.4. **CLOSING DATE** 6th September 1965.

## BOOKS INSTRUCTIONS, ETC.

CONVERT any TV set into an oscilloscope; instructions and diagrams 12/6.—Redmond, 42, Dean Close, Portslade, Brighton, Sussex. [112A]

MANUALS, circuits of all British ex-W.D. 1939-45 wireless equipment and instruments from original R.E.M.E. instructions; s.a.e. for list, over 70 types.—W. H. Bailey, 167a, Moffat Rd., Thornton Heath, Surrey. [143]

## ARTICLES FOR SALE

FERROGRAPH 5/AN (March 1964 £62, no offers (London).—Box WW 110, Wireless World.

EVERSHED Bridge Megger, 1,000 volt, as new with test certificate. £55. Multirange High Grade service test meters, as new. £9. Reflecting Galvanometer. £5.—Cooper, 513, Holmwood Rd., S. Yardley, B'ham. 26. [1291]

## SOUTH OF SCOTLAND ELECTRICITY BOARD COMMUNICATIONS AND ELECTRONICS

Applications are invited for a **THIRD ASSISTANT ENGINEER** in the Plant and Equipment Development Section of the **RESEARCH AND DEVELOPMENT BRANCH** at Board Head Office, Glasgow.

The duties of the Communications and Electronics group include the promotion and evaluation of new designs of equipment, the preparation of general specifications and technical standards, the technical assessment of tenders, and the association of service experience with this work.

Applicants should have had experience of either the design and testing, or application of telecommunications and electronics equipment. The successful applicant will be working in a group studying the latest developments in data transmission over both physical and radio channels and will advise on their application in the Board's telecommunications telemetering, control and protective systems.

Applicants should possess the necessary qualifications for Graduate Membership of the Institution of Electrical Engineers. A University Degree will be an advantage.

**Salary** (According to qualifications and experience). Commencing at £1,550 and rising to £2,045 per annum; or commencing at £1,460 and rising to £1,910 per annum. (In each case plus a supplementary payment of £60 p.a.)

Applications, quoting reference E65/65, should be submitted on the standard form to the Chief Personnel Officer, South of Scotland Electricity Board, Cathcart House, Inverlair Avenue, Glasgow, S.4, not later than 13th September, 1965.



The General Post Office has vacancies for  
**RADIO OPERATORS II**  
 at its  
**COAST RADIO STATIONS**

Applications are invited from men between 21 and 35 years of age holding either the Postmaster General's First or Second Class Certificate of Competence in Radiotelegraphy or an equivalent certificate issued by a Commonwealth Administration or the Irish Republic.

The posts, which will be temporary in the first instance, carry a salary scale of £674-£976, dependent on age at entry, but successful applicants will be eligible to enter the open competitive selection for permanent appointment to be held in September of this year.

Applicants should write to The Inspector of Wireless Telegraphy, Union House, St. Martin's-le-Grand, London, E.C.1. or telephone London HEADquarters 5545 for further information.



# PROJECT LEADER

An Electronics Engineer with experience in development work or in a Measurements Laboratory is required as Project Leader in the Laboratory Service Group of the Mullard Central Applications Laboratory.

The Projects are primarily:

- 1) Design of electronic equipment for specialised measurements.
- 2) Organisation of a unit for calibration and maintenance of a wide range of electronic measuring equipment.

A versatile person capable of carrying considerable personal responsibility is required for this post.

A good educational background is necessary, preferably to B.Sc. or at least H.N.C. level.

Applicants are invited to write to:

**The Personnel Officer,**  
**Mullard Limited,**  
**New Road, Mitcham Junction, Surrey**  
 quoting reference (PL/KBL)

### ARTICLES WANTED

**SPIRE**, plain, self locking nuts, screws and rivets, large quantities wanted for cash.—L. Kayser, 170, Highbury Quadrant, London, N.5. Canbury 6765.

**WANTED**, all types of communications receivers and test equipment.—Details to R. T. & I. Electronics, Ltd., Ashville Old Hall, Ashville Rd., London, E.11. Lev. 4986.

**URGENTLY** wanted, new valves, transistors, radios, cameras, binoculars, tape recorder and tapes, watches, any quantity.—S. N. Willetts, 43, Spion Lane, West Bromwich, Staffs. Tel. Wes. 2392.

**HIGH** prices paid for government surplus manuals and handbooks on radio and electronic equipment; also required, any books or publications on government surplus equipment and modification of same; single copies purchased—Apply Box W.W. 1277, Wireless World.

**THE MINISTRY OF DEFENCE** (ARMY DEPARTMENT) invites applications for Grade 5 Engineering appointments in the **BRITISH FORCES BROADCASTING SERVICE**. There are posts in Aden, Benghazi, Tobruk, and Cyprus.

#### DUTIES & QUALIFICATIONS

Operation and maintenance, of MF, HF, VHF Transmitters, Studio equipment and generating equipment. Appropriate ONC, City & Guilds, or equivalent qualifications are necessary.

**SALARY SCALE** for Grade 5 staff is £1,007 to £1,483 p.a. In addition generous non-taxable Foreign Service Allowances are paid according to location. Candidates must be at least 21 years of age.

For further details and application form please write to:

**The Director (EW),**  
**British Forces Broadcasting Service,**  
**Kings Building,**  
**Dean Stanley Street,**  
**London, S.W.1.**



# ELECTRONIC ENGINEERS & TECHNICIANS

The growth of our manufacturing facility has led to opportunities for Engineers and Technicians to join a group working on the Design, Development, and Maintenance of test equipment used in the manufacture of semi-conductor components. This work involves d.c. and a.c. amplification up to 1000 mc/s, high speed switching and pulse techniques, and the use of a wide variety of measuring instruments.

Engineers should have HNC or equivalent in Electrical Engineering, and at least 2 years' experience in a related field. Salary will be in the range £900-£1,675.

Technicians should have ONC, H.M. service training, or at least 3 years' radio and television servicing experience. Salary will be in the range £640-£1,200.

Salaries are reviewed every 6 months, and the non-contributory fringe benefit schemes include life assurance, pension, hospitalisation insurance and profit sharing.

Please apply, giving brief relevant details, to

**The Personnel Manager**  
**TEXAS INSTRUMENTS LIMITED**  
**Manton Lane, Bedford.**

# CIVIL AVIATION TELECOMMUNICATIONS

The Ministry of Aviation has vacancies for Radio Technicians at Airports, Air Traffic Control Centres, Radio Stations and other specialised Engineering Establishments throughout the United Kingdom.

The numbers and speed of air traffic today demand a complex, co-ordinated and reliable telecommunications system for airports, en-route navigation and air traffic control in order to ensure the highest standards of safety. The Ministry's Radio Technicians play a vital role in the installation, maintenance and technical operation of this system. Their duties embrace a wide range of equipment, including Primary Surveillance and Approach Radars, Secondary Surveillance Radars, Radio Navigational and Landing Aids, Radio and Line Communications, Electronic Data Displays, Closed Circuit T.V., Digital and Analog Computers.

Applicants should be aged 19 or over, of British nationality and possess a sound basic knowledge of Radio/Electronics with practical experience in at least one of the main branches of Telecommunications. The possession of formal qualifications would be an advantage.

Training on equipments and new techniques is provided at the Ministry's Civil Aviation Signals Training Establishment, Bletchley, Bucks.

Radio Technicians are encouraged to study for Technical and Professional Qualifications, and generous assistance, including part-time and, in special circumstances, full-time release, is provided.

There are good prospects of permanent pensionable posts and promotion to a higher class with a salary ranging from £1,032 per annum to £1,911 per annum.

Starting salary varies according to age: from £747 per annum at 19 to £962 per annum for entrants of 25 or over, and rises to £1,104 per annum. Annual leave is 3 weeks and 3 days, plus 9 days for public holidays.

For further details apply to:—

Mr. J. J. Robinson, M.I.E.R.E., A.M.B.I.M.,  
Ministry of Aviation,  
Room 754,  
The Adelphi,  
London, W.C.2.

## UNIVERSITY COLLEGE LONDON PSYCHOLOGY DEPARTMENT

- (1) Senior Technician to supervise laboratory store with assistance of technician. In addition to maintaining wide range of electrical and mechanical equipment, there will be opportunities for design and construction. Quote Ps/1.
  - (2) Senior Technician to be responsible for design and construction of variety of electronic equipment for research projects. Quote Ps/2.
  - (3) Technician to assist in running laboratory store and in design and construction of mechanical and electrical equipment. Quote Ps/3.
- Application forms from Establishment Officer, University College, London, Gower St., W.C.1.

### TAPE RECORDING ETC.

SAVE on cost of hi-fi. See Audio Supply notice (advert. No. 111). [109]

BRAND five polyester tapes, P & P free; send 5/- for sample 600 DP on 7in reel.—Minim (WW), Kenley, Surrey. [16]

UNIQUE Buy! Recording tape, top brand, 7in. 2,400ft. D.P., 25/-; 5 $\frac{1}{2}$ in 1,200ft. 19/6; p. & p. 1/6 per spool; bargains in all sizes: s.a.e. for list, we repair, buy and sell recorders.—E. C. Kingsley & Co., Ltd., 132, Tottenham Court Rd., London, W.1. Euston 6500. [113]

TAPE/DISC/TAPE transfer editing; duplicating; if quality and durability matter (especially with LPs from your precious tapes), consult Britain's oldest transfer service.—Fund raising records published for schools, musical societies (tax free)—Sound News Productions, 10, Clifford St., London, W.1. Reg. 2745. [108]

### NEW GRAM AND SOUND EQUIPMENT

GLASGOW.—Recorders bought, sold, exchanged; cameras, etc., exchanged for recorders or vice-versa.—Victor Morris, 345, Argyll St., Glasgow, C.2. [120]

RETURN of post service; record changers, players and tape decks, some at special prices; speakers, Martin tape kits, Mullard amplifier kits, test meters, all in stock, H.P. available; send for free illustrated lists, postal only.—Watts Radio, Ltd., 54, Church St., Weybridge, Surrey. Tel. 47556. [114]

### CHELSEA COLLEGE OF SCIENCE & TECHNOLOGY

Senior Technician required to take charge of Electronics Workshop and associated Electronics component stores in Department of Physics.

Applicants should have considerable experience in the design, construction and development of electronic apparatus and be able to instruct junior staff.

Appropriate City and Guilds or National Certificate qualifications desirable.

5-day week. Superannuation.

Salary £840—£1,040 with London Weighting up to £45 at 27 and qualification supplements. Good prospects of promotion.

Application forms from the Superintendent of Laboratories, Department of Physics, Manresa Road, S.W.3 (FLA 6421, Ext. 28).

### HAMMER FINISH PAINT

The modern finish for electronics. Can be BRUSHED or sprayed. Blue or Silver. 2 $\frac{1}{2}$  oz. tins 3s. 6d., post 8d.  $\frac{1}{2}$  pint 7s. 6d., post 1s. 9d. 1 pint 15s., post 2s. 9d. Orders over 30s. post free. Return of post service. Retailers supplied. S.A.E. for details. FINNIGAN SPECIALITY PAINTS, (W), Mickley Square, Stocksfield, Northumberland.

WW—151 FOR FURTHER DETAILS.

### "WIRELESS WORLD" TEST INSTRUMENTS

Complete sets of Metalwork, machine engraved Front Panels. Special Tag Boards and all specified 1st grade components. For professional appearance and performance.

Send 6d. in stamps for lists

### MALVYN ENGINEERING WORKS

Engineers to the Radio and Electronic Industries  
7 CURRIE STREET, HERTFORD, HERTS.  
TELEPHONE: HERTFORD 2264

WW—152 FOR FURTHER DETAILS.

### SURPLUS AIRCRAFT NAVIGATION EQUIPMENT

Originally part of an aircraft direction finding equipment and containing A.T.B. approved components.

POWER UNITS, 12 VOLT D.C. INPUT, 25 WATTS  
Outputs 2 at 350 v. D.C. smoothed, and 1 at 6.3 v. Contains 3—OC36, 2—OC72, 9—Diodes, transformer relay, etc. In mottle grey aluminium case, 5 $\frac{1}{2}$ in. x 5in. x 6in. Could be adapted for shaver operation.  
With circuit diagram 45/-, plus P. & P. 6/6. Diagram only 2/6, plus 9d. P. & P.

POWER UNITS AS ABOVE BUT 24 V. INPUT  
40/-, plus P. & P. 6/6.

M.F. RECEIVER 200-400 & 500-900 KC/s.  
Contains tuning and two I.F. stages, diodes and 2—OC170, 3—OC45, 2—OC702 and 2—OC318. In mottle grey aluminium case, 9in. x 5 $\frac{1}{2}$ in. x 3 $\frac{1}{2}$ in.  
With circuit diagram 55/-, plus P. & P. 6/6. Diagram only 2/6, plus 9d. P. & P.

#### INDICATOR UNIT

Contains 2 $\frac{1}{2}$ in. C.R.T. Type DG7-5 (CV.2175), 2—ECC83, 1—ECC81, E.H.T. rectifiers and numerous condensers and resistors. In mottle grey aluminium case, 9in. x 6in. x 3 $\frac{1}{2}$ in. and would form the basis of a miniature Oscilloscope.  
With circuit diagram 55/-, plus P. & P. 6/6. Diagram only 2/6, plus 9d. P. & P.

The above items are brand new and complete but have not been tested and cannot therefore be guaranteed. A small number of incomplete units of each version are available at 15/- each, plus P. & P. 4/-.

COMPONENTS—all first grade

Transistors OC36—matched pair	25/-
OC36—Single	10/-
OC170	7/-
OC45	4/-
AFZ12	12/6
Valves 12AT7 (ECC81)	4/-
12AX7 (ECC83)	5/-

P. & P. 9d.

E.H.T. Rectifiers K3.45	7/-
Vinkors LA2409	15/-
LA2103	15/-
Crystals 10.7 mc/s	15/-

P. & P. 1/-	
C.R. Tubes DG7-5	25/-
P. & P. 3/6	

Also many other items including capacitors, resistors, relays, diodes, slow motion drives, transformers, group wiring boards. Please send S.A.E. for list.

Enquiries and orders by post only to:—

N. J. GAWLER,  
40, Medina Road,  
COWES,  
Isle of Wight.

WW—153 FOR FURTHER DETAILS.





## Research Department Senior Technical Assistant

in the Instrumentation Section of the Engineering Research Division, Derby. He must have H.N.C. or equivalent in Engineering or Physics and be conversant with instrumentation for the measurement of static and dynamic phenomena occurring in mechanical and civil engineering. He must be capable of using and maintaining such instrumentation in the laboratory and in the field. He will be required to work as a member of a team under field conditions with men trained in other engineering disciplines.

**Salary range:** £1,090 – £1,325 with additions to salary for passing certain educational examinations.

The appointed candidate will join a superannuation fund (contributory) and enjoy attractive free and reduced rate travel facilities.

*Applications stating age, education, qualifications, experience and present salary should be sent to Headquarters Staff Manager (B.155),*

**British Railways Board,  
222 Marylebone Road, London NW1**

## Outstanding opportunities in computers in our Field Engineering Services

**Documentation Engineers** – Able to write clearly and concisely to provide technical information for engineers. Interesting work is in hand and experience in electronics or computer peripheral equipment would be fully used. These vacancies are at Kidsgrove which is well placed on the Staffordshire/Cheshire border—houses are not expensive.

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Able to work in liaison with development engineers to ensure full consideration of maintenance problems in the design of new computers. Experience on computer systems or peripherals would be desirable. These vacancies are at Kidsgrove, N.W. London and Chelmsford.

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– Able to be trained to maintain a computer installation. A sound knowledge of electronics is necessary, preferably including pulse circuitry and transistors, together with above average logical ability. Shift work would be compensated by generous allowances. Location could be London, Home Counties, Bristol, Leeds, Manchester, Lytham, Midlands, Glasgow or elsewhere, by mutual agreement.

**SPECIFICATION:** Aged approximately 25-35 years; keen to do a worthwhile job; a qualification or recognised training in electronic engineering maintenance; willing to work smoothly with others; determined to make a good career with a progressive company.

#### APPLICATION:

Age, qualifications and experience.  
Choice of work location.  
Choice of interview place—London,  
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Possible dates for interview.

By writing to:

*G. M. Bolton, Dept. WW/L.44,  
English Electric-Leo-Marconi Computers Ltd.,  
KIDSGROVE, Stoke-on-Trent.*



ENGLISH ELECTRIC LEO MARCONI

## MINISTRY OF TECHNOLOGY NATIONAL PHYSICAL LABORATORY Teddington, Middlesex. LIGHT DIVISION

**Scientific Officers/Senior Scientific Officers and Research Fellows (Junior and Senior)** required in Light Division which is concerned with the generation measurement, properties and use of electro-magnetic radiation throughout the spectrum from the far infra-red to the far ultra-violet. Lasers, thermal transducers, photo-detectors, colour vision, crystal optics and instrument development are a few of its fields of work. There is a strong emphasis on applied research, using the most modern electrical methods in the exploitation and extension of optical principles and techniques.

**QUALIFICATIONS:** S.O./S.S.O.—1st or 2nd class honours degree, Dip. Tech., or equivalent, or higher qualification in physics or electrical engineering and, for S.S.O., at least 3 years' post-graduate experience. For some posts, experience of industrial conditions, though not essential, would be valuable.

**Research Fellows:** Applicants should have the qualifications required for S.O. (as above) and must have reached a high standard of research ability. In addition the following are required:—  
Junior Research Fellow: 2 years' post-graduate research.  
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**SALARIES:** S.O. £940-£1,586.  
S.S.O. £1,750-£2,147.  
J.R.F. fixed in range £1,140-£1,520.  
S.R.F. fixed in range £1,685-£2,080.

Except for Research Fellowships which are tenable for 3 years, the above posts carry prospects of permanent pensionable appointment.

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Labour Manager,  
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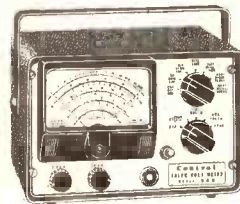
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Reads A.C. and D.C. voltages up to 5,000, Alternating and Direct Current up to 10 amps., Resistance up to 50 Megohms. Decibels from -10 to -42 dB. Internal buzzer for audible warning of short circuits or continuity, and fitted with automatic overload protection for movement. Meter size 4 1/2 in. x 2 1/2 in., overall dimension 7 1/2 in. x 5 1/2 in. x 3 1/2 in. Has rigid handle which can be swivelled for use as a tilt support. ONLY £17/10/-.

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Vacuum impregnated, interleaved, E.S. screen, universal mounting. Size 4in. x 3 1/2 in. x 2 1/2 in. ALL BRAND NEW 15/6 each Post 2/6.  
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Duties will include the teaching of technology and practical work to full-time first year of apprenticeship courses and day release classes leading to the City and Guilds examinations.

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Certificated teachers receive an additional payment of £70 per annum.

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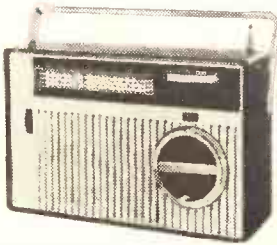
Further information and application forms, returnable by Friday, 27th August, may be obtained from the Director of Education, St. Giles Street, Edinburgh, 1.



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## THE "SKYROVER" RANGE

7-transistor and 2-diode superhet — 6 waveband portable receiver, covering the full Medium Waveband (150-575 M) and Short Waveband (32-94 M) and 4 separate switched Band Spread Ranges on 13M, 16M, 19M and 25M Bands. L.F. frequency 470 Kc/s. 5m. Ceramic Magnet P.M. Speaker. Telescopic and internal Ferrite Rod Aerial. The coil pack and tuning heart is completely factory assembled, wired and tested. Detailed and easy to follow instructions. Operates on four 1.4 v. torch batteries (U2 or equivalent).



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New supplied with redesigned cabinet, edgewise controls, black and chrome plastic cabinet. Size 10 5/8 x 3 1/2 in.

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5in. Double play, 1,200ft. Mylar base	15/-
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5in. Triple play, 1,800ft. Mylar base	35/-
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5 1/2in. Long play, 1,200ft. Acetate base	12/6
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5 1/2in. Triple play, 2,400ft. Mylar base	45/-
7in. Standard play, 1,200ft. Acetate base	10/-
7in. Standard play, 1,800ft. Mylar base	12/6
7in. Long play, 1,800ft. Mylar base	19/6
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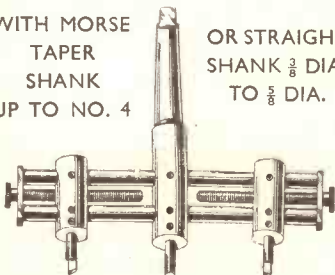
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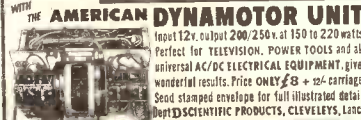
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(Twin coils—most values—add 1/-)  
Postage and Packing, 1/6 per relay

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Relays built to specification; light duty, platinum, heavy duty contacts, (makes, breaks, changeovers, make before breaks). Slugged coils etc.

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9-Bank 2-pole 8-way plus 2-Bank 4-way shorting, insulated to carry up to 10 Kv. on last two banks, operating voltage of solenoid 12-24 v. d.c. All wafers are standard size, removed from brand new equipment 32/6 ea. P.P. 2/6.

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RELAYS MINIATURE  
S.T.C. 4184GD, 24 v. 700 ohms, 2 C.O.  
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All above relays 8/6 each, plus P.P. on all relays 1/-.

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Six miniature relays 9-12 v., 1 make per relay, contained in neat aluminium case 6 x 4 x 1 1/2 in., with six half inch spaced crystal holders, designed to switch any desired crystal by remote control. Relays and crystal holders can be easily removed for other uses if required, terrific value, only 15/6. P.P. 1/6.

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Very latest type twelve C/O heavy duty silver contacts, these switches were designed for normal panel mounting, complete with chrome escutcheon plate and screws. Price 9/6 each, special terms for quantities.

D.C. TO A.C. ROTARY CONVERTERS. Input 220 v. D.C. at 1.5 amps., output 230 v. A.C. at 200 watts. The above rating is to Admiralty spec., normal motor mounting size 16 x 8 in. Weight 77 lbs. £12/10/-.

Johnson Air Spaced T/X Condensers, 500pf. ceramic insulation, 25/- P.P. 2/9.

**LONDEX AERIAL C/O RELAYS.**

Type 7026. Price 25/- P.P. 2/-.

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- ★ AR88D, as new . . . . . £45 P.P. 25/-
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**L.T. TRANSFORMERS**

5 v. C.T. three times, at 5 amps., 250 v. primary. These U.S.A. transformers are excellent for charging purposes. New boxed, 22/6. Carr. 3/6.  
12 v. 7 v. 13 v. at 1.5 A. Fully shrouded, tapped primary 240 A.C., small size, 12/6 each. P.P. 2/3.

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30K ohms, brand new stocks . . . . . 22/6. P.P. 1/3

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A source of power to operate your 1392 R/X or any equipment that requires a fully smoothed output of 250 v. d.c. + 6.3 v. at 6 amps., for bench or 19in. rack mounting, fully fused tapped input 200 to 250 v. a.c., brand new cased units at only 55/- P.P. 12/6.

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**ENGLISH ELECTRIC E.H.T. GENERATOR**

0-10 kv. audio and visual indication.  
Other types available up to 16 kv.

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Absorption type wavemeter by S.T.C. frequency range 100 kc/s to 48 Mc/s with nine plug-in coils. Powered by 1 1/2 volt dry cell and triode valve, complete with all calibration charts 250 micro amp meter, super slow motion dial, etc., the wavemeter coils calibration charts are contained in a neat wooden transit case, 14 x 13 x 8 in., excellent condition. £4/19/6. carr. 7/6.

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Ideal for VHF and 2-meter enthusiasts small portable instrument, comprising signal generator, RF watt meter to 30 watts, and AF output meter, frequency range 100 to 150 mc/s, complete with all leads and plugs, internal 24 v. power supply. New, boxed instruments. Price £12/10/- P.P. 10/-.

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Marconi type TF801 8-300 Mc/s. £45.  
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G.R. type 606S 95 Kc/s. 30 M/cq. £30.

**FREQUENCY METER G.R. TYPE 620A.** Range 300 Kc/s-300 Mc/s. on direct reading frequency scale, accuracy is better than 0.01% or better when the frequency is checked in terms of the crystal calibrator, internal power supply 105-250 v. A.C. As new. Price £75. P.P. 20/-.

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**P. F. RALFE**  
423, GREEN LANES,  
HARRINGAY, LONDON, N.4.  
MOUNTVIEW 6939

WW-159 FOR FURTHER DETAILS.

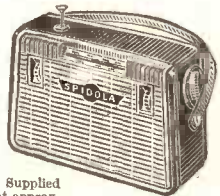
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WHEN ONLY THE BEST IS GOOD ENOUGH  
**GENUINE OFFERS!**

**"WALTER" METROPOLITAN**  
MAINS/BATTERY TAPE RECORDER  
MAKER'S ORIGINAL LIST PRICE 55 GNS.  
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Seven transistors with two watts output. High-Fi perfection with enough volume to fill a small hall on mains or battery. Only a very few now available. Complete with Mike, Tape, Spools, Leads, Instruction Book, and complete Service Manual.

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TRULY! A most amazing radio with world-wide performance on all eight wave-bands. Stations just roll in with bell-like clarity.  
LONG WAVES 2,000-730-3 metres (150-408 Kc/s.)  
MEDIUM " 571.4-186-9 " (525-1,605 Kc/s.)  
SHORT " (1) 41-50 " (5-95-7.3 Mc/s.)  
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" (3) 25 " (11.7-11.975 Mc/s.)  
" (4) 19 " (15.1-15.45 Mc/s.)  
" (5) 16 " (17.7-17.9 Mc/s.)  
" (6) 13 " (21.45-21.75 Mc/s.)



Internal ferrite rod aerial for reception of Long and Medium wave-bands and 8 section telescopic aerial extending to 38 in. for short wave ranges. Sockets for external aerial, earth and extension speaker or phones, also pick-up jack for use with gram, recorder or as amplifier. Exceptionally well designed two-tone cabinet with carrying handle. Supplied complete with batteries, weight approx. 5 1/2 lbs. Size 10 1/2 in. x 7 1/2 in. x 3 1/2 in. Comprehensive instruction book and technical manual all in at OUR PRICE £10/15/-.

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Medium and Long wave-bands. Exquisitely designed with Gilt finish fascia and two tone plastic cabinet. Ferrite rod internal aerial also telescopic aerial and horizontal station tuning indicator. Comes complete with real brown leather case, strap, battery and earpiece with pouch. Size 5 1/2 in. x 3 3/4 x 1 1/2 in., weight 14 oz. OUR PRICE £4/16/6. P. & P. 3/6.



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A real professional model for all speech and music recording. Twin track, two speeds 1 1/2 and 3 1/2 i.p.s. Six transistors, one diode, one thermistor. Cassette drive. Equipped with remote control switch on Microphone, allowing for stop/start at will. Recording level and battery condition VU meter. Dash board styled push-button controls with Special Record button to prevent accidental erasure. Records and plays in upright position. Housed in attractive two tone high impact poly-vinyl case featuring a handy snap-on plexiglass top for fast, efficient tape loading. Size 9 in. x 8 1/2 x 3 1/2 in. Weight 5 lbs. Complete with Tape, Spools, Batteries, Earphone for private playback—monitoring and microphone with instruction book. OUR PRICE £16/18/-, post paid. An A.C. mains Converter is available at 75/- extra.



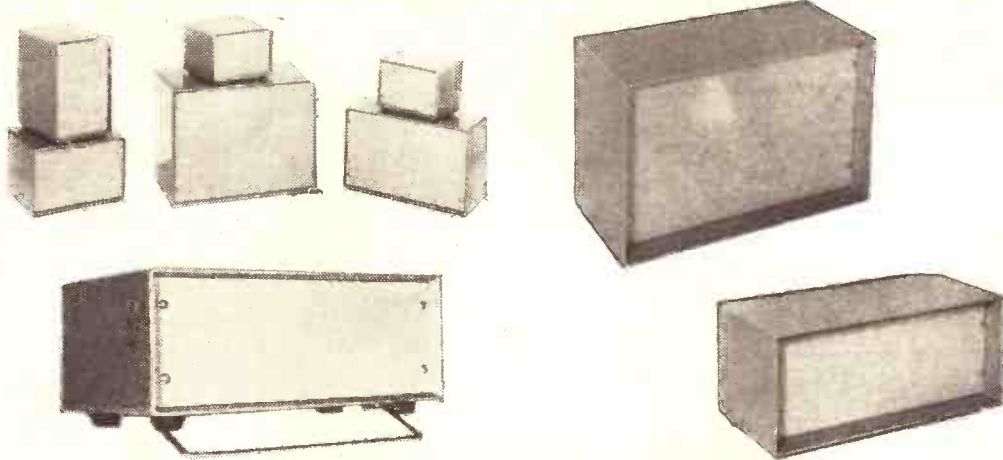
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Power output 10 watts per channel into a 16 ohm load or 15 watts into 4 ohm load. Combined amplifier and control unit for stereo or monaural. OUR PRICE £49/10/- Carr. paid. TERMS: CASH WITH ORDER ONLY. NO C.O.D. S.A.E. ALL ENQUIRIES PLEASE

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WW—160 FOR FURTHER DETAILS.

**H**RO Rx's, etc., AR88, CR100, BRT400, G209, S640, etc., etc., in stock.—R. T. & I. Electronics, Ltd., Ashville Old Hall, Ashville Rd., London, E.11. Ley. 4986. [142]

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**S**IGNAL generators, oscilloscopes, output meters, wave voltmeters, frequency meters, multi-range meters, etc., etc., in stock.—R. T. & I. Electronics, Ltd., Ashville Old Hall, Ashville Rd., London, E.11. Ley. 4986. [141]

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AUDIO EQUIPMENT MANUFACTURERS

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CHP 3

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The oldest Component Specialists in the Trade

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EST. 35 YEARS

## BARGAINS STILL AVAILABLE IN LOUDSPEAKERS

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### SCHEDULE OF LOUDSPEAKERS AVAILABLE

Diameter in inches	Gauss in Lines	Impedance in Ohms	Price	Diameter in inches	Gauss in Lines	Impedance in Ohms	Price	Diameter in inches	Gauss in Lines	Impedance in Ohms	Price
2	7,000	80	8/-	3½	9,500	35	10/6	4	7,000	35	11/-
2½	7,000	35	8/6	3½	9,500	8	10/6	4	9,600	35	11/6
2½	7,000	50	8/6	3½	7,000	35	8/6	5	7,000	3	8/6
2½	7,000	80	8/-	3½	9,500	50	10/6	5	7,000	3	9/-
3	8,500	3	10/-	4	9,500	25	11/6	5	9,500	3	10/6
3	6,000	5	8/6	4	9,000	50	11/6	5	9,500	15	12/6
3	6,500	80	9/6	4	9,500	15	12/-	5	8,500	25	10/6
3	7,000	5	9/-	4	7,500	5	9/6	6½	7,000	3	11/-
3	7,000	35	9/-	4	7,000	25	11/6	8	6,000	15	13/6
3½	8,000	15	10/-	4	6,000	35	10/6	8	8,500	3	13/6
3½	7,000	3	9/6								

Elliptical Size in ins.	Gauss in Lines	Impedance in Ohms	Price	Elliptical Size in ins.	Gauss in Lines	Impedance in Ohms	Price	Elliptical Size in ins.	Gauss in Lines	Impedance in Ohms	Price
5x3	7,000	3	8/-	6x4	9,500	35	12/-	8x2½	6,000	3	8/6
5x3	9,000	35	12/-	7x3½	7,000	3	9/6	8x2½	8,500	5	9/6
5x3	9,000	3	8/6	7x3½	9,500	3	10/6	8x2½	9,500	3	10/-
5x3	9,500	3	9/-	7x3½	9,500	8	11/6	8x5	8,500	3	11/-
6x4	8,500	3	9/6	7x4	9,500	3	11/-	8x5	11,000	3	13/6
6x4	9,500	3	10/-	7x4	9,500	30	12/6	10x6	11,000	3	22/6
				7x4	10,000	3	12/6	10x6	11,000	5	22/6
				7x4	12,000	3	15/6	10x6	11,000	25	23/6

ALLOW 2/6 each speaker for P. & P./handling charges, and please specify the exact requirements—the nearest available will be sent.

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Beautifully geared AM/FM 2-Gang Condensers 4/6; AM/FM IFT's 465 kc/s. and 10.7 Mc/s. 4/6 pair; Magnavox Crystal Tape Recorder Mikes 12/6; 3 watt Stereo Amplifiers complete ready to switch on. 79/6; Senterrell rectifiers R7 2½; 3D-3-1-V. 2/6 each. DIODES OA70, OA79, OA90, OC46H, G1916, 2/- each. TRANSISTORS: OC45 4/6; PXA 101 3/9; AF115 4/6. SILICON GERMANIUM DIODES 1/3. M.T. DIODES 8d. each. Silicon Diodes 400 PIV 330 mA. 2/6 each. Please send STAMPED AND ADDRESSED envelope with any enquiry. We regret no catalogues—our stocks move too quickly! Kindly make provision for sufficient postage and packing charges to avoid delay. TERMS: Cash with order or C.O.D. on orders over 30/-.

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GENERAL PURPOSE  
OSCILLOSCOPE  
MODEL T.L.4



£29.19.6

An extremely versatile instrument available direct from the manufacturers at a very low cost. Guaranteed for six months.

P. & P. 9/6.

- C.R.T. — 3 inches.
  - AMPLIFIER — 10 c/s—25 mc/s (±3 dB approx.).
  - TIME BASE — 1µ sec./cm.—1 sec./cm. Fully variable.
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  - TERMS — C.W.O. or C.O.D. Post only.
- WRITE TO — 14 Orle Street, London, W.1  
FOR FULL DETAILS:

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## SERVICE & REPAIRS

**S**PEAKER repairs, cones fitted, guaranteed satisfaction.—L.S. Repair Services, Pluckley, Ashford, Kent. [132]

**S**PEEDY and expert tape recorder and hi-fi repairs by England's leading hi-fi specialists.—Telesonic, Ltd., 92, Tottenham Ct. Rd., London, W.1. Mus. 8177. [126]

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**A**IRTRONICS, Ltd., for coil winding, assembly and wiring of electronic equipment, transistorised sub-units, sheet metal work.—5a, Walerand Rd., London, S.E.13. Tel. Lee Green 1705. [107]

## AGENTS

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17" — £5 : 19 : 0

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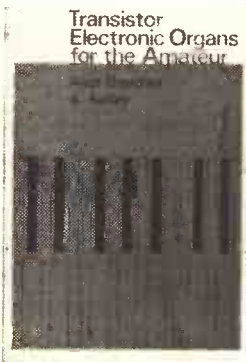


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## TRANSISTOR ELECTRONIC ORGANS FOR THE AMATEUR

Alan Douglas & S. Astley

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Transistor Electronic Organs for the Amateur

## PICK - UPS The Key to Hi-Fi J. Walton

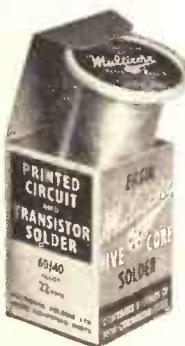
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All metal—beautifully plated—compact in size. Easily and permanently attached to a tape recorder. Clamps hold the magnetic or leader tapes in the precision cut channel—no damage to the edges. Right angle and oblique cutting slots.

Complete with Razor Cutter 18/6

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CMMS 25a

(See also advertisement on back cover)  
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- \* Unique design.
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having the following unusual features.

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Full details on request.

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* 75 ft. Plywood Aerial Masts .....	£35 0
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Total cost of all parts **£3.9.6**

Parts price list and easy build plans 2/- P. & P. 3/6.



"Transona Five" size 6½ × 4½ × 1½ in. approx.

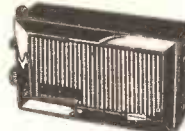
## TRANSONA FIVE or POCKET FIVE

★ 7 Stages—5 transistors and 2 diodes.

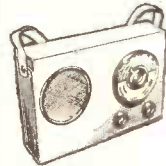
Covers M. and L. Waves and Trawler Bands, a feature usually found in only the most expensive radios. On test Home, Light, 208, and many Continental stations were received loud and clear. Designed round supersensitive Ferrite Rod Aerial and new type fine tone super dynamic 2½ in. speaker, attractive plastic cases with red grille.

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★ 8 stages—6 transistors and 2 diodes. ★ 6 waveband. ★ Now with Philco micro-alloy R.F. transistors.

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Parts price list and easy build plans 2/- Carrying Strap 1/6 extra. P. & P. 3/6.

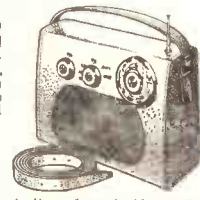
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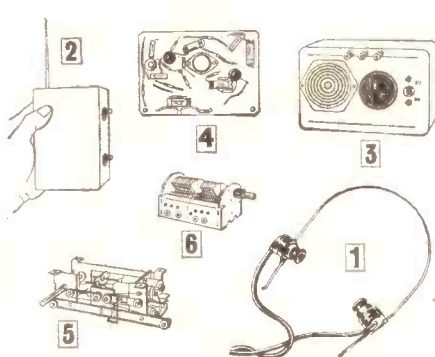
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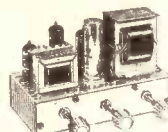
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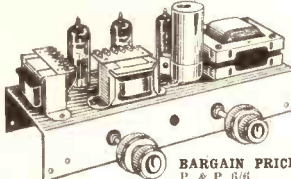
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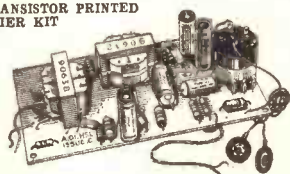
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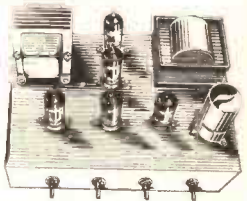
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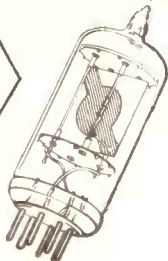
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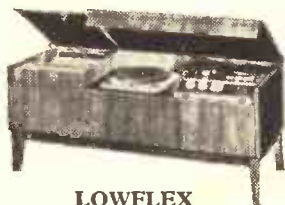
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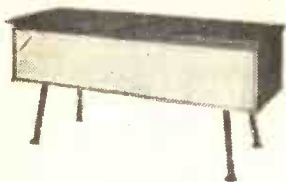
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18	.048	1.219	182
22	.028	.711	536
24	.022	.558	865
26	.018	.46	1,292
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30	.012	.3146	2,730
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