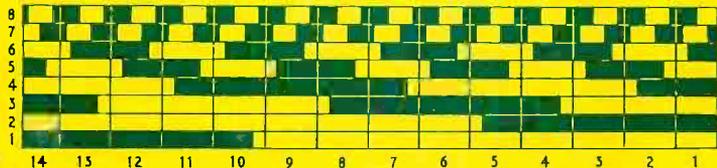


SILICON TRANSISTOR MILLIVOLTMETER

MARCH 1966  
Three Shillings

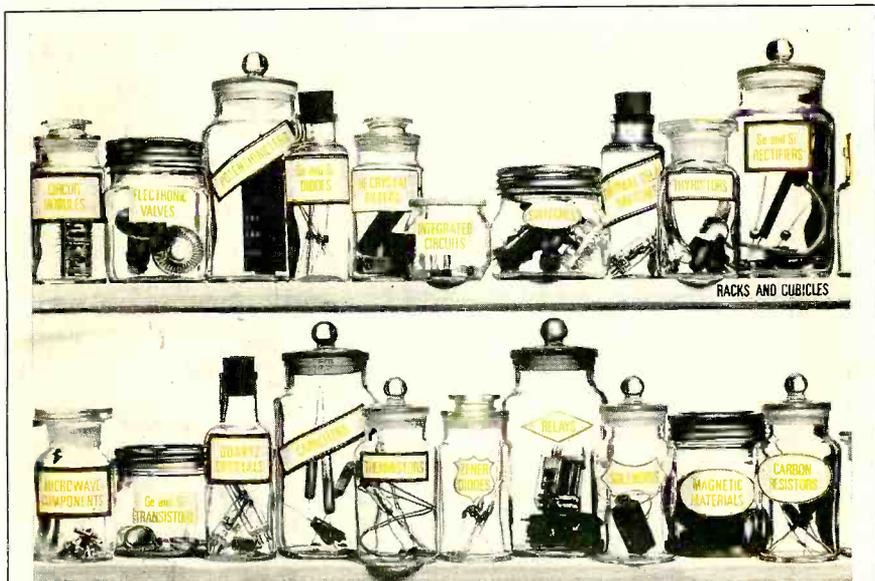
# Wireless World

ELECTRONICS • TELEVISION • RADIO • AUDIO



Coded Television Signals





### Only one-fifth of the story!

Yes, STC Components Group is able to supply you with about five times the number of different types of components shown—*off the shelf*. And the range of components is being extended all the time. If your requirements are urgent, STC Electronics Services Division offers *same day despatch*.

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Wherever your location on the map, STC Components Group, made up of nine successful Divisions and a single mobilized field force, can put the finest components service right on your

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To obtain your copy of the STC 'Designers Digest' write, phone or telex STC Components Group, Footscray, Sidcup, Kent. Telephone: FOOTscray 3333. Telex: 21836.

high-grade components by **STC**  
COMPONENTS GROUP



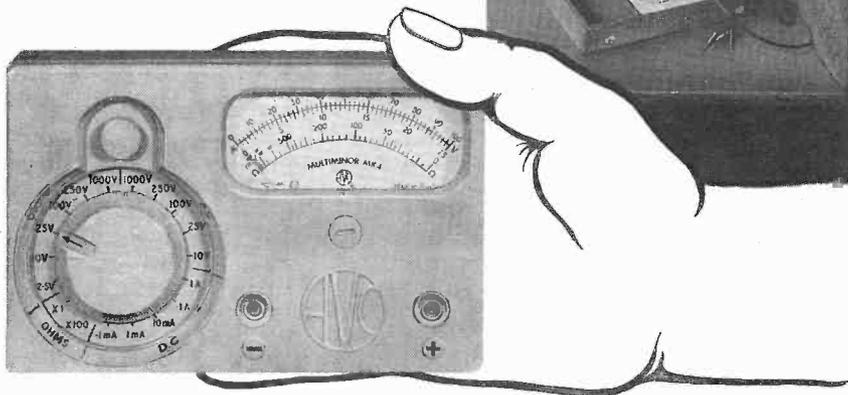
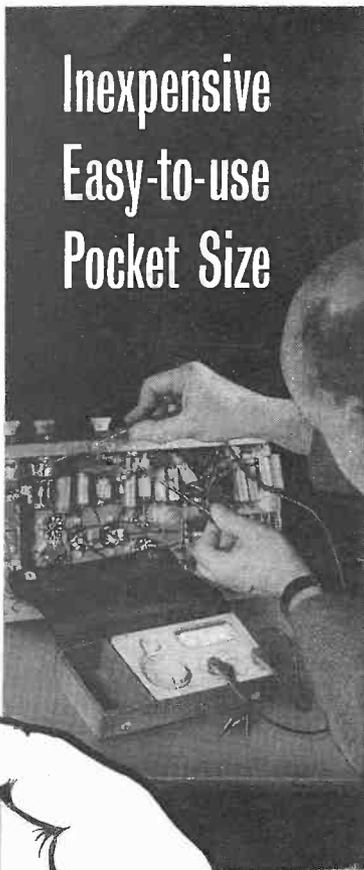
# MULTIMINOR

## Mk4

The Avo Multiminator Mk4 is the latest version of this well-proven multi-range measuring instrument. Designed and assembled to high standards of reliability, the Avo Multiminator offers simple yet instant range selection with a single rotary switch. There is only one pair of sockets for all measurements, and the scale plate is clearly marked for easy reading.

Accuracy is within the limits laid down in B.S.S. 99/1954 for up to  $3\frac{1}{2}\%$  scale length industrial portable instruments.

*Panclimatic construction enables the Multiminator to be used in all types of climatic conditions. The instrument is supplied in an attractive black carrying case, complete with interchangeable test prods and clips, and a multi-language instruction booklet.*



Write for full details.

**AVO LTD** AVOCET HOUSE · 92-96 VAUXHALL BRIDGE ROAD · LONDON S.W.1 Telephone: VICToria 3404

# 'ARKLONE'

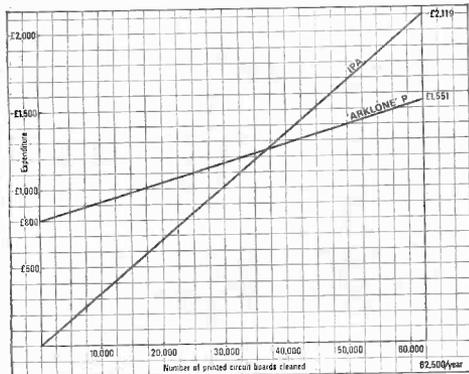
**THE  
COSTLY  
CLEANING  
SOLVENT**

**CHEAP  
AT  
20  
TIMES  
THE  
PRICE**



**First things first:**  
 'ARKLONE' is a pure liquid,  
 boiling point 47°C,  
 chemical nomenclature  
 1.1.2. trichlorotrifluoroethane;  
 non-flammable, non-toxic.

Now for the graph. Well, there was this customer who converted his cleaning process from hand cleaning, using isopropyl alcohol and a team of girls, to a total immersion process using 'ARKLONE' ultrasonically irradiated in a suitably designed plant.



This customer saved £570 on the first year's working after deducting capital cost. And, in fact, probably rather more than this, because the number of rejects formerly produced by harsh solvent action and handling was not known, nor the cost of insurance premiums (isopropyl alcohol is highly flammable and toxic—'ARKLONE' is neither, and makes working conditions safer and more pleasant). His operations are concerned with cleaning printed circuit boards, and 'ARKLONE' is particularly good at that, because it does not attack the metals, plastics, resins and elastomers normally used in this kind of construction.

'ARKLONE' is also first-class at cleaning computer core memories, tape recording and play-back heads, and other components consisting wholly or partly of plastics materials, or containing resins or elastomers—spectacle frames, for instance.

We'll say it again: 'ARKLONE' is a costly cleaning solvent that would be cheap at twenty times the price!

If you want to work out the cost of changing your cleaning process to 'ARKLONE'—get in touch with ICI. One of our representatives will be glad to assist you.

**BEFORE**

Hand cleaning, by girls using alcohol:

	£	s
Capital cost and depreciation	nil	
Labour charges	2083	
Solvent consumption (4 gals. per week at 3/6 per gal.)	36	8
Services	nil	
<b>Total/year</b>	<b>2119</b>	<b>8</b>

**AFTER**

Immersion cleaning with 'ARKLONE',  
 cleaning in batches in an ultrasonic plant  
 operated by one man:

	£	s
Capital cost (plant written off in one year)	800	
Labour charges	500	
Solvent consumption (1 gallon/week at £4.13.9 per gallon)	234	
Services (electricity and water)	17	
<b>Total/year</b>	<b>1551</b>	<b>8</b>

**'ARKLONE'**

'ARKLONE' is the ICI registered  
 trade name for 'ARCTON' 113

IMPERIAL CHEMICAL INDUSTRIES LIMITED, LONDON S.W.1

AR88

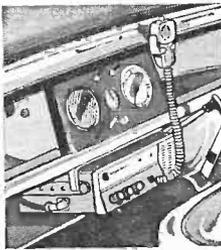
BY APPOINTMENT TO  
H.R.H. THE DUKE OF EDINBURGH



SUPPLIERS OF MOBILE  
RADIO/TELEPHONE EQUIPMENT



# 'CAMBRIDGE' transistor Mobile Radiotelephone



## A new high standard in Mobile Radiotelephone design

- Fully transistorised receiver
- Printed circuit sub-assemblies
- Sealed I.F. block filters
- Dustproof and splashproof
- GPO approved and meeting American and European specifications
- 100 Milliamps receiver drain
- A.M. or F.M. versions
- 25 Kc/s or 50 Kc/s channelling
- Single or six channel

**PYE TELECOMMUNICATIONS LIMITED**

CAMBRIDGE · ENGLAND · TELEPHONE: TEVERSHAM (CAMBRIDGE) 3131 · TELEX No. 81166  
WW-006 FOR FURTHER DETAILS.

# THE Bantam

TWO-WAY RADIOTELEPHONE

*a Fully Transistorised  
Walkie-Talkie!*

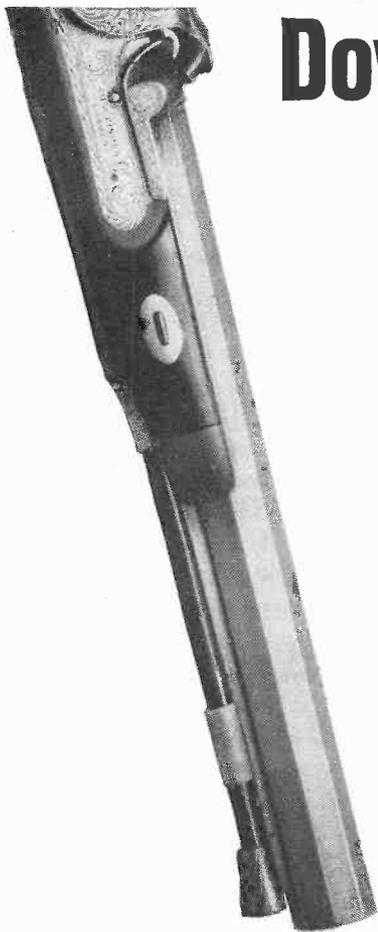


In the tradition of the outstanding Cambridge and Vanguard Radiotelephones, Pye have produced the Bantam, a brilliant fully transistorised Walkie-Talkie.

- Fully transistorised Transmitter and Receiver
- Long endurance with Rechargeable or Dry Batteries
- Crystal Filter selectivity
- Reliability and accessibility of components
- Very high performance Receiver
- Lightweight 4 lbs. (1.82 kg.)
- Frequency Band 25-174 Mc/s.
- Weatherproof
- Air Registration Board approved for light aircraft category III
- Approved by G.P.O. to Spec. W6345
- Intrinsically safe version available

**PYE TELECOMMUNICATIONS LTD.** CAMBRIDGE, ENGLAND. TEL. TEVERSHAM 3131 Telex No. 81166

# Down to 300 $\mu$ V



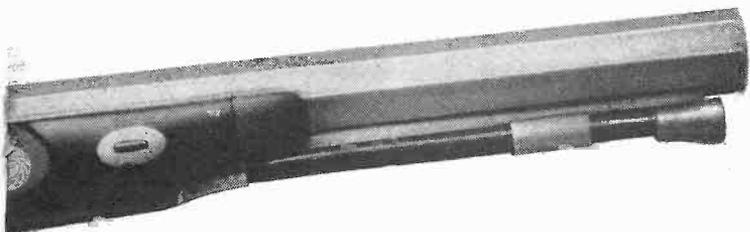
**Marconi Instruments  
present a new  
challenge in VHF  
voltage measurement**

## **VHF ELECTRONIC VOLTMETER TYPE TF 2603**

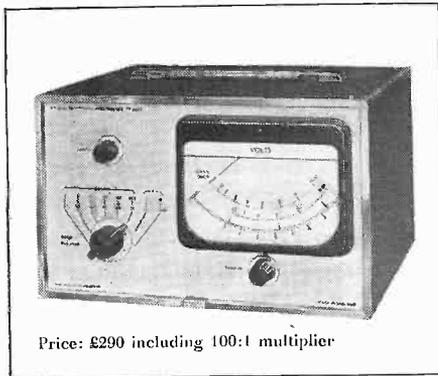
An entirely new, fully transistorised millivoltmeter for direct voltage measurement from 300  $\mu$ V to 3V at frequencies up to 1,500 Mc/s, and up to 300V at 500 Mc/s. The  $\frac{1}{2}$ -inch diameter probe uses a pair of fast germanium diodes in a full-wave circuit. Response is close to r.m.s. with inputs of less than 30 mV and peak in the 0.5V to 3V region. Accessories include a 100:1 multiplier for measurements up to 300V.

WW-008 FOR FURTHER DETAILS.

# up to 1500 Mc/s



Targeted for the real  
needs of the electronic industry



Price: £290 including 100:1 multiplier

- Low-level signal measurement in semi-conductor circuits
- Measurement of transistor parameters
- Voltage measurement on strip-line circuits
- Measurements at locations remote from mains supplies
- Elimination of measurement errors due to circuit earth loops
- Noise measurements. Distortion measurements
- Impedance measurements at low voltage using a Circuit Magnification Meter
- Detection of unwanted oscillations in wide-band amplifiers
- Tuning narrow-band amplifiers
- Testing frequency response in filters
- Null detection in wide-band bridge measurements

*Please write or telephone for full technical and commercial information about this new instrument. On specification, performance and value-for-money, Marconi instruments challenge comparison with any in the world.*

A GOOD NAME FOR GOOD MEASURE

## MARCONI INSTRUMENTS

Marconi Instruments Limited  
Longacres, St. Albans, Herts.  
Tel: St. Albans 59292 Telex: 23350

TREBLE



BASS



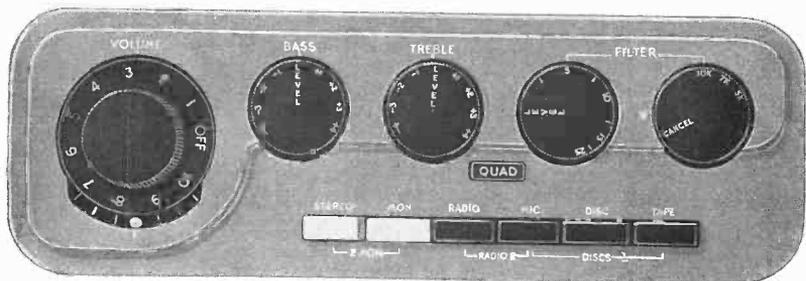
## musical balance

All amplifiers—or nearly all—have bass and treble controls. All bass and treble controls, not unnaturally, increase and reduce the bass and treble, but here the similarity ends!

The bass control on the QUAD varies both slope and turn-over in four frequency discriminative networks of equal impedance. The channels are locked to eliminate phase-shift so that the stereo image is maintained at all settings. The treble operates midway between variable slope and variable step so that it is possible to adjust musical brilliance while maintaining natural harmonic balance.

A Level position may be selected within 0.5 dB 20-20,000 c/s, while other settings are guaranteed within  $\pm 1.5$  dB of the published calibrations.

Of course, when programme sources become consistently good, tone controls will not be necessary, but meanwhile how is musical balance achieved on your amplifier?

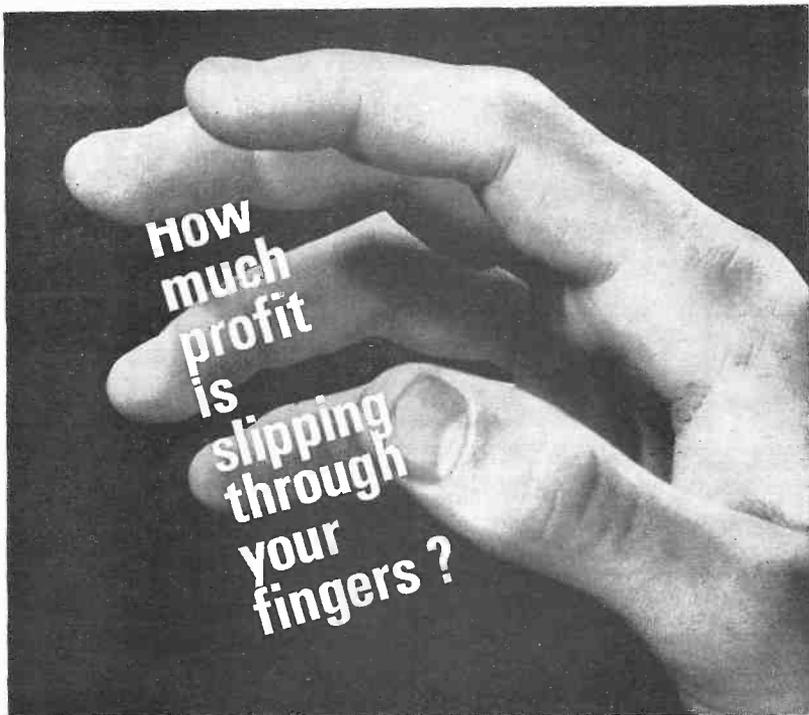


*For the closest approach to the original sound.*

Our slogan for fifteen years and our design objective for twice that long. Ask your dealer for details of the QUAD range of high fidelity units or write direct to Ref. W.W. Acoustical Manufacturing Co. Ltd., Huntingdon. Huntingdon 361.



W.W.—010 FOR FURTHER DETAILS.



## everyone can mechanize and profit . . .

Business may be brisk, with everyone working; but where are all the profits? Something is robbing your company of its expected returns. Labour costs are rising 8% a year; values of factory space and production machinery are rising fantastically. Under-utilization of these high-cost productive elements through inefficient handling operations is your worst enemy, and British industry is estimated to waste £800 million yearly in this way. Even if your business is not large, don't ignore the

big savings possible with mechanized handling. Many new ideas are discovered at every Mechanical Handling Exhibition—a survey in 1964 revealed that 47% of visitors had seen something new. Mechanization is your best investment—simple low-cost devices often produce remarkable results. See thousands of new ideas from over 300 exhibitors at the Mechanical Handling Exhibition, Earls Court, 10-20 May. Don't miss this important event—mail the enquiry coupon now.

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10/20 MAY, 1966, EARLS COURT, LONDON

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To the Manager, Mechanical Handling Exhibition,  
Dorset House, Stamford Street, London, S.E.1

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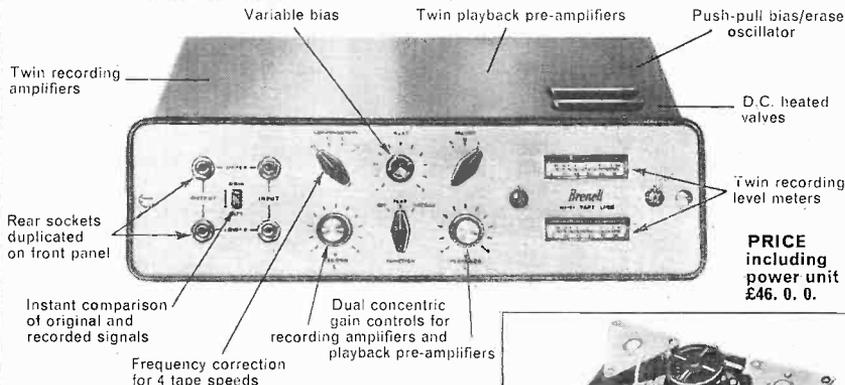
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# HERE'S VERSATILITY FOR YOU...

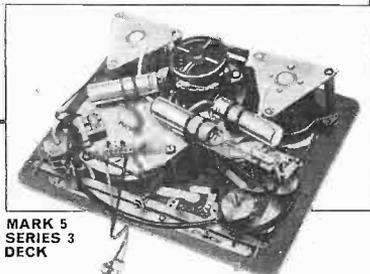
## The **Brenell** MONO/STEREO HI-FI TAPE LINK



**PRICE**  
including  
power unit  
£46. 0. 0.

Designed for use with 2½ or 2¼ track heads

Built to the same high standards as our tape recorders and decks this HI-FI TAPE LINK has been developed for use with your high fidelity equipment. It is capable of giving superb results when matched to one of our Mark 5 Series 3 decks fitted with the appropriate heads. Write for full details of this amplifier and deck and complete range of tape recorders.



**MARK 5  
SERIES 3  
DECK**



**MARK 5  
SERIES 3**

**MONO—HALF TRACK—TWO HEADS—  
MAGIC EYE**  
(Available with recording level meter at extra cost.)

High quality amplifier with power output of 2½ watts r.m.s. and a frequency response of 40–20,000 c/s—can be used independently of tape recorder—narrow gapped record/playback head for extended frequency response—double napped ferrite erase head to minimise erase noise—headphone monitoring.



**MARK 5  
TYPE M SERIES 3**

**MONO—HALF TRACK—THREE HEADS—  
RECORDING LEVEL METER**

Separate record and playback heads—separate record and playback amplifiers—amplifier frequency response 25–26,000 c/s ±3dB—power output 2 watts r.m.s.—separate bass and treble controls—mixing of input signals—speaker monitoring whilst recording.



**STB2**

**MONO/STEREO—HALF TRACK (Record/  
playback)—QUARTER TRACK (playback)**

**FOUR HEADS—TWO EDGEWISE METERS**  
Designed for use with high fidelity stereo installations—adjustable attenuators on all input channels to ensure perfect matching with all auxiliary equipment—dual concentric recording level and playback level controls—cathode follower output—four channel mixing on mono programme sources—twin recording and twin playback pre-amplifiers—comparison of original and recorded signal—adjustable bias level—recording facilities for 1½ and 2½ track—playback facilities for 1½, 2, 1¼ and 2¼ tracks—sound-on-sound facilities—two edgewise meters for recording level, tape output level and bias level. **Optional extra: stereo power amplifiers and monitoring speakers.**

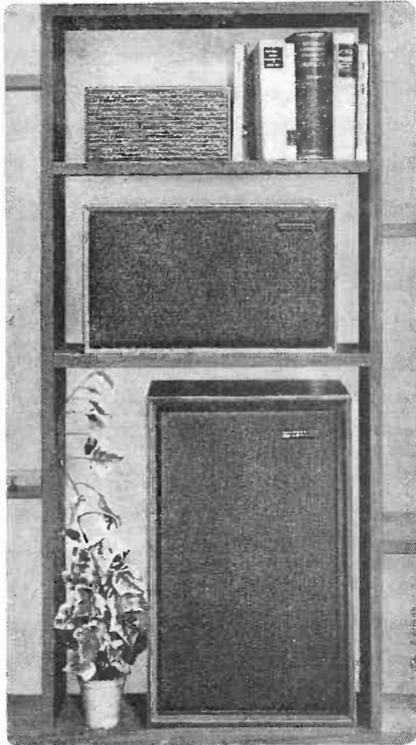
# Brenell

**BRENELL ENGINEERING CO. LTD.**  
231/5 Liverpool Road, London, N.1.  
Telephone: NORTH 8271 (5 lines)

WW-012 FOR FURTHER DETAILS.

# GOODMANS 'M' RANGE HIGH FIDELITY LOUDSPEAKER SYSTEMS

There is a Goodmans Complete High Fidelity Loudspeaker System to meet your requirements—to fit unobtrusively into your living room—to blend with your furnishings—enabling you to enjoy the finest quality sound reproduction, whichever System is your choice.



### MAXIM

A fine High Fidelity Loudspeaker system complete, the size of a shoe-box—104" x 51" x 7 1/2". The meticulously finished cabinet in hand-rubbed teak (or walnut) houses two tiny precision direct radiator drive units which cover the frequency range—45-20,000 c/s with less deviation from level response than almost any other High Fidelity Loudspeaker—and handle 8 watts of power easily. No problems in finding room for it—just shove a couple of books.

#### Specification

Dimensions	104" x 51" x 7 1/2" deep
Range	45-20,000 c/s
Power	8 watts
Impedance	15/16 ohms
Finish	Teak or Walnut

Price: £17. 10. 6. (inc. P.T.)

### MEZZO

Handles 15 watts of power—yet measures only 10 1/2" x 18 1/2" x 8" deep—the MEZZO will go in your bookshelf. The styling is restrained yet distinctive, making MEZZO an "easy" addition to any design-conscious furnishing scheme. The frequency range is a clear and clean 40-20,000 c/s with a control and smoothness accounted for by two newly developed and patented loudspeakers. The 8" bass unit is of very advanced design and construction, and is particularly notable for its very low distortion and extraordinary smoothness of performance. It is claimed to be the smoothest bass reproducer of its size ever produced. The treble unit completes the quality picture to give an overall performance unrivalled in a reproducer of this size. The L.C. crossover network operates at 2,200 c/s. The distortion level is extraordinarily low. The perfectly controlled balance of the MEZZO sound make it—the Loudspeaker to Live With.

#### Specification

Dimensions	10 1/2" x 18 1/2" x 8" deep
Range	40-20,000 c/s
Power	15 watts
Impedance	Suitable for 8 ohm—15 ohm amplifiers
Distortion	Less than 1% total harmonic at 30 c/s and above, for unaided pressure level of 80 db at 6 ft.

Finish Teak or Walnut to order

Price: £26. 5. 0. (inc. P.T.)

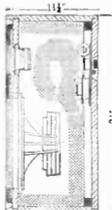
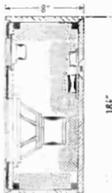
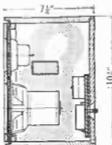
### MAGNUM-K

Designed to a very high standard for professional purposes, the MAGNUM-K brings this same standard to the audio enthusiast at home. It is a three-way system, and although reasonably compact (15" x 24" x 11 1/2") no performance compromises have been accepted. Every detail that could contribute to really accurate sound reproduction has been included. A new and patented 12" Bass reproducer gives minimal distortion down to 20 c/s. The Mid-range and High Frequency units are high efficiency direct radiators outstandingly smooth in performance. Multiple-section crossover network operates at 1,500 and 6,000 c/s and constant impedance controls for both middle and high frequency units permit individual balancing of the system. Power handling is 25 watts, but for domestic use amplifiers from 6 to 12 watts are quite adequate.

#### Specification

Dimensions	24" x 15" x 11 1/2" deep
Range	30-20,000 c/s
Power	25 watts
Impedance	8 ohms
Finish	Teak or Walnut to order

Price: £36. 15. 0.



### ELEGANZIA II

A full-sized 15 watt 2-speaker High Fidelity Loudspeaker system with the enormous advantage of a depth of ONLY 4 1/2". A classic example of slim, graceful efficiency, its exceptionally accurate performance was designed for the connoisseur. The 12" bass unit employs Goodmans exclusive SUPRIFOAM diaphragm. An L.C. crossover network transfers the electrical drive above 500 c/s to a back-loaded mid-range and high-frequency unit.

#### Specification

Dimensions	27" x 22" x 4 1/2" deep
Range	15-15,000 c/s
Power	15 watts
Impedance	15-16 ohms
Finish	Teak or Walnut

Price: £27. 10. 0.

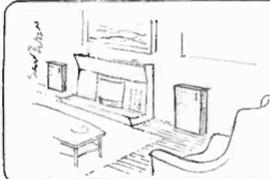
SEE AND HEAR them at your Goodmans Dealer

**FREE** Please send me a free copy of Goodmans High Fidelity Manual.

Name

Address

W.W.W.





## NEW SHAPES OF SOUND



### The Goldring-Lenco GL 68

The many proved features of Goldring-Lenco transcription units such as infinitely variable speed adjustment, pick-up lowering device, automatic idler wheel disengagement are retained on the GL 68, which is the first unit to incorporate the new G.65 arm. This is of low mass tubular construction with stylus pressure adjustment by sliding counterweight, and provision for height adjustment to suit any chosen cartridge. The interchangeable head slide (taking all cartridges with standard  $\frac{3}{8}$ " fixing centres) makes use of self-cleaning wiper contacts. Swiss precision motor. Continuously variable speed adjustment. Less than 1% speed variation for 13% mains voltage variation. Adjustable click-in positions for the four standard record speeds. Pick-up raising/lowering device coupled to on/off switch. Automatic disengagement of idler wheel. Full 12" diameter turntable. Wired for stereo.  
GL 68 Transcription Unit £16.16.0d. + £2.14.7 P.T.

Recommended cartridges for the GL68 are: Pickering V15 (AM1 and AME1) Pickering 380A, Goldring CS90 & CS91E.

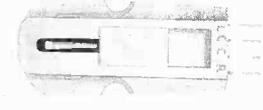


**Pickering V15 AM1 and AME1 Micro-Magnetic Cartridge**  
Weighing only 5 gm., these high output, high compliance stereo—mono cartridges are perfect for low mass arms. 15° tracking angle gives minimum distortion. Hermetically sealed. Replaceable push-in diamond stylus assembly, with retracting stylus arm for added protection to records (0.0007" tip radius for V15/AM1 and elliptical, with even higher compliance, for V15/AME1).  
V15/AM1 £9.9.0d. + £1.10.9d. P.T.  
V15/AME1 £13.15.0d. + £2.4.8d. P.T.



**Pickering 380A Cartridge**  
Moving-magnet for exceptional mono or stereo reproduction. Features the exclusive V-guard push-in diamond stylus unit which prevents damage through accidental dropping of arm on record. The Pickering 380A ensures high channel

separation and virtually eliminates needle talk, hiss or distortion. Hermetically sealed, it tracks at 2 gm., faultlessly reproduces the most exacting records.  
£12.12.0d. + £2.0.11d. P.T.



**Goldring CS90 and CS91E Cartridges**  
These are stereo ceramic cartridges with excellent frequency response and cross-talk separation. Low tip mass, replaceable diamond stylus (CS90—0.0005" or 0.0007" tip radius; CS91E—elliptical) coupled with high compliance enables these cartridges to be played at light tracking weights. CS 90 £4.4.0d. + £0.13.8d. P.T.  
CS91E £6.6.0d. + £1.0.6d. P.T.

**C68 Cabinet and Cover for GL68.**  
Elegant sapele mahogany cabinet with removable, clear Perspex dust cover.  
Size: 14" x 17" x 7".  
£8.19.6d. + £1.12.0d. P.T.



Goldring Manufacturing Company (G.B.) Ltd.,  
486-488 High Road, Leytonstone, London, E11  
Telephone: Leytonstone 8343

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# INCREASE THE SENSITIVITY OF YOUR OSCILLOSCOPE, VOLTMETER OR COUNTER



The TA401 is similar to the TA601 as illustrated

TA605  
ACTUAL  
SIZE

SPECIFICATIONS	TYPE TA401	TYPE TA601	TYPE TA605
GAIN	40dB 0.1dB	60dB ± 0.1dB	20, 30, 40, 50 and 60dB ± 0.2dB
BANDWIDTH ± 3dB	1c/s-3Mc/s	3c/s-1.2Mc/s	20-40dB, 1c/s-3Mc/s; 50dB, 2c/s-2Mc/s; 60dB, 4c/s-1.5Mc/s.
BANDWIDTH ± 0.3dB	4c/s-1Mc/s	10c/s-300kc/s	20-40dB, 4c/s-1Mc/s; 60dB, 10c/s-300kc/s.
INPUT IMPEDANCE	> 5MΩ < 40pF from 100c/s to 1Mc/s	> 1MΩ < 50pF from 100c/s to 300kc/s	> 5MΩ < 40pF from 100c/s to 300kc/s
INPUT NOISE	< 15μV, zero source < 50μV, 100kΩ source	< 15μV, zero source < 40μV, 100kΩ source	As TA401 and TA601 at 40dB and 60dB
POWER SUPPLY	PP3 battery, life 100 hours		PP3 battery, life 1,000 hours, or A.C. Power Unit
AVAILABLE OUTPUT	1V up to 1Mc/s, 300mV at 3Mc/s, into load of 100kΩ & 50pF		1V up to 3Mc/s into 100kΩ and 50pF
OUTPUT IMPEDANCE	100Ω in series with 6.4μF		
SIZE & WEIGHT	3in. × 1in. × 1½in. 7 oz.		2½in. × 4in. × 5½in. 2½lbs.
PRICE with battery and input lead	£17 0 0	£17 0 0	£27 0 0

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PORTABLE INSTRUMENTS

Fully detailed leaflets are available on our complete range of portable instruments.

**LEVELL ELECTRONICS LTD.**

PARK ROAD, HIGH BARNET, HERTS. Telephone: Barnet 5028

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and Microphone stands  
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Complete Line of Replacement Semiconductors

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**CADRE** Electronic Corp.

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Magnetic  
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Series 270 — Low Print Through  
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Studios  
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Tapes  
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the Amateur and Experimenter

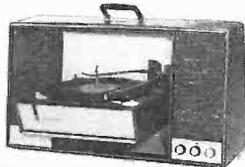
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**AMPEX** 4-track Stereo Tapes •  
Pre-Recorded Tapes • Extensive Library • Most Labels  
• Available From Stock • Immediate Delivery

**GOLDEN SHIELD CORPORATION,**  
Manufacturers of Stereo Phonographs and Table Radios

Quality & Design  
AM-FM Radios

Automatic Record  
Changer Phonographs



from  
**terado**  
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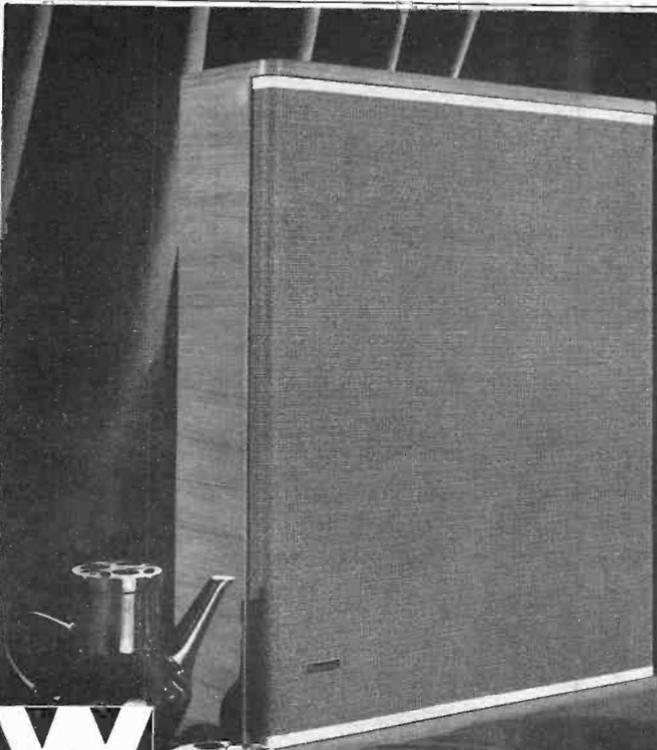
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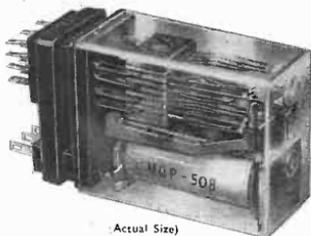
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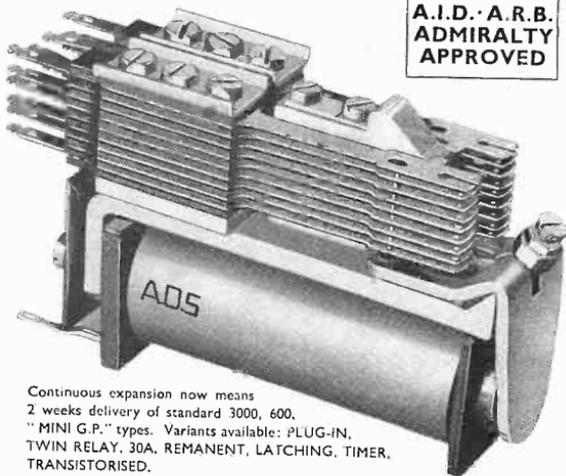
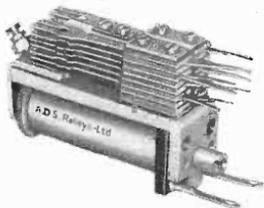
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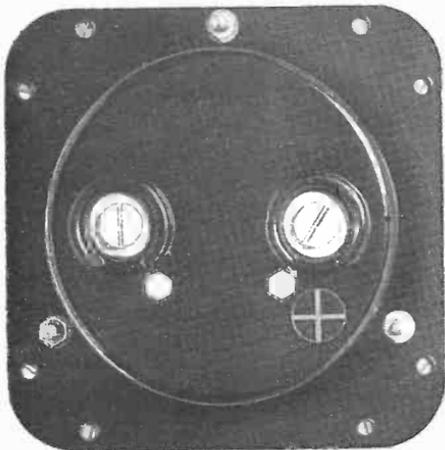
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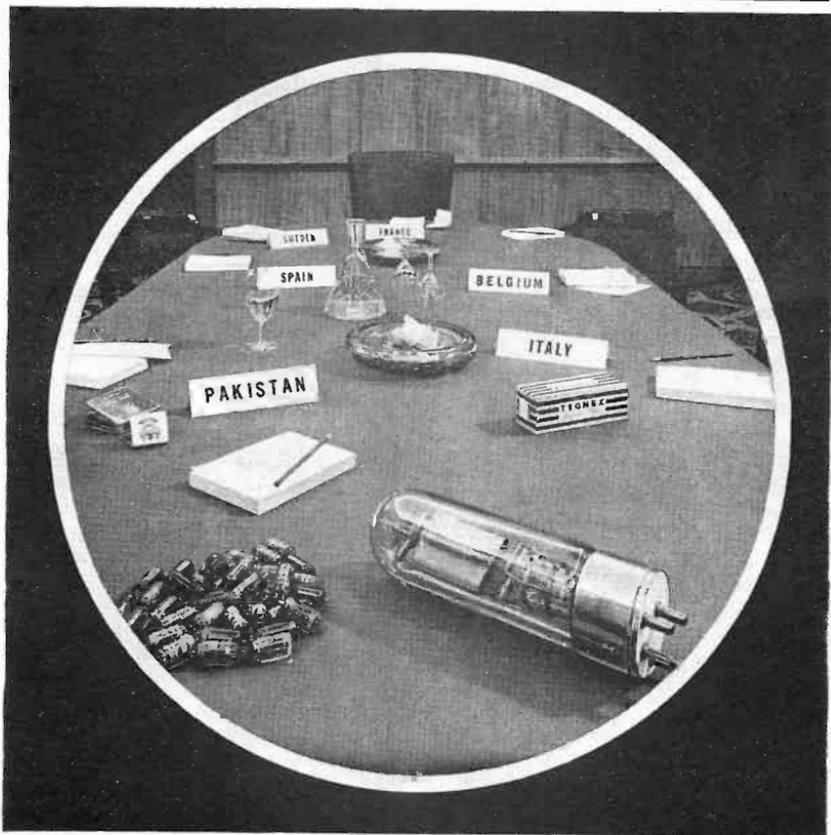
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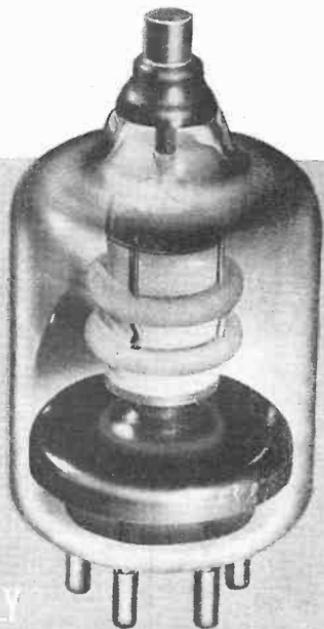
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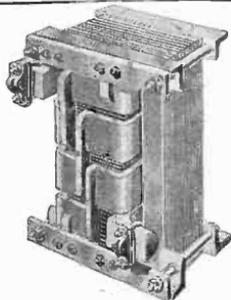
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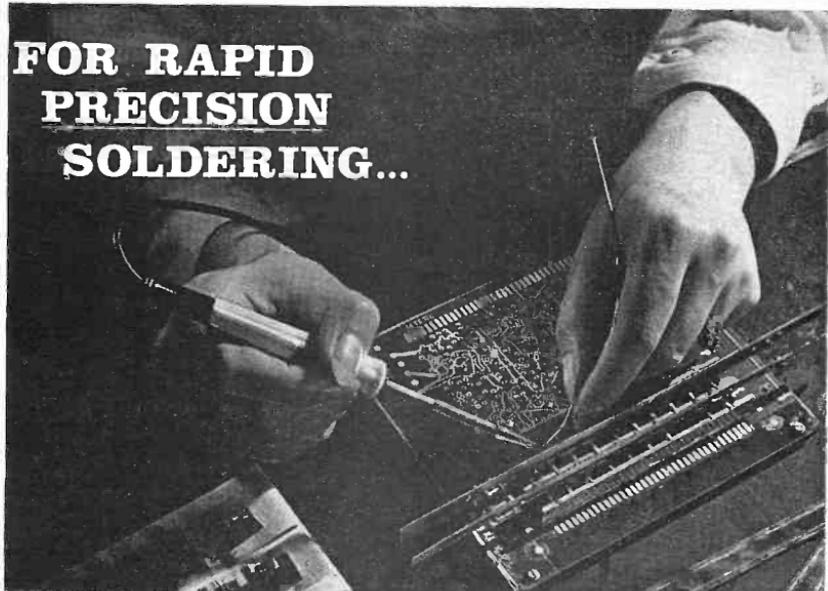
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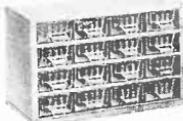
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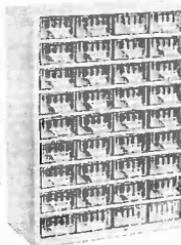


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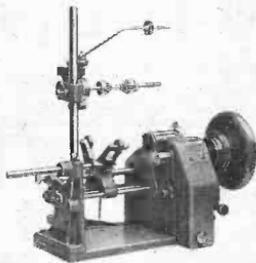
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# SUBMINIATURE CO-AXIAL CONNECTORS

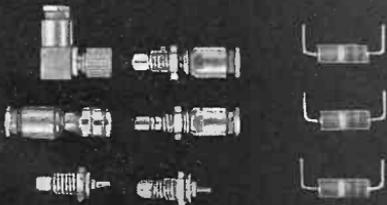
TO PATTERN 17 OF  
DEF 5322-A & A-4

## SPECIFICATION

- Designed to DEF 5322-A & A-4
- Max. frequency : 3 Gc/s
- Temperature category T6 ( $-55^{\circ}\text{C}$  to  $+125^{\circ}\text{C}$ )
- Humidity category H6
- 50 ohms impedance
- Field-serviceable, with improved cable clamping
- Push-on and screw-on types
- Captivated centre contacts

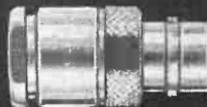
Illustrations, actual size

## PLUS SPACE SAVING



Amphenol sub-miniature co-axial connectors compared with one-tenth watt resistors. Illustrations actual size

EXAMPLES FROM OTHER  
AMPHENOL CONNECTORS TO DEF 5322-A & A-1/3



PATTERN 14  
(SEALED)

Illustrations actual size



PATTERN 15  
(UNSEALED)

PATTERN 16  
(SEALED)

Space-saving, weight-saving Amphenol 'Subminax' RF Connectors are designed for easy fitting to cables 'in the field' without special tools. They feature a new cable clamping fitment to meet the higher pull-out strength now specified in DEF5322A & A-4. Centre contacts are mechanically retained in position and do not rely on a soldered joint to the centre conductor.

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or order straight away, working out total area of material  
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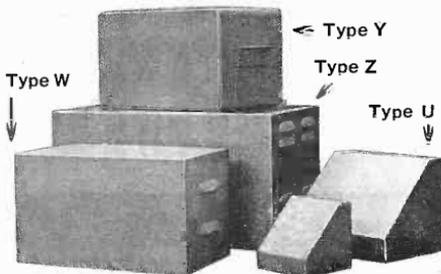
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112 sq. in. 6/6	240 sq. in. 11/2	368 sq. in. 15/9
144 sq. in. 7/9	272 sq. in. 12/6	and pro rata.

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U	15 x 9 x 9"	44/6	Y	15 x 9 x 7"	48/6
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W	12 x 7 x 7"	34/-	Z	19 x 10 x 8 1/2"	71/-
W	15 x 9 x 8"	44/-		*Height	

Plus post and packing

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CHP 1

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The LANCON I.S. has been developed from the extremely successful LANCON—the largest selling all-British pocket VHF radiotelephone.

### LANCON I.S.

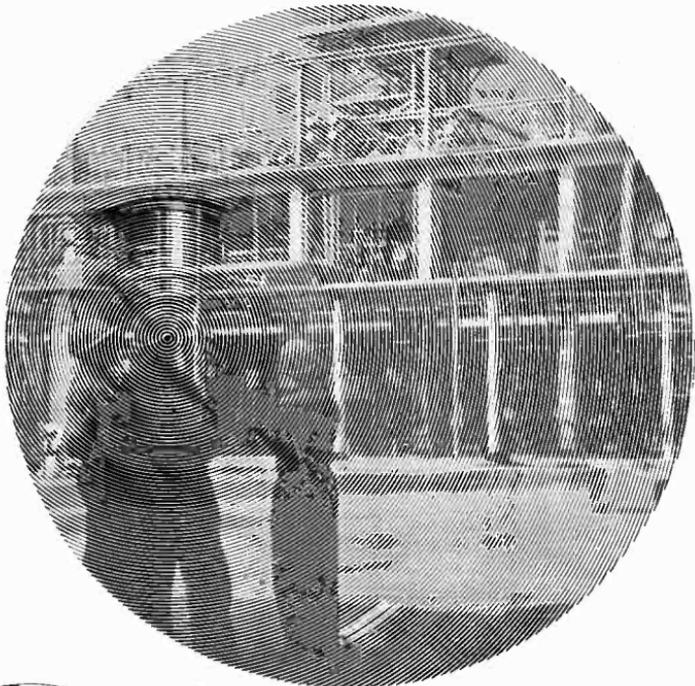
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- Completely concealed, patented

aerial system—avoids dangers of conventional trailing or extending aeri-

- Certificate No. 2735 covers Classes 2a, 2c, 2d

- Powered by rechargeable 12V battery—range up to 5 miles.

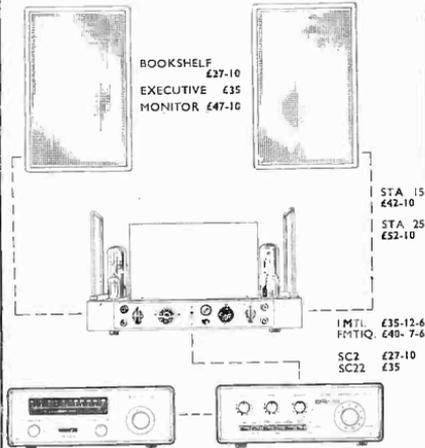
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For further information, please contact:  
**G.E.C. (ELECTRONICS) LTD.**, Radio Communications Group, Span Street, Coventry, Tel. Coventry 22027  
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High signal to noise ratio (no hum, no noise at maximum or any listening level); smooth and noiseless tone, volume and balance controls with virtually infinite life; concrete TIAA equalisation for correct response monitor; accurate tone control; potentiometers for flat response at zero position; flexible input and output level handling capacity to ensure low distortion under all conditions of use.

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Exceptionally smooth response achieved by using the best drive units obtainable and equalising them with complex networks (note the lack of jitters, fatigue after long listening periods, and directional stability in stereophony); wide-angle response (note that you can listen anywhere in the room with the same frequency balance with perfect integration on a stereo programme); lack of coloration (note the naturalness in voice reproduction and absence of boom at low frequencies).

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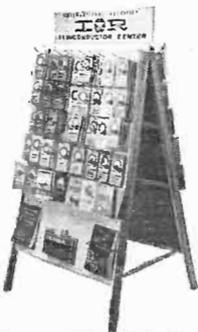
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## OUTPUT PER CHANNEL

10 watts R.M.S. into 15 ohm load.

15 watts R.M.S. into 3.75 ohm load.

## TOTAL HARMONIC DISTORTION

0.1% at 5 watts R.M.S.

0.2% at 10 watts R.M.S.

1,000 c.p.s.

## DAMPING FACTOR 20

FREQUENCY RESPONSE

± 1 db. 20-20,000 c.p.s.

## HUM AND NOISE

-80 db.

## CROSS TALK

-42 db. to -53 db.

## MAINS INPUT SELECTION

160-110-120-200-240-220-240 v.

50/60 c.p.s.

## SEMI-CONDUCTORS (per channel)

AC107, OC44(3), OC81Z(2), OA5, OC12Z

AD14(2)

## INPUT SENSITIVITIES

For 10 watts R.M.S. into 15 ohms

Pick-up Magnetic 3.5 mv. 221 r.p.m.

Pick-up Crystal/Ceramic 490 mv. 7 mv. 78 r.p.m.

Microphone 5 mv.

Tape Head 2 mv.

Aux. (Radio, Tape, Ceramic P.I. etc.) 100 mv.

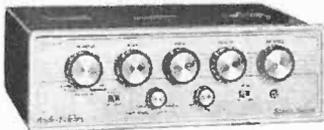
(Above sensitivities will be doubled when

output load is 3-4 ohms)

## BASS CONTROLS

+ 11db to - 16 db. at 40 c.p.s.

Incorporation of the very latest Mullard Transistors has made possible the really outstanding performance figures of this brilliant design. Compare them with other leading makes currently available.



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THE PRE-AMPLIFIER IS A COMPLETELY NEW DESIGN

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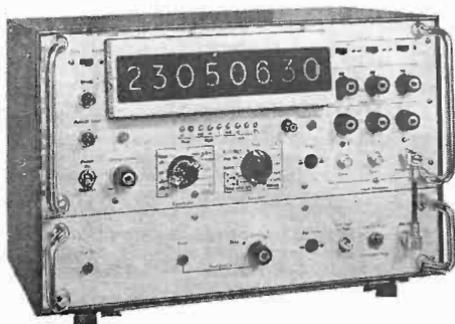
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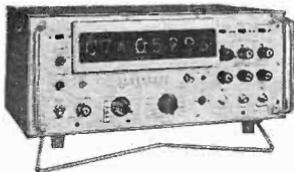
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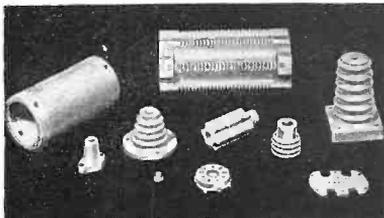
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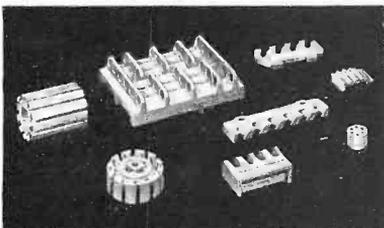
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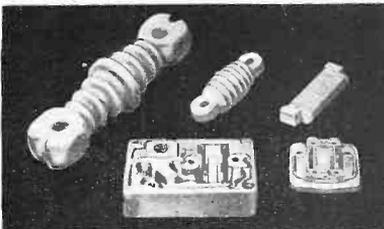
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2S322-2S302	-40v	15-60	5/5 QUANTITIES
2S323-2S303	-25v	25-85	9/3 ASK FOR A
2S324-2S304	-15v	45-150	13/6 QUOTATION

# QUARNDON ELECTRONICS LTD

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TELEX 37163

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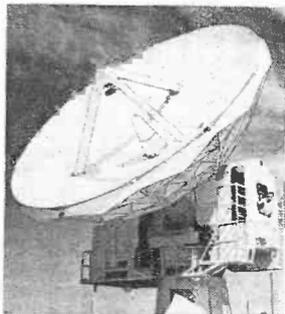


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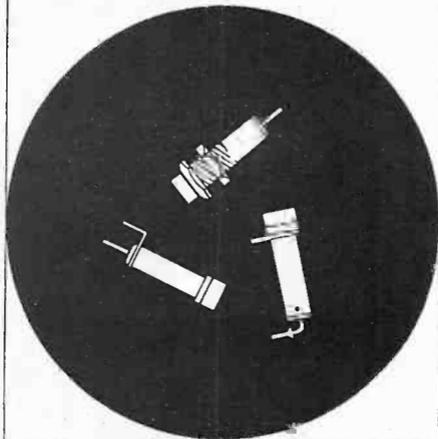
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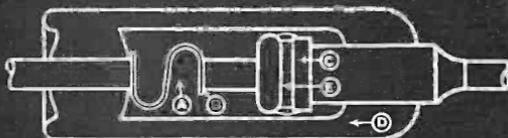
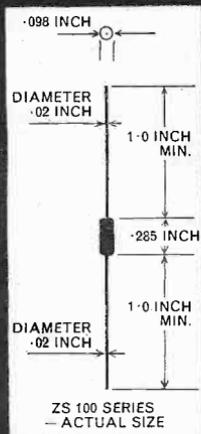
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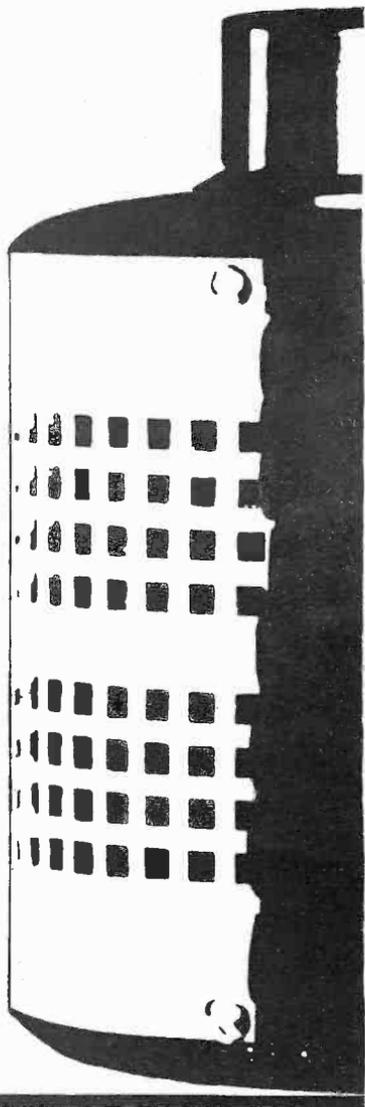
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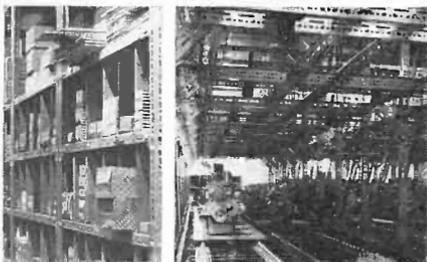
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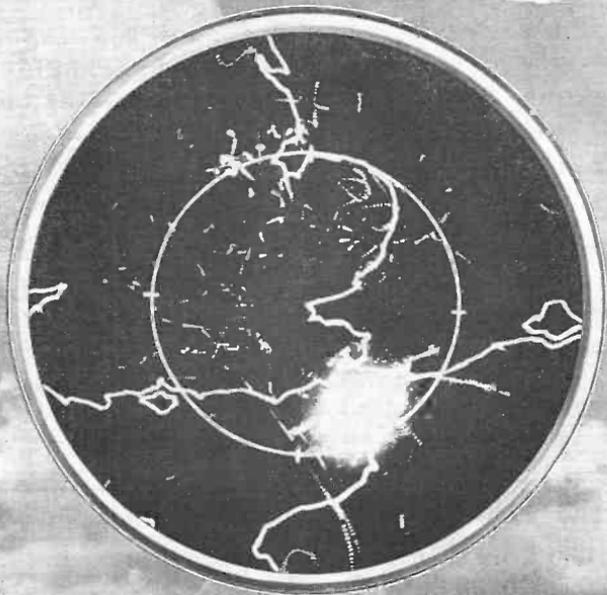
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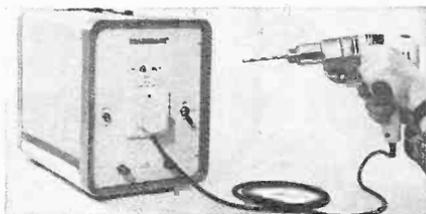
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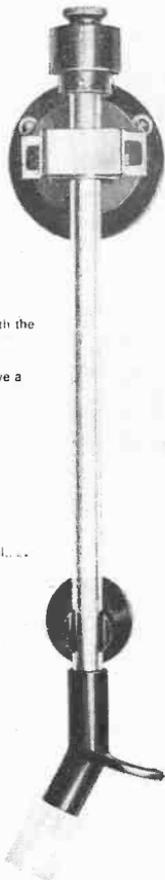
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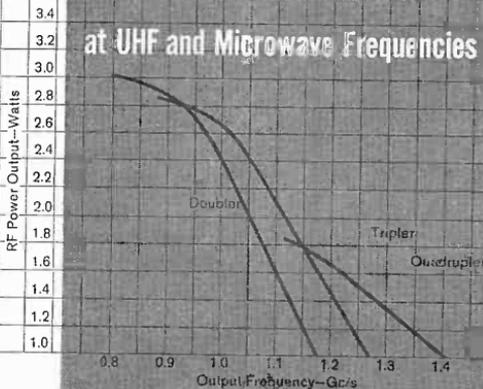


TO-60

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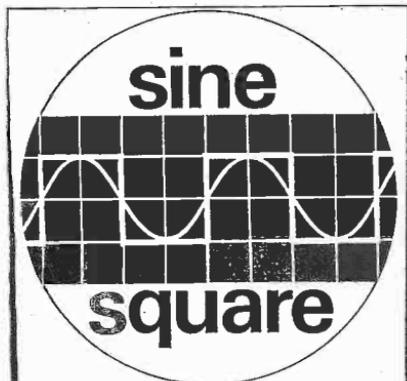
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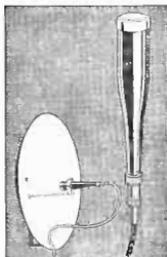
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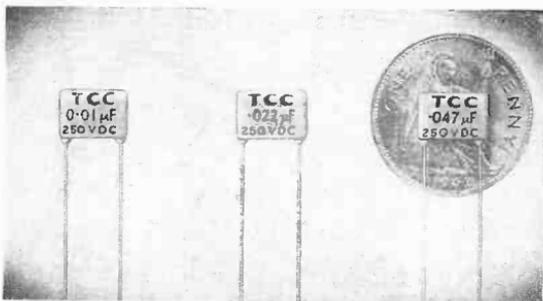
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Tel: RIC 3285 or 9352

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## MINIATURE METALLIZED POLYESTER CAPACITORS

These small moulded metallized polyester capacitors are ideally suited to the applications of printed wiring panels and transistorised circuits. The use of the new dielectric material and unique construction combine the advantages of small physical size and superior electrical characteristics which meet the requirements of H.5 DEF.5011 Specification.

### CONSTRUCTION

The windings are virtually non-inductive and the wire terminations are soldered direct to the metal electrodes eliminating contact resistance and ensuring the minimum possible inductance.

**Cap. Tolerance:**  $\pm 20\%$ .

**Voltage Rating:** Peak ripple voltage and D.C. voltage must not exceed rated D.C. voltage.

**Power Factor:**  $\leq 0.01$  at 1 kc/s. at  $+20^\circ\text{C}$ .

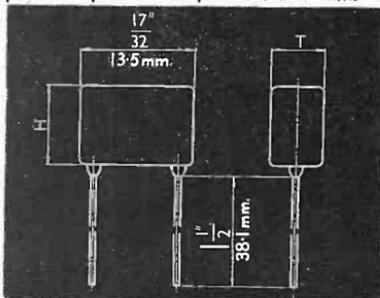
**Temperature Rating:** Suitable for working at  $+85^\circ\text{C}$ . without derating.

**Insulation Resistance:** 10,000 megohms or 2,000 ohm farad, whichever is less.

**Terminations:** 22 SWG solder-coated parallel wires for vertical mounting.

**Finish:** Insulated—special non-cracking heat resisting thermosetting compound providing good insulation and good protection against the ingress of moisture.

Capacitance $\mu\text{F}$	Dimensions		T.C.C. Type No.
	H	T	
250 V. D.C. at 85°C. working			
0.01	11.32in. 9mm	7.32in. 5.5mm	FMX1
0.015	11.32in. 9mm	7.32in. 5.5mm	FMX7
0.022	11.32in. 9mm	7.32in. 5.5mm	FMX2
0.033	11.32in. 9mm	7.32in. 5.5mm	FMX5
0.047	11.32in. 9mm	7.32in. 5.5mm	FMX3
0.068	7.16in. 11mm	9.32in. 7.2mm	FMX8
0.1	7.16in. 11mm	9.32in. 7.2mm	FMX4
400 V. D.C. at 85°C. working			
0.01	11.32in. 9mm	7.32in. 5.5mm	FMX41
0.022	11.32in. 9mm	7.32in. 5.5mm	FMX42
0.033	7.16in. 11mm	9.32in. 7.2mm	FMX45
0.047	7.16in. 11mm	9.32in. 7.2mm	FMX43



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also at CHESSINGTON, SURREY and BATHGATE, SCOTLAND

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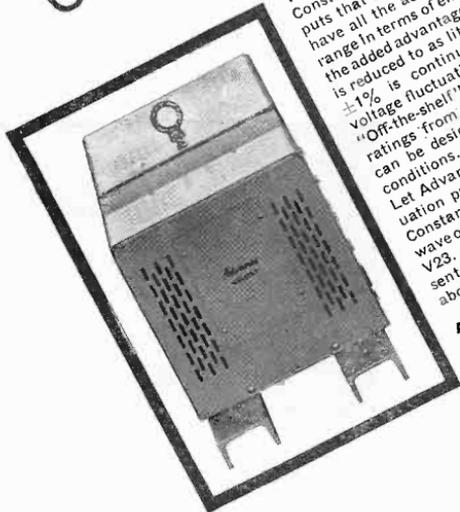
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- PERIOD (Single and multiple period measurements up to  $10^3$  periods)
- TIME ( $3\mu\text{s}$  -  $10^5\text{s}$ )
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10 c/s to 100 Kc/s in four decade ranges.  
Scale  $4\frac{1}{2}$ " dia. 180° rotation.

**Three outputs.**

- 0-6 v. r.m.s. SINE WAVE with low distortion.
- 0-9 v. peak to peak SQUARE WAVE with no droop and good H.F. rise time.
- 0-1 watt into 3 ohms, 50 c/s to 20 Kc/s.

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- Amplifier output available at low impedance with voltage gain of approximately 80 times on most sensitive range.
- D.C. range 0 to 400 v. in three ranges.

Isolated from case.  
Impedance 20 Kilohms/volt.  
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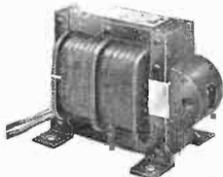
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**one small cabinet  
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cut out the 'bits and pieces' and get the resistor situation under control

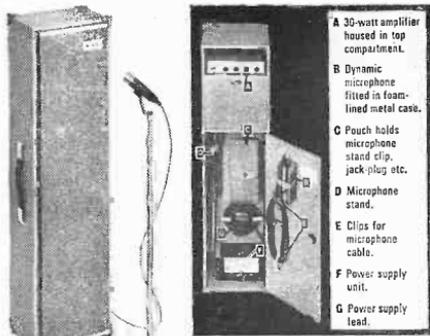
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- D Microphone stand.
- E Clips for microphone cable.
- F Power supply unit.
- G Power supply lead.

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PLUGS**  
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10 kc/s to 1,200 Mc/s

## Voltage Ranges

8 ranges, 1 mV.—3 V. full scale;  
with 100:1 divider to 300 V. full scale

## Accuracy

±3%, 100 kc/s—60 Mc/s  
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±10%, 10 kc/s—1,200 Mc/s

## Stability

No zero reset required over  
8 hours except on most sensitive range

## Response

RMS to 30 mV.; peak calibrated  
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100:1 divider RMS-responsive to 3 V.

## Input Impedance

High Impedance—2 pf. and 75 K $\Omega$ ;  
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Linear scale on all ranges  
D.C. recorder output—1.5 V. at 1 mA.  
Taut-band mirror scaled 6" galvanometer

## Accessories Supplied

Probe with high-impedance tip, 50 $\Omega$   
BNC termination adaptor, output plug

## Accessories Available

100:1 capacitive voltage divider,  
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- 5 Instantaneous mechanical stop and start of tape transit prevents slurring.
- 6 Accurate cueing indicator (turns counter) is scaled in revolutions of the take-up reel, and angled for easier viewing.
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- 9 Ability to accept 8 $\frac{1}{2}$ " reels (1750 feet of standard tape).
- 10 Ability to take a continuous loop cassette in place of standard reels.
- 11 90° hinge on head cover ensures easier tape loading.
- 12 Three tape speeds.

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# Permacon edge connectors



35

These inexpensive edge connectors feature polypropylene mouldings and brass or phosphor bronze contacts with a standard tinned finish. Silver plate, gold flash, or gold plate finishes are available to special order. .100" contact pitches provide a maximum of 40 positions whilst the .150" contact pitch range provides for a maximum of 26 positions. Contact tail variations (shown above) include solder slot tails projecting either vertically downwards or at 90° to the moulding, or tails for direct mounting to a "mother" printed circuit board. Mounting brackets provide "closed" or "open-ended" connectors or include contacts for direct earthing from the mating P.C. Board.

#### Electrical Ratings

Working voltage: 500 Volts D.C. or A.C. Peak (.150" pitch)

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## ELMA

### COUNT BATCH CONTROL



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3. **PLUG-IN** digits which can be easily interchanged without having to rewire.
4. **ELECTRICAL READ-OUT** which gives a separate contact closure for every number in addition to the predetermining signal—enabling direct print-out, etc.

In addition to these features, the ELMA counters will count at up to 25 impulses/sec.; have electrical zero reset; can be forward or backward counting, and can be wired in cascade to form a counter of any number of digits.

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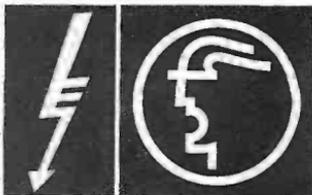
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4/6 (subject)

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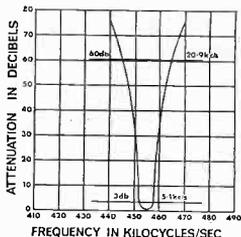
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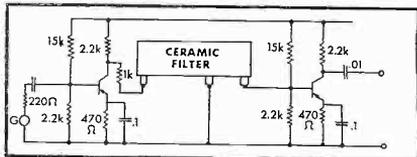
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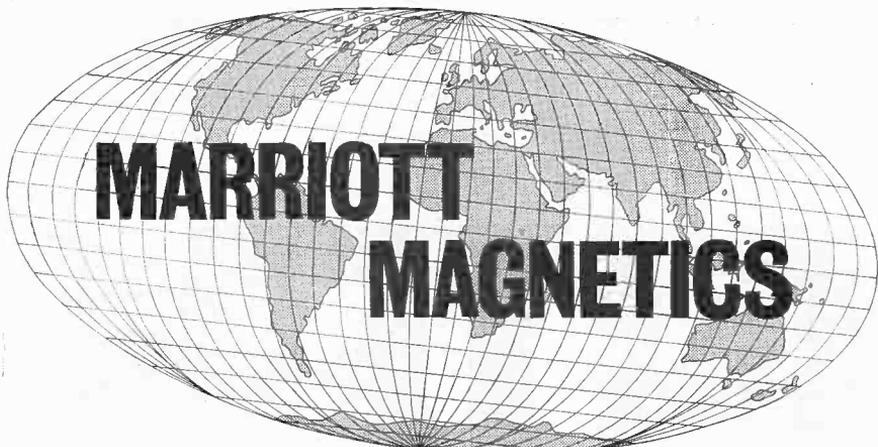


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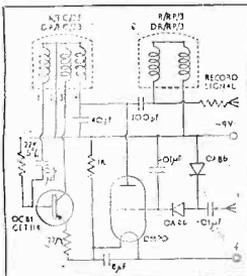
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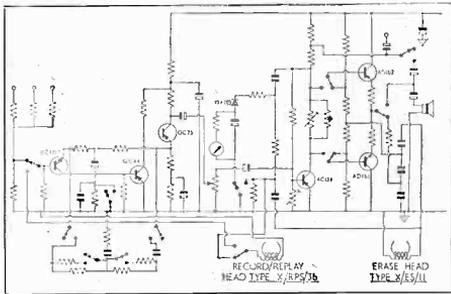
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Self-oscillatory erase head circuit with Marriott 'X'-type erase and record/play heads. Diagram reproduced by courtesy of Mullard Ltd.



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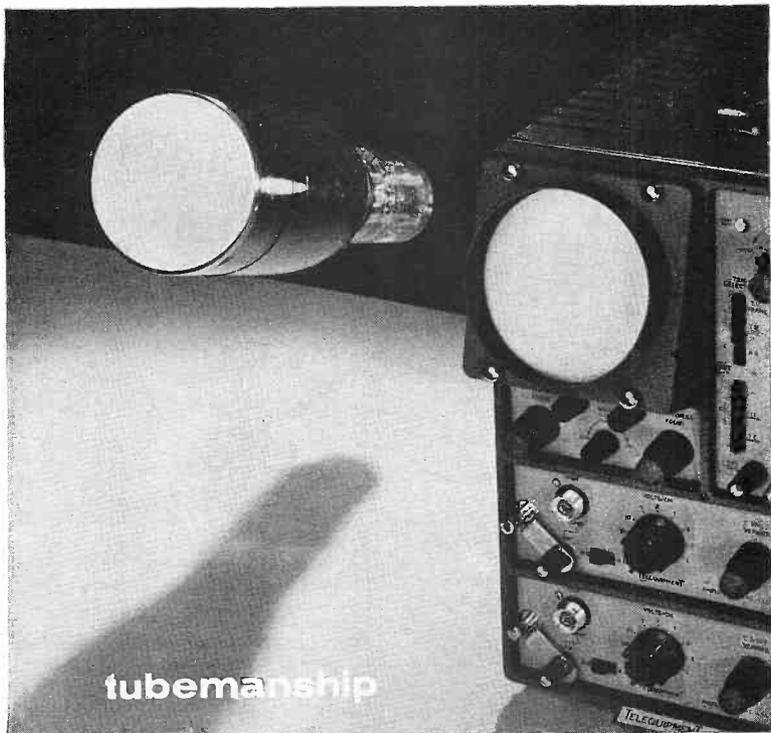
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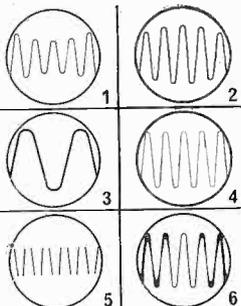


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# Wireless World

ELECTRONICS, TELEVISION, RADIO, AUDIO

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ELECTRONICS, TELEVISION, RADIO, AUDIO

## Radio Regulations: Need for Overhaul

IT is rumoured that plans are afoot to split the existing Post Office into two and create a new Department or Ministry of Telecommunications responsible for the "telecom" side of the existing department, leaving the Post Office responsible for the postal services. It was thought that the Minister of Telecommunications, as Mr. Wedgwood Benn (the P.M.G.) has called himself on several occasions, would make some reference to this proposal when speaking at the recent annual dinner of the Telecommunication Engineering and Manufacturing Association, but we were disappointed. Whether or not this severing of telecoms from the postal services is imminent the P.M.G. has several items on his agenda which call for prompt legislation.

First there is the question of the "pirate" radio and TV stations, which now number ten, around our coasts. A year ago this country was a signatory, with six other European countries, to an agreement to prevent the operation of broadcasting stations on vessels outside national territorial waters. Under the agreement signatories would treat as punishable offences, not only the setting up of these stations, but also the providing of supplies, equipment, transport or programmes to them. This meant, of course, that legislation would have to be drawn up in each country, making provisions necessary to take action against offenders. So far, nothing has been done in this country and the number of "pirate" stations goes on increasing. Some positive action must be taken—either that the operators are given the opportunity of becoming law-abiding citizens by being offered licences, or that they should be made outlaws and treated as such.

What may well be the biggest problem if the "pirates" were offered licences, is the question of operating frequencies. All the frequencies allocated to the U.K. under the 1948 Copenhagen Plan (the revision of which is long overdue) are in use. Would the "pop" stations be willing to operate on one of the two International Common Frequencies—1484 and 1594 kc/s—or would they expect a share of the frequencies used by B.B.C. stations?

On the purely programme side of their activities it may be that the "pirates" prefer to "fly the skull and crossbones" and brandish their cutlasses in the face of the authorities which limit the B.B.C. stations to but a few hours of recorded music a day!

Another item on the P.M.G.'s agenda is the question of Citizens' Band radio, as it is called in the U.S.A. Increasing imports of walkie-talkie transceivers, most of them from the Far East, have prompted us to ask the Post Office why these sets are permitted into the country—and we are certain they are not smuggled in—if it is illegal to use them. We were told blandly that the Post Office has no jurisdiction over imports! Is this "head in the sand" attitude good enough? These transmitter-receivers, which operate on a frequency of about 27 Mc/s and cause interference with licensed radio users in this part of the spectrum, can be purchased for a few pounds, and can be seen in use by youths in many parts of the country. If the P.M.G. has no intention of granting licences for these sets, their import should be prohibited by the Board of Trade and the Post Office should take action against their illegal use.

# Voltage-controlled Amplifier - 1

USING MODULATED PULSES TO GIVE VARIABLE GAIN AT A.F.

The circuit described uses a direct voltage to control a pulse-ratio modulated train which in turn operates a transistor-diode switch. The result is an amplifier whose gain can be controlled over a 26dB range and which may be used for a variety of purposes, some of which will be outlined in Part 2.

By  
**M. BRONZITE,**  
B.Sc.

**T**HERE are many applications, especially in analogue circuitry, where a voltage-controlled amplifier is required. In the past this has been achieved by using the physical properties of active elements such as f.e.t.s and ordinary transistors, as well as by using thermistors, optical methods, and servo motor systems. References 1, 2, 3 are representative of some of these methods, which all suffer from some form of inherent non-linearity, temperature dependence, narrow band of operation, and lack of interchangeability of active elements. It is proposed in this article to illustrate a mode of operation which is purely electronic, independent of the amplifier element used, shows a large degree of linearity and stability and is readily controlled by an applied direct voltage. Further, it will be shown that the circuit can be easily modified to perform other analogue functions.

The system depends on an application of pulse modulation, the principles of which have been discussed elsewhere<sup>4, 5, 6, 7, 8</sup>. Since, however, the basic pulse generator and its subsequent utilization might prove unfamiliar, they will be given some consideration before the circuit itself is discussed.

## Design philosophy

Most previous forms of pulse modulation consist of modulating either the pulse frequency or pulse duration with incoming a.f. signal. The resulting pulse train is then amplified and passed through some form of low-pass filter to recover the original signal. A system of pulse-duration modulation is outlined in Fig. 1 and

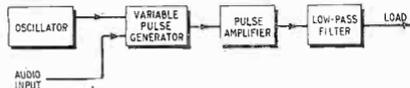


Fig. 1. Conventional pulse-width modulation system for a.f. amplification.

examination will show that there are practical difficulties associated with this system which are not, at first, readily apparent. In the first place, the required switching speeds of the pulse generator will normally preclude the use of

M. Bronzite graduated in physics and chemistry at Reading University in 1958 and after spending four years in industry, first with B.T.H. Rugby and then Plessey's, he went to Israel in 1962. He spent a short time in the Weitzman Institute and then worked in the Hebrew University on the design of equipment for Meteorological studies. His article on a d.c. transistor amplifier in the March 1964 issue arose from work at the University. After returning to this country he was with Kelvin Hughes until last June when he emigrated to Canada and is now with R.C.A. Victor on space electronics projects.



saturated switching circuitry as the following example will show. Let us assume that the upper end of the audio pass band is 25 kc/s and that the pulse repetition frequency (p.r.f.) of the oscillator is 100 kc/s. (This is about the minimum p.r.f. desirable to maintain a high signal-to-noise ratio on the audio output without recourse to an elaborate low-pass filter.) In order to maintain good efficiency of the system it would be reasonable to permit 90% modulation with the incoming signal. The original pulse width is  $5\mu\text{s}$  (half the pulse cycle time) and, with full modulation, this will vary from 1-9  $\mu\text{s}$ . Now, in order to maintain good modulating linearity, the pulse shape must remain the same under all operating pulse widths, which include 1  $\mu\text{s}$ , which in turn suggests a rise and fall time of not greater than 100 ns for the pulse generator, which is a far cry from audio frequencies. The system is also very poor with regard to the effect of overload. On one half-cycle the pulse width will become extremely narrow, with loss of pulse shape while on the other half cycle, "lock-on" of the pulse generator will occur, resulting in a very high increase in distortion at the output. Another practical difficulty arises over the tracking of the pulse generator timing network with that

of the oscillator. That is to say, with no signal input, the pulse width generated must be exactly half the pulse cycle time of the oscillator over the given temperature range, and over the life of the equipment. If they do not, a net d.c. shift will occur at the filtered output, which, at minimum, will alter the operating conditions of the last stage (see Fig. 2). This problem can be eliminated by the use of high-stability components in the timing networks, but the use of precision capacitors is neither convenient, nor cheap.

**Pulse-ratio modulation.**—These difficulties are significantly alleviated by the use of pulse-ratio modulation<sup>9</sup>, in which the frequency and pulse duration both vary non-linearly with input, but the duty ratio (pulse "on" time to pulse cycle time) is proportional to the input. Since the filtered output depends solely on the duty ratio, independent of which system of pulse modulation is used, this hardly constitutes a problem! In the absence of any input there is the usual 50% duty ratio on the output of the pulse generator. With increasing modulation (here "modulation" is loosely used with respect to only one cycle of the incoming signal and denotes a slowly varying change from the initial conditions) the pulse width becomes larger and larger over one-quarter cycle returning to its original value at one-half cycle. From there the pulse width becomes smaller, reaching an asymptotic value of half its original value. This is illustrated in Fig. 3. The frequency becomes smaller with increasing modulation and can (with signal overload) enter the audio band. The pertinent parameters of pulse ratio modulation are as follows:

$$(t_1)_a = (t_1)_0 \cdot \frac{1}{1-a} \quad \dots \dots \dots 1$$

$$f_a = f_0 (1-a^2) \quad \dots \dots \dots 2$$

$$d.r._a = \frac{1}{2}(a+1) \quad \dots \dots \dots 3$$

where  $(t_1)_a$  is the pulse width with modulation level  $a$ ;  $(t_1)_0$  is the pulse width with no modulation;  $f_0$  is the frequency with modulation;  $d.r._0$  is the duty ratio and  $a$  varies between  $-1$  and  $+1$ . These results are derived in Appendix 2. It will be seen that variation of the timing network will have no effect on these parameters, thus completely eliminating the problem of drift of these components, which in turn permits the use of cheap, low-toleranced components. With overload (i.e.  $a$  approaches  $+1$  or  $-1$ ) the output signal will be distorted but the original information will be detectable. With this form of modulation "lock-on" cannot occur providing  $a$  does not equal  $+1$  or  $-1$ , but the modulating frequency will fall within the passband and this will be the sole source of distortion.

It is of interest to note that equations 1, 2, and 3 are perfectly general, and equations of a similar form could be derived for a controlled conventional multivibrator, or for the circuit used in ref. 9. The particular advantage of the circuit to be considered here is that all the active elements operate in an unsaturated state, which is necessary for the high speed of operation that will be utilized.

**Bowes oscillator.**—The Bowes oscillator<sup>10</sup>, shown in a simple form in Fig. 4, is an emitter-coupled multivibrator with linear charge and discharge rates, which facilitates design and gives high stability. The description that follows, along with Appendix 1, will only consider first-order effects. Two current generators supply current  $i_1$  and  $i_2$  to the emitters of the two transistors. Assume that transistor Tr2 has just switched off. Then current  $(i_1 + i_2)$  passes through transistor Tr1, part

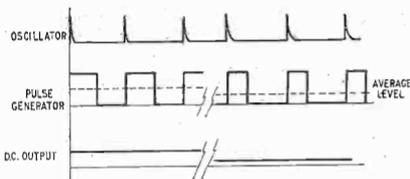


Fig. 2. Effect of one timing network altering with life or temperature, in a pulse-width modulated amplifier.

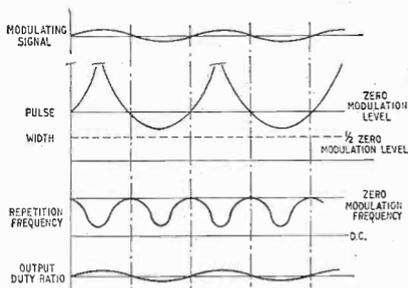


Fig. 3. Effect of modulation on a pulse-ratio modulated train.

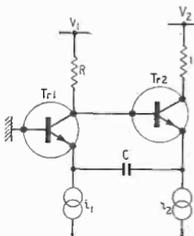


Fig. 4. The Bowes oscillator.

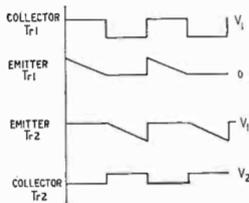


Fig. 5. Waveforms of the Bowes oscillator of Fig. 4.

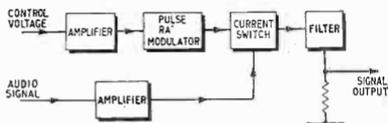


Fig. 6. Block diagram of the voltage-controlled amplifier.

direct, part through capacitor  $C$ . This provides a voltage step at the collector of  $Tr1$  which biases  $Tr2$  off. The voltage developed across  $C$  linearly reduces, due to the charging current, thus reducing the voltage at the emitter of  $Tr2$  until it becomes forward biased, and regeneratively switches on again. Since the value of resistor  $R$  is sensibly low, the base, and thus the emitter, of  $Tr2$  passes rapidly up to voltage  $V_1$ . This voltage change is transmitted through  $C$  to back bias  $Tr1$  and now the total current is supplied to  $Tr2$ . The action of the capacitor again reduces the back bias on  $Tr1$  until it switches on again, switching off  $Tr2$  and completing the cycle. The higher voltage  $V_2$  is required to prevent saturation of  $Tr2$ . The waveforms for operation are shown in Fig. 5 and the analysis of the circuit is given in Appendix 1. It has been shown<sup>19</sup> that second-order effects will alter the performance of the oscillator by about 3%, and that variation with temperature is less

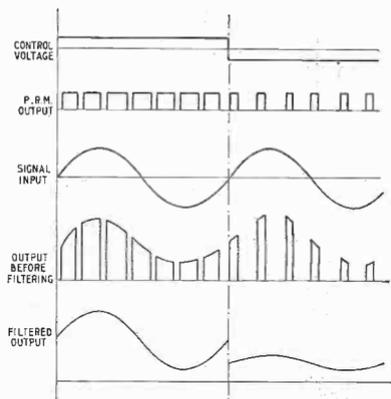
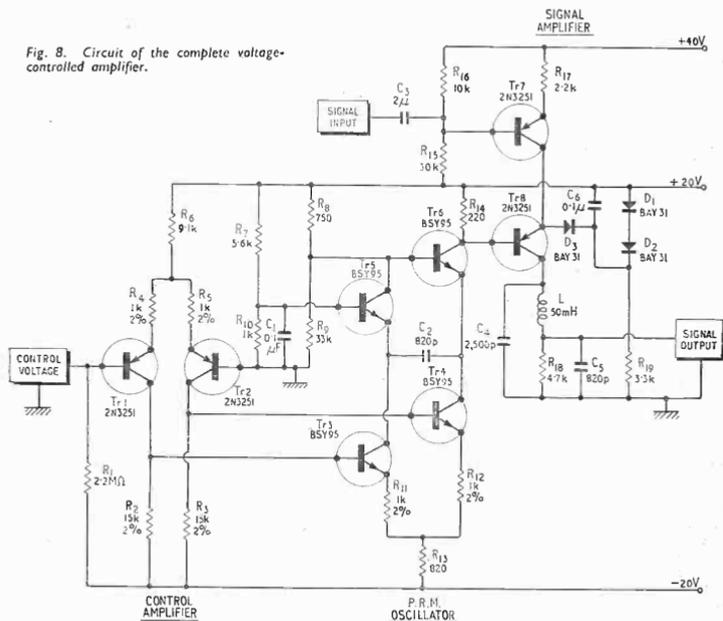


Fig. 7. Waveforms illustrating the change in output amplitude with control voltage in Figs. 6 and 8.

Fig. 8. Circuit of the complete voltage-controlled amplifier.



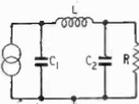


Fig. 9. Low-pass filter design.

$$C_1 = \frac{1.5}{R \times \omega} \text{ (FARADS)}$$

$$C_2 = \frac{0.3}{R \times \omega} \text{ (FARADS)}$$

$$L = 1.33 \times \frac{R}{\omega} \text{ (HENRIES)}$$

than 0.5% over an extended range, which suggests that it will be an ideal vehicle for instrumentation circuits.

In order to use this oscillator for modulation purposes it is necessary to modulate the current generators with two equal amplitude out-of-phase signals. This is accomplished by using transistors as current sources, and voltage driving the bases of these transistors with signals from a long-tailed pair amplifier. The output is taken from the collector of Tr2, and Appendix 2 shows how the output duty ratio will follow the control signal.

### Voltage-controlled amplifier

Having shown at some length a method of switching, it might be politic to try and relate it now to the title of the article! The block diagram of a complete voltage-controlled amplifier is shown in Fig. 6. The controlling signal is amplified and then fed to the pulse-ratio modulator which in turn controls the switching of current through a long-tailed-pair switch. The current itself has been derived from the output of the audio signal amplifier and after passing through a filter in one arm of the current switch, develops a voltage across  $100\Omega$ , which constitutes the output. The manner in which the control voltage will alter the amplitude of the output voltage is shown in Fig. 7.

The actual circuit is shown in Fig. 8. Transistors Tr1 and Tr2 amplify the control voltage to provide equal out-of-phase signals at the bases of Tr3 and Tr4, which in turn constitute the current generators to the oscillator Tr5 and Tr6. The voltage across  $R_{11}$  and  $R_{12}$  is made 5V without modulation and therefore for a 90% swing the voltage at the bases of Tr3 and Tr4 may swing  $\pm 4.5$ V. Knowing the control voltage range of operation, the gain of the first stage is thus fixed. The frequency of oscillation was made 500 kc/s, since with 90% modulation ( $a = 0.9$ ) the minimum value of frequency derived from equation 2 approximately becomes:—

$$(1 - 0.8) 500 \text{ kc/s} = 100 \text{ kc/s}$$

which, as explained earlier, is felt to be the lowest desirable modulator frequency.  $R$  and  $V_1$  shown in Fig. 4 are simulated by  $R_a$  and  $R_b$ , where  $V_1 = V_2 R_a / (R_a + R_b)$ , and  $R$  is  $R_a$  and  $R_b$  in parallel. The output at  $R_{14}$  is approximately a 2V pulse train with rise and fall times of about 15 ns. The current switch consists of transistor Tr8 and diode D3, and, while a transistor could have been used in place of D3, there would be little advantage since no second output signal is required. Diodes D1 and D2 provide a bias to the switch such that Tr8 is either fully on or fully off, depending on the output of the modulator. The switch will pass current generated by the audio signal amplifier (Tr7) through the filter to develop the output signal across  $R_{16}$ . If one excluded the switch and filter it would be apparent that the voltage gain of the signal amplifier is approximately  $2(R_7/R_{16})$ , and in the absence of a control signal, i.e. 50% modulation, the gain reverts to unity. This circuit has two additional advantages: (1) variations of supply voltages will not alter the duty ratio and (2) the amplifier can be readily modified for use with d.c. signals.

### Low-pass filter

The sensitivity of the amplifier in the final analysis depends on the noise level at the output. Since, in this case, the noise is represented by pulse train information, the action of the filter in suppressing the modulating signal becomes somewhat important. For this reason an 18dB/octave Butterworth filter was used with a turnover frequency of 20 kc/s. The necessary design information was abstracted from Ref. 11 and the approach is indicated in Fig. 9. While this filter uses an inductor, which is more inconvenient than a simple RC approach, it is felt that the results warrant it, with approximately 40 dB attenuation at 100 kc/s. In order to calculate the degree of "breakthrough" of a pulse train, it is first necessary to do a Fourier analysis to determine the amplitude of the fundamental sinusoidal component. It should be self-evident that with an 18dB/octave filter, all subsequent harmonics are at least an order of magnitude lower. For the same reason only the lowest operating p.r.f. need be considered. Ref. 12 shows the frequency spectrum of a pulse train with a pulse width of 500 ns and p.r.f. of 100 kc/s and gives the relative amplitude of the 100 kc/s component as 10% of the original pulse amplitude. Thus with such a pulse with a height of 5V, the fundamental amplitude will be approximately 0.5V and the resulting filtered output will be 5mV. The measured output was 7mV pk-pk which suggests that the approach is valid. For a signal-to-noise ratio of 20dB it becomes apparent that the signal at the output must not be less than 70mV (with maximum modulation), and to improve on this figure either a lower level of modulation must be used or the filter performance must be improved.

### Results

Because of the rapid rise and fall times of the generated pulses it proved expedient to locally decouple all supply rails, with 0.1μF capacitors, to the earth rail at the point where the load resistor was connected. The same was found to be necessary for the filter earth connections. Once this had been done the circuit was surprisingly well mannered and gave no further difficulty whatsoever. The maximum output voltage was 9V pk-pk and the

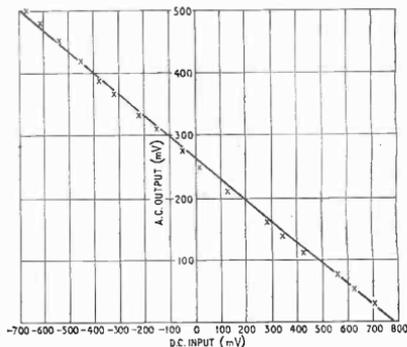


Fig. 10. Linearity of amplifier, showing signal input vs. output.

minimum was 20 mV (depending on the degree of distortion that is tolerable). Anywhere within this band the output could be varied over a 26 dB range, and the response was 3 dB down at 20 kc/s which was due solely to the filter response. It was observed that the inductor caused ringing on the output at a frequency of 30 Mc/s and with a peak amplitude of 20 mV. This occurred whenever the switch changed state and died away in about 300 ns. This should not prove a serious problem since it can be removed at a later stage if necessary. The linearity of the circuitry is shown in Fig. 10, the curvature shown being due to common mode amplification in the control voltage amplifier and can be readily improved. It should not prove difficult to extend the frequency response to 100 kc/s. The unmodulated oscillator frequency could be raised to 1 Mc/s, and at the same time the output duty ratio could be lowered to 90% (currently it is at 95%) which, at 1 Mc/s, would cause the minimum frequency to be

$$1 \text{ Mc/s} \times (1 - (0.8)^2) = 360 \text{ kc/s.}$$

This would be almost two octaves above the maximum signal frequency. Finally, if necessary, the filter could be improved using more elements.

### Summary

A circuit has been described that uses pulse-ratio modulation to control the effective gain of an audio amplifier over a 26 dB range, and since the circuit was only constructed to illustrate a principle there should be little difficulty in extending its performance to meet any given requirement. It should be noted that no trimmer or "setting-up" is required, the active elements are readily interchangeable with no loss of performance and variation of supply rails and temperature will give only second order effects.

Next month it is hoped to conclude this article with some possible applications.

### APPENDIX I

#### Operation of the Bowes Oscillator (Figs. 4 & 5)

Assume Tr1 has just switched on.

Voltage step at collector of Tr1:

$$V_c = (i_1 + i_2)R \quad \dots \quad (1)$$

This step also represents the degree of back bias on transistor Tr2 since the emitter cannot change instantaneously.

Thus, after time  $t_2$  transistor Tr2 will conduct again, where:—

$$i_2 = CV_e / i_2 \\ = \frac{C(i_1 + i_2)R}{i_2} \quad \dots \quad (2)$$

At this instant, transistor Tr1 switches off and is back biased by  $V_c$  (via Tr2 and C). Tr1 switches on again after time  $t_1$  where:—

$$t_1 = \frac{C(i_1 + i_2)R}{i_1} \quad \dots \quad (3)$$

$$\text{Total period } (t_1 + t_2) = CR(i_1 + i_2) (1/i_1 + 1/i_2) \\ = \frac{CR(i_1 + i_2)^2}{i_1 i_2} \quad \dots \quad (4)$$

$$\text{i.e. frequency, } f = \frac{i_1 i_2}{(i_1 + i_2)^2 CR} \quad \dots \quad (5)$$

$$\text{and if } i_1 = i_2, \quad f = 1/4CR \quad \dots \quad (6)$$

### APPENDIX 2

#### Pulse ratio modulation with the Bowes Oscillator

With no modulation  $i_1 = i_2 = i$

With instantaneous level of modulation  $a$ , let

$$\left. \begin{aligned} i_1 &= i - ai \\ i_2 &= i + ai \end{aligned} \right\} \quad -1 < a < +1$$

i.e.  $i_1 = i(1 - a)$  and  $i_2 = i(1 + a)$ .

Now, from Appendix 1:—

$$\text{Pulse width, } t_1 = \frac{CR(i_1 + i_2)}{i_1} \\ (t_1)_0 = 2CR \quad \text{without modulation} \\ (t_1)_a = \frac{CR \cdot 2i}{i(1 - a)} \quad \text{with modulation.} \\ = \frac{2CR}{(1 - a)} \\ = \frac{(t_1)_0}{(1 - a)} \quad \dots \quad (1)$$

From Appendix 1:—

$$\text{Frequency, } f = \frac{i_1 i_2}{(i_1 + i_2)^2 CR} \\ \text{thus } f)_0 = 1/4CR \\ \text{and } f)_a = \frac{i^2(1 - a^2)}{4i^2 CR} \\ = 1/4CR \cdot (1 - a^2) \\ = f)_0(1 - a^2) \quad \dots \quad (2)$$

From Appendix 1:—

$$\text{duty ratio, (d.r.) } \frac{t_1}{(t_1 + t_2)} = \frac{CR(i_1 + i_2)}{i_1} \cdot \frac{i_1 i_2}{CR(i_1 + i_2)^2} \\ = \frac{i_2}{i_1(i_1 + i_2)} \\ \therefore \text{d.r.)}_0 = \frac{i(1 + a)}{2i} \\ = \frac{1}{2}(1 + a) \quad \dots \quad (3)$$

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# Silicon Transistor Millivoltmeter

WIDE RANGE VOLTMETER WITH GOOD FREQUENCY RESPONSE AND HIGH INPUT IMPEDANCE

By D. E. O'N. WADDINGTON, A.M.I.E.R.E.

UNTIL fairly recently, the high price of silicon planar transistors has precluded their use by the electronic experimenter, particularly as similar performance, with regard to gain and  $f_T$ , has been obtainable from the very much cheaper germanium alloy diffused transistor. However, the introduction, by several manufacturers, of plastic-encapsulated silicon planar transistors at competitive prices, has made it possible for these to be used more generally. Some of the advantages of these transistors are:—

- Low leakage current—less than 0.5  $\mu$ A (total)
- Good performance at low collector currents
- Good frequency response
- Low noise figure

Both n-p-n and p-n-p types are available.

These features make the use of silicon planar transistors very attractive as the design can, to a large extent, ignore

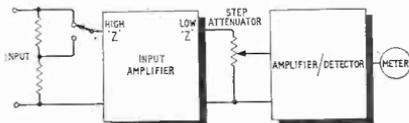


Fig. 1. Basic arrangement of the millivoltmeter.

variations in the transistor parameters and control the overall performance by the application of suitable negative feedback techniques. The author has used them in several home projects, of which the millivoltmeter is an example.

## General design

In the design of a millivoltmeter there are two main factors, namely, voltage range and frequency range, which dictate what system should be used.

In order to obtain a good frequency response from an attenuator, the simplest method is to operate at low impedance where stray capacitance has less effect and, with luck, there will be no need to apply compensation. This conflicts with the common requirement for all voltmeters i.e. that the input impedance should be high so that the voltage being measured is disturbed as little as possible by the test gear. Thus, it is expedient to use the system shown in Fig. 1. Here, the first stage will have a high input impedance and a low output impedance. This makes it possible for the low impedance attenuator to be used without affecting the input. However, as the dynamic range of the input amplifier is limited both by the maximum input signal which it can accept and by the amount of power which it can accommodate, it is necessary to include a range switch right at the input. As this will necessarily be a high impedance, capacitive fre-

## SPECIFICATION

- Ranges  
1 mV, 3 mV, 10 mV, 30 mV, 100 mV, 300 mV;  
1 V, 3 V, 10 V, 30 V, 100 V, 300 V.
- Accuracy  
Better than  $\pm 5\%$ . The attenuator accuracy can be improved if necessary.
- Frequency response  
 $\pm 1\%$ , 50 c/s to 100 kc/s  
 $\pm 10\%$  (better than 1 dB), 16 c/s to 1.5 Mc/s.
- Noise level  
Around 10  $\mu$ V with input open circuit.
- Input resistance  
Better than 1 M $\Omega$  for 1 mV-300 mV ranges  
10 M $\Omega$  for 1 V-300 V ranges.
- Consumption  
11 mA at 12 V.

quency compensation circuits will be necessary. This will not add much to the complication as it need only be a two-position switch. The output from the low impedance attenuator is fed to the main amplifier/detector circuit and thence to the meter.

## Input stage

Many forms of high input-impedance, low output-impedance circuits could be used here with very little change in overall performance. In this case the complementary feedback pair was chosen as it is economical and, at the same time, provides adequate performance for the application.

The use of a low noise, low leakage-current transistor in the first stage made it possible to use high value resistors (3.3 M $\Omega$ ) in the base bias chain without any fear of adverse thermal effects. Thus, an input impedance of greater than 1 M $\Omega$  was achieved without using bootstrap circuits which increase the complexity. No over-

D. E. O'N. Waddington, who was born at Pietermaritzburg, South Africa, received his early training in light engineering at the Natal Technical College. He was for some time in the Aircraft Division of Marconi (South Africa) Ltd., and since 1957 has been in the development department of Marconi Instruments, Ltd., working on semiconductor applications for electronic measuring instruments.



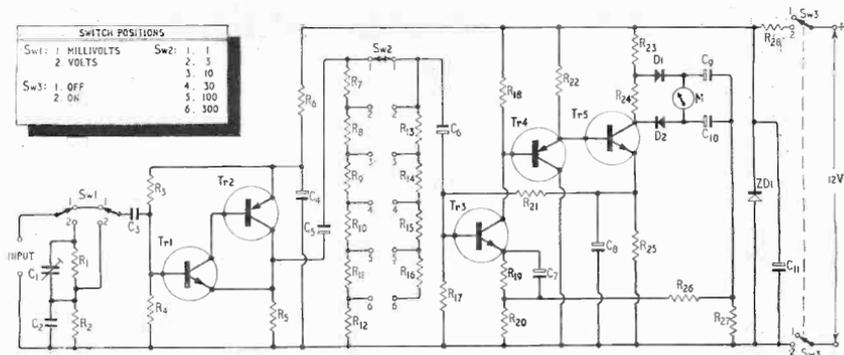


Fig. 2. Circuit of the silicon transistor millivoltmeter.

#### Resistors

R1	10M $\Omega$	$\pm 5\%$	$\frac{1}{2}$ W
R2	10k $\Omega$	$\pm 5\%$	$\frac{1}{2}$ W
R3	3.3M $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W
R4	3.3k $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W
R5	3.3k $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W
R6	1k $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W
R7	2.16k $\Omega$	$\pm 5\%$	$\frac{1}{2}$ W
R8	68 $\Omega$	$\pm 5\%$	$\frac{1}{2}$ W
R9	216 $\Omega$	$\pm 5\%$	$\frac{1}{2}$ W
R10	68.3 $\Omega$	$\pm 5\%$	$\frac{1}{2}$ W
R11	21.6 $\Omega$	$\pm 5\%$	$\frac{1}{2}$ W
R12	10 $\Omega$	$\pm 5\%$	$\frac{1}{2}$ W
R13	470 $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W
R14	180 $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W
R15	68 $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W
R16	22 $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W
R17	47k $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W
R18	68k $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W
R19	6.8k $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W
R20†	22 $\Omega$	$\pm 5\%$	$\frac{1}{2}$ W

R21	47k $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W
R22	5.6k $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W
R23	2.7k $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W
R24	100 $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W
R25	3.3k $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W
R26†	53.2 $\Omega$	Use 56 $\Omega$	5% shunted to give correct calibration
R27†	22 $\Omega$	$\pm 5\%$	$\frac{1}{2}$ W
R28	300 $\Omega$	$\pm 10\%$	$\frac{1}{2}$ W

#### Capacitors

C1	3-8pF	Philips trimmer
C2	0.015 $\mu$ F	30V
C3	0.1 $\mu$ F	350V
C4	100 $\mu$ F	12V
C5	25 $\mu$ F	6V
C6	5 $\mu$ F	6V
C7	100 $\mu$ F	6V
C8	500 $\mu$ F	6V

C9	2 $\mu$ F	6V
C10	2 $\mu$ F	6V
C11	1000 $\mu$ F	12V

Tr3	TI415, 2N2925
Tr4	TIS04, HT101
Tr5	TI415, 2N2925

#### Semiconductor Devices

D1	1S44, 1N914
D2	1S44, 1N914
ZD1	OAZ206
Tr1	TI415, 2N2925
Tr2	TIS04, HT101

#### Miscellaneous

M	100 $\mu$ A f.s.d.
S1	d.p.d.t. toggle switch
S2	two-pole, six-position wafer switch
S3	d.p.s.t. toggle switch

#### Notes:

†Non-inductive types (carbon).

R7 2.16k $\Omega$  = 2.2k $\Omega$  in parallel with 120k $\Omega$  ( $\pm 10\%$ )

R9 216 $\Omega$  = 220 $\Omega$  in parallel with 12k $\Omega$  ( $\pm 10\%$ )

R11 21.6 $\Omega$  = 22 $\Omega$  in parallel with 1.2k $\Omega$  ( $\pm 10\%$ )

R8 { The use of the nearest preferred value (i.e. 680 or 68  $\Omega$ )  
will introduce an error of only 0.5% in addition to  
the normal component tolerance.

If greater accuracy is required, the attenuator resistors can be given closer tolerances.

load protection circuit was included in the original voltmeter as it increases the input-capacitance, and may also affect the overall frequency response. (The modification necessary to add this protection if it is required is very simple and is shown in Fig. 3.)

#### Meter-range switch S.2

This is a simple voltage-divider circuit with the values chosen such that the steps are in the ratio  $\sqrt{10}$ :1 thus making it possible to use the same dB scale on all ranges

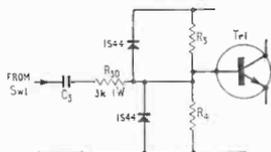
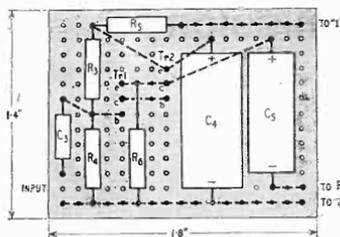


Fig. 3. Alternative input circuit with protection diodes included.

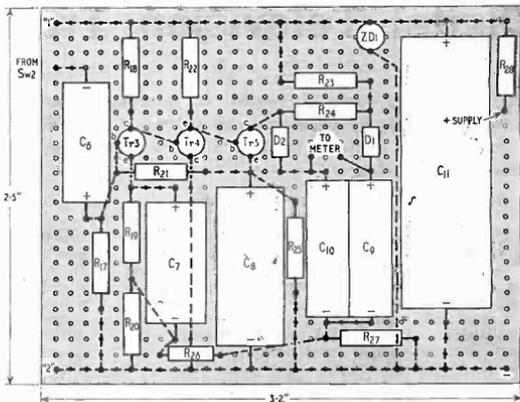
of the meter. The series resistors included in position 3 to 6 of the switch, serve to keep the output impedance of the divider more or less constant. This minimizes errors due to loading of the divider chain by the input impedance of Tr3. In order to prevent large transients during range switching, both the input and output of the attenuator are isolated by means of capacitors.

#### Amplifier and detector

This section consists of two common-emitter amplifier stages, coupled by an emitter follower. Overall d.c. feedback from the emitter of Tr5 to the base of Tr3 stabilizes the working points of the transistors very effectively. The rectifier circuit, which is of the voltage doubling type, is connected in the feedback loop from the collector of Tr5 to the emitter of Tr3. The effect of this is two-fold: it provides a high source-impedance feed for the rectifier circuit thus ensuring a linear scale shape and it also stabilizes the gain of the amplifier. In building this circuit, care must be taken to ensure that R20, R26 and R4 are all non-inductive as these resistors control both the gain and



▲ Fig. 4. Input amplifier layout.



▶ Fig. 5. Amplifier-detector layout.

the frequency response. Silicon planar diodes are used as rectifiers and, in order to help the signal to overcome the pedestal voltage, a standing bias potential is applied across them by means of R24. Meter protection is accomplished by limiting the current through the output transistor and thus the drive to the rectifier circuit.

### Construction

The layout of the circuit is not very critical provided that lead lengths are kept reasonably short and the input circuitry is not mixed up with the output. In the experimental model it was convenient to make the input amplifier on one piece of "Lektrokrit" board and the amplifier-detector on another. (Figs. 4 and 5.)

### Setting up

There are two adjustments (gain and frequency response) which need to be made in order to ensure that the voltmeter works correctly. To set up the gain, switch the voltmeter to the 1 V range, apply a signal having a frequency of approximately 400 c/s but with level set to 1 V as precisely as possible to the input. Adjust the value of R26, by shunting it with resistors having values in the range from 330 Ω to 10 kΩ, until the meter reads exactly full scale. The frequency response is not quite so easily set up as it requires the use of a signal source capable of providing an accurate volt at 100 kc/s. If this is available, the procedure is to use this as the input signal on the 1 V range and to adjust C1 for full scale deflection. The meter scale will be identical with that given on p. 270 of the June 1964 issue.

### Performance

The accuracy of a voltmeter, such as has been described, is very dependent upon the accuracy with which the gain may be set and also the accuracy of the resistors used in the voltage divider chains. However, an accuracy of better than ±5% is fairly easily attainable with generally available components. If a better accuracy is required, the attenuator resistors can be given tighter tolerances. The frequency response may be set to be flat to within ±1% from 50 c/s to 100 kc/s. In the experimental model,

the response was found to be ±10% from 15 c/s to 1.5 Mc/s. The noise level indicated on the meter, with an open circuit input but with the instrument installed in its metal box, was of the order of 10 μV. Battery consumption is approximately 11 mA.

## CONFERENCES & EXHIBITIONS

Further details are obtainable from addresses in parentheses

- Mar. 10-11 Burlington House  
Circular Dichroism—Electronic & Structural Principles  
(Royal Society, Burlington House, W.1)
- Mar. 15-17 King's Head, Harrow  
Public Address Exhibition  
(A. J. Walker, 394, Northolt Road, South Harrow, Middx)
- Mar. 23-31 Alexandra Palace  
Physics Exhibition  
(Inst. of Physics & Phys. Soc., 47 Belgrave Sq., S.W.1)
- Mar. 23-30 Earls Court  
Electrical Engineers Exhibition  
(A.S.E.E. Exhibition, 25 Museum Street, W.C.1)

### CRANFIELD

- Mar. 21-24 College of Aeronautics  
Aerospace Instrumentation Symposium  
(M. A. Perry, College of Aeronautics, Cranfield, Beds.)

### EASTBOURNE

- Mar. 22-23 Grand Hotel  
Exploiting Instrument Development  
(Scientific Instrument Research Assoc., Chislehurst, Kent)

### OXFORD

- Mar. 30-Apr. 1 The University  
Nuclear and Particle Physics  
(Inst. of Physics & Phys. Soc., 47 Belgrave Sq., London, S.W.1)

### OVERSEAS

- Feb. 25-Mar. 6 Copenhagen  
International Electronics Fair  
(Secretariat, Julius Thomsens Plads 1, Copenhagen V)
- Mar. 2-4 Washington  
Semiconductor Counter Symposium  
(I.E.E.E., 345 East 47th St., New York, N.Y. 10017)
- Mar. 10-15 Paris  
Festival du Son  
(S.I.E.R.E. 16 rue de Presles, Paris 15)
- Mar. 28-31 Paris  
Electronic Switching  
(Colloque de Commutation Electronique, 16 rue de Presles, Paris 15)

# Digital Television Transmission

Why has there been a revival of interest in transmitting television signals by pulse code modulation? This article takes a look at some of the experimental work in progress and the incentives behind it

**A**LTHOUGH the transmission of television pictures by pulse code modulation has been the subject of experiments for 15 years or more,<sup>1</sup> it is only recently that this technique has been looked at seriously as a means for satisfying practical needs. It has been a case of a good idea waiting for applications. One of the main problems, of course, has been that a pulse coded television signal requires considerably more bandwidth than the original video signal—although in exchange for this one gains a valuable increase in signal/noise ratio.

There are several reasons for the current resurgence of interest. In the first place, p.c.m. telephony has shown itself to be a practical proposition for use in public services.<sup>2</sup> Secondly, the advent of solid-state circuitry has made it possible to design complex digital encoding, decoding and regenerating equipment that is reliable, compact and economical to manufacture. Thirdly, the wide-band transmission systems needed for transmitting p.c.m. signals are becoming cheaper and cheaper. Present systems use coaxial cable, but there are possibilities of even wider bandwidths with the long-haul waveguides and coherent light guides of the future.

Allowing that new electronic techniques—and the practical experience gained with them—have put the means of p.c.m. television in a more attractive light, what are the particular ends our systems engineers have in mind in 1966? There are, of course, the spectacular applications in the exploration of space. The successful transmission to Earth of pictures of the planet Mars

from the Mariner IV spacecraft<sup>3</sup> showed what could be done in overcoming extreme signal/noise ratio problems. Military television applications arise from the possibility of using secret codes for the p.c.m. signals. But the widest use of p.c.m. television is likely to be in broadcasting—in conveying signals between studio centres, outside broadcasting sites and transmitters. Most of this, of course, would be done through the communications network operated by the Post Office, and here it is necessary to consider television signal transmissions as merely one part of the whole communications pattern. Forward thinking in this field envisages increasing use of digital techniques, not only in conveying the information but in switching as well. This means, in the first instance, p.c.m. telephony and high-speed data transmission. First, a number of "digital areas" centred on the large cities might well be developed, and then these would be linked by digital trunk routes. Efficient use of channel capacity depends on time division multiplexing of the pulse trains representing different types of information. Thus, in the future it is likely that the transmission of television signals would have to fit into some such comprehensive scheme of time division multiplexing, and pulse coding is necessary to enable this to be done.

Broadcasting organizations are investigating the possibility of using pulse coded signals within their own television studio centres. It is thought that this coding will facilitate automatic methods of switching and control

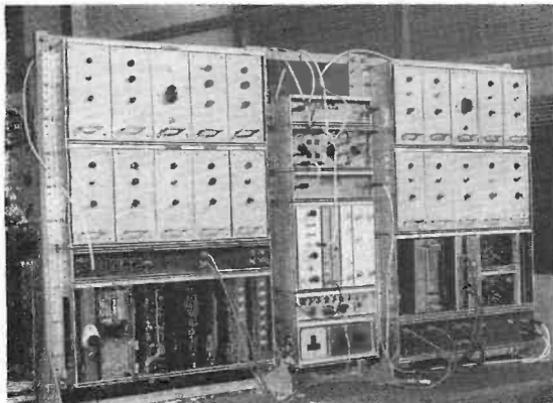


Fig. 1. Experimental encoding and decoding equipment at Standard Telecommunication Laboratories.

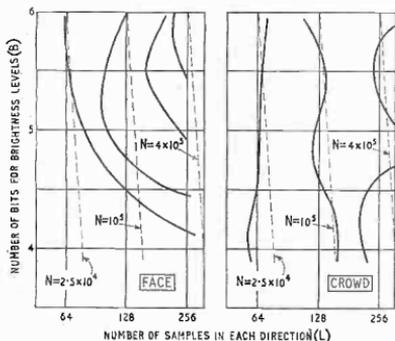


Fig. 2. Workers in the Research Laboratory of Electronics, Massachusetts Institute of Technology, U.S.A., have been studying subjective assessments of the quality of quantized still pictures, using a computer-simulated p.c.m. system with variable system parameters and a picture input/output device. On the graphical results shown here for two subjects, a face and a crowd scene, the solid lines are isopreference curves (curves of constant preference) and these indicate how picture quality varies with the number of brightness levels used ( $=2^B$ ) and with the spatial sampling rate (number of samples in a picture  $=L \times L$ ). The number of bits per picture is  $N = L \times L \times B$ , and for guidance, curves of constant  $N$  are shown by the broken lines. (Further details in "PCM picture transmission" by Thomas S. Huang in the December 1965 issue of IEEE Spectrum, to which acknowledgement is made.)

and so reduce the dependence of the final transmitted picture on the skill of individual operators.

Pulse code modulation was invented in 1938 by Alec H. Reeves, and it is only to be expected that the main British work on p.c.m. television is being done in the organization where he still works—Standard Telecommunication Laboratories at Harlow, Essex. Here experimental equipment has been developed by which 625-line television pictures can be transmitted over 960 yards of coaxial cable (see Fig. 1). *Wireless World's* reporter found the received picture indistinguishable from the original when both were viewed at the correct distance on adjacent 23-inch K-B television sets. Closer examination of the received picture showed that

extremely small flaws were being introduced by occasional coding errors in the transmission system. These appeared as tiny black spots or slots in individual lines, but were so infrequent and so randomly distributed over the picture as to be hardly discernible. S.T.L. state that these impairments will be almost completely eradicated in future equipment.

### Code for sync pulses

As is well known, the principle of p.c.m. is to take samples of the analogue signal waveform at a rate at least twice that of the highest component frequency to be distinguished (the Nyquist rate) and to encode each amplitude value into a binary number represented by a sequence of pulses. Whereas the analogue waveform is a continuous function of time, the encoding process introduces quantization and consequently the p.c.m. representation of the waveform is constructed from a finite number of amplitude levels. In the S.T.L. equipment the total swing of the picture waveform from peak white to black level (excluding sync pulses) is divided into 80 amplitude levels, and the rate at which these levels are sampled is 12.5 Mc/s. The sync pulses are not treated as part of the waveform because, being cyclic and of constant amplitude, they have a high degree of redundancy, and it would be a waste of channel capacity to use 30% of the available amplitude levels (and the corresponding code characters) to represent them. Thus the sync pulses are represented by one additional amplitude level (making 81 levels altogether for the composite waveform) and the presence of this amplitude level is signalled by one corresponding code character.

Choice of the sampling rate and number of amplitude levels has been determined mainly by the spectrum of the 625-line television signal, by the transmission channel bandwidth available and by the limitations of present-day pulse circuits. Other considerations may enter into it, however, and, for example, a group at the Massachusetts Institute of Technology, U.S.A., is studying how sampling rate and number of amplitude levels affect subjective assessments of picture quality (see Fig. 2).

Block diagrams of the S.T.L. encoding and decoding equipment, which uses solid-state circuitry, are shown in Figs. 3 and 4. In the encoder it will be seen that the television sync signal is separated at an early stage and used to initiate the appropriate code character. The picture waveform passes to the sampler and here the amplitude samples are temporarily held as analogue

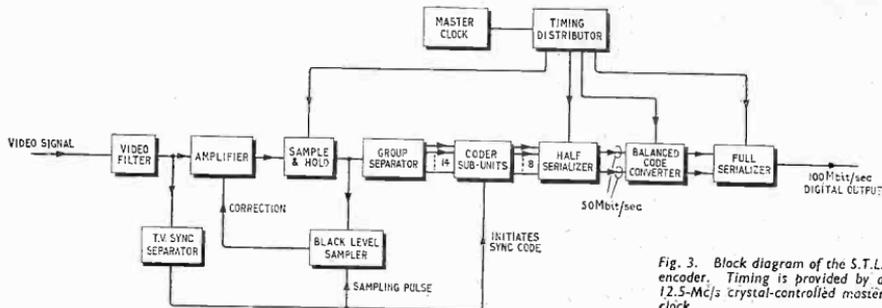


Fig. 3. Block diagram of the S.T.L. encoder. Timing is provided by a 12.5-Mc/s crystal-controlled master clock.

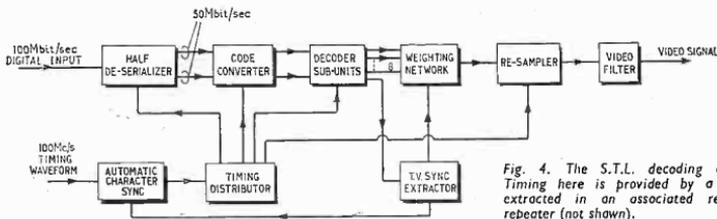


Fig. 4. The S.T.L. decoding equipment. Timing here is provided by a waveform extracted in an associated regenerative repeater (not shown).

voltages for 50 nsec to allow time for the coder to operate. At this point it is essential to ensure that the black level of the picture is represented by a constant analogue voltage value—that is, the d.c. component must be maintained—otherwise, the coder will generate incorrect characters. This is the function of the “black level sampler,” which is part of a sampled-data control loop providing a feedback signal that adjusts the d.c. level of the picture signal.

The next stage is the process of analogue-to-digital conversion. In order to represent 81 amplitude levels in the type of signalling code employed, 8-digit binary characters are necessary. With a sampling frequency of 12.5 Mc/s this means a final transmitted digit rate of 100 Mbit/sec. To achieve the high speed of analogue-to-digital conversion necessary for this signalling rate, the conversion is performed on a parallel basis—that is,

each amplitude sample is converted into a binary character represented by eight bits appearing *simultaneously* on eight wires. It is not, however, possible to use a single parallel coder to convert all the 81 amplitude levels as this would raise considerable problems in drive, propagation time and instability as a result of interconnecting large numbers of solid-state logic circuits. Instead the total range of amplitude levels is first separated into 14 groups of 6 levels each (except in two groups) and for each of these 6-level groups a separate parallel coder sub-unit is provided. The outputs of the 14 coder sub-units are then combined. The separation into 6-level groups is performed by a chain of voltage discriminators set by appropriately graduated reference voltages.

In the encoder each amplitude level is converted into a pattern of 8 simultaneous digits according to the scheme shown in Fig. 5 (a). This code was devised by K. W. Cattermole of S.T.L. and its features will be described later. Next the parallel code characters have to be transformed into serial characters for transmission, and for economy in transistor circuitry in the “balanced code converter” this is done in two separately operating sections of the “half-serializer”—one section producing digits 1, 3, 5, 7 as a serial pulse train at the same time as the other section produces digits 2, 4, 6, 8 as a similar pulse train (e.g. digits 1 and 2 occur simultaneously). The two resulting 50 Mbit/sec serial pulse trains then pass through a code converter and are finally interleaved in the “full serializer” to produce a 100 Mbit/sec output which is transmitted through the 960-yd coaxial cable.

### Need for balanced code

The function of the code converter in Fig. 3 is to achieve a type of code which simplifies the transmission system equipment—notably the pulse-regenerating repeaters needed to make up the losses and distortions in long distance communications circuits. Pulse regeneration is basically a matter of amplification followed by amplitude slicing to restore the incoming distorted waveform to square-pulse form. If, however, the incoming pulse code waveform is unbalanced—that is, contains long sequences of similar digits (all 1s or all 0s)—d.c. restorers are necessary in the repeaters to ensure that the waveform is sliced at the correct levels. If, however, a balanced code can be used (waveform containing approximately equal numbers of 1s and 0s) d.c. restoration is unnecessary and the repeaters are consequently simplified. In addition, with a balanced code, the repeaters can work at lower supply voltages, allowing more repeaters to be supplied in series through the same cable; all amplifiers are uniformly loaded and they need not be linear; and the necessary extraction of the pulse repetition frequency in the repeater is simplified and the timing errors due to level changes

(Continued on page 117)

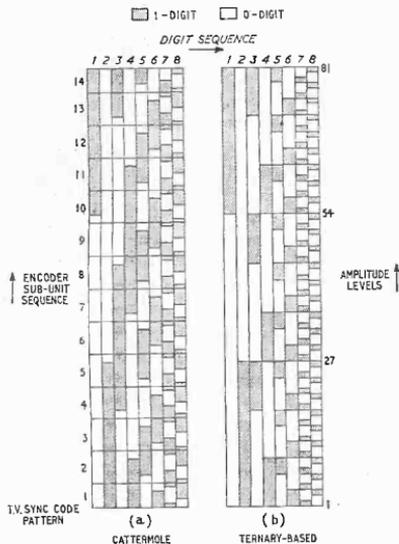


Fig. 5. Binary codes used in the S.T.L. encoding/decoding equipment: (a) Cattermole unit-distance code; (b) ternary-based code which can be translated into and from a balanced code.

# NEW Reslo

## cardioid pencil dynamic microphone

The type CPD, the latest in the Reslo range of dynamic (moving coil) microphones, incorporates a rugged but miniaturised dynamic insert specially designed to have a unidirectional sound pickup pattern.

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The overall result is a smooth and wide frequency characteristic well maintained throughout the audio frequency spectrum. The CPD microphone is very suitable for high quality music recording and relay purposes, and can, in addition, be used for loud, close speaking and singing with impressive realism. The microphone incorporates an on-off switch and is supplied with a detachable holder.

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Low impedance model - £15.0.0  
Medium and High impedance - £16.0.0  
For more detailed information and prices, please write to  
Reslosound Limited,  
Spring Gardens, London Road,  
Romford, Essex.  
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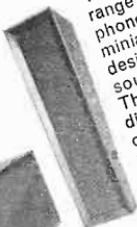
SR430

The RESLO range of Public Address Equipment.

Line source and cabinet loudspeakers. The LS100A line source loudspeaker is one of a range specially designed for Public Address installations in churches, assembly rooms, factories, theatres etc.

Audio amplifiers.

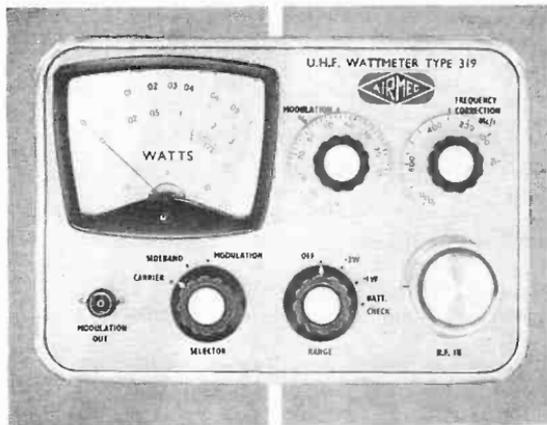
A range of amplifiers with outputs of 15 to 250 watts, employing the 100 volt line system, is also in continuous production and development. The SR430 30 watt amplifier has been designed for Public Address work combining high reliability with a smooth frequency response of 100 c/s to 15 Kc/s.



LS100A



# To measure C. W. Power . . . Sideband power . . . Modulation depth



- Frequency Range:  
1-1400 Mc/s
- Ranges: 0-100mW,  
0-300mW
- Input Impedance:  
50 ohms.

The U.H.F. Wattmeter Type 319 is a light and compact instrument for measuring C.W. power, sideband power, and modulation depth in the frequency range 1-1400Mc/s. Carrier and sideband powers are indicated directly on a 3½" scale meter in two ranges. Percentage modulation depth is shown on a potentiometer scale.

For carrier measurement no additional power is necessary; internal dry batteries provide power for sideband and modulation measurement. This instrument is one of the units in the Airmec range of U.H.F. equipment which includes connectors, adaptors, attenuators, reactance lines, slotted lines etc.

## Airmec UHF Wattmeter Type 319



**Airmec** for peak performance consistently

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TELEPHONE: HIGH WYCOMBE 21201 (10 LINES)

are reduced. The purpose of the code converter in Fig. 3 is therefore to transform the generated Cattermole code into a balanced code providing these substantial advantages.

This transformation is performed on the basis of a ternary code, as shown in the table below. A ternary code is one in which numbers are represented in terms

Ternary code	Binary coded version	Balanced code
0	01	01
1	00	00 or 11
2	10	10

of three digits, 0, 1, 2, instead of the two digits of the binary scale or the ten of the decimal scale—the digit positions in a ternary number having the weights of powers of 3, that is,  $3^0$ ,  $3^1$ ,  $3^2$ ,  $3^3$  etc. The three digits of the ternary code can be represented in binary form, as shown. Here the ternary digit "1" is represented by 00, but it could equally well have been 11 because this combination is not used by either of the other two ternary digits, 0 or 2. This fact is made use of to produce a balanced code, by representing the ternary "1" alternately by 00 and 11. The waveform of the balanced code has the properties that its mean value is always equal to half its peak-to-peak amplitude and that never more than four 1s or four 0s follow each other.

The Cattermole code generated by the encoder is one of a class of what are called "unit-distance codes." A more familiar member of the class, and also used in p.c.m. television, is the reflected binary or Gray code. In analogue-to-digital conversion these codes have the property that, in handling a transition between adjacent analogue levels, only one digit changes. (This can be seen from Fig. 5(a).) This property is valuable because it avoids the encoding errors which might arise if several digits changed simultaneously, as they do in pure binary (e.g. with a five-digit binary code a transition between analogue values 15 and 16 would cause all five binary digits to change simultaneously), and it is to avoid such errors that the Cattermole code is used in the Fig. 3 equipment. It is used in preference to the more familiar Gray code because its particular cyclic pattern simplifies the circuitry for the subsequent transformation into a

balanced code. In this last-mentioned process the Cattermole code is first converted into a ternary based code, of the type shown in the table above and in Fig. 5(b), which is then transformed into the balanced code. All these operations are performed by solid-state logic circuits.

In the decoder (Fig. 4) the incoming 100Mbit/sec pulse train is first divided into two 500Mbit/sec trains, each of which is then converted back to the ternary-based code of Fig. 5(b). There are eight decoder sub-units, one for each digit position, and each sub-unit produces a sequence of analogue voltages corresponding to the arriving digits in that position. These voltages then pass into a weighting network where proportions of them are taken and combined according to the weights of the digits in the respective positions (the television sync pulse being also restored by this process). The resulting sequence of discrete voltages is then smoothed into a continuous wave-form by the video filter and passes to the picture display equipment.

### Regenerative repeater

Synchronization of the decoder with the encoder is achieved by a 100-Mc/s timing waveform extracted from the 100Mbit/sec p.r.f. in a regenerative repeater at the decoder terminal. This waveform is applied to the "automatic character sync" unit which controls the timing of the various decoding operations. The regenerative repeater (Fig. 6) operates by sampling the incoming distorted waveform—after it has first been amplified by 65 dB—with accurately timed short pulses derived from the 100Mbit/sec repetition rate of the input. These short sampling pulses are obtained by amplifying, slicing and differentiating the incoming signal and then applying the differentiated pulses, after further amplification, to a filter with a high Q factor (400), the resulting 100 Mc/s sinewave being then once again sliced and differentiated. The short code pulses resulting from the sampling process have a duration of 4 nsec and have to be stretched to restore them to their full width of 10 nsec as generated by the encoder.

A certain amount of work on pulse coded television has also been done by the Automatic Telephone and Electric Co. at Liverpool. At last year's Physics Exhibition in Manchester they showed an experimental equipment for encoding signals with a bandwidth of 6.5 Mc/s. It used a 7-bit parallel code of the Gray type and the parallel characters were subsequently serialized to give an output digit rate of 91 Mbit/sec. The company claimed that this type of encoder would allow full quality colour transmission to be achieved.

In the U.S.A. the main work on pulse coded television is being done at Bell Telephone Laboratories in New York. Little need be said about it here as the experimental equipment (see Fig. 7) is very fully described in three papers in the *Bell System Technical Journal* for November 1965. Suffice to say that the equipment is not for television transmission alone but multiplexes television, telephony and high-speed data into a final pulse code stream of 224 Mbit/sec. The system will handle two television pictures; 3,456 voice channels; or 864 voice channels plus a television picture plus a composite signal comprising 600 frequency division multiplexed voice channels. The complete television waveform, including the sync pulses, is quantized into 512 amplitude levels, requiring a 9-bit unit-distance (Gray) code, and the sampling rate is 12.352 Mc/s. Encoding is performed by either a solid-state encoder or a special deflected-beam

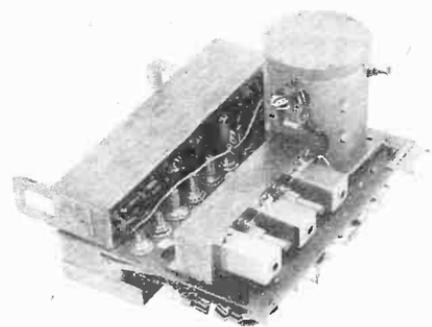


Fig. 6. Regenerative repeater used at the receiving terminal of the S.T.L. experimental equipment.



Fig. 7. Part of the Bell Telephone Laboratories experimental p.c.m. equipment. This unit simulates the pulse jitter that would accumulate over a 4000-mile transmission system. Automatic compensation for jitter is provided.

coding tube. At present the tube still gives a slightly better performance, though it is expected that solid-state circuitry will catch up soon.

In the time-division multiplexing of the different signals, an interesting method of synchronization called

"pulse stuffing" is used to avoid the necessity of locking the digit rate of the lower speed signals to that of the high speed line. Furthermore, the technique also allows information to be readily added or taken off along the route. Pulses from each coder (or from lower speed digital inputs) are written into a small digital store and then read out at a slightly faster rate which is an exact sub-multiple of the line rate of the high speed system. Each time the store is about to be exhausted, an extra pulse having no information-carrying value is generated and "stuffed" into the stream transmitted on the line. This produces a pause in the read-out from the store and allows it to refill. Thus, input sources whose rates differ by small amounts are synchronized to the digit rate of the high speed line. At the receiving terminal, the pulses are demultiplexed and each signal is written into its receiving digital store and read out at the original rate which that signal had. This is possible because the transmitting terminal sends control signals to the receiver to inhibit the writing of stuffed pulses into the receiving store.

Pulses leaving the multiplexer are converted to a balanced code, for the reasons explained above, but this is a three-level code called paired selected ternary. In this code, sequences of binary digits are grouped into pairs and transmitted as combinations of positive pulses, negative pulses and absence of pulses.

#### REFERENCES

1. One of the earliest accounts of work in this field was "Television by Pulse Code Modulation," by W. M. Goodall, in *Bell System Technical Journal*, Vol. 30, January 1951, pp. 33-49.
2. See, for example, "P.C.M. for G.P.O. Telephones," *Wireless World*, February 1965, p. 87.
3. "Picture transmission from Mars," *Wireless World*, August 1965, p. 385.
4. See "Information Theory and Pulse Communication," by D. N. Tilsley. *Wireless World*, June 1965, p. 265.

## LITERATURE RECEIVED

A wall chart giving "A summary of Texas Instruments silicon transistors" has been published by their stockists Quarndon Electronics (Semiconductors) Ltd., Slack Lane, Derby.  
WW 301 for further details

Airpax Electronics Inc. have produced a 6-page bulletin (F-8) on "Electromagnetic Pickups." It contains details of seven of their transducers and discusses the application of magnetic pick-ups to tachometry, counting, positioning, motion study, timing, vibration measurement and synchronising. Copies are available from the Seminole Division of Airpax Electronics Incorporated, P.O. Box 8488, Fort Lauderdale, Florida 33310.  
WW 302 for further details

A short-form catalogue of the "Medical Electronic Instruments" manufactured by San'ei Instrument Company, of Tokyo, is available from Instrumentarium Ltd., 28 Manchester Street, London, W.1.  
WW 303 for further details

The complete range of Zener and reference diodes currently made by Motorola Semiconductor Products Inc. are included in a selection guide—which takes the form of a wall chart—obtainable direct or from the U.K. stockists, Celdis Ltd., Trafford Road, Richfield Estate, Reading, Berks.  
WW 304 for further details

A 28-page catalogue on the range of Variac variable transformers made in this country by the Zenith Electric Company (under licence from General Radio) has been sent to us by the exclusive U.K. distributors, Claude Lyons Ltd., of 76 Old Hall Street, Liverpool 3.  
WW 305 for further details

Vibro-Meter Corporation, of Switzerland, have produced a short-form catalogue on their transducers and associated electronic equipment. This is obtainable from the company's recently opened British Office at Haletop Civic Centre, Wythenshawe, Manchester 22.  
WW 307 for further details

Arcoleetric Switches Ltd., of Central Avenue, West Molesey, Surrey, announce that their 1966 catalogue (No. 136) covering their range of switches, neon indicators and signal lampholders is now available. A price list appears in the front of this 62-page publication.  
WW 308 for further details

Lind-Air (Supplies) Ltd., of 53 Tottenham Court Road, London, W.1, announce that a new catalogue containing details of over 100,000 different types of British and American plugs, sockets and connectors is now available. A number of supplementary leaflets, on pen recorders, transducers and accelerometers, microwave components, and semiconductor devices and valves, are to be found within the catalogue.  
WW 309 for further details

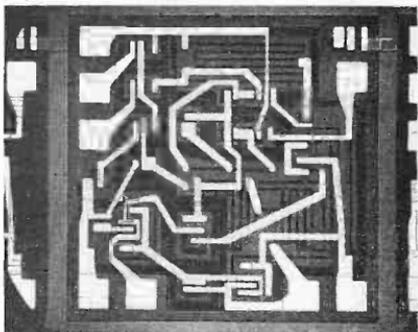
# INTEGRATED CIRCUITS FLOOD INTO EUROPE

NEW LINEAR AND DIGITAL TYPES AT PARIS ELECTRONIC COMPONENTS SHOW

ALTHOUGH there is a great deal of talk about the commercial invasion of Europe by American electronics companies, it is only when one goes to a truly international exhibition like the *Salon International des Composants Electroniques* (Paris, Parc des Expositions, 3-8 February) that one appreciates its full impact. Here one is faced with the combined forces of the latest American product technology before they have become absorbed into the native industry. This year in Paris the latest invasion force was obviously integrated circuits.\* Of the 22 exhibitors of these devices counted by our reporter, 16 were American, four were French and two were British. The Americans, it would seem, are desperately anxious to capture as much of the European market as possible. Integrated circuits only become competitive with conventional circuits when they are made in sufficiently large quantities. This means that there is room for only a small number of manufacturers, and it has been estimated that even the U.S.A. market may support only about five companies. Thus the question of who will survive and who will have to pull out in the U.S.A. may well depend on how much of the European market each manufacturer can secure.

In such an atmosphere the European producers of integrated circuits, although well advanced in technology, have their backs to the wall commercially. At the *Salon*, for example, two major French companies, Coserm (controlled by C.S.F.) and Sescro (controlled by C.F.T.H.) revealed that they were exploring the possibility of a co-operative agreement to meet the American competition. In Britain, Ferranti and Marconi are jointly manufacturing a range of circuits, and in Holland, the Philips company have tied up with

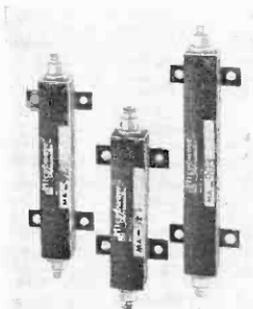
\*Wireless World uses this term in the broadest sense to cover monolithic semiconductor devices, thin-film circuits and hybrid circuits.



The semiconductor chip of a monolithic operational amplifier with a voltage gain of 45,000 recently introduced by SGS-Fairchild.

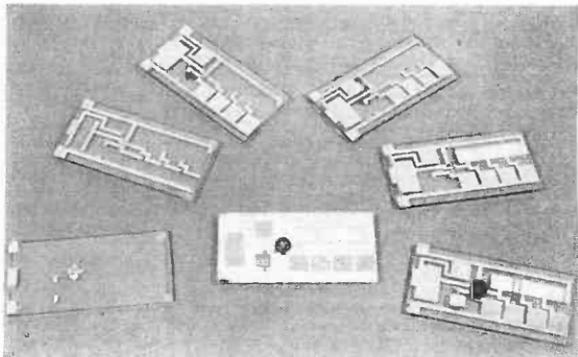
Westinghouse Electric International in a technology exchange agreement.

A noticeable technical trend was the increasing number of linear integrated circuit devices coming on the market. These were mostly general-purpose amplifying devices—operational amplifiers, video amplifiers, d.c. amplifiers, differential amplifiers and the like. One of the latest was a monolithic operational amplifier from SGS-Fairchild, the 759C  $\mu$ A 709, which had a high voltage gain of 45,000 and an output voltage excursion of  $\pm 14$  V. An operational ampli-



Examples of Microwave Associates' miniature i.f., pulse and logarithmic amplifiers using integrated circuits. Frequency range: 30 to 350 Mc/s. Bandwidths: 5 to 100 Mc/s. Gain factors: 60 dB to 100 dB.

Stages in the construction of a hybrid integrated circuit as demonstrated by LCC-Steajix—one of the many passive-component manufacturers who are going into the thin-film business.

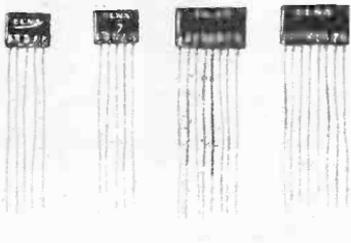




This English Electric u.h.f. klystron will operate at the high peak output power of 40 kW.



Numerical indication of signal level in decibels with respect to 0dB reference (1mV into 600  $\Omega$ ) is given by this Compagnie des Compteurs instrument designed for the range 10 c/s to 100 kc/s.



A return to the multiple resistor elements of the 1950s? Examples shown by Elna Denshi offer resistance values from 500  $\Omega$  to 220 k $\Omega$ .

fier in a TO-5 can shown by Motorola allowed a choice of input impedance—20 k $\Omega$  with conventional input circuit or 2 M $\Omega$  with a Darlington circuit.

For higher frequency working several manufacturers were offering wide-band amplifiers with -3 dB bandwidths of 100 Mc/s and voltage gains of the order of 10-15. The Philco monolithic SA-20, for example, packaged in an 8-lead TO-5 can, has an input impedance of 1.6 k $\Omega$ , an output impedance of 5  $\Omega$  and operates from a 24-V supply. Comprising three direct-coupled transistors and six resistors, it has -65 dB intermodulation distortion, a pulse response of 10 ns and provides terminals by which an external feedback capacitor or filter network can be connected into the second stage. Other amplifiers had smaller bandwidths, up to 35 Mc/s, and voltage gains in the range 10-50. Monolithic a.f. amplifiers—particularly suitable for hearing-aid amplifiers carried in the ear—included a three-transistor circuit made by La Radio-technique, with a gain of 80 dB and package dimensions of 2.7  $\times$  2.7  $\times$  1.1 millimetres. Noise figures are about 4 dB.

Because of their small size and monolithic construction the majority of linear amplifiers now available are very low power devices of not much more than 50 mW dissipation, but this is not a fundamental limitation. An a.f. amplifier circuit in a TO-5 can shown by Motorola, for example, gave an output of 1 watt (with 0.5% total harmonic distortion). For higher powers the hybrid integrated circuit technique is necessary. A good example was a servo amplifier, shown by C.S.F., with a power output of 3.5 watts. It comprised four separate transistor chips—a preamplifier, an amplifier and two power transistors—with thin-film tantalum or nickel-

chrome resistors and aluminium interconnections on a silicon substrate, all mounted in a transistor-type package of about  $\frac{1}{2}$  in diameter. The gain at 400 c/s (the amplifier being designed to work in synchro circuits at this frequency) was 60 dB. Another servo amplifier of hybrid construction, this time with an output of 5 W was shown by Solitron.

Digital integrated circuits still dominate the scene, however, in a variety of circuit techniques with different power, speed, loading and noise immunity characteristics—DCTL (direct coupled transistor logic), DTL (diode/transistor logic), RTL (resistor/transistor logic), TTL (transistor/transistor logic) and several others. Apart from the usual gates (mostly NAND/NOR logic) and flip flops, a whole host of more complex functional units was to be seen, including shift registers, code converters, memory sensing amplifiers, counters, and half adders. RCA, having entered the integrated circuit field rather late, came out with a comprehensive range of digital and linear circuits, and these included a family of exceptionally high speed OR/NOR gates with propagation delay times of only 3.6 ns. This company were also showing monolithic ferrite memory modules, using 1-inch square ferrite wafers, each providing the equivalent of 4096 ferrite cores, with associated integrated-circuit diode selection matrices. The type MF2100 module, for example, had a storage capacity of 64 words with 64 bits per word, used 128 diodes and had a switching speed of 35 ns.

Another advanced technique, shown by General Micro-electronics, was the use of the m.o.s. insulated-gate field-effect transistor as the basic element in monolithic integrated logic circuits. Because of the high input impedance of the IGFET—the gate draws no input current—a very large number of the elements can be driven from the output of one element, and elements can function as memory cells by virtue of the charge storage effect. The IGFET elements work in the enhancement mode and this is stated to give good noise immunity because a threshold voltage must be exceeded before current will flow through the device. The number of elements per circuit can be 10 to 100 times greater than with epitaxial junction integrated circuits and, in fact, the economic competitiveness of the system depends on having at least 30 NAND/NOR elements per package.

**Other items noted.**—A whole range of off-the-shelf colour television receiver components and subsystems (OREGA) ● Artificial reverberation introduced mechanically in loud-speaker enclosures by coiled-spring resonant structures driven by rods from the cone, reverberation times being 8-15 sec over passbands between 50 c/s and 16 kc/s (Audax) ● Direct-current motors without brushes and synchro resolvers using the Hall effect (CSF) ● Small variable autotransformers as alternatives to potentiometers in low power circuits (Radiophon) ● Magnetrans for industrial heating (Varian and CSF) and rod-type heating elements heated by electron bombardment of a diode anode (Eimac) ● A water tap for hospitals, laboratories, etc., controlled without touching by a proximity detection device (Hosiden Electronics).

# A Graphical Method of Harmonic Analysis

By V. O. STOKES

It often happens that a quick harmonic analysis is required in circumstances where speed is more important than a high order of accuracy. The following method is a ready means of determining the amplitude and phase relationships in a complex waveform, provided that the levels of the 5th and higher orders are relatively low.

The accuracy obtainable depends upon the plotting accuracy and the relative levels of harmonics and fundamental, with higher harmonic levels giving a greater accuracy. It is possible to obtain values of  $\pm 0.5$  dB for harmonics at  $-20$  dB and  $\pm 3$  dB for harmonics at  $-40$  dB, from the plotted curves.

Before proceeding with the description, however, it must be mentioned that the method is not new. It was devised by J. Harrison many years ago and has since appeared in several text books, one of which is Castle's "Manual of Practical Mathematics" published as long ago as 1920. A more theoretical explanation of the method was given in *Experimental Wireless* in 1934<sup>1</sup>. Another graphical method was also described in *Wireless World* in 1962<sup>2</sup>. However, a recent sampling (admittedly a small one) taken among younger engineers and students seems to indicate that it has fallen into disuse—indeed, it was quite unknown to them—which is a pity, for it can often save valuable time.

## Description of the method

Perhaps the simplest way of describing the process of waveform analysis by this method is by practical illustration. Fig 1 is a plot of a complex waveform, the main constituents being fundamental, 2nd harmonic and

V. O. Stokes, joined the Marconi Company in 1926, at the age of 20, after two years with Western Electric. He spent seven years in the Test Department and in 1935 transferred to research and development. In 1950 he took charge of the group responsible for the design and development of transmitters. In 1963 he became assistant chief transmitter engineer and since last November has been assistant to the chief engineer, telecommunications. He is also editor of the Company's journal Point-to-Point Telecommunications.



3rd harmonic. Points 0 to 11 are marked on the waveform at  $30^\circ$  intervals: 0 at  $0^\circ$ , 1 at  $30^\circ$ , 2 at  $60^\circ$ , etc.

On a separate strip of paper, also shown in Fig. 1, the amplitude of points 0 to 11 are marked with respect to zero level. In practice, the paper strip is moved along in  $30^\circ$  steps, to obtain the best accuracy.

This marked strip is used to plot curves—shown in Fig. 2 and described later—of the constituent components of the waveform, by subtracting and adding the amplitudes of the various points in accordance with Table 1.

In Table 1, mathematical expressions representing component parts of a Fourier expansion are given for the three curves. As can be seen from these expressions half the amplitude of curve A gives the peak amplitude of the fundamental 3rd harmonic, ignoring the 5th,

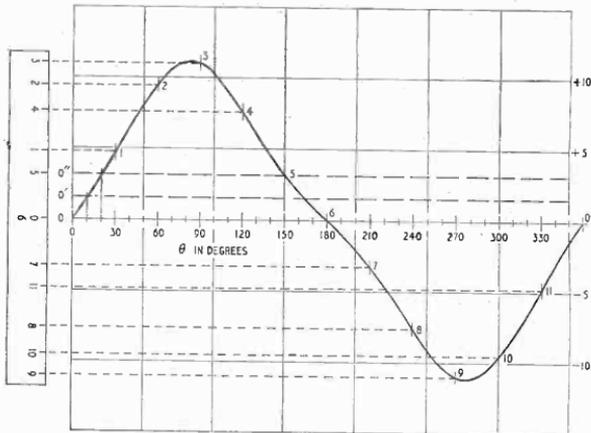


Fig. 1. A complex waveform with second and third harmonic content. The points identified numerically every  $30^\circ$  on the waveform are projected to determine the graduations on the card strip.

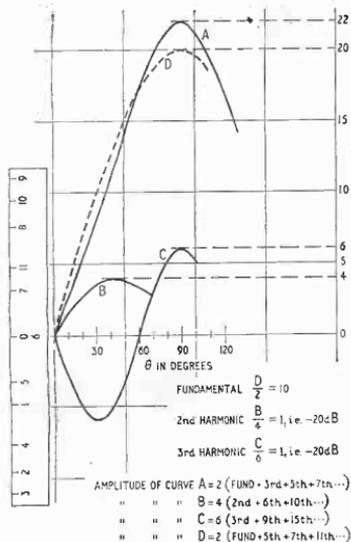


Fig. 2. The constituent components of Fig. 1 waveform plotted from the information given in Table 1. Note: For clarity sub-divisions have not been shown on the graph, but in the scale referred to in the text under the heading Accuracy, one unit would be represented by two small divisions.

$\theta$	A 2(Fund. + 3rd + 5th)	B 4(2nd + 6th + 10th)	C 6(3rd + 9th + 15th)
0°	0-6	(0-3) + (6-9)	(0-2) + (4-6) + (8-10)
30°	1-7	(1-4) + (7-10)	(1-3) + (5-7) + (9-11)
60°	2-8	(2-5) + (8-11)	(2-4) + (6-8) + (10-9)
90°	3-9	(3-6) + (9-0)	(3-5) + (7-9) + (11-1)
120°	4-10	(4-7) + (10-1)	(4-6) + (8-10) + (0-2)

7th, etc. One quarter of the amplitude of curve B gives the peak amplitude of the 2nd harmonic, ignoring the 6th, 10th, etc. One sixth of the amplitude of curve C gives the peak amplitude of the 3rd harmonic, ignoring the 9th, 15th, etc.

The peak amplitude of the fundamental is obtained by subtracting one third of the amplitude of curve C from curve A, at every 10° point, giving curve D, which is twice the fundamental amplitude.

The relative phase of the three components of the original waveform is obvious from Fig. 2.

Because the peak amplitudes of curves A and C are coincident at 90° in the example, both relative phase and amplitude could be obtained without drawing curve D, but in the general case it is necessary to plot curve D for an accurate assessment.

### Plotting the curves

To plot the curves, the strip is reversed and points marked at 30° intervals, as shown in Fig. 3. The method

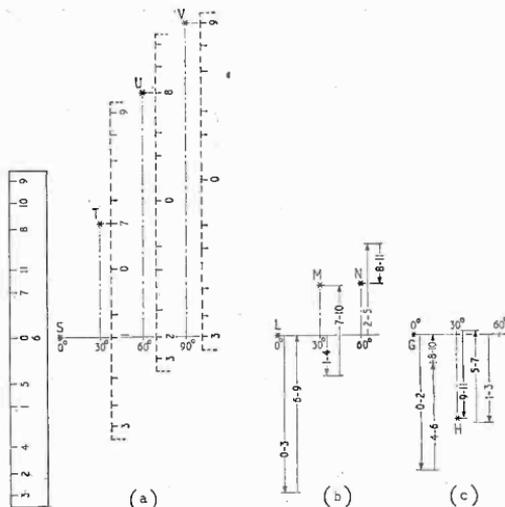


Fig. 3. The positions of the marked up paper strip which give points for curves A, B and C from the information in Table 1.

of plotting the points for curves A, B and C is shown in Fig. 3(a), (b) and (c) respectively. Points S, T, U and V are points for curve A, with points L, M and N for curve B, and points G and H for curve C, all at 30° intervals.

Fig. 3 is used to give an explanation of the method of using the inverted strip. The actual curves should be plotted as shown in Fig. 3, in order that the relative phase of harmonics and fundamentals can be determined.

From these points a rough approximation of curve A could be drawn, but they are quite inadequate to draw B and C.

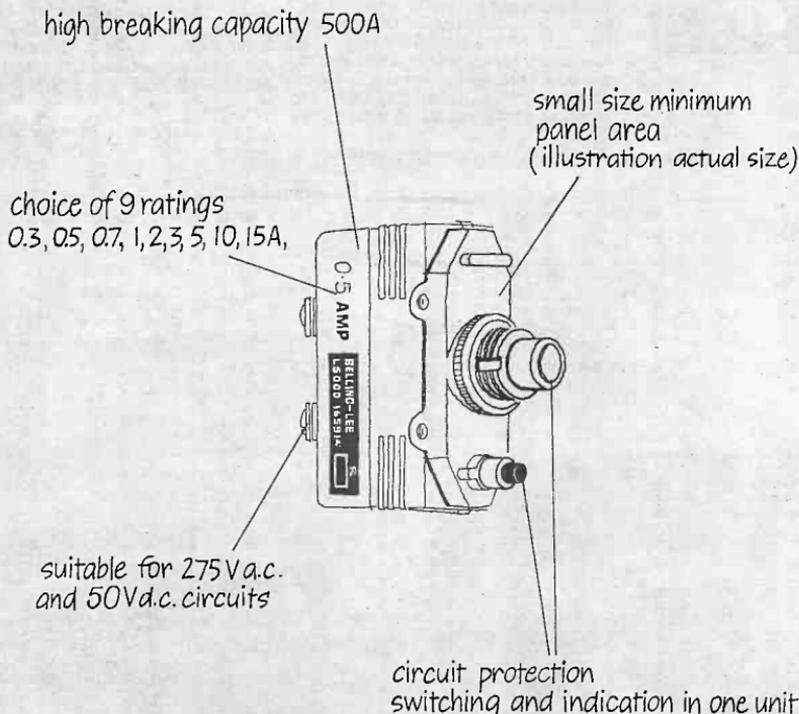
Additional points can be obtained at 30° intervals, starting at 10° and 20°, by using two more paper strips. On these strips, points 0 to 11 are marked, as before, but with reference to new zero lines, 0' and 0'' (see Fig. 1). Points on the 0' strip are marked 0 at 10°, 1 at 40°, 2 at 70°, etc., giving points for curves A, B and C when inverted and transferred to Fig. 3, at 10°, 40°, 70°, etc.

Similarly the other strip, 0'', will give points at 20°, 50°, 80°, etc., when marked with reference to level 0'. It is seen that 0' is the baseline drawn at the level of the complex waveform at 10°, and 0'' is the level at 20°.

### Accuracy

For a second harmonic level of -20 dB and the scale used (see Fig. 2 note), the limits of measurement are about ±half of one small division in eight small divisions (curve B), giving an accuracy of approximately ±0.5dB. Also the limit of measurement of about one small division corresponds to a harmonic level of -40 dB (one tenth of curve B or C). At this harmonic level, ±half of one small division represents a tolerance of ±3 dB.

(Continued on page 123)



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Table 2 gives the amplitude of curve D at every 10°, showing that in the example the plot of the fundamental does not depart from a sine wave by more than 2%.

It should be pointed out that these limits of accuracy assume that the plot of the original waveform is in itself correct within fine limits. In practical cases where the method of obtaining the original waveform does not enable the plot to be very accurate, the results will not be within such fine limits. For example, when the waveform is obtained from an oscilloscope, photographically or by tracing, the initial error is of the order of 5%. Thus the results obtained will be less accurate by this amount, giving total tolerances of approximately  $\pm 1$  dB for harmonics 20 dB down and  $\pm 5$  dB for harmonics 40 dB down.

## Applications

It is obvious that there are many applications for this method of harmonic analysis, particularly in making early assessments, where quick answers are of more immediate importance than extreme accuracy.

One example is the determination of the harmonic content to be expected from valves and transistors under various operating conditions, based on the published characteristics.

Another example is the measurement of the harmonic content in a coaxial feeder at v.h.f., obtained from a

TABLE 2

	Level from Fig. 2	Rationalised level	sin $\theta$
0°	0	0	0
10°	3.5	175	-1736
20°	6.7	335	-342
30°	10.0	5	-5
40°	12.6	63	-6428
50°	15.0	75	-864
60°	17.0	85	-766
70°	18.5	925	-9397
80°	19.5	975	-9848
90°	20.0	1.0	1.0

plot of the feeder voltage along a slotted line. In an application of this nature several precautions are necessary, but with a relatively high harmonic content and low v.s.w.r., the results obtained can be substantially correct.

## Acknowledgement

The author wishes to express his thanks to the Director of Engineering, The Marconi Company Ltd., for permission to publish this article.

## REFERENCES

- 1 D. C. Espley and L. I. Farrer. "Direct Reading Harmonic Scales." *Experimental Wireless*, April, 1934, p. 183.
- 2 H. C. Parr. "Harmonic Analysis," *Wireless World*, March, 1962, p. 106.

# BOOKS RECEIVED

**101 Ways to Use your Audio Test Equipment**, by Robert G. Middleton. A book which the home constructor of audio equipment will find interesting. Test equipment used includes an audio oscillator, square wave generator, audio wattmeter, harmonic distortion meter, valve voltmeter and multi-purpose (current-ohm-volt) meter. Initially, nine checks are described for testing the test equipment. The remaining equipment tests are grouped under three main sections—amplifiers, components and systems. Originally published in America in 1959. Pp. 136; Figs. 150. Price 18s. W. Foulsham & Co. Ltd., Yeovil Road, Slough, Bucks.

**Pick-ups: The Key to Hi-Fi**, by J. Walton. In this book, the author, who has spent many years on research into the design of pickups and whose name is familiar to W.W. readers, presents practical advice based on the conclusions drawn from his research. In the introductory chapters definitions of fundamental terms are given, including compliance and tracking weight, stylus mass and distortion and stereo pickup separation. Succeeding detailed chapters cover recording characteristics, requirements from the pickup, pickup arms, practical use of the pickup, and fault diagnosis. Three appendices give details of calculations, record-reproduction correlators, references and further reading. Pp. 100; nearly 40 Figs. Price 10s. Sir Isaac Pitman & Sons Ltd., Pitman House, Parker Street, Kingsway, London, W.C.2.

**Musical Instruments and Audio**, by G. A. Briggs. A comprehensive, lucidly written and sometimes humorous treatment of audio characteristics, and the acoustic principles of musical instruments. The breadth of coverage is very wide and includes aspects such as directional characteristics, formants, distortion, electronic instruments, harmonic structure and tone generation. Separate chapters are devoted to the piano and to the tuning of different instruments. Where the humorous approach has been made, points in the text are supported by cartoons, some of which are reproduced from Punch. Pp. 240; Figs. 212. Price 32s 6d. Warfedale Wireless Works Ltd., Idle, Bradford, Yorkshire.

**B.B.C. Handbook 1966**. Contains facts, figures and general information relating to the organization and services of the B.B.C. These cover the radio and television services including analysis of programme material and audiences. Comprehensive sections are also included on the external services and engineering arrangements: the latter contains maps showing the limits of television service areas and notes on how to get the best reception, local interference, etc. Pp. 259. Price 7s 6d. British Broadcasting Corporation, Broadcasting House, London, W.1.

**ITV 1966**. The annual publication of the Independent Television Authority which contains a wide variety of information ranging from audience figures, programme popularity, advertising control, staff organization and technical operation. In a separate section covering I.T.A. transmitters, details of location, channel frequencies, and e.r.p., together with maps showing primary, secondary and fringe area coverage of each station, is given. Another section gives details of each of the programme companies. Pp. 224. Price 7s 6d. Independent Television Authority, 70 Brompton Road, London, S.W.3.

## OUR NEXT ISSUE

The April issue of *Wireless World*, which will be published on March 21st, will include a survey of communications receiver techniques, together with tabulated information on the receivers available in this country. It will also contain a preview of the Audio Festival and Fair which is to be held at the Hotel Russell, London, W.C.1, from April 14th to 17th.

There will also be the usual quota of technical articles including one on the applications of the variable gain amplifier discussed theoretically in this issue.

# WORLD OF WIRELESS

## Moon Signals via Jodrell Bank

THE soft-landing of instruments on the moon for the first time by the Russian Luna 9 on February 3rd enabled close-up pictures of the moon's surface to be transmitted to earth. The frequency of the transmitter, 183.6 Mc/s, was made known by the Russians and signals were received by the Manchester University 200 ft radio telescope at Jodrell Bank at 10 dB above noise level. The frequency modulated carrier, when demodulated gave a.f. signals which were recognized to be facsimile transmissions and efforts were then made to locate a suitable photographic receiver. A Mufax machine, similar to normal newspaper photographic receivers, was provided by the *Daily Express*. The receiver required a.m. signals of 1.3 kc/s or 1.9 kc/s (with bandwidths of 1 kc/s or 1.5 kc/s respectively), but the information available took the form of a 1.9 kc/s tone, frequency modulated with a deviation of  $\pm 400$  c/s (the limits representing black and white) and consequently an f.m. to a.m. converter was required—also a Muirhead equipment and supplied by the *Daily Express*. Recordings made prior to the acquisition of the receiver and converter were found to be of no value. Picture transmissions continued, interposed with telemetry information, and eight pictures were received, not all complete, some of which appeared in the British Press before they were shown publicly in the U.S.S.R. The cessation of transmissions a few days later was reported to be due to failure of the supplies—batteries and/or "solar" cells.

The Muirhead photographic receiver (a modified D700) uses light from an intensity-modulated gas-discharge tube focused on to a drum covered with photosensitive paper. The drum is rotated at 60 rev/min (being controlled by a tuning fork standard of 1,020 c/s, amplifier and synchronous hysteresis motor) and the light beam scans the drum helically so that a density of 100 lines/in is obtained. The formation of an 8 in picture would thus take about 14 min. The exposed photographic paper is then required to be developed in the normal manner. The exact form of the scanning equipment aboard Luna 9 is not known, and the "index of co-operation" (drum diameter  $\times$  scanning density) was not the same, resulting in distorted pictures.



## Results of Servicing Examinations

IN the annual report for the year ended February 28th 1965 of the Radio Trades Examination Board, the results of the four practical examinations conducted by the Board late in 1964 are recorded, and these are shown in the table. 1963 results are given in brackets.

Examination	Entered	Passed	Failed	Absent
Intermediate Radio and Television Servicing	1,704 (2,110)	1,081 (1,430)	565 (601)	58 (59)
Final Radio and Television Servicing	698 (547)	462 (400)	226 (139)	110 (8)
Intermediate Electronic Servicing	218 (151)	154 (89)	61 (51)	3 (11)
Final Electronic Servicing	21 (10)	14 (7)	5 (2)	0 (0)

For three of the examinations the number of candidates has been increasing but for the Intermediate Certificate in Radio and Television Servicing the number has decreased. The Council has been very concerned about this decrease and the Report contains some of the possible reasons to explain the decrease. As pointed out in the Report, entry for the practical examination is dependent on the number of candidates who pass written papers set by several institutes and there has been a drop in the number of students attending approved courses of study. Another factor is the growing popularity and interest in the wider aspects of electronic servicing rather than the limited field of radio and television servicing. In addition, however, it appears that there has been lack of support and encouragement from employers, reflected by their reluctance to release staff for attendance at courses.

## Integrated Circuits

THE increasing use of integrated circuits is reflected by recent announcements from two American firms. The Radio Corporation of America is now manufacturing colour television receivers for marketing later this year with silicon chip integrated sound circuits containing up to 26 components. The second announcement was made by Motorola Semiconductor Products, Inc. The Company has started marketing integrated circuits for use by the amateur. Circuit configurations available are a binary bias driver, two types of flip-flop and a 3-input expandable gate.

## Audio Fair

TICKETS for the International Audio Festival and Fair, to be held at the Hotel Russell, Russell Square, London, W.C.1, from April 14th to 17th, are now available free. Requests to the Editorial Office of *Wireless World* for tickets, which admit two, should be accompanied by a stamped addressed envelope. They are valid from 4-9 p.m. on the 14th, from 11 a.m.-9 p.m. on the 15th and 16th and from 11 a.m.-8 p.m. on the 17th. A limited number of tickets are available for the trade session from 11 a.m. to 4 p.m. on the opening day but requests for these must be made on business notepaper.

The illustration shows an experimental model of a video telephone developed by the Automatic Electric Company, a subsidiary of General Telephone and Electronics Corporation in the United States. A 16 mm vidicon television camera is used, and voice communication can be made either by a conventional telephone handset or by a microphone installed within the console.

The number of exhibitors at this year's Fair is approximately the same as last year but many of the rooms being used for demonstrations are larger. Most of the 85 exhibitors will have demonstration rooms as well as booths in the main exhibition area. In our next issue we will include a review of the Show.

**Help for the Housebound.**—A joint experiment by the G.P.O., the Manchester Corporation Welfare Services Department, the North Western Electricity Board and the Post Office Engineering Union is being conducted in Manchester to investigate the use of the electricity mains wiring for emergency communication between an elderly housebound person and a nearby neighbour. The system used is the Labgear Portaphone, a loudspeaking intercommunications arrangement which utilizes mains wiring for interconnection purposes. Communication is possible over a distance of approximately  $\frac{1}{2}$  mile depending on the complexities of the mains distribution network. Two units, one at each end of the communication path, are connected to any mains points on the same phase and provide simple two-way voice communication controlled by a press-to-talk arrangement. In the experiment, announced by the P.M.G. last December, about 40 housebound people in selected districts on the eastern side of Manchester are to be provided with equipment by the Post Office and installation will be undertaken on a voluntary basis by members of the Post Office Engineering Union.

An international hook-up for high-speed news transmission was used recently by Standard Telephones and Cables Ltd. when demonstrating its GH 205 telephone-speed data communication system. The hook-up took place between the *Washington Post*, the Newspaper Society in London and Agence France Press in Paris; the equipment was installed in the Council Room of the Newspaper Society. Using normal telephone speech channels copy was passed at speeds up to 1,250 words per minute—18 times faster than conventional teletypewriter speeds. In the system, messages are punched on paper tape as for standard teletypewriter or automatic telex transmission. Contact is then established by telephone, the information on the tape is converted into pulses which are transmitted over the telephone line via suitable tone conversion apparatus. At the receiving end, incoming tape is fed into reproducer sets to obtain printed copy which if necessary can be transmitted to local offices over normal teletypewriter channels.

**Broadcast Receiving Licences.**—During the last six months of 1965 the number of combined television and sound licences in the U.K. increased by 157,891 bringing the total to 13,515,894. Sound only licences fell by 88,719 to 2,678,155; this figure includes 658,200 for receivers in cars which represents an increase of 19,588.

**Police Use New Facsimile Communication System.**—Instead of using the conventional methods of communication between headquarters and divisional offices, Bristol police are now using a facsimile system. By this method the facsimile of any written or printed matter—for example, maps, sketches, identikit pictures—can be transmitted to different centres. Advantages are a much higher speed of transmission of typed material, freedom of errors on the received copy and the fact that the system cannot be tapped. The system has been produced by Muirhead & Company in liaison with the Bristol Constabulary and with the assistance of the General Post Office Advisory Service.

**T.E.M.A. Awards.**—For the eighth successive year the Telecommunication Engineering and Manufacturing Association has held a competition for the best final-year apprentice of its eight member-firms. Awards of £25 were presented to J. Daniel, B.Sc., graduate-in-training with G.E.C., P. S. Casey, student apprentice (A.T. & E.) and P. G. Howard, technician apprentice (A.T. & E.), at the Association's annual dinner on February 8th.

**Computer Presented to College.**—A 10-year-old Ferranti Pegasus computer has been presented to the Northampton College of Advanced Technology, London, E.C.1, by the National Research Development Corporation. During its life the computer, which has always been based at the College, has averaged a 12-hour day. The N.R.D.C. paid £45,000 for the computer but they have recovered more than this sum by charging industrial and commercial firms £30 an hour for use of the computer. A great deal of work has also been done for universities on a non-profit basis.



A new American 140-ft radio telescope can be sighted to within 0.003" and will maintain this accuracy in winds up to 15 m.p.h. The telescope is in use at the U.S. National Radio Astronomy Observatory, Green Bank, West Virginia. Shouldering the weight of the massive yoke and dish are a 210 ton shaft and a 167 ton mirror-finished bearing of 17 ft 6 in diameter. Five months were spent in carefully grinding and polishing the bearing and the resultant accuracy is such that the telescope rotates on a film of oil only 0.005 in thick.

**N.E.R.C.**—The first annual report of the National Electronics Research Council, presented by the chairman, Earl Mountbatten, records a proposal to alter the Articles of Association so as to incorporate in its constitution "every organization, large and small, which is interested in the success of the British electronics research effort." This change has been necessitated by the need for increased income.

A new £550 studentship for research purposes is announced by the Department of Electrical Engineering at the University of Newcastle-on-Tyne; normal period of tenure will be two years but with the possibility of renewal for a third year. The studentship has been endowed by Electrosil Ltd., of Pallion, Sunderland, Co. Durham.

A two-day course of lectures on Component Reliability, under the leadership of G. W. A. Dummer, of R.R.E., is being held at the Bristol College of Science and Technology, Ashley Down, Bristol 7, on March 8th and 9th. The fee, including meals, is £5.

# PERSONALITIES

The forty-fourth award of the I.E.E. Faraday Medal has been made to J. A. Ratcliffe, C.B.E., F.R.S., "in recognition of his extensive researches on the physics of the ionosphere, and of his studies on the propagation of low-frequency radio waves." Mr. Ratcliffe, who graduated at Sydney Sussex College, Cambridge, remained at the University, apart from the war years, until his appointment in 1960 as director of what is now the Radio and Space Research Station at Slough. He is retiring at the end of February. At Cambridge he divided his time between teaching physics and research work on radio propagation. During the war Mr. Ratcliffe was closely concerned with the development of radar at the Telecommunications Research Establishment, where he formed



J. A. Ratcliffe.

the Post-Design Service which is instrumental in converting experimental gear into radar equipment for service in the R.A.F. Mr. Ratcliffe also founded the radar school for the Army at Peterham.

J. R. Brinkley, managing director of Pye Telecommunications Ltd., and R. M. A. Jones, managing director of E. K. Cole Ltd. and vice-chairman of the Telephone Manufacturing Company, have been appointed additional deputy managing directors of Pye of Cambridge Ltd., the holding company of the Pye-Ikco group. Mr. Brinkley was in the Home Office Communications Directorate from 1942 until 1948 when he joined Pye and a year later became technical director of Pye Telecommunications. He is a member of the board of the British Space Development Company. Mr. Jones, who was a Lieut. Colonel in Royal Signals during the war, joined Pye in 1936 and has for many years been managing director of Pye TV Manufacturing Co. at Lowestoft. On the acquisition of Ikco by Pye in 1962 he also became managing director of E. K. Cole Ltd.

R. J. Lees, M.A., B.Sc., director of the Ministry of Aviation Signals Research & Development Establishment at Christchurch, Hants, for the past three years, was recently appointed deputy director (equipment) at the Royal Aircraft Establishment, Farnborough. Mr. Lees, who is 48, joined the Telecommunications Research Establishment, Malvern, in 1939 where he remained until 1959 when he was appointed head of the Instruments and Air Photography Division at R.A.E., Farnborough. While at Malvern he was successively director of scientific research (guided weapons) and head of airborne radar.

Detek D. Arnold has been appointed director of production for the Solartron Electronic Group. He was formerly works manager with Hewlett Packard Ltd., and was for three years manufacturing manager with Tektronix in Guernsey.

Sir Harold Bishop, C.B.E., B.Sc. (Eng.), F.C.G.I., M.I.E.E., director of engineering of the B.B.C. from 1952 until his retirement in 1963, has been elected an honorary member of the I.E.E. "for his contributions to the science and art of sound and television broadcasting and their application both at home and overseas." Sir Harold, who received a knighthood in 1955, started his professional career in the engineering division of the Office of Works. He joined Marconi's in 1922 and was concerned with the setting up and operation of the London 2LO broadcasting station in Marconi House, Strand. In 1923 he transferred to the newly formed British Broadcasting



Sir Harold Bishop.

Company as senior superintendent engineer. Sir Harold is now a consultant to B.I.C.C. and a director of International Research & Development Company of Newcastle-upon-Tyne.

David D. Jones, B.Sc., M.Sc., D.I.C., has been appointed head of the laboratories of Associated Semiconductor



D. D. Jones.

Manufacturers Ltd., in succession to the late Dr. E. G. James. He joined the Hirst Research Centre in 1947. During 1951 and 1952 he was a post-graduate student at Imperial College, London, where he obtained his diploma in electrical engineering. On returning to G.E.C. he helped to build up a semiconductor applications team. Mr. Jones, who is 44, studied at the University College of Wales, Aberystwyth, where he graduated with an honours degree in physics. He obtained his M.Sc. in mathematics by evening study at Chelsea Polytechnic, London. Associated Semiconductor Manufacturers Ltd., is the joint Mullard-G.E.C. company developing and manufacturing Mullard semiconductor devices.

Graham D. Clifford, C.M.G., secretary of the Institution of Electronic & Radio Engineers since 1937, left London on February 8th on a world tour. He will be visiting Israel, India, Singapore, Australia, New Zealand, Fiji, Hawaii, the U.S.A. and Canada with the object of promoting the exchange of information in electronic and radio engineering. Mr. Clifford will be in Canada when Lord Mountbatten speaks in Ottawa on April 14th on the work of the British National Electronics Research Council (of which Mr. Clifford was honorary secretary until last September) and the selective dissemination of information.

J. P. Wykes, O.B.E., A.M.I.E.E., manager of the Maritime Division of the Marconi Company since 1956, retired on January 31st. After 11 years' service as a radio operator with Marconi Marine he worked as a design engineer with the Marconi Company. In 1946 he became assistant engineering-chief (test), and was works manager at Chelmsford from 1949 to 1956.

Dr. G. G. Macfarlane, director of the Royal Radar Establishment, Malvern, since 1961, is to receive the honorary degree of LL.D. from the University of Glasgow on its Commemoration Day—June 22nd. Dr. Macfarlane, who graduated at Glasgow in 1937 and then did two years' postgraduate research at Dresden where he obtained his Dr. Ing. degree, was throughout the war at T.R.E. (now R.R.E.) concentrating on mathematical problems in radar and microwave physics. He became head of the mathematical group in 1945 and from 1953 to 1960 was deputy chief scientific officer at R.R.E. He then became deputy director of the National Physical Laboratory but returned to R.R.E. the following year as director.

E. J. Jordan, Assoc.I.E.R.E., recently joined Audio & Design Ltd., of Maidenhead, as a director. He will be responsible for the development and design of specialized professional and domestic loudspeakers. After spending six years in the service department of the G.E.C. he was for twelve years with Goodmans Industries where from 1959 to 1964 he was senior engineer.



E. J. Jordan

Since 1964 until his new appointment Mr. Jordan has been technical director of Jordan-Watts Ltd., of Hayes, Middx., where he produced the first "modular" loudspeaker.

A. C. Robb, M.Eng., Ph.D., M.I.E.E., has joined Counting Instruments Ltd., of Borcham Wood, Herts, as chief engineer. Dr. Robb, who graduated at Liverpool University where he obtained a master's degree for postgraduate work, had been with Belling & Lee since 1961, first as technical manager and, since 1962, as technical director. Prior to joining Belling & Lee he spent some time at Glasgow University as a research fellow working on the design of high-voltage particle accelerators where he gained his doctorate for related studies. In 1963 Dr. Robb contributed an article to *Wireless World* on the problems associated with u.h.f. television reception.



The 40th anniversary of Baird's first demonstration of television to members of the Royal Institution at his Frith Street, Soho, laboratory, was commemorated recently at a dinner attended by members and guests of the Television Society. In the photograph, taken in the building in which the original demonstration was staged, W. C. Fox (left) The Times correspondent who attended the demonstration, is describing the occasion to members and guests. On the right is W. Toynton, the first man to be televised by Baird in 1926.

W. I. Flack, Assoc. I.E.E., a member of the panel whose discussion on integrated circuits we published in our January issue, has been appointed technical director of G.E.C. (Domestic Equipment) Ltd. Mr. Flack is also a member of the management team of Radio & Allied Industries, the radio and television receiver manufacturing company in the G.E.C. Group. He joined R.A.I. in 1957 after spending 14 years with the Telegraph Condenser Company.

Roy F. Stevens, the new president of the Radio Society of Great Britain, which has a membership of some 13,500, is not in radio professionally but has been a licensed amateur transmitter (G2BVN) since 1937. Throughout the war he was in the R.A.F. His special interest in amateur transmitting is s.a.b. operation in the h.f. band. The Society's executive vice-president is F. K. Parker (G3FUR) who last year formed Park Air Electronics, of Stamford, Lincolnshire, who market electronic aids for aircraft.



R. F. Stevens

B. R. Coles, B.Sc., D.Phil., reader in physics at Imperial College, London, has been appointed to the chair of solid state physics at the College.

J. B. Race, AM.I.E.E., has been appointed general manager of the Cambridge Instrument Company's factory at Chesterton Road, Cambridge. He was formerly works director of E.N.V. Engineering Ltd. During the war he served in the Fleet Air Arm, leaving with the rank of Lieutenant Commander.

## OBITUARY

Edred Jeffrey, AM.I.E.E., who will be known to many readers of *Wireless World* as contributor of the articles on a high-gain phase splitter in 1947 and a low-cost stereo amplifier in 1961, died on January 5th at the age of 49. Mr. Jeffrey had been with the Sperry Gyroscope Company since 1956 prior to which he was for a short time technical executive to Modern Telephones Ltd. At Sperry's he was successively manager engineering services and product group manager guided weapons. In this latter capacity he was responsible for all the missile activities in the company.

Gordon Scott Whale, who died on board R.M.S. *Andes* on January 9th, founded the North Wales Wireless College in Colwyn Bay, of which his son Neville is now principal. Mr. Whale, who was 72, was an operator with the Marconi Company at their stations in Clifden, Ireland and Caernarvon, N. Wales, until 1918 when he opened the Colwyn Bay college. He also opened (in 1937) the Wireless College, Southampton, which was closed in 1940 due to enemy hostilities.

James Norman Walker, technical sales engineer with Eddystone Radio since 1946, died on January 30th, aged 60. "Jerry" Walker, as he was affectionately known, was an active radio amateur with the call G5JU. He was commissioned in the technical branch of the R.A.F. in 1940 and was involved in the development and operation of "Oboc."

# NEWS FROM INDUSTRY

## ELECTRONIC TELEPHONE EXCHANGES

RECENTLY at the annual dinner of the Telecommunications Engineering and Manufacturing Association, the Postmaster General stated that approximately £350M is to be spent during the next four years on telephone exchange equipment. In addition, he has decided that in future all new small and medium sized telephone exchanges will be electronic.

Several British companies—Associated Electrical Industries, the Plessey group (including Automatic Telephone and Electric Company and Ericsson Telephones) and Standard Telephone and Cables—have collaborated with the G.P.O., under the auspices of the Joint Electronic Research Committee, on the development of electronic exchange systems. These systems, REX (from A.E.I.) and PENTEX (from Ericsson) use only one electromechanical component. This is a reed switch comprising two blades of magnetic material sealed in a glass envelope and actuated by an external magnetic field.

Advantages of electronic exchanges are the high speed of operation, high reliability and low servicing charges, and saving of space.

The basis of an electronic exchange as in, for example, the REX system, is the control equipment which consists of three main sections. These are—scanners and registers which determine the source and destination of a call; markers and interrogators which decide switching and speech paths; and common control which co-ordinates the activities of the scanners, registers, markers and interrogators in accordance with stored programme instructions to ensure that a call is routed by using the available switching equipment as efficiently as possible.

## SWISS DEFENCE CONTRACTS

THE Swiss Government have signed a multi-million dollar contract with the Hughes Aircraft Company, of California, for an air defence system coded Florida. The value of this order is believed to be about £15M.

The system will comprise a network of military radar stations and a number of air defence centres which will be used to control Switzerland's surface-to-air missiles and interceptor aircraft. The majority of the equipment will be made by Hughes and will include the company's new long-range, three-dimensional radars. These will provide simultaneous range, height and bearing

data, even under heavy pressure from counter-measure apparatus. The computing will be on Hughes H-3324 general-purpose computers.

Ferranti Ltd. are manufacturing the data link equipment, believed to be worth about £0.5M, for this project.

The Plessey Company have also received a Swiss defence contract. This contract, which is understood to be worth over £1M, is for a comprehensive u.h.f. ground-to-air communications system for use by the Swiss Air Force. Similar equipment to that called for in the contract is being used in the armed forces of the U.K., the Commonwealth and many other countries throughout the world.

## Microelectronics Firms Join Forces.—

Two major microelectronics companies in Britain—Marconi Company and Ferranti—have signed a licensing agreement under which Marconi's will manufacture and sell the advanced range of silicon microcircuits designed and sold by Ferranti under the name of Micronor II. Extensive production plant for Micronor II is being commissioned by Marconi's microelectronics division at Witham, and by Ferranti at their Manchester headquarters. Micronor II is a new range of ultra fast silicon integrated circuits designed for use in computer and other logic applications. Many different circuits are available including multiple gates, power stages, J-K flip-flops, etc. The full range is already in quantity production in Manchester. The two companies now manufacture more than 70 per cent of the silicon integrated circuits made in the United Kingdom and the new agreement should further strengthen their position in the U.K. and also aid them in overseas markets. Marconi's microelectronics division will continue to develop and manufacture micro-electronic components and units. Up to now, their range has been radar specialized, mainly producing units for their Myriad and (E.E.L.M.) System 4 computers.

## G.E.C. Win \$3.5M Contract.—G.E.C.

(Telecommunications) Ltd., of Coventry, have received a contract worth over £1M for a complete semiconductor microwave telecommunication system for the northern zone of Chile. It will link Santiago—the capital—and Arica, a distance of 1,120 miles, and will provide up to 960 two-way telephone circuits. Twenty-seven repeaters are used in the system and spur links are to be provided to 21 towns en route. This order is the ninth that G.E.C. have received for its new range of semiconductor microwave radio equipment, which was introduced only a few months ago. The first of these nine orders is

scheduled to be completed this year and the Chile order in 1968.

## Satellite-tracking Aerial Contract.—

The British Aircraft Corporation have received a contract from the SHAPE Technical Centre for a 30-ft diameter satellite-tracking aerial, with a Cassagrain sub-reflector. The parabolic dish is to be constructed out of stretch-formed light-alloy sheet. This method of construction has resulted from the company's experience in the aircraft field. Profile accuracy using this method of construction is maintained to within 0.1 in. The aerial is to be delivered in May of this year to the Technical Centre in The Hague.

Rediffusion are to provide a wired television and sound network to all Corporation owned homes of the Welwyn Garden City and Hatfield Development Corporation. The network will be installed and maintained as a Rediffusion Community Service and, to quote the company, "Maintenance will, of course, be by locally based technicians up to the full standard of a public service." Four television and four sound programmes will be supplied initially with room for more at a later date. Rediffusion are to install the system at their own cost and the Corporation will pay an annual premium for this service.

## £100,000 Bulgarian Order.—Standard

Telephones and Cables Ltd. have received a contract worth more than £100,000 from the People's Republic of Bulgaria for ground and air navigational and communications equipment. S.T.C., who are the prime contractors for this contract, will supply v.h.f. omni-directional ranging beacons (V.O.R.), v.h.f. direction finders and v.h.f. transmitters and receivers.

## Amalgamated Wireless (Australia)

Ltd., of Sydney, have appointed Livingston Laboratories Ltd., of Greycaines Estate, Bushey Mill Lane, North Watford, Herts, as sole U.K. representatives for their range of telecommunication test equipment.

Radiotelevisione Italiana, the Italian broadcasting organization, have placed an order for 150 image orthicon camera tubes with the English Electric Valve Company, of Chelmsford. This follows an earlier order for 250 E.E.V. image orthicon tubes.

Microcircuits.—Electrosil Ltd., of Pallion, Sunderland, are to start manufacturing integrated circuits later this year. They are also to market automatic integrated circuit testers.

# RC ACTIVE FILTERS

—OR THE DEATH OF THE INDUCTOR?

THE interest created in the last decade or so in RC active filters, i.e. filters using combinations of R, C and active elements, is understandable in view of the scorn now placed upon the inductor. This has arisen partly because the inductors required for low-frequency selective filters are undesirably large. In addition, the constraints placed upon components in the field of microelectronics have left us with no alternative but to search for methods of simulating either the inductor or tuned circuits. (Inductors have been used in thin-film circuits, but there is a serious limitation in that the Q of inductors decreases as the square of the scaling factor.) Although it would be premature to forecast the fate of the inductor, it would seem that the decline has set in and for low frequencies, at least, RC filters can be made which are as good as LC circuits.

The recent I.E.E. colloquium on this subject was mainly concerned with low frequencies, but some of the techniques discussed can be extended to higher frequencies. The subtitle is perhaps a little unfair because whilst RC active filters are ousting the inductor at low frequencies, it would appear that for high-frequency work passive acoustic or mechanical resonators hold more promise than active filters.

## Sensitivity and Q

It was pointed out by R. C. Foss (Plessey) that some configurations of active filter were no more complex than some present-day integrated circuits which are available quite cheaply in the U.S.A. There were problems, of course, and in a common type of active filter (using high gain amplifiers) the sensitivity (of Q, mainly) to component variations and tolerances was a major headache, particularly for integrated circuits. However, the situation was somewhat eased by the fact that resistor ratios can be maintained fairly accurately—to better than 1%—and gain was a commodity relatively easy to come by. Gain is important, of course, because the Q of an RC active filter is proportional to the square root of gain. For example, for a Q of 100 with a stability of 5%, the required gain is over 100 dB. A relation connecting these quantities has been derived by McVey<sup>1</sup> and is  $Q_{max} = \sqrt{A\delta}$  where  $Q_{max}$  represents the maximum Q (quality factor) resulting from an amplifier gain of A, and  $\delta$  is the maximum permissible departure of Q from its required value ( $\Delta Q_{max}/Q$ ). (For some applications Dr. Foss felt that this relation was more appropriate than that giving the limiting value of  $Q_{max} = \frac{1}{2}\sqrt{A}$  since a circuit operating with this would be unduly sensitive to variation in the unstabilized loop gain.)

Broadly speaking two general approaches to the synthesis of RC active filters to give desired transfer functions have been recognized since the early 1950's. One uses R and C elements, with amplifiers (of very high gain) as the active elements, and the other uses negative impedance converters (n.i.c.s) as the active elements to provide simulated inductance. A third, less common, approach is referred to later.

R. J. A. Paul (University College of North Wales) out-

lined a new synthesis technique using amplifiers with voltage gains of 2 (and also -1 in some cases) and one-port or two-terminal RC networks. This is described in detail in a recent paper<sup>2</sup>. The method also permits the realization of transfer functions with adjustable coefficients.

A. G. J. Holt and J. I. Sewell (University of Newcastle-upon-Tyne) described a method employing multiple-loop feedback and a single operational amplifier, based upon what is known as node introduction in a  $2 \times 2$  admittance matrix—a procedure which involves a substantial amount of matrix algebra. Two approaches for obtaining circuits to represent both voltage and current-inversion n.i.c.s using high-gain amplifiers were outlined by A. G. J. Holt and J. Carey. Dr. Holt pointed out that while designs for active filters using high-gain operational amplifiers were made stable with a well-defined gain by feedback, n.i.c.s not using such high-gain amplifiers tend to be somewhat dependent on transistor characteristics.

## R.R.E. approach

The Royal Radar Establishment was represented in force—four out of the ten papers read were from Malvern—by P. J. Baxandall, F. E. J. Girling, E. F. Good and R. L. Ford. Mr. Baxandall discussed generally various active filters developed at R.R.E. including symmetrical twin-T feedback types (the normal twin-T network is not exactly symmetrical but is made so by addition of two series RC chains), integrator-plus-lag and two-integrator types. He stressed the advantages in avoiding mathematical complexity as much as possible and maintained that comparatively simple, and perhaps more familiar,

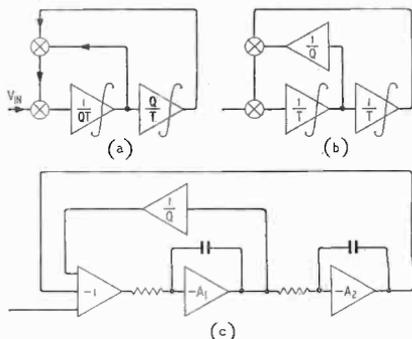


Fig. 1. A two-integrator type of active RC filter, requiring only two reactances.

techniques could be used to obtain the same results as with some of the more sophisticated methods.

A series LCR circuit may be simulated by providing three voltages with the same phase relationship as the voltages across the  $L$ ,  $C$  and  $R$  elements. Girling showed how two integrators plus feedback could be arranged to give these voltages with respect to a common earth. The ratio  $V_{ol}/V_i$  was equal to  $R/pL$ , in operator notation, hence  $V_R$  could be obtained from  $V_i$  by integration. Similarly  $V_C$  could be obtained from  $V_R$  by integration.  $V_L$  was clearly required and was derived by feedback from  $V_L = V_{in} - (V_R + V_C)$ . This system could be interpreted as shown in Fig. 1(a), but since it was not easy to adjust two integrators separately the arrangement of Fig. 1(b) was adopted. (To achieve the correct signs four amplifiers would be required.) Such a system might appear as Fig. 1(c), requiring only two reactances. A simple modification was described by which corrections could be made for the integrating amplifier gains. With this approach any second-order transfer function could be provided, and such units could be used to produce factors of higher-order functions. Mr. Girling stated that high  $Q$  values and good stability could be so obtained and also both frequency and  $Q$  could be independently varied.

Good described a general second-order active filter based on a single amplifier and the balanced twin-T network plus an additional RC branch. The circuit makes an economical building block for higher-order filters and can provide low-pass, tuned circuit, high-pass or notch response. Even though this type of active filter

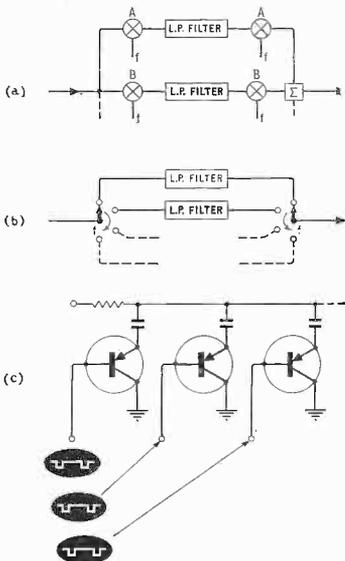


Fig. 2. The basis of the  $n$ -path, digital or sampled data type of active filter.



Fig. 3. The low-pass function is translated in  $n$ -path filters to a band-pass function centred about frequency  $f$ .

is more sensitive to component variations it is well suited to some applications.

A form of active filter was outlined by Ford in which integrators replaced the reactive elements used in passive LC ladder networks. One advantage of this technique is the ease with which bandwidth and centre frequency can be made continuously variable by a voltage-controlled switching technique.

### N-path filters

The third type of active filter referred to earlier is the  $n$ -path filter, which is also known as a digital filter or sampled-data filter. The essential difference between this type and preceding types is that operation is dependent on non-linear active elements rather than the usual linear elements. The  $n$ -path filter falls in the general category of time-varying circuits. Basic work in this field was done in the 1940's and interest was stimulated again in 1960<sup>3</sup> mainly because this method allows sensitivity and high- $Q$  problems to be overcome.

A. R. Owens (University College of North Wales) and R. K. P. Galpin (A.E.I.), gave separate papers describing such filters. Basically, a low-pass filter function is arranged using passive elements only.  $N$  identical low-pass filters are arranged in parallel, each operating between input and output modulators.

The general case is shown in Fig. 2(a), where the modulators (multipliers)  $A, B, \dots$  are supplied with suitably phased sine-waves of frequency  $f$ . (A particular case was referred to in which only two paths are required, the functions supplied to  $A$  and  $B$  being in phase quadrature.) The property of interest is that a band-pass transfer function is obtained which is a translated version of the low-pass characteristic and centred about the frequency  $f$  (Fig. 3).

A particular system of interest was described in which the modulating functions were achieved by the use of a synchronous switch, operating at the frequency  $f$ , as shown in Fig. 2(b). Fig. 2(c) shows partly how this may be accomplished. Tuning of such a filter was by simply varying the frequency  $f$ . By the use of such techniques  $Q$ 's in the order of thousands can be obtained and centre frequencies of hundreds of kc/s are quite feasible.

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1. "Sensitivity in some simple RC active networks", P. J. McVey, *Proc.I.E.E.*, July 1965.
2. "Active networks synthesis using one-port RC networks", R. J. A. Paul, *Proc.I.E.E.*, January 1966.
3. "An alternative approach to the realization of network transfer functions: the  $n$ -path filter", L. E. Franks and I. W. Sandberg, *B.S.T.J.*, September 1960.

### European Station Chart

UNFOLDED copies of the chart showing the operating frequencies of Europe's long-wave and medium-wave broadcasting stations which was included in last month's issue, are obtainable from our Publishing Dept. price 2s including postage and packing.

# Low-impedance Tape Pre-amplifier

By R. HIRST

THE output from a tape head is more often than not treated as a voltage output to be fed into a substantially high impedance. If the output voltage is monitored when replaying from a standard reference tape, at a speed of  $3\frac{1}{2}$  in/sec with a constant current recording, we arrive at the shape of Fig. 1. This is a curve familiar to most engineers. Normally the pre-amplifier would be of high impedance, the compensation taking the form of a low-frequency boost "mirroring" the curve of Fig. 1. The use of a high impedance presents a difficulty in maintaining good signal-to-noise ratio and is also conducive to hum pick-up. As transistors are basically low-impedance, current-operated devices, they appear at first sight an incompatible match to replay head characteristics, as normally presented, i.e., as an open-circuit e.m.f.

Advantage may, however, be taken of the open-circuit reance with frequency characteristic below 1 kc/s. If the magnetic flux in the toroid is constant and a low enough resistance  $R$  is placed in series with  $L$  (Fig. 2a) the current through  $R$  will remain relatively constant. This in itself is not quite so, as the d.c. resistance ( $r$ ) of the coil  $L$  (Fig. 2b) determines that the low-frequency current response is down by 3 dB when  $R + r = X_L$ .

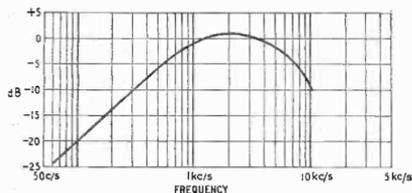


Fig. 1. Playback characteristic from 140  $\mu$ s ref. tape at  $3\frac{1}{2}$  in/sec.

Replacing  $R$  by a transistor in the common-base configuration is the basis of the circuit, shown in Fig. 3. (The input impedance is equal to  $30/I_e + r_{bb'}$ , where  $I_e$  is in mA, for a post alloy-diffused device).

## Input stage

In the circuit shown in Fig. 3, post alloy-diffused transistors (NKT 677) were used for the following reasons:—

- high frequency cut-off
- low noise
- low leakage (typically  $1\mu$ A)
- low  $r_{bb'}$

An  $I_e$  of 3 mA had been chosen for low-noise operation. Under this condition, the input resistance is about 100  $\Omega$ . In order to reduce the impedance further, it would have been necessary to increase  $I_e$ , thus detracting from the low-noise operating point.

Robert Hirst, who recently joined Dictaphone Ltd. where he is working with the research and development team on closed-circuit systems, was previously a senior engineer with Newmarket Transistors Ltd. He is 31.

This low  $I_e$  is also advantageous in allowing a large collector load (22 k $\Omega$ ) to be used, so that the voltage gain of Tr1 is substantial:—

$$\frac{R_L}{R_{in}} = \frac{22 \times 10^3}{10^2} = 220 \text{ approximately.}$$

Should this be fed into a conventional grounded-emitter stage with an input impedance of 1 k $\Omega$  then  $R_L$  would be modified to 950  $\Omega$  and the voltage gain modified to  $950/100 = 9.5$  times.

## Second stage

In order to make use of the voltage gain of Tr1, a grounded-emitter stage was used with an un-bypassed  $R_E$ .

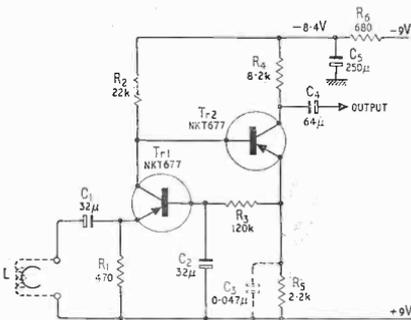
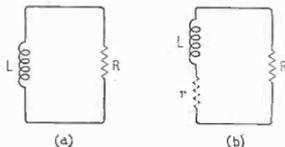


Fig. 3. Circuit of the tape pre-amplifier.

A reasonably high-beta transistor (about 100) was used so that the load presented to Tr1 is around 220 k $\Omega$  ( $\beta R_{L1}$ ) the shunt effect of R3 in series with C2, across R5, being negligible. This value of input resistance was sufficiently high to prevent any appreciable loading of Tr1 collector load.

The voltage gain of Tr2 would normally have been about 100, but this is modified by the unbypassed emitter resistor to approximately—

$$\frac{R_L}{R_e} = \frac{8.2 \times 10^3}{2.2 \times 10^3} = 3.7.$$

In order to check the frequency response of the pre-amplifier (less C3) a 1 H tape head in series with the input was fed from a 10  $\Omega$  source, the generator voltage being constant at 10 mV. (The response is shown in Fig. 4.)

As the C.C.I.R. play-back curve at 3  $\frac{1}{2}$  in/sec indicates an RC time constant of 140  $\mu$ s (Fig. 4) a further C was connected across R5 (C3, dotted in Fig. 3), so that the amplifier turnover point was approximately 1.5 kc/s, this being the point where the actual frequency response was 3 dB below the required response (see Fig. 4). The value of C3 was then calculated so that the amplifier gain was increased by 3 dB at 1.5 kc/s, this being when  $X_{C3} = R_{e1}$ . Since  $f_c = 1.5$  kc/s and  $X_{C3} = R_e = 2.2$  k $\Omega$ , then—

$$C(\mu F) = \frac{10^6}{2\pi f_c X_{C3}} \approx 0.047$$

This produced the final curve of Fig. 5 curve B. (The peculiar small rise in frequency at 8 kc/s and then the resultant gradual fall as the frequency increased was due to the loading of Tr1 collector load, as the reactance of C3 in parallel with R5 modified the input impedance of Tr2. At 15 kc/s,  $X_{C3} = 212 \Omega$ , and

$$R_{i2} = \frac{\beta \cdot X_{C3} R_{e1}}{\sqrt{X_{C3}^2 + R_e^2}} \approx \beta \cdot X_{C3} \approx 20 \text{ k}\Omega$$

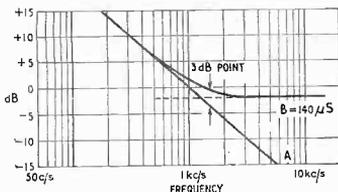


Fig. 4. Curve A shows response of pre-amplifier without C3. B shows the required output with time-constant of 140  $\mu$ s.

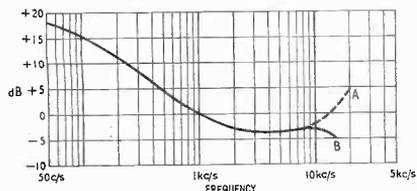


Fig. 5. Response of pre-amplifier including C3 from 10  $\Omega$  source in series with 1 H tape head.

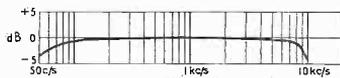


Fig. 6. Response of pre-amplifier to 3  $\frac{1}{2}$  in/sec 140  $\mu$ s ref. tape.

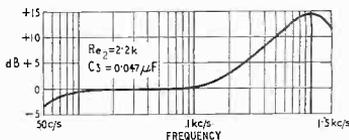


Fig. 7. Response of pre-amplifier when measured from a constant voltage source.

Without this loading of Tr1 collector, the treble response curve would have continued rising (Fig. 5, curve A). However, the decrease of  $R_{i2}$  at high frequencies helps to reduce high-frequency recording bias pick-up when the pre-amplifier was used in a three-head system and also when used as a low-impedance microphone pre-amplifier on record.

#### D.C. conditions

The d.c. conditions are relatively standard but careful thought had to be given to the design, so that the following conditions were met.

- $V_{CE1}$  of Tr1 approximately 1V, for low noise considerations.
- $I_C$  of Tr1 to be small for low noise; also to accommodate a large collector load to implement high voltage gain.
- Collector load and emitter resistor of Tr2 to be a favourable ratio for gain considerations.
- $R_e$  of Tr2 to be large enough to—
  - effect high input impedance.
  - provide a direct voltage for feedback purposes.
  - be complementary with C to provide adequate treble lift.
- R3 to be large enough to obviate loading of R5 and yet sufficient to compensate for temperature variation.

As a result of this the pre-amplifier will accept transistors with a beta between 80 and 180 without any modifications. As this range was thought to be substantial no further measurements were made to accommodate lower betas, although a 220 k $\Omega$  potentiometer in place of R3 and setting Tr2 collector to 4.5V would ensure that almost any transistor may be used in Tr1 position, even down to a beta of 15.

The curves shown in Figs. 5 and 6 did not measurably alter in the temperature range 15°C–45°C. Fig. 7 shows the response of the pre-amplifier when fed from a constant voltage source (e.g. low-impedance microphone) this could quite well be compatible with the treble-lift response required in the record position of a tape recorder operating at 3  $\frac{1}{2}$  in/sec, thus possibly obviating a necessity for compensation switching when used as a replay or record pre-amplifier.

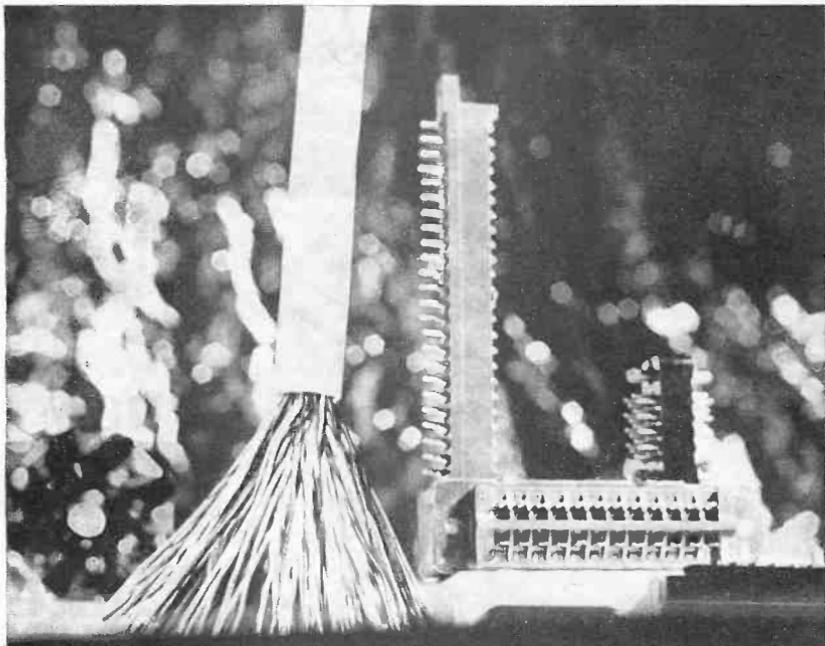
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# 3—Random Events and Variability

By D. A. BELL,\* M.A., B.Sc., Ph.D., M.I.E.E., F.Inst.P.

**Question:** "What is the similarity between the number of Prussian soldiers kicked to death by horses in the years from 1875 to 1894 and the shot noise in a thermionic valve?"

**Answer:** "Both phenomena can be described by Poisson distributions."

THE Poisson distribution is often described as the distribution applicable to "rare events," but the two examples given above indicate dramatically that the word "rare" is meaningless unless a time scale is attached. An event is rare in the Poisson sense if two conditions are satisfied. Firstly, it must be possible to choose elementary intervals of time such that the probability of more than one event occurring in such an interval is negligibly small. This is what is meant by "rare events," but the appropriate elementary interval of time might be a day for the Prussian soldiers and  $10^{-24}$  second for the thermionic valve. Secondly, the (small) probability of an event must be the same for all equal intervals of time. These conditions can be expressed by saying that the events occur individually and randomly: *individually* because we have ruled out the possibility of more than one occurring simultaneously; and *randomly* because the probability of an event is the same for all intervals of time.

## Deriving the Poisson formula

The formula for the Poisson distribution can be derived as follows: there are two ways in which exactly  $n$  events can have happened in total time  $t+dt$ : either  $n$  had already happened at time  $t$  and none has happened in  $dt$ , or  $n-1$  had happened up to  $t$  and one in  $dt$ . If the probability of an event is  $a$  per unit time (and therefore

the probability of no event is  $1-a$ ) and  $P(n,t)$  stands for the probability of exactly  $n$  events in time  $t$ , then  $P(n,t+dt) = (1-a)dt \cdot P(n,t) + a dt \cdot P(n-1,t) \dots (1)$  This can be treated as a differential equation in time:

$$\frac{d}{dt} P(n,t) = \lim_{dt \rightarrow 0} \frac{P(n,t+dt) - P(n,t)}{dt} = -aP(n,t) + aP(n-1,t) \dots (2)$$

The relationship (2) is satisfied if the probability of exactly  $n$  events after lapse of time  $t$  is given by

$$P(n,t) = c^{-at} (at)^n / n!$$

or more generally, the probability of exactly  $r$  events when the average number would be  $m$  is given by

$$P(r) = c^{-m} m^r / r! \dots (3)$$

Note that time is not necessarily the variable involved, and the Poisson distribution is also important in inspection by sampling. Suppose the average defect rate in a certain component is 8 per 1,000, then what are the chances of finding 0, 1 or 2 defective specimens in a box containing a gross? The average risk per component is 8/1,000, so the average or "expected" number of defective components per box of 144 is  $144 \times 8/1,000 = 1.152$ ; and this is the value to be given to  $m$  in formula (3). Putting  $r=0, 1$  and  $2$  in turn, and remembering that  $r! = 1$  and  $0! = 1$ , the values of the probabilities are found to be:  $P(0) = 0.316$ ;  $P(1) = 0.364$ ;  $P(2) = 0.210$ . Since these three probabilities add up to 0.890, subtraction from unity shows that the probability of finding more than two defective components in a gross, i.e.  $\sum_{r=3}^{144} P(r)$ , is 0.11. Tables are

available† of the terms in the Poisson distribution (3) for various values of  $m$  and  $r$  and of the "summed Poisson distribution,"  $\sum_{r=0}^{\infty} P(r)$ , for various values of  $m$  and  $x$ . Fig. 1 shows the Poisson distributions for  $m=0.1, 1$  and  $10$ . The Poisson distribution for  $m=10$  has been re-drawn to a larger scale in Fig. 2, and a corresponding Gaussian distribution superimposed on it. The two distributions are fairly similar, and in the limit as  $m$  becomes large the Poisson becomes identical with a Gaussian distribution. Remembering that the condition for Poisson to be applicable is not that events should be infrequent but rather that they should occur individually at random, there is no reason why  $m$  should not be large: returning to the example of thermionic emission, a current of 1.6mA corresponds to an average of  $10^7$  electrons per nanosecond, so  $m$  in this case is likely to be large for any practicable time interval.

In Fig. 2 we said that "a corresponding Gaussian was superimposed on the Poisson": how, then, do we pick

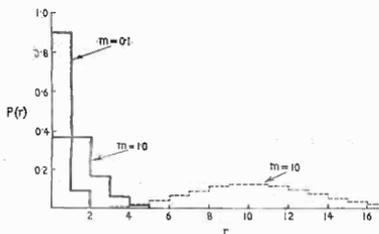


Fig. 1. Full lines, Poisson distributions for  $m=0.1$  and  $m=1$ ; dotted line for  $m=10$ .

\*University of Hull.

†In books by Fry and Huntington and May as listed in the bibliography last month. More extensive tables are given by E. C. Molina in "Poissons exponential binomial limits," Van Nostrand, 1942.

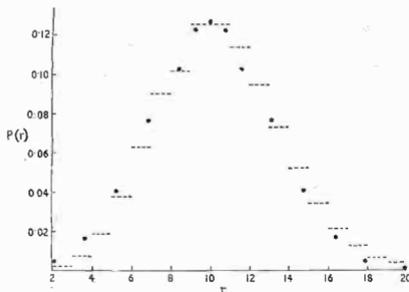


Fig. 2. Comparison of Poisson and Gaussian distributions. Dotted steps: Poisson with  $m = 10$ ; points: Gaussian with  $x = 10$  and  $\sigma = \sqrt{10}$ .

the parameters of the Gaussian to correspond with the Poisson? The characteristics of a probability distribution can be summed up by its position along the axis, its spread, and its shape, the first two being definable by a single number each while the shape is more complex.

At this point it is desirable to recapitulate the meaning and purpose of a "probability distribution." Suppose we measure accurately the resistances of a large number of carbon composition resistors of nominally  $1k\Omega$  resistance, and for the sake of illustration let us make the rather doubtful assumption that the values will be spread at random round the nominal according to the "normal law of errors," i.e. a Gaussian distribution. If we measure on a bridge using a decade resistance box, the values will not be spread continuously in the mathematical sense, but will be grouped in "classes" of extent corresponding to the smallest step on the decade box. But even if the decade box goes down to steps of  $0.1\Omega$  we may decide to use steps of  $10\Omega$  as our classes, both because differences of less than 1% are of little significance in this class of resistor and because one needs as many as possible in each class to get a smooth distribution ("to minimize the fluctuations due to sampling" is the formal statement); and in order to obtain a sufficient number in each class without making an excessive number of measurements in total, one must restrict the number of classes.

### Probabilities of classes

The values will occur in random sequence, but hopefully when we count them up by class at the end there will be most in the classes 990 to 999 and 1,000 to 1,009, with decreasing numbers in the outer classes and only the odd one or two below 800 or above 1,199. (Note that the classes run from  $.10$  to  $.09$  so that they are mutually exclusive and there is no doubt about placing the  $.10$  value in its proper class if measurements are taken to a higher accuracy. To make the distribution exactly symmetrical about 1,000 one would have to have a central group of 995.00 to 1,004.99 but this would not arise naturally from a Wheatstone bridge with decade adjustments). If the number in each class is divided by the total number, this gives the fraction in a particular class or the probability of that class. A histogram displaying the probabilities of the classes corresponding to successive values of the variable therefore represents a probability

distribution; and if the variable is continuous it is possible by reducing the range of a class—narrowing the columns in the histogram—to approach in the limit a continuous probability distribution curve.

The obvious means of identifying the position of the distribution along the variable axis (resistance) is to take the value of the class which occurs most frequently, and this value is known as the *mode*. This is easy, since no further data-processing is required after counting the number in each class; but it is inefficient since it discards all data falling outside the one class having the highest frequency. In practice one may arrive at a situation like that shown in Fig. 3(a). With modest numbers the class frequencies do not fall exactly on a smooth curve, and one would like to interpolate the curve shown dotted, but the mode automatically selects the one largest peak. Even if the curve is smooth it may be skew (asymmetric) as shown in Fig. 3(b), and the mode is then towards one side of the distribution.

The simplest measure of position using all the data is the mean, and for symmetrical curves the mean and mode coincide. But for skew curves they signify different things: the mode is the position of the peak but the mean indicates the position of the centre of gravity. A third measure of position is the *median*. This is the value of the variable such that equal numbers of objects have values greater and less than the median. The median is particularly useful when the members of the population are considered in ranking order: e.g. in a class list the student in the middle has the median mark, but this need not be equal to the average mark.

### Mean values

If we have a collection of objects having various values of  $x$ , we find the mean value of  $x$  for this collection by multiplying each value of  $x$  by the number of objects having that value, adding together all such products, and dividing by the total number of objects. But in a probability distribution function the individual numbers have already been divided by the total number, so as to give the fraction of the population having any specified value of  $x$ . Therefore the mean value of  $x$  is  $\bar{x} = \sum xP(x)$  for discontinuous distributions like the binomial or Poisson, or  $\int xP(x)dx$  for continuous distributions like the Gaussian. If  $P(x)$  is likened to a set of weights or forces distributed at various distances from the origin, then the mean is also the *first moment about the origin of the system*.

Of the various possible measures of spread or dispersion, the variance (and its square root, the standard deviation) is by far the most generally used. It follows from the definition of the mean that the average distance of all members of the population from the mean is zero; but the mean-square distance is always a positive quantity, which is called the *variance* and denoted by  $\sigma^2$ , and the r.m.s. value  $\sigma$  is called the *standard deviation*. In the Gaussian or normal-law-of-errors distribution, 68.26% of the area under the curve lies between limits  $\pm \sigma$  about the mean; so these limits are rather wider than the so-called "probable error" which refers to points at  $\pm 0.6745\sigma$  such that half the area under the curve is between these points.

A good deal of labour is involved in computing the variance, and for a rapid estimate of dispersion one might look at the *range* of a sample, i.e. the difference between the largest and the smallest value in the sample. For example, statistical quality control (usually called simply "Quality Control") is a technique of using samples

drawn from production which is either too large in quantity for 100% inspection or such that testing involves destruction (e.g. testing the speed of a photographic emulsion). One deduces the probable characteristics of the bulk production from measurements on small samples, and it is obviously desirable to have the answer quickly so that faulty production can be stopped or corrected. Is it possible to take a handful out of a bin of nominally similar resistors, and use the difference between the highest and lowest resistances found in the handful as a measure of the variability of the whole batch? Under certain conditions it is, but this method involves a dilemma. The general rule is that large numbers or large samples are necessary to secure statistical reliability, yet the larger the sample taken from a given population the greater the range is likely to be. Considering a Gaussian distribution, the most probable values are near the mean, and these are the ones we shall usually get in a small sample; but in a very large sample we may get the odd one differing from the mean by more than  $3\sigma$ , since this has a probability of about 1 in 500.

The successful method is therefore to take a small sample (less than 20 individuals in each), determine the range  $R$  in this sample, and then improve the statistical reliability by taking a number of such samples, finding the range in each, and evaluating  $R$ , the mean of  $R$  over all the samples. Details will be found in text books on quality control, but one of the best presentations is to be found in B.S.600: "The Application of Statistical Methods to Industrial Standardization and Quality Control," by E. S. Pearson, published by the British Standards Institution. The standard deviation may be derived from the mean range by the formula

$$\sigma = k_n R$$

where  $k_n$  is a multiplier depending on the number of units in a sample. For  $n = 2, 5$  and  $10$ , the values of  $k_n$  are 0.8862, 0.4299 and 0.3249.

Returning to the more theoretical aspect, the variance is the second moment about the mean. Moments about the mean are always denoted by  $\mu_2$ , while moments about another point, such as the origin, may be denoted by  $\mu'_r$  or by an entirely different symbol such as  $v_r$ , so the first and second moments may be tabulated as follows:

- $\mu_1 = 0$  (i)
- $\mu'_1 = \text{mean}$  (ii)
- $\mu_2 = \text{variance} = \sigma^2$  (iii)
- $\mu'_2 = \mu_2 + (\mu'_1)^2$  (iv)

The last relation is identical with the rule of parallel

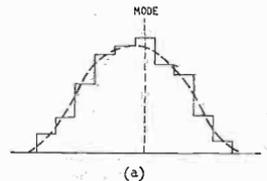


Fig. 3(a). Mode taken from a histogram. (b) The mean and mode in a skew distribution.

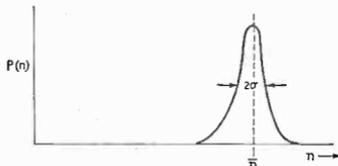
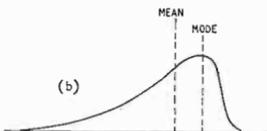


Fig. 4. Mean and standard deviation of rate of transit of electrons through a thermionic valve correspond to d.c. and r.m.s. a.c. components of current.

axes in mechanics; and the variance could be found without evaluating the distance of each point from the mean by transposing (iv) to read

$$\mu_2 = \mu_2' - (\mu_1')^2$$

Usually  $\mu_1'$  is not then taken relative to the true origin, but relative to a convenient point which will simplify calculation, e.g. the whole number nearest to the mean.  $\mu_1'$  is then the distance of the mean from this arbitrary reference point.

### Specifying curve shape

The remaining consideration is the shape of the curve, and this can be partly defined by specifying the skewness and the kurtosis. Skewness is obvious—the degree of asymmetry between the two sides of the curve—and kurtosis indicates whether the distribution function is sharply peaked (like the resonance curve of a single tuned circuit) or flat-topped (like the resonance curve of a critically coupled pair); and both these characteristics can be quantitatively specified in terms of the various moments of the distribution. All the odd moments about the mean would vanish for a symmetrical distribution, so conversely the third moment should give a measure of skewness; and to normalize the measure relative to the spread the coefficient of skewness is defined as  $\gamma_1 = \mu_3/\sigma^3$  (There is also Pearson's measure of skewness (mean-mode)/ $\sigma$ .) Similarly the kurtosis is  $\beta_2 = \mu_4/\sigma^4$ . Since the Gaussian distribution is for many purposes a standard, and has a kurtosis of exactly 3, the behaviour of other distributions is sometimes described by the "excess kurtosis" which is  $\gamma_2 = \mu_4/\sigma^4 - 3$ .

Two distributions which have equal values of mean, standard deviation, skewness and kurtosis must be pretty similar, but they need not be identical. However, specification of the mean and all the moments  $\mu_2, \mu_3, \mu_4, \mu_5, \dots$  up to the highest which has a significant value will exactly define the distribution. An important property of variances is that if the random variations in the quantities  $x$  and  $y$  are uncorrelated, the variance of their sum is the sum of the individual variances: if  $z = x + y$ , then  $\sigma_z^2 = \sigma_x^2 + \sigma_y^2$ .

Now let us apply some of this to the noise component of a simple thermionic current: consisting of  $n$  electrons per second. The mean current is  $\bar{n}e$  where  $e$  is the charge on each electron. Hence if we draw the Poisson distribution of the rate of electron flow as in Fig. 4, the mean value  $\bar{n}$  gives a measure of the mean current which would be indicated, for example, by a moving coil meter. The spread of the curve indicates that the instantaneous current will be sometimes greater and sometimes less

<sup>†</sup>The current is treated as temperature-limited to avoid the complications of space-charge smoothing, and electron transit-time is ignored.

than the mean; and it indicates *how often* a particular value of current will be found but not *when*.

We know from experience, and could deduce from the random nature of the phenomenon, that the various values occur in random sequence and so produce the familiar spiky noise waveform shown in Fig. 5(a). If the waveform is produced on a cathode-ray tube and a narrow slit is placed in front of it, the amount of light passing through the slit will be proportional to the frequency with which the waveform departs so far from the mean, and if the slit is moved across the trace this frequency should vary in accordance with the  $P(n)$  shown in Fig. 4. This can be verified by placing a photocell behind the slit as shown in Fig. 5(b) and plotting the photocell current against slit position. But in centering the trace on the screen, i.e. placing the mean on the zero mark of our scale, we have in electrical terms suppressed the d.c. component and the noise deflection represents the a.c. component. The latter is to be measured by its r.m.s. value, which is none other than the standard deviation of the statistical distribution.

If two thermionic currents are added, the variances will be added, or in electrical terms the mean square noise currents will add. Since the constituent currents are no longer distinguishable after they have been added, any current could be divided into hypothetical components; and it follows that the mean-square noise current is linearly proportional to the mean current or d.c. component.

### Rule-of-thumb for variance

The Poisson distribution has the singular property that its variance is always equal to its mean. This is the origin of a rule-of-thumb that in a statistical phenomenon involving a large number, the variation in the number is likely to be of the order of the square-root of the average number—a rule which is exact if the Poisson distribution applies. If  $\bar{n}$  is the mean rate of arrival of electrons, the mean current is  $\bar{n}e$  where  $e$  is the charge of an electron. Let  $\Delta n$  be a fluctuation in  $n$  so that  $e\Delta n$  is a fluctuation in current. Then the mean-square noise current is  $I^2 = e^2(\Delta n)^2$ . But  $(\Delta n)^2$  is the variance of  $n$

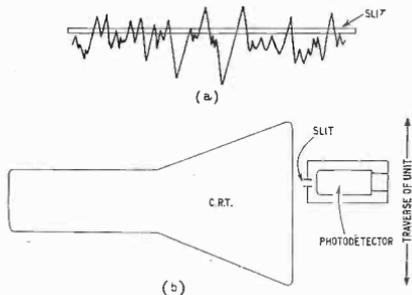


Fig. 5(a). Noise waveform, with slit for detecting the occurrence of a particular level in the distribution. (b) Arrangement of cathode-ray tube, slit and photodetector. Light passing through the slit falls on a photomultiplier, and the whole measuring unit can be traversed across the tube face as indicated by the double-headed arrow.

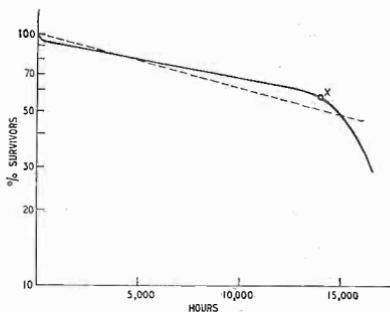


Fig. 6. Logarithm of percentage survivors of thermionic valves plotted against time. Point X can be regarded as the end of useful valve life. The broken-line curve represents a uniform random failure rate.

and from the property of the Poisson distribution must be equal to  $\bar{n}$ .

$$\therefore I^2 = \bar{n}e^2 = \bar{i}e$$

The additional mathematical manipulation needed to obtain the answer in the form of a spectrum can be found in text-books on noise and the result is

$$I^2 df = 2i e df$$

where  $I^2 df$  is the mean-square noise current as measured in a narrow bandwidth  $df$ .

If Poisson had been alive today he would no doubt have worked on the statistics of fatal accidents on the roads rather than those of equine accidents to cavalrymen. The other modern application is to "reliability"; and in terms of reliability of passenger transport vehicles and their associated traffic control systems, reliability of electronic systems will have some relationship to accident probabilities if human error can be substantially eliminated. There is a long range of time—some thousands of hours for thermionic valves and tens of thousands of hours or more for solid-state devices—over which electronic apparatus does not seem to wear out; it just has a small risk of "death by misadventure" which is the same throughout this long range of time. But a small but uniform probability of an event in any time interval  $dt$  is the basis of the Poisson distribution, so these random failures follow a Poisson distribution. If the failure risk is constant, the number of failures is proportional to the number of items exposed to the risk. Hence the rate of occurrence of failures at any time in a large group is proportional to the number surviving up to that point, and the decay in numbers is therefore exponential:

$$N = N_0 e^{-at}$$

The mean life of a single item is  $1/a$  and in a system containing  $N$  items the mean time before one of them fails is  $1/Na$ .

### Mean time between failures

In a system which is repaired when a failure occurs, so that  $N$  is constant, the mean time to the next failure will be the same, so  $1/Na$  is also the mean time between failures (m.t.b.f.). Unfortunately the mean in m.t.b.f. indicates the mean over an ensemble, either of many systems or of the same system on many occasions. Therefore,

when dealing with any single system, e.g., the instrument-landing equipment on a particular aeroplane, one will probably want the m.t.b.f. to be much greater than the operating life: this is because a single sample time before failure may be either greater or less than the m.t.b.f.

The constant failure risk of the Poisson law never applies exactly and departures from it indicate some systematic fault which should be capable of elimination. For example, instead of the dotted straight line in Fig. 6 which represents a uniform random failure rate, thermionic valves often show a sharp initial fall, a long constant slope, and then an increasing slope at the end. The early failures of valves are usually the result of latent mechanical defects such as cracks due to strain glass envelopes or imperfect welds; and the increasing failure rate after a long time represents wearing out, e.g. cathode exhaustion by evaporation or barium or by poisoning. It is logical to regard the point X as the end of useful life, and in the Poisson regime preceding this point there is no advantage in replacing a valve: a new valve will be just as likely to fail as the old one, or in fact more likely unless it has been aged through the early-failure period before being put into use. Any attempt at preventive maintenance must therefore depend on detecting some symptom of wear-out, such as decline in maximum emission of a thermionic valve or increase in leakage current  $I_{cp}$  of a transistor. Components in general and solid-state devices

usually do not show such a clear-cut three-part characteristic, but the plot of logarithm of percentage survivors against time will show a slight curvature indicating a failure rate which either increases or decreases with time. An analytical expression which is often applicable is the Weibull formula, which may be put in the form

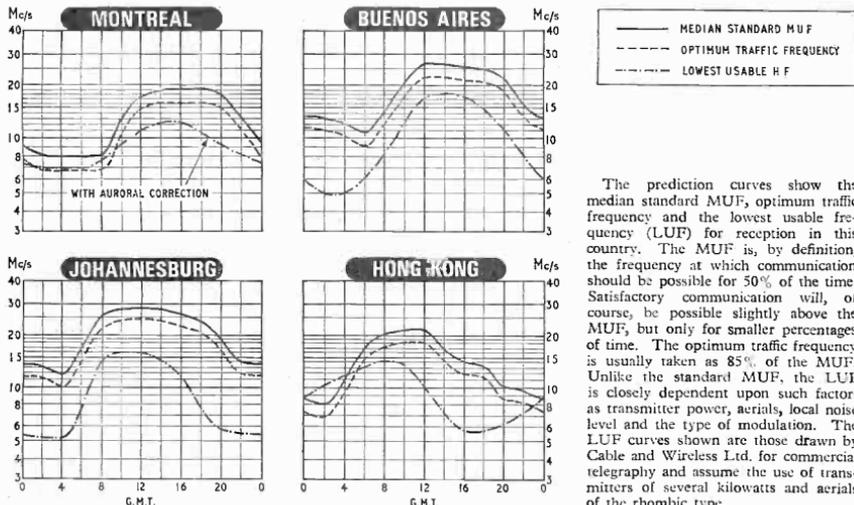
$$N = N_0 \exp(-at)^w$$

where the exponent  $w$  is greater or less than unity for failures rates increasing or decreasing with time.

However, in most electronic systems (such as computers) the failures will be repaired; and therefore the m.t.b.f. is more important than the survival rate. There is some evidence that in computer installations there may be a clustering of faults which will show up as a different kind of departure from the Poisson distribution. Two possible causes of this clustering are: (a) that an intermittent fault may not be cleared by the first remedial action, and so will reappear and be reported as another fault repeatedly until the correct remedy has been found; or (b) that the maintenance activity has disturbed other components and so provoked additional faults.

So it was perhaps a lucky coincidence that life tests on thermionic valves provided a very good illustration of a Poisson distribution of failures; the more reliable components used now have failure characteristics which are both more complex and more difficult to determine because the times involved are so long.

## H. F. PREDICTIONS — MARCH



The prediction curves show the median standard MUF, optimum traffic frequency and the lowest usable frequency (LUF) for reception in this country. The MUF is, by definition, the frequency at which communication should be possible for 50% of the time. Satisfactory communication will, of course, be possible slightly above the MUF, but only for smaller percentages of time. The optimum traffic frequency is usually taken as 85% of the MUF. Unlike the standard MUF, the LUF is closely dependent upon such factors as transmitter power, aerials, local noise level and the type of modulation. The LUF curves shown are those drawn by Cable and Wireless Ltd. for commercial telegraphy and assume the use of transmitters of several kilowatts and aerials of the rhombic type.

# LETTERS TO THE EDITOR

The Editor does not necessarily endorse opinions expressed by his correspondents

## "British Made"

YOUR Editorial (October, 1965) and the subsequent rash of letters would have us believe that there are no hi-fi television sets on the market; this may be the case with sets of British manufacture. Your edition for December proves the absence of advanced design car radios; not a single set being capable of receiving v.h.f. How many audio appliances are there available from British sources equipped with reverberation, I wonder.

All these refinements are available through various foreign agencies, at reasonable prices. For instance, my 19 in television set (a medium-priced Japanese model) is equipped with a 10 in bass speaker and a 3 in tweeter crossover network with tone controls.

When will the British manufacturer wake up to the fact that we are being left behind and that what might have suited "Gran" just will not gell with the modern minded?

Singapore.

E. H. DAVIES

## Integrated Circuits Discussion

I FEAR that in publishing in the January issue such an interesting, but rather restricted and misleading discussion on integrated circuits, you may well stir up a hornet's nest. Perhaps this was your intention!

Integrated electronics as a new art is not merely the use of standard, mass-produced, "not quite right for our application," circuits put together to make systems.

It is an activity in which, at one extreme, a single technology can be used to produce similar components in connected groups, and at the other, where a variety of technologies and materials are unified to make multiple functions.

The unification has barely begun. To many working in the field, the "writing on the wall" is plain; one may list the basic requirements of electronic circuitry and realize that resistive paths, conducting paths, dielectrics, magnetics, cryogenics, and semi-conducting junctions are ultimately more likely to achieve a successful "housing development" on passive substrates rather than semiconductor.

Further, a simple truth languishes little-headed in Mr. Lawton's statement:—"In present day practice, 90% of all circuitry used in the electronics industry is analogue."

For this 90%, evaporated and screen-printed metal and insulating "integrated circuit" films on glass or ceramic have already assumed great importance. The 1965 sales value of film circuits in the U.S.A. was double that of Mr. Padwick's little pellets! (*sic*).

Mr. Flack and the entertainment and professional parts of the industry will soon be able to buy a "brick" of ten stable, reliable integrated film resistors/capacitors for a fraction more than they now pay for one component.

Certainly semiconductor integrated circuits will achieve a miniscule inroad into the analogue field; perhaps more where miniaturization is important. But how does the digital field look today? During a very recent visit to the U.S.A., I was told that the largest computer manu-

facturer in the world was ordering more than 100 million film circuits in 1966/7, and that other large manufacturers in the field are following suit (I saw first hand evidence of the latter).

For an expensive base material like silicon the process currently used by most manufacturers seems very wasteful. Nearly 50% of the ingot (it costs about 8s per gram) is lost in slicing, lapping and etching operations. Of the parts actually used to make circuits, only the top 20 microns of a 100 micron thick chip are required; the rest is both thermal and electrical embarrassment. To cap this, average overall yields run at about 15%; though many will feel this figure optimistic except for simple circuits produced in large quantity. The idea is good but "state of the art" execution is poor.

Only the most primitive natives still fashion canoes by chiselling out logs!

Engineers accept the logic that it can be more economic to put several components made by a unified technology into one package. Yet if an "active" component technique is bent to produce inferior and/or expensive "passive" components—as often appears to be the case—the logic no longer applies.

For a variety of reasons the passive components used either in the silicon, or over the passivating oxide, have tolerance and stability problems. Some of these arise from sheer small size and can be readily eliminated only by increasing area, and hence price.

Resistors and capacitors in available monolithic semiconductor integrated circuits tend to exhibit poor electrical isolation, poor linearity, comparative lack of stability, lack of space for power dissipation, lack of close tolerance ability and high temperature coefficients and be high priced.

On the reliability issue it appears that the accepted improvement for digital semiconductor integrated circuits does not necessarily apply to the analogue ones. Analogue circuits are far more sensitive to parametric drift.

It should not be inferred from this letter that I am of the opinion that semiconductor integrated circuits as we now know them are poor devices. Far from it; the message is simply that there is a strong probability that they will be priced out of large areas of the market by improved integration techniques among their humbler brethren—the passive components.

The techniques most likely to succeed in the long run are those most suitable for component and circuit definition by computer control. In this respect one may forecast that this year, Company A will be able to feed punched tape into its Telex machine and directly control a slave pattern generator in Company B, hundreds of miles away. This will make a film integrated circuit within a few seconds—with resistors and capacitors accurate to  $\pm 0.5\%$  or better.

I hazard a guess that by 1970 in the 90% application, we shall mainly have each passive and active component technology producing integrated groups of its own particular kind; and optimized for lowest price and best performance.

Finally, and with the greatest respect, W.W. will be

guilty of neglect if it imagines it has generated, from so learned a panel, an adequate discussion on integrated circuits—merely by dramatizing\* the effect of silicon planar technology on 10 to 15% of electronics. May I suggest that early in 1966 you reassemble your panel. Perhaps it could then be stiffened with expert† from the passive component fields and move on to discuss the more important aspects of integrated electronics, i.e. the 90% and the longer-term implications.

D. BOSWELL  
(Manager, Film Circuit Unit.)

Standard Telephones & Cables Ltd.,  
Paignton.

\* It was not our intention to "dramatize."—Ed.  
† Least our choice of "experts" should again be criticized, we suggest the discussion continues in the correspondence columns.—Ed.

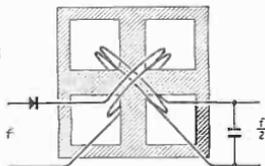
## "Magnetic Frequency Divider"

I READ with interest Mr. F. Butler's article "Magnetic Frequency Divider" in the January issue, and note that he ascribes this device to Rakov and Shumkov, who published a paper in 1965. In fact, to my own knowledge, the divider described was studied at length in this country some twelve years ago by B. W. Glover,<sup>1</sup> with whom I had many discussions regarding this and other forms of magnetic divider used for the production of both even and odd order sub-harmonics.

The circuit shown in Fig. 1 of Mr. Butler's article is exactly that which we classified as the "transductor" type of divider since almost any transductor could be used as a divider by connecting in the manner shown. Two identical transformers with primaries in series aiding and secondaries in series opposition were often used to avoid the overwinding of two separate coils with one output winding which was regarded as the preferred method of construction for transductors.

Prior to Glover's work other forms of magnetic divider for the production of even-order sub-harmonics had been developed, first by MacCreary<sup>2</sup> and later by myself. All of these devices had the same basic requirements of diode input and capacitor output. MacCreary's original device used a lattice window type of magnetic core wound as shown in Fig. 1.

Fig. 1



Two other forms of construction which were successfully developed by myself are shown in Fig. 2.

Fig. 2 (a) shows a magnetic toroid with a hollowed-out channel in the centre, this channel containing a winding orthogonally disposed with reference to the second winding which was applied to the toroid in the normal way. Fig. 2 (b) shows a tape wound toroid in which the magnetic tape itself was used as one of the divider windings.

For those who may wish to experiment with any of these devices I would add that MacCreary Cross Valves can be most readily made by using double yoke laminations such as the Inter Service Pattern No. 524. If

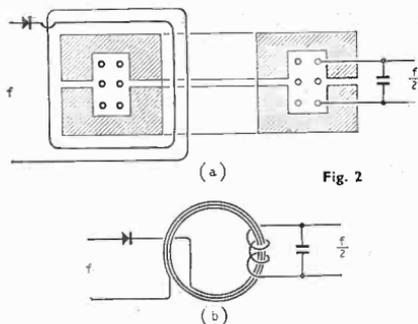


Fig. 2

these laminations are inserted in the directions North, East, South, West cyclically the lattice window pattern will appear.

Experience with these devices has shown that, as Mr. Butler comments, the theory is very abstruse. As far as I can recollect no really satisfactory design mathematics were evolved and design was based on data obtained empirically. I have not yet had the opportunity of reading the Russian paper and it may be that the theory of operation is now fully understood.

F. R. Davey<sup>3</sup> developed a divide-by-three system for the generation of 163 cycles ringing tone for G.P.O. telephone systems as long ago as 1943 using saturated magnetic cores. Transductor types of divider can also be used for production of odd sub-harmonics, particularly the third sub-harmonic, but are much more critical than the simple divide-by-two circuits. For the production of odd sub-harmonics the diode input circuit is not used.

The principal objection to the application of any of the forms of divider mentioned is that the drive power required is considerable, a point which Mr. Butler has emphasized.

J. W. MCPHERSON  
(Technical Manager)

Garnders Transformers Ltd.  
Somerford, Hants.

1. "Transductor Frequency Dividers," B. W. Glover, G.E.C. unpublished report No. SL104, 1954.

2. "The Magnetic Cross Valve and its application to Subfrequency Power Generation," H. J. MacCreary, *Proc. Nat. Electronics Conf.*, Vol. 5, 1949.

3. "A Means Frequency Converter for Ringing Supplies," F. R. Davey, *Post Office Electrical Engineers Journal*, Vol. 36, 1943.

### The author replies:—

Mr. McPherson's letter is one of a number which have been received, all making the point that magnetic frequency dividers of one sort or another have been in use for many years. The correspondence shows that I was less than fair to the pioneer workers in this field and I welcome an opportunity to set the record straight.

Considering only the generic type of circuit shown in my Fig. 1, it is clear that there is nothing new in the binary divider described by Rakov and Shumkov, but their divide-by-four and divide-by-six circuits are new. At the same time, it must be pointed out that these modes are quite difficult to excite, although the simpler divider presents no such problems.

The MacCreary Cross Valve and the two circuits

developed by Mr. McPherson are of particular interest and I would have welcomed a little more information about the performance, frequency range, drive power and suitability for transistor operation.

Another correspondent, Mr. N. G. Dobson, of York, also points out that the circuit of my Fig. 1 is exactly that of a low-frequency divider which has been used by the Post Office since 1959. Presumably this equipment is the same as, or is related to, that described by B. W. Glover in 1954.

Finally, I have received from Mr. J. C. Barton a reprint of his paper "Simple Core Scaling Circuits," published in *Nuclear Instruments and Methods*, Vol. 5, 1959, pp. 332-334. This describes a scale-of-two counter which also employs two saturable cores associated with diodes and capacitors. The two main windings are placed in the collector circuit of a transistor. A third (common) winding is connected between base and emitter, through a capacitor, the combination forming a species of blocking oscillator. Thus the cores themselves determine the duration of the current pulse which switches them. Mr. Barton's paper continues with a description of a scale-of-ten circuit and concludes by discussing a high-speed scale-of-two circuit suitable for driving other identical stages.

All correspondents stress the complexity of the underlying theory and a study of the Soviet paper which I quoted will show how right they were to do so. This need not prevent the interested reader from developing a satisfactory divider by empirical means. An intelligent use of trial and error methods, backed by a qualitative understanding of the basic mode of operation, is enough to ensure success. The aim of my elementary descriptive treatment of the topic was to supply this need.

Cheltenham, Glos.

F. BUTLER

### Torsional Stability and the Unipivot

THERE were two points in Mr. J. Walton's letter in the February issue which interested me greatly, but first I must say that although I accept without question the importance of rumble reduction, I cannot accept that the method advocated is necessarily the best. As far as I can see the only means of reducing rumble without risk of compromising some aspect of pickup performance is to tackle it near its source. One such method is to fix lumps of metal at strategic points to the underside of the motorboard. This has not the elegance of the anti-rumble pickup but it is effective and is a means which the amateur at least can quite easily use.

Unfortunately, I did not see the article on the Hi-light arm and consequently it was most interesting to read that this pickup uses induced torsional motion to reduce vertical inertia.

It was also interesting to learn the effects of (presumably) small torsional movements on the stereo image as I had no exact idea as to what this might be. On hunch, I tried to limit tilt due to the arm "sticking" on its pivot to within  $\pm 1^\circ$  from vertical so as to minimize any possible trouble this might cause. However, since any image displacement in this case would be more or less static, it may well be that greater tilts would be acceptable and the maximum pivot friction limit safely raised.

The reason for my attempting to prevent all torsional motion is that with an arm such as mine suspended close to its centroid on a low-friction pivot and relying on "dry" friction to limit "wobbles," there is hardly any alternative. One could juggle with the arm's reaction movement and/or pivot friction in order to permit

torsional motion with warp accelerations greater than a predetermined value, but since the resultant wobbles would tend to occur at the arm's torsional resonance rather than the warp frequency, there would be no guarantee they would occur in-phase. Apart from this then offering no certain improvement in the ability of the arm to track warps, there is a great risk that the wobbles get out of control and result in the "elbow" of the arm hitting the record.

Incidentally, it has been suggested on occasions that a straight arm be used with the stylus situated on its longitudinal axis. Whilst this would result in a slight overall reduction in arm inertia, a more massive cartridge attachment would likely be needed, so little, if anything, could be gained. (A bent shape offered a more simple means of attaching the cartridge and was chosen mainly for this reason.) However, one could probably get away with this scheme without stabilizing provided (a) somewhat higher pivot frictions were used and (b) the centroid of the arm was dropped to suit.

On the question of low inertia, I go along wholeheartedly with Mr. Walton, but from the point of view of stability to shock rather than rumble reduction and it will be noticed that the inertia of my wobble arm (should it be anti-wobble?) has been reduced to a practical minimum (the stabilizers add only about 1.4 gm). The total inertia with the Deram anti-rumble cartridge fitted would be about 11 gm which, with the vertical stylus compliance of  $2.5 \times 10^{-6}$  cm/dync for this cartridge, should give a resonance around 30 c/s. So although the arm was not specifically designed for this cartridge, a degree of rumble reduction might be possible when used with it.

Finally, if I may, I would like to apologize for a number of errors which were almost certainly due to my atrocious hand-writing. I think the only error likely to cause puzzlement is the counterweight's "rubber back," as printed in Pt. 1, which should read, of course, rubber bush. The lengths of the connecting wires between arm and pivot assembly were unfortunately omitted from Pt. 2 and these should be  $1\frac{1}{2}$  in for each live lead and 2 in for the common E. Lastly, the point S on the alignment scale, referred to in Pt. 2, is at the intersection of the middle guide line with the line from the spindle hole.

Appleby, Westmorland.

J. BICKERSTAFFE

### Colour Television

A CONSIDERABLE amount of talking goes on about the introduction of colour television, but we do not seem to get very much progress. There are those who think we cannot afford it anyway, and they may be right. Certainly the cost of a network of u.h.f. stations for three 625-line programmes capable of providing a colour service is formidable. It has been suggested that upwards of 4,000 transmitters would be needed, many of course would be co-sited.

The problem for I.T.A. is particularly difficult, as they would seem to need to spend a very large sum of money for little or no immediate return.

There is thus no burning desire on the part of the I.T.A. to start on the establishment of a 625 u.h.f. network, nor any reasonably quick profit if they did. In any case it would be a very lengthy process.

During talks with a number of people who earn their living in the television industry, it has seemed to the writer that the objections to a dual-standard colour system are not very valid.

If colour programmes were made available on both

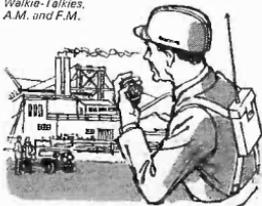
(Continued on page 141)



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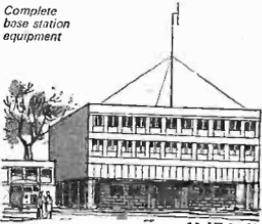
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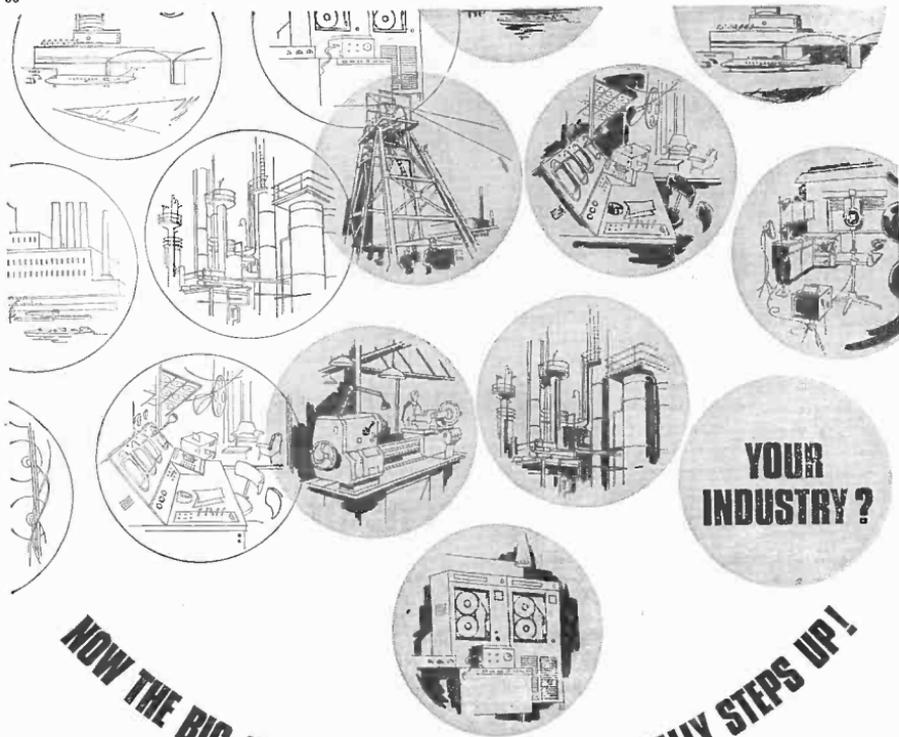
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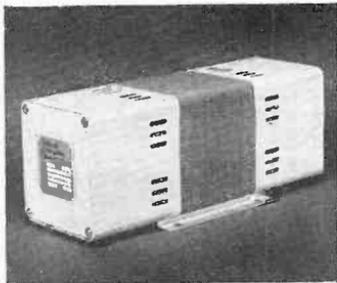
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listener. First, "free-field" means that the speaker must be several wavelengths away from any appreciable reflecting surface. At 30 c/s, three wavelengths is nearly 100 feet and this gives rise to obvious difficulties in measurement. In any case loudspeakers are normally used in close proximity to the ground, this giving improved bass loading and about 6 dB more bass output.

Again a rear wall is normally present along with a ceiling, and the effect of these is to increase bass efficiency to an even greater degree. If side walls are added as well, then the bass efficiency can be lifted even more, as the higher frequencies are not reflected to the same extent as the bass. Hence a "flat" free-field response will sound intolerably bass-heavy at the correct volume level under domestic conditions. It was for this reason that I used a room so as to approximate to domestic conditions.

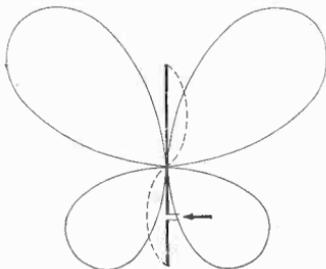
In a lecture at the Northern Polytechnic, London, I had an independent check on the speaker performance, and it produced about 84 dB level at 24 c/s with 20 watts input. This was in a fair sized lecture room and was definitely and rather painfully audible. Reduction of the frequency to 22 c/s removed all audible sound, showing that it was fundamental radiation that was being produced.

Bradford.

ARTHUR R. BAILEY

### "Unconventional Television Aerial"

IN your January 1966 issue Mr. V. Wilson presents an "unconventional" television aerial. One is tempted to say that it is so unconventional it won't work although



experience has shown me that this would be a dangerous statement: all aerials work but some work better than others.

While Mr. Wilson's explanation of the input impedance is broadly correct he makes no mention of the polar diagram of a radiator one wavelength long. I need only refer to Fig. 10.25 (a) of the Services Textbook of Radio, Volume 5 which shows (above) that such an aerial has a null in its pattern at right angles to the aerial axis.

Were it not for the fact that Mr. Wilson is presumably obtaining a reasonable signal I would suggest that he tried inclining the wire at 45° towards the transmitter.

Granger Associates Ltd.,

P. A. C. MORRIS

Walton-on-Thames.

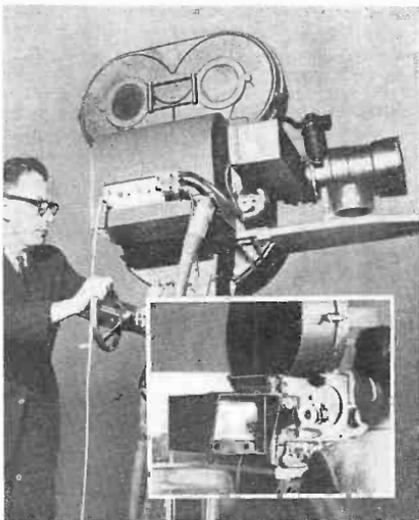
## ELECTRONIC FILMING AID

A COMPACT electronic "conversion pack" that fits on the side of a standard 35 mm film camera and provides the instant monitoring and play-back facilities afforded by television studio cameras has been produced by the Communications Division of the Livingston Group at Watford. Known as "Add-a-Vision" it has been designed around a Plumbicon pick-up tube and provides the cameraman with a 7in television picture instead of that on the normal optical viewfinder.

A zoom lens with a prismatic light-splitting system has been fitted to a standard Mitchell B.N.C. camera. One of the optical outputs forms the image on the film and the other goes to the Plumbicon. The advantage of the Plumbicon is that it requires only a very small amount of light being led from the optical system and therefore does not degrade the film image. The pick-up tube housing can be seen in the larger photograph at right angles to the lens assembly. To the rear of this housing is the unit containing the associated equipment. The viewfinder is mounted on the opposite side of the film camera, as can be seen in the inset. This electronic viewfinder, which is said to facilitate accurate focusing, is hinged to give unimpeded access to the film loading doors.

The video processing unit, which with its associated power supply is rack mounted, provides a video outlet which may be used to feed a number of television display monitors thus enabling production executives to watch action during rehearsals to decide when a scene is ready for shooting. No film need be exposed until the sequence is ready to be taken, and then the monitors relay exactly what the cameraman is shooting.

The picture signals are to full broadcast television standards.



# Mobile Communications

SOME POINTS FROM THE RECENT I.E.E./I.E.R.E CONFERENCE ON SYSTEMS AND EQUIPMENT

**B**ACK in 1945, J. R. Brinkley (Pye) wrote the first paper to be read before the Institution of Electrical Engineers on the subject of mobile radio telephony. At the I.E.E. and I.E.R.E. conference "V.H.F. and U.H.F. Mobile Communication Systems and Equipment," held at the I.E.E. on 12th and 13th January, it was fitting that the same author opened the proceedings by presenting a paper which dealt with the past, present and future development of mobile communication equipment.

In tracing the evolution of the equipment over the last twenty years it is obvious that channel spacing has become a major problem. Twenty years ago the author estimated that less than 1,000 civil equipments (used mainly for police, fire and civil defence purposes) with 100 kc/s channel spacing were in use. Today, the author estimates the figure to be 70,000 which are used for every conceivable purpose, and channel spacing has now been decreased to 25 kc/s and in some cases to 12.5 kc/s.

The ever-increasing demand for more channels has dictated the development of equipment for operation in the u.h.f. bands, and within the auditorium the author demonstrated a 450 Mc/s pocket radiotelephone by contacting Millbank Tower just over one mile away and holding a brief conversation.

## The user

An extensive v.h.f. mobile radio network covering most parts of the country has been established by the Electricity, Gas and Coal Boards and an interesting paper was presented by C. E. Dadson (Joint Radio Committee, nationalised power industries). Electricity is the most extensive user having 377 base stations and 7,369 mobiles. Channel requirement demands have been a problem. In 1958, 22 v.h.f. channels with 25 kc/s spacing were allocated for the exclusive use of these industries. However, the increasing use of mobile equipment has necessitated the recent allocation of four u.h.f. channels in the frequency range 450-470 Mc/s and six additional v.h.f. channels, but the latter are to be used with 12.5 kc/s spacing.

As regards the question of a.m. or f.m., an interesting point was made by the author. When the industries were first considering the establishment of their mobile communication networks, the advantages of a.m. were greater because of the complexities of the f.m. equipment then available. Once a.m. systems were established it was obviously necessary to maintain compatibility as the networks expanded. This could account for the apparent increasing popularity of a.m., but the author stated that there is a tendency for new networks to be developed with f.m. systems.

In considering the use of selective calling with its associated advantage of the increased number of operators in one channel, Mr. Dadson mentioned that the facility had not been widely used because of the apparent reluctance of manufacturers to incorporate the facility as a standard feature. He thought that the need for a cheap form of digital pattern-recognition decoder existed.

In the January 1963 issue of *Wireless World* a detailed description of the pilot scheme of the Netherlands Simoon selective calling system was given. A paper presented by the same author, G. M. Uitermark (Netherlands PTT), described the system which was put into service in September, 1964. After being in operation for a year it had about 2,000 subscribers.

## Quartz crystals

One of the problems arising from reduction of channel spacing is the improved frequency stability required of the local oscillator which in turn depends upon the characteristics of the crystal. In a paper entitled "Recent Developments in Quartz Crystals" by N. C. Rolfe and E. W. Kentley (Cathodeon Crystals) the authors considered that six main factors affect frequency stability—variation of load reactance—level of crystal drive—stability of other components—general environmental conditions—temperature—long-term ageing. Only the last two were considered in detail; the first four, the authors considered, could be eliminated by careful design.

The problems associated with ageing, the authors stated, were successfully mastered quite a few years ago for specially processed high stability crystals. However, the techniques were complicated, selective and costly, and today the demand for bulk production of high stability crystals with rigid specifications is a further problem. However, the problem of ageing has been overcome by the perfection of a glass seal which ensures both a high degree of cleanliness and the exclusion of flux vapours and other volatile matter during the sealing process—two factors which if ignored can accelerate ageing.

The temperature problem has been countered by arrangements which compensate for the change occurring in equivalent circuit parameters during temperature changes. One method described by the authors was that by which temperature dependent d.c. voltage is applied to a voltage dependent reactance, such as a silicon capacitance diode forming part of the oscillator load reactance. By using a thermistor network to obtain a preselectable, temperature dependent voltage, different voltages can be obtained for compensation of individual crystals, and factory set temperature compensated oscillator modules have been developed which have a stability of about  $-1$  p.p.m. from  $-40^{\circ}\text{C}$  to  $+70^{\circ}\text{C}$ .

## Microwave equipment

An unusual mobile communication system was the subject of a paper by E. Goldbohm of the Netherlands Radar Research Establishment. The paper described a microwave tracking system for communication between mobile vehicles. The author explained the arrangement as a line-of-sight relay system (with many of the features of a fixed microwave link) in which the aerials of two identical equipments track with each other. Both aerials radiate narrow beams about  $1.9^{\circ}$  wide and have a forward gain of about 29 dB. The directivity decreases effects of ghosting, multiple path propagation and other signal distortions and also ensures a high degree of

privacy. However, if the system is to be used with a base station controlling several vehicles, then the base station would be equipped with an omnidirectional aerial and the vehicles would operate as individual tracking stations—but with separately modulated carriers which can be filtered out after demodulation of the r.f. signal.

Each equipment uses a reflex klystron for both transmitter and local oscillator functions. Because of the wide bandwidth of the klystron, the system is suitable for television signals and the author stated that good quality television pictures had been received at distances of up to eight miles over land and 10 miles over water.

## INEXPENSIVE TAPE RECORDING AMPLIFIER

By GEORGE WAREHAM

MODIFICATION OF THE GRUNDY/COLLINS/WATSON DESIGNS TO ALLOW USE OF CHEAP N-P-N SILICON PLANAR TRANSISTORS

**I**N the August, 1965, issue (p.403) J. B. Watson presented a design for a recording amplifier which avoids the need for high-voltage transistors as used in the Ferranti design (*W.V.* July-Aug. 1965). Mr. Watson's circuit specified germanium transistors and a negative collector supply. However, it can be readily adapted for use with n-p-n silicon transistors and a positive collector supply. The cheap epoxy-encapsulated planar transistors now coming on the British market can then be used instead of expensive high-voltage types.

Readers may wish to use Mr. Watson's high-impedance transformerless output stage in conjunction with either his own or some other input

circuitry, such as the first two stages of the Ferranti design (July, 1965, issue p.328, Fig. 5). For this reason the last stages of the Watson circuit have been redesigned as a complete single unit, as shown in the accompanying diagram. Some simplification has been achieved in the interstage coupling network. Overall a.c. negative feedback has been increased by increasing the size of the unbypassed emitter resistors of the output transistors from 560Ω to 1500Ω. Linearity is good.

Typical performance data are as follows:—

Input impedance ..	100 kΩ
Output impedance ..	180 kΩ
(driven from 1 kΩ source)	

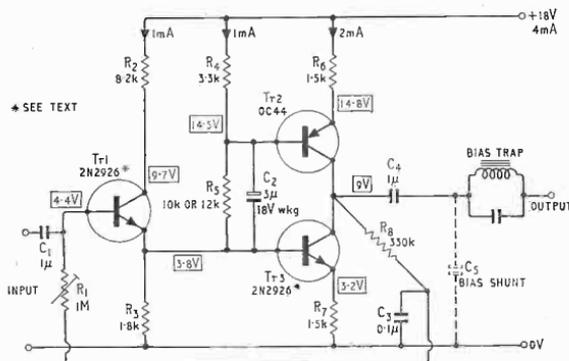
Output impedance (driven from 10 kΩ source) ..	120 kΩ
Maximum undistorted output current ( $Z_L = 0$ ) ..	1 mA r.m.s.
Maximum undistorted output voltage ( $Z_L = \infty$ ) ..	4 V r.m.s.
Input voltage for 125 μA in 18 kΩ load ..	100 mV
Input voltage for 4 V r.m.s. ( $Z_L = \infty$ ) ..	20 mV
Cut off frequencies (-3dB)	6c/s and >30 kc/s

Silicon transistors type 2N2926 have a wide range of current gain (35 to 470), but are divided into five narrow gain groupings, identified by a colour code. To obtain the stated performance, Tr1 should preferably be a "yellow" type ( $h_{fe} = 150$  to 300) but an "orange" type ( $h_{fe} = 90$  to 180) may also be used, the main effect being a reduction in output impedance to about 100 kΩ. Tr3 may be either a "yellow", "orange" or "red" ( $h_{fe} = 55$  to 110) type. (Readers should note that at least one manufacturer omits the colour-code dot on the commonest type, "orange".) This transistor type may also be used in both the Ferranti and Watson low-level circuits. Again, "orange" or "yellow" types are preferable.

The resistor  $R_2$  is inserted to protect Tr1 against excessively high collector voltages. It has virtually no effect on performance, but provides a possible pick-off point for the signal supply to a recording level indicator (500 mV when the amplifier output current is 125 μA).  $C_2$  may be omitted if the signal-source impedance is 1 kΩ or less, since most of the resulting negative feedback voltage is then lost across  $R_3$  and  $R_1$ .

The bias trap must have a very high impedance to be effective, since it forms an inverted-L attenuator with the output impedance of the amplifier, which is itself high.

Transistors type 2N2926 are obtainable from Amatronics Ltd., 396 Selcote Road, Croydon, price 5s each.



The redesigned circuit. All resistors are  $\pm 5\%$  tolerance. Voltages boxed are d.c. voltages measured with a high resistance voltmeter.  $R_1$  is adjusted to obtain 9V at the collectors of Tr2 and Tr3.

Marconi self-tuning H.F. system—  
the first in the world to be station  
planned from input to output.



# breakthrough

## MST 30kW transmitter type H1200

An h.f. linear amplifier transmitter for high-grade telecommunications.  
Frequency range: 4-27.5 Mc/s.  
Output power: 30 kW p.e.p., 20 kW c.w.  
Meets all CCIR Recommendations.

### saves 80% floor space

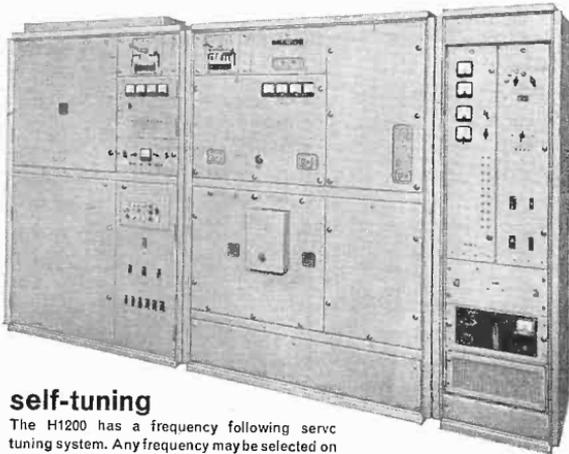
Transmitters can be mounted side by side and back to back or against a wall. Floor-ducts are eliminated and all power supply components are built-in. These features lead to smaller, simpler, cheaper buildings or more services in existing buildings.

### rugged reliability

R.F. circuits have been simplified and the number of mechanical parts reduced to a minimum. Highest engineering standards are applied to the design of these parts: stainless steel shafts in ball-bearings in heavy, rigid, machined castings; stainless steel spur gears meshing with silicon bronze; heavy r.f. coil contacts with high contact pressure. Specified performance is maintained with ample margins.

### simplicity

MST reliability allows continuous unattended operation with extended or remote control, saving maintenance and operating staff. Any fault in the servo control circuits can quickly be located with simple test routines. Transistors and printed wiring give these circuits maximum reliability.



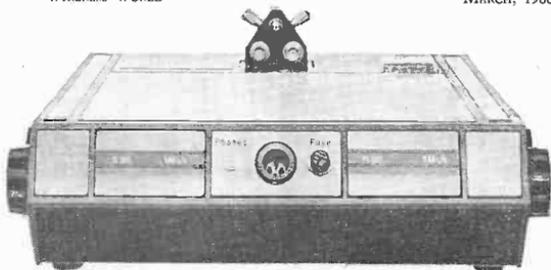
### self-tuning

The H1200 has a frequency following servo tuning system. Any frequency may be selected on the synthesizer decade dials in the associated MST drive equipment; the unattended transmitter automatically tunes itself in an average time of twenty seconds. Final stage tuning and loading servos continuously ensure automatic compensation for changes in aerial feeder impedance caused by weather conditions. Self-tuning gives *one-man* control of an entire transmitting station.

## Marconi telecommunications systems

The Marconi Company Limited, Radio Communications Division, Chelmsford, Essex, England  
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LTD/H51



**This new capacitance-conductance bridge is more than good-looking**

### 0.1% at 1 Mc/s

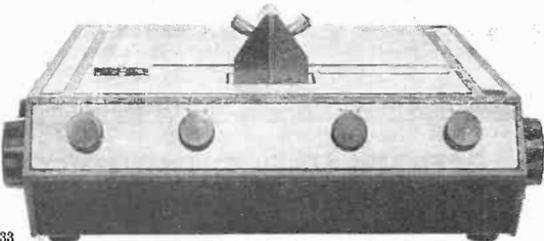
—that's the accuracy this new Wayne Kerr RF Bridge B201 gives you, *plus* the ability to measure conductance and capacitance simultaneously over the 100kc/s to 5Mc/s range. It is completely self-contained, has a variety of plug-in source and detector units, adjustable level control, gain control, visual and aural nulls, clear four-figure readout, and extremely wide measurement ranges: 10aF (10<sup>-5</sup>pF) to 0.1μF and 0.1nMho to 1Mho. For details of *all* the many features with which this remarkable new bridge speeds and simplifies component testing, however, you need the B201 leaflet. Please ask for your copy.



**.. it has the best range-plus-accuracy combination in the business**

## **WAYNE KERR**

The Wayne Kerr Laboratories Limited  
Sycamore Grove, New Malden, Surrey  
Telephone: MALden 2202  
Telegrams: Waynkerr New Malden. Telex: 262333



WW-121 FOR FURTHER DETAILS.

# NEW PRODUCTS

equipment systems components

## SURVIVAL TRANSCIVER

A SOLID-STATE transceiver called Safcom is being produced by K. W. Electronics Ltd., for fitting to fishing vessels' liferafts. Last year the Merchant Shipping Rules (17-8) were amended making it compulsory for fishing vessels of more than 60 ft in length to carry emergency rescue beacon equipment. This transceiver conforms to the regulations and has received British P.O. type-approval.

The transceiver contains a crystal-controlled transmitter and receiver operating on the international marine distress frequency of 2182 kc/s. The output of the

output of 1.3 and 2.2 kc/s. Eight silicon planar transistors are used in the receiver section which employs a superhet circuit with a tuned r.f. stage and Class B output for battery economy. All the receiver circuits—and the tone generator and tone switching circuits—are voltage stabilized.

The transceiver is powered by two mercury batteries that give a nominal voltage of 16 V. Battery life, with a 1 to 9 transmit-receive ratio, is in excess of 100 hr.

The Safcom is contained in a cylindrical watertight container measuring 24 in long by 4 in in diameter. An auxiliary tube containing a telescopic aerial (74 in extended) and "earthing" lead is bonded to the side of the main tube. The end cap of the main tube houses the microphone, loudspeaker and transmit switch. (Even with the end cap removed from the body of the main tube, the transceiver is watertight.) A separate switch is provided for radiating the two-tone alarm signal.

The Safcom will float, even when dropped into the water from a height of 20 ft. It weighs 9½ lb.

Although exclusively manufactured by K.W. Electronics Ltd., of Vanguard Works, 1 Heath Street, Dartford, Kent, this transceiver is being distributed by several companies including Marconi International Marine, who are marketing it under the name "Lifesaver," and Kelvin Hughes.

WW 309 for further details

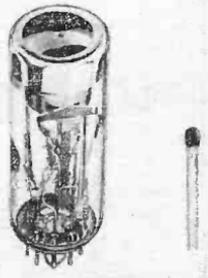
## ANTI-MAGNETIC TWEEZERS

STAINLESS heat-resistant alloy is used for the tips of a pair of tweezers recently introduced by Henri Picard & Frere Ltd., of 34 Furnival Street, London, E.C.4. These tweezers are anti-magnetic and will withstand temperatures in excess of 500° C (normal hardened steel becomes noticeably soft above 300° C).

WW 310 for further details

## PHOTOMULTIPLIERS

TWO new devices have been added to the Mullard range of photomultiplier tubes, a four-stage device designated XP1114 and the six-stage XP1113 tube. Both devices measure 68 mm by 19 mm in diameter and have cathode sensitivities of 40  $\mu$ A/lumen. The photocathodes are deposited directly onto the



inside of the end face of the tube and focused by a dynode electrode system giving an overall sensitivity of 4 mA/lumen for the four-stage tube (illustrated) and 400 mA/lumen for the other.

The cathode material in both tubes is antimony-caesium and has a response peaking in the blue region. At a later date it is hoped to offer tubes that will operate in the infra-red and ultra-violet regions.

Both tubes are available in development quantities. The address of Mullard Ltd. is Mullard House, Torrington Place, London, W.C.1.

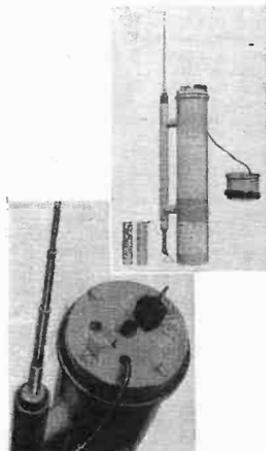
WW 311 for further details

## TRANSISTORS

QUANTITY price reductions of up to 50% in a broad range of silicon planar and planar epitaxial transistors are announced by Transistron Electronics Ltd., of Gardner Road, Maidenhead, Berks. As an example the 2N2784, which is a hermetically sealed device with an  $f_T$  of 1 Gc/s, is now under 10s at 1,000 up. For small orders the price has not been changed; the 2N2784 costing 18s 11d.

Units with relaxed specifications such as the ISP6120, a general fast switching device with an  $f_T$  of 1 Gc/s, are also cheaper in quantity. At the 1,000 level, the ISP6120 costs 8s 6d; one-off they are 15s 4d.

WW 312 for further details



transmitter is in excess of 1 W and the receiver sensitivity is 1  $\mu$ V for standard output. Audio output is quoted as 4 V pk-pk across the transducer.

Thirteen silicon planar n-p-n transistors are used in the transmitter section. Eight of these are employed in a tone generator, which provides an alternating

## Loudspeaker Units

TWO 12 watt loudspeaker units have been introduced by Jordan-Watts Ltd., of Benlow Works, Silverdale Road, Hayes, Middx. Both enclosures are fitted with their standard drive unit and are suitable for use with amplifiers having output impedances from 7.5 to 16 $\Omega$ .

The Juno, as one is called, is an

0.6 cu ft bass reflex unit and has a frequency response of about 40 to 20,000 c/s ( $\pm 6$  dB). Although based on their current enclosures, the Juno has been stiffened and the port and tunnel modified to improve the bass frequency response. Distortion with a low input is approximately 5% at 50 c/s and 1 $\frac{1}{2}$ % at 100 c/s. The external dimensions of the unit are 24 $\frac{1}{2}$  x 12 x 5 $\frac{1}{2}$  in, and the price is £24 10s.

The other unit, which measures 8 x 16 $\frac{1}{2}$  x 3 $\frac{1}{2}$  in, is called the Jumbo. It is a totally enclosed unit and has a frequency response of about 70 to 20,000 c/s ( $\pm 6$  dB). The price is £17 12s 6d.

Both units are finished in light teak. A Vynair covering forms the fascia panel.

WW 313 for further details



## Milliwatt Test Set

REDESIGNED versions of Standard Telephones and Cables 74166-A milliwatt test set—an instrument for measuring signal levels on unbalanced 75 $\Omega$  circuits at frequencies up to 30 Mc/s—have recently been introduced. The new instruments, the 74166-H and 74166-J, are about half the size of the earlier instrument, and incorporate push-button switches.

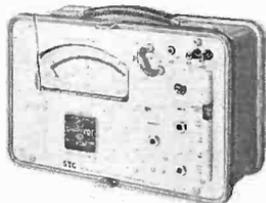
The two models (H and J) are identical apart from their input connectors, the H being fitted with Post Office No. 1 co-axial plugs, and the J having

B.N.C. connectors (Amphenol 31-221). They will make accurate terminated level measurements of +1 dB to -1 dB referred to 1 mV on 75 $\Omega$  unbalanced circuits at frequencies up to 30 Mc/s, and they will also measure heater voltages of 5.6 to 7.0 V.

The instruments cannot be used for measuring "through levels" as a wired-in thermocouple is incorporated with the heater impedance shunted down to 75 $\Omega$ . A miniature Weston standard cell is included to maintain a high measuring accuracy; the measuring circuits being standardized by a series of simple switching and adjusting operations. A further feature is that the standardizing circuit can also be used to send a d.c. power level of 1 mW into external 75 $\Omega$  circuits for calibrating other apparatus. Both instruments are powered by three internal 1.5 V dry cells. The overall dimensions are 12 $\frac{1}{2}$  x 8 x 7 $\frac{1}{4}$  in, weight is 1 lb.

The address of S.T.C.'s Testing and Apparatus Division is Corporation Road, Newport, Monmouthshire.

WW 314 for further details



## Transistor for Driving Number-tubes

A BREAKDOWN voltage of 120 V and a d.c. gain of 35 (at an operating current of 3 mA) are features of a new transistor from SGS-Fairchild. Known as the C 407, it is a silicon planar device designed for use as a high-voltage driver for neon indicator tubes, such as the Nixie.

Being a silicon planar device, the leakage current is less than 200 nA and thus will eliminate the soft glow effect caused by a numeral other than the one desired drawing current. The C 407 is encapsulated in epoxy resin and has a lead pin circle identical to that of the popular TO-5 can.

The one-off cost of the C 407 is 6s 9d and at 100 up the cost is 4s. The company's address is 23 Stonefield Way, Ruislip, Middx.

WW 315 for further details

## WIDE RANGE VOLTMETER

FIFTEEN a.c. ranges and three d.c. ranges are provided on the new Type M1 voltmeter now available from Linstead Electronics Ltd., 35c Newington Green, London, N.16. The input impedance is 10 M $\Omega$  on all but the lowest a.c. ranges where it is between 6 and 10 M $\Omega$ . The mV ranges provided are as follows: 1-10, 2-20, 5-50, 10-100, 20-200 and 50-500 mV; and the voltage ranges 0.1-1, 0.2-2, 0.5-5, 1-10, 2-20, 5-50, 10-100, 20-200 and 50-500 V. The frequency range of the M1 is 10 c/s to 100 kc/s.

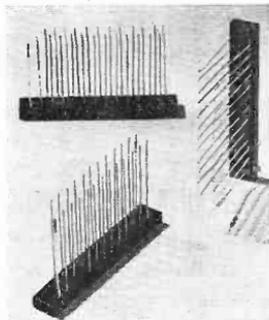
The three d.c. ranges provided are 0 to 4, to 40 and to 400 V. The sensitivity is 20 k $\Omega$ /V.

The transistor instrument contains a four-inch meter and is powered by an internal 9 V battery. An amplifier output—at low impedance—is provided with a voltage gain of approximately 80 on the most sensitive range.

The overall dimensions of the M1 are 6 $\frac{1}{2}$  x 8 $\frac{1}{2}$  x 5 in, the weight is 5 lb and the price is £24.

WW 316 for further details





## Multiple Capacitor Units

FOUR types of multiple capacitor unit for use in the manufacture of delay lines are now being made by Johnson, Matthey & Co. Ltd., of 73-83 Hatton Garden, London, E.C.1. The units contain a number of silver-mica capacitors—with or without interconnection—and are encapsulated in an epoxy resin to give a high humidity resistance and a wide operating temperature range.

Units with various combinations of capacitance value will be made to customers' specifications from the four standard types of unit. The available capacitance ranges are as follows: 50 V, 440 to 1,500 pF; 200 V, 300 to 439 pF; and 350 V, 1 to 299 pF. The temperature range of the units is from  $-55^{\circ}$  to  $+100^{\circ}$  C. Temperature coefficient is  $15 \times 10^{-6}/^{\circ}$  C at 1 kc/s and  $5 \times 10^{-6}/^{\circ}$  C at 1 Mc/s.

WW 317 for further details

## Standard Integrated Circuit Boards

TWO standard printed circuit boards are being manufactured by the Triad Division of Litton Industries to enable manufacturers to quickly assemble integrated circuits. Both boards are double-sided with flat-pack mounting tabs on one side and TO-5 pads on the other. Up to six TO-5 cased components or six flat packs—or a combination of both—may be mounted on each board. The boards are designed for use with either 25-contact or 18-contact double-sided connectors.

Litton products are handled in the United Kingdom by Litton Precision Products, 503 Uxbridge Road, Hayes, Middx.

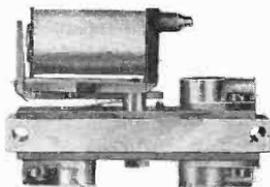
WW 318 for further details

## Aerial Changeover Relay

A NEW co-axial aerial changeover relay, having no plugs or sockets on the body of the relay, is now available from Magnetic Devices Ltd., of Newmarket, Suffolk. Designated Series 951, it is a d.c. operated device and is suitable for switching signals at frequencies of the order of 450 Mc/s. It can be used in applications where low inter-contact capacitance is important.

The relay contains a single changeover contact enclosed in a brass housing and is designed for use with U.R. 43 cables—which are soldered directly to the relay and secured by brass clamps. The soldering operation does not affect the relay contact setting and the brass clamps provide continuity of screening and cable outlets in any three directions. Operate time is 20 ms and release time is 8 ms.

The maximum d.c. working voltage of



the relay is 100 V; maximum coil wattage is 1.5 W and maximum coil resistance is 9.35  $\Omega$ . The contact rating is 1 A or 30 W maximum with a nominal impedance of 50  $\Omega$ . Other specification details include a voltage standing wave ratio of approximately 1.1:1 at 450 Mc/s, and a cross talk figure of 39 dB.

WW 319 for further details

## DIGITAL VOLTMETER

THE range of instruments made by G. & E. Bradley has been extended and now includes a digital voltmeter. Designated Type 160, it covers 0 to 1,000 V d.c. in four ranges and has an accuracy of 0.1%.

A four-digit in-line display is em-



ployed in this solid state instrument, which contains a standard cell for calibration. A filter is also provided that can be switched into the input circuits to suppress superimposed noise or a.c.

The basic version of the 160 does not have an output for driving printers and costs £240. A version with a printer output is available and costs approximately £20 more. The dimensions of the 160 are  $4 \times 11\frac{1}{4} \times 8$  in, and its weight is 8  $\frac{1}{2}$  lb.

The address of G. & E. Bradley Ltd. is Electral House Neasden Lane, London, N.W.10.

WW 320 for further details

## CO-AXIAL CONNECTORS

A SERIES of small B.N.C. two-pin co-axial connectors made by the French company Radiall are now available through Lectrotron Ltd., of Kinbex House, Wellington Street, Slough, Bucks. Designated B.R. 2, this series of connectors is suitable for use with twin screened cables having diameters of 4, 5 or 6 mm.

The maximum current capacity is 3.5 A and the working voltage (at ground level) is 500 V r.m.s. Other electrical characteristics include an insulation resistance at 500 V d.c. of 100 G $\Omega$ , a contact resistance of 1 m $\Omega$  at 1 A, and a between

pin capacity of 1.7 pF at 1 kc/s and 1.3 pF at 1 Mc/s. Between pins and case, the capacity is 4 pF at 1 kc/s and 3.2 pF at 1 Mc/s.

WW 321 for further details



## PARAMETRIC A.F. PRE-AMPLIFIER

A HIGH input impedance, low noise transistor pre-amplifier is announced by Isewirth Electronics, of Frederick St., Waddesdon, Bucks. Noise voltages referred to the input are 10 and 20  $\mu$ V pk-pk with input short and open circuited respectively. With a 100 k $\Omega$



metal film resistor across the input the noise voltage is 25  $\mu$ V pk-pk. The high input impedance of 10 M $\Omega$  and the low noise performance are achieved with a 10-stage differential amplifier, the first stage of which is a parametric amplifier

using a varactor diode and operating with a pump frequency of 10 Mc/s. An output of 1 V pk-pk with a 10 k $\Omega$  load is provided. Output impedance is less than 500  $\Omega$ . A switched gain of either 100 or 1,000 times is provided and common mode rejection is 120 dB.

The amplitude-frequency response is variable, switched high- and low-pass filters being provided—giving 3 dB-down frequencies of 20 kc/s, 10 kc/s, 1 kc/s, 200 c/s and 50 c/s for the low-pass filter, and 2 c/s, 20 c/s and 200 c/s for the high-pass filter.

Power supply units (type P101) are available for the amplifier (designated A101), giving a stabilized supply of 150 mA at 9 V, which is sufficient to operate 10 amplifiers. Operation from an internal 8.4 V mercury battery would provide 40 hours of use. It is arranged that the amplifier will automatically switch to battery operation in the event of mains supply failure. A 19-in rack mounting kit is available including a drilled rack panel.

The ex-works price is £45.

WW 322 for further details

## Conductive-plastic Potentiometers

A NEW series of conductive-plastic potentiometers have been added to the extensive range of precision potentiometers made by the Markite Corporation, of New York. Non-linear laws—which prior to the advent of this track material were considered impossible—are included in the new series known as the Slimline. Also included are units with sine-cosine and rectilinear track laws.

Stainless-steel bearings are used in these multi-gang potentiometers, which under test have performed without failure for up to 200 million operations. Accuracies of up to 0.01% are quoted for the larger units in the series.

These potentiometers are available in

the United Kingdom through Davies Integrated Sales, 252 Kempshott Lane, Basingstoke, Hants.

WW 323 for further details



### INFORMATION SERVICE FOR PROFESSIONAL READERS

To expedite requests for further information on products appearing in the editorial and advertisement pages of *Wireless World* each month, a sheet of reader service cards is included in this issue. The cards will be found between advertisement pages 16 and 19.

We invite professional readers to make use of these cards for all inquiries dealing with specific products. Many editorial items and all advertisements are coded with a number, prefixed by WW, and it is then necessary only to enter the number(s) on the card.

Postage is free in the U.K. but cards must be stamped if posted overseas. This service will enable professional readers to obtain the additional information they require quickly and easily.



## VIBRATION & DISPLACEMENT MEASURING INSTRUMENT

MEASURING complex vibration effects in delicate structures where the measuring device must not load the body being measured, is one of many jobs within the scope of the Model DF/2 detector/filer unit now available from Associated Engineering Ltd., Cawston, Warwick. The instrument has been designed for use with matched pairs or double versions of A.E. displacement transducers and will measure displacement or vibration at frequencies from zero to 10 kc/s at a distance of 0.015 in. Resolution is up to 10  $\mu$ in, depending on the material.

The overall temperature stability, including the transducers, is better than  $\pm 2 \mu$ in/ $^{\circ}$ C when the transducers are temperature cycled. Long-term stability for static displacement measurement over an 8 hr period is better than 100  $\mu$ in for ferrous materials.

WW 324 for further details

## Miniature Connectors

CIRCULAR connectors manufactured by Souriau et Cie. of France, are available in the United Kingdom through Lectrotron Ltd., of Kinbex House, Wellington Street, Slough, Bucks. The range offered, called Miniphi, has six shell sizes ranging from 0.43 to 0.93 in in overall diameter. The number of pins range from 7 to 61.

A nominal current rating of 3 A is quoted for the connectors, which will operate in the temperature range  $-55^{\circ}$  to  $+125^{\circ}$  C. Reinforced diallyl phthalate is used as the insulation material and a light metal alloy for the shell. The insulation resistance is  $10^6$  M $\Omega$ .

WW 325 for further details



# **Vortexion** quality equipment

The 120/200 watt Amplifier can deliver its full power at any frequency in the range of 30 to 20,000 c.p.s. for which the response is accurate within 1 db with less than 0.2% distortion at 1,000 c.p.s. Noise level -90 db. It can be used to drive mechanical devices, i.e., synchronous capstan or projector motors, etc., for which the power is over 140 watts on continuous sine wave. A floating series parallel output is provided for 100-120 v. or 200-250 v., and additional matching transformers for other impedances are available. The input is for 1 mW, 600 ohms.

## 30/50 WATT AMPLIFIER

The Vortexion 30/50 watt Amplifier can deliver 50 watts of speech and music or over 30 watts of continuous sine wave and the main amplifier has a response of 30 to 20,000 c.p.s. within 1 db at 0.1% distortion and outputs for 4, 7.5, 15 ohm and 100 volt line. Models are available with two, three or four mixed inputs which may be low impedance balanced line microphones, P.U. or Guitar inputs. Price £70 with 4 mixed inputs.



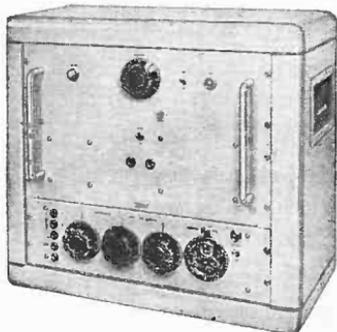
The 12-way electronic mixer has facilities for mixing 12 balanced line microphones. Each of the 12 lines has its own potted mumetal shielded microphone transformer and input valve, each control is hermetically sealed. Muting switches are normally fitted on each channel and the unit is fed from its own mumetal shielded mains transformer and metal rectifier.

Also 3-way mixers and Peak Programme Meters.  
Price £60.

4-way Mixers from £40/8/6.

2 x 5-way stereo mixers with outputs for echo chambers, etc., available.

## 120/200 WATT AMPLIFIER



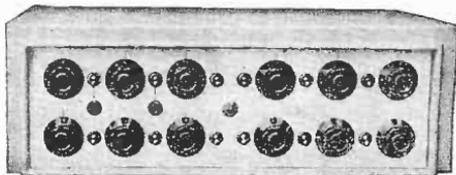
## ELECTRONIC MIXER AMPLIFIER

This high fidelity 10/15 watt Ultra Linear Amplifier has a built-in mixer and Baxandall tone controls. The standard model has 4 inputs, two for balanced 30 ohm microphones, one for pick-up C.C.I.R. compensated and one for tape or radio input. Alternative or additional inputs are available to special order. A feed direct out from the mixer is standard and output impedance of 4-8-16 ohms or 100 volt line are to choice. All inputs and outputs are at the rear and it has been designed for cool continuous operation either on 19 x 7in. rack panel form or in standard ventilated steel case.

Size 18 x 7½ x 9½in. deep.

Price of standard model £49.

## 12-WAY ELECTRONIC MIXER



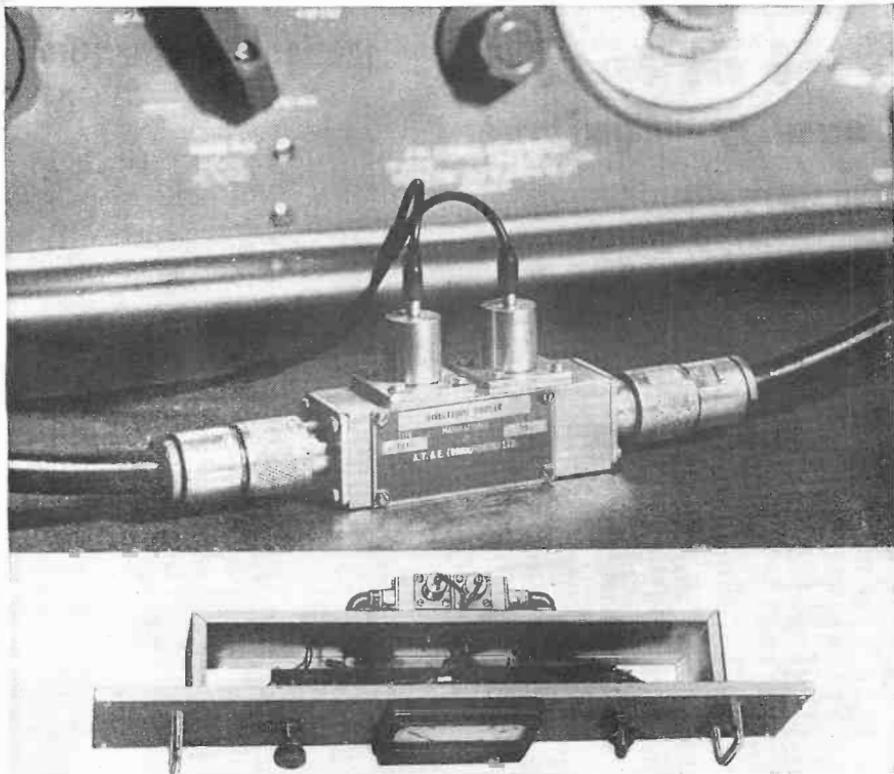
Price of standard model £98.

Full details and prices of the above on request

**VORTEXION LIMITED, 257-263 The Broadway, Wimbledon, London, S.W.19**

Telephone: LI Berty 2814 and 6242-3

Telegrams: "Vortexion London S.W.19"



## now you can monitor VHF-UHF power and VSWR without affecting transmitter output

With a primary line SWR less than 1.05 and negligible insertion loss, this range of coaxial directional couplers Type PRI gives you continuous monitoring of power levels up to 300 watts, without interfering with your transmitter, transmission line or aerial. Available for frequency bands between 50 Mc/s and 500 Mc/s, these couplers weigh only 8 ounces and measure only 5" x 2½" x 1". They have sensitivities of 50 microamps (DC) per watt (RF), nominal impedances of 50 or 75 ohms, and Type N connectors.

Type PRI directional couplers are also supplied incorporated into complete coaxial reflectometers Type M2X, suitable for mounting in 19-inch racks or in portable units. Both forward and reflected power can be measured directly, and accuracy is independent of

line VSWR. Full-scale power readings of 10 watts and 100 watts are standard, as are direct readings of VSWR from 1.0 to above 10.0.

For easy-to-install, non-interfering, high-accuracy VHF and UHF power measurements, the directional couplers and coaxial reflectometers from AT&E provide an ideal inexpensive solution. AT&E will be happy to supply additional details; just write to AT&E (Bridgnorth) Ltd., Bridgnorth, Shropshire, England.

**PLESSEY**  
**Electronics**



PECTA

## Subminiature Pressure Transducers

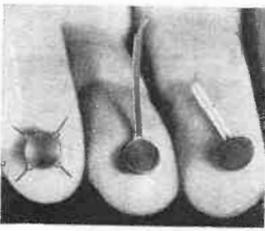
THE range of subminiature pressure transducers made by Scientific Advances Incorporated, of Ohio, are now available in the United Kingdom through Wessex Electronics Ltd., Royal London Buildings, Baldwin Street, Bristol, 1. There are a number of basic models in the range, each covering a variety of pressure ranges. The models differ mainly in the geometry of lead attachment—see illustration. (Model M-5 on the left, M-6 centre and M-7F on the right.)

A four arm, bonded-foil strain gauge is employed, to take maximum advantage of the strains on a flat diaphragm, and is cemented to the inside surface of the diaphragm. The transducer itself will, through its small dimensions, cause little interference in gas or liquid flow systems.

Typical of the physical and operating characteristics of the range are those of the Model M-5. This particular model is available in four pressure ranges—from 0 to 15, to 30, to 100 and to 150 p.s.i.—and its thickness ranges according to pressure range from 0.02 to 0.035 in. The weight of the M-5 is 0.1 gm.

The recommended input voltage for all models is 3V d.c. or a.c. and the working temperature range is  $-40^{\circ}$  to  $+150^{\circ}$ F.

WW 326 for further details



## High-voltage Transistors

A RANGE of high-voltage silicon n-p-n transistors, manufactured in the U.S.A. by Inductro Transistor Corp., are available from Lectrotron Ltd. of Kinbex House, Wellington St., Slough.

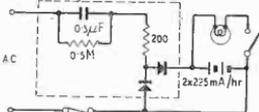
The range includes types with  $V_{CE}$  and  $V_{CB}$  of 100-800 V (at 200  $\mu$ A) with an  $L_{FE}$  of 20-30 at 25mA. Peak collector current is 400mA and dissipation varies between 3W and 15W at 25°C case temperature. Prices vary between 9s and £19 depending on ratings required.

WW 327 for further details

## Miniature Charger Modules

A RANGE of miniature constant-current charger modules for use with nickel-cadmium batteries is now available from Kynmore Engineering Co. Ltd., 19 Buckingham Street, London, W.C.2. The range is based on an earlier module developed for incorporation in rechargeable torches and pocket lamps.

Three- and four-lead modules are available and, having low reverse current figures, may be permanently connected to the batteries they are to recharge. The three-lead modules use a circuit similar to the original module for the torches and pocket lamps (illustrated), while the four-lead modules employ a bridge circuit. As can be seen from the illustrated circuit, a capacitor is



used to drop the voltage before rectification by a pair of gold-bonded semiconductor diodes. Six different sizes are available in the standard range, with



capacities ranging from 2 to 45 mA—assuming a 230 V a.c. supply. On 115 V supplies the current ratings are halved. The maximum load is ten cells.

The smallest in the range measures 0.8 in long by 0.6 in diameter and the largest 1.7 in long by 1.25 in diameter. The price of the modules varies according to current rating. Hundred up prices are from 10s, for a 2 mA unit suitable for driving up to five cells, to 19s 6d for a 45 mA unit, suitable for driving up to ten cells.

WW 328 for further details

## V.H.F. HIGH-POWER TRANSISTORS

A NEW series of high-power v.h.f. silicon n-p-n transistors, from TRW Semiconductors Inc., includes a device which will deliver up to 40W, with a 6dB power gain, at 175 Mc/s. Designated PT5690, it is a silicone encapsulated device with the dice completely isolated. It is mounted on a beryllium oxide stud and has radially-mounted leads making the device suitable for printed circuit board mounting. The transistor geometry makes use of a unique symmetrical method of paralleling devices on a single chip. The complete transistor comprises 24 transistor elements arranged in four clusters of six and each element contains a thin film emitter resistor to balance the input r.f. voltage characteristics of the base-emitter diode. Other specification details include a  $V_{CEO}$  60,  $V_{CBO}$  40 and a  $V_{BEBO}$  3. One-off price is £44.

The other two in the series, available in the United Kingdom through M.C.P. Electronics Ltd., of Station Wharf Works, Alperton, Wembley, Middx., are both 150 Mc/s devices. The PT5692 has a 6dB gain and will provide a 20W output, and the PT5694 a



power gain of 8dB and a 12W output. The respective prices are £22 and £12. WW 329 for further details

## U.H.F. TV Tuner

A TRANSISTOR quarter-wave television tuner for the band 470-860 Mc/s was announced by Plessey at the Paris Components Show—a report of which appears on p. 119. The tuner has four push-buttons which operate directly a 60° tuning capacitor, thus eliminating the more usual switches. Two versions are available, to cater for both 75Ω unbalanced and 300Ω balanced inputs. The tuner is obtainable from the Electro-mechanical Division, New Lane, Havant, Hampshire.

WW 330 for further details

# MARCH MEETINGS

Tickets are required for some meetings: readers are advised, therefore, to communicate with the secretary of the society concerned

## LONDON

1st. I.E.E. & I.E.R.E.—Discussion on "Infra-red camera techniques" at 2.0 at Savoy Pl., W.C.2.

2nd. I.E.E.—Colloquium on "Microphones" at 9.0 at Savoy Pl., W.C.2.

7th. I.E.E.T.E.—"Control by computer" by A. St. Johnston at 6.0 at Savoy Pl., W.C.2.

7th. I.E.E. Grads—"An introduction to silicon controlled rectifiers" by P. J. N. Norris at 6.30 at Savoy Pl., W.C.2.

8th. I.E.E. & Soc. of Instrument Tech.—"A new approach to measurement and data transmission for process-control systems" by I. R. Young, A. T. Keefe and G. Moss at 5.30 at Savoy Pl., W.C.2.

8th. Radar & Electronics Assoc.—"Where are we with radar?—some highlights in radar development and achievement" by K. F. Sizer at 7.0 at R.S.A., John Adam St., W.C.2.

9th. I.E.E.—"Applications of electrostatics" by A. W. Bright and P. L. Secker at 5.30 at Savoy Pl., W.C.2.

9th. I.E.E.—"The scanning electron microscope and other electron probe instruments" by Prof. C. W. Outley at 6.0 at Savoy Pl., W.C.2.

9th. S.E.R.T.—"Electronic organs" by K. G. Borge at 7.0 at the London School of Hygiene, Keppel St., W.C.1.

9th. R.S.G.B.—"Aerial farming in a monastery" by Rev. P. Sollow (G3BGL) at 7.0 at R.S.A., John Adam St., W.C.2.

9th. B.K.S.T.S.—"Auditorium acoustics" by C. C. Buckle at 8.0 at Central Office of Information, Hercules Rd., S.E.1.

10th. I.E.E.—Discussion on "The multicarrier performance of communication-satellite repeaters" at 5.30 at Savoy Pl., W.C.2.

11th. I.E.E.—"Some recollections of the early days of radio research" by Dr. R. L. Smith-Kose at 5.30 at Savoy Pl., W.C.2.

14th. I.E.E.—"The explanation of some fundamental phenomena of modern physics using a ballistic theory of light" by R. A. Waldron at 5.30 at Savoy Pl., W.C.2.

14th. I.E.E.—"The ten-element band-pass filter section and its applications" by G. C. S. Brown at 5.30 at Savoy Pl., W.C.2.

16th. B.K.S.T.S.—"The B.B.C. television film department" at 7.30 at Central Office of Information, Hercules Rd., S.E.1.

21st. I.E.E.—"Electron-beam welding and machining" by H. N. G. King at 6.0 at Savoy Pl., W.C.2.

22nd. I.E.E.—Discussion on "Solid-state switching—for better or for worse?" at 6.0 at Savoy Pl., W.C.2.

23rd. I.E.E.—Discussion on "Technical information—a new teaching subject" at 5.30 at Savoy Pl., W.C.2.

23rd. I.E.R.E.—"The propagation of sound through liquids" by Dr. R. W. B. Stephens at 6.0 at 9 Bedford Sq., W.C.2.

24th. I.E.E.—"The Graham Clark Lecture—'The place of the engineer in society'" by Lord Snow at 5.30 at Savoy Pl., W.C.2.

28th. I.E.E., I.E.R.E. & Television Soc.—"Semiconductors in television receivers" by P. L. Mowers, R. Bridgen and K. E. Martin at 5.30 at Savoy Pl., W.C.2.

29th. I.E.R.E. & I.E.E.—Symposium on "Computer control in industry: equipment design and application engineering" at 2.30 at the London School of Hygiene and Tropical Medicine, Keppel St., W.C.1.

30th. B.K.S.T.S.—"The use of magnetic tape" by P. T. Hobson at 7.30 at Central Office of Information, Hercules Rd., S.E.1.

31st. I.E.R.E.—A symposium on "Monitoring of ground and airborne I.L.S. equipment for automatic landing" at 2.30 at the London School of Hygiene and Tropical Medicine, Keppel St., W.C.1.

## ARBORFIELD

10th. I.E.R.E.—"Random signal testing" by P. Atkinson and A. Ley at 7.30 at R.E.M.E. School of Electronic Engineering.

## BIRMINGHAM

7th. I.E.E.—"Radar—present position and future trends" by Dr. E. V. Glazier at 6.30 at the Midlands Electricity Board, Summer Lane.

23rd. S.E.R.T.—"Colour television" by B. J. Rogers at 7.30 at College of Advanced Technology, Gosta Green.

28th. I.E.E.—"A review of laser devices and applications" by N. Farries at 6.30 at the Midlands Electricity Bd, Summer Lane.

## BRIGHTON

30th. I.E.E.—"The radiophonic workshop of the B.B.C." by F. C. Brooker at 6.30 at College of Technology, Moulsecoomb.

## BRISTOL

23rd. I.E.R.E. & Brit. Computer Soc.—"High-speed magnetic thin film memories" by A. T. Gibson at 7.0 at University Engineering Laboratories, University Walk, Clifton.

## CAMBRIDGE

10th. I.E.E.—"A traffic simulator" by Dr. F. G. Heath at 8.0 at the University Engineering Dept., Trumpington St.

## CARDIFF

7th. I.E.R.E. & I.E.E.—"Telemetry—the present position and future trends" by R. E. Young at 6.0 at South Wales Institute of Engineers.

## CARSHALTON

30th. S.E.R.T.—"The installation and maintenance of domestic colour receivers" by D. J. Seal at 7.0 at the College of Further Education, Nightingale Rd.

## CATTERICK

8th. I.E.E.—"Speech compression" by Dr. J. Swaffield at 6.30 at the School of Signals, Catterick Camp.

## CHELMSFORD

22nd. I.E.R.E.—"Various aspects of microwave ferrites" by J. A. Penney at 6.30 at the Technical High School, Patching Hall Lane, Broomfield.

## CHESTER

14th. I.E.E.—"Telemetry—the present position and future trends" by R. E. Young at 6.30 at the College of Furnier Education.

## CHRISTCHURCH

23rd. I.E.E.—"Radio interference problems in the Royal Navy" by B. N. Amos at 6.0 at the King's Arms Hotel.

## COVENTRY

14th. I.E.R.E.—"Radio astronomy" by H. Gunt at 7.0 at the Lanchester College of Technology, Priory St.

## CRAWLEY

23rd. I.E.E.—"Systems engineering" by R. L. Smith at 6.30 at the College of Further Education.

## DORKING

16th. I.E.E.—"Applications of masers—what they are and what they do" by Dr. K. Hozelitz at 7.0 at Star and Garter Hotel.

## DERBY

31st. I.E.E.—"The problems of block release courses" by T. S. Hopkinson at 6.0 at College of Technology, Kedleston Rd.

## EDINBURGH

9th. I.E.R.E. & I.E.E.—"Laser range finders—systems analysis and electronic circuits" by G. Hamilton and A. Fowler at 7.0 at the Dept. of Natural Philosophy, The University, Drummond Street.

29th. I.E.R.E. & I.E.E.—Symposium on "Tape recording of biological signals" at 9.30 at the Royal Infirmary, Lauriston Pl.

## EVESHAM

29th. I.E.R.E.—"U.H.F. tuners" by R. Bridgen at 7.0 at the B.B.C. Club, High Street.

## FARNBOROUGH

1st. I.E.E.—"Colour television transmission systems" by W. Wharton at 6.30 at the Technical College, Boundary Rd.

31st. I.E.R.E.—"Random access communication system" by L. C. Walters at 7.15 at the Technical College.

## GLASGOW

10th. I.E.R.E. & I.E.E.—"Laser range finders—systems analysis and electronic circuits" by G. Hamilton and A. Fowler at 7.0 at the Institution of Engineers and Shipbuilders, 39 Elmbank Cres.

14th. I.E.E.—"Faraday Lecture—'Computers, control and automation'" by P. D. Hall at 7.0 at the Concert Hall.

## HARLOW

8th. I.E.R.E.—"Automatic tracking from surveillance radars" by Dr. T. Buckley at the Technical College, The High.

## Huddersfield

3rd. I.E.R.E.—"Automatic tracking from surveillance radars" by Dr. T. Buckley at the College of Technology.

## LEICESTER

8th. I.E.E.—"Development of satellite communications" by F. J. D. Taylor, W. J. Bray and R. W. White at 6.30 at the College of Technology.

15th. I.E.E.—"Lasers and direct energy weapons" by Dr. R. C. Smith at 6.30 at the University.

15th. Television Soc.—"Pulse-width modulated amplifiers" by G. M. Sinclair at 7.15 at Vaughan College, St. Nicholas St.

## LIVERPOOL

16th. I.E.R.E.—"Radiophony—the synthesis of sound effects for radio and television" by F. C. Brooker at 6.30 at Walker Art Gallery, William Brown St.

21st. I.E.E.—"Electronic design" by H. V. Beck at 6.30 at the Electrical Engineering Department, The University.

25th & 26th. I.E.E.—"Faraday Lecture—'Computers, control and automation'" by P. D. Hall at 6.30 at Philharmonic Hall.

## LLANDAFF

14th. Television Soc.—"TV colour systems" by S. Sansom at 7.30 at the Technical College.

## MANCHESTER

1st. I.E.E.—"Faraday Lecture—'Computers, control and automation'" by P. D.

Hall at 2.15 (students) and 7.30 at the Free Trade Hall.

#### MIDDLESBROUGH

23rd. I.E.E.—“Communications satellite systems” by Dr. H. C. Husband and H. Stanesby at 6.30 at Cleveland Scientific Institute.

#### NEWCASTLE-UPON-TYNE

2nd. S.E.R.T.—“Industrial electronics” by E. Surtees at 7.15 at Charles Trevelyan Technical College, Maple Terrace.

8th. I.E.E.—“Faraday Lecture ‘Computers, control and automation’” by P. D. Hall at 7.15 at City Hall.

9th. I.E.E.—“The application of analogue computers” by C. Cox at 6.0 at Institute of Mining and Mechanical Engineers, Westgate Rd.

#### NOTTINGHAM

29th. S.E.R.T.—“Current trends in transistor radio design and servicing” by D. E. A. Harvey at 7.30 at East Midlands Gas Board, Lower Parliament St.

#### PLYMOUTH

22nd. I.E.E.—“Electronic circuits” by G. King at 7.0 at City of Plymouth College of Technology.

#### PORTSMOUTH

2nd. I.E.E.—“Proximity sensing by magnetic induction applications and techniques” by D. Barnard at 6.30 at Highbury Technical College, Cosham.

16th. I.E.E.—“The future of automation” by Dr. A. M. Utley at 6.30 at the College of Technology, Anglesea Rd.

#### READING

28th. “Planning of communication satellite systems” by J. K. S. Jowett at 7.30 at the Great Western Hotel.

#### SALISBURY

9th. I.E.E.—“Electronic circuits—past, present and future” by G. King at 6.30 at College of Further Education.

#### SCUNTHORPE

15th. I.E.E.—“Computers in control of processes” by Dr. D. N. Ruscott at 7.0 at the Technical College.

#### SOUTHAMPTON

8th. I.E.E. & I.E.E.—“Electron microscopy and micro-electronics” by W. C. Nixon at 6.30 at University.

29th. S.E.R.T.—“Insulation and earth resistance measurements” by E. A. King at 7.30 at the College of Technology.

#### STOKE-ON-TRENT

29th. I.E.E.—“Lasers and Lasers” by Professor D. J. E. Ingram at 7.0 at North Staffs College of Technology, College Rd.

#### SWANSEA

17th. I.E.E.—“The application of secondary surveillance radar to air traffic control” at 6.0 at University College.

#### THURSO

17th. I.E.E.—“Telemetry—present position and future trends” by R. E. Young at 7.0 at the Technical College.

#### WHITLEY

24th. I.E.E.—“Radar, present position and future trends” by Dr. E. V. D. Glazier at 6.45 at Botham's Cafe, Skinner St.



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### A COMPLETE RANGE OF PRECISION MOULDED INSULATION SWITCHES

Produced on our highly automated plant these switches are inexpensive but completely reliable, giving a normal maximum life of 25,000 operations. Strict quality control during all production stages and top quality materials ensure that the finished products are superbly finished in all respects.

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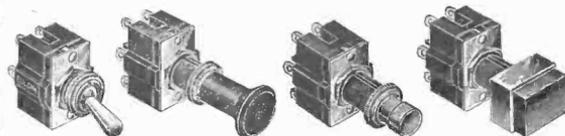
List No.  
S.M.315/PD/TERM

List No. S.M.443

List No. S.R.M.265/  
TERM/SQ.

This series is based upon two basic switch units giving Change-Over, Make-Break either biased or non-biased switching, which can be actuated by many different methods. Lever-toggles are the normal means but Push-button, Push-pull and Push-successional action are also available. Connections to tags or screw terminals.

#### TWO POSITION DOUBLE POLE TYPES



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S.M.270/PD

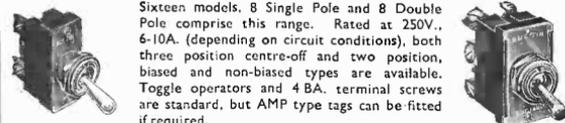
List No. S.M.446

List No. S.R.M.270

List No. S.R.M.270/SQ.

The basic switching arrangement in this range is Change-Over, which can, if desired be wired for Make-Break. Actuators are as for the Single Pole range above, but connection is to tags only.

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List No. S.780

List No. S.780

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CROWN AGENTS	U.K.A.E.A.	D.S.I.C.

# 1000W LOUDSPEAKER

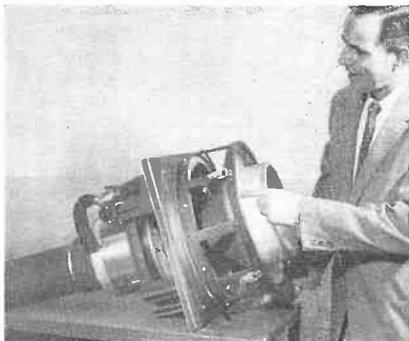
2-IN CONE DISPLACEMENT AND AIR-COOLED  
VOICE COIL

WHAT is claimed to be the most powerful single acoustic reproducer ever built has been developed by Stromberg-Carlson, a division of General Dynamics, in the U.S.A., on behalf of Convair. The loudspeaker, rated at 1 kW and weighing about 150 lb, will be installed in Convair's acoustical laboratory, where it will be used in research into the effects of high-intensity noise on components and structures of missiles and jet aircraft.

A number of unique design features are incorporated in the speaker to make its remarkable acoustic capabilities possible. The most unusual portion of it is the low-frequency unit extending up to 300 c/s. This is driven by a powerful 24-lb ring magnet of Alnico V, having a total flux in the air gap of 696,000 Maxwells. The heavy-duty cone is specially mounted to allow excursions of up to two inches. Because of the large amounts of power that must be dissipated, the voice coil is made of materials to withstand high temperatures, so that it is capable of continuous operation at temperatures up to 500°F. A small fan blows air through the voice coil while the loudspeaker is in use.

In addition to the big "woofers," the loudspeaker also includes a high-powered acoustic compression driver and coaxial horn for reproducing mid-range frequencies (300 to 2400 c/s). Thus the speaker reproduces the first six standard octave bands, as defined by the American Standards Association.

Although, in the initial application of this loudspeaker, there was no need for producing the extreme upper end of the



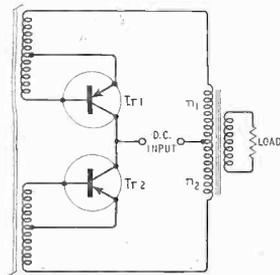
1 kW loudspeaker developed for investigating high-intensity acoustics. The unit weighs 150 lb and is mounted in a frame 18 in square. Cone displacement can be 2 in and the voice coil is air cooled.

audible frequency spectrum, Stromberg-Carlson has designed, and is now producing, high-frequency "tweeters" which will operate the range of the speaker to 15 kc/s. For any future application of the loudspeaker where this high-frequency response is required, 13 of these tweeters will be mounted in a ring around the mid-range horn.

The entire loudspeaker structure is mounted in a heavy cast aluminium frame only 18 in square, and has been designed so that each of the various moving components, where trouble is most likely to develop, can be easily removed and replaced without dismantling the entire speaker or removing it from its mounting.

## LOW-VOLTAGE TRANSISTOR CONVERTER

WITH the current interest in "unconventional" sources of electrical power (thermionic and thermoelectric generators, fuel cells, and solar cells) which produce high-current low-voltage outputs, it has become necessary to develop low-voltage d.c. to a.c. converters which offer a high efficiency.

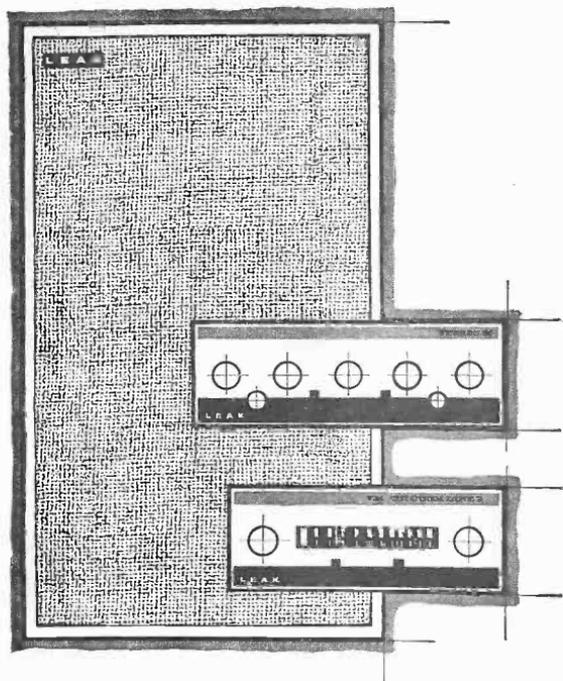


Switching converter giving an efficiency of 80% at an input of 1 V.

Normally, transistor converters give only a low efficiency when operated at low input voltages, and to avoid this the RIPPLE isotope-powered thermoelectric converters developed at Harwell use tunnel-diode converters. The problem is particularly relevant to space vehicles, and a transistor design has been developed under a N.A.S.A. contract, which provides an efficiency claimed to be about 80% for a d.c. input of 20 A at 1 V. At an input of 3 V the efficiency is said to be increased to 94%.

This high efficiency is, of course, obtained by operating the transistors as switches. When an input voltage is applied to the circuit shown one of the transistors will start to conduct (Tr1 say). When the saturable-core transformer becomes saturated, the base current in Tr1 will be turned off. The energy stored in the transformer then causes Tr2 to turn on. The alternate saturation and desaturation of the transformer causes the input voltage to appear alternately across  $n_1$  and  $n_2$ , thus providing a rectangular output in the load.

The transistors should be reasonably well matched and mounted on a common heat sink. However, a high degree of mismatch can be tolerated between the base-emitter voltages of the transistors by adjusting the relative number of turns on the base-emitter windings of the saturable-core transformer.



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**WIRELESS WORLD** Editorial, May  
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"People sometimes ask why there is any necessity to change to  
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sufficient reason now that solutions of the problem of linearity in the  
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additional bonuses we get smaller size, cooler running and the prospect  
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**THE  
WORLD'S  
SMALLEST**

# SINCLAIR MICRO-6 SIX STAGE RECEIVER

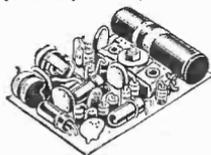
**smaller  
than a  
box of matches**

## FANTASTIC RANGE AND POWER

THE SINCLAIR MICRO-6 is proving more and more the modern way to listen to radio. This fantastic set takes up less room in your pocket than a box of matches. It has impressive power and selectivity, yet can never interfere with the privacy of other people. Often you will find your MICRO-6 giving satisfaction in places where other radio sets simply cannot be heard at all. It is economical to run and most dependable in use. The 6-stage circuit developed by Sinclair Radionics centres upon the use of special Micro-Alloy Transistors (Sinclair M.A.T.s) to achieve such phenomenal performance. Yet building is easy, and by following the well-prepared instruction manual success is assured even if you have never put a transistor set together before—so start yours today. Over 30,000 constructors have now built the Micro-6.

### REMARKABLE CIRCUITRY

In the Sinclair Micro-6 three Micro-Alloy Transistors are used in a unique and highly efficient 6-stage circuit as follows: Two stages of RF amplification are followed by an efficient double-diode detector which drives a high-gain AF Amplifier. Powerful A.G.C. applied to the first RF stage ensures fade-free reception from the most distant stations tuned in on the medium waveband. Everything including ferrite rod aerial and pill-size batteries are contained within the elegant tiny white, gold and black case. Inserting the plug of the earpiece included, switches the set on.



- **SIZE**—1½" x 1½" x ¼"
- **WEIGHT**—One ounce, including batteries.
- **BANDSPREAD** FOR LUXEMBOURG.
- **PLAYS ANYWHERE**—IN CAR, BUS, TRAIN, ETC.

Building is simple. All parts including transistors, lightweight earpiece, case and dial, and 8-page instruction manual come to

**Molloy Mercury Cell Type 274312 (2 required), each 1/11. (Pack of 6 10/6.)**

**59/6**

## SINCLAIR Z.12 COMBINED AMPLIFIER AND PRE-AMP

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*Designed to laboratory standards  
Ideal for 12v. battery operation*

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**CONTINUOUS  
SINE WAVE  
(24 w. PEAK)**  
**15 w. R.M.S.  
Music Power  
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**Ready built, tested  
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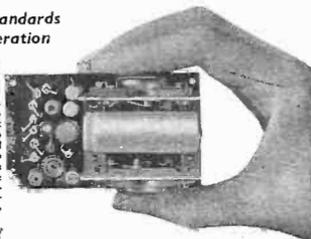
THE SINCLAIR Z.12 is a universally flexible amplifier, exceptionally powerful, fantastically small. It is supplied ready built, and is very easily installed. Intended as the heart of any high quality hi-fi system, its small size and high efficiency of the Z.12 make it equally applicable for a guitar, for car radio, P.A. system or any other application where the highest possible quality is the first requirement. The Z.12 incorporates its own pre-amplifier to which you add the tone and volume control system of your choice for mono or stereo as shown in the manual supplied with every Z.12. The size, the performance, and the price of the Sinclair Z.12 all favour the constructor who wants the best in modern transistor equipment; in fact, the Z.12 is today's finest buy in top grade high fidelity.

*"I am extremely pleased with the Z.12" writes H.M. of Dublin who saw the Z.12 advertised in "Practical Wireless". "The quality is excellent and is better with my hi-fi, speaks than my high amplifier with 3 speakers. It is far more sensitive and produces a very pleasing tone with a 12 v. supply. With no signal input, I can detect an audio amplifier to resonance."*

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- For 6-20 v. D.C. operation; ideally suitable for use with 12 v. battery.
- 8 special H.F. Transistors in special circuit having ultra-linear class B output.
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# SINCLAIR MICRO FM

## POCKET SIZE COMBINED F.M. TUNER

## RECEIVER

# 1

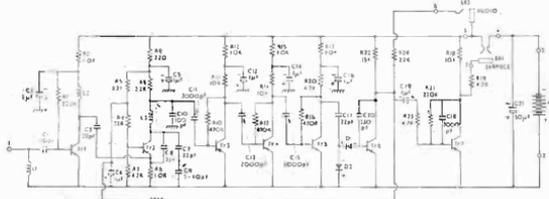
**ST. WITH PULSE COUNTING DETECTOR  
WITH LOW I.F. TO CUT OUT ALIGNING  
WITH TWO OUTPUTS FOR DOUBLE PURPOSE  
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TO INCORPORATE THESE AND MANY MORE  
EXCLUSIVE FEATURES IN A POCKET SIZE  
DESIGN OF OUTSTANDING EFFICIENCY**

**7 TRANSISTORS  
2 DIODES  
SUPERHET FM  
2 OUTPUTS  
ELEGANT  
PROFESSIONALLY  
STYLED CASE**

- Size—2 1/4" x 1 1/4" x 3/4" plus aerial.
- Tunes from 88 to 108 Mc/s.
- One output for amplifier, recorder, etc., and one for personal listening.
- In neat black case with polished and brushed aluminium escutcheon and matching tuning control.
- No alignment problems.

**£5.19.6**

Once again Sinclair Radionics prove to constructors that very high standards of efficiency can be successfully combined with micro-techniques. The Sinclair Micro FM is an outstanding example. It incorporates a number of advances over conventional practice to achieve amazing standards of performance. Despite its small size, this fully fledged Transistor 2 diode FM superhet has two outlets to enable it to be used both as a tuner for hi-fi or tape recorder and as an independent pocket receiver for personal listening. Pulse counting detection assures improved linearity and therefore better audio quality, low I.F. does away with alignment problems. Such is the sensitivity of this tuner that the telescopic aerial is sufficient for good reception almost everywhere. In styling, the Sinclair Micro FM is the most elegant, professional looking design ever offered to constructors, yet with all these plus features, this set costs pounds less, so that anyone can enjoy the advantages of FM to the full today.



**BRIDGED TECHNICAL  
DESCRIPTION OF THE  
SINCLAIR MICRO F.M.**



**GUARANTEE:**  
If you are not fully satisfied with your purchase when you receive it, return it to us when your money will be refunded at once in full.

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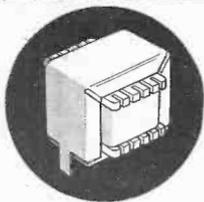


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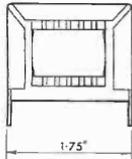
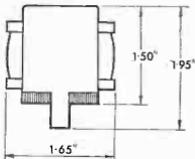
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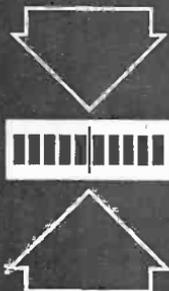
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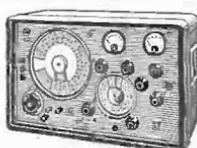
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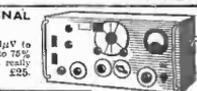
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Kit.....£24.15.0 Assembled £34.0.0



### TRANSISTOR TESTER Model 1M-30U

Unmatched for quality and performance at the price.

Provides a complete d.c. analysis of PNP and NPN transistors and diodes. D.C. gain (Beta, Alpha) is read directly on calibrated scales. Four lever switches facilitate fast, easy test selection. Internal batteries for tests up to 9 v. Provision for connection to ext. power supply for higher

voltage and current tests. Modern functional styling. Size 5 1/2 in. high x 10 1/2 in. deep x 10 1/2 in. wide.

Kit.....£24.18.0 Assembled £35.10.0

## OUTSTANDING EQUIPMENT FOR THE DISCERNING HI-FI ENTHUSIAST



### "STARMAKER 33" TRANSISTOR PA GUITAR AMPLIFIER Model PA-2

This is a high performance amplifier whose size and weight allows easy transportation. Ideal for vocal and instrumental groups, P.A., electronic organs, guitars, etc. Features include: 20w. amplifier (33 watts. I.H.F.M.), two heavy duty speakers, 4 inputs on two channels, variable tremolo, modern elegant cabinet. Size: 18in. h. x 29in. w. x 10in. deep. Wt. 51 lb.

Costors or legs available as optional extras.

Kit.....£44.19.0 Assembled £59.10.0



### New! BERKELEY Slim-line SPEAKER SYSTEM

A new concept in Heathkit loudspeaker design. The cabinet shell is assembled and finished in superb Queensland walnut veneer. Two specially designed speakers, a 12in. bass unit and 4in. mid/high frequency unit and an L.C. cross-over network provide the smooth 30-17,000 c/s. frequency response. Its professional cabinet styling will blend with both traditional and contemporary decors. 15 ohm nominal impedance. Size 26" x 17" x 7 1/2" deep.

Kit.....£18.10.0 Assembled £23.0.0

## MODELS FOR THE MUSIC LOVER AND FOR FAMILY ENTERTAINMENT

### A WELL DESIGNED F.M. TUNER Model FM-4U

Tuning range 88-108 Mc/s. Flywheel tuning. Attractive Plastic Front Panel in two-tone grey with golden trim surround and motif. Thermometer type visual tuning indicator. Pre-aligned. I.F. transformers. Three stages. Wide-band low distortion Ratio Detector. R.F. Unit, wired, tested and pre-aligned. Printed circuits for I.F. amplifiers and ratio detector. Built-in power supply. Output socket for stereophonic adaptor (for stereo transmission when available).



TUNER UNIT Model FMT-4U with 10.7 Mc/s. I.F. output. £2/15; (inc. P.T.). I.F. AMPLIFIER and power supply Model FMA-4U complete with case and valves, £13/13/-. Sold separately.

Kit Total.....£16.8.0

Assembly can be arranged on your behalf.

### "OXFORD" LUXURY TRANSISTOR PORTABLE Model UXR-2

This superb transistor radio is the ideal domestic or personal portable. Medium and Long Wave receiver. Solid leather case and handle. Easy-to-read tuning scale. Extra large loudspeaker. Push button L, MW and tone. 10 semi-conductors (7 transistors plus 3 diodes). Sockets for personal earphone, tape recorder, car aerial. Internal 9-volt battery (not supplied), lasts for months. Latest printed circuit techniques.



Kit.....£14.18.0 incl. P. Tax.

Assembly can be arranged on your behalf.

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ALSO "AMATEUR" RADIO BROCHURE COVERING BRITISH & AMERICAN MODELS

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So easy to build



So easy to use

**TRANSISTOR MIXER**  
Model TM-1

"A must for the tape enthusiast"



Four channels with individual, continuously variable controls, plus a master volume control to allow for recording from a wide variety of sources, e.g. dynamic and crystal microphone, radio tuners, record players, etc.

- ★ 7 transistor circuit and internal 9 v. battery (not supplied) allows unit to be used "in the field" as well as in the home, studio, etc.
- ★ Printed circuit board ensures consistent performance, easiest possible construction.
- ★ Professional, modern, compact, low silhouette styling.
- ★ Beautiful walnut veneered, fully finished cabinet.
- ★ Attractive anodised aluminium front panel.
- ★ Size: 11 1/2 in. x 7 1/2 in. x 3 1/2 in. high.

Kit £11.16.6 incl. cabinet Assembled £16.17.6 incl. cabinet  
Full specification leaflet sent on request.

The Outstanding  
**20 ± 20 WATT TRANSISTOR**  
**STEREO AMPLIFIER**  
Model AA-22U



This "International Class" amplifier offers you a realism and beauty of music never before obtainable at such a competitive price.

- ★ Professional, elegant, compact, slim-line styling.
- ★ The best of American transistor techniques in a British amplifier.
- ★ Beautiful walnut veneered, fully finished cabinet available as an optional extra.
- ★ 5 stereo inputs (five on each channel) accommodate pick-up, radio tuner, tape and two other sources.
- ★ 20 transistor 10 diode circuit.
- ★ Dimensions: 15 1/2 in. wide x 3 1/2 in. high x 12 in. deep.

Kit £39.10.0 less cabinet  
Walnut cabinet for free standing use £25.0 extra.

**COMPARE ANY HEATHKIT MODEL FOR PRICE, PERFORMANCE, QUALITY**

**3+3 W HI-FI STEREO AMPLIFIER**

**Kit Model S-33H** An inexpensive stereo-organ amplifier with the high sensitivity necessary for lightweight miniature ceramic pick-ups (e.g., Decca Dynam). De laux version of the S-33 with attractive two-tone grey Perspex panel.  
Kit £15.17.6 Assembled £21.7.6



**5 W HI-FI MONO AMPLIFIER**  
**Kit Model MA-5**

A low-priced general purpose Hi-Fidelity amplifier based on the popular S-33 for those who do not require a stereo-gram and radio inputs. Suitable for most crystal pick-ups. A printed circuit simplifies construction.  
Kit £10.19.6 Assembled £15.10.0

**HI-FI MONO POWER AMPLIFIER**  
**Kit Model MA-12**

A compact Hi-Fidelity power amplifier (including auxiliary power supply), 12 watts output. Wide frequency range and low distortion. A variable sensitivity control is fitted enabling it to be used with an existing amplifier in a stereophonic system. Other applications include sound reinforcement systems, transmitter modulators, for use with tape recorders, also as a general purpose laboratory amplifier.  
Kit £11.18.0 Assembled £15.18.0

**STEREO CONTROL UNIT KIT**  
**Model USC-1**

Incorporates all worthwhile features for Hi-Fidelity stereo and mono. Push-button selection, accurately ±1 dB. Negative feedback rumble and variable low-pass filters. Printed circuit boards. Accepts inputs from most tape-heads and any stereo or mono pick-up.  
Kit £19.10.0 Assembled £26.10.0

**HEATHKIT-THOMAS (Transistorized) ELECTRONIC ORGAN KIT**  
(with Colour Glow) Model GD-325E

Can be built with no knowledge of electronics.  
Kit £205.0.0 (Price includes carriage and duty)

**HI-FI EQUIPMENT CABINETS**

A range of equipment cabinets is now available. Designed for maximum operating convenience or for where room space is an over-riding consideration, this range includes easy-to-build kits or ready-assembled cabinets in the white for finish to own requirements.

- ★ "MALVERN" (Illustrated) Kit, £18.1.0 (inc. P.T.). Assembled (left in the white) £23.6.0.
- ★ "GLOUCESTER" for Tape Deck and Record Player, Kit £18.10.0 (inc. P.T.). Assembled £23.15.0
- ★ "CHEPSTOW" for Record Player or Tape Deck, Kit £11.12.6 (inc. P.T.). Assembled £16.17.6

**How to install Hi-Fi in YOUR home**

If you are planning to install a Hi-Fi system in your home, and are uncertain of the type of equipment to use, our widely experienced technical staff will wish pleasure put forward recommendations. All you have to do is state the type of installation contemplated, the price you are prepared to pay and give details of existing equipment you wish to include, if possible.

**HI-FI STEREO AMPLIFIER**  
**Kit Model S-99**

18 w. output (9 per channel) with 0.2 per cent. distortion at 9 w. per channel. It has ganged controls. Stereo/Mono gram, radio and tape recorder inputs and push-button selection. Ultra-linear push-pull output. P.C. board. Attractive Perspex front panel with golden surround and grey metal cabinet.  
Kit £28.9.6 Assembled £38.9.6



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Deferred Terms available on orders above \$10

**MONO CONTROL UNIT KIT**

**Model UMC-1**  
Ideal for use with MA-12 or similar amplifier. Output 0.25 v. Send for full details.  
Kit £8.12.6 Assembled £13.12.6



**HI-FI SPEAKER SYSTEM KIT**  
**Model SSU-1**

Ducted-port bass reflex cabinet "in the white". Frequency response is 40-16,000 c/s. Power rating 10 watts. Matched speaker units: Bin, high flux (12,000 lines) with hyperbolic cone and 4in. wide angle dispersion type for higher frequencies.  
Kit (with legs) £12.12.0 (less legs) £11.17.6 (inc. P.T.)



**"COTSWOLD" SPEAKER SYSTEM KIT**

This acoustically designed enclosure measures 26 x 23 x 14 1/2 in. and houses a special 12in. bass speaker with 2in. speech coil, elliptical middle speaker together with a pressure unit to cover the full frequency range of 30-20,000 c/s. Its polar-distribution makes it ideal for really Hi-Fi Stereo. Delivered complete with speakers, cross-over unit, level control, grille cloth, etc. Let in the white for finish to personal taste, all parts are pre-cut and drilled for ease of assembly.  
Kit £25.12.0 Assembled £33.17.0



**"COTSWOLD M.F.S." SPEAKER SYSTEM KIT**

This model, based on the standard Cotswold, measures only 36in. high, 16 1/2 in. wide by 14in. deep. Particularly recommended to those who require the best results in small rooms.  
Kit £25.12.0 Assembled £33.17.0



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Technically



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## NEW! LOW-COST 3in. OSCILLOSCOPE Model OS-2

- ★ Vertical amplifier 2 c/s to 3 Mc/s.
- ★ Modern professional styling.
- ★ Vertical sensitivity 100 mV/cm.
- ★ Compact size 5in. x 7 1/2in. x 12in.



- ★ Light weight—under 10lb.
- ★ Time base range 20 c/s to 200 kc/s.
- ★ Horizontal input 100 mV/cm.
- ★ Mamelet c.r.t. screen.

### MULTIMETER KIT Model MM-1U

Provides wide voltage, current, resistance and dB ranges to cover hundreds of applications. Sensitive 20,000 ohms/volt D.C. and 5,000 ohms/volt A.C. Ranges: 0-1.5 v. to 1,500 v., A.C. and D.C.; 0-150µA to 15 A., D.C. Measures resistance from 0.2Ω to 20MΩ. 4 1/2in. 50µA meter. A polarity reversing switch eliminates transferring test leads when alternately measuring  $\pm$  and  $-$  voltages



Kit £12.18.0 Assembled £18.11.6

### OSCILLOSCOPE TRACE DOUBLER KIT Model S-3U



This device will extend the use of your single-beam oscilloscope and, at a nominal cost, will give you the advantages of a double (or other multiple) beam scope.

Kit £12.18.0 Assembled £18.10.0

### R.F. SIGNAL GENERATOR KIT Model RF-1U



Provides extended frequency coverage on six bands from 100 kc/s. to 100 Mc/s on fundamentals and up to 200 Mc/s on calibrated harmonics.

Kit £13.8.0 Assembled £19.18.0

**DECADE RESISTANCE BOX KIT Model DR-1U.** Range 1-99,999Ω in 12 steps. Ceramic switches throughout. Current rating from 500 mA. to 5 mA, according to decade in circuit. Polished wooden cabinet supplied complete. Kit £10.8.0 Assembled £14.8.0

### RESISTANCE-CAPACITANCE BRIDGE KIT Model C-3U



Measures capacitance 10pF. to 1,000pF. Power-factor and resistance 100Ω to 5M ohms. Test voltages 5-450 v. Safety switch provided.

Kit £10.10.0 Assembled £16

### AUDIO SIGNAL GENERATOR KIT Model AG-9U



10 c/s. to 100 kc/s., switch selected. Distortion less than 0.1%. 10 v. sine wave output metered in volts and dB's.

Kit £22.10.0 Assembled £30.10.0

● Prices quoted are Mail Order Prices. ●

This compact oscilloscope offers excellent performance, is professional in appearance and is an instrument you will be proud to own. Apart from its obvious uses by radio/TV engineers, etc., it is ideal for construction, study and use by workshop apprentices and by students in schools, technical colleges and universities.

Kit £22.18.0 Assembled £30.8.0

### A.M./F.M. TUNER KIT

Tuning range 88-108 Mc/s. (FM) 16-50, 200-550, 900-2,000 m.



Physwell tuning. Attractive Perspex front panel in two-tone grey with golden trim. Thermometer type tuning indicators, pre-aligned I.F. transformers. Switched wide and narrow A.M. bandwidths. **TUNING HEART Model AFM-T1** £41/13.6 (inc. P.T.). **I.F. AMPLIFIER and Power Unit Model AFM-A1.** Complete with metal cabinet and valves £22/11.8. Sold separately. Kit Total £27.5.0

### DUAL-WAVE TRANSISTOR PORTABLE RADIO KIT Model UXR-1

Presented in elegant real hide case with careful gold relief.

Can be assembled in 4 to 6 hours and you have a set in the top light of transistor portables. Pre-aligned I.F. transformers, printed circuit and a 7in. x 4in. high flux speaker. Covers both Long and Medium waves. Dimensions 9 1/2in. x 7 1/2in. x 3 1/2in. Kit £12.10.0 (inc. P.T.)



### SINE/SQUARE GENERATOR Model IG-82U



Covers 20 c/s-1 Mc/s. in 5 bands. Simultaneous Sine and Square Wave outputs. Loss than 0.15µs rise time and on Square Wave. Less than 0.5% distortion on Sinewave. Up to 10 volts output. This attractively styled generator is designed for maximum operating convenience. Size 13in. x 8 1/2in. x 7in. deep. Kit £24.10.0 Assembled £36/10/0

### ELECTRONIC WORKSHOP KIT EW-1

20 exciting experiments can be made with this one kit.

Kit £17.13.6 (incl. P.T.)

● Deferred Terms available on all orders above £10. ●

### 4 1/2in. VALVE VOLTMETER KIT Model V-7A

The world's most popular valve voltmeter with printed circuit and 1 per cent. precision resistors to ensure consistent laboratory performance. It has 7 voltage ranges measuring respectively D.C. volts to 1,500 and A.C. to 1,500 r.m.s. and 4,000 peak to peak. Resistance measurements from 0.1 ohm to 1,000 megohms, with internal battery. D.C. input resistance is 11 megohms and dB measurement has a centre-zero scale. Complete with test prod. leads and standardising battery. Power requirements, 200-250 v. 40-60 c/s. A.C. 10 watts.



H.V. and R.F. Probes available at optional extras. Kit £13.18.6 Assembled £19.18.6

### 6in. VALVE VOLTMETER Model IM-13U

Modern styling. Many extra features. Unique gimbal brackets allows bench, shelf or wall mounting. Measures A.C. and D.C. volts 0-1.5, 15, 50, 150, 500, 1,500. Resistance 0.1 to 1,000MΩ. Size 5in. x 12 1/2in. x 4 1/2in. Complete with test prod. and leads.



Kit £18.18.0 Assembled £26.18.0

### DECADE CAPACITOR KIT Model DC-1

Capacity values 100µF to 0.11µF in 100µF steps. Precision silver-mica capacitors and minimum loss ceramic water switches ensures high accuracy.

Kit £7.5.0 Assembled £10.8.0

### TELEVISION ALIGNMENT GENERATOR KIT Model HFV-1

Offers the maximum in performance, flexibility and utility at the lowest possible cost. Several outstanding features have been incorporated in this model which are unusual in instruments in this price range. Frequency coverage 3.6 Mc/s. to 220 Mc/s. on fundamentals. Unique non-mechanical sweep oscillator system. High level output on all ranges. Sweep deviations up to 42 Mc/s. Built-in fixed and variable marker. Kit £27.18.0 Assembled £47.10.0

### CAPACITANCE METER KIT Model CM-1U

The Direct-Reading Capacitance Meter is a very low priced, time-saving instrument which is so useful that it should be part of the general equipment of every electronic laboratory and production line. Easily built in a few hours. It can be used 0.001µF, 0.1-1,000µF, 0.001µF, 0.01µF. The meter has 4 1/2in. scale and can be operated by an unskilled operator after a few minutes' instruction.



Kit £15.15.0 Assembled £21.14.0

● Prices include Postage U.K. ●

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**AMATEUR TRANSMITTER KIT**

**Model DX-40U**

Covers all amateur bands from 80 to 10 metres, crystal controlled. Power input 75 watts C.W. 60 watts peak controlled carrier phone. Outstanding provision for VFO. Filters minimise T.V. interference. Modulator and power supplies are built-in. Single knob band switching is combined with a pi-network output circuit for complete operating versatility. A high-grade moving-coil meter indicates the final grid or anode current. Provision is made for the use of 3 crystals with access through a trap-door in the back of the cabinet. A 4-position switch selects the appropriate crystal or a jack for external VFO which can be used instead of the crystals).

Kit ... £33.19.0 Assembled ... £45.8.0

**SINGLE SIDEBAND ADAPTER KIT**

**Model SB-10U**

May be used with most A.M. transmitters with certain provisions. Allows full use of existing equipment for SSB facilities. Band coverage: 80, 40, 20, 15, 10 m. Unwanted sideband suppression, better than 30 dB. Carrier suppression: better than 40 dB. Power requirements: 300 v. D.C. 85 mA. (average) 30 mA, standby, 140 mA reading. 200 V. A.C. 3.5 A. Meter: 2 1/2 in. Scale edge 600 V. A.C. movement, indicates carrier will and relative power output. Cabinet 11 in. high x 8 in. wide x 1 1/4 in. deep.

Kit ... £39.5.0 Assembled ... £54.18.0

**AUDIO SINE-SQUARE WAVE GENERATOR KIT. Model AO-1U**

Covers 20 c/s. to 150 kc/s. in four ranges with choice of sine or square waves. The latter up to 25 kc/s. Output 10 w. max. and distortion less than 1%. Ideal for audio testing. Size 9 1/2 x 6 1/2 x 5 in.

Kit ... £14.15.0 Assembled ... £21.5.0

**GRID-DIP METER KIT. Model GD-1U**

Functions as oscillator or absorption wameter. With plug-in coils for continuous frequency coverage from 1.8 Mc/s. to 230 Mc/s.

Kit ... £10.19.6 Assembled ... £13.19.6  
Additional Plug-in Coils Model 341-U extend coverage down to 350 kc/s. With dial correlation curves, 17/6.

**TRANSISTOR INTERCOM KITS Models XI-1U and XI-R-1U**

Ideal for home or business use. Up to five remote stations can be operated with each Master. The Master unit can call any one, any combination, or all five Remote stations and any Remote station can call the Master. A private Any Remote station cannot be interrupted or overheard by any other while a conversation is in progress. Any Remote station can talk to any one or all others provided the Master is manned. These kits have been designed for easy construction and high performance. The mahogany veneered wooden cabinets are supplied completely assembled and finished. The Master unit has a 4-transistor amplifier and is operated by an internal 9 v. battery as are the Remote units. Batteries are not included with the Kits.

Model XI-1U (Master) Kit ... £10.19.6 Assembled ... £16.19.6  
Model XI-R-1U (Remote) Kit ... £4.7.6 Assembled ... £5.16.0

**A WIDE RANGE OF BOOKS ON ELECTRONICS AND RADIO AVAILABLE.**  
Send for Lists and Prices.

**"MOHICAN" GENERAL COVERAGE RECEIVER KIT**

**Model GC-1U**

This fully transistorized receiver which includes 4 piezo-electric transistors, is in the forefront of receiver design. It is an excellent portable or fixed station receiver. The R.F. "front-end" is supplied as a pre-assembled and pre-aligned unit. Its many features include a 10-transistor circuit, printed circuit board, telescopic whip antenna, tuning meter, and a large slide-rule dial giving tuning meter, and a large slide-rule dial giving a total length of approximately 70 inches. Housed in a steel cabinet and powered by two 6 volt dry batteries (not supplied), mounted internally, it gives frequency coverage from 500 kc/s. to 30 Mc/s. in five bands, thus enabling world-wide reception. Electrical bandspread covers the amateur bands from 80 to 10 metres—each band having a scale length of approximately 8 inches. BFO tuning and Zener diode stabiliser. Size 6 1/2 x 12 in. x 10 in.  
Please write for specification leaflet.

Kit ... £37.17.6 Asmbld. ... £45.17.6

**STABILISED POWER PACK Models MSP-1M and MSP-1W**

Specialy recommended for industrial and laboratory use, meeting the need for a reliable and versatile stabilised power pack capable of a very high performance. Input 200-250 v. 40-60 c/s. Output fully fused. Outputs: H.T. 200-410 v. D.C. at 0.225 mA, in 3 switched ranges. Unstabilised A.C. 6.3 v. at 4.5 A. centre-tapped. Two 3 in. "screw-over" meters for reading voltage and current simultaneously. Separate L.T. and H.T. supply transformers. All output circuits are isolated. Size 13 in. x 8 1/2 in. x 9 1/2 in.

MSP-1M (with meters) Kit ... £36.12.6 Asmbld. ... £43.12.6  
MSP-1W (less meters) Kit ... £29.17.6 Asmbld. ... £36.17.6

**BALUN COIL UNIT KIT Model B-1U.**

Will match unbalanced co-axial lines to balanced lines of either 75 or 300 Ohm impedance. Frequency range 10-80 m., input up to 200 watts.

Kit ... £4.15.6 Asmbld. ... £5.8.6

**TAPE PRE-AMPLIFIER KITS Models TA-1M and TA-1S**

This Combined Tape Record/Reply Amplifier is available in both monophonic and stereo-phonetic models. Model TA-1M can be modified to the stereo version with modification kit TA-1C.  
TA-1M Kit £19.8.0 Asmbld. £28.18.0  
TA-1S Kit £25.10.0 Asmbld. £35.18.0  
TA-1C Kit ... £6.15.0

All prices include free delivery in the U.K.

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**AMATEUR TRANSMITTER KIT**

**Model DX-100U**

The World's most popular

**Amateur TX Kit**

- Completely self-contained. 150 w. D.C. input.
- Built-in highly stable VFO and all Power Supplies.
- The KT88 high-level anode and screen modulator stage gives over 100 watts of audio from less than 1.5 m.v. input.
- Keying on CW is via the VFO and buffer amplifier cathodes: the other RF valves are biased beyond cut-off.
- Provision has been made for remote control operation.
- Covers all Amateur bands up to 30 Mc/s. 'phone or CW.

Kit ... £79.10.0 Assembled ... £104.15.0

**AMATEUR BANDS RECEIVER KIT**

**Model RA-1**

The ideal economically priced fixed station, portable or mobile receiver covering the Amateur bands from 160-10 m., each band separately calibrated on a large illuminated slide-rule dial. Features: Signal strength meter, tuned RF amplifier stage, half-lattice filter, adjustable noise limiter. Freq. coverage 160, 80, 40, 20, 15, 10 metre bands. I.F. 1620 kc/s.

Kit ... £39.6.6 Assembled ... £52.10.0

**AMERICAN HEATHKIT SINGLE SIDE BAND EQUIPMENT**

For direct delivery from U.S. Plant. Send for details of models. Fully Illustrated American Catalogue of Heathkit range sent for only 1/- post-paid.

**REFLECTED POWER METER KIT**

Model HM-1U. Indicates, reliably but inexpensively, whether the R.F. power output of your transmitter is being transferred efficiently to the radiating antenna.  
Kit ... £8.5.0 Assembled ... £10.10.0

**VARIABLE FREQUENCY OSCILLATOR KIT. Model VF-1U**

Specialy designed to meet the demand for the maximum possible flexibility from an amateur Transmitter which would otherwise be subject to certain limitations imposed by crystal control. Calibrated for all Amateur bands 160-10 metres, fundamentals on 160 and 40 m. Ideal for Heathkit DX-40U and similar transmitters.  
Kit ... £10.17.6 Assembled ... £15.19.6

**Q MULTIPLIER KIT. Model QPM-1**

A reasonably priced Q Amplifier for the amateur and short-wave enthusiast. This self-powered unit (200-250 v. 50/60 c/s.) may be used with communications receivers to provide both additional selectivity and signal rejection.  
Models QPM-1 for 470 kc/s. I.F. QPM-16 for 1.6 Mc/s. I.F. Kit, either model ... £10.14.0  
Assembled ... £12.14.0

By arrangement, with RECORD HOUSING we can now supply you with any one of their large range of fully finished Equipment Cabinets.  
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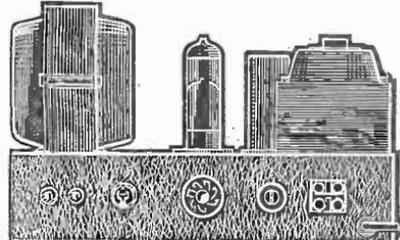


# STERN-GLYNE ELECTRONIC CENTRES

## HI-FI AND TAPE • RADIO • KITS • ELECTRONIC COMPONENTS

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Homebuild Kit form. Either way provides performance per £ unequalled anywhere. If you are working to a budget, kits offer a real saving plus real building satisfaction. Each is absolutely complete and backed by comprehensive, easy-to-follow building instructions.



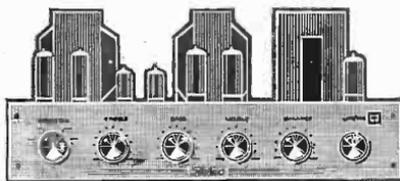
#### FIVE-TEN AMPLIFIER

One of the most famous amplifiers ever made—thousands are in service as the nucleus of high quality installations throughout the world. Match the phenomenal performance demonstrated by any other amplifier obtainable in this price range! Power response 2 db to 20 kHz. Dist. < 1 db. Distortion 0.1%, at full to watts output. Noise—60 db, below 10 watts. Input—over 40 mV for 10 watts. Out. Imp. 8 to 16 ohms. Valves E281, E282, E283, E284, E285. Size overall: 10 x 7 x 4 1/2 in. Incapacitated means

outlet for mono and aux. supply of 250 v, at 45 mA and 4.2 at 21 amps. for pre-amplifier, tuner, etc. To full Mullard specification. Assembled and tested **£13-10-0** Kit **£10-0-0** Add 8/6 carriage.

**FIVE-TEN AMPLIFIER AND TWO-VALVE PRE-AMP.** Assembled and tested **£21-10-0** Add 8/6 carriage. Kit **£15-0-0**

**FIVE-TEN AMPLIFIER AND THREE-VALVE PRE-AMPLIFIER** Assembled and tested **£25-10-0** Add 8/6 carriage. Kit **£21-10-0**



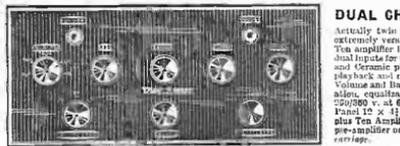
#### TEN PLUS TEN STEREO AMPLIFIER

Basically two Five-Ten amplifiers with extra modifications that enable the reproduction of the Mullard 131,186 Triode, Tri-tone. Add stereo crossovers to a very exciting specification, and the result is superb performance of the highest quality at astonishingly low cost. Power response 8 db to 60 kHz. Dist. < 1 db. Noise 25 mV, for full 10 watts output each channel. Noise—65 db, below 10 watts. Cross talk:

—50 db. Distortion 0.2% at 10 watts. Out. Imp. 8 to 16 ohms from sectionalized zone of special Ultra Linear output transformer. Valves 2 x E280, 4 x E281, E282. Size 14 1/2 x 6 1/2 x 4 1/2 in. Aux. output for rec.-amp. 200 v, at 6 mA, and 6.5 v, at 11 amps. Illustration shows amplifier fitted with Passive Control Unit (see right).

Assembled and tested **£20-0-0**

Add 8/6 carriage. Kit **£16-0-0**



#### DUAL CHANNEL PRE-AMPLIFIER

Actually two Two-Valve Pre-amplifiers which, together provide an extremely versatile and sensitive input arrangement for the Ten Plus Ten amplifier in place of the Passive Control Unit. Features include dual inputs for mono and stereo listening; Variable Rebalance; Crystal and Ceramic pick-ups; dual inputs for direct and pre-amplified tape playback and radio; separate continuously variable Bass, Treble, and Volume and Balance controls. Bucking pre-amp Noise or Stereo operation, equalization conforms to RIAA on line replay. Power input 250/250 v, at 8 mA, and 6.5 v, at 11 amp. Size 11 1/2 x 8 x 4 in. Panel 10 x 4 1/2. Assembled and tested, and supplied complete with Ten Plus Ten Amplifier: **£25-0-0** Kit **£21-0-0** Add 8/6 carriage. Dual channel pre-amplifier only. Assembled and tested **£15-0-0**. Add 5/6 carriage.

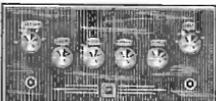


#### TWO-VALVE PRE-AMPLIFIER

Specifically designed for use with the Mullard series of 2, 10 and 20 watt amplifiers but entirely suitable for all Hi-Fi power units not requiring input of more than 100 mV for full output. Features include inputs for crystal and variable reluctance pick-ups with RIAA equalization; three multi-coil selective telephones; and tape replay direct or from pre-amp. Control includes 6-position selector, volume, and with range tap also treble boost valves. Valves E280, size 9 1/2 x 4 1/2 x 2 1/2 in. Panel 10 1/2 x 4 1/2 in. Requires 200 v, at 3 mA, and 6.5 v, at 6 amp.

Assembled and tested **£9-10-0**

Add 8/6 carriage. Kit **£6-6-0**



#### THREE-VALVE PRE-AMPLIFIER

Specifically recommended for use with the 2-10 amplifier, but also suitable for use with all Mullard series mono amplifiers and any high quality unit requiring an input of up to 200 mV for full output. Features include wide range Bass and Treble controls, high and low pass filters, auxiliary input and record output sockets, switched limits for crystal or magnetic pick-ups, radio, tape pick-ups and auxiliary. Power required 200 v, at 3 mA, and 6.5 v, at 11 amp. Valves 2 x E280, and E282. Size 11 1/2 x 4 1/2 x 4 1/2 in. Panel 12 x 4 1/2 in.

Assembled and tested **£13-13-0**

Add 8/6 carriage. Kit **£10-10-0**

#### PASSIVE CONTROL UNIT

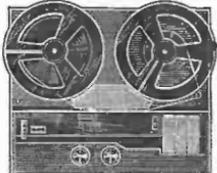
Specifically designed self-contained unit for use with the Ten Plus Ten, either for direct attachment to chassis or for remote fitting. Incorporates switched inputs for crystal or ceramic pick-ups, radio and tape replay, together with Vol., Bass, Treble and Balance controls on an attractively styled and finished front panel. Price, £20 for 10 watts. Imp. 500 K. Size 14 1/2 x 2 1/2 x 2 in. Panel 11 1/2 x 2 1/2 in. For 20 watts or later output pick-ups, use Dual Channel pre-amplifier described below.

Passive Control Unit, assembled and tested and complete with Ten plus **£24-0-0**

Ten Amplifier. Kit **£20-0-0**

Add 10/6 carriage.

#### MAGNAVOX 363 TAPE TRANSPORTER



Manufactured to precise limits that permit recording and tape playback to the highest standard set by the Music Industry.

Simple, reliable design employs a single high-duty motor with heavy flywheel. Features include: fast wind on and rapid rewind, pause control, 3-reel section with tick-tock. Built-in revolutionary indicator, piano key controls. Playing time 21 and 71 1/2 hrs. Worn and flatter E218 on 71 1/2 hrs. Max. speed 18 in. Speeds 18 in. to 120 mm. min. track from 1.000 in. standard tape, size 1 1/2 x 1 1/2 in. plus film, before mounting tape.

With 1 track head, **£10-10-0**

With 3 track heads, **£13-19-6**

Add 10/6 carriage and insurance.

#### TAPE REAMPLIFIER TYPE 'C'



Specially developed by Mullard Laboratories for use with high quality replay systems, and supplied specifically matched for use with the Magnavox 363 tape deck.

Features include: Ferrite-core pot core inductors for treble equalization, push pull oscillator incorporating ferrite-core transformer, adjustable output for matching to existing high-quality amplifier systems; inputs for Mils., Pick-up, Radio, etc. Valves: 5X E280, E282 & E281. Totally enclosed in case. Size 11 1/2 x 6 1/2 x 4 1/2 in. Panel 11 1/2 x 4 1/2 in. Power supply of 200V ac at 65 mA, and 6.5 v at 1.1 A. Is an separate sub-chassis size 6 1/2 x 4 1/2 x 4 1/2 in. High to facilitate remote location. Input terminals: Pre-amp and power pack RK of parts E281. Assembled and tested **£16-10-0**. Add 7/6 carriage.

#### HF/TR3 TAPE AMPLIFIER



Essentially the best complete tape amplifier available to the home builder. Supplied already matched for the Magnavox 363 tape deck.

Features include: switched equalization for all speeds (CTR, standard at 7 1/2 i.p.s.), Treble boost incorporated during Record. Bass boost during playback; speaker output matched for 3, 7.5 and 16 ohms, additional outputs for extension speaker, phone monitoring on VCR and Hi-Fi playback through existing systems; tape for Mils. pick-up and VCR. Radio Valves: E280, E282, E281, E283, E284. Size overall: 11 1/2 x 6 in. (Panel) 11 1/2 x 4 1/2 in. Power pack on separate chassis size 7 1/2 x 3 1/2 in. Amp. Power Pack Kit of Parts: E219. Assembled and tested **£19-0-0**. Add 7/6 carriage.

**CLEAR-OUT OFFERS OF WELL KNOWN HIGH-GRADE EQUIPMENT**

Prices slashed to make way for new stock ranges! Genuine Bargains! Original prices quoted are exactly those at which we have sold previously.



**FAMOUS MULTI-TESTER AT TWO-THIRDS USUAL PRICE**

Size only 12.4 x 4.1 in. deep with ingenious design providing an extra large, easily read scale. Magnificently slanted levered meter movement. Fitted with low loss, long life omnium-colour switch, complete with hook and test leads, battery and full instructions. **Model 1000: P.C.C. 1-3-25-20-250-2500. A.C. 2-10-30-100-500-1000. D.C. Current: 0-20mA, 0-2-5, 200mA. Resistance: 20-1000 Ohms. Cap. 10uF-1000uF and 0-0.01-100uF. Output: 20-10-225V.**

**Was £5.50 NOW £3.10. SAVE 15.15.** Add 2p. p. & p.

**BULK TAPE ERASERS**



There are actually industrialized, high quality versions of the powerful demagnetizers used in instrument and aircraft manufacture and represent the most effective way of restoring recorded or noisy tape to its original unrecorded condition. Essential when using high fidelity recorders in conjunction with high-grade tape: (part for itself over and over in preventing degradation). Bulk erasers can also be used to demagnetize small parts and tools, and for demagnetization purposes, etc. Recommended types include:

**Model 100-120**  
Cleans up to 100 ft. reels of tape in seconds. For 230/250 v. A.C. operation. Size: 4.3 x 4.2 x 2.1 in. black. Finished grey enamel.

**Was £5.50 NOW 67/6 SAVE £1.17.6** Add 4p. post.

**Model 178**  
Extra powerful, professional model. Cleans tape reels in all sizes up to 100 ft. diam. Size 7.1 x 4.1 x 2.1 in. high. Finished grey enamel.

**Was £7.70 NOW £5.15 SAVE £2.7.0** Add 4p. post.



**WESTWELL CT-2B TWEETER**  
Adds sparkle and realism to the performance of almost any high quality reproducer. Nominal 75 ohm. slim, moving coil unit in standard 1/2" transient range with total black grille for mounting in or outside cabinet; alternatively, detachable tweeter can be used. Impedance 16 Ohms. Rating 10 w. max. 3 w. mean. Recommended crossover frequency 4000 cps. Sensitivity 100dB/1W. Size: overall 3.2 x 1 1/2 in. deep.

**Was 27/6 NOW 19/6 SAVE 8/-** Add 2p. p. & p.

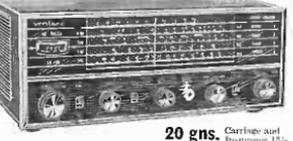
**EXCLUSIVE OFFER OF TOP QUALITY RECORDING TAPE**

New American branded tape by world renowned manufacturers and equal in quality to the best available anywhere. Guaranteed 99.99% free red oxide coating, with full frequency response and uniform output. Resistant to moisture, heat, dust and abrasion. Available in a wide range of acetate and polyester qualities, each individually boxed and endcaped, wrapped in colour coded cartons showing recording times at 7 1/2, 15 and 1 1/2 ips. Also, compare the prices!

Reels available:	Acetate	Polyester
Half types post and packing 1p. per reel. Four or more reels post free.	3 1/2 in. 600ft. Double Play 11/6 7 in. 1200ft. Standard 12/6 1 1/2 in. 1200ft. Double Play 15/- 7 in. 1800ft. Long Play 10/- 3 1/2 in. 1200ft. Long Play 12/6 7 in. 2400ft. Double Play 25/-	3 1/2 in. 600ft. Double Play 11/6 7 in. 1200ft. Standard 12/6 1 1/2 in. 1200ft. Double Play 15/- 7 in. 1800ft. Long Play 10/- 3 1/2 in. 1800ft. Double Play 22/6 7 in. 2400ft. Double Play 25/-

**NEW ADVANCED DESIGN - Veritone Compact Communications Receiver**

New, highly developed, extra-modern compact design. Veritone SR 150 has variable ratio proportions and a DX performance comparable with many high-end receivers. professional reference frequency coverage in continuous form from 440 to 20 Mc. 4 BPFs plus 2nd-order on 440. High frequencies of 3-5, 7, 11 and 22 Mc. Features: variable extra large, clearly defined dial "m" meters, variable pitch BFO, noise blanker, built-in bandpass filter and extending low antenna to receive all but most distant stations.



Extra include phone output jack, standby switch, etc. Size only: 12.1 x 3.6 x 6.0 in. deep. **Veritone SR150: £24.95, £24.95 and 5000 10000 reels. Invaluable for DX, a marine band listener, etc. Also the handily mounted metal case. For 200/250 volts A.C. or D.C. Supply with 125 page "Wireless World Guide to Broadcasting Stations".**

**20 gns.** Carriage and 15/- postage. **121/3.50** deep. **Veritone SR150: £24.95, £24.95 and 5000 10000 reels. Invaluable for DX, a marine band listener, etc. Also the handily mounted metal case. For 200/250 volts A.C. or D.C. Supply with 125 page "Wireless World Guide to Broadcasting Stations".**

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162 Holloway Road, N.7. **NORth 7941**

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**DIVIDAL CROSSOVER NETWORKS**



Superb construction using selected high-grade components, each handily enclosed and constructed in metal case with integral mounting feet. Inputs and speaker outputs are ready to standard screw terminals. Full constructional equipment.

**CV4 Variable Crossover—Standard**  
2-way unit for use with low to medium power woofer and tweeter arrangement. Variable control permits adjustment of bass and treble outputs. In bronze finished case with black plastic panel size 4.2 x 2.1 x 1 1/2 in. high.

**Was £12.6 NOW 12/6 SAVE 10/-** Add 2p. p. & p.

**CV5 Crossover Network—Hi-Fi**  
2-way iron-core choke and filter system offering high frequency crossover at 2500 or 3500 cycles/second. Totally enclosed in bronze finished case size 3.2 x 2.1 x 1 1/2 in. high.

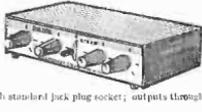
**Was £23.5 NOW 25/- SAVE £1.4.6** Add 2p. p. & p.

**CV6 Variable Crossover—3-way**, medium and high power variable level unit offering mid-range crossover at 2000 cps and tweeter crossover at 3,000 cps. Together with 1" 2" Pad variable level controls for mid-range and tweeter outputs. Matching arrangements also permits use as 2-way crossover, or without level controls when speaker efficiencies are equal. Handily finished in 2-tone grey metal case size 5.2 x 2.2 in. high.

**Was £44.10 NOW 50/- SAVE £2.0.0** Add 3p. p. & p.

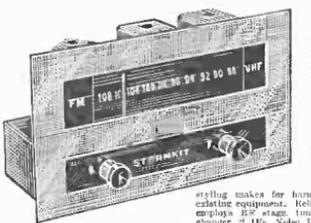
**DIVIDAL SM-5 TRANSISTORISED MONO-STEREO MIXER**

Compact, self-contained 4-channel audio mixer providing 4 separate, identically variable inputs on mono or twin inputs left and right channels on stereo. Separately constructed and handily finished and finished in bronze enamel case size 6.2 x 2 1/2 in. high. Internal PPM battery gives approximately 400 hours operation. Inset suitable for stall, loudspeaker used as mixer, low impedance with trans. radio, etc. Max. input 1.5 v., max. output 2.5 v. gain 18. Input through standard Jack plug socket; outputs through phono plugs.



**Was £31.75 NOW £21.50 SAVE £10.25** Add 3p. p. & p.

**SUPERB NEW STERN-CLYNE**



**F.M.I. VHF TUNER**

Features sparkling performance—phercant stability.

Values are: 4x BPFs plus 2nd-order. Input noise: 100dBV. For 40 dB. Dist. less than 1% at full deflection. Power loss: 200 v. at 20 mA and 100 v. at 1 A. Patent black and silver-grey. Size 8 x 5 in. Chassis: medium plate, overall depth 4 1/2 in.

Specially designed for the Amateur builder, a new, sensitive tuner unit that provides stable, interference-free reception of BBC FM transmissions. High quality output signal ensures optimum performance from all VHF audio systems. Repairs writing tuner for homebrew installation with existing equipment. Includes easily aligned circuit employs 21F stage, tunable-coil, tuned-pull frequency, 2 1/2" VHF Valve Liner & Radio Detector.

**FMI Kit of parts with Instruction Handbook, £7/9/6, carriage 4/-.** **Handbook only 8/-.**  
**FMI Assembled and tested, £10/9/6, carriage 4/-.** **Post free. Despatched on request.**  
**Optional Power Pack Type D Kit of Parts, £2/15/-, carriage 2/6.**  
**Power Pack Type D, assembled and tested, £3/10/-, carriage 3/6.**

**GUARANTEED BY STERN-CLYNE**—Value for money. Quality Facility. Merchandise offered by Stern-Clyne is critically selected and exhaustively tested before it is offered for general sale: where valuable equipment does not exist, certain items are exclusively manufactured to our own strict specifications. In all cases, Stern-Clyne offers the finest and quality selected. Satisfaction guaranteed.

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**PORTABLE OSCILLOSCOPE CT-52**  
A compact general purpose instrument with many unusual features. Size 9in. high, 8in. wide, 16 $\frac{1}{2}$ in. deep. Time base 10 c/s. to 40 Kc/s. Y plate sensitivity 40V per cm. Tube  $\bar{2}3$ in. Frequency compensated amplifier up to 28 dB gain. Bandwidth up to 1 Mc/s. Single sweep facilities. Operates from A.C. mains 100-250 volts c/s. Complete with all test leads, metal transit case, instruction book and circuit diagram. **BRAND NEW**. Tested and guaranteed. £22/10/-, Carr. 10/-

#### MICROAMMETERS

R.C.A. 0-500 microamps, 2 $\frac{1}{2}$ in. circular flash panel mounting. Dials are engraved 0-15, 0-600 volts. As used in the American version of the No. 19 set. 15/-, P. & P. 1/6.

#### AR-88 SPARES

R.C.A. Headphones ..... 12/6  
Eucuthrons (Windows) ..... 8/6  
Knobs. Medium size. Set of 8 ..... 10/-  
Knobs. Large size. Set of 8 ..... 5/6  
Lead Condenser (3 x 4 mfd.) ..... 12/6

#### AR-88D RECEIVERS

A good selection is available for callers at from £30. All are in good condition and are functioning perfectly. Reigned.

**HEAVY DUTY TRANSFORMER**  
Input 220 volts to 250 volts at 50 cycles, tapped every 5 volts. Secondary, 50 volts at 15 amps. Very conservatively rated. Size 7 $\frac{1}{2}$  x 5 $\frac{1}{2}$  x 7 $\frac{1}{2}$ in. Wt. 28 lb. Brand new. £5/19/6. Carr. 7/6

**SILICON RECTIFIER**. 800 P.A.V. The Modern Marvel. 8in. x 2in. Can be used to replace TV. rectifiers up to 500 mA. (40: ballast resistor). 7/-

#### IS-175 HETERODYNE FREQUENCY METER

A high frequency version of the well known IS-221. Accuracy 0.05%. Frequency range 80 to 1,000 Mc/s. As new condition with original calibration book. Tested and guaranteed. £75.

#### BC221 FREQUENCY METER

155 Kc/s to 20 Mc/s. This crystal controlled heterodyne frequency meter is too well known to need further description. Those who offer are complete with correct individual calibration book and are carefully tested and guaranteed. New condition. Carr. 10/-

Laboratory Standard

**OSCILLOSCOPE**  
A 12in. demonstration oscilloscope with all controls at rear. **BRAND NEW** £80.



**SANGAMO WESTON VOLTMETERS**  
561 Dual range 0-5 and 0-100 v. D.C. FSD 1 mA. 3in. scale. Recent manufacture. Ideal for schools. Complete in super quality canvas carrying case, with test probes and leads. **BRAND NEW**. Boxed 37/6. Post 2/6.

**STANDARD SIGNAL GENERATOR**  
**MARCONI TF-144G** Carr. 30/- **£25**  
Overhauled, guaranteed accurate and in perfect working order. Complete with mains lead and technical manual.

**SIGNAL GENERATOR CT-218 (FM/AM)**  
**MARCONI TF 937**. Covers 85 Kc/s to 30 Mc/s in 8 switched ranges. Effective length of film scale is 50ft. Output level variable in 1 dB steps from 1 $\mu$ V to 100 mV (75dB). Also IV Outputs down to 0.1 $\mu$ V from an outlet at 7.5dB. Int. mod. at 400 c/s. 1 Kc/s, 1.6 Kc/s and 3 Kc/s. FM at frequencies above 394 Kc/s. Variable mod. depth and deviation. Crystal calibrated 200 Kc/s and 2 Mc/s. Monitor speaker for beat detection. Fully metered, blower cooled, Panclimatic. A.C. mains 100 to 150 and 200 to 250 volts, 45 to 100 c/s. 17 x 20 $\frac{1}{2}$  x 7 $\frac{1}{2}$ in. Weight 117 lbs. Fully tested and guaranteed. Under 10% of original price. £65. Carr. 50/-

**CINTEL EQUIPMENT**  
**ELECTROLYTIC CAPACITANCE AND INCREMENTAL INDUCTANCE BRIDGE**. No. 36601  
A modern instrument, all solid state, which accurately measures the capacity of electrolytic condensers from 0.1 $\mu$ F to 1,000 $\mu$ F under operating conditions. Leakage current and polarizing voltage are separately metered. Inductances from 100 mH to 100 H can also be measured with currents up to 100 mA. A.C. mains operation. Unused with handbook. £100.  
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A matching instrument to the above. All solid state. Mains operation. Measures from 0.002 $\mu$ F to 100 $\mu$ F. Unused with handbook. £100.

**V.H.F. SIGNAL GENERATOR**  
**MARCONI TF-801A**. Covers 10 to 300 Mc/s (4 bands). Directly calibrated. Int. Mod. at 400, 1,000 and 5,000 c/s. Accutuned or force output. Guaranteed overhauled, accurate and in perfect working order. £32/10/-, Carr. £1.

**AN/USM-44A**. A precision signal generator. U.S.A. manufacture. A.F. only. 10 to 420 Mc/s (5 bands). Directly calibrated. An instrument of the highest possible quality with 1 Mc/s and 5 Mc/s. Xtal calibrators. Separate "see carrier" and "set mod" meters. Output cont. variable from 0.1 $\mu$ V to 350 mV. **BRAND NEW**. £150.

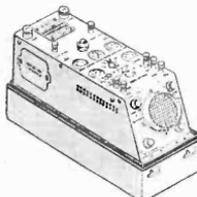
**DISTORTION FACTOR METER**  
**MARCONI TF-142E**. This instrument measures the percentage of total harmonic distortion in the fundamental frequency range 10 to 8,000 c/s. The lowest scale engraving is 0.5%. Will handle 2 watts (continuous) and will give satisfactory readings with only 1mW input. Mains operated. Output impedance 600 ohms. Very good condition. £30. Carr. £1.

**MINIATURE RELAYS**. 240 v. A.C. coils. Contact assembly "2" makes" and 1 C.O. 3 amps. Size 2 x 1 $\frac{1}{2}$  x 1in. Unused and removed from brand new equipment. 8/6 post paid.

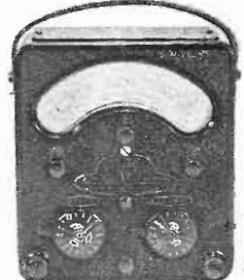
**B. & R. RELAYS Type CO3**. 230 volt A.C. coils. Very heavy duty contact assembly. Size 4in. x 3 $\frac{1}{2}$ in. x 2 $\frac{1}{2}$ in. Weight 2 1/2 lb. **BRAND NEW**. 27/6. P. & P. 2/6.

#### HICKOCK OSCILLOSCOPE OS-8B/1J

A high grade general purpose instrument made to excelling U.S.A. Navy specification. Detachable cover with carrying handle. Compact (13 $\frac{1}{2}$  x 6 x 8 $\frac{1}{2}$ in.), weight 17 $\frac{1}{2}$  lbs. Green and black finish. 3in. tube. Bandwidth "Y" amplifier D.C. to 2 Mc/s (D.C. coupled). Sensitivity 40 mV/cm. 500 $\mu$  amp. can be used separately, similar spec to 500 $\mu$  amp. Leads are housed in case. For A.C. mains 105 to 125 v. 50 to 1,000 c/s. **BRAND NEW**, tested and guaranteed. £25. Carr. 10/-  
Auto transformer 15/6 extra.



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Complete with leather carrying case, leads and batteries ready for use. Fully guaranteed. £13/13/-, Post 7/-

#### PHASE MONITOR ME-43/U

**(AN/URM-47)**  
Designed to measure directly the phase angle between two applied single frequency signals of from 20 to 20,000 c.p.s. 1. Direct indication on a panel meter. Input can be sinusoidal or non-sinusoidal from 2 to 30 volts peak. Of recent manufacture (1957) by Control Electronics Inc. and ex-U.S.A. Air Force. In first class condition with handbook. A complex instrument worth 19 valvies. £40. Carr. 30/-

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Those who offer are the modern Mark 3 version and are in really first class condition. Please do not confuse these with older well used instruments. One which will convince you they are a bargain at £45. Carr. 30/-

**T.C.C. VISCONAL CONDENSERS**. 8 mfd. 800 v. D.C. wkg. at 71°C. CP 152 v. Size 3 x 1 $\frac{1}{2}$  x 5in. high. **BRAND NEW** (boxed), 8/6 each. **DUBILIER NITROGL**. 8 mfd. 350 v. D.C. wkg. at 71°C. Size 1 $\frac{1}{2}$  x 1 $\frac{1}{2}$  x 4 $\frac{1}{2}$ in. high. With four clips. **BRAND NEW** (boxed), 8/- each. **T.C.C. or DUBILIER**. 4 mfd. 600 v. wkg. CP 130T or similar. 1 $\frac{1}{2}$  x 1 $\frac{1}{2}$  x 4 $\frac{1}{2}$ in. high. **BRAND NEW** (boxed), 4/6 each. All post paid.

#### STANDARD TRANSFORMERS

Vacuum impregnated, interleaved, E.S. screen, universal mounting. Size 4 $\frac{1}{2}$  x 3 $\frac{1}{2}$  x 2 $\frac{1}{2}$ in. All **BRAND NEW**. 21/- each. Post 2/6.  
Type 1. 250-0-250 v. 80 mA. 6.3 v. 3 a. tapped at 4 v. 4 a. 6.3 v. 1 a. tapped at 4 v. and 5 v. 2 a.  
Type 2. As above but 350-0-350 v. 80 mA.  
Type 3. 30 v. 2 a. tapped at 12, 15, 20 and 24 v. to give 3-4-5-6-9-10 "a", etc.  
Type 5. 0.6-9-15 v. 4a. Ideal for chargers.



**LOW CAPACITANCE BRIDGE**  
**MARCONI TF 1342**. Range 0.002 pF. to 1,111 pF. Accuracy 0.2%. Three terminal transformer ratio arm bridge allows "in situ" measurements. Internal oscillator frequency 1,000 c/s. 12 x 17 x 8 $\frac{1}{2}$ in. Weight 2 $\frac{1}{2}$  lbs. A.C. m. m. 200 to 250 and 100 to 150 v. 40-100 c/s. With leads and handbook **ABSOLUTELY BRAND NEW**. £45.



# R.S.C. SUPER 15 HI-FI AMPLIFIER R.S.C. SUPER 30 STEREO AMPLIFIER

- FULLY TRANSISTORISED**
- \* 200-250w. A.C. Mains Operation.
  - \* **OUTPUT R.M.S. CURRENT** 100 WATTS into 8 ohms.
  - 16 WATTS into 3 ohms.
  - \* Max. Instantaneous Peak Power Output 28 watts.
  - \* **PRINTED CIRCUIT CONSTRUCTION**
  - \* **LATEST MULLARD TRANSISTORS** (A101, AD114, OC81, OC82, OC4, OC4A, OC81A, OC41, AC107 (Total of nine))
  - \* **5-POSITION INPUT SELECTOR SWITCH** Equalization to Standard I.C.S.A. and C.C.I.R. Characteristics for Gram and Tape Heads
  - \* **FULL TAPE MONITORING FACILITIES**
  - \* **SENSITIVITIES:** Magnetic P.U. 4 m.v. Crystal or Ceramic P.U. 100 m.v. (Radio) A.C. or Ceramic P.U. 110 m.v.
  - \* **FREQUENCY RESPONSE:** 20-20,000 c.p.s.  $\pm 2$  db. **TONE CONTROL:**  $\pm 12$  db. to  $\pm 14$  db. at 10 kc/s.
  - \* **BASS CONTROL:**  $\pm 12$  db. to  $\pm 15$  db. at 50 c.p.s.
  - \* **HARMONIC DISTORTION AT 10 WATTS R.M.S., 1,000 c.p.s. 0.35 %**
  - \* **HUM LEVEL:**  $-73$  db.
  - \* **NEGATIVE FEEDBACK 92 db.**

INTRODUCING TWO COMPLETELY NEW UNITS WITH TECHNICAL SPECIFICATIONS MORE THAN FAVOURABLY WITH SIMILAR AMPLIFIERS OFFERED AT 2-3 TIMES THE COST.

**IMPORTANT Note.** Rated output figures are given in R.M.S. and not speech and music or I.H.F.M. otherwise we could obviously quote much higher outputs.



Complete Kit of parts with full constructional details and point-to-point wiring diagrams. **1 Car. 10/-**

**9 1/2 Gns.**

If preferred printed circuit can be supplied with parts soldered and tested for **2 Gns. extra.** Terms for point 8 car. 5 g. only, plus postage. **Set of 200-250W. Hi-Fi** Walnut Case, 12 months guarantee and fitted cover mentioned above. **19/- and 8 monthly payments 13/2 (Total £61/7).** Kit equally assembleable ready for use. **Setted cover 12 months guarantee.** **Car. 10/- 29 Gns.**

## A DUAL CHANNEL VERSION OF THE SUPER 15 Employing Twin Printed Circuits

- \* Close Tolerance Gauged Pots
- \* Matched Components
- \* CROSSLINK  $\pm 52$  db. at 1,000 c.p.s.
- \* CONTROLS: 5-Position Input Selector, Bass Control, Treble Control, Volume Control, Balance Control, Stereo Mono Switch, Tape Monitor Switch, Mains Switch.
- \* INPUT SOCKETS (Matched Pairs.) (1) Magnetic (2) Ceramic or Crystal P.U. (3) Radio A.U. (4) Head Microphone
- \* Operation of the Input Selector Switch assures appropriate equalization.
- \* **REED 18 g.w. Chassis.** Size approx. 12in. wide, 6in. high and 8in. deep.
- \* Attractive Face Plate and Matching Knobs.
- \* NEON PANEL INDICATOR

Above facilities are, except for Gauging and Balance Control, apply also to Super 15. ALL COMPONENTS ETC. ARE OF A HIGH STANDARD AND SUPPLIED BY LEADING BRITISH MANUFACTURERS. THESE UNITS ARE ESSENTIALLY SUITABLE FOR USE WITH ANY MAKE OF PRECISION MICROPHONE (Crystal, Ceramic, Magnetic, Moving Coil, Ribbon, HEADPHONE OR THE COST. SUPPLYING COST OF THE CABLES TO THE SUPPLIER'S OFFICE USING WITH PHONO TAPES AUXILIARY EQUIPMENT.

## Audioline High Fidelity Speaker Systems

Designed to provide a smooth frequency response from 40-20,000 c.p.s. consisting of 12in. 12,000 line 16 ohm speaker, Crossover Unit and Tweeter. Highly recommended for use with any High Fidelity Amplifier. **10 Watt Unit.** Impedance 16 ohms or 16 ohm/16 ohm. **54/19/9.** Price includes postage of 10/10 (Total **£5 12/6**) 20 Watt Unit **£59/9** Car. 10/- (Total **£71/6**). 21" and size mentioned in details of 12" (Total **£71/6**).

**W.B. 'STENTORIAN' HIGH FIDELITY P.M. SPEAKERS.** 110/12 10 watt rating. Where a really good quality speaker at low price is required we highly recommend this unit with an amazing performance. **£42/9/6.** Please state whether 3 ohm or 16 ohm required.

**19 1/2 Gns.** Car. 12/6. Or Deposit **£3 2/0** and nine monthly payments of 49/8. (Total **£23/8/-**).

**15 WATT HI-FI SPEAKER**

Very compact construction box. 2in. Diameter VOICE COIL. Mini Cone. plastic treated surround. smooth frequency response 20-20,000 c.p.s. Speech Coil 3 ohm or 16 ohm. **£5/15/0**

Exceptional value at

## AUDIOTRINE HIGH FIDELITY LOUDSPEAKER ENCLOSURES

All types are of pleasing modern 'slimline' (single cylindrical) lined and in alternative finishes (1 light or medium walnut).

**SE8** Designed for optimum performance with any Hi-Fi speaker. Size 22in. high, 12in. wide. **Deposit 18/- and 9 monthly payments 12/3 (Total £50/3).** Car. 7/6. **£5/15/6**

**SE10** For 10in. High Fidelity Speaker with provision for tweeter. Especially recommended for use with Audioline HI-FIDIO speaker. Size 24in. high, 13in. wide, 6 1/2in. deep. **Deposit 21/- and 9 monthly payments 12/6 (Total £71/6/-).**

**SE12** For outstanding performance with any 12in. Hi-Fi speaker but especially suitable for types with low fundamental resonance. A tweeter cut out is provided. Size 24in. high, 13in. deep. **Deposit 27/- and 9 monthly payments 17/10 (Total £9/7/6).** Car. 10/6.

## INTRODUCING A NEW RANGE OF HIGH FIDELITY LOUDSPEAKER UNITS

**AUDIOTRINE 'PETITE'**

Size only 10 1/2in. x 6 1/2in. x 7 1/2in. Rating 8 watts. Frequency range 40-20,000 c.p.s. Cabinet beautifully finished in Teak (light) or Walnut (medium). Fitted specially designed heavy cast iron speaker with large pole pieces extra long voice coil and rubber surround. Impedance 3 ohms or 16 ohms. **8 Gns. Car. 7/6.** Or Deposit 27/- and 9 monthly payments 17/10 (Total **£9/7/6**).

**The AUDIOTRINE 'MINI-TEN'** Size only 12 1/2in. high, 6 1/2in. wide, 8 1/2in. deep. Rating 10 watts. Impedance 15 ohms. De luxe Teak or Walnut cabinet. Fully recommended for use with heavy cast iron. Bass speaker with extra high flux density ceramic magnet and rubber surround. Low fundamental resonance. Crossover Capacity Cross-over and Tweeter. Really outstanding performance. Frequency range 40-20,000 c.p.s. **Deposit £2 and 9 monthly payments 27/8 (Total £14/8/-).** **12 Gns. Car. 8/6.**

## AUDIOTRINE CORNER CONSOLE CABINETS

Strenuously used. Beautiful polished walnut veneered finish. Pleasing design.

**JUNIOR MODEL:** To take up to 8in. speaker. Size corner 20in. x 11in. x 11in. **£45/9.**

**STANDARD MODEL:** To take up to 10in. speaker. Size 27in. x 18in. x 12in. **£59/9.**

**SENIOR MODELS:** To take up to 12in. speaker and with Tweeter cut-out. Size 30in. x 21in. x 12in. (Recessed) for use with Audioline speaker systems. **8 Gns. Car. 7/6.** or more.

**The 'GLOUSETER'** Handsome 'slimline' cabinet. Acoustically lined. Size 24in. high, 20in. wide, 6 1/2in. deep. Finished light teak or medium walnut. 12in. high flux 12,000 line speaker. Cross-over unit, and Tweeter. Rating 10 watts. Smooth response 40-20,000 c.p.s. Impedance 16 ohms. **Deposit 26/- and 9 monthly payments 24/8 (Total £19/1/6).** Car. 10/6. **11 Gns.**

**The 'BRONTE'** Handsome cabinet of modern styling. Acoustically lined and finished Teak or Walnut. Size 32in. high, 18in. wide, 7 1/2in. deep. Fitted Wharfedale Super 8 N5DD speaker, with Koll surround and dual cone. Rating 15 watts. Impedance 15 ohms. **Or Deposit 39/- and 9 monthly payments 12 Gns. 26/10. (Total £14/-6).** Car. 15/6.

**The 'STANWAY'** Attractive contemporary style cabinet finished Teak (light) or Walnut (medium). Acoustically lined. Size 24in. high, 20in. wide, 8 1/2in. deep. Fitted 12in. high flux Bass speaker with plastic treated surround giving extremely low fundamental resonance and high sensitivity. The smooth frequency response 20-20,000 c.p.s. is achieved by addition of high flux tweeter and choke capacity cross-over system. Rating 20 watts. Impedance 15 ohms. **Deposit 3 Gns. and 12 monthly payments 32/8 (Total £22/13/-).** **19 1/2 Gns. Car. 7/6.**

## R.S.C. JUNIOR BASS REFLEX CABINET

Designed for above speaker, but suitable for any good quality 8in. or 10in. speaker. Acoustically lined and ported. Medium volume vents. Size 24in. x 12in. x 16in. Strongly made. Handmade in Britain. Superb reproduction for only **£27/6.** **Deposit 14/6 and 9 monthly payments 10/4 (Total £57/6).**

## R.S.C. 15 AND 20 WATT AMPLIFIER WITH INTEGRAL PRE-AMP AND TONE CONTROL

Fully Transistorised Orthodox Circuitry. Maximum Output 20 watts R.M.S. (28 watts music rating). Sensitivity 9 millivolts for full output. Frequency Response  $\pm 1$  db. 20-20,000 c.p.s. Harmonic Distortion 0.1% measured at 1,000 c.p.s. Bass Control  $\pm 8$  db. to  $\pm 14$  db. at 40 c.p.s. Treble Control  $\pm 9$  db. to  $\pm 15$  db. at 10 kc/s. Extremely high signal to noise ratio. Kit of parts consisting of printed circuit, all required resistors, condensers and transistors and 12in. S.H. Full diagrams and instructions. **£6/19/9** Or with printed circuit fully wired and tested extra. **£8/19/9** Post 2/6. Power pack available for 39/6 in kit form or 59/6 ready for use.

**Full Output without thermal run-away.** Suitable for 5, 7, 7 1/2, 10 ohm speakers. Great for inputs of any impedance. For Hi-Fi in the home or public address.

## LATEST MAGNVOX 363 TAPE DECKS

7 speeds 1 1/2, 3 1/2, 7 1/2 in. per sec. A robust high quality Deck with built-in fully recording heads. Includes: Digital Counter, pause control, Heavy 4 pole fully screened output, Record Interlock to prevent accidental erasure, Auto Stop. For 200-250 W. A.C. mains. **10 Gns.** **Model Car. 7/6**

**Four Track £13/9/6** **Model Car. 7/6**

**Texas on 4 Track Model only Deposit 47/9, and 9 monthly payments 28/11 (Total £154/8/-)**

## R.S.C. 4 WATT GRAM. AMPLIFIER KIT

Complete set of parts to build a good quality compact unit suitable for use with any record playing unit. Means for use with separate Hi-Fi and Treble controls. Output for 2-4 ohm speaker. For 200-250 W. A.C. **59/9**

## SPECIAL TAPE RECORDING OFFER

Very limited number of Linear LT45 high quality Tape Amplifiers, retail price 12 Gns. Magnetic Echo Record level indicator. Output for 3in. and 7 1/2in. per sec. Supplied with latest Magnavox 363 7 1/2 in. tape deck for only **£19/9/6**. Car. 10/6. Both units fully guaranteed. **19 Gns. 15/-**

WW-145 FOR FURTHER DETAILS.

# IMMEDIATE DESPATCH

## FULL SPARES AND SERVICE AVAILABLE

### CONSTANT VOLTAGE TRANSFORMER



★ **CORRECTED WAVE**  
Modern design in 2-tone grey hammer steel case with handle. Complete with lead and plug.

#### 1,000 WATT MODEL

Input 240 v. A.C.  $\pm 20\%$ . Output accuracy  $\pm 1\%$ . Fitted signal lamp and switch. **£29.10** Carr. and pkg. 25/-

### AUTOMATIC MAINS STABILIZER

Maintain "spot-on" test gear readings at all times.  
★ No Moving Parts ★ No Maintenance ★ No Attention.

Specification  
★ Input: 240 v. A.C.  $\pm 20\%$ —50 cycles  
★ Output: 240 v. A.C.  $\pm 1\%$   
★ Accuracy:  $\pm 1\%$   
★ Capacity: 250 watts.  
★ Size: 11 x 6 1/2 x 6 in. high.  
★ Weight: 21 lbs. Fitted signal lamp and switch.  
**£11.10** Carr. & Pkg. 20/-

## VARIABLE VOLTAGE TRANSFORMERS

WORLD FAMOUS "SLIDE-TRANS" AVAILABLE ONLY FROM I.M.O.

★ RATED CURRENT CONSISTENT AT ALL POINTS ALONG THE WINDING



Output: 0-260 v. Input: 230 v. A.C. 50/60+. Shrouded fully variable transformers for bench or panel mounting.



1 Amp. **£4.10.0**  
2.5 Amp. **£5.17.6**  
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20 Amp. **£32.10.0**

Carr. & Pkg. extra.

Inset shows latest type brush Gear providing 1 volt variation.

### PORTABLE TRANSISTOR TESTER



#### SPECIFICATION.

Alpha 0.7 to 0.997  
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I.C.O. 0-50uA. 5mA.  
Capable of measuring GERMANIUM AND SILICON DIODES.  
DESIGNED WITH RESISTANCE SCALE 200 ohms to 1 Megohm as an ADDED FEATURE.  
Housed in heavy duty plastic case, c/w internal battery. Only **£7/7/-**

Plus 5/- P. & P.

### TRANSISTORISED MEGOHMMETER



★ NO WINDING  
★ PUSH BUTTON TO READ  
USE 1966 EQUIPMENT

500V-1,000 MEGOHMS  
Superb portable instrument. Supplied c/w batteries, probes and carrying case.  
**ONLY £23.10.0**

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### PORTABLE VARIABLE A.C. POWER SUPPLY UNIT

Designed for engineers whose requirements call for a visual indication of volts applied.

OUTPUT:  
0-260 v. 1 1/2 amps.

INPUT:  
230V. A.C. 50/60-. Fitted with fuse, voltmeter, safety indicator, on-off switch and lead. Size: 8x5x5 1/2 in. high.



PRICE **£8.10.0** Carr. & Pkg. 10/-.

### AC/DC VALVE VOLTMETER



Price **£35.0.0**  
C/W probes and leads—no extras. LOOK AT THIS SPECIFICATION:  
★ 11 megohms per volt.  
★ 5 mV-1,500 V A.C.  
★ 100 mV-1,500 V D.C.  
★ 0.1 ohm-1,000 Megohms. PLUS ★ 1 Kc Oscillator Test Source

★ Complete with Test Probe with BUILT-IN A.C./D.C. switch, no fumbling or fiddling with out-of-reach knobs.  
Light grey crackle steel case with satin alloy front. Mains operated.  
Size and weight: 5 1/2 x 3 x 8 in. high, 5 1/2 lb.

### VARIABLE HIGH-VOLTAGE UNIT

DI-ELECTRIC BREAKDOWN TESTER  
★ Range: Infinitely variable up to 3,000 volts and can be accurately set. 0.1 amp.  
★ Entirely suitable for continuous testing.  
★ Built-in Automatic safety cut-out meter.  
Input: Mains voltage.  
Robustly constructed for bench use. Complete with input and test leads with clips. Model T30, 0-3,000 v. A.C. **£32**

### WALKIE TALKIE '88' SET

Made by M. Cole & Co. This Transmitter/Receiver weighs only 5 1/2 lb. (approx.) and measures 3 1/2 x 5 1/2 x 9 1/2 in. A crystal controlled 4 frequency set operates from standard dry battery—H.T.T. (i.e. Vidor LS537), 14 current series BTG valves used.  
As supplied by us to Overseas Govt. Depts. Supplied complete with valves and crystals. Details & Prices of all Accessories enquired on request. **ONLY £10 each**

### 20 Amp. L.T. SUPPLY UNIT



Plus 40/- Carr. & Pkg. G.B. (Inland) **£29.10.0**

BUY DIRECT FROM MANUFACTURER

### 5 AMP. A.C. & D.C. VARIABLE SUPPLY UNIT



Specification:  
Output: 0-260 V A.C. 0-240 V D.C.  
★ Smooth stepless voltage variation from 0-Max.  
★ Current consistent throughout the controlled range.

★ Ammeter and voltmeter fitted, and Neon indicator.  
★ Fully fused input and output.  
Strong steel case with carrying handle and rubber feet. 11 in. x 7 in. x 1 1/2 in. high. MADE IN ENGLAND  
PRICE **£30.0.0** Carr. & pkg. 40/- (Gt. Britain/Inland)

## 36ft. AERIAL MASTS

### NEW LATEST PATTERN TUBULAR MASTS

Check these vital points:

- ★ Made from 6 x 1 1/2 in. dia. Sherardized steel sections, for durability and strength.
- ★ Extra strong loading base.
- ★ Top cap with fitted pulley and halyard.
- ★ 2 sets (8) Rotproof Guys.
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**ONLY £13.10.0** ex works  
Carr. 17/6. Returnable wooden case 20/-.



### 30 Amp. L.T. SUPPLY UNIT

0 to 18V. D.C. WITH SMOOTH STEPLESS VARIATION.

Designed for CONTINUOUS use at max. loading:

- ★ Fitted voltmeter and ammeter.
- ★ Input and output fully protected.
- ★ Input: Mains A.C. robust construction.
- ★ 2 tone grey hammer finish. Steel case.

**£49.10.0** Carr. & Pkg. 40/- G.B. (Inland)  
Entirely suitable for plating plants, laboratory supplies, etc.

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### 7 VALVE AM/FM RADIO GRAM CHASSIS

Valve line-up: ECC85, ECH81  
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Three Wavelength and Switched Gram positions. Min. 200-500 cm. Long 1,000-20,000 cm. VHF/FM 88-108 Mc. Philips personality tuning range. Full range equalizer. 450 W. 100 VA transformers. Latest circuitry including AFD and Meg. Feedback. Three watt output. Sensitivity and reproduction of very high standard. Choice of 101 or 410. High fidelity. 7 1/2" Edge illuminated glass dial 11 1/2" x 20". Vertical scale. Horizontal station names. Gold on brass background. A.C. 200-250 V. operation. Maclogene coating. Great listening ease available.

**Aligned and tested ready for use \$13. 19. 6**

Complete with Tube Off Socket, set, apr. and P/U Sockets 4 Kinds - without or heavy to choice and In-hub P/U serial 318 extra.

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Complete with Tube Off Socket, set, apr. and P/U Sockets 4 Kinds - without or heavy to choice and In-hub P/U serial 318 extra.

### CO-AX 80 ohm CABLE

Highgrade low loss Cellular Air Spind Polythene - 1/4 in. diam. Standard Coax.

BARBAIN PRICES - SPECIAL LENGTHS

50 yds. 3/8"	1.60	1.75	1.90
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200 yds. 3/8"	6.20	7.00	7.60
300 yds. 3/8"	9.30	10.50	11.40
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500 yds. 3/8"	15.50	17.50	19.00
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700 yds. 3/8"	21.70	24.50	26.60
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3168; 3185; 3202; 3219; 3236; 3251; 3268; 3285; 3302; 3319; 3336; 3351; 3368; 3385; 3402; 3419; 3436; 3451; 3468; 3485; 3502; 3519; 3536; 3551; 3568; 3585; 3602; 3619; 3636; 3651; 3668; 3685; 3702; 3719; 3736; 3751; 3768; 3785; 3802; 3819; 3836; 3851; 3868; 3885; 3902; 3919; 3936; 3951; 3968; 3985; 4002; 4019; 4036; 4051; 4068; 4085; 4102; 4119; 4136; 4151; 4168; 4185; 4202; 4219; 4236; 4251; 4268; 4285; 4302; 4319; 4336; 4351; 4368; 4385; 4402; 4419; 4436; 4451; 4468; 4485; 4502; 4519; 4536; 4551; 4568; 4585; 4602; 4619; 4636; 4651; 4668; 4685; 4702; 4719; 4736; 4751; 4768; 4785; 4802; 4819; 4836; 4851; 4868; 4885; 4902; 4919; 4936; 4951; 4968; 4985; 5002; 5019; 5036; 5051; 5068; 5085; 5102; 5119; 5136; 5151; 5168; 5185; 5202; 5219; 5236; 5251; 5268; 5285; 5302; 5319; 5336; 5351; 5368; 5385; 5402; 5419; 5436; 5451; 5468; 5485; 5502; 5519; 5536; 5551; 5568; 5585; 5602; 5619; 5636; 5651; 5668; 5685; 5702; 5719; 5736; 5751; 5768; 5785; 5802; 5819; 5836; 5851; 5868; 5885; 5902; 5919; 5936; 5951; 5968; 5985; 6002; 6019; 6036; 6051; 6068; 6085; 6102; 6119; 6136; 6151; 6168; 6185; 6202; 6219; 6236; 6251; 6268; 6285; 6302; 6319; 6336; 6351; 6368; 6385; 6402; 6419; 6436; 6451; 6468; 6485; 6502; 6519; 6536; 6551; 6568; 6585; 6602; 6619; 6636; 6651; 6668; 6685; 6702; 6719; 6736; 6751; 6768; 6785; 6802; 6819; 6836; 6851; 6868; 6885; 6902; 6919; 6936; 6951; 6968; 6985; 7002; 7019; 7036; 7051; 7068; 7085; 7102; 7119; 7136; 7151; 7168; 7185; 7202; 7219; 7236; 7251; 7268; 7285; 7302; 7319; 7336; 7351; 7368; 7385; 7402; 7419; 7436; 7451; 7468; 7485; 7502; 7519; 7536; 7551; 7568; 7585; 7602; 7619; 7636; 7651; 7668; 7685; 7702; 7719; 7736; 7751; 7768; 7785; 7802; 7819; 7836; 7851; 7868; 7885; 7902; 7919; 7936; 7951; 7968; 7985; 8002; 8019; 8036; 8051; 8068; 8085; 8102; 8119; 8136; 8151; 8168; 8185; 8202; 8219; 8236; 8251; 8268; 8285; 8302; 8319; 8336; 8351; 8368; 8385; 8402; 8419; 8436; 8451; 8468; 8485; 8502; 8519; 8536; 8551; 8568; 8585; 8602; 8619; 8636; 8651; 8668; 8685; 8702; 8719; 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All Primaries Tapped 200-250V. Pri. sec. 350-350 250mA 6.3V 4A. 6.3V 4A. 6.3V 3A. 5V. 4A. 59/6. P.P. 6/-. 350-350V. 180mA. 6.3V. 4A. 6.3V. 3A. 5V. 3A. P.P. 5/-. Pri. 130V. C core. 450 mA. 3 cycles, 45/-. P.P. 5/-.  
**SIEMENS MINIATURE RELAYS** Plug-in type, 9,000G 6 makes, 16,000G 6 makes, 5,000G 4 CO. Complete with base, all at 8/6c. 1/6 P.P. Magnetics devices. Size 1 x 2 x 1/2in. 2000C 2 c/o contacts, 10/6. P.P. 1/-.  
**AMERICAN MINIATURE LEAD AC** Set of four, one 6V. 1.2 A.H. and three 36V. 0.2 AH supplied brand new in sealed metal container, size 3 1/2 x 1 1/2 in. Weight 5 oz. Fully fitted with hypodermic syringe, 12/6 set plus 2 1/2 p.p. P.P. 6/-. Battery separately, 7/6. P.P. 1/6. Hypodermic syringe with needle, 5/6. P.P. 1/6. Sold separately if required.

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A.C. input 200-240 v. D.C. output 50 volts 8 amps. Built in metal case. Size 15 x 6 x 6 in. Fitted with on/off switch, panel fuse, and output socket, £9/19/6. Carr. 10/-.

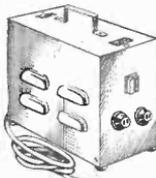
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A.C. input tapped 110-220-230 v. D.C. output 24 volts 1.5 amps. 2.25 amps. with case cover removed. Choke and condenser smoothed. Fitted on/off switch and fuses. Built in metal case. Size 15x9x9in. Supplied new and guaranteed. £3/17/6. Carr. 10/-.

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## AUTO TRANSFORMERS



American sockets or terminal blocks. Please state which type required.

Wattage	Price	Carr.
5,000	£4 19 6	6/6
300	£2 9 6	5/6
150	£1 19 6	5/6
80	£1 6 6	5/6

## G.P.O. HIGH SPEED COUNTERS

Latest Design Type 1000 A. H. 300 cycles. 150, P.P. 1/6.  
Type 100. 110 v. 200 watts. By famous makers. Guaranteed. 45/-. Carr. 5/-.  
**A.C. ELECTRIC CHECK METERS** 120-240 v. 40 amps. by Sangamo Weston Ltd. in perfect condition, 35/-. P.P. 4/-. Chamberlain & Hookham Ltd. 25 amp. 27/6. P.P. 4/-.  
**PAINTON PRECISION POTENTIAL METERS.** Completely screened. Dia. 3 1/2in. Standard 1in. dial spindle. 50/1 or 1.1k/1. 10/6. P.P. 2/6.  
**AMERICAN MINIATURE LEAD AC** Set of four, one 6V. 1.2 A.H. and three 36V. 0.2 AH supplied brand new in sealed metal container, size 3 1/2 x 1 1/2 in. Weight 5 oz. Fully fitted with hypodermic syringe, 12/6 set plus 2 1/2 p.p. P.P. 6/-. Battery separately, 7/6. P.P. 1/6. Hypodermic syringe with needle, 5/6. P.P. 1/6. Sold separately if required.

**TS 36A1 POWER METER**, with accessories, used for checking radar outputs, £5 each, 10/- carr.

**DE-ICER, Controller Mk. 3**. Contains 10 relays D.P. changeover heavy duty contacts, 1 relay 4f, C.O. (235 ohm coil). Stud switch 30-way relay operated, 24 v. D.C., timing motor with Chronometric governor 20-30 volts 12 R.P.M.; geared to 30-way stud switches and two Ledex solenoids, 1 delay relay, etc., sealed in steel case, size 4 1/2 x 7 1/2 in., £3 each, post 5/-

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28 v. 150 r.p.m., 25/-, post 2/6.  
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**VOLTMETERS VT-28-B-1**,

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150 volts. Fitted with probe

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230 v. minus input, post 5/-.

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**T.C.S. MODULATION**

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ohm. 25/- each, post 3/6.

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Sec., 125,000 ohm. 10/- each,

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three H.F.O. outputs for operation of diversity receivers where fixed

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supplies 100/220 v. A.C., 50/60 cps, £30 each, car. 30/-, Wt. 80 lb.

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to provide accurate measurement of position by the reception of a known Loran

transmitter. Power supplies, external X Inverter. This unit will make a

very good Oscilloscope, £8/10- each, car. £1.

**RADIO TELEPHONE GR300 V.B.F.** 75 Mc/s two channels, complete

with control box, 12 v. D.C. supply, as new, £50, car. £1. Control

unit 10/-, £3 each; also power supply unit 12 v. D.C., £3/10-

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**AVO METER MODEL 7** with test leads and case, £12/10- each, post 7/6.

**BLOWERS MOTORS**. 115 v. A.C., 50 or 60 c/s., 1.80 hp., 0.2 amps

3,200 r.p.m., cont. duty new in cartons £2/10- each, post 5/-, Smaller

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**RELAYS SEMI ROTARY**. 3 pole DT, contacts suitable for 10 amps.

(silver), coil 12 v. D.C., new in cartons 12/6 each, post 2/6.

**TRANS/RECEIVER UNIT Mk. 3**. 12v. 2 to 8 mc/s. RT or CW.

MCW, external external power supply. Complete station £9. Trans-rec

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Complete installations can be quoted for. Please write further details. List available 6d. S.A.E. for all enquiries.

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**TRANSFORMERS**. 230 to 115 v., isolation 300 va, £3 each, plus 5/-, 230/115 auto 300 va, £2, post 5/-, 230 v. pri., 24 v. at 2 amp., 22/6, plus 5/-, 230/115 v. pri., 230/275 v. at 120 ma., 6.3 v. at 4 amp., 6.3 v. at 1 amp., 25/-, post 5/-.

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**CONVERTERS**. Type Ba, 24 v. D.C., 115 v. A.C. at 1.8 amps 400 cycles, 3-phase, £6/10- each, post 8/-.

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£3/10- each.

**ANTENNA SHIELD (for UPX 6)** CW224/U. £5 each, carriage 10/-.

**DESK TELEPHONE**. 30/- each or £2/15/- per pair, post 5/-.

**TEST EQUIPMENT**. SGA/ARN. Transmitters T164/AT7. AN/UMF11A. T217A. GR. Also Modulator MD199A. GR. F1003 Training Equipment (Please write for further details on these items).

**MARCONI TYPE TF-144G SIGNAL GENERATOR**. Freq. 85 Kc/s-25 Mc/s., internal and external modulation, power supplies 200/250 v. A.C., price £25, car. 30/-.

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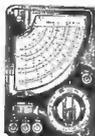
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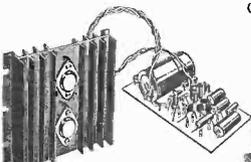
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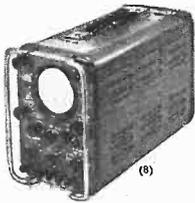
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**(1) ROADSTER MW/LW CAR RADIO**

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10 watts R.M.S. output. 10 mV sensitivity, 30 c/s to 20 Kc/s. MPA10/13 to 5 ohm Speaker. MPA10/15 12 to 16 ohm Speakers. Panel size 4 1/2 x 1 1/2 in. 11 1/2 size 4 x 1 1/2 in. \*MPA10/3, £5/10/-, p.p. 2/6. \*MPA10/5, £5/19/6, p.p. 2/6. (Mains Unit 59/6, p.p. 2/6. State type required.)

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High sensitivity 'scope, fully portable with Mullard DG7/5 2 1/2 in. tube. 10 c/s to 40k c/s. FREE running Time Base. Single Sweep. Pulse Monitoring 50 msec. to 0.1 u.s. Y Plate Sensitivity 40 v. per cm. 3 dB 25 c/s. to 2 Mc/s and up to 35 dB Gain on Amplifier. Full Input Facilities and Controls. 110 to 250 volt A.C. mains operated. Complete in portable case with leads. in new condition.

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Two Channel Preamplifier for (2) 10 watt or 25 watt amplifiers. 8 inputs per channel. Sel./Treble/Bass/Balance/Vol./etc. Controls. 150 mV. input. For P.U.'s, Tuner, Tape, mic. etc. Size 9 x 3 1/2 x 1 1/2 in. \*SP £10/19/6, p.p. 3/6. (Front Panel 12/6.)

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MW/LW Superhet tuner. Output up to 1 volt peak. Full coverage with excellent sensitivity and selectivity. 9 volts operated. Complete with front panel, etc. Total cost build 79/6, p.p. 2/-.

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**BRAND NEW STOCKS**

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1 m.c/s. HCGU (miniatur) 20/-  
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Parts list and circuit diagram 2/6. Free with parts.



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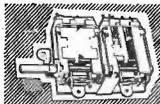
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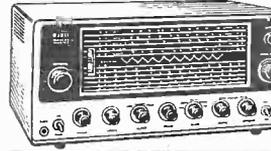
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Will extend years for this. Join latest P.P. history, plug sockets, easy to fit, phone, and an incoming call is amplified. No need to stop work waiting for numbers to answer. Fast with large receiver coil. MINV. see above! perfect, recording of conversation can be made. Ideal gift sales present.

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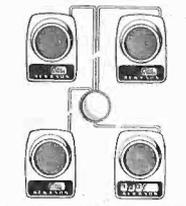
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Bank purchase has cut retail price by half! A top quality, fully transistorized system designed for hotel office and professional use. Consists of one master and two three stations with built-in call system. Absolute privacy for each extension. Push-button control. Crystal clear reproduction through this speaker. Suitable for use with 30 v. cable. American built. Instructions etc. **\$7.10.0** (Post & Insurance 5/-).

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12A7	9/0	12A7T	7/6	D118	12/6	EP91	2/6	PL91	6/0	UP80	8/0
312	4/0	12A10	4/6	D122	7/6	EP188	8/0	PL82	5/6	UL11	3/6
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3A0	6/0	12A81T	8/6	D123	2/0	EP194	4/0	PL81	7/6	UL21	4/6
3A3	4/0	12A7T	3/6	D124	5/6	EP195	5/6	PL82	7/6	UL21	4/6
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3V5	5/6	20A1	11/6	D124	5/6	EP199	5/6	PL86	7/6	UL18	8/0
3V6	5/6	20A1	11/6	D124	5/6	EP200	5/6	PL87	7/6	UL18	8/0
3V7	5/6	20A1	11/6	D124	5/6	EP201	5/6	PL88	7/6	UL18	8/0
3V8	5/6	20A1	11/6	D124	5/6	EP202	5/6	PL89	7/6	UL18	8/0
3V9	5/6	20A1	11/6	D124	5/6	EP203	5/6	PL90	7/6	UL18	8/0
3V10	5/6	20A1	11/6	D124	5/6	EP204	5/6	PL91	7/6	UL18	8/0
3V11	5/6	20A1	11/6	D124	5/6	EP205	5/6	PL92	7/6	UL18	8/0
3V12	5/6	20A1	11/6	D124	5/6	EP206	5/6	PL93	7/6	UL18	8/0
3V13	5/6	20A1	11/6	D124	5/6	EP207	5/6	PL94	7/6	UL18	8/0
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3V15	5/6	20A1	11/6	D124	5/6	EP209	5/6	PL96	7/6	UL18	8/0
3V16	5/6	20A1	11/6	D124	5/6	EP210	5/6	PL97	7/6	UL18	8/0
3V17	5/6	20A1	11/6	D124	5/6	EP211	5/6	PL98	7/6	UL18	8/0
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**CARTRIDGES:** Ronette Stereo 25/-; Acos GP67 15/-; G.C.2 Garrard 15/-; AT5 Shells 5/-, p. and p. 6d. HG983 Stereo 20/-

**SPEAKER ENCLOSURES:** "TONY" Corner Cabinet 20 x 10 x 7in. takes 10 x 6 speaker covered in grey Roxine and Vynal 45/-, P & P 5/-

"BLAKE" 12in. heavy duty cabinet size 24 1/2in. x 18in. x 9in. The battle is 2in. thick. Covered Roxine and Vynal 45/-, P & P 10/-

"BLAKE DE LUXE" veneered with woodgrain Formica and standing on smart 6in. legs £6/5/-, P & P 10/-

"HAYDON" 16 1/2 x 15 x 7 1/2in. Fabric covered suitable for 12in. speaker 45/-, P & P 7/6

Critical Mike 200C replaces BM3 30/-, P & P 2/- for 2/-

Stand for same 9/6, P & P 1/9

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**BARGAINS IN TRANSISTORS**  
AC127, AC114, 114, 117, 118, 119, OC169, 170, 171, 172, 5/6 ea. OC72, 75, 92, 3/6, OC71, 81M3, n.a. RF Packs 1 OC44, 2 OC15 8/6, AF Packs 1 OC81D, 1 OC151, AF Pack 112 GET Pack 12, OC15, OC26, 28, 29, 7/6, ORP12 Light Coil 7/6. Diodes OAB1 2/3, OAB1 1/9, P & P on all these 6d.

**EMERSONS** with cord and 3 1/2 mm. plug, 8 ohm magnetic 3/-; 250 ohm 4/-; 170 ohm magnetic with clip 6/6; Crystal 4/-, P & P 6d.

**SPEAKERS:** ELAC Heavy Duty Ceramic Magnet 11.000 pins. 10in. round, 10 x 6in. 15 or 3 ohm 42/6, P & P 3/6. 8in. round 15 or 3 ohm 38/6, P & P 3/6. F.M.I. 13 x 8in. 15 or 3 ohm 42/6, P & P 3/6. Stockists for Eagle Products, Goodman, W.B., Wharfedale, Bakers, Tripletone, Linear, all makes of Amplifiers and speaker systems. Let us quote for your requirements. S.A.E. please. NO C.O.D.



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WW-151 FOR FURTHER DETAILS.



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Table of Transistors with columns for part number, gain, and other specifications.

Table of Zener Diodes with columns for voltage, power, and tolerance.

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WW-153 FOR FURTHER DETAILS.

# FEATURE PAGE

## Brand New German & British PVC RECORDING TAPES also Pre-Recorded Language Courses in French, Italian, German & Spanish

Our tapes are manufactured by world famous firm and offered at less than half-price. All tapes are 100% tested, have fitted leaders, are boxed and fully guaranteed. These tapes are comparable with any other on the market today.

S.P.	3in.	150ft.	2/3
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L.P.	7in.	1,200ft.	10/-
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D.P.	5 1/2in.	1,200ft.	11/-
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Postage and  
Packing 1/-  
per spool, 4  
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Learn foreign languages the easy way from brand new pre-recorded tapes in German, French, Spanish, Italian.

26 easy step-by-step lessons on each tape, recorded at 3 1/2 i.p.s. and supplied complete with hand-book. Normal retail price 59/6 each. Our price 19/6 each. Postage 1/- each.

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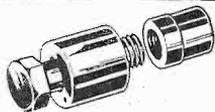
Known as the Radio Photograph, it measures 10 1/2in. x 7in. x 1 1/2in. Skilfully designed and a technical achievement in size, power and reception. Plays 45 & 33 r.p.m. records using high efficiency crystal pick-up. Transistorised and powered by 4 U7 batteries (6v.). A unique bargain, guaranteed and serviced by us, the only supplier in Britain. Send cheque or P/O plus 6/- to: A.T.M.O. (Imports), 59 Whitehicks, Letchworth, Herts. Tel.: 3590

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### HOLE PUNCHES

Instant Type		6/10 ea.
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Complete Set £9 3 6.

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# sales engineers

Due to the continual expansion of the company's activities in the Radio communications field, vacancies exist for SALES ENGINEERS in both U.K. and EXPORT Sales Departments.

Duties will comprise preparation of proposals and customer liaison and give opportunities for travel at home and abroad.

A fast-growing company, RACAL COMMUNICATIONS LIMITED is in the forefront of the communications field, and is located at Bracknell, Berkshire, approximately 30 miles from London.

Successful applicants will be expected to possess a thorough knowledge of communications techniques.

Drive, enthusiasm and team spirit are essential. Previous commercial experience is highly desirable.

Salary scale will be determined by qualifications and experience.

In the first instance applicants should write giving brief details of education, experience and qualifications to:-

**RACAL**  
THE RACAL GROUP

Sales Director,  
Racal Communications Limited,  
Western Road,  
Bracknell, Berkshire.

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SERIES DISCOUNT: 15% is allowed on orders for twelve monthly insertions provided a contract is placed in advance.

BOX NUMBERS: Replies should be addressed to the Box number in the advertisement. c/o Wireless World, Dorset House, Stamford Street, London, S.E.1.  
No responsibility accepted for errors.

Advertisements accepted up to MARCH 7 for the APRIL issue, subject to space being available.

## SITUATIONS VACANT

**COMMERCIAL RADIO STATION (U.K.)**  
BROADCASTING in medium wave band, requires three high power transmitter engineers with associated audio and line equipment experience; salary up to £1,500 p.a.—Write Personnel Director, Box W.W. 1457, "Wireless World."

**DYE CAMBRIDGE WORKS, Ltd., Haig Rd., Cambridge.**  
• SINGLE sideband equipment.  
• VHF radiotelephone equipment.  
• HI-FI reproduction equipment.  
WE require trained personnel for production testing and fault finding of modern equipment.  
WE have limited vacancies for more senior and experienced men with drive, who can lead small teams engaged on this work.

WE have also limited vacancies for persons of less experience who can be trained for such work.  
APPLY to: The Personnel Director, 151

**UNIVERSITY OF OXFORD, Inorganic Chemistry Laboratory.**  
HEAD of Electronics Section. Qualified electronics Technician required to take charge of section of Research School in the Inorganic Chemistry Laboratory. Some experience with stabilised power supplies, spectrophotometers, oscilloscopes, electron microscopes, etc. would be useful. Salary on Senior or Principal Technician scale according to qualifications and experience. University pension scheme. Good holidays and conditions of work.—Applications to the Secretary, Inorganic Chemistry Laboratory, South Parks Road, Oxford. 11405

**PERMANENT and progressive** for first-class ROYAL Engineer (Mech and field), N.W. area, good salary, transport and subsistence allowance; if you are a top class man—field work only. 11383

**GRAMPLAN REPRODUCERS, Ltd., Harworth Trading Estate, Featherthorpe, Notts.** require a senior engineer for development of audio equipment. Fully equipped in public address applications. 11405

**FULL-TIME** technical experienced Salesman required for retail sales, write, giving details of age, previous experience, salary required to: The Manager, Henry's Radio, Ltd., 3-5, Edwars Road, Wotton, W. 11409

**TEST Service Engineer, adventurous young man** required capable of working on own initiative in busy 24-hour shop; of advanced company manufacturing complex control systems, WCI—Apply Box W.W. 1349, Wireless World.

**BEST LONDON AERO CLUB** invite A & D licensed engineer with capital and/or necessary equipment to commence radio workshop; alternative propositions may be considered.—Write full details to White Waltham Aerodrome, near Maidenhead, Berks. 11417

**ELECTRONICS**, enthusiastic man required for production development laboratory, practical electronics and O.N.C. Maths. (Maths) essential, age unimportant, salary according to merit and experience.—Ed. Chiswick 6661/2/3 for appointment. 11426

**CHIEF** transformer Designer required for wide range of small transformers, degree of A.M.I.E.E. preferred and a very attractive salary will be paid. We are part of a public company and operate a pension scheme.—Write: Managing Director, Drake Transformers, Ltd., Kemnal Lane, Hitherley, Essex. 11426

**CIVIL AVIATION, Telecommunications.**—The Ministry of Aviation has vacancies for Radio Technicians at airports, Air Traffic Control centres, radio stations and other specialised engineering establishments throughout the United Kingdom. The numbers and speed of air traffic today demands a complex, co-ordinated and reliable telecommunications system for airports, en-route navigation and air traffic control. In order to ensure the highest standards of safety, the Ministry's radio technicians play a vital role in the installation, maintenance and technical operation of this system. Their duties embrace a wide range of equipment, including primary surveillance and approach radars, secondary surveillance radars, radar navigational and landing aids, radio and line communications, electronic aids to display, radio circuit TV, digital and analog computers. Candidates should be aged 19 or over, of British nationality and possess a sound basic knowledge of radio electronics with practical experience in at least one of the main branches of Telecommunications. The possession of formal qualifications would be an advantage. Training and equipment and new techniques are provided by the Ministry's Civil Aviation Studies Training Establishment, Hitherley, Essex. Holders of the award are encouraged to study for technical and professional qualifications, and receive assistance, including part-time study, in special circumstances. Full-time use of salary provided. There are good prospects of permanent pensionable posts and promotion to a higher class with a salary ranging from £1,032 per annum to £1,911 per annum. Starting salary will be according to age: £747 per annum at 19 to £962 per annum for entrants aged 25 or over, and rise to £1,163 per annum. Annual leave is 3 weeks and 3 days, plus 9 days for public holidays.—For further details apply to: Mr. J. A. Robinson, M.P.E.E., A.M.I.E.E., Ministry of Aviation, Room 754, The Adelphi, London, W.C.2. 11419

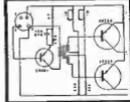


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Due to continued expansion it is now desirable that we should increase our technical staff, and opportunities for advancement are readily available for men with the right experience and ability.



We are able to offer highly competitive rates of pay, with excellent conditions of employment, which include Superannuation and Life Insurance Schemes.

Please apply to the Personnel Manager,  
Mr. G. J. Sharkey,

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Goodwood Works, North Circular Road, N.W.2  
Telephone GLAdstone 0171 Ext. 129

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Our dynamic organisation is geared to obtain for you the best job available in the area you require. If you are seeking employment in S.E. England and have at least two years' experience in British industry, contact Electronics Appointments Ltd., who are the foremost source of employment in Great Britain. Write or phone for details of our free and confidential service.



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Norman House, 105-109 Strand,  
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## SYSTEMS TEST ENGINEERS

Pye Telecommunications Limited require Systems Test Engineers for work on custom-built control systems for v.h.f./u.h.f. radio schemes. Knowledge of line and/or radio techniques essential. Experience on carrier equipment or v.f. telegraphy or telephone exchange equipment is desirable.

*Apply to:* Personnel Manager,  
Pye Telecommunications Ltd.,  
Newmarket Road,  
Cambridge. Tel. No.: Teversham 5131.

## ASSISTANT TELECOMMUNICATIONS ENGINEERS

Required by the EAST AFRICAN POSTS AND TELECOMMUNICATIONS ADMINISTRATION on contract for one out of 24 months in the first instance. Commencing salary £1,094 in scale rising to £2,262 a year including allowances. Terminal Gratuity 25% of salary drawn. Generous disturbance allowance. Free passages. Liberal leave on full salary. Accommodation provided at low rental.

Candidates should be aged between 28 and 45 years and possess the relevant City and Guilds Certificates, or equivalent, and have gained experience in one or more of the following: (1) Automatic Telegraphy, (2) Carrier and Telegraph Equipment, (3) H.F. and V.H.F. Radio, (4) External General, (5) Underground Cable Planning.

Apply to CROWN AGENTS, M. Dept., 4 Millbank, London, S.W.1, for application form and further particulars, stating name, age, brief details of qualifications and experience, and quoting reference M2T/62721/WF.

## MARCONI INSTRUMENTS LIMITED

ST. ALBANS · HERTFORDSHIRE

ARE YOU A SKILLED AND EXPERIENCED ELECTRONICS TECHNICIAN?  
HAVE YOU BEEN A WIRELESS OR RADAR FITTER IN THE ARMED FORCES?  
CAN YOU DO A PROFESSIONAL REPAIR JOB ON A T.V.?  
DO YOU HAVE GOOD TECHNICAL QUALIFICATIONS BUT LACK INDUSTRIAL EXPERIENCE?

If you can answer "YES" to at least one of these questions then we should like to hear from you.

We need new test and calibration engineers to help us increase the output of our very wide range of telecommunication measuring instruments.

The work requires the understanding of the most modern and varied circuit techniques and embraces all frequencies up to U.H.F.

The posts are permanent and pensionable; they offer first class staff conditions in a key export Company of English Electric; they will prove attractive to men who believe strongly that there is a real career for them in production.

Call and talk it over if you live close to us at St. Albans. If you would prefer to phone, then ring ST. ALBANS 59292 during the day, or COLNEY HEATH 475 in the evenings, and ask for Mr. Dyson. Alternatively, write to our Personnel Officer, giving details of your training and experience and quoting reference WW2890A.

The Personnel Officer, Marconi Instruments Limited, c/o Directorate of Personnel, English Electric House, Strand, London, W.C.2.

**SERVICE Engineer**—Due to continued expansion of our Audio Division, we now require two first-class Service Engineers who are experienced in working with high quality audio and tape recorder equipment. Applications in writing, giving full details of experience, age and salary requirements, to Personnel Officer, Trivox, Ltd., Neusten Lane, London, N.W.10.

**TEST engineers**—Applications are invited from test engineers with previous industrial experience of radio transmitting and receiving and transmitters; successful applicants will be offered positions on the company's permanent staff, starting commensurate with qualifications and experience. Apply in writing, giving full details of qualifications to Personnel Officer, Reddon, Ltd., Bromhill Rd., S.W.18. 1124

**CITY OF GLOUCESTER EDUCATION COMMITTEE**—Laboratory Technician required in the Department of Electrical Engineering. Some knowledge of electrical engineering and electronics. Salary £705 to £805, ten on satisfactory report to £895 p.a.—Further particulars from the Principal, Technical College, Bristol Rd., to whom letters of application should be sent within 10 days of this advertisement. 1151

**NORTHERN POLYTECHNIC**, Halloway, London, N.7. The Governing Body invites immediate applications for appointment as (a) Senior Lecturer, and (b) Lecturer in the Department of Electronics and Telecommunications. The lecturers will be expected to cover the graduate syllabus of the I.E.R.E. and Part III of the I.E.E. and should hold a degree of a British University or equivalent qualification and be Corporate Members of an appropriate professional engineering institution. Previous teaching and industrial experience an advantage. Salary scales—Senior Lecturer £2,140-£3,030 p.a. Lecturer £1,975-£2,860 p.a. Plus £70 London Allowance. Apply for further particulars (state post, in which interest) and form of application, R. H. Carrell, F.C.A., Clerk.

**UNIVERSITY of the West Indies**, Department of Physics, Electronics Engineer. The University of the West Indies invites applications for the post of Electronics Engineer to help establish an electronic workshop. The workshop will be intended to assist all departments throughout the University and the Teaching Hospital in connection with electronic equipment. The equipment has the widest variety from a mass spectrometer to high powered K.F. transmitters. Applicants should have had a wide experience. The total emoluments for the post will be between £1,500 p.a. upwards to about £2,100 p.a. Applications should be addressed to Professor R. W. H. Wright, Department of Physics, University of the West Indies, Kingston, Jamaica, and should state in detail the qualifications and experience with the names of 3 referees. 11412

**RADAR Technician** required by the Government of Zambia Meteorological Services, on contract for one out of 36 months in the first instance. Commencing salary according to experience in scale rising to £1,525 p.a. plus allowances. Terminal gratuity 25% of total salary drawn. Free passages. Children's educational allowances. Generous leave. Industrial Conditions preferably aged between 25 and 45, must possess Intermediate Certificate or its equivalent or its equivalent and have five years' experience in the installation and maintenance of radar and sea band radar. Familiarity with Plessey (Dracon) Weather and Wind-measuring equipment would be an advantage. The duties of the post will involve travel to various parts of Zambia. Apply to Crown Agents, M. Dept., 4 Millbank, London, S.W.1, for application form and further particulars, stating name, age, brief details of qualifications, experience, and quoting reference M2T/62827/WF. 11520



## VHF TEST ENGINEERS

**CAMBRIDGE WORKS LIMITED** have vacancies in their expanding Test Organisation for men with experience of VHF Transmitters and Receivers.

Men with Service training in VHF equipment would be suitable.

Progressive rates of pay and promotion and good facilities for training are offered.

*Apply:* Personnel Manager,  
Cambridge Works Limited,  
Haig Road, Cambridge.

Be where the break-through is being made in



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Opportunities in the following Product Groups:

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Big things are happening at RBM Electronics. Big break-throughs. In every field RBM technologists are pushing forward the old frontiers, to pave the way for tomorrow. With RBM at Welwyn, research is the key-note. There are immediate opportunities in new and expanding fields for **PROJECT LEADERS, DESIGN and SALES ENGINEERS** as well as vacancies in other Departments for qualified technicians and graduates in such fields as Test and Installation. In the factory we need a first-class Chief Production Engineer, Estimators and Rate Fixers. This expansion could open the door for you to share in important development growth. All positions offer genuine promotion prospects as expansion continues. Attractive working conditions too - Welwyn, with its modern buildings and open spaces, is located in pleasant Hertfordshire countryside less than 30 minutes from London. Assistance with housing in certain cases. Participation in all Rank Organisation benefits, including pension and non-contributory life assurance. Make the break-through now: tell us about your career to date, specifying any qualifications you have attained and which division you are interested in,

The Personnel Manager, Rank Bush Murphy Electronics, Welwyn Garden City, Herts. Tel. No. Welwyn Garden 23434

*Outside normal working hours, use our telephone answering service, Ring Welwyn Garden 27906.*

*Give your name, address and the type of vacancy that interests you. An application form - and details of our operation and current vacancies - will be in the post to you tomorrow morning.*



**RANK BUSH MURPHY  
ELECTRONICS**

**STC**

## RADIO DIVISION

**TEST  
METHODS  
ENGINEERS**

We require engineers to specify test methods and design test equipment. Education to H.N.C. standard and two years practical experience are desirable and an interest in automatic test methods would be an advantage.

Starting salary up to £1,225 p.a., Pension Scheme and non-contributory benefits apply to these positions, which offer good prospects for promotion.

For further details write or telephone the:—

Personnel Manager, Radio Division,  
**Standard Telephones and Cables Limited**  
Oakleigh Road, New Southgate, N.11.  
telephone ENTERprise 1234, ext. 489.

**I**MPERIAL COLLEGE, South Kensington, S.W.7, Electronics development; we have a new and interesting vacancy in our electronics group concerned with the application of electronics techniques to our chemical engineering and technological research; several years' practical experience and a good knowledge of transistor circuitry are essential; H.N.C. would be an advantage; this is a unique opportunity to enter the department at a time of rapid expansion and re-equipment; there are excellent opportunities for working on instrument design and systems engineering; starting salary will be in the range of £1,000 to £1,200; write in confidence to—Professor G. R. Hall, Department of Chemical Engineering and Chemical Technology, Imperial College, London, S.W.7.

**TELECOMMUNICATIONS  
ENGINEERS**

required by the GOVERNMENT OF MALAWI on contract for one tour of 24-36 months in the first instance. Commencing salary according to experience in scale (including overseas addition) rising to £1,905 a year. Gratuity 15% of total salary drawn. Outfit allowance £30. Free passages. Liberal leave on full salary. Generous education allowances. Quarters at low rental.

Candidates, preferably aged 25-45 years, must have at least 5 years experience in one or more of the following branches of telecommunications engineering, after completion of two years approved training: Automatic exchanges and Subscribers Apparatus; carrier and V.H.F. equipment; HF radio; overhead lines or underground cables (construction). They must possess at least one appropriate City and Guilds Certificate. Previous overseas experience and experience in training and supervision of subordinate staff would be advantages. For certain posts the ability to instruct and control large numbers of low graded staff is essential.

Apply to CROWN AGENTS, M Dept., 4 Millbank, London, S.W.1, for application form and further particulars, stating name, age, brief details of qualifications and experience, and quoting reference M2T/626-8/WF.

**NEW TELECOMMUNICATIONS  
DEVELOPMENTS**

Involving some of the most advanced equipment in the world, offer careers of outstanding interest, secure and well-paid, to science and engineering graduates. A Royal Signals Officer is trained to command men. He leads a full and satisfying life, much of it out of doors. During his career, he has ample opportunity to obtain professional qualifications and to use them in tackling interesting problems in many different countries. The Royal Corps of Signals is responsible for the network, and also for a world wide static communications system. It needs graduates as officers, and offers immediate commissions to suitable candidates. Pay and allowances now compare very favourably with anything a young graduate could earn in civilian life. Applicants should be under 25, and should hold (or be studying for) a degree or a diploma recognised by the National Council for Technological Awards, preferably in: Mathematics, Physics, Applied Science, Natural Science, Electrical Engineering, or a diploma acceptable to the Institution of Electrical Engineers or the Institution of Electronic and Radio Engineers, as giving exemption from these Institutions' examinations. Service can be either for a short period (minimum three years with tax-free gratuity) or as Limited Service Regular Officer (initially for 16 years with a pension and gratuity at the end) or for a full career up to at least 55. For further details write stating age and educational qualifications held (or for which studying) to: Lt.-Col. D. L. Pounds, Room 045, Ministry of Defence, Dept. 48, Old War Office Building, Whitehall, S.W.1.

**E**NGINEERS and Technicians required with Electronic or Physics education for research, development and maintenance on a wide range of medical and electronic equipment. Current development projects include: in-circuit pressure measurements, Radiocisometry according to age and experience plus London Allowance.—Application forms from the Secretary (EW), The Honorary Miss Children, Great Ormond Street, London, S.E.1. 11424

**U**NIVERSITY OF NOTTINGHAM. The Department of Civil Engineering has a vacancy for a Senior Technician with electronics and electrical experience. Duties will include the maintenance and development of data measuring and recording systems, strain bridges and allied equipment. Salary scale should be capable of and filled under the minimum of supervision and a recognised trade apprenticeship with O.N.C. or equivalent will be considered an advantage. Salary within the range £280 to £1190 according to qualifications and experience. Applications in writing to the Head of Department, Civil Engineering Department, University of Nottingham, Nottingham. 11467

**E**LECTRONICS Technician required in physiological laboratory, re-assigning with transistORIZED recording facilities for co-operative work with the Hospital and services equipment. There are excellent opportunities for co-operative work with the Hospital Department of Physics. The person appointed will be expected to undertake some administrative responsibility in the Dept. Applicants, aged 25-30, should hold an O.N.C. or equivalent with London Weighting in the range £280-£1190. London Weighting of £45 p.a. with superannuation. Apply giving details of experience to the Secretary, Guy's Hospital Medical School, London, Bridge, S.E.1. 11428



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### Television Rental Service Managers.

The present Service organisation and procedures are simple and efficient and the quality of engineers is extremely high. These factors have enabled us to meet the requirements of BBC-2 without undue difficulties. The resultant increase in subscribers has created these vacancies.

Applications for these positions should be made to this BOX NO. 5020, c/o "Wireless World", and show evidence of an understanding of all facets of Service Management and of effectiveness in implementing speedy and efficient service. Ability to undertake further responsibility in the future will be welcomed. Conditions of employment are generous. Removal expenses will be paid if necessary.

**ELECTRONICS** Technician wanted to aid in design and construction of apparatus for Psychological research—Application forms from Educational Officer, University College London, Gower St., W.C.1. quoting Psy/5. (1438)

**IMPERIAL COLLEGE** Research Assistant required R for a space research group centred at Silverton Park, near Ascot, working on rubidium and proton magnetometers for rocket measurements of magnetic fields in the ionosphere, currently concerned with the national Skylark and ESRO rocket programmes. Candidates with 1st or 2nd class degree in electronics or physics required. Salary in the range £1,110-£1,335 according to qualifications and experience, with P.S.U.—Applications to Geophysics Dept., Imperial College, London, S.W.7. (1439)

**ROYAL MILITARY COLLEGE OF SCIENCE, SHRIVENHAM, SWINDON, WILTS.** OPPORTUNITY FOR RESEARCH—Experimental Officer is required for a research project in the field of electromagnetic radiation. Excellent facilities and conditions. Work suitable for publication and submission for higher degrees. Qualifications: Appropriate H.N.C., Pass Degree or equivalent. Experience in electronics generally, and aerial and microwave measurements in particular an advantage. Age: Applicants must be at least 26 years of age. Salary: Within the incremental scale: £1,365x6 annual increments to £1,734 p.a. Accommodation: Temporary single accommodation in the Officers' Mess or the possibility of a married quarter.—Please write for further details in confidence to Professor M. H. F. Pook, Electronics Branch, or for form of application to C.E.P.O. Royal Military College of Science, Shrivenham, Swindon, Wilts. (Please quote reference R.3225/67). (1435)

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An expanding new Company wishing to enter electronics field requires services on a part-time basis of men experienced in the field of H.F. circuitry/transformer design. Reply in complete confidence to

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Established Sound Equipment Manufacturer requires experienced Agents for Sales and Service of Public Address equipment in the following areas:

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Existing contracts advantageous, but the manufacturer will provide new leads. Generous terms available. Write: Box No. 5021 c/o "Wireless World."



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### PYE TELECOMMUNICATIONS

require

#### SYSTEMS ENGINEERS FOR THE DESIGN OF CONTROL SYSTEMS FOR USE WITH RADIO COMMUNICATIONS NETWORKS

Applicants must be experienced in the design and maintenance of telephone switching equipment or multi-channel telephone systems and be familiar with the principles involved.

Experience of the application of such systems to radio bearer circuits is desirable but not essential.

Corporate membership of the I.E.E. is desirable but applicants without such qualifications who can prove wide experience up to a recent date will be considered.

Apply to: Personnel Manager,  
Pye Telecommunications Ltd., Newmarket Road, Cambridge.



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We have vacancies at almost all levels for men or women with enthusiasm. For the Senior posts a degree or equivalent is required and several years design experience on products COMPARABLE with ours.

Please write to Personnel Manager,  
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South Eastern Region  
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BRADWELL NUCLEAR  
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require

MAINTENANCE CRAFTSMEN  
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Applicants should have had experience in the maintenance of physical instruments, electronics and/or telecommunications equipment.

Gross weekly wage £20.10.9 for a 40 hour 5 day week on staggered day working plus service increments after 2 and 3 years' service.

Rented housing accommodation may be available to the successful applicants.

Applications quoting Vacancy No. 1057/66 (W.W.) and stating age, present position and previous experience should be sent to the Station Superintendent, Central Electricity Generating Board, Bradwell Generating Station, Southminster, Essex.

RADIO ENGINEERS  
and COMMUNICATORS

Required by the GOVERNMENT OF ZAMBIA, Department of Civil Aviation, on contract for one tour of 36 months in the first instance. Gratuity at the rate of 25% of total salary drawn. Children's allowances. Free passages. Quarters available at moderate rental.

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Salary according to experience in scale £1,615 to £1,855 a year. Candidates, aged 32 to 50 years, must have had 12 years' experience following a 5 years' apprenticeship or gaining a Services Trade Certificate or a M.O.A. or I.C.A.O. Certificate of Competency (or equivalent). They must have a sound theoretical knowledge of and experience in the maintenance, overhaul and installation of ground terminal radio communication equipment and navigational aids used at Airports and Flight Information Centres.

## RADIO ENGINEERS GRADE II —(M2T/62809/WF)

Salary according to experience in scale £945 to £1,580 a year. Candidates aged 21 to 50 years, require qualifications as for Grade I Engineers but less experience is acceptable.

## COMMUNICATORS GRADE I —(M2T/62812/WF)

Salary according to experience in scale £945 to £1,580 a year. Candidates, aged 21 to 50 years, must have a 1st Class P.M.G. Certificate, or Air Force, Naval or Marine Communicators Trade Certificate of Competency, together with three years' experience and Certificate of Competency, speeds of 25 w.p.m. and 20 w.p.m. respectively. Proficiency in radio telephony operation to international standards is required.

Apply to: CROWN AGENTS, M. Dept., 4 Millbank, London, S.W.1, for application form and further particulars, stating name, age, brief details of qualifications and experience, and quoting the relevant reference.

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Salaries, fringe benefits and conditions of employment are all that you might expect from such a successful organisation.

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To obtain more information about the exciting possibilities that exist for you, write to:—  
The Personnel Officer,  
Department WW.M.18,  
English Electric-Leo-Marconi Computers Ltd.,  
24 Minerva Road,  
London, N.W.10.

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Due to Company expansion, The Decca Navigator Company Limited wishes to recruit the services of Test Engineers for the testing of Radio Navigation and Survey Equipment.

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Applicants with a first class background of T.V. and Radio Servicing or Telecommunication Electronic and Control Circuiting are required.

The salary paid will be commensurate with ability and experience.

Please apply for interview giving brief details of experience, qualifications and present salary to:—

The Personnel Officer,  
The Decca Navigator Company Limited,  
88 Bushey Road, Raynes Park, London, S.W.20.  
Telephone: WIMbleton 8011.

## TEST GEAR ENGINEER

We manufacture and develop Precision Electro-Mechanical Components and Electronic Control and Measuring Instruments. We have a vacancy for a Test Gear Engineer who will be responsible for the analysis of test requirements, the establishment of test methods and the development of test units. The work would include the precision measurement of D.C. and A.C. at low frequency.

Applications are invited from persons with suitable practical experience who need not necessarily have any formal qualifications. The position demands a sense of responsibility, attention to detail and initiative. The starting salary will be in the range £1,000—£1,200 per annum.

Please write or telephone for an application form, quoting reference ARN to the Personnel Manager,

Rank Pullin Control,  
Great West Road,  
Brentford, Middlesex.

### RADIO TECHNICIANS

A number of suitably qualified candidates will be required for testing, leading to permanent and pensionable employment, normally at Cheltenham but with opportunities for service abroad or appointment to other UK establishments including London.

Applicants must be 19 or over and be familiar with the use of Test Gear and have had Radio/Electronic Workshop experience. They must offer at least "O" level (GCSE) passes in English language, Mathematics and/or Physics or both. The City and Guilds Telecommunications Production Intermediate Certificate or equivalent technical qualification.

They continue to age, e.g. at 19 £247, at 25 £262 (highest pay on entry) rising by four annual increments to £1,104.

Prospect of promotion to grades in salary range £1,032-£1,681.

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Normal Civil Service sick leave regulations apply.

Apply:  
Recruitment Officer (RT70),  
Government Communications Headquarters,  
Gable, Price's Road, Cheltenham, Glos

A UNIQUE opportunity occurs for an enthusiastic but capable engineer with wide interests to take charge of the control room for the Theatre and Recording Studios at one of Britain's leading entertainment agencies; must have knowledge of recording, high overhauling and maintenance, a working knowledge of public address system and mixing panels, some knowledge of lighting, be able to operate film film projection equipment and able to carry out first line maintenance and/or installation; an interesting position for a hard-working person.—Apply, in writing, giving as full details as possible to: The General Manager, West One Entertainments, Ltd., 20, Manchester Square, London, W.1. 11414

ELECTRONIC Technician. Do you enjoy playing around with electronic gadgets? Here is a chance to make a career of your hobby. We offer you interesting and varied work in the field of electronic instrumentation. This small but expanding department is concerned with the design and application of electronic circuits required for the testing of diesel engines and their fuel injection systems. Staff conditions are good and include sickness and contributory pension and life assurance schemes, restaurant facilities, etc.—In the first instance, applicants should write in confidence, giving only brief personal details to: The Personnel Manager, Simms Motor Units, Ltd., Oak Lane, East Finchley, N.2. Fin. 2592. 11421

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Write giving brief details of background, and salary required to:

Mr. R. J. Mundy,  
Manager, Service & Calibration Dept.,  
Livingston Laboratories Ltd.,  
Greycoines Estate, Bushey Mill Lane,  
North Watford, Herts.  
Telephone: WATFORD 41291

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# The Civil Service

## Professional and Technical Appointments

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Current vacancies include the following:—

### EXECUTIVE ENGINEERS POST OFFICE

At least 30 posts in London and Provinces for mechanical, electrical and electronic engineers to develop and design communications systems and postal service equipment.

**QUALIFICATIONS:** Degree or Dip. Tech. in Mechanical or Electrical Engineering, Physics, or Applied Physics or, exceptionally, very high professional attainment. Final year students may apply.

**SALARY (Inner London):** £877-£1,806. Salary under review. Promotion prospects.

**AGE:** At least 21 and normally under 35 on 31.12.66. Some extensions for service in H.M. Forces or Overseas Civil Service. (Reference: S/322.)

### ELECTRICAL ENGINEER MINISTRY OF DEFENCE (ARMY DEPARTMENT)

Engineer required at ROYAL ORDNANCE FACTORY, Bishopston, Renfrewshire, for the maintenance and extension of the Electrical Installation of the explosives factory, including 11 KV distribution system, Power Station, and special plant, etc.

**QUALIFICATIONS:** Applicants should have satisfied the basic training and examination requirements for Corporate Membership of the I.E.E. Knowledge of the Factory Acts and Electrical Safety Regulations including Explosive Electrical Regulations and I.E.E. Wiring Regulations is essential. Opportunities for promotion. Candidates under age 35 may apply immediately for permanent appointment. Older candidates can be considered for a pensionable appointment after nine months' service.

**SALARY (interim):** £1,068-£1,633.

**APPLICATION FORMS** from Ministry of Defence, C.E.2(g)2(A/D), Northumberland House, Northumberland Avenue, London, W.C.2. Candidates under age 35 applying for permanent appointment should obtain forms from the Civil Service Commission, Savile Row, London, W.1, quoting S/85.

### ENGINEERING CADETSHIPS

providing training and experience in accordance with the requirements of the major Professional Institutions are open to young engineers (under 26) holding Degrees or Diplomas in Technology with First or Second Class Honours. Graduate Members of the major Institutions will also be considered.

The appointments provide interesting employment and wide experience for Civil, Electrical and Mechanical Engineers ranging from

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practical shop or site work to design and management duties in Government Departments including opportunities of service overseas.

On completing training Cadets are offered appointments which should provide professional responsibility and experience leading to Corporate Membership of one of the Institutions. Promotion to the Main Grade (maximum salary (under review) £2,227) can be expected after three to six years.

**SALARY (Inner London):**

First Year	£996
Second Year	£1,055
Third Year	£1,119

(Reference: S/565.)

There are also vacancies in the Scientific Civil Service as follows:—

### MINISTRY OF DEFENCE (ARMY DEPARTMENT)

### THE ORDNANCE BOARD LONDON, W.14

**EXPERIMENTAL OFFICER** required for examining the electrical safety of a wide range of weapon systems to assess their behaviour under various fault conditions as well as when exposed to electro-magnetic fields; co-ordination of the organisation for and reporting of trials. Ability to chair meetings essential.

**QUALIFICATIONS:** Degree, Dip. Tech., H.N.C., or equivalent in appropriate subject. A good knowledge of radio engineering would be an advantage.

**SALARY:** (Interim age 26) £1,440-£1,819. Prospects of permanent pensionable appointment.

**APPLICATIONS:** To Ministry of Defence, CE2(F)AD, London, W.C.2.

### EXPERIMENTAL OFFICER CLASS SPRING—1966—RECRUITMENT

Careers in SCIENCE and TECHNOLOGY are offered to men and women with qualifications in MATHEMATICS, PHYSICS, CHEMISTRY, BIOLOGY, METEOROLOGY, ENGINEERING and GEOLOGY as Assistant Experimental Officers and Experimental Officers, in Government Scientific Establishments.

**QUALIFICATIONS:** University Degree, Dip. Tech., H.N.C., etc., and candidates under age 22 may offer lower qualifications (minimum: G.C.E. "A" level in 2 scientific or mathematical subjects).

**SALARY and AGE LIMITS:**  
Experimental Officer (age 26-30) £1,365-£1,734.  
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Salaries supplemented in London area. Aid given for further education. Promotion prospects.

Closing date 18th March, 1966. (Reference: S/577-578/66.)  
(Further recruitment in Autumn, 1966.)

SP has vacancies in the Cable Branch of its Head Office in London for a **TECHNICAL ASSISTANT (TELEPHONE SYSTEMS)** and a **DEPUTY TECHNICAL ASSISTANT (TELECOMMUNICATIONS)**. Responsibilities will include the maintenance and servicing of—

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Applicants should have had at least 5 years previous experience in this field and possession of City and Guilds Certificate in Telephone Engineering 1st or 2nd Grade A (with honours), or equivalent, or range 29-40 years' instruction and introductory training on new equipment will be given on joining. The Company also offers several other benefits including a Longshore Unit, Non-vacillatory Pension Scheme, 2 weeks holiday, etc.

Please write giving details of age, and experience to: **P. G. Andrews, Central Staff Department, The British Postphone Company, 85F House, Roper's Green, E.C.H.** quoting reference H.2457 (W).

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**BOOKS, INSTRUCTIONS, ETC.**  
**MANUALS** circuits of all British ex-W.D. 1959-45 wireless equipment and instruments from original W. R. Bailey, 167A, Moffat Rd., Thornton Heath, W.143

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**Service Manager,  
SUMLOCK COMPTOMETER LTD.,  
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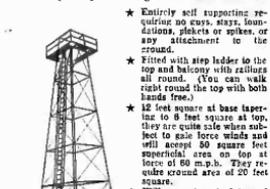
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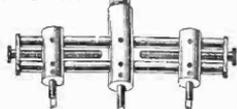
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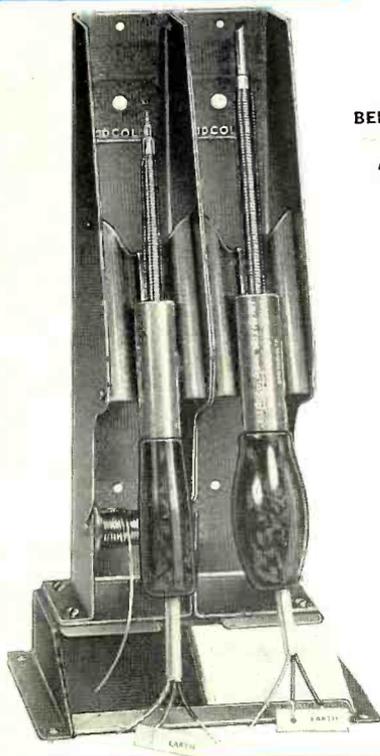
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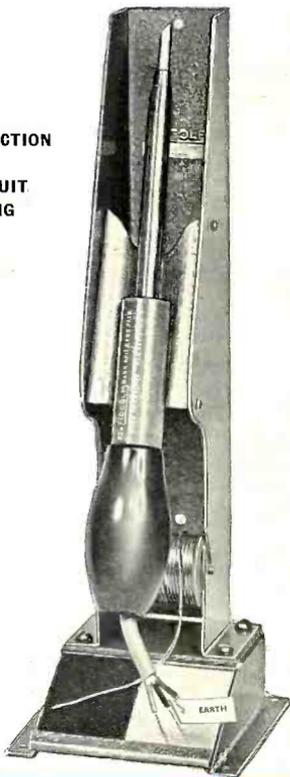
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S.W.G.	INS.	M.M.	FT. PER LB.	
			60/40	SAVBIT
10	.128	3.251	25.6	24
12	.104	2.642	38.8	36
14	.080	2.032	65.7	60.8
16	.064	1.626	102	98.2
18	.048	1.219	182	170
19	.040	1.016	252	244
20	.036	.914	324	307
22	.028	.711	536	508
24	.022	.558	865	856
26	.018	.46	1292	1279
28	.014	.375	1911	1892
30	.012	.3146	2730	2695
32	.0108	.274	3585	3552
34	.009	.233	4950	4895

STANDARD ALLOYS INCLUDE LIQUIDS

TIN/LEAD	B.S. GRADE	MELTING TEMP.	
		°C.	°F.
60/40	K	188	370
50/50	F	212	414
45/55	R	215	419
40/60	G	234	453
30/70	J	255	491
20/80	V	275	527

HIGH AND LOW MELTING POINT ALLOYS

ALLOY	DESCRIPTION	MELTING TEMP.	
		°C.	°F.
T.L.C.	Tin/Lead/Cadmium with very low melting point	145	293
L.M.P.	Contains 2% Silver for soldering silver coated surfaces	179	354
P.T.	Made from Pure Tin for use when a lead free solder is essential	232	450
H.M.P.	High melting point solder to B.S. Grade 5S	296-301	565-574

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SAVBIT ALLOY REDUCES WEAR OF SOLDERING IRON BITS.



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Contains 102 ft. approx.  
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C1SAV14 11ft. of 14  
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C1SAV16 16ft. of 16  
s.w.g.

C1SAV18 30ft. of 18  
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