

Wireless World

May 1969 Three Shillings

Review of digital microcircuits
Logic display aid



If you design and manufacture electronic equipment such as computers, radar systems, avionics etc., you will know all about Ferranti high precision transformers. You will know all about their quality and reliability, in short they are engineered by Ferranti standards. They have always been pretty popular—a bit too popular if anything, for we were continually pushed to meet delivery dates. Faced with this situation, we did the obvious thing—expanded production. Not just a bit—but dramatically. A brand-new factory was raised at Dundee. New equipment installed—more production teams recruited and trained.

Now it's all ready. You can have the same transformers, built to the same high standards, but more of them and a lot quicker.

Right now there are 5000 different designs in existence. If we can't suit your system out of that lot, number 5001 will be just for you. And you can have a prototype more quickly than you thought possible.

If you need transformers of outstanding precision and reliability—however adverse the operating conditions, get in touch with Ferranti.

Write or telephone for immediate attention:
FERRANTI LTD., TRANSFORMER GROUP, DUNSINANE AVENUE, DUNDEE, SCOTLAND. Telephone 0382-89311

Trans formation

in transformer production at Ferranti, Dundee



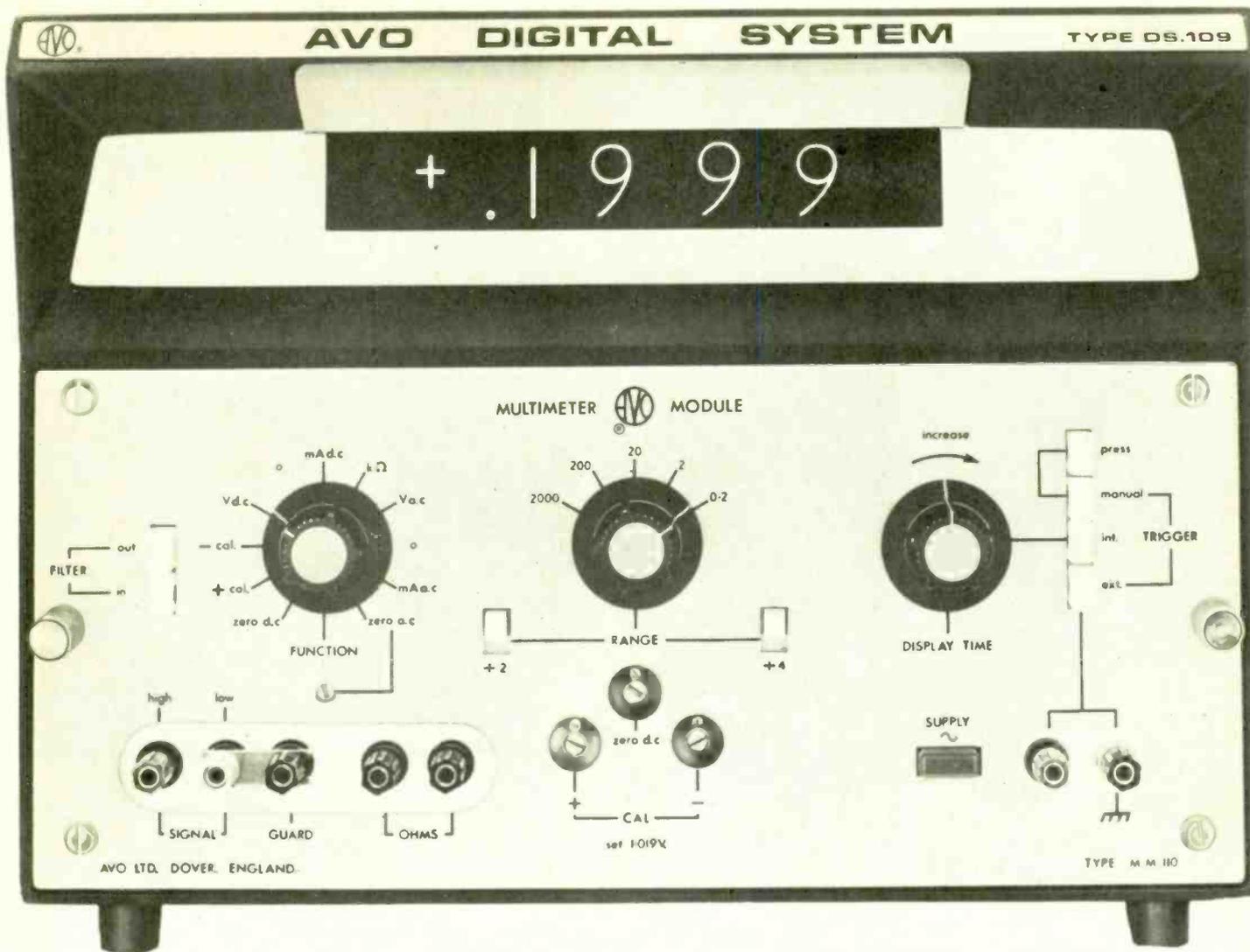
Now in production at Ferranti Dundee; resin-cast and oil-filled hermetically sealed transformers, chokes, pulse transformers and delay lines for electronic and electrical applications, including special lightweight versions for airborne use. High temperature transformers for use in aircraft with operating winding temperatures of 250°C. A range of open type 'C' cored transformers for commercial applications. Resin cast HV current-limiting power units for electrostatic applications.

VISIT FERRANTI'S STAND E202 AT THE INTERNATIONAL LONDON ELECTRONIC COMPONENT SHOW AT OLYMPIA

FERRANTI

DS/T199 

WW-001 FOR FURTHER DETAILS



SEE US ON STAND NO. C105
AT THE INTERNATIONAL COMPONENT SHOW
OLYMPIA 20-23RD MAY

this new modular Digital System from Avo is much more than a DVM

With the Multimeter module and an optional a.c. converter, the new Avo Digital System measures not only a.c. and d.c. voltages but also a.c./d.c. current and resistance.

Other plug-in modules convert the Display Unit into a Digital Timer/Counter, a Digital L.F. Generator and other high-performance laboratory digital instruments.

Even with the Multimeter module the System gives you:

- 45 ranges of d.c. voltage, current and resistance measurement
- 75 ranges of measurement including a.c. voltage and current if the optional a.c. converter card is inserted
- 10% over-range on all ranges without loss of accuracy
- fully floating guarded input
- accuracy (Vdc): 0.05% of indication \pm 0.05% of full range value
- full-range accuracy at quarter or half of full range
- 50-way socket for print-out signal

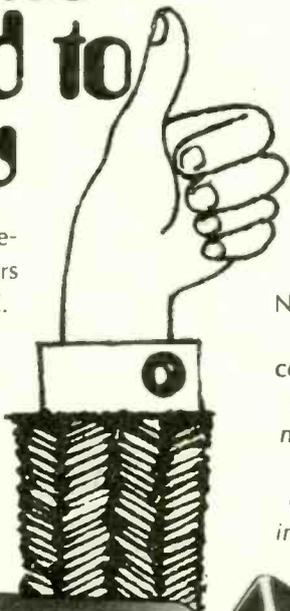


Get full details of the versatile new Avo Digital System from Avo Limited, Avocet House, Dover, Kent. Telephone: Dover 2626. Telex: 96283. THORN

WW-006 FOR FURTHER DETAILS

Anders is the name- pleased to meter you

No matter what your meter requirements, we meet them. Fast. Anders holds the largest stocks in the U.K. for off-the-shelf delivery, so the meters you need yesterday, ordered today, can probably be with you tomorrow. In quantity, too. If you've got special problems like non-standard requirements, give us a ring. Our technical department creates panels to individual needs.



Anders offers the most comprehensive and efficient meter service — and we do mean service — available.

N.B. The variety of meters in our new catalogue is a revelation — and now we've got extensive new centralised premises for a better-than-ever service. *Manufacture and distribution of electrical measuring instruments and electronic equipment. The largest stocks in the U.K. for off-the-shelf delivery. Prompt supply of non-standard instruments and ancillaries. Sole U.K. distribution of FRAHM vibrating reed frequency meters and tachometers.*

ANDERS METER SERVICE

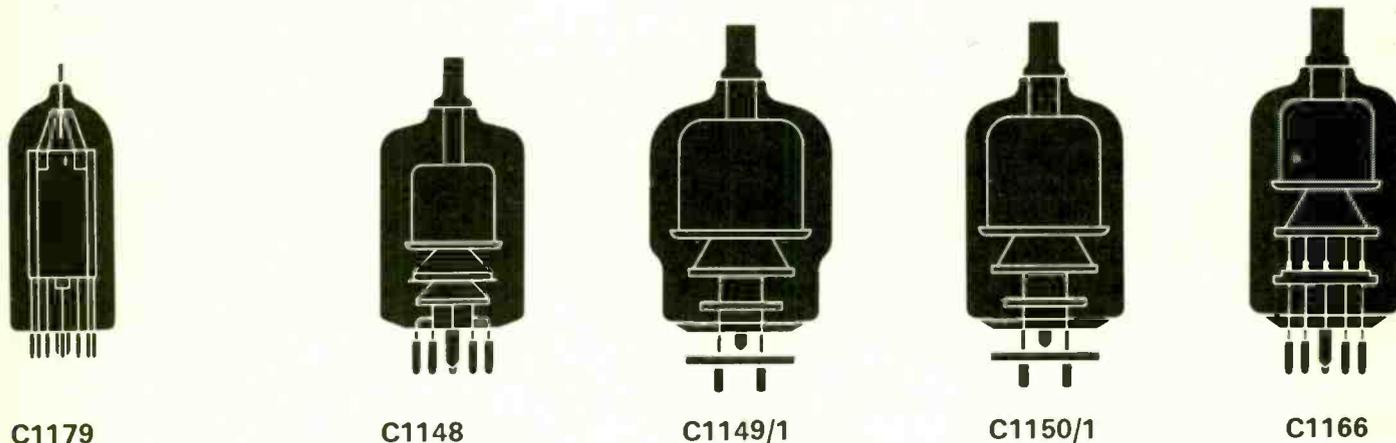
Anders Electronics Ltd.,
48-56 Bayham Place,
Bayham Street,
London, N.W.1.
Telephone: 01-387 9092



WW—007 FOR FURTHER DETAILS

New pulse tetrode for low power radars added to EEV's range

The new C1179—a high vacuum beam tetrode designed primarily for the output stage of power amplifier pulse modulators in 5kW-10kW radars.



Type	Service type	Anode dissipation max. (W)	Pulse output power (kW)	Anode voltage max. D.C. (kV)	Pulse anode current max. (A)	Heater ratings		Base
						(V)	(A)	
C1148	—	40	130	14.0	12	6.3	5.0	B5F
C1149/1	CV6131	60	330	20.0	18	26.0	2.15	B4A
C1150/1	CV427	60	205	17.5	15	26.0	2.15	B4A
C1166	—	60	205	17.5	15	6.3	9.0	B5F
C1179	—	18	65	8.0	9.0	6.3	2.8	B7A

Send for full data on the EEV range of pulse amplifier tetrodes



English Electric Valve Co Ltd
 Chelmsford Essex England Telephone: 61777
 Telex: 99103 Grams: Enelectico Chelmsford



Please send me full details on your range of pulse tetrodes. I am particularly interested in using a pulse tetrode with the following parameters:

Pulse output power	Anode dissipation	Anode voltage	Pulse anode current
NAME	POSITION		
COMPANY			
ADDRESS			
TELEPHONE NUMBER		EXTENSION	

WW-008 FOR FURTHER DETAILS

QUAD 50 is a single channel 50 Watt amplifier designed for Broadcast, Recording and other applications in the Audio industry, completely proof against misuse and giving the highest quality of reproduction.



INPUTS - 0.5 Vrms unbalanced with provision for an optional plug-in transformer for bridging 600 ohms lines.

OUTPUTS - isolated providing 50 watts into almost any impedance from 4 to 200 ohms.

DIMENSIONS - 12 $\frac{3}{4}$ " x 6 $\frac{1}{4}$ " x 4 $\frac{1}{2}$ "

Complete the coupon and post today.

QUAD
for the
closest approach
to the
original sound

Please send me full details of the QUAD 50 Amplifier

NAME

POSITION

COMPANY

ADDRESS

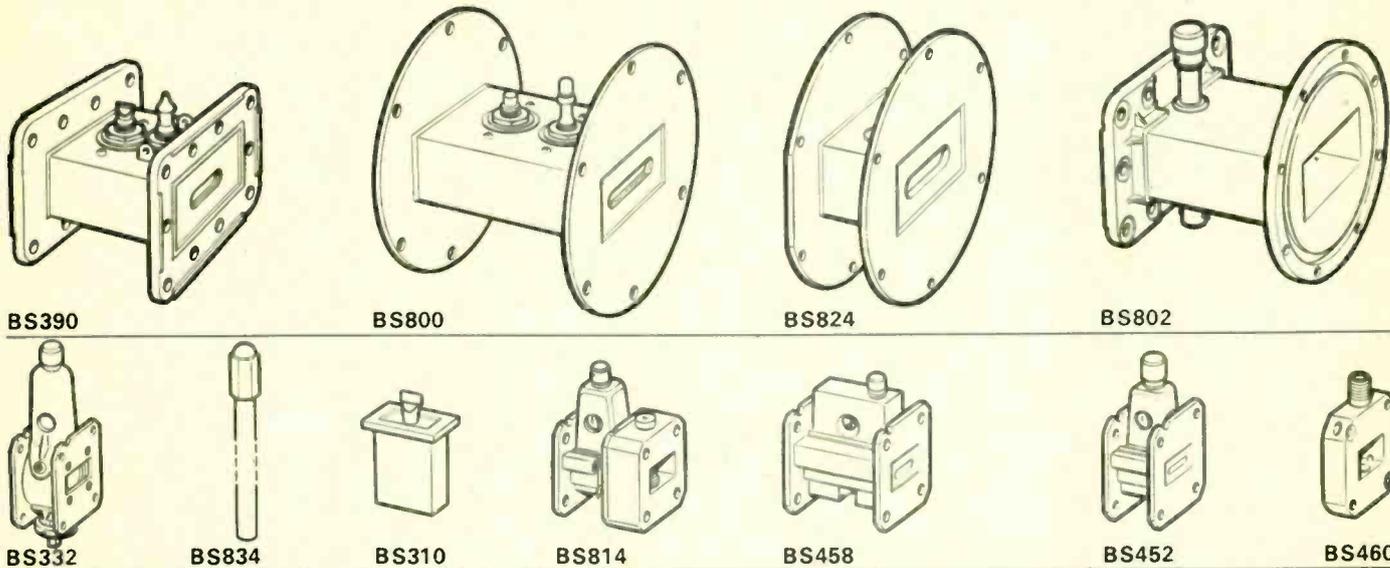
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(BLOCK CAPITALS)

ACOUSTICAL MANUFACTURING CO. LTD.,
HUNTINGDON. Telephone: Huntingdon (0480) 2561/2

W W

Choose your duplexer devices from EEV's extensive range

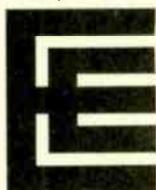


Brief data on some of the many types available.

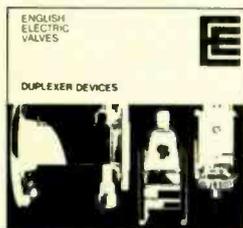
Product	Type No	Band	Frequency range (MHz)	Peak power (kW)
Pre TR cells	BS834	—	2000-12000	2500
	BS870	—	1240-1365	2500
	BS390	S	2925-3075	1250
TR cells	BS800	S	2840-3100	1250
	BS824*	S	2700-3100	250
	BS156	X	9000-9600	200
	BS452	X	9310-9510	100
	BS810	X	9250-9550	75
	BS850	X	9300-9500	50
	TB cells	BS310	X	9375
TR limiter cells	BS814	X	9000-9700	200
	BS828	X	9325-9425	50
Solid state microwave switches	BS392	S	2925-3075	0.5
	BS460	X	8500-12000	0.5

*For protection of travelling waveguide amplifiers

Send for this booklet giving full details of the complete range of EEV duplexer devices and waveguide switches.



English Electric Valve Co Ltd
 Chelmsford Essex England Telephone: 61777
 Telex: 99103 Grams: Enelectico Chelmsford



Please send me a copy of "Duplexer Devices". I am interested in a tube with the following parameters:

Frequency range _____ Power _____ Type of cell _____

NAME _____ POSITION _____

COMPANY _____

ADDRESS _____

TELEPHONE NUMBER _____ EXTENSION _____

WW—010 FOR FURTHER DETAILS

prepare now for tomorrow's world

Today there is a huge demand for technologists such as electronics, nuclear and computer systems engineers, radio and television engineers, etc. In the future, there will be even more such important positions requiring just the up-to-date, advanced technical education which C.R.E.I., the Home Study Division of McGraw-Hill Book Co., can provide.

C.R.E.I., Study Programmes are directly related to the problems of industry including the latest technological developments and advanced ideas. Students claim that the individual tuition given by the C.R.E.I. panel of experts in each specialised field is comparable in technological content with that of technical colleges.

Why C.R.E.I. Courses are best

No standard text books are used — these are often considerably out-of-date when printed. C.R.E.I. Lesson Material contains information not published elsewhere and is kept up-to-date continuously. (Over £50,000 is spent annually in revising text material.)

Step-by-step progress is assured by the concise, simply written and easily understood lessons.

Each programme of study is based on the practical applications to, and specific needs of, Industry.

Take the first step to a better job now—enrol with C.R.E.I., the specialists in Technical Home Study Courses.

C.R.E.I. PROGRAMMES ARE AVAILABLE IN:

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City and Guilds of London Institute: Subject No. 49 and Advanced Studies No. 300.



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Correspondence Colleges
C.R.E.I. (London), Walpole House,
173-176 Sloane Street, London S.W.1.
A subsidiary of McGraw-Hill Inc.

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To C.R.E.I. (London), Walpole House, 173-176 Sloane Street, London, S.W.1.
Please send me (for my information and entirely without obligation) full details of the Educational Programmes offered by your Institute.

My interest is City and Guilds please tick General

NAME _____

ADDRESS _____

EDUCATIONAL BACKGROUND _____

ELECTRONICS EXPERIENCE _____

WW118

WW-011 FOR FURTHER DETAILS

EEV thyratrons- for better high speed switching

EEV glass and ceramic hydrogen thyratrons are extensively used to provide more precise and efficient high speed switching. Here are some of the reasons why:

- 1 Their short anode delay time of between 20 and 120 nanoseconds depending on triggering method.
 - 2 Low jitter generally of 1 to 2 nanoseconds but down to less than 1/2 nanosecond depending on heater supply.
 - 3 The negligible change in anode delay time—typically only 10 nanoseconds over a long period of use.
 - 4 A high peak inverse voltage capability of 20kV immediately following pulse.
 - 5 The low trigger power required.
 - 6 The wide operating voltage range of 1kV-120kV with four tubes.
 - 7 The ability to control anode delay time and rise time of current, using reservoir.
 - 8 The wide reservoir range for maintenance of gas pressure typically 4.5V to 5.7V.
- The standard range plus EEV's ability to meet special requirements means that virtually any high speed switching application can be met.

Here are a few:

Radar modulators with a system output power of 10kW – 10MW.

Medical linear accelerators with RF accelerating powers up to 15MW.

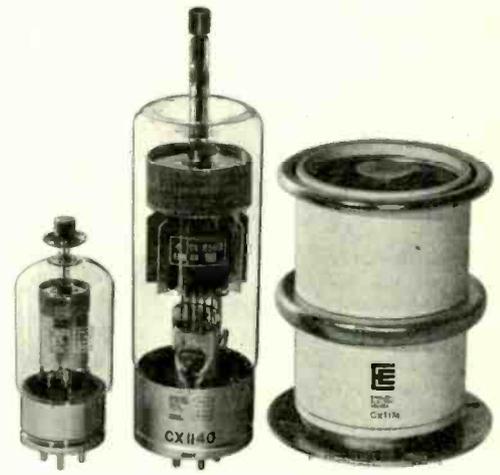
Particle linear accelerators with RF accelerating powers up to 50MW. They may also be used in first-stage particle beam choppers.

Particle beam benders where a network of stored energy needs to be discharged into a deflection coil or other device somewhere on the accelerating ring.

Spark chambers

For pulsing light shutters such as Kerr or Pockel cells.

Electronic crowbars and energy diverters



Brief data on some of the ceramic types available.

Type	Peak power output max (MW)	Heating Factor (V.A.p.p.s.)	Peak forward voltage max (kV)	Peak anode current max (A)	Mean anode current max (A)
CX1154	50.0	30 x 10 ⁹	40	2500	3.0
CX1157	3.5	7 x 10 ⁹	20	350	0.35
CX1168	100.0	70 x 10 ⁹	80	2500	2.5
CX1171	150	70 x 10 ⁹	120	2500	2.5
CX1174	120	60 x 10 ⁹	40	6000	6.0
CX1175	200	140 x 10 ⁹	80	5000	6.0
CX1180	12.5	9 x 10 ⁹	25	1000	1.25

Send for full details of the complete range of EEV thyratrons.



English Electric Valve Co Ltd
Chelmsford Essex England Telephone: 61777
Telex: 99103 Grams: Enelectico Chelmsford



I am particularly interested in using a thyatron with the following parameters:

Application

Peak power output

Peak forward voltage

Peak anode current

Please send me full data on your complete range of glass and ceramic hydrogen thyratrons

NAME

POSITION

COMPANY

ADDRESS

TELEPHONE NUMBER

EXTENSION

WW—012 FOR FURTHER DETAILS

WW15

AP 359

PYE SPANS THE WORLD



Pye Telecommunications is the world's largest exporter of radiotelephone equipment. Pye Radiotelephones are used all over the world to ensure *instant* contact. Pye research development and quality control really *do* keep in touch with tomorrow.

rely on

the vital contact



Pye 'Pocketfone' Personal Radiotelephone
 New battery economy circuit - Extremely light-weight and compact - Reception free from noise and interference - Minimum of controls - Transmit button automatically extends antenna - Hearing aid socket - Easily accessible batteries.



Pye 'Bantam' Portable VHF Radiotelephone
 Fully transistorised transmitter and receiver - Very high performance receiver - Crystal filter selectivity - 0.5W transmitter output - 250mW audio power - Long endurance with rechargeable or dry batteries - Can be used with external antenna to give greater range - Weatherproof.



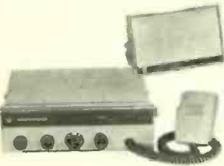
Pye VHF Radiotelephone Fixed Station
 Solid-state receiver and transmitter - 10-15W R.F. output - Field-effect transistors used in receiver - Suitable for all climates - Electronic squelch - Designed to meet all relevant specifications.



Pye UHF Radiotelephone Fixed Station
 Solid state receiver and transmitter - 8-10W R.F. output - Very high R.F. selectivity using field-effect transistors - Very low noise factor - Electronic squelch - A. C. or 24V d.c. operation - Suitable for all climates - Designed to meet all relevant specifications.



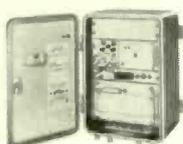
Pye 'Westminster' Remote Mounted Radiotelephone
 Completely solid state - 5-8W R.F. output - 1-10 channels with solid state switching - Illuminated channel indicator - Suitable for all climates - Meets all relevant specifications.



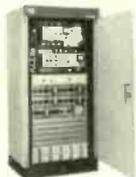
Pye 'Westminster' Front Mounted Radiotelephone
 Completely solid state - 5-8W R.F. output - 1-10 channels with solid state switching - Suitable for all climates - Meets all relevant specifications.



Pye Single-Sideband Radiotelephone
 125W (p.e.p.) R.F. output - Fully transistorised receiver - C.W. facilities provided - Sideband selection by crystal filter - Carrier insertion for a.m. compatibility - Fixed or mobile application - Advanced transmitter design.



Pye 'Pioneer' Radiotelephone
 Fully transistorised - For use with automatic, CB manual, or magneto exchanges - Weatherproof cabinet - Unattended operation over long periods - Facility for fitting privacy equipment - Optional single antenna operation.



Pye 5-Circuit UHF Radiotelephone
 Compact 5-circuit radio terminal - Fully transistorised channelling equipment - Frequency-shift signalling - Continuous unattended operation in all parts of the world - Twelve standard plans for terminals and repeaters.

PYE
 equipment gives you instant-contact with mobility

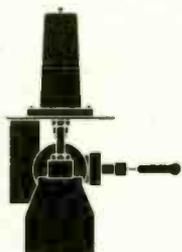
PYE TELECOMMUNICATIONS LTD. Cambridge England Telephone: Cambridge (0223) 61222 Telegrams: Pyetelecom Cambridge Telex: 81166

WW-013 FOR FURTHER DETAILS

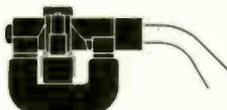
Be safe...use EEV magnetrons in your marine radar

Brief data on some of the many types available. The complete range covers S-Band and X-Band types from 3-80kW.

Type	Frequency Range (MHz)	Peak Output Power (kW) (Typical Operation)	Equivalents (not complete)
M5063	3025-3075	50	2J70B
2J42	9345-9475	8	ME1101, CV3676, MAG3, M526
BM1002	9415-9465	21	JP9-15B
M513B	9345-9405	22	JP9-15, YJ1110
M515	9380-9440	25	YJ1120
M597	9380-9440	10	
M598B	9380-9440	22	
599A/B	9415-9475	3	JP9-2.5D, JP9-2.5E, 7028
M5022	9415-9475	30	YJ1121
M5031	9345-9405	9	
M5043	9380-9440	5.8	
M5039	9345-9405	22.5	



M5063



M515



M599A/B



M513B

Send for full details of EEV marine magnetrons.



English Electric Valve Co Ltd
Chelmsford Essex England Telephone: 61777
Telex: 99103 Grams: Enelectico Chelmsford



Please send me full data on your range of marine magnetrons. I am particularly interested in using a marine magnetron with the following parameters.

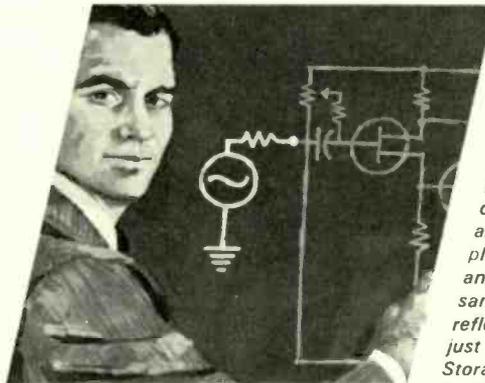
Frequency Range (MHz)	Peak Output Power (kW)	Pulse Length (μs)	Pulse Repetition Rate (p.p.s.)
NAME	POSITION		
COMPANY			
ADDRESS			
TELEPHONE NUMBER		EXTENSION	

WW-014 FOR FURTHER DETAILS

Exploring the Hewlett-Packard Universe of Electronics Instrumentation

...it keeps expanding to reveal new solutions to your measuring problems.

- 1 Two oscillators from among 17
- 2 Plug-in scope system
- 3 Low-priced digital voltmeter
- 4 Universal counter
- 5 Hewlett-Packard Journal



1 Do you work with ac circuits? You'll then want to explore our soft spot for oscillators.

The very first instrument from hp was a Wien Bridge RC oscillator. That was back in 1939. We've had a soft spot for oscillators ever since... to the point where hp oscillators are today, world known for their excellence.

Now there are 17 different oscillators, including two new ones we'd like you meet. Both feature 0.5% (0.05 dB) flatness, FET's in the bridge for improved stability, < 0.1% (-60 dB) distortion, and balanced output.

Model 204C has a 5 Hz - 1.2 MHz frequency range and an output of 5 Vrms.

You can operate it with line power, mercury battery or rechargeable battery pack. Price: £142 including duty

Model 209A generates simultaneous sine and square wave outputs from 4 Hz to 2 MHz. Output amplitudes independently adjustable to 10 Vrms (sine wave) and 20 V peak-to-peak (square wave).

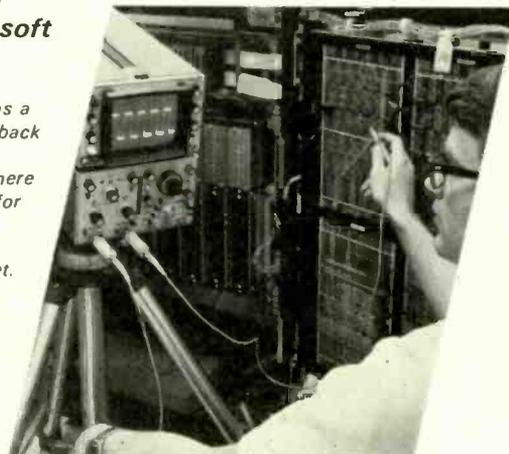
Price: £180 including duty

Get in touch with us for the full story about our complete selection of oscillators.

2 A scope system that's big in versatility and small in size

This is about an expansion-happy scope system. We call it the hp 180A. It is guaranteed against obsolescence by our determination to keep adding to the already respectable lineup of versatile plug-ins. This list already includes 50 MHz and 100 MHz amplifiers, 4 and 12 GHz samplers, a 35ps time-domain reflectometer and a four-channel amplifier just to mention a few.

Storage and variable persistence come with the 181A main frame. You can store traces for hours or weeks, and see slow signals by varying persistence from 0.2 sec to more than one minute.



The all-solid-state 180A scope system is compact and portable. It has the ruggedness and environmental tolerance you need for field applications. The large 8 x 10 cm CRT assures excellent viewability.

hp 180A main frame: £375

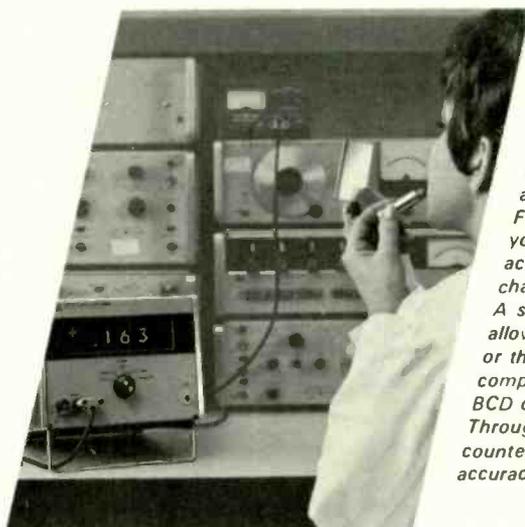
hp 181A main frame, with variable persistence and storage:

£848 excluding duty.

WW—015 FOR FURTHER DETAILS

E 26-UK

3 A digital voltmeter for the fair sex?



Why not? Isn't many a production line staffed by girls? And don't the ladies also contribute their share to quality control? Don't they rate a rugged, foolproof digital voltmeter of their own? Of course they do. That's why hp designed the 3430A, for use by inexperienced personnel. And this low-priced instrument is equally handy for repair and laboratory work.

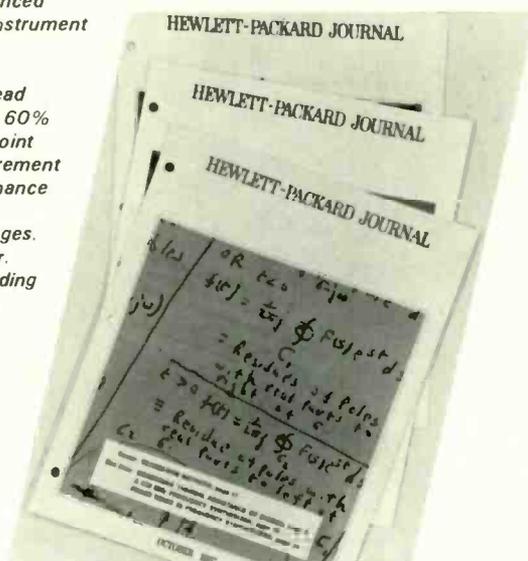
The 3430A has a large, easy-to-read 3-digit display, with a 4th digit for 60% overranging. Polarity and decimal point are indicated automatically. Measurement range: ± 100 mV to ± 1000 V. The chance of circuit loading is reduced by the 10 megohm input resistance in all ranges. No need for frequent calibrations either. The 3430A maintains its $\pm 0.1\%$ of reading + 0.1% of range accuracy for 90 days. May we send you the data sheet? The 3430A is priced at £259 and it's made in Britain.

just about all the measurements for which electric counters are used. The 5325B thus measures frequency, period, multiple period averages, ratio, multi-ratios and simple or complex time intervals from 100 ns to 10^8 s.

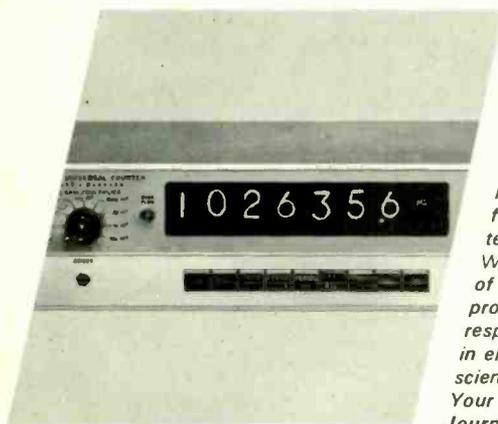
The frequency range is 0 to 20 MHz. The nine gate times, from 0.1 μ sec to 10s, are derived from a crystal oscillator whose aging rate is less than 1 part in 10^8 /day. For accurate time interval measurements, you can select slope, level and either ac or dc coupling for the start and stop channels.

A scope marker output from the 5325B allows you to intensify the triggering points or the entire measured segment. It has complete remote programming capabilities, BCD output, and buffer storage. Throughout, it was our aim to give you a counter combining high versatility, high accuracy and low price. £695 including duty.

5 An insider's view of R&D at Hewlett-Packard



4 Why we call it a universal counter



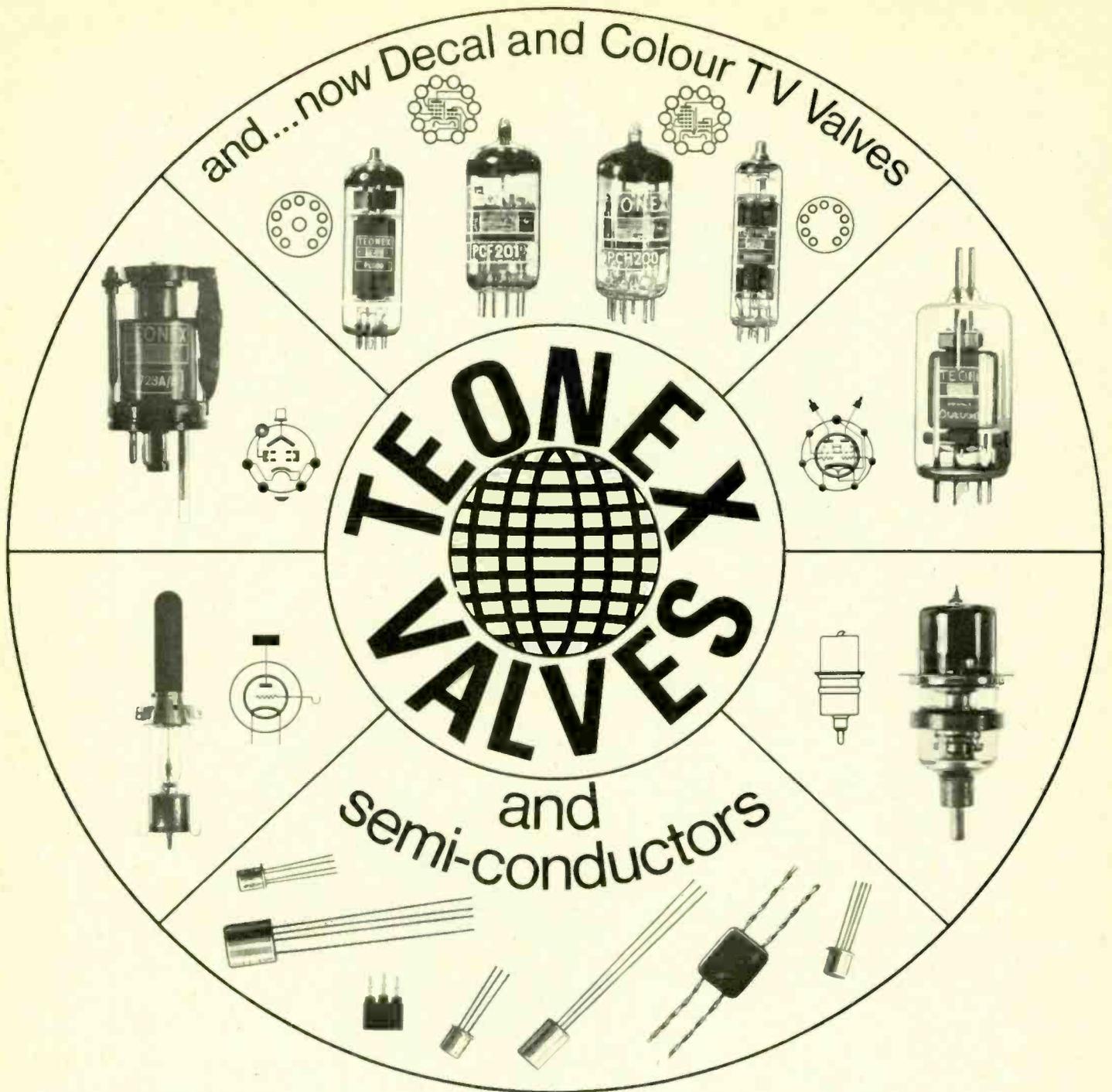
We call the hp 5325B a universal counter because it has built-in capability to perform

The Hewlett-Packard Journal is a monthly publication written by members of the hp research and development team. Their articles may be devoted to the design considerations behind our latest instruments. Or they may deal with applications. Or they may discuss such diverse research projects as atomic hydrogen masers, new writing techniques for graphic recorders, or precision temperature measurements. What it all adds up to is an insider's view of our research and development programme; a close-up of the ideas responsible for hp's consistent leadership in electronic measuring instruments and scientific data processing equipment. Your subscription to the **Hewlett-Packard Journal** will cost you no more than a postcard asking us to add your name to the mailing list.



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Comprehensive range for civil and military authorities as well as domestic users in more than 50 countries.

Teonex now supplies a full range of British made valves and semi-conductors (or their Continental equivalents) to authorities operating stringent quality control, and to private individuals right across the world. Current price list and further particulars available on request from:

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LONDON · W11 · ENGLAND



AVAILABLE ONLY
FOR EXPORT

WW—017 FOR FURTHER DETAILS

Ferrograph Series 7 - a lifetime of recording

Ferrograph Tape Recorders have been famous ever since 1949. A lifetime's experience of making fine recorders goes into every one of Ferrograph's brilliant new Series 7.

And there is a lifetime's recording in every Ferrograph instrument. Many of the earliest Ferrographs are giving perfect service today, nearly twenty years later. You can be sure your Ferrograph will do the same for you. It will give dependable service for many, many years to come. It will keep its value. It will need the minimum of service. Spare parts will remain available for a lifetime's recording. That's how Ferrograph got its name.

Available in Mono, and in Stereo with and without end amplifiers: combining a unique range of 30 recording facilities, including:

- All silicon solid-state electronics with FET input stages and wide input overload margins.
- Vertical or horizontal operation.
- Unit construction: The 3 individual units i.e. tape deck, power unit and amplifier complex are mounted on a single frame easily removable from cabinet for service or installation in other cabinets or racks.
- 3 motors (no belts). 3 tape speeds.
- Variable speed spooling control for easy indexing and editing.
- Electrical deck operation allowing pre-setting for time-switch starting without need for machine to be previously powered.
- Provision for instantaneous stop/start by electrical remote control.
- Single lever-knob deck operation with pause position.
- Independent press-to-record button for safety and to permit click-free recording and insertions.
- 8 1/2" reel capacity.
- Endless loop cassette facility.
- Internal loud speakers (2)—1 each channel on stereo, 2 phased on mono.
- 4 digit, one-press re-set, gear-driven index counter.
- 2 inputs per channel with independent mixing (ability to mix 4 inputs into one channel on stereo machine).
- Signal level meter for each channel operative on playback as well as record.
- Tape/original switching through to output stages.
- Re-record facility on stereo models for multi-play, echo effects etc, without external connections.
- Meters switchable to read 100 kHz bias and erase supply with accessible preset adjustment.
- Three outputs per channel i.e. (1) line out—level response. (2) line out—after tone controls. (3) power output—8-15 ohms.
- Power output 10W per channel.
- Independent tone controls giving full lift and cut to both bass and treble each channel.
- Retractable carrying handle permitting carrying by one or two persons.



U.K. Retail prices from £150 incl. P.T.

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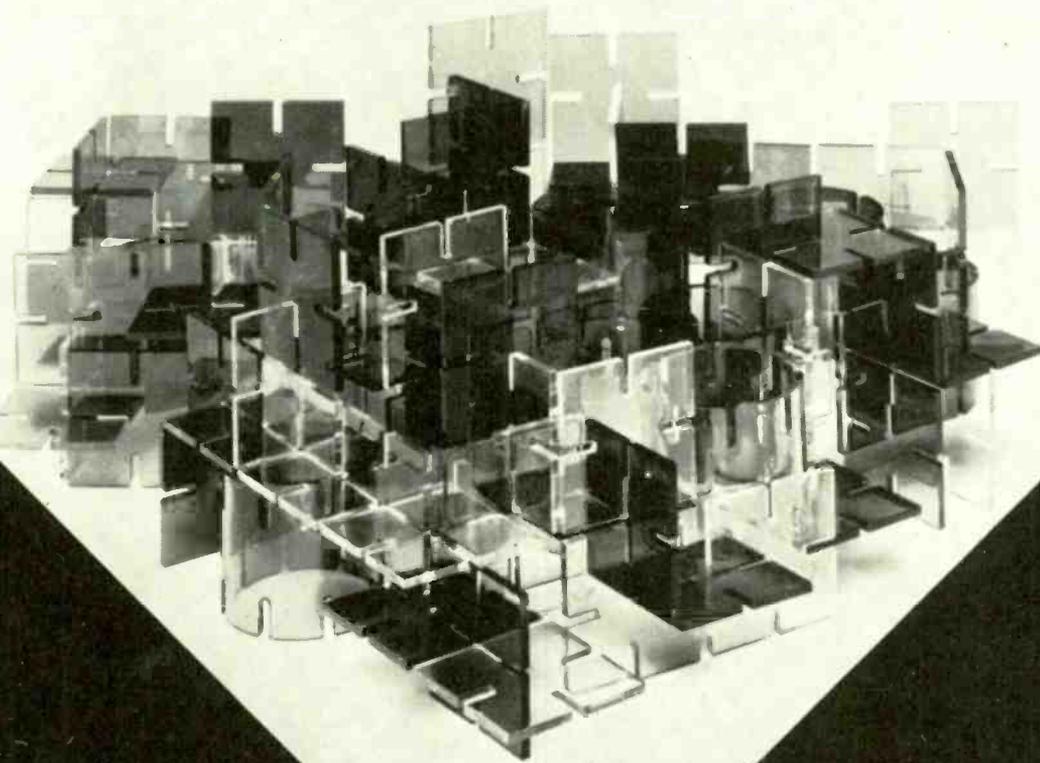
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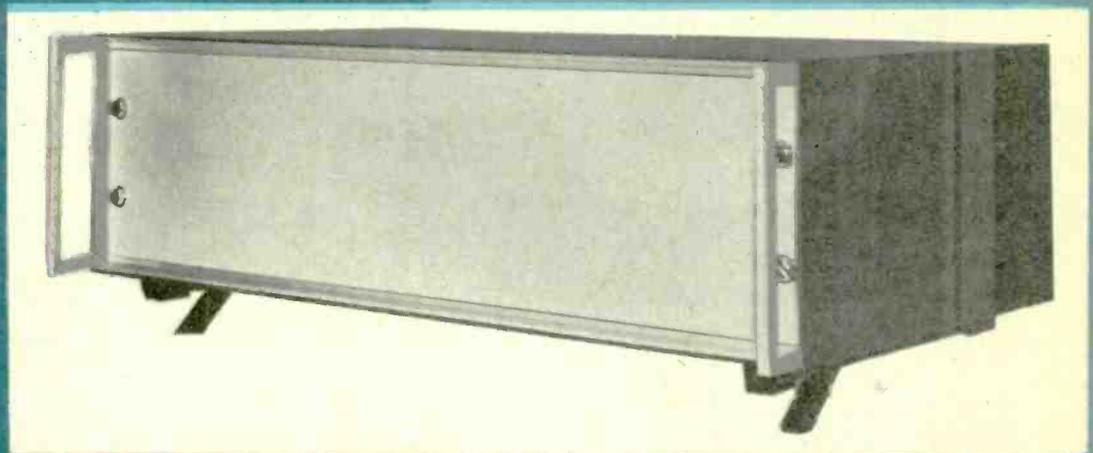
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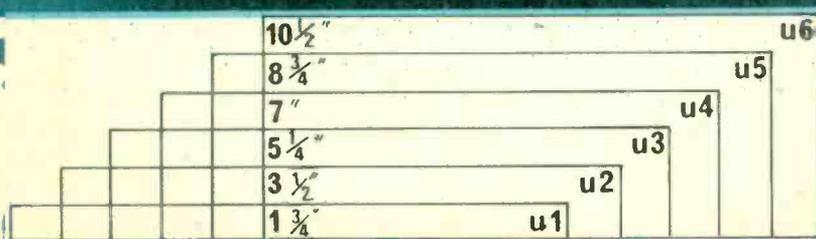
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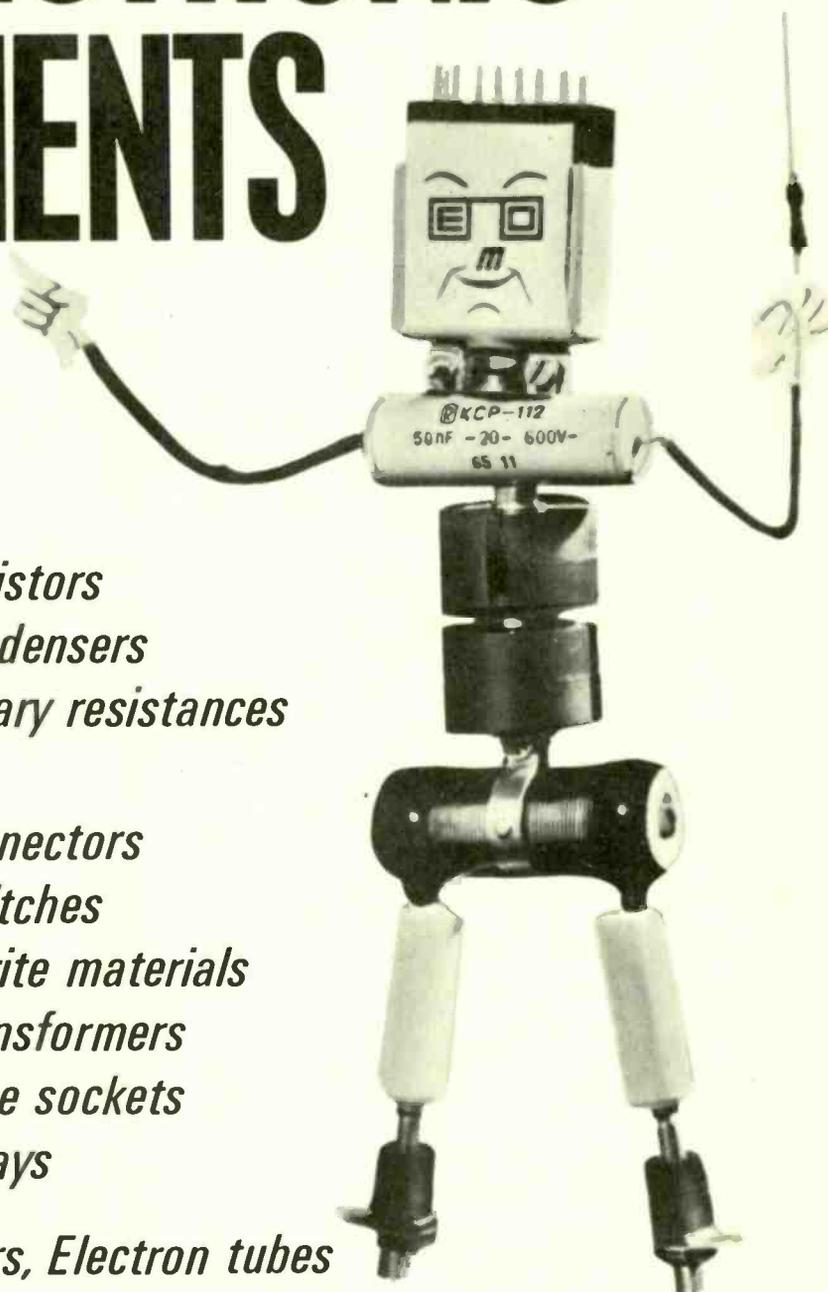
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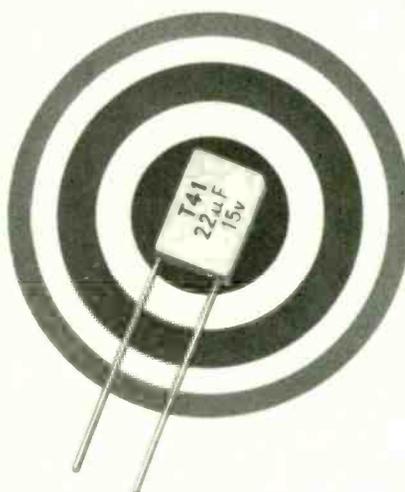
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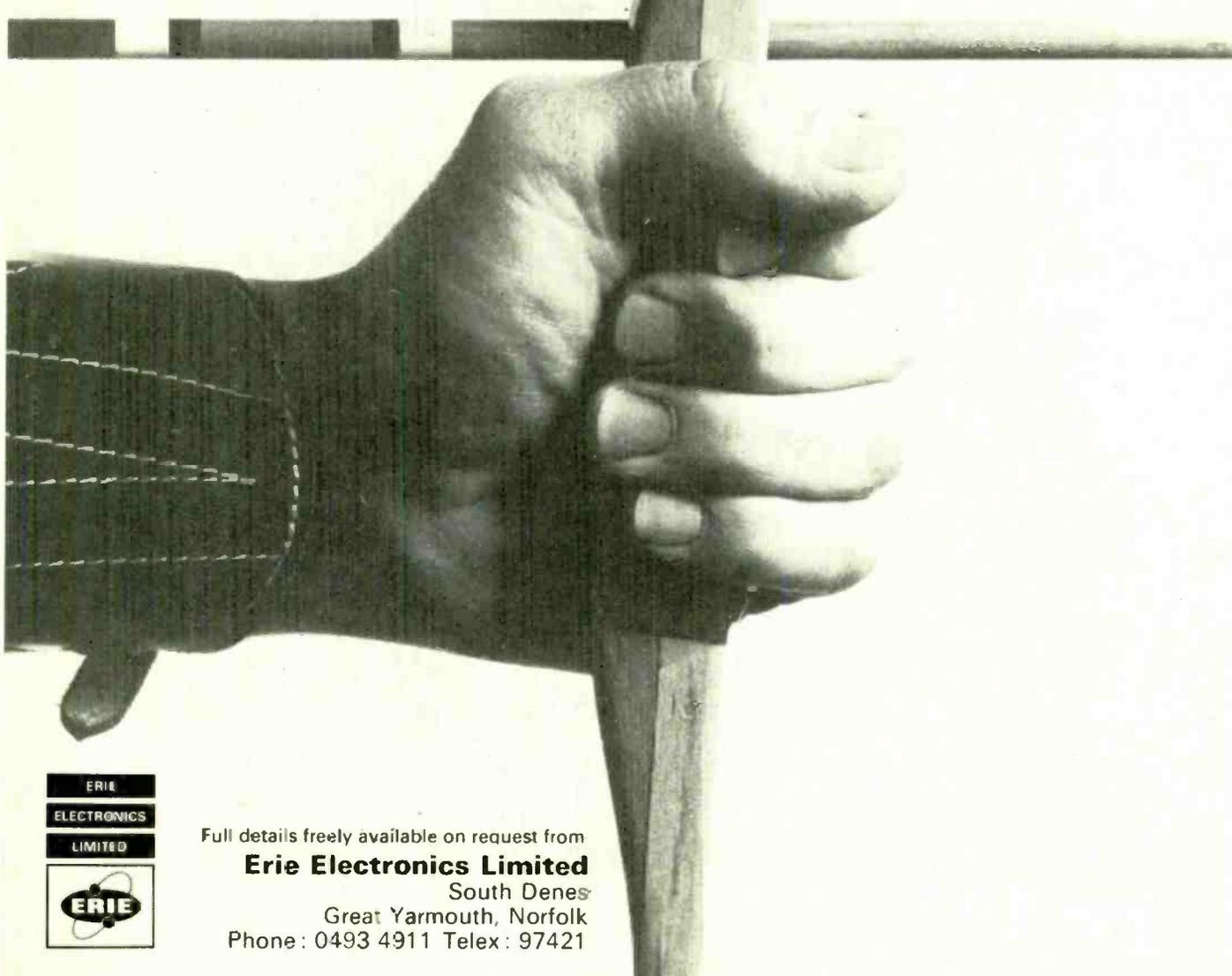


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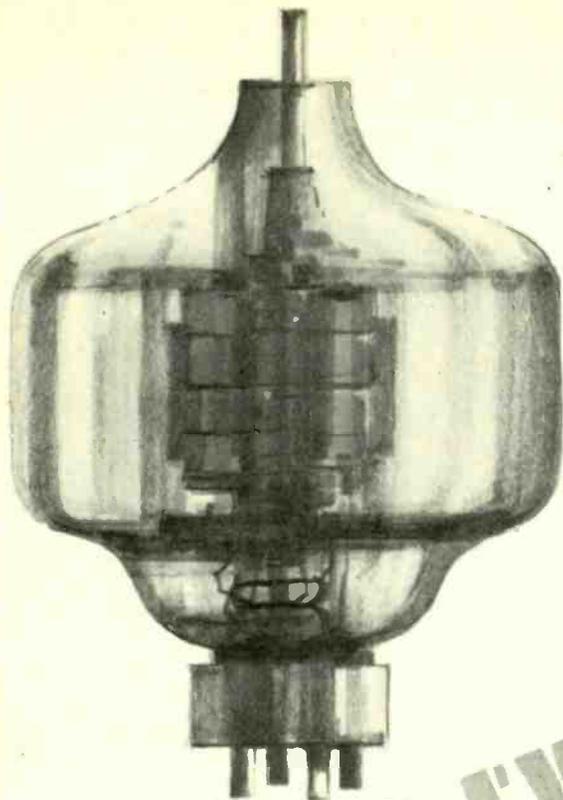


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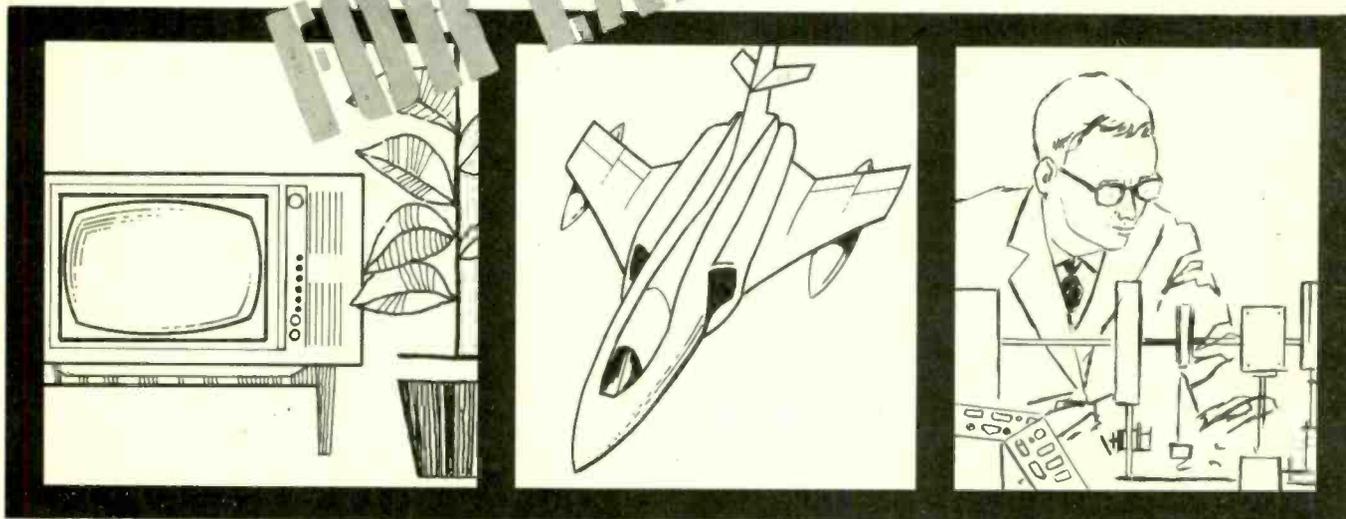
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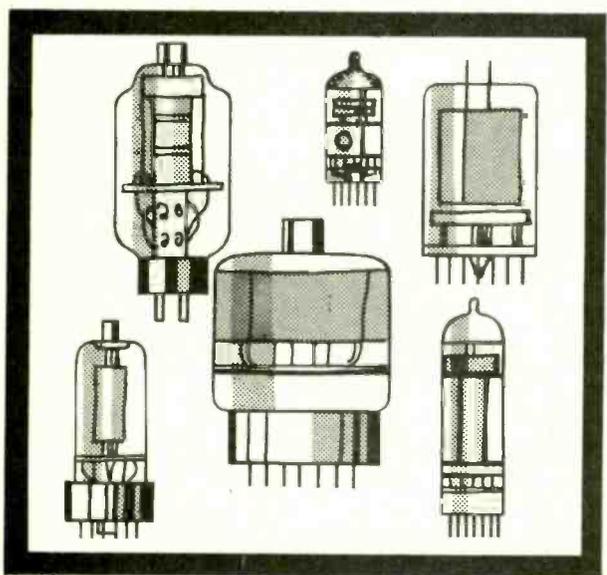
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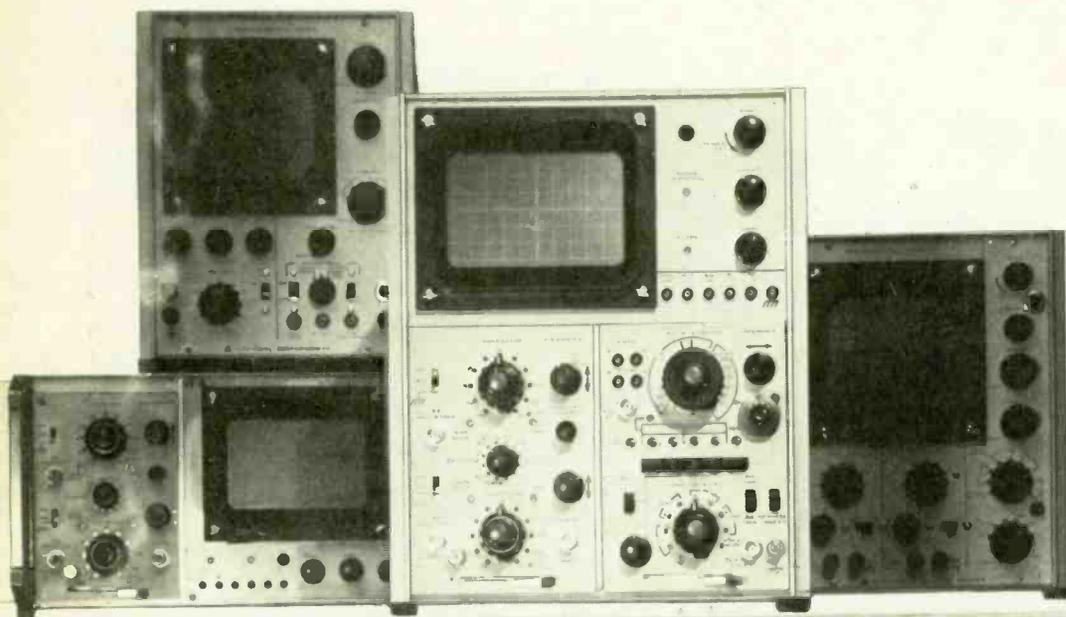
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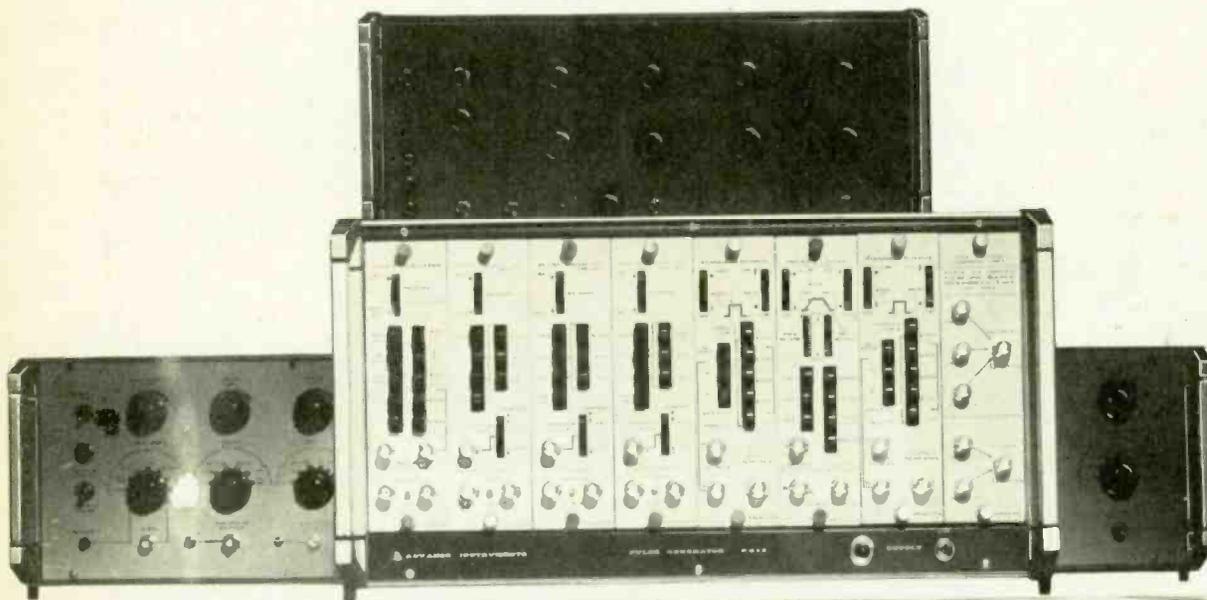
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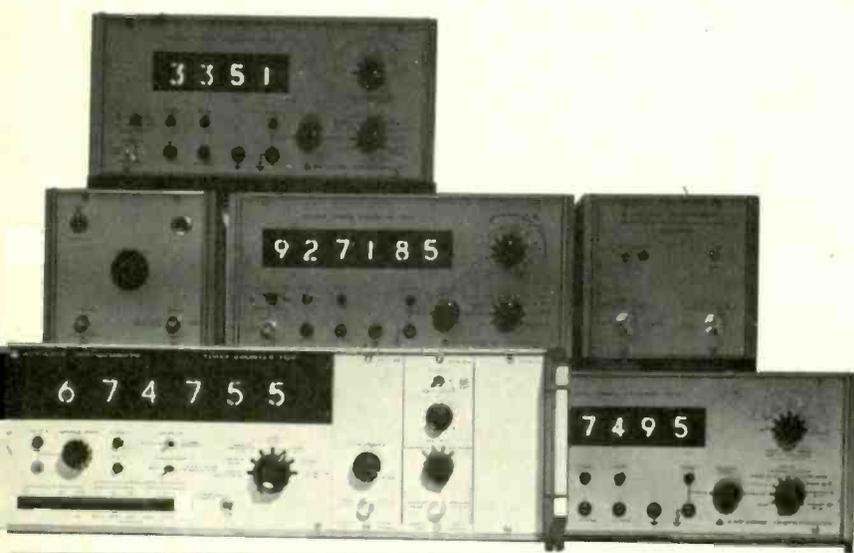
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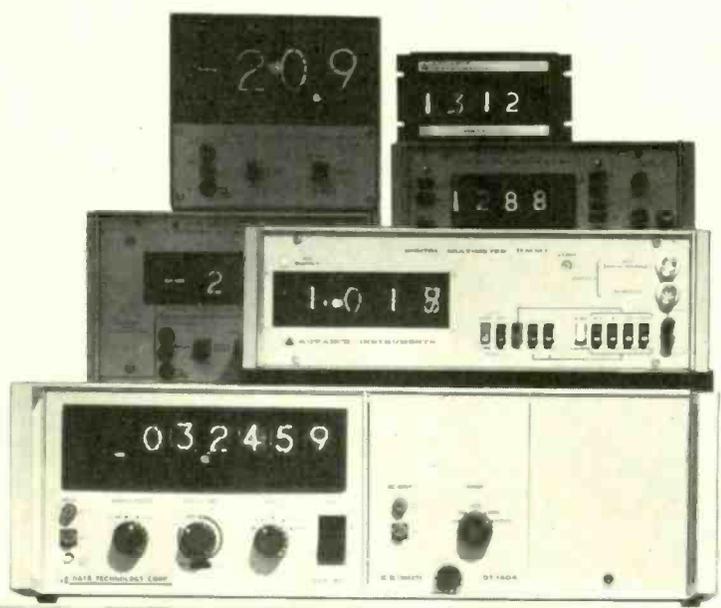
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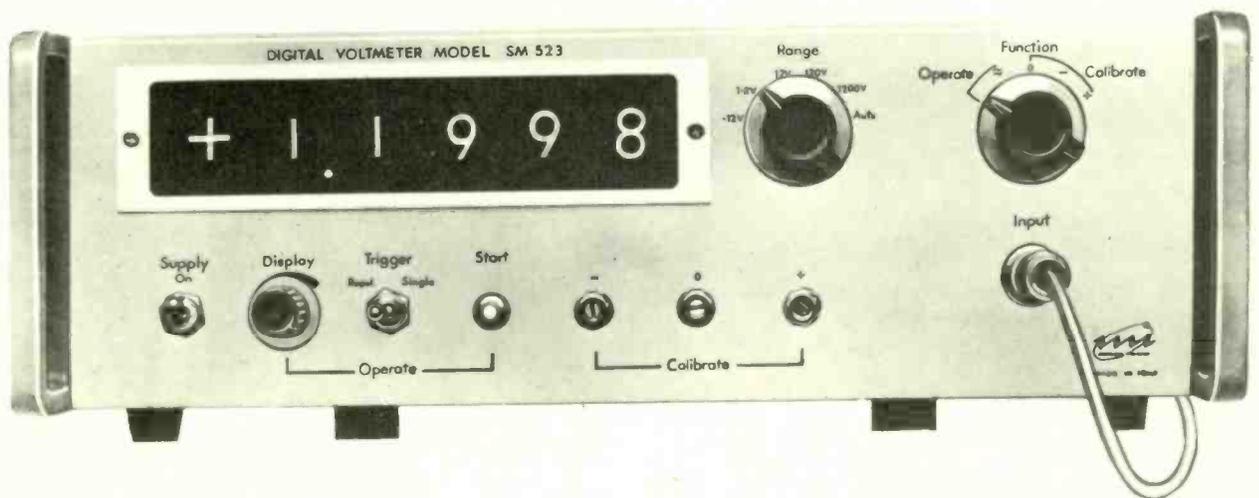
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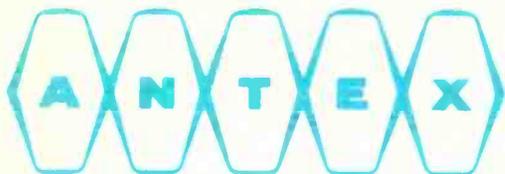
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15 watts - 240 volts

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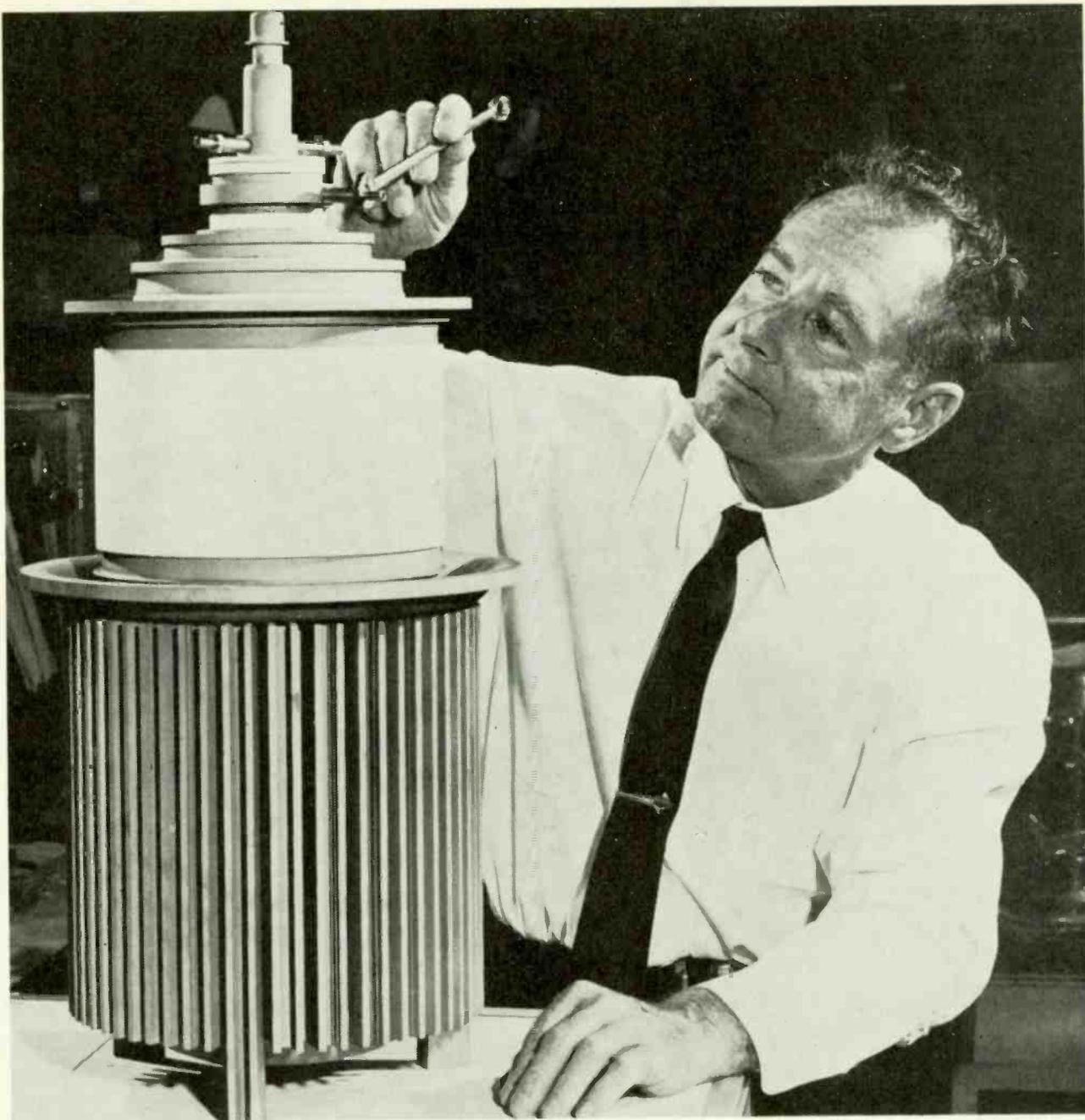
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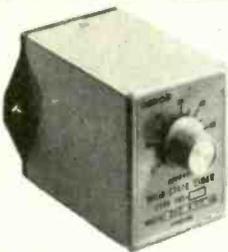
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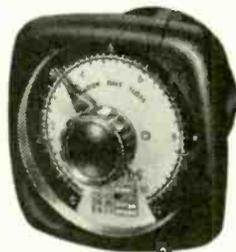
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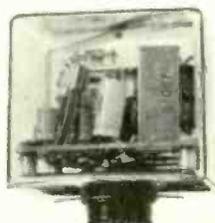
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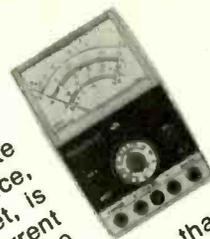
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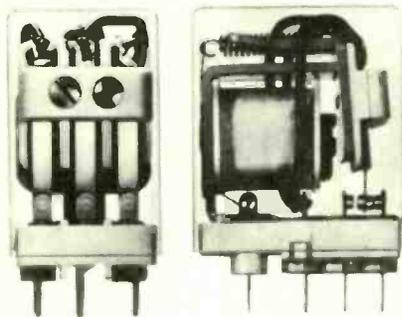
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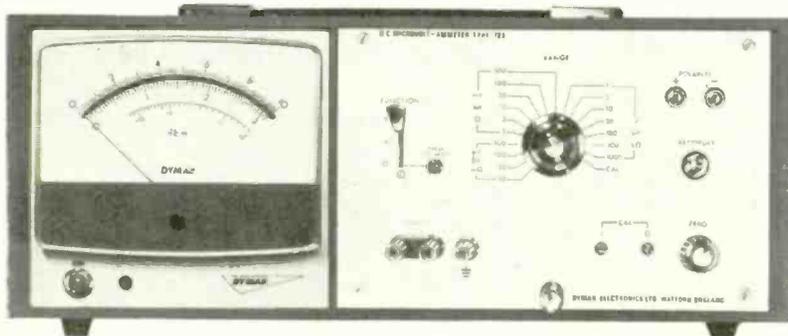
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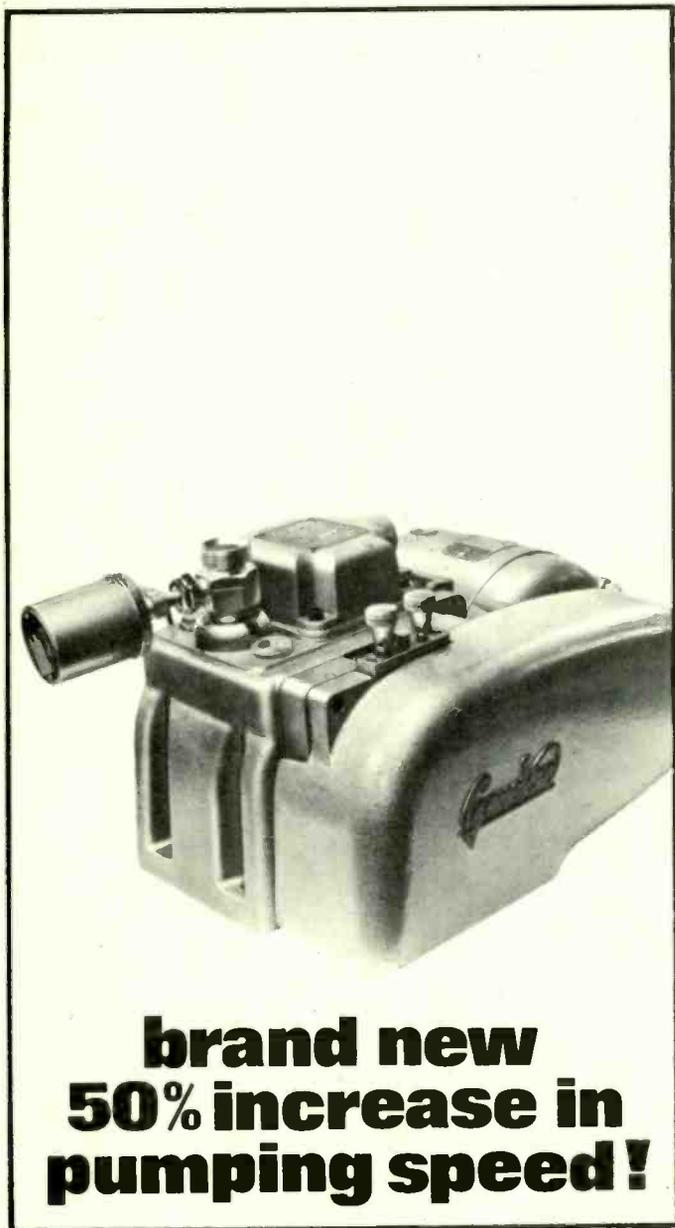
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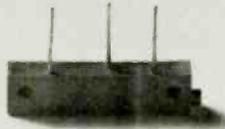


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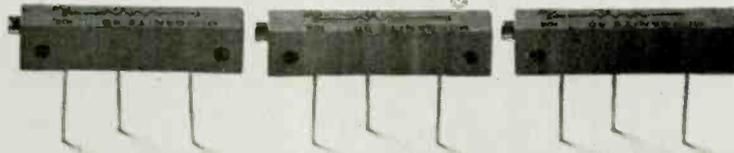
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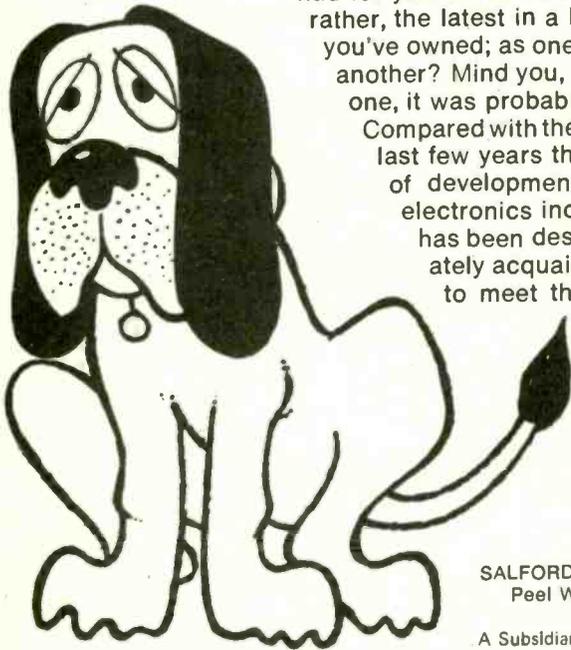
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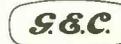
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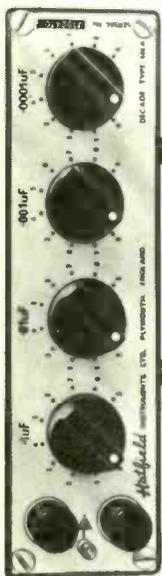
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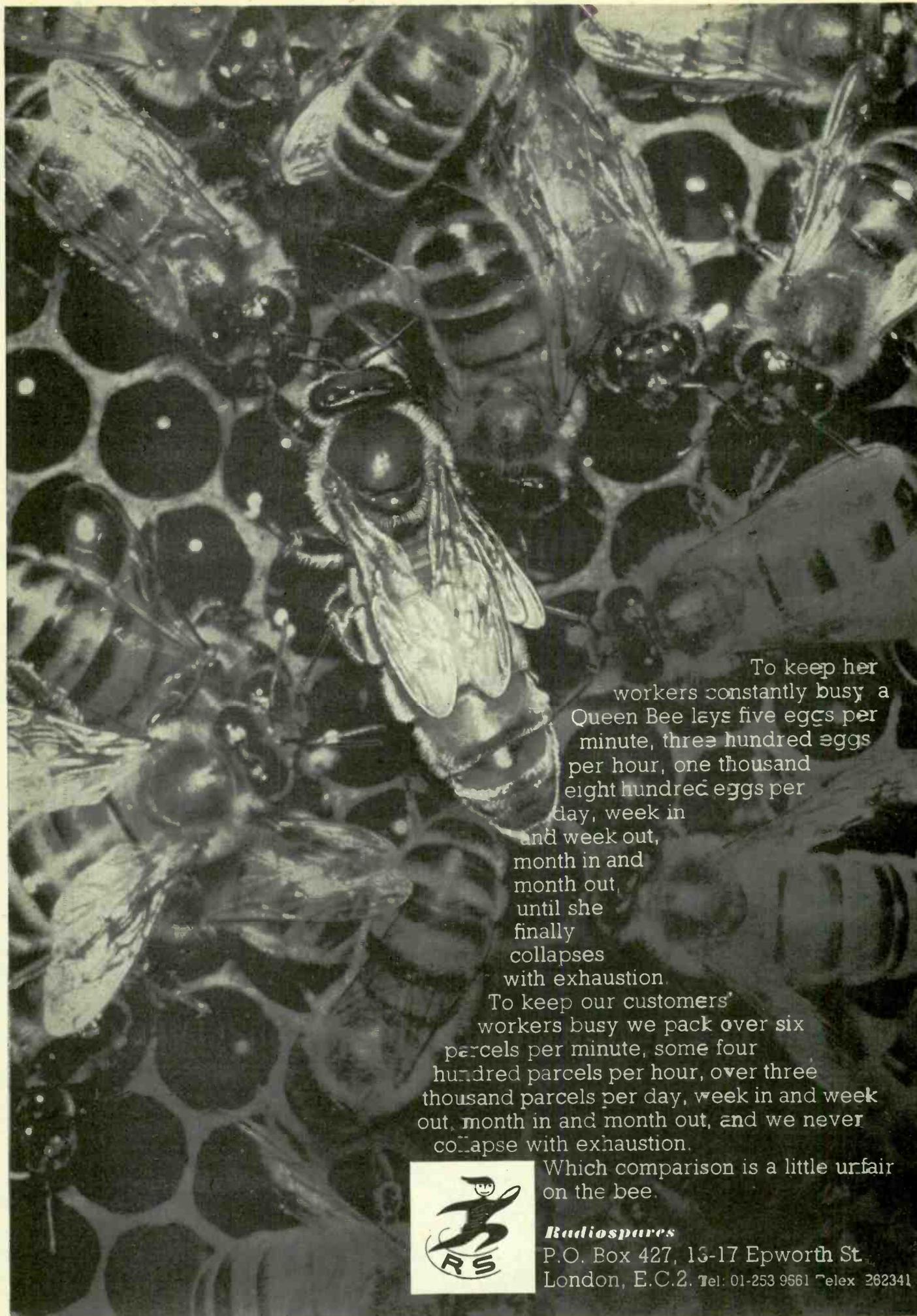
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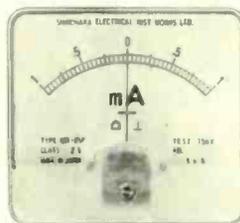
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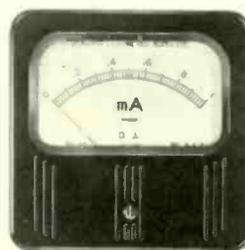
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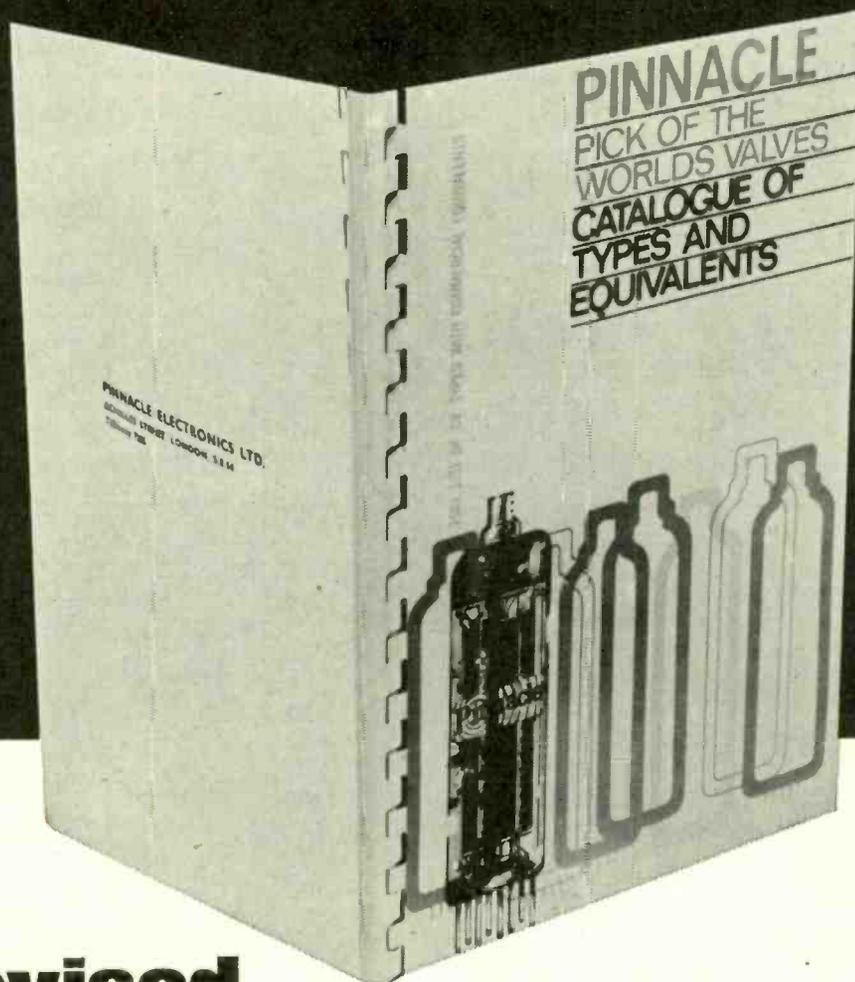
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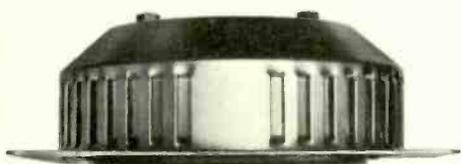
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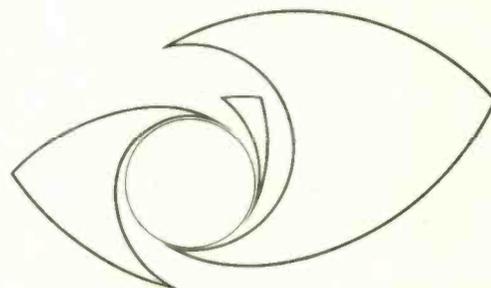
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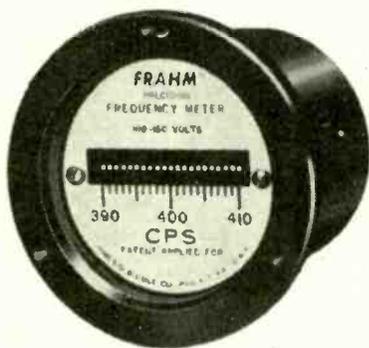
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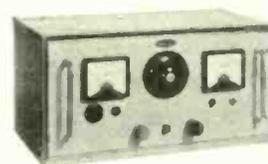
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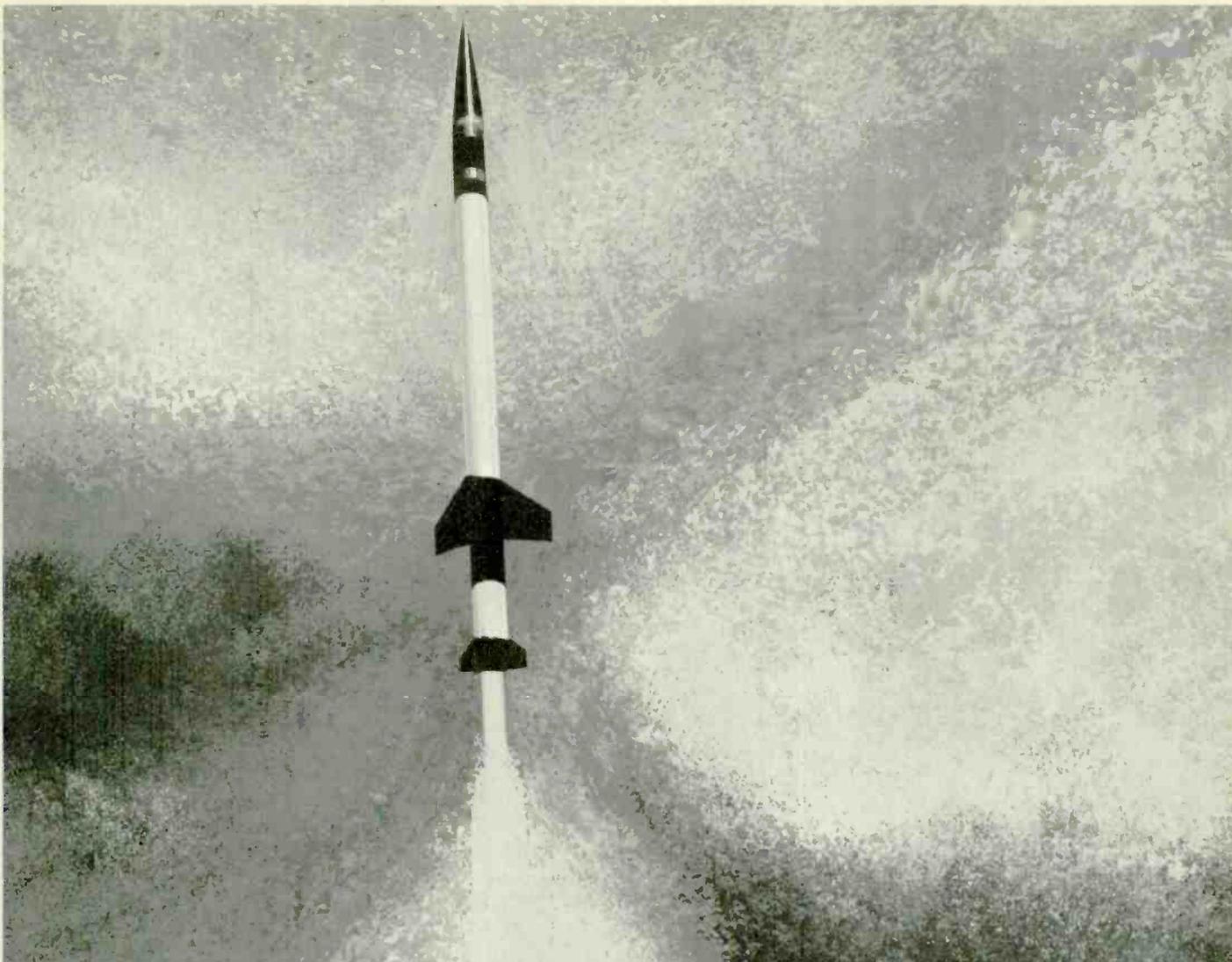
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"15" (3.81 mm) TAPE HEADS (CASSETTE)					
TRACK CONFIG.	SERIES	APPLICATION	INDUCTANCE mH		TYPE No.
			R/P	E	
1/2	W	Rec/Play Rec/Play Erase	75 65 —	— — 0-65	W12RP56* W12RP65 W12E340*
	AW	Rec/Play Rec/Play/Erase Erase	110 110 —	— 1.5 1.5	AW12RP90 AW12RPE91 AW12E360
2/2	AW	Rec/Play Rec/Play/Erase Erase	70 70 —	— 1.5 1.5	AW22RP103 AW22RPE104 AW22E366
2/4	AW	Rec/Play Rec/Play/Erase	110 70	— 1.2	AW24RP92 AW24RPE93
4/4	AW	Rec/Play Rec/Play/Erase	30 30	— 1.0	AW44RP94 AW44RPE95



AW12RP

Width .44". Height .32". Length .65". Head for .15" wide tape for Cassette Application. The mounting plate is an integral part of the head providing simple azimuth adjustment. Built in tape guides are another feature of this head. Various special Record/Play and Erase heads are made to customers own requirements.

W10RP

Various special versions of narrow track and protruding pole heads are available in the W series, for Cine and Dictating machine applications etc. Example shown is for 8 mm. Cine and is a Record/Play head having protruding pole of .02" track width.



X10RPE

An example of narrow track Record/Play/erase heads for Dictating machine application—Record/Play section .010", Erase section .014". Can be supplied in self oscillatory version if required. Erase section gives self biasing effect. Deep drawn mumetal case $\frac{1}{2}$ " x $\frac{1}{2}$ " x .55" deep provides adequate shielding.

1/4" (6.35 mm) TAPE HEADS					
TRACK CONFIG.	SERIES	APPLICATION	INDUCTANCE mH		TYPE No.
			Parallel	Series	
1/1	X	Rec/Play	1.25 7.5 27.5 162.5	5.0 30.0 110.0 650.0	X11RP26 X11RP70 X11RP25* X11RP20
		Record	1.0 6.0 20.0	4.0 24.0 80.0	X11R71 X11R72 X11R27
		Erase	— — —	0.55 2.5 8.5	X11E350 X11E316* X11E351
1/2	X	Rec/Play	1.25 7.5 17.5 27.5 162.5 250.0	5.0 30.0 70.0 110.0 650.0 1000.0	X12RP23 X12RP42 X12RP41 X12RP15* X12RP14* X12RP21
		Record	1.0 6.0 20.0	4.0 24.0 80.0	X12R73 X12R74 X12R16*
		Rec/Play/Erase	R/P — E —	200.0 0.5	X12RPE107
	BX	Rec/Play	1.25 7.5 30.0 140.0	5.0 30.0 120.0 560.0	BX12RP75 BX12RP76 BX12RP77* BX12RP63*
		Erase	— — — —	0.4 1.75 2.5 6.0	BX12E356 BX12E357 BX12E343* BX12E358 BX12E344*
					3 mA D.C.

XC28RP

$\frac{1}{2}$ " x $\frac{1}{2}$ " x .55" deep drawn mumetal case. This type of head is for 8 tracks on $\frac{1}{2}$ " tape. Movement of the head across the tape is used to achieve this result. Cross talk figure better than -70 dB's is obtained with this arrangement. Can be supplied in variety of inductances to customers own requirements.



X24RP

Standard "X" series Head in deep drawn mumetal case $\frac{1}{2}$ " x $\frac{1}{2}$ " x .55". For use in high quality tape recorders and available in a wide range of inductances. Excellent high frequency performance, efficient screening, very low cross talk. Over a million and a half of these heads have been manufactured.



X12RPE107

$\frac{1}{2}$ " x $\frac{1}{2}$ " x .55" deep. 1/2 track combination head for applications such as telephone answering machines. Particularly useful where head space is limited. Overcomes any problems of alignment of Erase to R/P tracks. Deep drawn mumetal case offers perfect screening. Other impedances are available to customers requirements.



BX Series

A new series of Record/Play head in $\frac{1}{2}$ " x $\frac{1}{2}$ " x .55" deep mumetal case. This type has been developed particularly as a replacement for $\frac{1}{2}$ " square heads commonly used on various tape recorders of the more mass produced variety. Lower priced than the X series. An Erase head of similar size is available in deep drawn brass case.



WW-058 FOR FURTHER DETAILS

DR Series

.437" x .437" x .625" depth in die-cast body with nickel silver front provided with fixing holes for PK screws. The R/P head has internal mumetal screen. The Erase head is double gap, double field variety. The cheapest series of heads made by Marriott Magnetics. An improved design of the first mass produced head to be made in the world in 1957 by our company.



R Series

Size of the front .437" x .437" with 3/8" body diameter and 3/8" long. This head is available in a wide range of Record/Play Impedances electrically similar to DR type. Head body is made in brass and has internal mumetal screens. Offers special advantages for easy mounting and azimuth adjustment. Erase heads, electrically as DR series, are available.



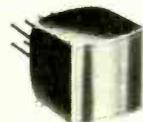
A12RP

3/8" diameter, 3/8" long. Standards available are for 1/2 track configuration but many special versions can be made such as narrow track, protruding poles, cut away edge for cine use etc. The round body makes for easy azimuth adjustment and takes up a minimum of space. The head incorporates an internal screen and flying leads. Special versions are available with ferrite poles for drum applications.



X24RPE

Combination Record/Playback/Erase head in deep drawn mumetal case 1/2" x 1/2" x .55" deep. Particularly useful where head space is limited. Combination arrangement ensures correct alignment of Erase tracks to Record/Play tracks. Available in various impedances other than those listed.



X24E

This 2/4 stereo head size 1/2" x 1/2" x .55" deep is a companion to all X series Record/Playback heads and is available in a wide range of impedances. It is a highly efficient double gap erase head which leaves the tape with a very low noise level after erasure.



CX88RP

This remarkable head built into a standard deep drawn mumetal case 1/2" x 1/2" x .55" deep gives 8 track Record/Playback facilities on 1/2" tape. Marriott Magnetics are once again the first Company in the world to quantity produce such heads and at prices not previously thought possible. Possibilities now created for digital data collection etc., utilising 1/2" tape transport mechanisms. Already being fitted to various Cassette systems in the U.K. The 4/8 version offers low enough crosstalk figures for audio applications.



T10RPE

Dimensions .5" by .3" by .55" length. Example of a protruding pole type of head with special narrow track developed for Dictating Machines. Example shown is a Record/Playback/Erase head of self oscillatory variety and each section incorporates a transformer coupling so that DC can be passed direct through the head. Mumetal shielded case and fully screened leads.



A new series of narrow width Erase heads (not illustrated) will shortly be available for mounting alongside standard X series Record/Replay heads. Width of these heads is only .16"

*Types produced in large quantities and usually held in stock.

1/4" (6.35 mm) TAPE HEADS contd.					
TRACK CONFIG.	SERIES	APPLICATION	INDUCTANCE mH		TYPE No.
			Rec/Play	Erase	
1/2	DR	Rec/Play	5.0	—	DR12RP50
			30.0	—	DR12RP43
			70.0	—	DR12RP45
			110.0	—	DR12RP33
			250.0	—	DR12RP35
	650.0	—	DR12RP31		
	DR	Erase	—	0.2	DR12E354
			—	1.5	DR12E301
			—	2.5	DR12E305
			—	3.0	DR12E355*
—			7.0	DR12E307*	
R	AVAILABLE IN ALL DR TYPES				
A	Rec/Play	2.25	—	A12RP37	
		5.0	—	A12RP98	
		30.0	—	A12RP99	
		70.0	—	A12RP100	
A	Erase	—	0.15	A12E364	
		—	0.7	A12E365	
		—	1.25	A12E330*	
		—	—	—	
2/2	X	Rec/Play	5.0	—	X22RP80
			30.0	—	X22RP81
			110.0	—	X22RP46*
	X	Record	4.0	—	X22R82
			24.0	—	X22R83
			80.0	—	X22R48*
X	Erase	—	.56	X22E341	
		—	1.4	X22E359	
		—	2.5	X22E333*	
—	5.0	X22E336			
1/4	X	Rec/Play/Erase	180.0	1.0	X14RPE55
2/4	X	Rec/Play	4.0	—	X24RP24
			30.0	—	X24RP30*
			70.0	—	X24RP36*
			110.0	—	X24RP18*
	X	Record	4.0	—	X24R84
			15.0	—	X24R44
			30.0	—	X24R85
			100.0	—	X24R49*
	X	Rec/Play/Erase	110.0	1.0	X24R28
			—	—	X24RPE108
X	Erase	—	0.5	X24E332A	
		—	0.2	X24E342*	
		—	1.0	X24E311*	
		—	5.0	X24E335	
4/4	X	Rec/Play	110.0	—	X44RP105
		Rec/Play/Erase	110.0	1.0	X44RPE106
1/8 2/8 4/8 8/8	CX	Rec/Play	30.0	—	CX18RP86
			30.0	—	CX28RP87
			30.0	—	CX48RP88
			30.0	—	CX88RP89
T	Rec/Play	85.0	—	T10RP53	
		40.0	Self Osc.	T10RPE54	
		100.0	—	T10P60	
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1/2" (12.7 mm) and 1" (26.4 mm) TAPE HEADS

Marriott Magnetics have hitherto concentrated principally on special versions of such heads to customers own requirements. We are about to embark on producing a standard range of heads for 1/2" and 1" tape. We would like to hear of your own requirements in this field. Our prices will be considerably lower than any other to be found in the world, in view of the quantities we intend to produce.

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Celestion PA

Loudspeakers for all Public Address Systems

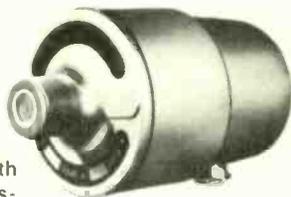


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These Horns are capable of delivering a highly concentrated beam of sound over long distances. They are recommended for recreation centres, noisy factories and workshops and all indoor and outdoor locations where a high noise level has to be overcome.

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Pressure type units are available with or without tapped 100V line transformers. The following 'built-in' features are on all models—High Sensitivity, Weatherproof, Phase Equalising Throat and Self-centring Diaphragm Assembly.



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Rola Celestion re-entrant loudspeakers are designed for use wherever conditions demand compactness, toughness, high efficiency and unfailing service. They are rainproof and built to withstand prolonged exposure to vibration and adverse conditions.

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The Celestion Glass Fibre Loudspeaker is a compact robust and watertight unit, precision built for use on open boat decks, docks, chemical plants, plating shops, etc, where protection from the weather or corrosive atmosphere is vital.



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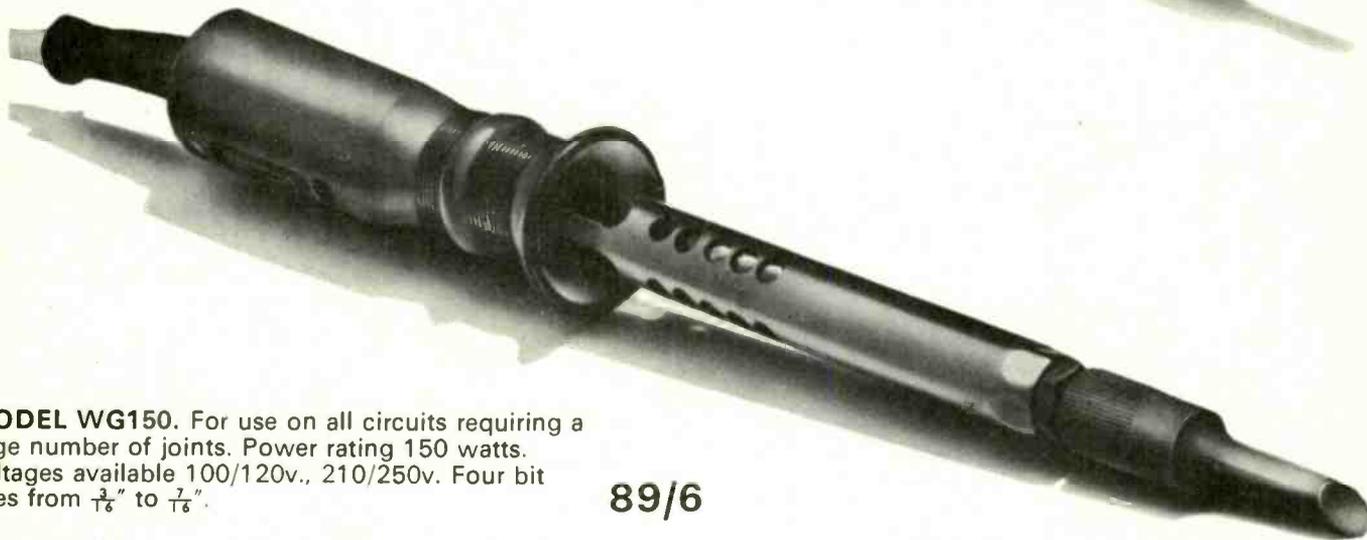
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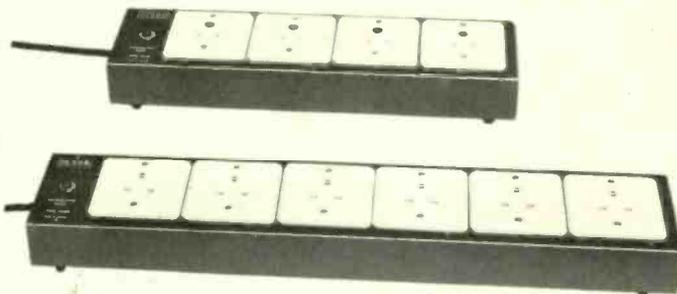
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Type	Width Dim. A	Height Dim. B	Depth Dim. C	Type	Width Dim. A	Height Dim. B	Depth Dim. C
	inches	inches	inches		inches	inches	inches
25A	6½	4½	4½	61	15½	7½	9½
25B	6½	4½	6½	62	17½	8½	9½
26A	8½	5½	6½	63	16½	9½	9½
26B	8½	5½	8½	64	15½	7½	12½
27A	12½	7½	5½	65	17½	8½	12½
27B	12½	7½	8	66	16½	9½	12½
28A	14	10½	6½	75A	12½	5	6½
28B	14	10½	8½	75B	12½	5	9
29A	10	4	6	76A	12½	7½	6
29B	10	4	8	76B	12½	7½	9
30A	12	5	6	77A	14½	6	6½
30B	12	5	8	77B	14½	6	9
31A	14	6	6	81	4	4	6½
31B	14	6	8	82	5	5	8
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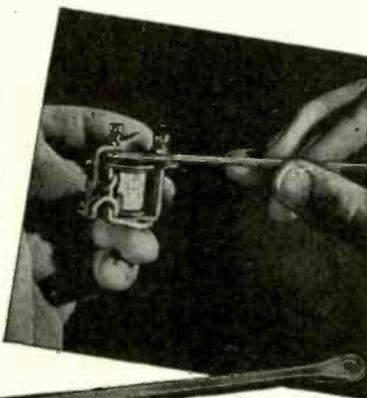
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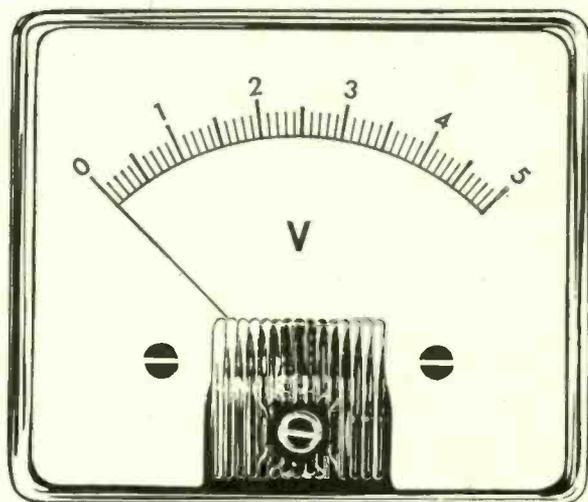
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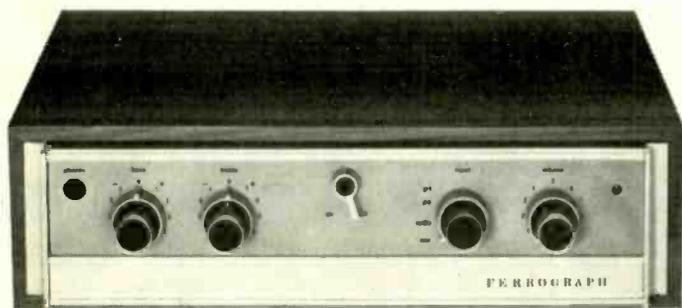
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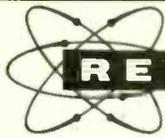
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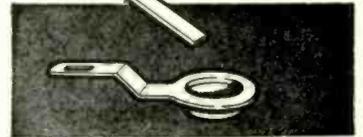
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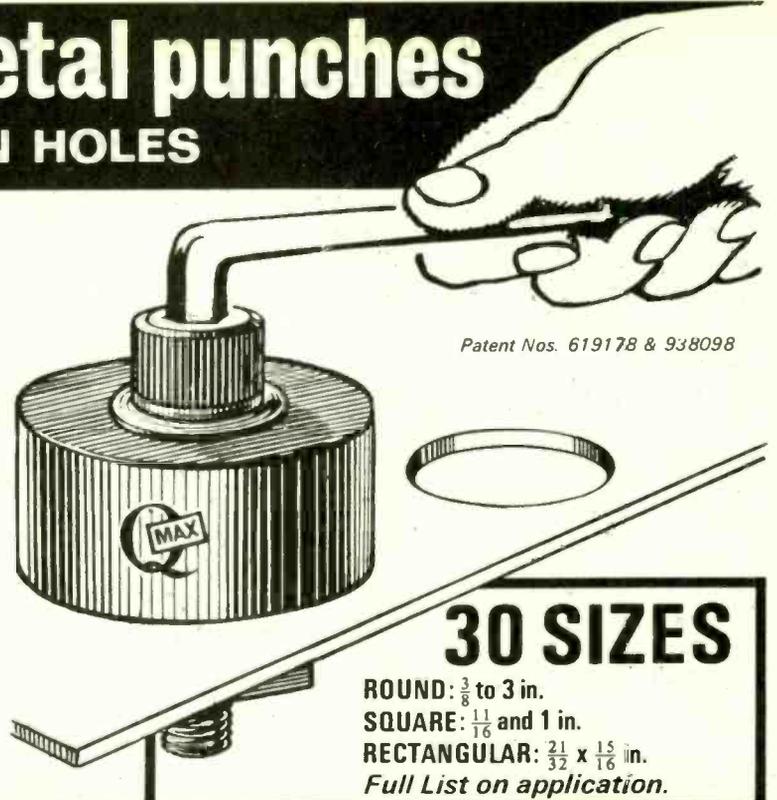
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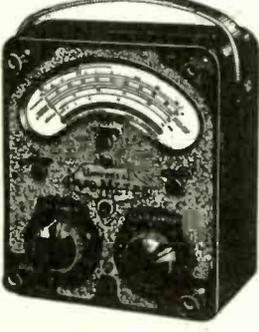


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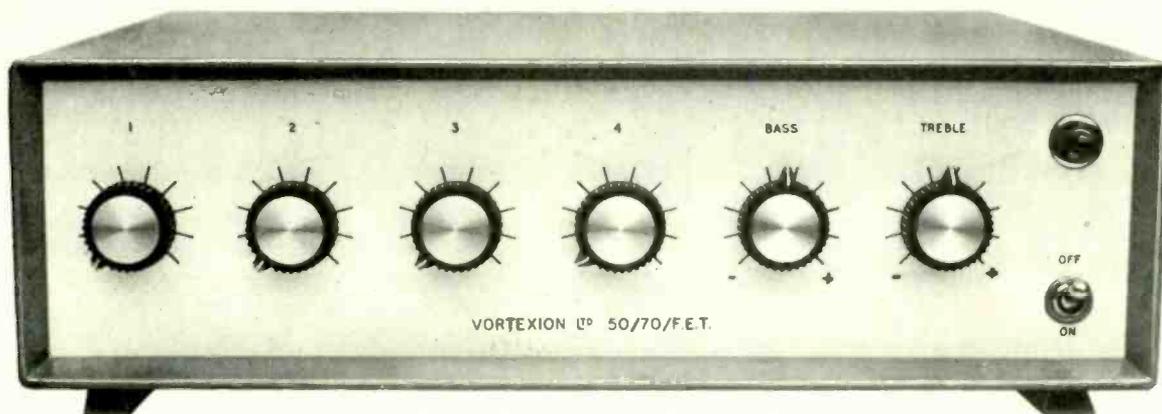
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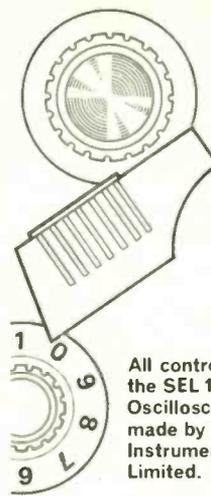
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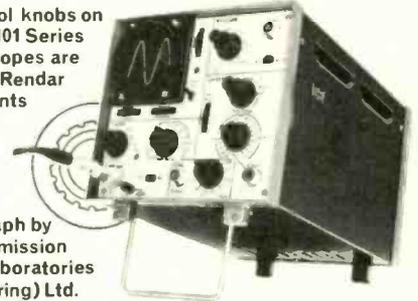
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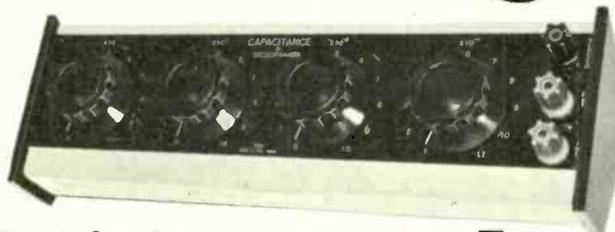
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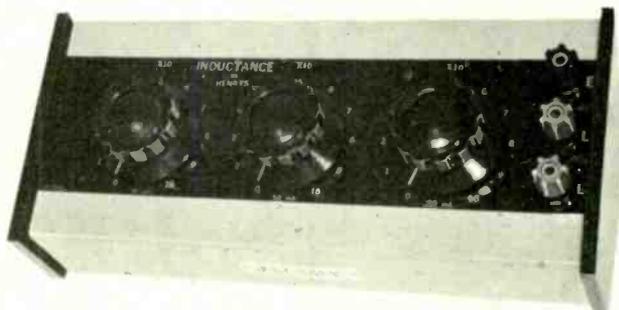
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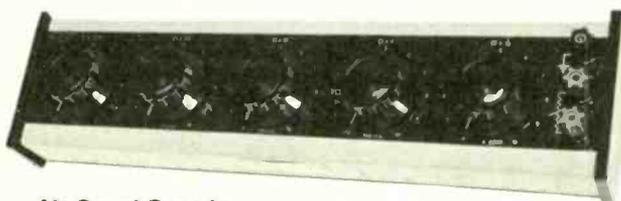
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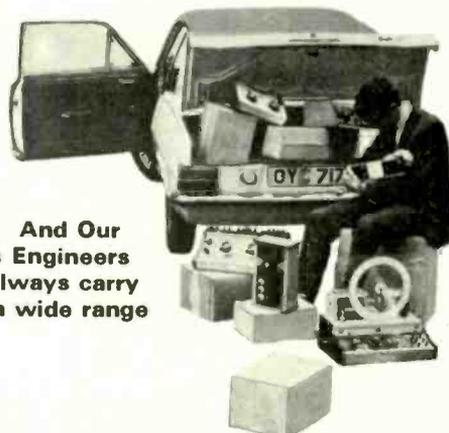


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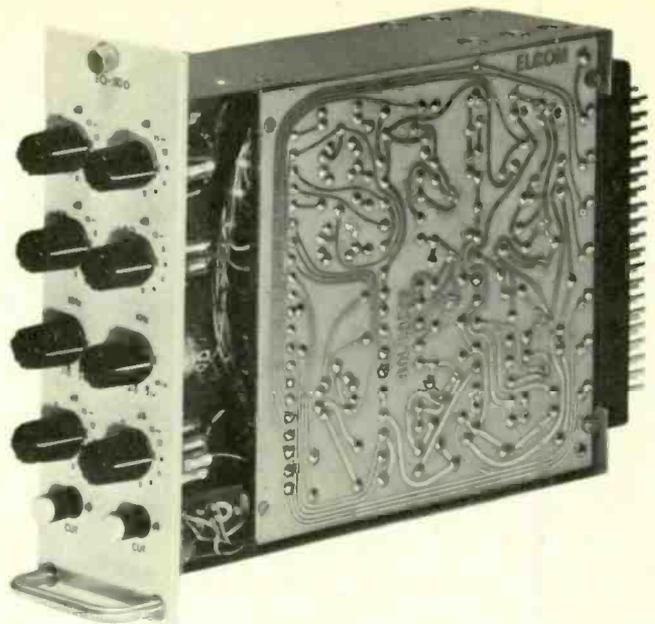
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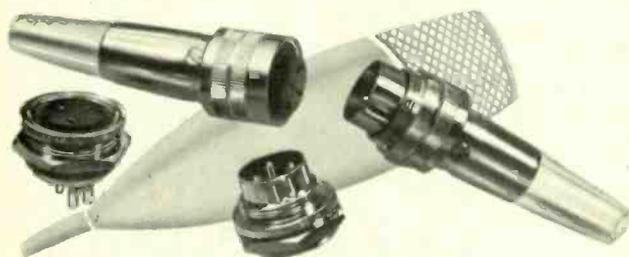
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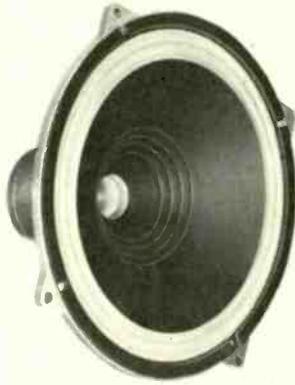
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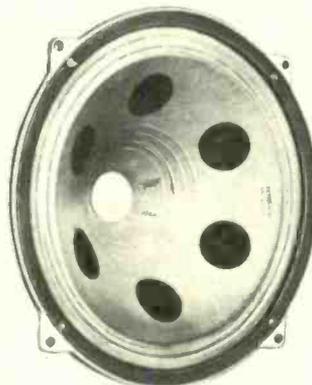
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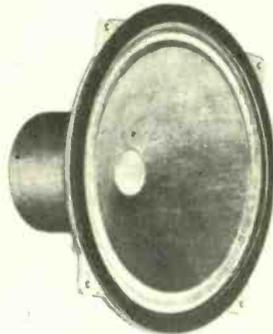
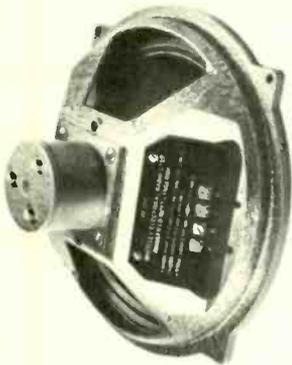
HF.1016

HF.1012

HF.816

T816

P2.585



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	Depth	Dia.								lb.	oz.	
HF.816	4.218"	8"	16,000	1.0	63,000	U	6	63	50—15 K	4	8	£8.15.0
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HF.1016	4 1/8"	10"	16,000	1.0	63,000	U	10	35	30—15 K	5	13	£10.4.2
HF.1016 Major	5 1/4"	10"	16,000	1.0	63,000	15	10	39	30—16 K	6	0	£13.1.11
HF.1214	6 1/2"	12"	14,000	1.5	106,000	15	15	39	25—14 K	9	10	£14.0.7
HF.1216	7 1/2"	12"	16,000	1.5	121,140	15	15	37	20—16 K	13	0	£21.10.3
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P2.585	1 1/2"	2 1/2"	8,500	0.375	6,400	3	0.3	330	250—9 K	—	3	£1.10.6

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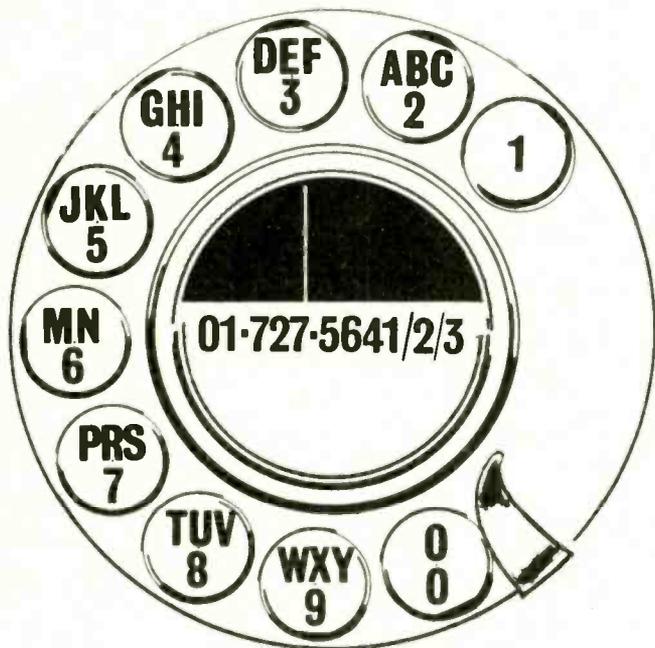
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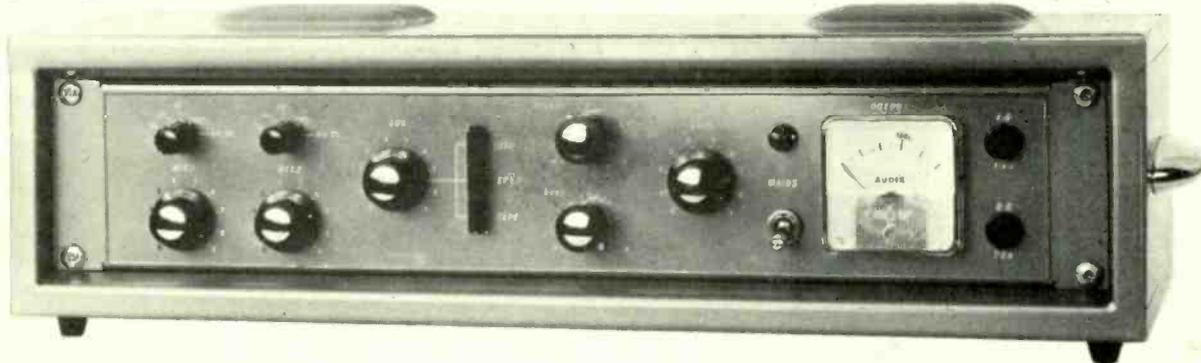
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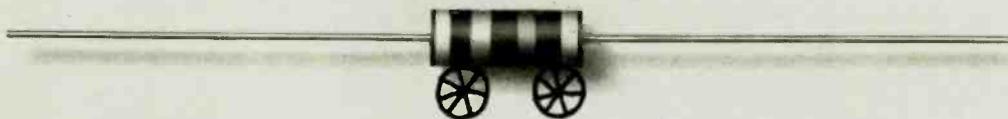
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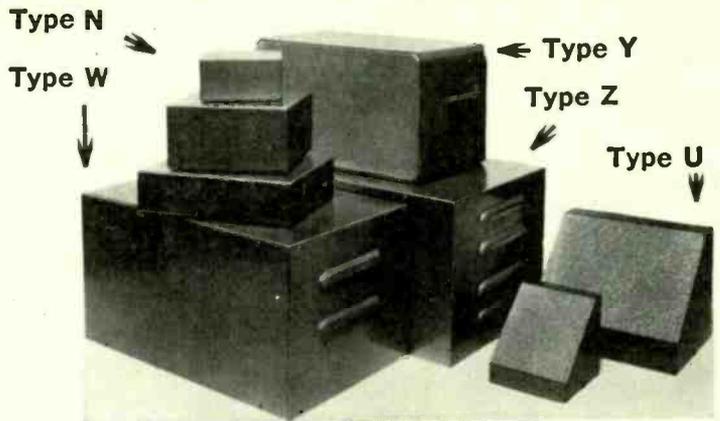
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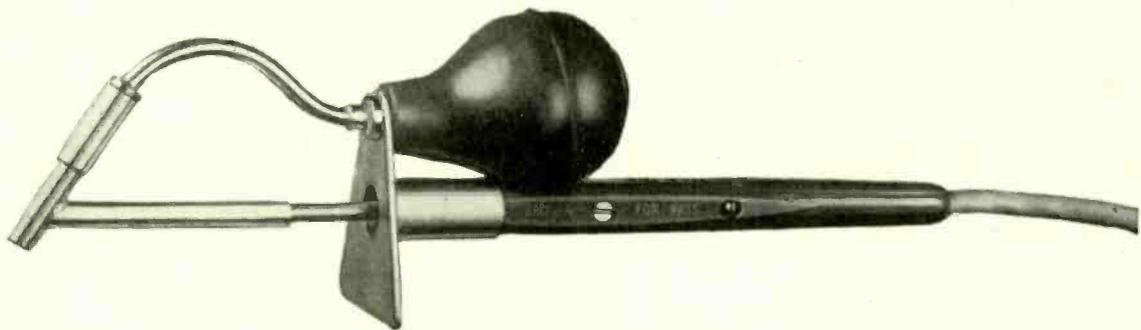
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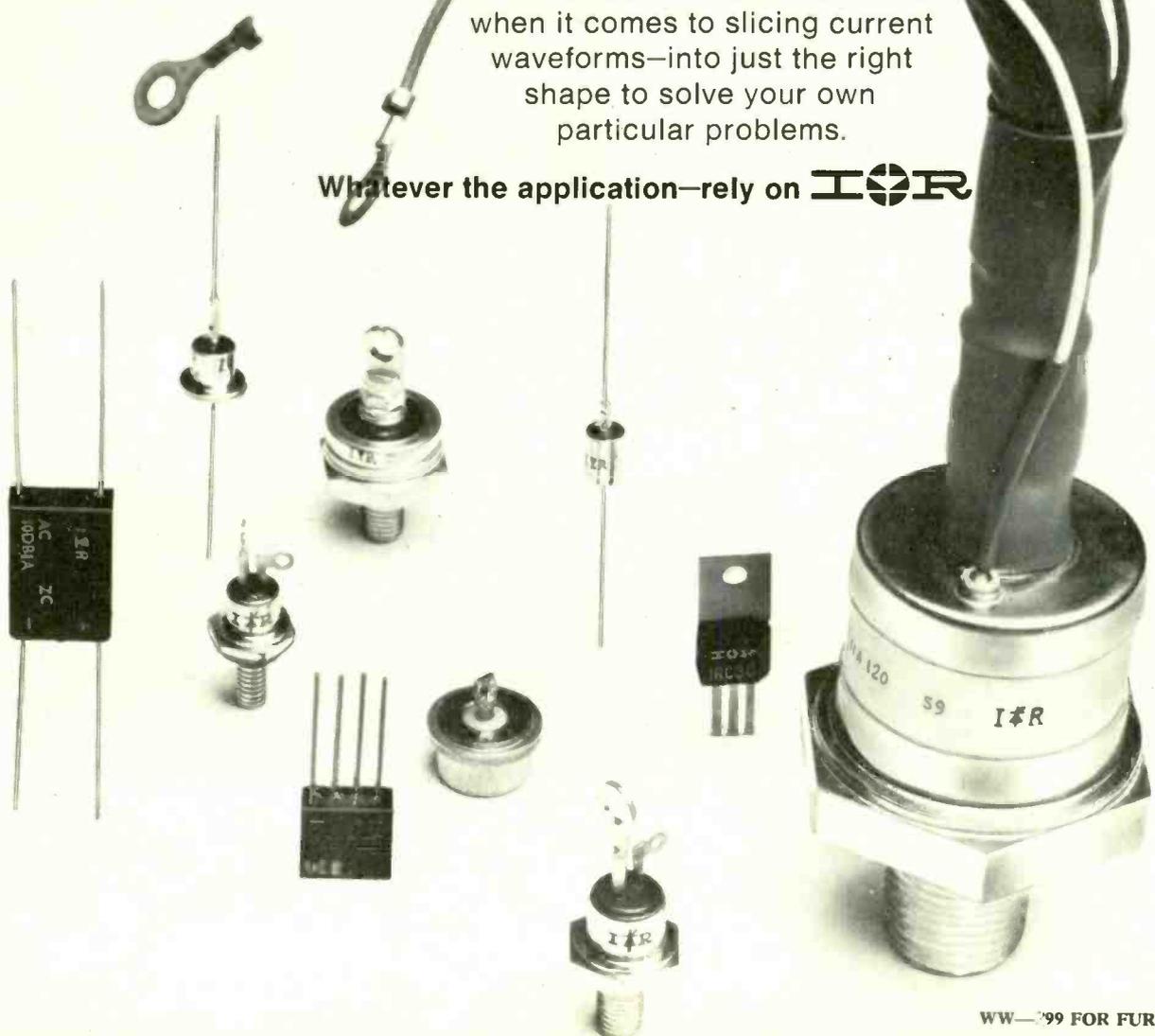
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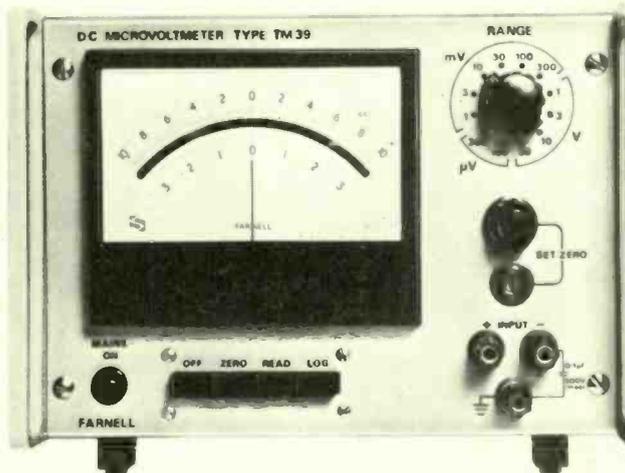
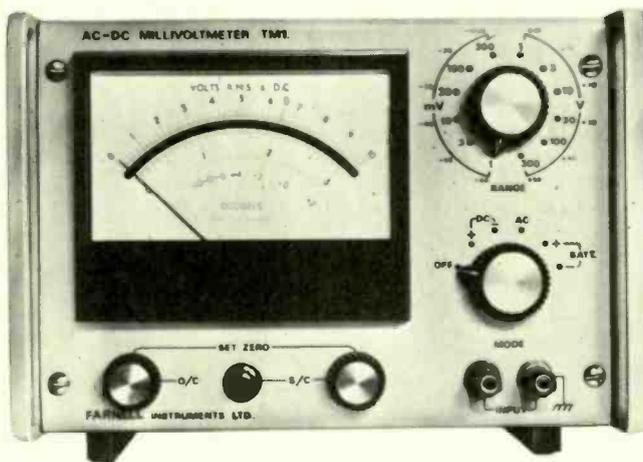
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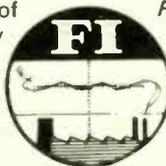
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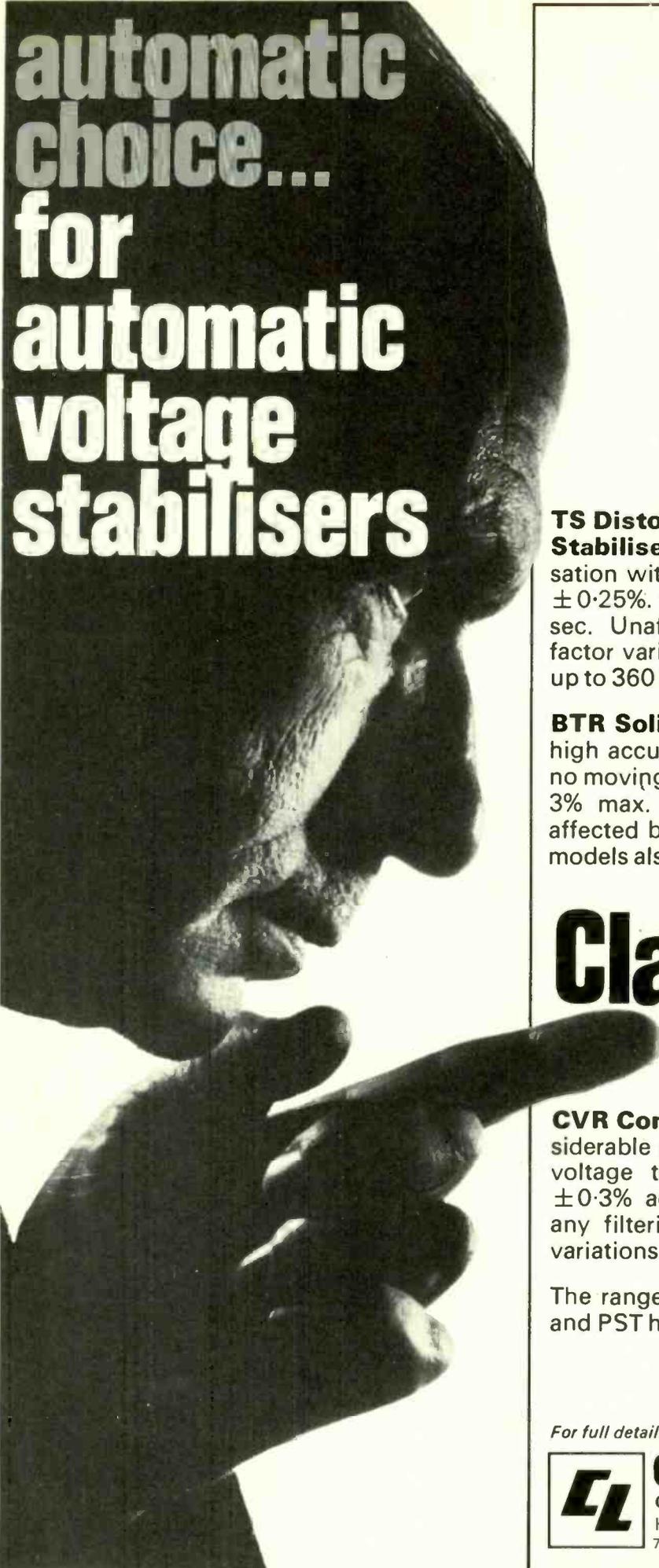
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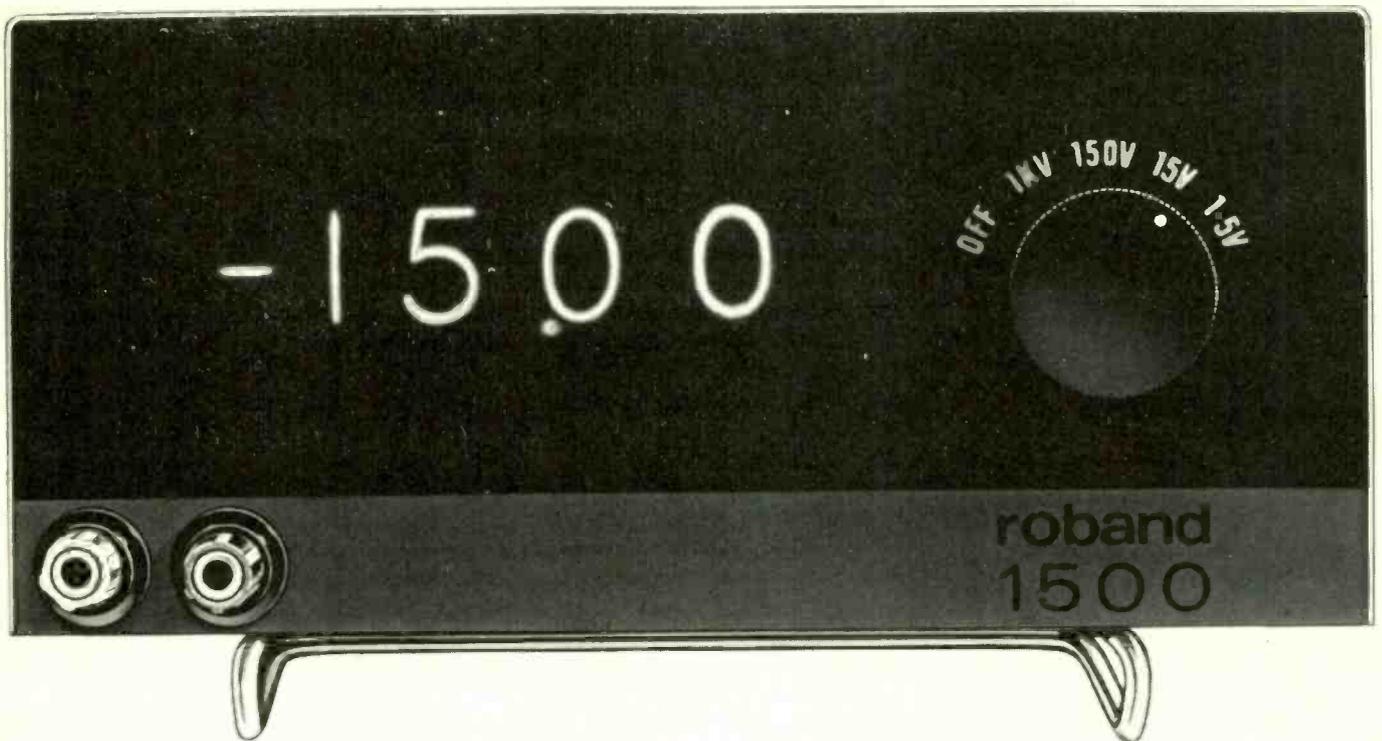
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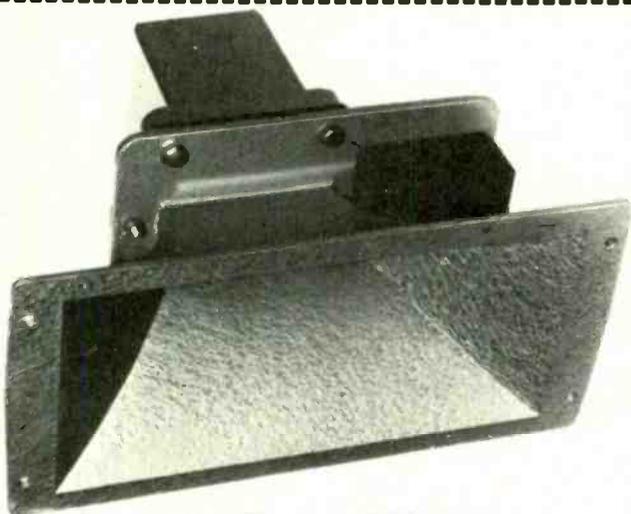
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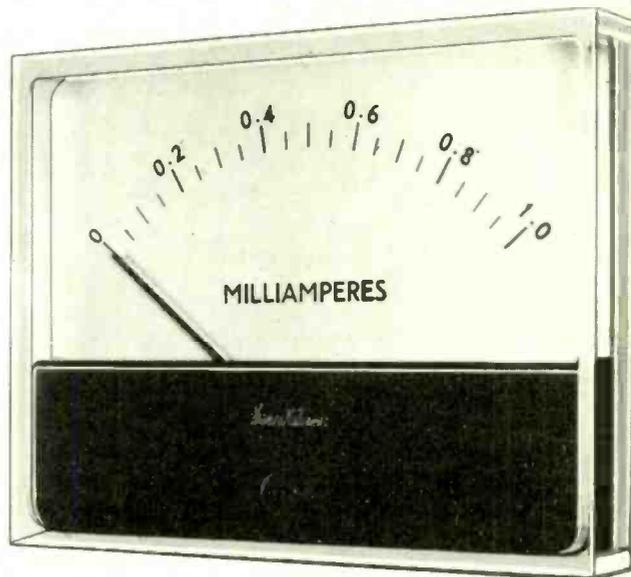
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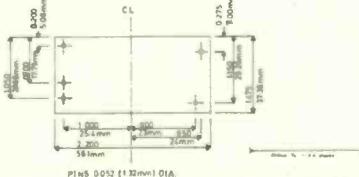
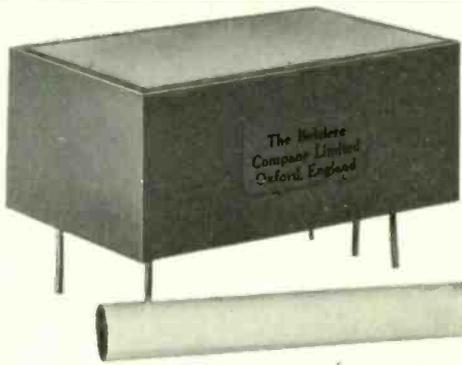
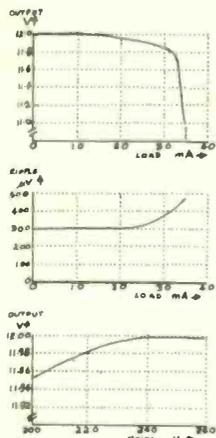
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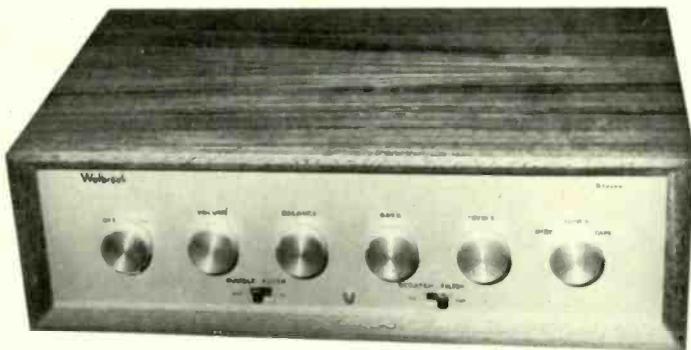
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basis of your first low-cost installation. This is unique flexibility—means you can build up your own application-matched system of Ampex videotape recorders. You get maximum benefit from Ampex professional broadcasting techniques, and ease of operation over a vast range of 'instant-replay' uses. Think. Couldn't there be a place for Ampex in your professional life?



VR-5103 Videotape Recorder. Basic Price: £856
 (Above) the basic low cost recorder in the range offers a better picture than any other in its price range needs minimum operator training its tapes play back on VR-7003, VR-7803 and vice-versa 5-minute forward and reverse spooling remote control facilities for play, record and stop high-quality audio response built-in amplifier and speaker weight only 65 lbs.

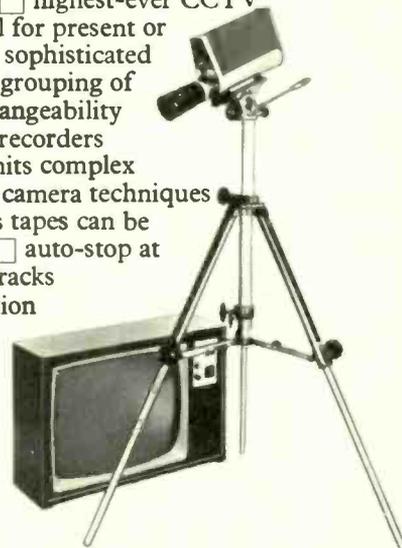


VR-7003 Videotape Recorder. Basic Price: £1,440
 This recorder (below) out-performs more costly equipment minimal operator training interchangeable with other Ampex CCTV recorders high-quality audio response built-in amplifier and speaker audio can be added after picture has been recorded second audio channel for cue purposes is optional extra slow-motion —2 to 20 fields per sec is also optional.



VR-7803 Videotape Recorder. Basic Price: £4,650
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Video Tape Recommended for all Ampex CCTV recorders—high quality 1-inch 1-mil polyester base (Ampex 161 series) 3,000 ft for 1 hour on 9 $\frac{3}{4}$ " reel.

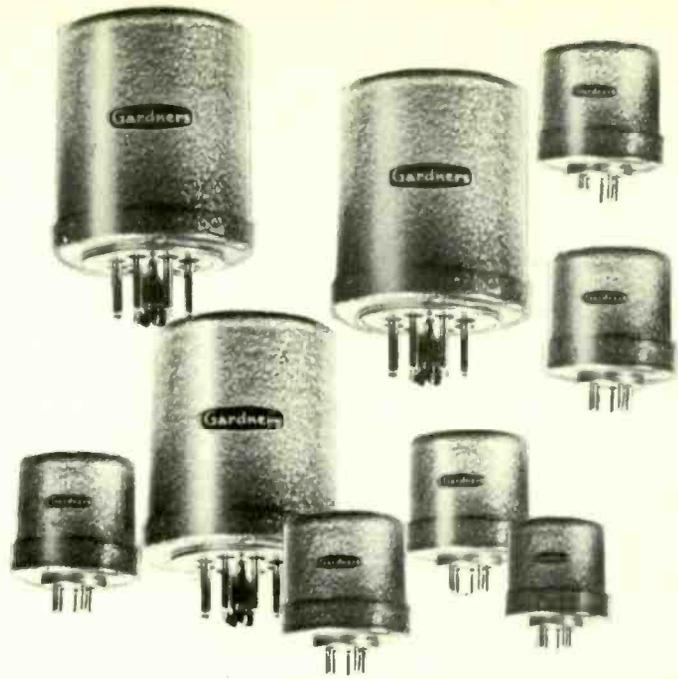


For a special presentation kit detailing all Ampex recorders and applications in your field, write to: AMPEX GREAT BRITAIN LTD., Dept. WW2, 72 Berkeley Avenue, Reading, Berks. Tel: 844111

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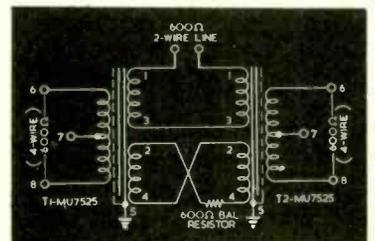
For professional recording and broadcast transmission equipment, these Octal-based plug-in transformers have a frequency response extending well beyond the audio range. The design achieves dynamic performance with minimum distortion at all levels

Type No.	Input Z Ohms	Pin Nos.†	Output Z Ohms	Pin Nos.	Sec./Pri. Turns Ratio	Applications
MU.7521	3.75/15*	1-3, 2-4	600 (C.T.)	6-7-8	6.32:1/12.64:1	Low Z. Mic/Line
MU.7522	3.75/15*	1-3, 2-4	100K.	6-8	82:1/164:1	Low Z. Mic/Grid
MU.7523	75/300*	1-3, 2-4	600 (C.T.)	6-7-8	1.41:1/2.82:1	Line/Line
MU.7524	150/600*	1-3, 2-4	600 (C.T.)	6-7-8	1:1/2:1	Mixing: Bal./Unbal.
MU.7525	600 (C.T.)	6-7-8	300/1.2K*	1-3, 2-4	1+1:1.41 (C.T.)	Mixing: Hybrid‡
MU.7526	600 (C.T.)	6-7-8	2.5k/10k.*	1-3, 2-4	2.04:1/4.08:1	Line/Grid
MU.7527	150/600*	1-3, 2-4	100K.	6-8	13:1/26:1	Line/Grid
MU.7528	7.5/30*	1-3, 2-4	600 (C.T.)	6-7-8	4.47:1/8.94:1	Low Z. Mic./Line
MU.7529	50/200*	1-3, 2-4	600 (C.T.)	6-7-8	1.73:1/3.46:1	Mic. or Line/Line
MU.7530	10K. (C.T.)	6-7-8	10K.	1-4	1 (C.T.):1	600 Line Bridging
MU.7532	7.5/30*	1-3, 2-4	100K.	6-8	58:1/116:1	Low Z. Mic./Grid
MU.7534	50/200*	1-3, 2-4	100K.	6-8	22.4:1/44.8:1	Mic. or Line/Grid

Type MU.7525 may be used in "Hybrid" circuits, as shown, to establish 2 to 4 wire operation in telephony. Accurate balancing of the windings enable guaranteed rejection of better than — 55 dB from 50 c/s to 10 kc/s. Up to — 75 dB may be expected for normal rejection levels.



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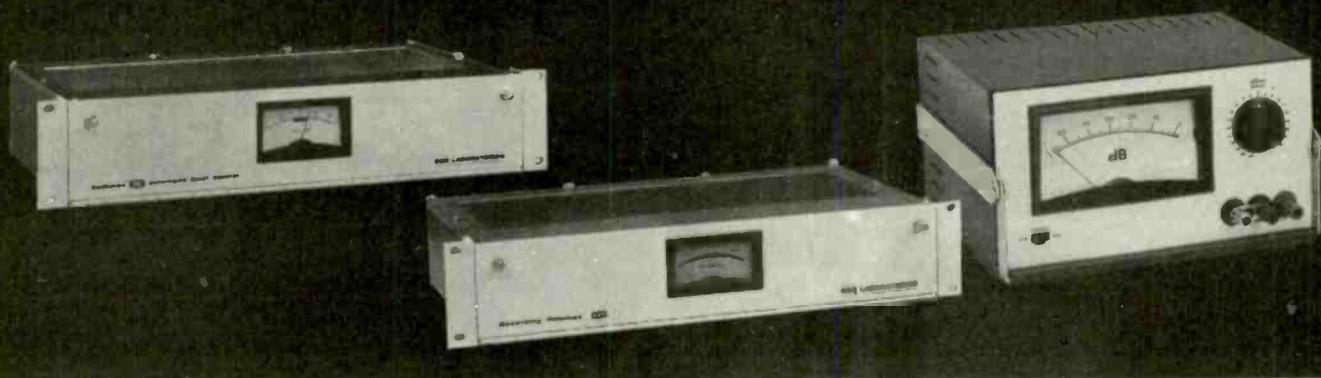


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How to record on a higher level



With automatic level control

Unconditionally guaranteed to outperform ordinary compressors, limiters or AGCs, the solid-state Audimax III offers the ultimate in automatic level control for recording engineers.

The exclusive **Gain Platform** principle permits gain to remain on a stable plateau over a wide range of input levels rather than the continuous rise and fall—with consequent distortion, thumping and pumping, and audio “holes”—so frequently encountered with ordinary AGC amplifiers. Its unique **Gated Gain Stabilizer** acts to bridge through program lapses and thus eliminates “swish-up” of background noise. A special **Return-to-Zero** feature returns gain to normal during standby conditions. In short, the Audimax reacts to any gain situation in exactly the same manner as a human engineer—but more efficiently. (Stereo model also available).

With automatic peak control

CBS Laboratories presents its new automatic peak controller for disc recording, the Recording Volumax Model 420. Now you can achieve higher recorded levels without overloading.

The Model 420 eliminates the distortion of clippers and the thumping and pumping of conventional limiters. It provides the maximum peak output at all frequencies, even as a function of record diameter.

The completely solid-state Model 420 Recording Volumax is unconditionally guaranteed. (Stereo model also available).

With the world's first 60 dB-wide linear scale meter

CBS Laboratories presents its new Model 600 Wide Range Program Monitor. It's the first monitor to combine the latest developments in audio technology with the reliability of solid-state design for accurate audio measurement and analysis on a single 60 dB-wide scale.

Where the standard Volume Indicator measures only the top 23 dB of signal level logarithmically, this new Program Monitor displays information from +3 to -57 dB on a single linear, decibel scale, thus permitting accurate reading of low level audio material as well as line noise during program pauses. The 0 dB reference settings are adjustable from +18 to -22 dBm.

The 600 is also equipped with a separate DC output for graphic logging over the full 60 dB range or to drive a second meter for remote monitoring. It is also available in a standard 19-inch mounting rack from which it can be easily removed for portable use.

While not intended as a replacement for the standard Volume Indicator, the 600's meter ballistics are such that its readings are compatible with VU indications. It's a practical program monitor as well as a valuable measuring tool.

FOR FURTHER INFORMATION, WRITE:

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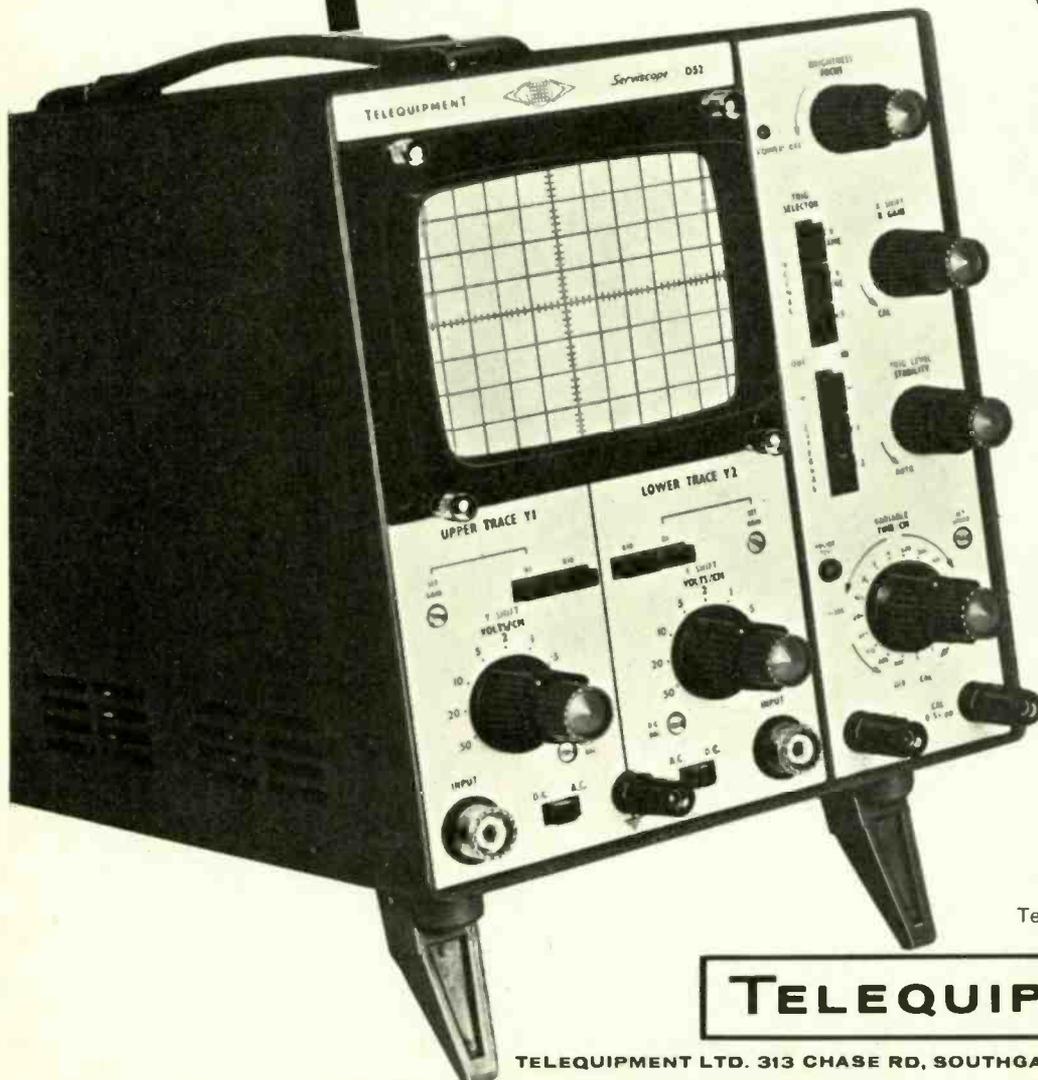
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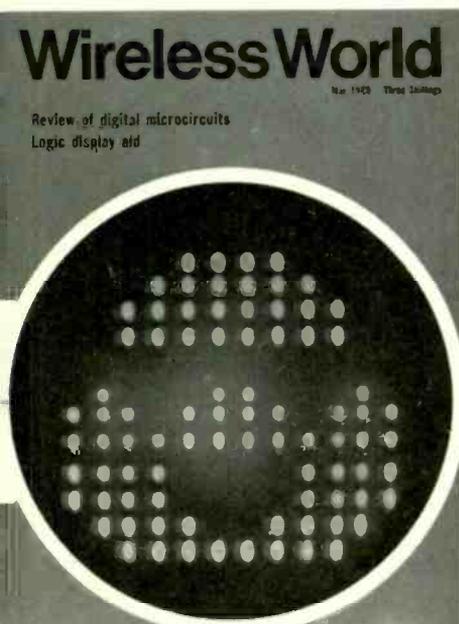
Wireless World

Electronics, Television, Radio, Audio

Fifty-ninth year of publication

May 1969

Volume 75 Number 1403



Our cover picture this month is the Venn diagram for the sum output of a full adder, produced on the screen of an oscilloscope, by the Logic Display Aid described in the series of articles beginning in this issue. The oscilloscope was deliberately defocused to produce the extra-large dots.

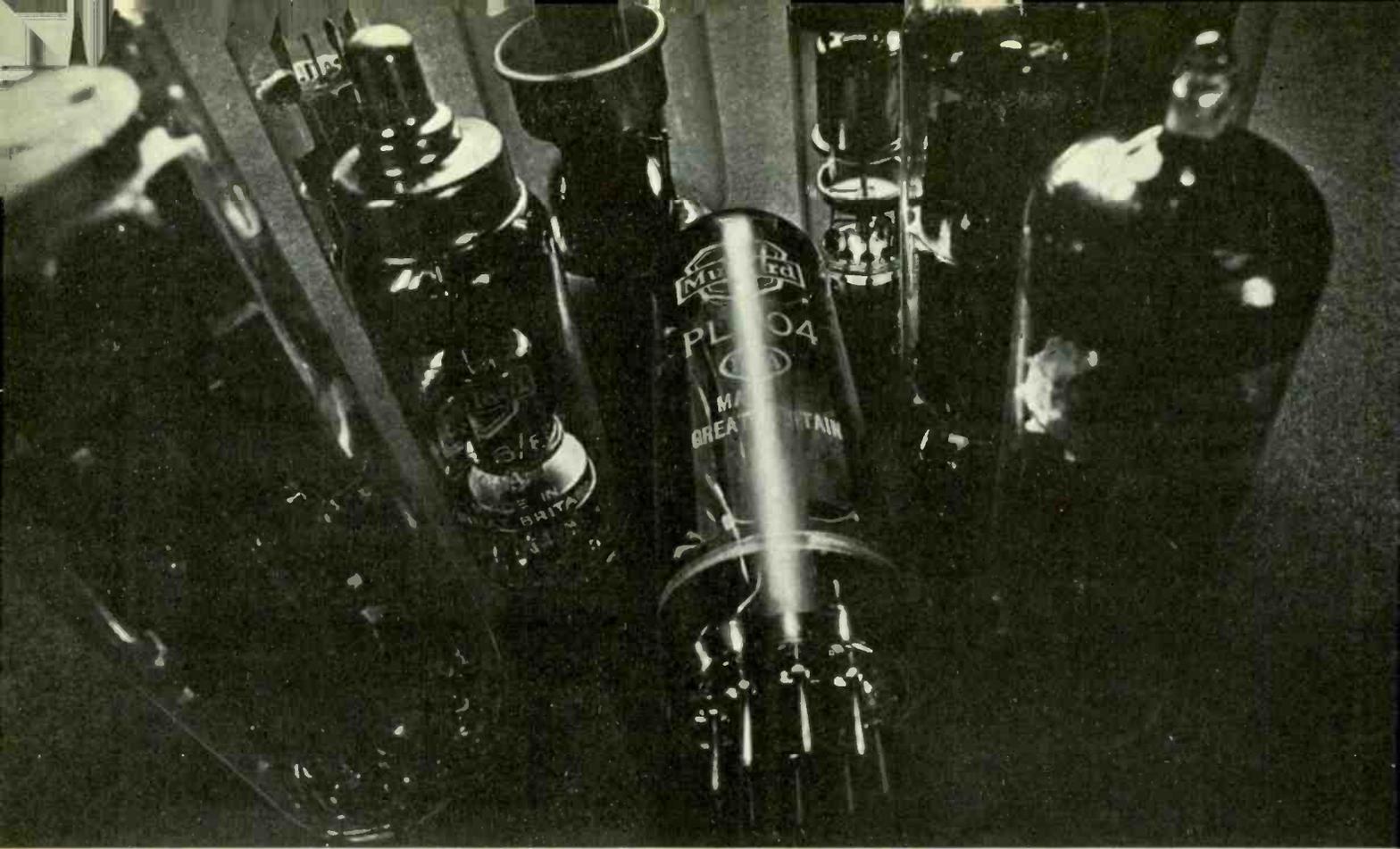
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How Mullard developed the valves for today's hybrid TV sets

During the earliest stages of semiconductor development, Mullard recognised that the all-valved television receiver, whilst giving reliable performance and economic set design, could with advantage incorporate semiconductor devices in place of those valves used in the low signal handling stages. Consequently, Mullard pioneered the design of hybrid television and were the first to offer a complete set of valves for the purpose. Today, we are Europe's major supplier of complete ranges of valves both for colour and monochrome sets.

Each valve provides a low cost solution to the design problems found in the critical high power deflection and output stages of television receivers.

Purpose designed Each valve performs a specific function in part-transistorised receivers. But, before developing these valves, Mullard applications laboratories had to solve the complex problems of matching the optimum specification for each

individual valve stage in a hybrid circuit layout. Nothing was left out—chassis tolerances, component stability, reliability, life performance, supply variation—all were investigated and specified.

Consistent quality All the plant, equipment and component parts for manufacturing valves were designed and built by ourselves at our Blackburn factory. In fact, our reputation for consistent product quality is a direct result of this 'do-it-yourself' policy, coupled with quality control that starts at the raw-material stage. We even produce our own grid wires from tungsten powder. And we process the critical cathode-emission coating, using barium, strontium and calcium nitrates that comply with our very tight specifications. The same tight control is exercised right down the production line, offering setmakers top-quality, reliable products at an economic price.

Continuous improvements Just because we produced the best possible valves to start with, it doesn't mean that development is forgotten. Whenever a new material or a new method of production arises from research studies or factory development projects, we investigate to see if it offers an improvement.

Complete data for set designers Mullard valves are supported by comprehensive data in the form that designers appreciate. For example, the data for deflection valves includes

design charts which make full allowance for valve and component tolerances, for performance changes with valve life and for mains voltage variations.

Sales Setmakers appreciate the overall quality and economy of Mullard valves for hybrid TV, because most new television sets, both colour and monochrome, in the UK, now have them fitted as standard. Overseas customers are also specifying Mullard valves in large quantities.

Worth it? Right from the beginning we've had everything under our control, so that we can be sure the product will give consistent service. This also enables us to relate quality with the best possible price. Something which applies across the very wide Mullard component range. Our components find applications as unexpected as Astronomy and Zoology. And because of the many and unusual applications for our components, we have experience in many technologies. Experience our customers now take for granted.

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A recent announcement from one of this country's major electronics companies stated that the product about which they were writing was developed as a *private venture*. It was obvious that the company, or at least its P.R.O., considered that this fact was worth shouting about, presumably because it was the exception to the norm.

Hard on the heels of this announcement came the news from the National Research Development Corporation that, at the request of the Ministry of Technology, the Corporation is to invest nearly £5m in "the development and manufacture of microelectronic devices by Ferranti Ltd, Marconi-Elliott Microelectronics Ltd, and the Plessey Company Ltd. . . . The Corporation expects to recover its investments with interest by 1980 through a levy on the companies sales of silicon integrated circuits".

Such announcements as these only underline the fact that the electronics industry in general is becoming more and more dependent directly or indirectly on Government support. In addition to such direct financial assistance as that cited above—and there are many others—the Ministry of Technology is the country's biggest customer for electronic equipment.

In our report, elsewhere in the issue, on the Paris components show reference is made to the possibility of the U.S.S.R. becoming a major contender in the international microelectronics race. If this does happen, as is highly probable, then in the face of such *national* competition and that already facing us from across the Atlantic (from companies bolstered up by military and space spending) it may well be inevitable for our own industry to have substantial Government backing if it is to survive. On the other hand there is a lurking danger in the security enjoyed under a beneficent Government. It can, of course, have a stultifying effect on initiative; indeed the N.R.D.C. microelectronics announcement mentioned above stresses that "an important feature of the arrangements has been the establishment of a collaborative agreement between companies themselves. Each company has undertaken to disclose broad details of its own research and development to its collaborators". It would therefore appear that it is no longer necessary for any one of the three companies to try to get the edge on the others by research, ingenuity, skill, or what have you. It can be, and is of course, argued that duplicated, or in this case triplicated, research and development is wasteful. However, a much more serious aspect of corporate research was stressed by Commander H. Pasley-Tyler, retiring president of the Electronic Engineering Association, speaking at the annual luncheon of the E.E.A. on March 26th. That is, that too high a percentage of our research and development resources are locked up in laboratories which serve a number of official and semi-official organizations for the fulfilment of their own narrow purposes without any relevance to the wider possibilities of international sales.

Our industry (and for that matter much of the technology on which it is based) was built on Government spending during World War II and over the years it has tended to rely, perhaps a little too heavily, on this source of income. Military spending has, however, been drastically cut and the industry is feeling the pinch. This may be a good thing as it could stir us to seek new pastures, but it would appear that the industry is still relying on the umbilical cord to the Mintech remaining intact. Cmdr. Pasley-Tyler criticized in relation to the curtailment of military spending, the "confident belief that the civil side of the Ministry of Technology will somehow look after our technological future".

With the growing number of mergers, resulting in a few large units making up the bulk of the industry, which is becoming increasingly dependent upon Government support, one is tempted to ask how long it will be before there is a move to make unofficial nationalization official.

Wireless World Logic Display Aid

1: Introduction

designed by B. S. Crank*

The current methods of teaching logic design are lacking in some respects as there is a gulf between the practical and theoretical aspects of tuition.

The normal procedure is to introduce the student to a "logic tutor" after some initial training has been done in the elements of Boolean algebra. Representative circuits are "patched-up" and the outputs are interpreted from lights, meters or in fact from anything that is capable of a two-state indication.

Excellent ways of representing logic functions graphically already exist, in the form of Venn diagrams, Karnaugh maps and Truth tables, and these have the advantage of presenting the abstract functions in ways that can be easily visualized. This latter point is important as the student who can visualize logic combinations will soon reach a much deeper understanding of the underlying fundamentals. It is almost certain that during the theoretical instruction at least one of the above methods of representation, more likely all three, was employed.

As soon as practical work is started the method of display is reduced to flashing lights and other two-state indicators. These types of indicators have to be interpreted by the student and, since they are not graphically representative it is most unlikely that he will be able to visualize the function being demonstrated and, therefore, he may miss the point.

The *Wireless World* Logic Display Aid[†] combats this problem by producing, on a standard oscilloscope, the Venn diagram, Karnaugh map or the Truth table of any gate or logic circuit that is connected to the display aid.

For instance, if a binary adder circuit were connected to the display aid, and if the instrument were switched to the Truth table mode, the rules of binary addition, which is the adder Truth table, would be displayed on the oscilloscope. In other words the hardware itself produces exactly the same display as was used by the instructor on the blackboard during the theoretical sessions and, as a result, the problems confronting the instructor and the student are much reduced.

Some applications of the instrument are listed below: others will suggest themselves to readers as they become more acquainted with the device.

Applications

1. Teaching Boolean algebra.
2. Introducing and explaining the properties of Venn diagrams, Truth tables and Karnaugh maps.
3. Demonstrating the basic logic functions: AND, OR, NAND, NOR, etc.
4. Showing how gates can be combined to satisfy complex Boolean equations.

5. Explaining the difference between positive and negative logic and demonstrating the relationships between AND — OR — NAND — NOR and the effects on the hardware of a change in logic convention.
6. Explaining what minimization is and how it is accomplished.
7. As an aid to minimization of logic systems.
8. Shows how binary arithmetic can be performed with logic.
9. As an aid to teaching modern mathematics.
10. Quickly tests the results of practical work carried out by students.
11. Can be used as check-out equipment on production lines manufacturing logic sub-assemblies.
12. As a bench test equipment for rapid fault finding on logic assemblies.
13. Can be built into equipment for monitoring purposes.

By way of an experiment the writer introduced the instrument to his seven- and five-year old daughters who had no prior knowledge of the Venn diagram. The



The completed prototype which incorporates all the extra facilities mentioned on page 198. The four sets of function control switches, one set for each display area, can be clearly seen. Two input sockets for the external logic circuits are provided. The two push-buttons on the right of each set select either external circuit 1 or 2 for the appropriate display area; pressing both of these buttons results in the difference between the two circuits being displayed. The set of terminals on the left are for the variable outputs (A, B, C, D), the set in the centre are for the outputs of the external logic circuits (Z_1, Z_2) and the terminals on the right are power supplies for external logic circuits and for the extra variables (E, F) when the instrument is used in the 6-variable Karnaugh map mode.

*Assistant editor *Wireless World*.

† Provisional patent specification No. 14062/1969.

"Lesson" was treated as a game. The square on the oscilloscope screen which contains the three interlocking circles of the Venn diagram (*universe*) was called a garden. The three circles representing the variables were called the areas where plum, apple and orange trees grow. Within five minutes both children could recognize all the individual areas of the Venn diagram. Encouraged, the writer introduced the children to the Karnaugh map and Truth table in turn. In a very short time they could interpret the meanings of both.

The form which the display takes can be clearly seen in the accompanying photographs which show the instrument operating in its various modes.

Before commencing the description of the instrument a few words about the form of the series of articles in *Wireless World* would not go amiss. The instrument can be easily divided into a number of small sections, each section carrying out a particular sub-function. One sub-function at a time will be described in its entirety. That is, first the theory behind the sub-function will be discussed followed by a description of the circuit, construction and testing. This means that construction work could, if desired, be started long before the series of articles is finished. However, the instrument is a fairly complicated one and the inexperienced constructor is advised to wait until part five of the series is published before deciding if he is competent to start the project.

This first article is introductory; the overall functioning of the instrument will be discussed and some of the relevant basic theory will briefly reviewed. Subsequent articles will give detailed constructional information and will also describe some accessory units that may be used with the instrument.

The instrument is constructed using 42 integrated circuits. In general components are mounted on small plug-in cards. The integrated circuits are from the Ferranti series 300 Micronor II range of diode-transistor logic units which are in 14-lead plastic dual-in-line packages. These will be described in more detail later. The design cost was considered to be secondary to versatility, reliability and ease of operation.

General description

The block diagram of the complete instrument is shown in fig. 1. Although not immediately obvious from this drawing, the instrument is divided into two distinct sections: circuits for deriving oscilloscope scan voltages and logic circuits for obtaining the video signals. The external logic circuit connected to the instrument by the user exercises a significant amount of control over the internal logic section which produces the video signal.

The scan voltages and the video signals are derived from two counters called the X and Y counters and it is with these that the description will begin.

Each counter consists of four bistables connected to count in natural binary as shown in table one. The table corresponds to the output of the Y counter, the bistables of which are labelled A, B, C and D. The bistables in the X counter are labelled E, F, G, and H and follow the same counting sequence as the Y counter. A and E are the least significant. In the table, 1 corresponds to a positive voltage and 0 to a voltage very near to earth potential. The Y counter is driven by a multivibrator at about 20kHz. The output of the Y counter forms the input to the X counter.

Table one

D	C	B	A
0	0	0	0
0	0	0	1
0	0	1	0
0	0	1	1
0	1	0	0
0	1	0	1
0	1	1	0
0	1	1	1
1	0	0	0
1	0	0	1
1	0	1	0
1	0	1	1
1	1	0	0
1	1	0	1
1	1	1	0
1	1	1	1
0	0	0	0

etc.

In a television set the spot is moved across the face of the screen by two sawtooth voltages. A similar method of deflection is used in this unit, the only difference being that the scan voltages are staircase waveforms instead of sawteeth.

The staircase scan waveforms are produced by the two digital-to-analogue converters (dians), one of which is connected to each counter. The voltage output of each dian is proportional to the numerical contents of the counter to which it is connected. Taking the Y counter as an example; at each input pulse the contents of the counter increase by one and the output of the dian alters by one unit. After the counter has received 16 input pulses the next pulse will return the counter to the "all-zero" position; this transition corresponds to flyback. The staircase produced by the Y dian is shown in Fig. 2. The Y deflection voltage is precisely 16 times the frequency of the X deflection voltage because each counter divides by 16. The outputs of the dians drive the c.r.t. deflection plates.

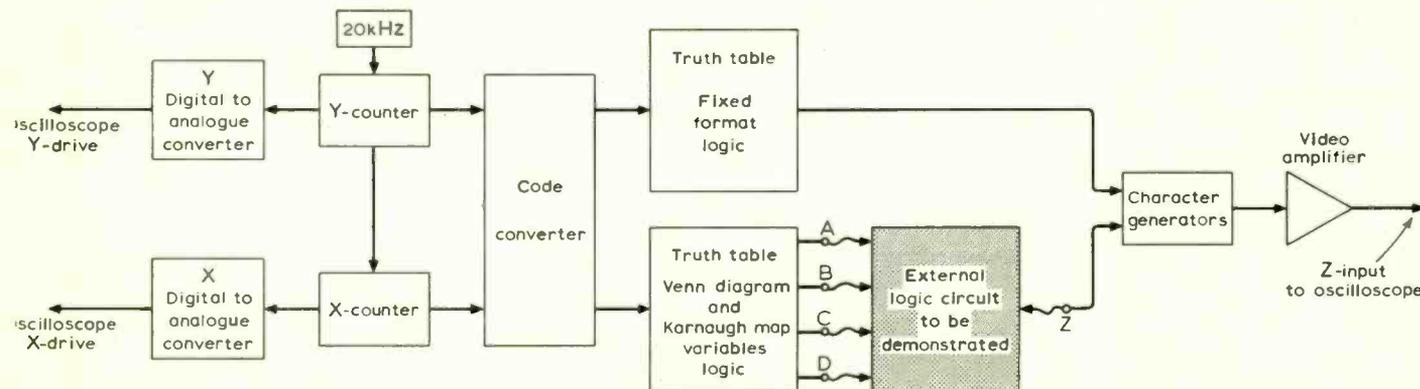


fig. 1. A block diagram of the complete instrument.

It is arranged that as the contents of the Y counter increase, the output of the Y dian goes negative moving the spot down the face of the screen. With the X waveform the reverse is true; as the contents of the counter increase the putput of the X dian goes positive, moving the spot to the right.

Imagine that only the Y output voltage is connected to the oscilloscope. The spot will be moved down the face of the screen in 16 discrete steps so that a vertical column of 16 dots will be traced on the tube face.

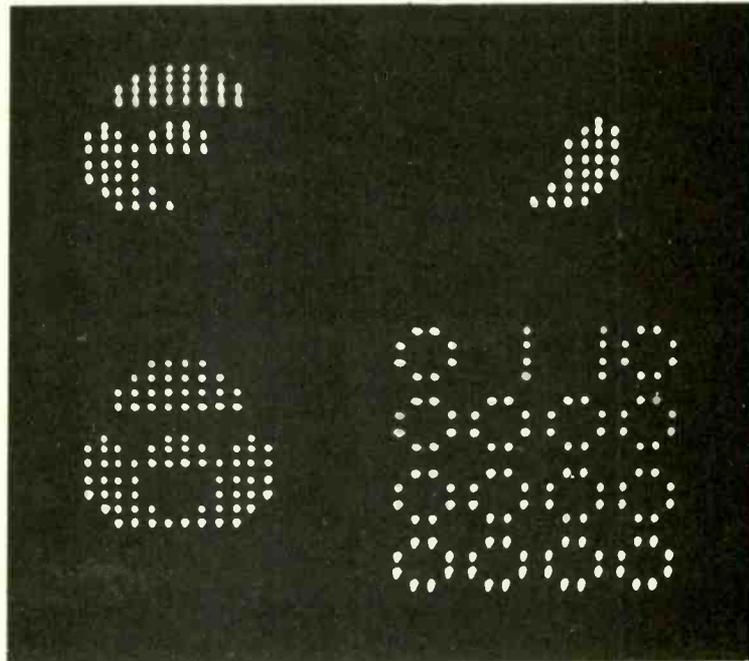
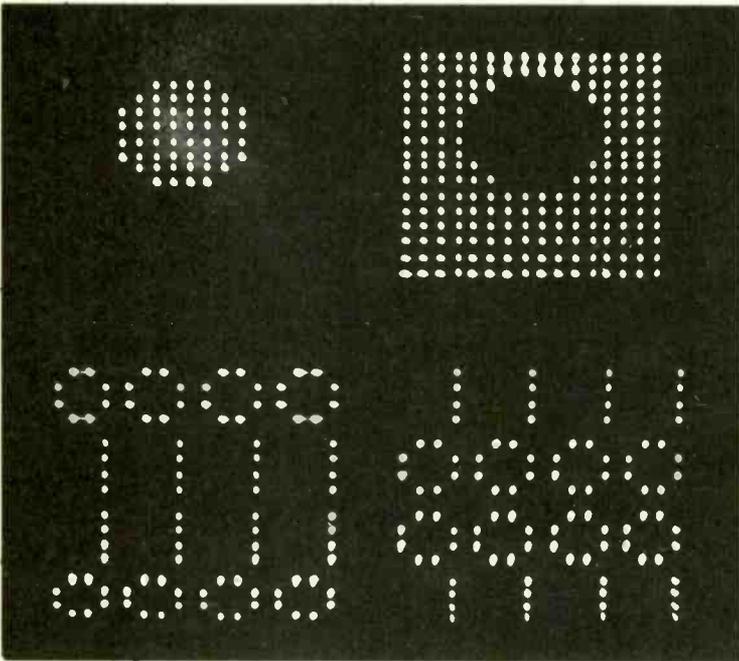
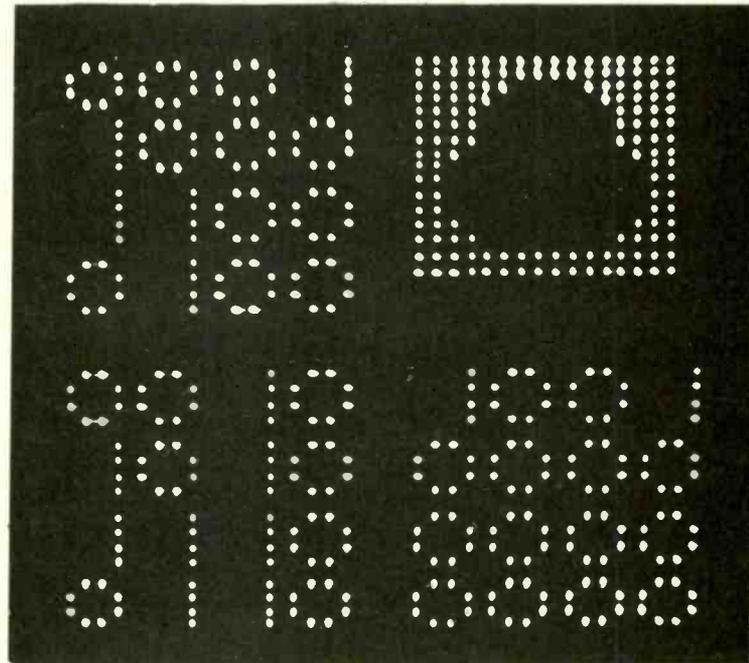
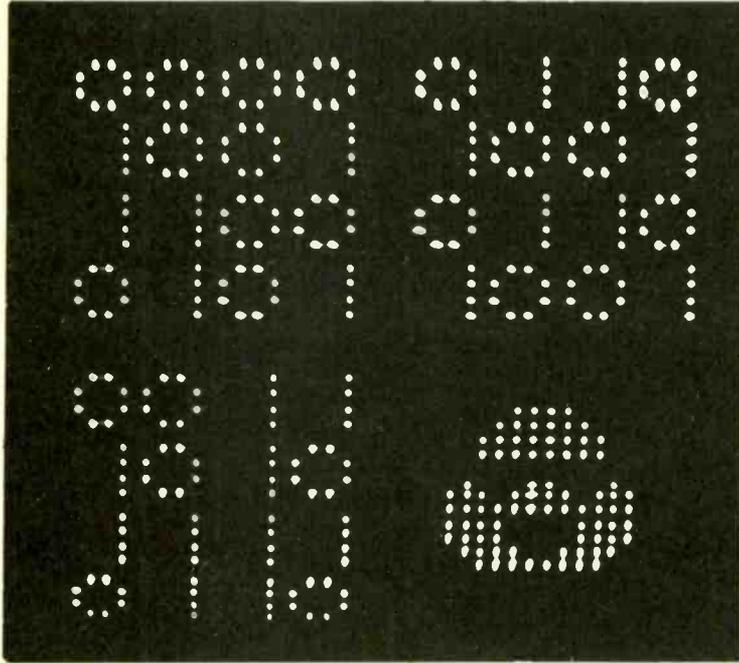
With both deflection voltages (X and Y) connected to the oscilloscope, when the spot is at the bottom of the screen the next pulse from the multivibrator will cause the contents of the Y counter to fall to zero and the out-

put of the Y counter will increase the contents of the X counter by one. As a result the spot will fly back to the top of the screen in a position slightly to the right of the column of dots it has just traced out. Column after column of dots will be traced until both counters are "full". The next input pulse causes both counters to return to zero and the spot to fly back to the top left-hand corner of the screen.

The "raster" produced by these circuits will consist of a square of dots with 16 rows and 16 columns, 256 dots in all. It is on this matrix of dots that all patterns are based. The matrix-raster is shown in Fig. 3.

The next section of the instrument, the circuits for forming the video signal will be discussed in principle

A



C

Photographs of the oscilloscope screen showing the display in operation. It is stressed that these patterns were produced by the prototype which has all the additions mentioned on page 198. The basic Logic Display Aid will only produce one of the four maps shown in each photograph at any one time. In photograph (a) the instrument was connected to a full binary adder and the SUM output is displayed. The whole left-hand part of the photograph is the Truth table for the SUM output of the binary adder; the first column is A, the second B, the third C and the fourth the result or SUM. The top right-hand display (still photograph (a)) is the Karnaugh map for the function and below it is the appropriate Venn diagram. In photograph (b) the external logic circuit was an AND gate connected to the \bar{A} , \bar{B} and \bar{C} terminals, the positions of the Venn diagram and Karnaugh map are reversed when compared to (a).

Photographs (c) shows how two different circuit functions can be displayed simultaneously, the Venn diagram and Karnaugh map for A and \bar{A} being displayed. For photograph (c) two binary adders, one of which was not functioning correctly, were connected to the display aid. The left side of the picture shows the Venn diagram for each of the two adders; the top right display is the Venn diagram, and the bottom right is the Karnaugh map, for the difference between the two adders showing that the term $\bar{A} \bar{B} C$ is missing in one adder.

only at this stage, a fuller description being given later.

If a binary-to-decimal converter was connected to the Y counter it would have 16 outputs to cope with all possible conditions of the counter. In such a converter one of these outputs would correspond to each state of the counter. Therefore each output of the converter would correspond to a particular row in the matrix raster. This point is illustrated in Fig. 4. The same sort of converter could be connected to the X counter, only this time the outputs would correspond to particular columns in the matrix.

If one of the outputs of the Y converter is AND gated with one of the outputs of the X converter the output of the AND gate will be "up" (at a positive voltage) only when the spot is at the intersection of the row and the column chosen. In other words a particular dot within the matrix can be selected. This point is illustrated in Fig. 5. If the output of the AND gate is presented to the Z terminal (intensity modulation) of the oscilloscope, and the brightness control is correctly adjusted, only the selected dot, in its correct position, will be visible on the tube face. It is easy to see how the process could be extended to select a number of dots to form any particular pattern.

In the instrument, although the above principle is employed, binary to decimal converters are not used because such an approach would be very expensive. The code converters shown in the block diagram of Fig. 1 modify the binary output of the converters in such a way as to

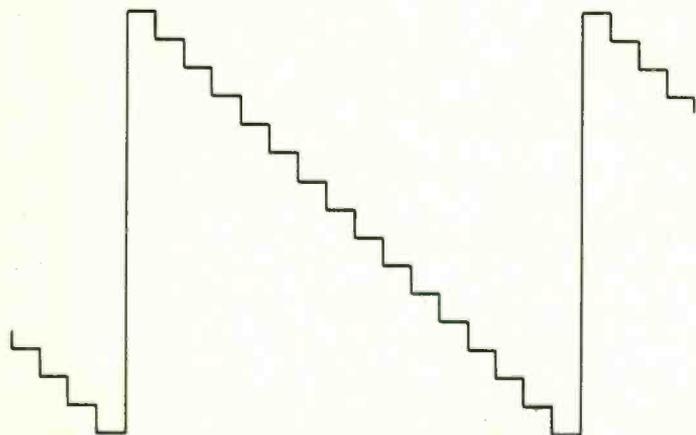


Fig. 2. The staircase waveform produced by the Y digital-to-analogue converter.

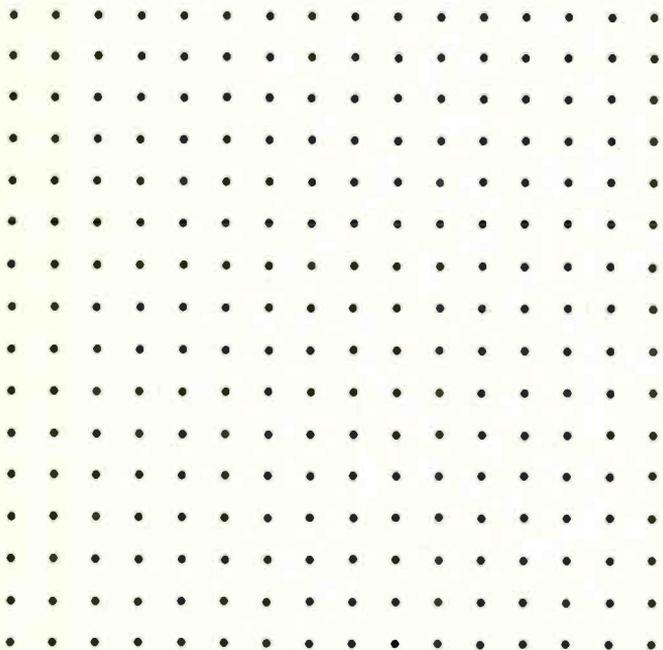


Fig. 3. The 16 x 16 matrix-raster on which all the patterns are used.

make the subsequent decoding of the various patterns an easier task. We will break from the description of the instrument for a short while and briefly review some important points of theory.

Boolean algebra

It is beyond the scope of this article to give any comprehensive explanation of this subject. Much has been written in these pages in the past and there are numerous books available. However a few of the basic rules are stated below:

$$\begin{aligned}
 A + 0 &= A & A \cdot A &= A \\
 A + 1 &= 1 & A + \bar{A} &= 1 \\
 A \cdot 0 &= 0 & A \cdot \bar{A} &= 0 \\
 A + A &= A & A \cdot 1 &= A \\
 \overline{A \cdot B \cdot C} &= \overline{A} + \overline{B} + \overline{C} \\
 \overline{A \cdot B \cdot C} &= \overline{A} + \overline{B} + \overline{C} & & \text{(De Morgan's Theorem)} \\
 A \cdot \overline{B \cdot C} + A \cdot B \cdot C &= A \cdot B \cdot (C + \overline{C}) = A \cdot B \\
 (\overline{A} + \overline{B}) \cdot (A + B) &= \overline{A} \cdot B + A \cdot \overline{B} \\
 \overline{\overline{A}} &= A
 \end{aligned}$$

Venn diagrams

The Venn diagram is a method of graphically representing a Boolean function. It consists of three interlocking circles within a square as shown in Fig. 6. Each circle represents one variable. The circles are normally labelled A, B and C. Everything that is outside circle A represents \bar{A} so the area outside all three circles is $\bar{A} \bar{B} \bar{C}$. The square is divided into eight separate areas by the circles as there are eight possible ways of com-

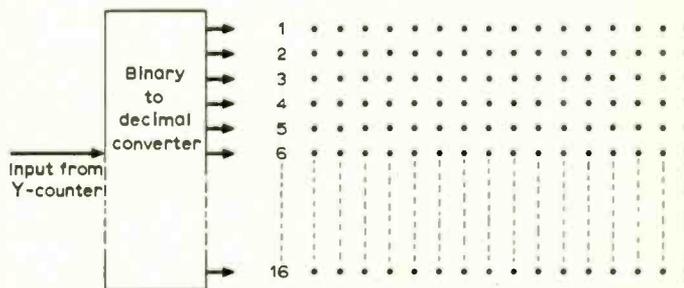


Fig. 4. Shows how a binary-to-decimal converter could be used to address any particular row of dots in the matrix-raster.

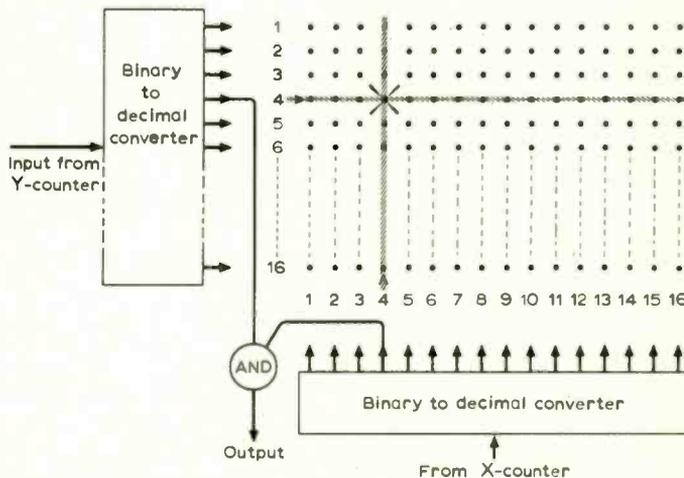


Fig. 5. Two binary-to-decimal converters in conjunction with an AND gate can select any one dot within the matrix.

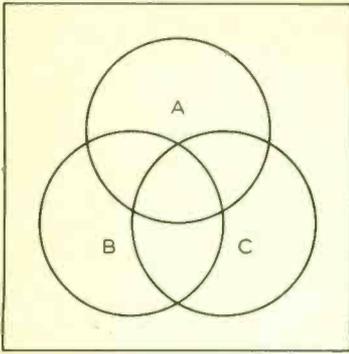


Fig. 6. The Venn diagram.

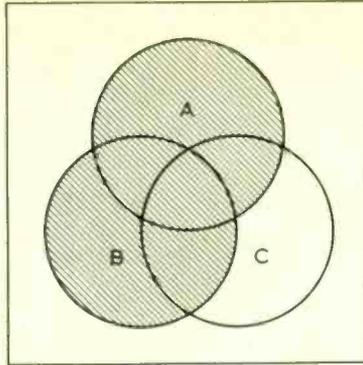


Fig. 7. The Venn diagram for $A + B$. The shaded area represents the required function.

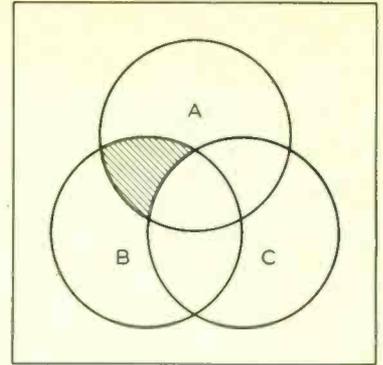


Fig. 8. The Venn diagram for $A \bar{B} \bar{C}$. The shaded area represents the required function.

binning A, B and C. Fig. 7 shows the Venn diagram for $A + B$, Fig. 8 shows the Venn diagrams for $A \bar{B} \bar{C}$.

Truth tables

The Truth table lists all possible combinations of the variables employed and takes the form shown in Fig. 9. Each variable has one column. The last column is reserved for showing the truth, or otherwise, of the function being illustrated for a particular combination of the variables concerned are true. This Truth table therefore represents the AND function.

Karnaugh maps

The construction of a Karnaugh map is shown in Fig. 10. Each variable is allocated half the area of a square, the other half of the square represents the complement of that variable. The positions that the variables occupy are shown in Fig. 10(a), (b), (c) and (d). The composite map is made up by superimposing these four divided squares upon each other as shown in (e). Sixteen squares result, each representing one unique combination of the variables, and each square differs from its neighbour by the negation of one variable.

Suppose one wished to construct a Karnaugh map for the function:

$$\bar{A}\bar{B}\bar{C}\bar{D} + \bar{A}\bar{B}C\bar{D} + A\bar{B}\bar{C}\bar{D} + ABCD$$

The map is drawn and 1 is placed in every square that represents one of the terms in the expression and an 0 is placed in all vacant squares. For convenience an addressing system is placed at the sides of the map so that each square can be easily identified. The map for the chosen expression is shown in Fig. 11. By definition

all terms that are in adjacent squares differ only in the negation of one variable and may therefore be combined. All the 1s in our example are adjacent so all the terms can be combined. This is done by only selecting variables that are common to each adjacent square:

$$\begin{aligned} &\bar{A}\bar{B}\bar{C}\bar{D} \\ &\bar{A}\bar{B}C\bar{D} \\ &A\bar{B}\bar{C}\bar{D} \\ &ABCD = AC \end{aligned}$$

$$\therefore \bar{A}\bar{B}\bar{C}\bar{D} + \bar{A}\bar{B}C\bar{D} + A\bar{B}\bar{C}\bar{D} + ABCD = AC$$

A point which must not be overlooked is that squares on the right-hand side of the map are adjacent to squares on the left-hand side and the squares at the bottom are adjacent to squares at the top.

We will now return to the description of the instrument.

Obtaining the video signal

The three circles of the Venn diagrams can be drawn on the matrix-raster as shown in Fig. 12. To derive a signal corresponding to A it is only necessary to have a system of AND gates to select all the dots that are within circle A. And, in a similar fashion, signals corresponding to circle B and circle C can be obtained. These signals, A, B and C, are fed to front panel terminals for connection to external logic circuits. A video amplifier provides the Z drive for the oscilloscope and the input terminal of this amplifier is taken out to a front panel terminal which is labelled Z.

It follows if the terminal A is connected directly to the Z input then all the dots within the area defined by circle

A	B	C	X
0	0	0	0
1	0	0	0
1	1	0	0
0	1	0	0
0	0	1	0
1	0	1	0
1	1	1	1
0	1	1	0

Fig. 9. Truth table for AND function.

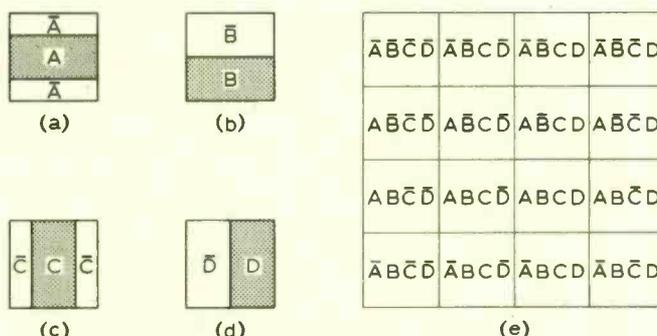


Fig. 10. (left) The position of the variables in, and the construction of, a Karnaugh map.

B A	D	0	0	1	1
	C	0	1	1	0
0 0	0	0	0	0	0
0 1	0	1	1	0	0
1 1	0	1	1	0	0
1 0	0	0	0	0	0

Fig. 11. (right) A Karnaugh map of a particular function described in the text.

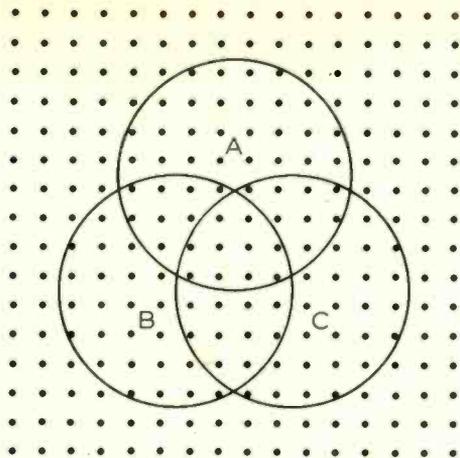


Fig. 12. How a Venn diagram can be formed from the dots of the matrix-raster.

A will be visible on the screen. The same reasoning holds for B and C.

Now if the terminals A, B and C are connected to the inputs of an AND gate and the output of the AND gate is connected to the Z terminal, only the area common to A and B and C will be displayed. In other words the Venn diagram for the AND function will be shown on the screen.

The variables are negated to form \bar{A} , \bar{B} and \bar{C} so that the complement of the variables can also be made available on the front panel. Any logic gate or any logic circuit may be connected to the terminals and the function it performs will be displayed on the screen in terms of its Venn diagram.

In the Karnaugh map mode the situation is slightly more complicated because the information is presented on the screen as a pattern of 0s and 1s. The fact that four variables can be accommodated in this mode means, as mentioned earlier, that 16 characters have to be displayed at the same time as there are 16 possible combinations of four variables. In order that the displayed characters are separated, the output of the digital-to-analogue converters producing the scan waveforms are modified to produce the pattern shown in Fig. 13. The 16 x 16 matrix

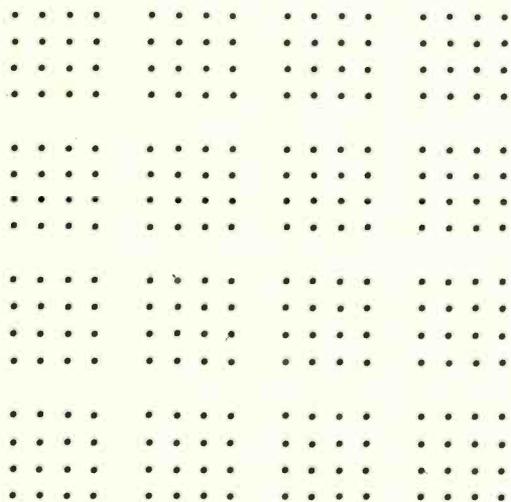


Fig. 13. How the matrix-raster is modified in the Karnaugh map and Truth table modes of operation to achieve character separation.

of dots is divided into 16 smaller 4 x 4 matrices each consisting of 16 dots. Each small matrix forms an area where a 1 or an 0 may be displayed.

The Karnaugh map, like the Venn diagram, consists of a square in which various areas represent the variables; this was shown in Fig. 10. All the dots falling in an area representing a variable are selected by a series of AND

gates, in the same way as was done for the Venn diagrams, so that four signals corresponding to the variables A, B, C and D are extracted. These are routed to the front panel terminals via the mode selection circuits.

These variables are connected to the logic gate or circuit that is to be demonstrated and the output of that gate or circuit is connected to the Z input terminal of the instrument. It follows that, as a Karnaugh map consists of every possible combination of the variables used, each of these combinations will be presented to the input of the logic circuit being demonstrated in turn as the spot scans the matrix. And, furthermore, when a particular combination is being presented the spot on the c.r.t. face will be scanning the area of the Karnaugh map representing that combination.

When the output of the logic circuit demonstrated is "up" it means that the section of the map that is being scanned by the spot is true for that particular logic circuit. It is arranged that an "up" signal to the Z input causes the character 1 to be formed in dots within the 4 x 4 matrix representing the combination of variables to the demonstration logic. When the Z input is "down", meaning that the combination of variables existing at that time is false, for the logic circuit being demonstrated, an 0 is formed in the area of the map being scanned.

The fact that a Truth table has various areas allotted to the variables is not so obvious as was the case for the Venn diagram and Karnaugh map. A Truth table for three

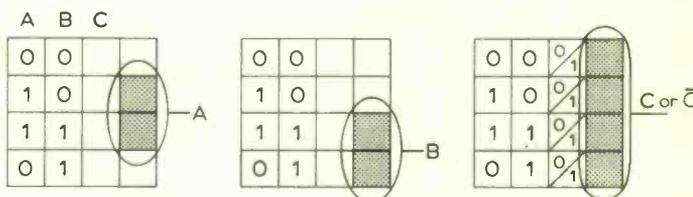


Fig. 14. How the variables are obtained in the Truth table mode.

variables consists of eight rows and four columns; an example was seen in Fig. 9. To show the complete table, 4 x 8 = 32 characters would have to be displayed at the same time. Unfortunately, as we have already seen, the maximum capacity of the instrument is 16 characters. To overcome this problem the table is displayed in two sections, one section when C is true and the other when C is not true. When only two variables are being used the problem does not arise because only 12 characters are needed.

The first two or three columns, depending on how many variables are being used, never alter as can be seen in Fig. 14 — the same pattern of 0s and 1s being displayed continuously. In Fig. 1 the logic to produce these columns is contained in the box labelled "truth table fixed format logic" which controls the 1 and 0 character generating circuits directly. The column 'C' of the truth table is controlled from a switch mounted on the front panel so that all 1s or all 0s, representing C or \bar{C} , can be selected.

The areas representing the variables are confined to the last column and are as shown in Fig. 14. The dots within these areas are gated out, as was done before, and used to form the output variables A, B and C. Whether a 1 or an 0 is displayed in the last, result column of the truth table is dictated by the logic circuit being demonstrated in exactly the same way as was done for the Karnaugh map.

A point which could lead to some confusion will now be cleared up.

Positive and negative logic

The Ferranti integrated circuits used are described as NOR gates in the manufacturer's catalogue. In this article they are referred to as NAND gates. The reason for this

is that Ferranti used the negative logic convention when they specified the function that their circuits would perform and here, (as with previous) *Wireless World* articles we use the positive logic convention. Clearly the difference between the two conventions must be understood by the constructor who wishes to make the display aid. A brief explanation follows.

The difference between positive and negative logic can be summed up in one sentence. In positive logic the higher of two voltages represents 1 and in negative logic the lower of two voltages represents 1. The effect on the hardware of logic circuits of a change between the two conventions is profound.

The explanation here will start with the Truth table below. This was made-up by applying various inputs to an unspecified logic gate in an attempt to find out what sort of gate it was.

A	B	X
0V	0V	0V
0V	+4.5V	0V
+4.5V	0V	0V
+4.5V	+4.5V	+4.5V

Because we have not decided which logic convention to use, the inputs and outputs have been specified as voltage levels. As usual all possible combinations of the two input variables, A and B, have been covered. Now if we are working in positive logic—the higher voltage representing 1—we can reconstruct the Truth table by writing 1 for +4.5V and 0 for 0V. This is done below.

A	B	X
0	0	0
0	1	0
1	0	0
1	1	1

Examining this table we see that the gate we are testing gives an output only when A = 1 and B = 1, therefore $X = AB$, in other words the output is only true when both A AND B are true. Our once unspecified logic gate can clearly be seen to be an AND gate.

What happens if we work in negative logic? That is, the lower of two voltages is equal to 1. We have to reconstruct the truth table, writing 1 for 0V and 0 for +4.5V.

A	B	X
1	1	1
1	0	1
0	1	1
0	0	0

Examining this table we see that whenever A or B are 1 then the output is also 1, therefore $X = A+B$. This is the Truth table for an OR gate.

From the above it can be deduced that a gate that performs the AND function when the positive logic convention is used performs the OR function when the negative logic convention is used. When changing from positive to negative logic change AND to OR.

Selecting another gate, we will again produce three truth tables from it—that obtained by measuring voltage levels and those obtained by using the positive and the negative voltage convention. This has been done below.

voltage			positive logic			negative logic		
A	B	X	A	B	X	A	B	X
0V	0V	+4.5V	0	0	1	1	1	0
0V	+4.5V	+4.5V	0	1	1	1	0	0
+4.5V	0V	+4.5V	1	0	1	0	1	0
+4.5V	+4.5V	0V	1	1	0	0	0	1

In the positive logic case:

$$\bar{X} = AB$$

$$\therefore \bar{\bar{X}} = \overline{AB} \text{ (negate both sides)}$$

and $X = \overline{AB}$ (double negatives cancel)

In positive logic the gate produces the NAND function.

For negative logic:

$$X = \bar{A} \bar{B}$$

$$\therefore X = \overline{A + B} \text{ (De Morgan's Theorem)}$$

So in negative logic the gate performs the NOR function.

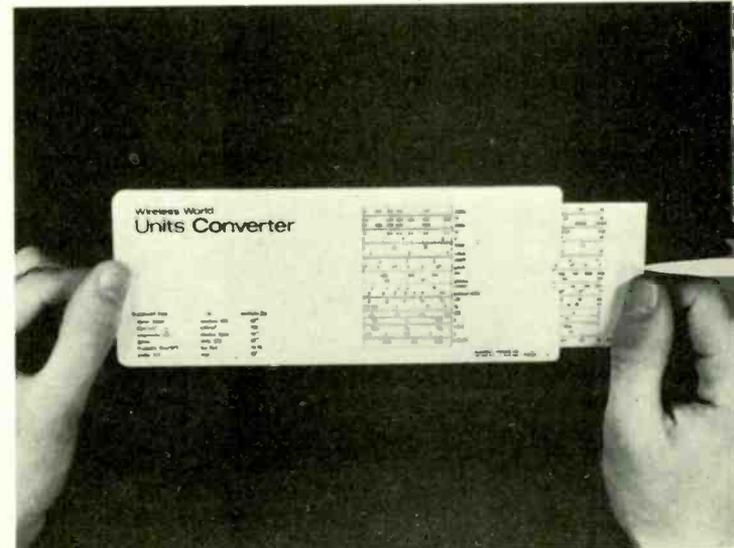
Next month: the digital-to-analogue converters will be described. The general method of construction and the integrated circuits will be discussed.

Since this article was written development work on the display aid has continued and a number of additions have been made that greatly extend the instrument's usefulness. However, it is stressed that the extra facilities result from additions, rather than modifications, to the basic circuits. The reader is therefore advised to build the basic instrument first and then decide which of the options he wishes to add.

Many versions of the instrument are possible, ranging from the basic instrument; through a version with only one control switch (on/off) that will produce simultaneously the Venn diagram, Karnaugh map and Truth table on the same oscilloscope for any external logic circuit; to an instrument bristling with 32 push-button switches that will produce four separate displays on the same instrument. Each of the display areas can be switched individually to show a Truth table, Karnaugh map or Venn diagram. Also, with this instrument, two external logic circuits can be accommodated at the same time and any of the four display areas can be individually switched to show either external circuit number 1 or number 2 or the difference between the two circuits. This latter facility is useful for demonstrating De Morgan's theorem and for logic card testing. Finally, all four areas can be switched to the Karnaugh map mode to form a single Karnaugh map of six variables.

Calculation Time Saver

This units converter "slide-rule" has been designed by *Wireless World* specially to suit the needs of the electronics or radio man. It will be available at an advantageous price exclusively to readers of this journal—details next month.



Microelectronics at Paris Components Show

From the microelectronic point of view the theme of this year's Salon des Composants Electronics was undoubtedly a move into the domestic consumer market by most of the main integrated circuit manufacturers. Television seemed to be the area of major interest with audio amplifiers coming a close second, and even the motor car and the camera did not escape the attention of some enterprising manufacturers.

Major reasons for this apparent *volte-face* are that only recently have the set makers accepted that microelectronics can offer them any real economic advantages and, having catered well for the industrial market, the i.c. manufacturers are looking elsewhere in order to sell on the broadest front possible.

It would now appear, for instance, that a complete stereo tuner-amplifier including the i.f. strip, stereo multiplex decoder, audio pre-amplifiers and main amplifiers can now be built from monolithic integrated circuits. Such an equipment would probably fall into the medium quality class offering up to 5W per channel, or if one were to have hybrid thick film main amplifiers, up to 15W per channel.

It will probably be only a matter of time before the i.c. manufacturers attack the very high quality audio market and we will be hearing the arguments for and against nonolithic sound (or mono-stereo?) as against transistor and valve sound. And taking things to their ultimate conclusion, as the manufacturers of m.o.s. l.s.i. circuits appear to be on the look-out for new applications, perhaps in a few years we shall see the programmable hi-fi system. This might contain a number of tape cassettes with digitally coded information on the tape identifying each piece of music. A programming system would allow any piece of music to be selected and played back in any order—the possibilities could be almost endless.

Many more medium scale integration (m.s.i.) m.o.s. integrated circuits were to be seen in manufacturers' catalogues, and it is apparent that much work is being done to increase the speed of this type of circuit. Although offering many advantages in the industrial process control field and in any other application where speed is not paramount, such as desk calculators, m.o.s./l.s.i. arrays will not replace e.c.l. circuits in computers for a long time to come. However, it is possible that m.o.s. circuitry will start to replace large ferrite core stores in a couple of years as it is expected that m.o.s. dynamic

storage will become cheaper than its ferrite counterpart after taking into account the cost of the drive circuitry.

Discussing this application, a representative of Texas Instruments said that it is possible that four chips, each with a one to two thousand bit storage capacity, could be mounted in the same package, and if a suitable package was designed and the beam lead interconnection technique was employed, it would be possible to replace an individual chip within the package should it fail.

Also on the industrial front some examples of m.o.s. complementary arrays were seen.

The U.S.S.R. was represented at the Salon for the first time this year and a wide range of r.t.l., d.t.l., t.t.l., m.o.s., monolithic and hybrid integrated circuits for industrial and domestic applications was on show, although no examples of l.s.i. were seen. A representative said they were exhibiting in Europe to gauge the general reaction to their products and that they may exhibit in the U.K. sometime this year. Does this herald the entry into the world microelectronic market of another large contender?

The first example of a product employing l.s.i. intended for what could be considered the consumer market was shown by Schneider Radio and Television and was presented as their contribution to what they call "price decrease technology". The product, a low-cost digital multimeter, will be marketed in the U.K. by Honeywell Ltd. (Hemel Hempstead) in the near future.

The instrument, known as the Digitest 500, employs a single chip which incorporates a three-stage decade counter, all the

decoding logic for the display, all of the instrument's control logic and part of analogue-to-digital converter. The chip is manufactured by General Instruments Europe and it is certainly an achievement to incorporate all these functions within the limitations imposed by a 16-lead dual-in-line flat pack.

The instrument has 17 ranges and is capable of measuring a.c. and d.c. voltage and current, and ohms. The price of the meter is expected to be about £110 in this country.

Digressing slightly for a moment, it is worth while mentioning a novelty item seen on the Schneider stand that could be called an innovation awaiting an application. A Swiss engineer, Herr Vogel, has designed a multitrack automatic tape replay mechanism intended for inclusion in a digital voltmeter, or other instrument operating in the b.c.d. code, that gives an audible, as well as a visual, indication of the quantity being measured. On the Schneider stand the tape mechanism was seen built into a digital voltmeter and the combination was called "Voltmètre Numérique Parlant".

Microcircuits for television

The main area of activity as far as integrated circuits for television is concerned was in f.m. i.f. amplifiers. SGS have produced one (type TAA661) which is suitable for operation at 6 or 10.7MHz so that it may be employed in television or radio receivers.

In this circuit after three stages of amplification and limiting the signal is split into two. One signal, now a square wave because of the limiting, is fed directly to a discriminator which is a coincidence detecting circuit. The second signal is fed to an external tuned circuit, the output of which is a sine wave. This sine wave is also fed to the coincidence detecting discriminator.

As the applied modulation varies the frequency of both the sine wave and the square wave vary in unison; however, the sine wave will be subjected to a phase shift which depends on frequency because of the tuned circuit. The net result is that the output of the coincidence detector will be a series of pulses the mean value of which are proportional to the modulation. The discriminator circuit, together with explanatory waveforms, is shown in Fig. 1.

The TAA661 will operate with a supply



Schneider digital multimeter

voltage from 4.5 to 15V, 12V at 15mA being typical. It has a frequency range 5kHz to 60MHz and will provide a 60-dB gain at 5.5MHz; a.m. rejection is typically 40dB with a modulation frequency of ± 50 kHz to a depth of 30%.

Another f.m. i.c. (type TAA710) was shown by Intermetall; this incorporates an oscillator, mixer, i.f. amplifier and discriminator and requires very few external components. It has an a.m. rejection of 40dB and requires an input between 1mV and 1V.

The French subsidiary of the Philips group, La Radiotechnique-Compelec (R.T.C.) announced a frequency modulated i.f. amplifier which included a discriminator and a variable gain i.f. stage. The a.f. output voltage could be varied by altering the potential at one of the i.c. input pins.

R.T.C. is currently developing an integrated decoding matrix (TAA 470) for colour television receivers which produces the R, G, and B signals from Y, R-Y, G-Y and B-Y.

Integrated voltage regulators intended for supplying tuning potentiometers in varicap tuned receivers were shown by both R.T.C. (TAA550) and Intermetall (ZF33, ZTK33). In all cases the output voltage was 33V.

A colour decoder (MC1325) in a dual-in-line flat pack announced by Motorola produces the R-Y, G-Y and B-Y signals from the composite chroma signals and the two reference phases.

Hybrid microcircuits are usually designed for a particular customer application and are not generally sold as standard production items. There are, of course, a number of exceptions to this, voltage regulating circuits being an example. N.S.F. Telefunken are producing three thick film hybrids for television use. These are a PAL flip-flop, an a.f. input and driver amplifier which is intended for use with an external output transistor to provide up to 1W, and an a.f. amplifier with a 50-mW output intended to drive an external complementary output

pair. This latter amplifier has an open circuit voltage gain of $>5,000$ and a distortion factor of 1%.

Plessey have seven i.c.s for television at present under development, these include a colour decoder, i.f. amplifier and a synch separator.

..... for audio

The most powerful microcircuit audio amplifier seen was a thick film hybrid made by Bendix, that could deliver 15W r.m.s. into a 3Ω load at about 1% distortion at 1kHz. The microcircuit is housed in a ceramic package ($5 \times 2.5 \times 0.7$ cm) that is designed to be attached to a heat sink. The amplifier has a 60-dB power gain and requires a 350-mV input for full output.

A monolithic amplifier in a dual-in-line package with special arrangements for heat sinking was announced by General Electric (PA246). This amplifier provides 5W r.m.s. into a 16Ω load. The distortion performance depends on the external components employed; however, a typical figure is 0.7% although this can rise to as high as 5% with careless selection of the external components. The 3-dB points of the frequency response are 30Hz and 100kHz at 2.5W output.

A large number of manufacturers were showing audio amplifiers with 1 or 2W outputs and it is not proposed to mention all of them as some of these have already been described in *Wireless World*.

Motorola manufacture two 1-W monolithic audio amplifiers offering different performances. The better of these (MC1554G) is designed to operate with a 16Ω load and is capable of offering only 0.4% total distortion at full output power with suitable selection of external components. Under these conditions the frequency response is flat from about 50Hz to 500kHz. Because of the very wide bandwidth very great care must be taken to keep all wiring as short as possible and to avoid stray coupling between input and output to prevent v.h.f. instability.

RCA introduced an interesting microcircuit (type CA3048) which houses four independent a.c. amplifiers in a dual-in-line flatpack. Each amplifier has a minimum 53-dB gain, an open loop bandwidth of 330kHz, an input impedance of $90k\Omega$ and will provide 2V output at low distortion.

Fig. 2 shows the CA3048 connected as a complete stereo preamplifier, the gain is 46dB and the total harmonic distortion at 2V r.m.s. output at 1kHz is $<0.2\%$. Another audio application for this i.c. would be as a mixer.

Secosem-Recherche described work they had been doing in applying the piezo-m.o.s. effect to gramophone pickup arms. An experimental model produces 50mV output but later it is hoped to increase this by a factor of ten with improved mechanical coupling.

..... for radio

A major, but unfortunately publicity-shy, British manufacturer who will have to remain anonymous, mentioned at the exhibition that they are producing a complete car radio as a single chip. This in itself is not outstanding as other firms announced fully integrated radio chips. The difference is that the firm in question has provided its car radio with a 4-W audio amplifier on the same chip and seems to have solved the problem of local heat generation and the difficulty of heat spreading through the chip and upsetting earlier circuits.

A complete monolithic stereo multiplex decoder in a dual-in-line flatpack (MC1304) was shown by Motorola. A choice of a plastic package (suffix P) or ceramic package (suffix L) is available. This circuit requires three external coils and a few assorted resistors and capacitors. A 200mV r.m.s. multiplex input signal is required and the left and right channel audio information is available at the outputs. An output is also provided for a 12V, 40mA, stereo indicator lamp. The

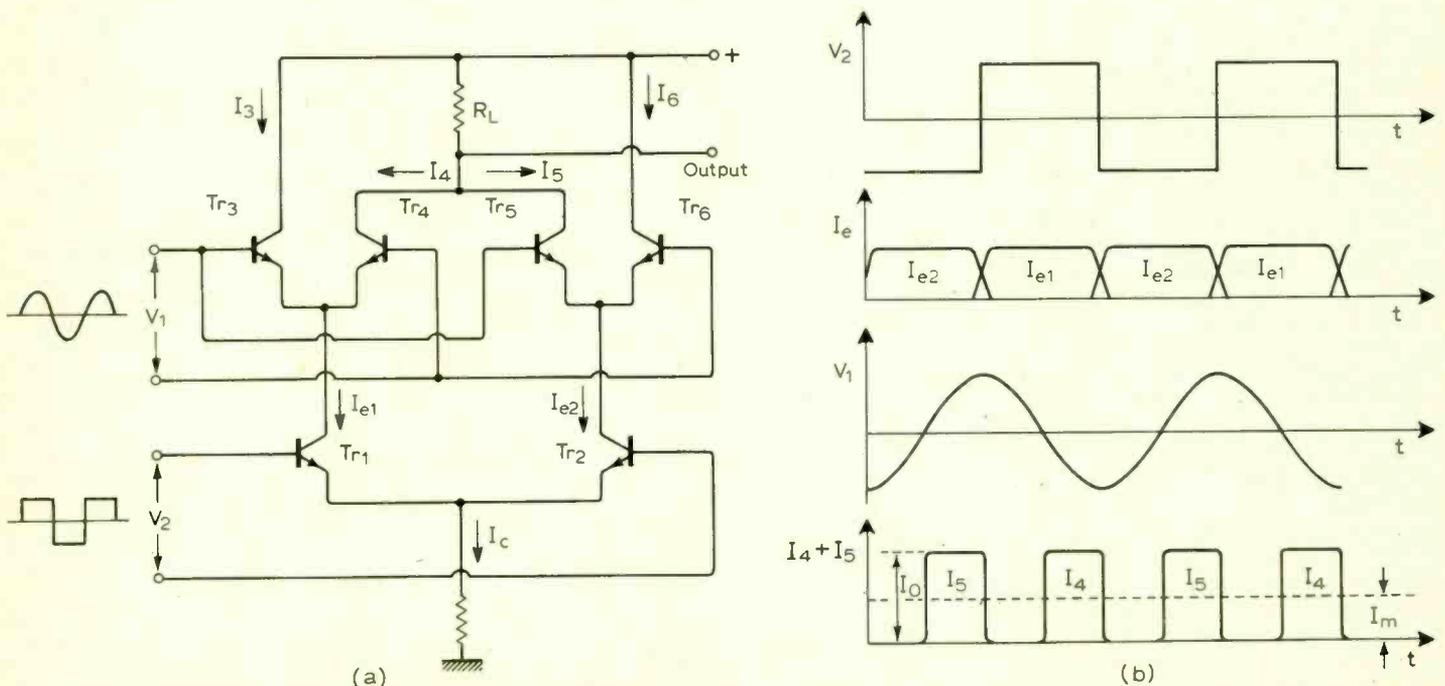


Fig. 1 A monolithic discriminator

Three-dimensional Television

Holography offers possibilities for analysis and reconstruction of stereoscopic images in monochrome and colour

by R. Brown

A successful three-dimensional television system has long been a dream of many people in the television field; but such a system would be very difficult to construct and until recently none of the techniques available has appeared to meet with wide acceptance among the viewing public. Recently, however, the technique of holography has been arousing great interest as a means of producing three-dimensional photographs without using special spectacles, and it seems worth considering whether a holographic television system could be produced. If it could, the received picture would be a tremendous advance on existing two-dimensional systems. In addition to being three-dimensional without the use of special glasses it would have several other characteristics not found in existing 3D systems. If a viewer moved to the right or left objects in the foreground of the picture would move relative to more distant objects so that it would be possible to look around them to see what was behind. In addition, a viewer would have to refocus his eyes to look at distant objects after looking at close objects. In fact, the picture would be

indistinguishable from the original scene. The scenes produced from existing holograms do indeed bear an uncanny resemblance to the original scene, and, what is more, they can be produced in full colour as well as in black and white.

Making a hologram

To understand how a hologram is made it might help if we first took a look at what happens when we view a scene. Any object, however complex, can be thought of as being made up of many thousands of small points. Each of these points, when the object is illuminated by the sun or by artificial light, reflects light in all directions. Each point can indeed be thought of as a point of source from which light waves radiate in expanding spherical shells.

The ideal recording system would be one in which the viewer was presented with exactly the same information in exactly the same form as when looking at the original scene. In other words he should be presented with replicas of the expanding spherical shells of light waves coming from that scene. Ideally, we should dispense with a lens and find some means of "freezing" the light waves from the scene in a photographic emulsion and then "unfreezing" these waves at a later time so that they can continue on towards the eye of the observer. If this can be done the observer will "see" the scene just as it would appear to him had he looked at it directly. This is just what we can do with holography.

Photographic emulsions can certainly record the amplitude of the light waves; but they cannot record that other essential characteristic of a wave—its phase. They do, in fact, respond only to the amplitude or intensity of light waves; but to any engineer it must be clear that one way in which the phase information can be recorded is by using interference effects. This is, however, impossible with conventional light sources because even the so-called monochromatic light sources are in fact generators of a quite wide band of light wavelengths which have random phase relationships. We can, however, produce suitable interference effects by using a laser, which gives a highly coherent monochromatic beam.

To record light waves directly without a lens, the scene or object is illuminated by laser light and some of the light from the laser

is also directed straight on to a photographic plate where it interferes with the light reflected from the scene.

If we take as an example a single point object it can be seen from Fig. 1 that the spherical wavefronts travelling from the point interfere with the plane wavefronts coming direct from the laser. At points where the two wavefronts are in phase the light intensity in the photographic emulsion will be a maximum; at points where the two wavefronts are 180° out of phase they will cancel out and there will be a minimum. Thus there will be a series of dark and light areas on the photographic emulsion. It can be seen from Fig. 2, that in the case of a single point object the spacing of these light and dark areas increases from the top to the bottom of the plate. The brightness of the light areas depends upon the intensity of the light reflected from the point and the spacing of the light and dark areas depends upon the distance of the point from the plate. Thus the recording contains all the information about both the brightness and the distance of the point object. If the object consists of a number of points the light waves reflected from these points will set up a number of different sets of interference patterns and, what is more, the spacing of the lines in the interference patterns will depend upon the relative distances of the points.

To reconstruct an image of the point object the photographic plate is first developed so that the light areas become clear and the dark areas opaque. Then it is illuminated with a laser beam coming from the direction of the original reference beam used during the recording of the hologram. The light passes through the clear areas and each clear area can be thought of as a thin line source of light. The light spreads out from the many line sources and interference occurs between the many different sets of light waves. It can be seen from Figs. 3 and 4 that there will be at least three different sets of wave fronts on the far side of the photographic plate as a result of this interference!

An attenuated version of the illuminating beam will continue on in the same direction because the light from the different opening is in phase in that direction. There are also two other beams going off at angles to this beam. One of these other beams goes off in a direction in which the wavefronts of the light from one opening is in phase with the previous

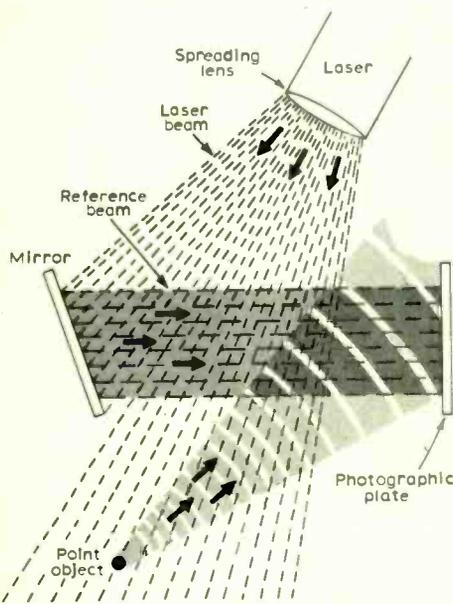


Fig. 1. Making a hologram. The point object to be recorded reflects some of the laser light back towards the photographic plate in expanding spherical shells. There it interferes with the plane waves coming from the laser via the mirror.

wavefronts of the light from the adjacent opening. The other beam is in a direction in which the light from one opening is in phase with the light in the preceding wavefront coming from the adjacent opening.

There is an important difference between these latter two beams. It can be seen from Fig. 5 that both wavefronts are spherical but in the case of the top beam the wavefronts are expanding and in the case of the lower beam the wavefronts are converging. In fact, the wavefronts from the top beam are exactly the same as those that were reflected from the point object during the recording processes. If an observer positions himself on the far side of the photographic plate, these waves will enter his eye and he will "see" the original point object on the far side of the plate. What is more, the position of this point object relative to the plate will be the same as the position of the original object relative to the plate during the recording processes: the observer will indeed see the point as though he was looking through a window in the position of the photographic plate, or hologram as it is called. If the object recorded were more complex, the observer would see each of the points of which it was composed in their proper positions. He would, in other words, see a three-dimensional image of the original object.

The converging spherical wavefronts in the lower beam eventually concentrate into a spot. A photographic plate placed there will record an image of the point object without the need for a lens. Again, if the object is a complex one all the different points in it will be reconstructed and a photographic plate will record an image of the object.

Full colour holograms

Full colour holograms can be made fairly easily if rather expensively by making use of the fact that the angle at which the reconstructed images can be seen depends upon the angle of the reference beam used in the recording process. We can, for example, make a full colour hologram by directing red, blue and green laser beams on to the photographic plate at different angles. The same laser beams also illuminate the scene, of course. To display the full colour image recorded, the hologram is illuminated by red, blue and green laser beams coming from the same angles as during the recording process. If this is done the red, blue and green images are reconstructed at the same spot and the observer sees a full colour image. Each laser beam will also reconstruct images from the interference patterns of the other two beams but these images will be in a different place and if the image is viewed through a suitable mask these spurious images will be blocked.

A more interesting and economically more attractive way of producing full colour images involves directing the three reference beams on to the back of the photographic plate during the recording process.

Holographic television

What, then, do we need to do to transmit holograms by television? First of all, to televise a scene it must be illuminated with high intensity pulsed laser light. Probably several

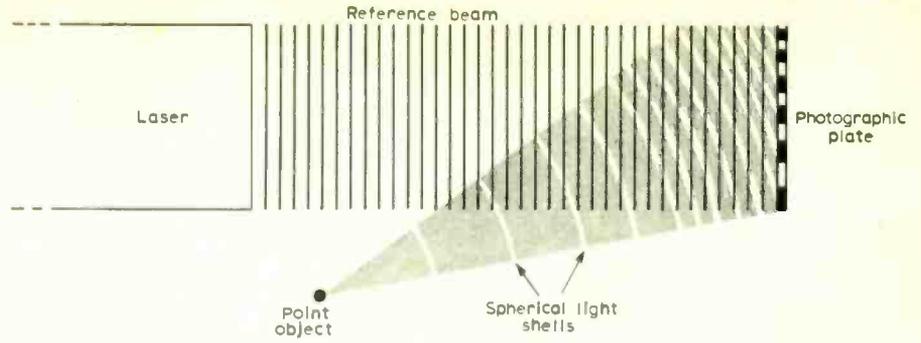


Fig. 2. When the plane wave coming direct from the laser meets the spherical waves reflected from the point object, constructive and destructive interference occurs. This produces a series of bright and dark fringes whose spacing increases down the photographic plate.

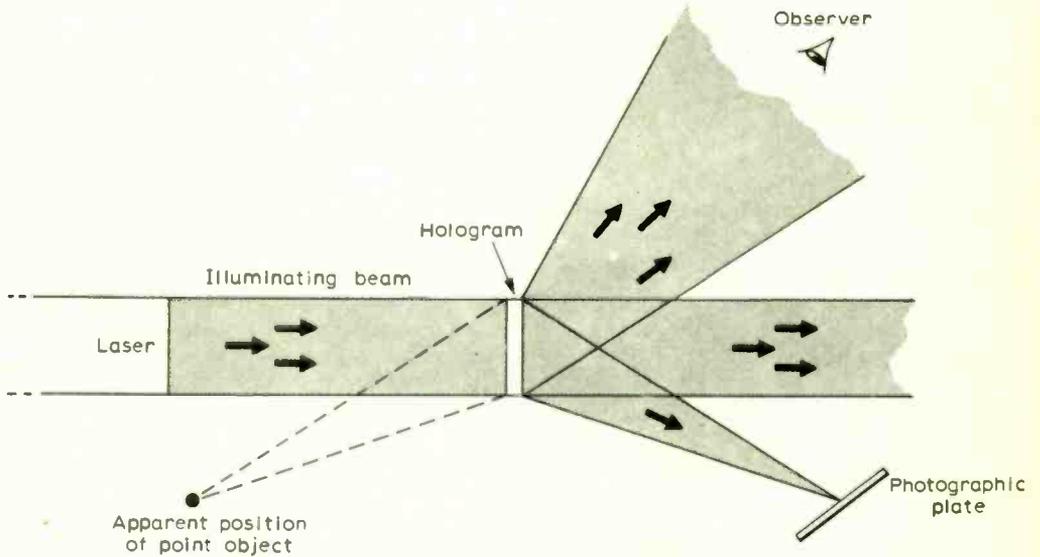


Fig. 3. When a hologram is illuminated with a laser beam three new beams are formed. An observer in the position shown will see the original point object in the position shown. The photographic plate will record an image of the point object without the need for a lens. The third beam is an attenuated version of the illuminating beam.

phase locked lasers would have to be used because the picture would be very harsh if only one laser was employed. Pulsed operation is essential because the scene must remain almost perfectly still during the exposure time of each frame, otherwise the interference pattern will be smeared and made useless. It has been suggested by Professor Leith of Michigan that movement during the exposure must be kept down to less than one-quarter of the wavelengths of the light.² Movement at rates of up to about six metres per second could be allowed if the pulse length were restricted to about ten nanoseconds. This means that it would be possible to record and reproduce images of a person walking quite quickly, but movement much faster than this might present some problems. However, there have been very great strides in the development of high-power short-pulse lasers in recent years and speeds much greater than six metres per second, which was quoted at a meeting in Montreal several years ago, will soon be possible.

There is another rather serious limitation—the relatively short coherence length of lasers. Clearly, there must be no abrupt changes in the phase of the light from the laser between the time the light illuminating the front of the scene has left it and the time

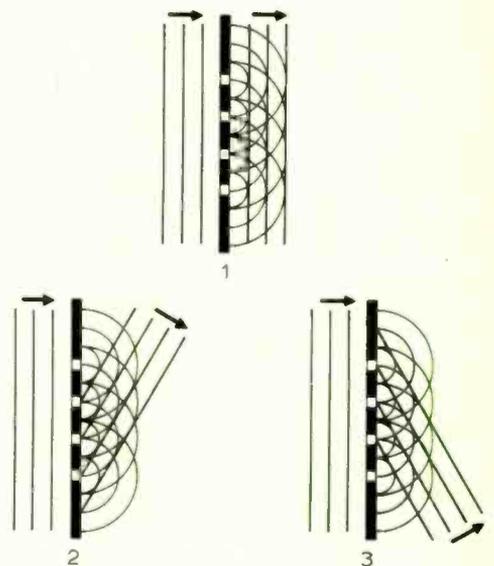


Fig. 4. When the simplest hologram of all, one in which the light and dark fringes are equally spaced, is illuminated with a laser beam the interference between the light getting through the spaced openings produces the three beams in the manner shown in 1, 2 and 3.

that the light illuminating the back of the scene has left it. In other words, the coherence length of the laser beam, that is the distance between points with a constant phase relationship, must be longer than the depth of the scene to be televised. Unfortunately, pulsed ruby lasers, for example, have a coherence length of only several inches and even the best continuously operating gas lasers have coherence lengths of only six feet or so. This means that the width of the scene that can be viewed is limited to a few inches if a ruby laser is used and to a few yards if a gas laser plus a high-speed shutter is used.

Again, however, steps are being taken to reduce the seriousness of this problem. The Radio Corporation of America's Princeton

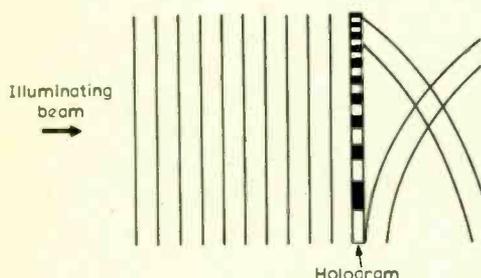


Fig. 5. How the expanding and converging wavefronts are produced when the hologram of a point object is illuminated.

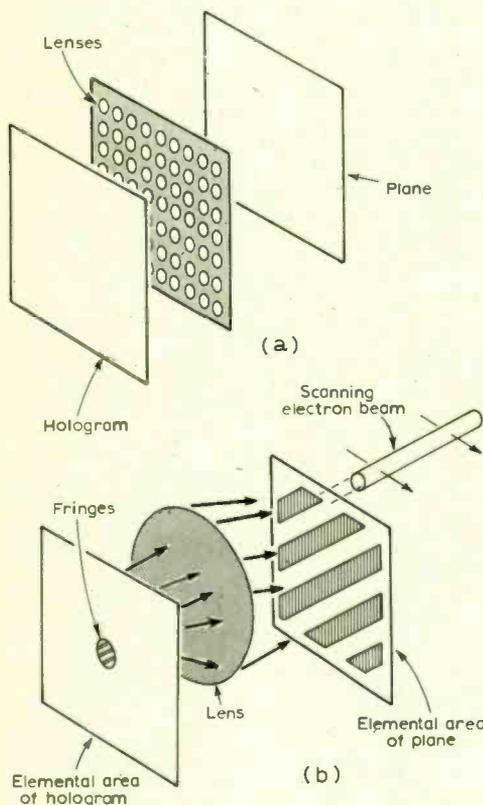


Fig. 6. Reducing the bandwidth requirements by discarding most of the information contained in the hologram. Each of the lenses in (a) selects a small part of the area of the hologram, (b), and magnifies it so that it fills the space allocated to that lens in the plane indicated. It is the very coarse fringe pattern in the plane that is scanned by the electron beam and transmitted.

laboratories have recently demonstrated a gas laser in which one of the mirrors is replaced by a piezoelectrically driven interferometer. This greatly increases the coherence length of the laser and holograms of scenes of much greater depth can now be recorded.

A conventional television camera can be used to convert a black-and-white hologram into a video signal suitable for transmission. The thick holograms recorded with the reference beam on the far side of the recording surface might present more serious problems, but no doubt a solution to them can be found.

The most difficult problems in the way of a successful television transmission system arise from the very large bandwidth requirements. E. N. Leith has calculated that to transmit all the information in a single colour hologram would require about 30,000 times as much bandwidth as a conventional television transmission system.³ This is clearly an impossible requirement at the present time and might still be impossible even if millimetre or laser wavelengths could be used for the transmission link. However, all the detail in the hologram does not necessarily have to be transmitted. If it were, the picture would have a much higher definition than present television pictures. We can thus greatly restrict the amount of information transmitted and still have a three-dimensional picture every bit as detailed as present day two-dimensional pictures.

Several ways of doing this are being investigated. It is, for example, possible to make use of a very attractive feature of the hologram—the fact that the information from every small point in the scene is spread over the whole of the photographic plate. This means that we can tear the hologram in half and still extract the entire scene from either half. This is why computer manufacturers, for example, are very interested in the idea of holographic memories. Tears and scratches have little or no effect because all the information is contained in the undamaged parts of the film. This, of course, is quite unlike conventional photographic memories where even a tiny blemish can destroy important information.

One could, in principle, simply transmit only the information contained in a tiny central area of the hologram. However, the size cannot be reduced far enough because definition is lost as the size is reduced, and too much detail is lost before the bandwidth requirement comes down to a practical figure. In the United States the National Aeronautics and Space Administration has developed a technique in which a metal mask containing

a large number of small holes is placed in front of the hologram at the sending end and a similar mask is placed in front of the reproducing system at the receiving end.⁴ In this technique tiny samples spread over the whole area of the hologram are transmitted. This is sufficient to reduce the bandwidth requirements to practical limits and yet leave a reasonably detailed picture.

An alternative way of dividing a hologram into a number of elements and then discarding all but a tiny portion of each element has been developed by the Bendix Corporation. W. E. Kock, who joined Bendix from N.A.S.A. has pointed out that the optical interference patterns on a hologram correspond to a definition of 50,000 lines an inch, so that on a 4-inch square hologram there are about $(4 \times 10)^{10}$ picture elements as compared to the 250,000 elements present in a 500-line square television picture. He proposes having one small lens for each of the basic picture elements.⁵ As shown in Fig. 6, these lenses will image a few fringes at the centre of each of the basic areas of the hologram into a greatly magnified form that will fill the elemental area in the plane indicated. Producing the tens or hundreds of thousands of lenses may not be quite the formidable task it might appear because Mr. Kock has devised a way of producing tiny zone plates that can perform just as well by a photographic technique.

The coarse fringe pattern formed in the plane (Fig. 6) is scanned by an electron beam as in conventional television and the resulting signal is transmitted to the receiving end. There the pattern in the plane is reconstructed and a second array of lenses de-magnifies the fringes back to their true optical fringe size. In this way a great deal of the information is discarded but again a 3D picture of acceptable definition is obtained.

Holographic TV receiver

So far as the receiver is concerned the sign circuits would be quite conventional up to point; certainly the extra electronic processor circuits would not present any serious problems. Also, once the hologram had been reproduced it could be illuminated with a laser or white light to reproduce the scene in the same way as standard holograms are illuminated. The real problem is going to be reproduced

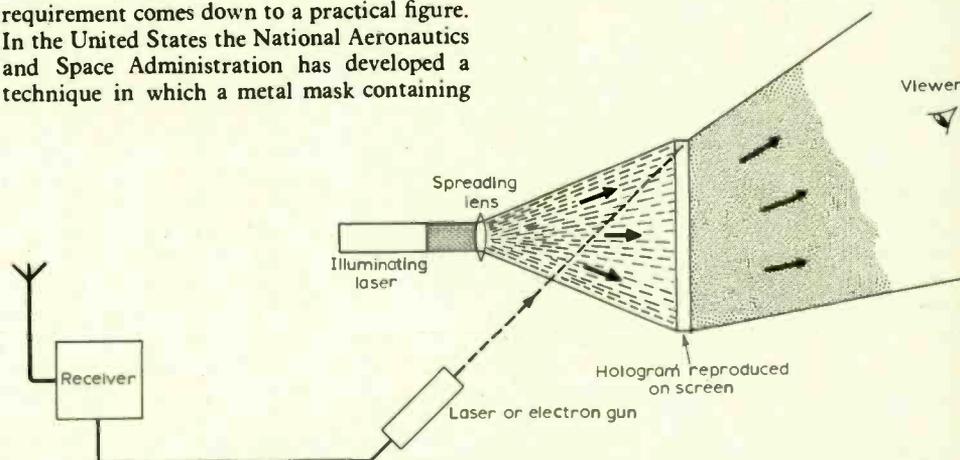


Fig. 7. A holographic television receiver. The intensity of the laser or electron beam (depending upon the system) is varied in accordance with the hologram interference pattern. This reproduces the hologram pattern on the screen which is then illuminated by the illuminating laser and the viewer sees reconstructed 3D images.

ducing the interference pattern. J. Upatnieks, a colleague of E. N. Leith, told the Montreal meeting referred to above that there appeared to be two techniques which after considerable development might be used to reproduce the hologram.

One of these techniques is based on the Fischer system which was developed in the early 1940s in Geneva by Fritz Fischer as the basis of a large screen theatre television receiver.^{7 8} It consists basically of a thin film of oil between two systems of shutters which are placed between the light source and the screen. When the oil film is perfectly smooth the shutters completely block the light. To produce a picture, the film is scanned by an electron beam which distorts its surface. This diffracts light past the system of shutters and illuminates the screen in the appropriate places to produce the picture. In principle there would seem to be no reason why some modification of the basic Fischer system could not be used to produce the characteristic hologram interference pattern.

The other proposed solution to the problem uses photochromic glass. This glass has been known for over a century and possesses the useful characteristics of darkening when exposed to light or other electromagnetic radiation close to the visible part of the spectrum. In a hologram television receiver, this darkening could be produced by a laser beam scanning across the glass from side to side and up and down in much the same way as the electron beam scans a conventional cathode-ray tube screen. Varying the intensity of the laser beam would vary the amount of darkening of the glass and so the hologram patterns could be reproduced.

There are several hundred photochromic compounds known. They all involve the use of atoms or molecules which are bistable in that they can have two states with different atomic, molecular or electronic configurations. The molecules are colourless in their normal state and darken as the result of switching over to their other state when light shines upon them. When the light is removed they switch back to their original state.^{9,10}

Silver chloride glass sensitive to the ultraviolet region of the spectrum might be suitable for use in a holographic television receiver. It is thought that the colouring effect in this glass is due to the formation of neutral silver atoms as in ordinary photographic film. All the radiation is then captured by the silver. This process is non-reversible in the case of photographic film; but in photochromic glasses, because of the extremely small size of the crystals, the process reverses when light is removed. The much greater volume of the crystal in a photographic emulsion encourages the neutral silver atoms to aggregate into stable colloidal particles; but this does not occur in glass because the crystals are about one sixty-millionth the size of the photographic emulsion crystals. Other factors, such as the impermeability of the glass, are also important. At the moment all of the photochromic compounds available are slow acting by the standards required for a television system. But, as yet, there has been no incentive to develop fast acting photochromic glass.

All the basic requirements for 3D colour television would seem to be present; but there is equally no doubt that the problems that

remain to be solved are very formidable. Even if holographic television was technically feasible it is very unlikely that we would see it in use for broadcasting for several decades because of the high cost of the equipment. Nevertheless, there are many applications where the transmission of even still 3D pictures would be very useful. The advantages of a having a 3D television system on a space probe on the surface of, say, Mars, which could transmit still pictures only, would, of course, be very great. This perhaps explains the N.A.S.A. interest in the technique.

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Announcements

The **International Aerospace Instrumentation Symposium** erroneously announced for March 23-26 at the College of Aeronautics, Cranfield, will in fact be held on those dates next year. Further information may be obtained from N. O. Matthews, Department of Flight, The College of Aeronautics, Cranfield, Beds.

The **Manchester Electronic Instruments Exhibition** organized for the past two years on behalf of a group of 16 manufacturers is being enlarged this year but will again be held at the Hotel Piccadilly, from September 23rd to 25th. The organizers, Industrial Exhibitions Ltd, are this year arranging a similar exhibition (restricted to 16 companies) at the Hotel Leofric, Coventry, from September 16th to 18th.

A new M.Sc. degree course in **microwave and communications engineering**, organized jointly by the Electrical and Electronic Engineering Departments of the Universities of Leeds and Sheffield, will begin in October 1969.

An international conference on **earth station technology** for satellite communication, sponsored by the I.E.E., I.E.R.E. and other institutions, is to be held during October 1970 at the I.E.E., Savoy Place, London W.C.2.

A **new standards laboratory** installed by G. & E. Bradley Ltd., at its Neasden, London, factory, has been approved by the British Calibration Service for a wide range of measurements at radio frequencies. This is the first laboratory to obtain B.C.S. approval for r.f. calibration.

The **Radio Advisory Service**, which was established jointly by the London Chamber of Shipping and the Liverpool Steam Ship Owners' Association some years ago, is no longer a separate organization. It recently became the Radio and Navigation Department of the Chamber of Shipping, 30/32 St. Mary Axe, London E.C.3.

The names of two **RCA companies in the U.K.** have been changed. RCA Ltd, of 50 Curzon Street, London W1Y 8EU, will in future operate as RCA International Ltd. The title RCA Ltd has been adopted by what was RCA Great Britain, of Sunbury on Thames.

Corning Glass International, S.A., the Belgian-based subsidiary of Corning Glass Works of America, have opened a London Office at 3 Cork Street, W.1. Corning subsidiaries with facilities in England include Electrofil Ltd in Sunderland and Miniature Electronic Components Ltd in Woking.

Motorola Inc. is to establish a further subsidiary company in Britain with the title **Motorola Automotive Products Ltd**. The company will be located at Stotfold, near Hitchin, Herts, and will provide complete engineering, production, marketing, sales and service facilities for the Motorola eight-track stereo tape player for cars.

Brookdeal Electronics Ltd, 2 Myron Place, Lewisham, London S.E.13, manufacturers of signal recovery equipment, have appointed J. Arndt Jensen, Kongevejen, Allerød, Denmark, and Into Oy, P.O. Box 10153, Helsinki 10, Finland, as agents for their products.

B & K Instruments Ltd, 59 Union Street, London S.E.1, have been appointed distributors of the range of variable frequency filters, variable frequency a.c. power sources and laboratory power amplifiers manufactured by the **Krohn-Hite Corporation**, of America.

G. A. Stanley Palmer Ltd, Island Farm Avenue, West Molesey Trading Estate, Surrey, have been appointed agents for **Arco**, of Bologna, Italy, manufacturers of electronic components.

The digital systems department of Ferranti Ltd, has been awarded a contract to supply **SHAPE Technical Centre** at The Hague, with an FM1600B computer and associated peripheral equipment. The computer will be used in experimental and research work.

A contract for the design, construction and flight testing of a full-scale experimental **airborne early warning radar** has been placed by the Ministry of Technology with Elliott-Automation Radar Systems Ltd.

International Marine Radio Company Ltd, of Croydon, have received an order worth over £120,000 for **marine communication and navigation equipment** from Scottish Ship Management Ltd. The equipment will be installed in 12 new bulk carriers on order from British and Norwegian yards.

The Marconi Company has won an order valued at almost £250,000 to provide remote-controlled, high-frequency **radio communications equipment** at Nandi Airport in Fiji.

The London office of **Marconi International Marine Co. Ltd**, is now at 30/34 New Bridge Street, E.C.4. (Tel: 01-236 8113; Telex 884729).

The marketing department of **Racal Instruments** has moved from Crowthorne, Berkshire, to Bennett Road, Reading, Berks. (Tel: Reading 85571.)

V. N. Barrett & Co. Ltd., suppliers of high-vacuum and scientific equipment, have moved to new premises at 1 Mayo Road, Croydon, Surrey, CRO 2QP.

Fluke International Corporation have moved to larger factory and office premises at Garnett Close, Watford, WD2 4TT.

Cadmium Nickel Batteries Ltd has moved from factories in Park Royal to premises at Castle Works, Station Road, Hampton, Middx. (Tel: 01-979 7755).

News of the Month

Skynet terminal delivered

Skynet, the military satellite communications system, will begin to operate early in 1970. Two satellites, one in operation and the other a standby, will move in a synchronous orbit 23,000 miles above the Indian Ocean. Of the nine earth stations to be employed, five will be fixed, two (to be built by Plessey) installed in the assault ships H.M.S. *Fearless* and *Intrepid*, and two will be capable of transportation by air. The whole system will provide interference free communication for British armed forces, and nation-wide communication from the Atlantic to the Far East, including Hong Kong.

The satellites and launchers, and some specialized control and monitoring equipment, are being built in the U.S.A. under an agreement with the U.S. Government which allows the U.K. to benefit greatly from the American space investment. The satellites contain some British designed equipment and are capable of meeting the conflicting requirements for communicating to large and small earth-stations simultaneously. The operating functions of the satellites, and their positions in the sky, will be controlled

from the U.K. command and monitoring station at Oakhanger, Hants. For long-life (3-5 years) switchable duplicate equipment has been installed in each satellite. The first satellite will be launched late this summer.

G.E.C.-A.E.I. (Electronics) has handed the first of the four air-transportable earth stations over to the Ministry of Defence. The terminal was designed and built in only 18 months.

Each terminal is made up of three basic sections each light enough to be carried by standard transport aircraft and helicopters. Once 'on-site', six semi-skilled men can erect it, and 'lock' it on to the satellite's wavelength, in only three hours. Each station's 7m diameter reflecting dish provides a number of voice channels, and is assembled from 12 petal sections.

Base-band and i.f. circuitry is housed in a control unit separate from the aerial structure. From the unit, in the transmit mode, processed information at the i.f. enters a travelling-wave tube amplifier feeding a klystron. The standard power output is about 5kW. For the reception of satellite signals a Ferranti liquid-nitrogen-cooled pa-

rametric amplifier is employed.

The three other stations will be completed by the middle of this summer.

At Christchurch, Hants., another terminal will support the Skynet project by making highly accurate measurements for initial calibration and testing of the spacecraft in orbit.

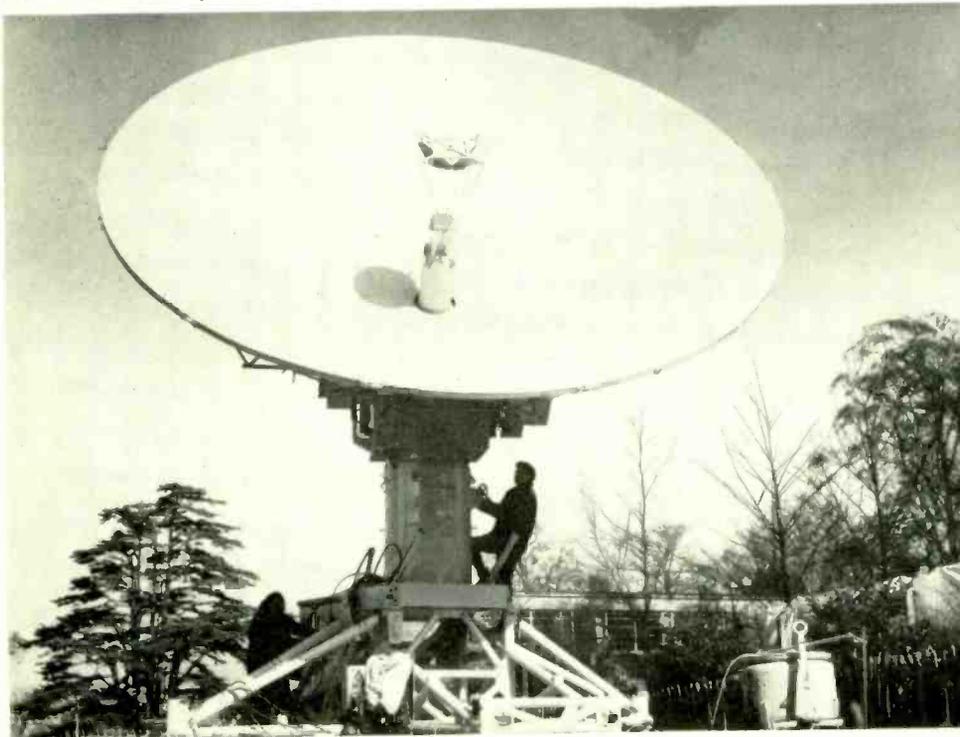
Computer-aided design presses on

A massive four-day conference on computer-aided design—the collected papers weigh 3½ lb—has just ended at Southampton University. A short while earlier Racal Research Ltd announced that the electronic c.a.d. service called "REDAC" which they started in 1966* now has 50 major British companies using it. At the time of launching there was some scepticism about the value of such a service in electronics design work and, indeed, individuals in Racal feel that it might have been rather "oversold", but since then the Ministry of Technology has come in as a partner, a good deal of experience has been gained and the service has apparently consolidated itself.

The Racal establishment, at Tewkesbury, Glos., consists basically of a digital computer (Elliott 4130), with means for transmitting and receiving customers' data (Datel 200, Telex, phone, post) and 25 engineers for translating customers' electronic design requirements into forms suitable for computer processing. The engineers are also continuously engaged in up-dating information stored in the computer (mainly component parameters); developing computer programmes; making component measurements producing equivalent-circuit device "models" suitable for computer operations training customers; and other tasks to do with the day-to-day development of the service. At present there are 31 computer programmes available to customers in a manual. Some of these programmes are directly concerned with particular types of electronic circuits. For example, one of them calculates, and if required optimises, the component values of an active RC filter to give required bandpass response with gain. The programme gives a full nominal component list and the results of worst-case d.c. and a.c. analyses. Other programmes are of more general applicability, such as calculating the harmonic content of a waveform over a specified band of frequencies, or computing the elements of a hybrid- π model of a transistor from the measured 'y' parameters.

The main justification for operating such a service is, of course, economic—the saving of engineers' time on the innumerable calculations that should be done (but often aren't) to ensure that a reliable design is obtained. This is particularly important in tolerance sensitivity analysing and optimising the component values of electronic circuits intended for mass production. To do such work properly one must calculate a complete set of performance figures (e.g. gain, frequen-

7 metre diameter Skynet dish



* "Computer-'designed' Circuitry, *Wireless World* July 1966 p.373.

response, noise) for every possible value within tolerance of every component or device in the circuit—a huge task far beyond the capabilities (or willingness) of a computer-unaided engineer. The main limitation of the service seems to be that the customer concerned with active circuits is at present restricted to a small range of particular circuit topographies—those for which computer programmes have been written—and if he has some other configuration outside of this range his work cannot be handled immediately, or at least fully.

In the June issue we hope to report on some aspects of the Southampton conference referred to above.

E.I.D. apprentices

The four-year apprenticeship scheme introduced by the Electrical Inspection Directorate (Ministry of Technology) in 1955 with five boys now has an annual intake of over 70. The total number of trainees going through the centre is about 250. Recently the title of E.I.D. was changed to Electrical Quality Assessment Directorate (E.Q.D.) but the programme of basic training at the school which forms part of the E.Q.D. headquarters at Aquila, Bromley, Kent, remains unchanged.

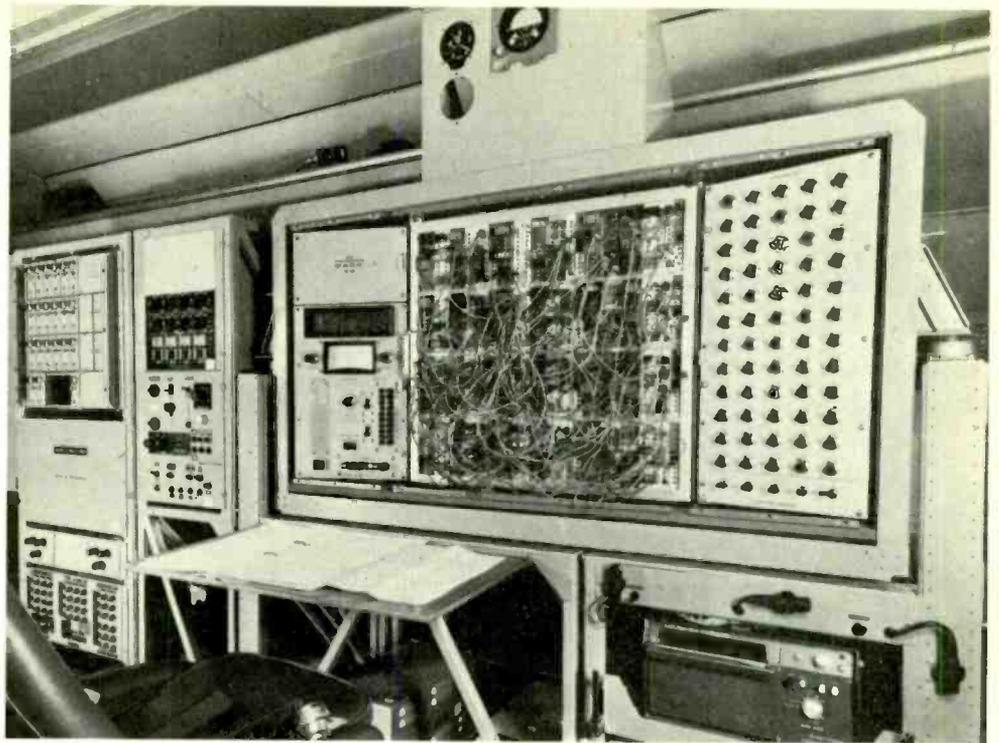
The apprentices are normally placed in courses on block release at Bromley College of Technology and follow the National Certificate course (electronics or telecommunications) or City & Guilds technician course. In addition to a full electronics training the apprentices also cover basic mechanical engineering practices.

The necessary qualifications for entry to the apprenticeship scheme is that the boys must be studying for G.C.E. 'O' level or C.S.E. in mathematics, physics, or an acceptable science subject, and must be between sixteen and eighteen years of age. The period of apprenticeship may be extended in respect of those boys who wish to complete Higher National Diploma, Bachelor of Science or other advanced academic courses. At present five are taking B.Sc. and four H.N.D.

At the annual prize-giving on April 2nd the recipient of the Rowland Memorial Cup for the best electronic work of the year was A. J. Smith, of Maidenhead, Berks.

Computer speeds aircraft blind landing experiments

A new development in the blind landing experimental programme being carried out by the Blind Landing Experimental Unit at R.A.E., Bedford, involves the use of a small-scale analogue computer. It is incorporated into a standard autopilot in a Comet B aircraft and in conjunction with a variety of sensors and an inertial platform, it enables rapid changes of equipment parameters to be made during investigation of a wide range of control laws. The computer, model TR48 supplied by Electronic Associates Ltd, is "ruggedized" to withstand the rigours of



Interior of the Comet 3B showing the E.A.L. computer and patchboard

airborne use. "Automatic Landing in Airline Service" was the subject of a 6-page article by R. E. Young, in the November 1967 issue of *Wireless World*.

The current automatic landing situation is that Tridents of B.E.A. and Super VC10s of B.O.A.C. have been making automatic landings on scheduled services in Europe and North America although always in conditions of good visibility. The ultimate objective is to make the blind landing so safe and reliable that aircraft can operate in any weather conditions, even dense fog, with no reduction in movement rate, i.e. no change in the flight schedule. Experiments are being conducted in an area within the restricted straight-in approach at a shallow angle of 3°, dictated by international agreements, using the existing instrument landing system. Those now in progress are concerned with improving existing control laws and at present a system is being studied which mixes inertial terms with the main i.l.s. guidance signals. The i.l.s. is susceptible to interference, especially that caused by reflections when other aircraft are taking-off in the path of an aircraft making a landing, and inertial mixing provides the possibility of making the flight control system less susceptible to such interference.

The difficulty at R.A.E., until use was made of the TR48 computer, was that in order to introduce a new or different factor into a test flight, the autopilot electronics required to be dismantled for wiring modifications, to provide a change of operating characteristics. Now, with the computer, the required parameters can be programmed before take-off and switched-in during flight. A second TR48 computer is installed in a flight simulator in a ground laboratory and programmed via a large patchboard. When a successful landing has been made on the simulator with the required inputs fed into the autopilot system, the actual patchboard is then taken from the simulator and connected to the computer in the aircraft for a

comparative flight test. Recordings of flight activities for subsequent analysis are made on a 14-track tape recorder and on a chart recorder.

The computer is used in an experimental role only and one would not be installed in operational aircraft. At some stage in development of blind landing, safety standards acceptable to airline operators and the Air Registration Board could be optimized in the autopilot which would then be constructed in conventional size and housed in the equipment bay in the normal way. In all, well over 20,000 blind landings have been accomplished by the B.L.E.U. at Bedford and at London Airport. The A.R.B.'s safety target is that there should be not more than one fatal accident in 10 million landings. Although control performance is the concern of R.A.E., equipment reliability would be the responsibility of the manufacturers. It was said during a demonstration of the blind landing equipment at Bedford that if aircraft movement could be reliably maintained in all weathers it would be possible to dispense with the excess fuel carried to cater for a possible diversion from the destination airport. As an example of the possible saving involved figures were quoted from the Concorde's estimated performance. The passenger payload of this aircraft is only 6% of the all-up weight but the excess fuel carried is 10%.

Home-made X-rays

According to a report in the *Daily Telegraph* a two-year survey of 5,000 colour TV receivers in Long Island, U.S.A., has shown that 20% of them are emitting potentially dangerous X-rays. Of 37 different makes of receiver at least one of each make was found to be radiating at more than 0.5 milliroentgens an hour which is said to be

the danger level established by the National Council of Radiation and Measurement in 1960. The report did not state if the radiation was emanating from an area on the receiver to which viewers are normally exposed.

Optical fibre telecommunications

The Post Office, having staked its claim to an early, God-given medium of communication ("Let there be light"), is now thinking seriously of using it for the large-bandwidth telecommunications systems of the future. At present the optical fibre waveguide seems to be the most attractive way of conveying the light waves, according to a paper given by F. F. Roberts (P.O. Research Department) at an I.E.R.E. conference on lasers and opto-electronics at Southampton University. In common with the piped optical and millimetre-wave systems, it offers a transmission attenuation substantially independent of bandwidth "up to any bandwidth of interest". All three systems are expected to be cheaper per channel-kilometre than coaxial cable for bandwidths greater than certain break-even values. But the optical fibre system should be "appreciably easier" to install than the other two in a congested country like Britain. The main problem, discussed at length by Roberts, seems to be in finding a suitable optical fibre material that will keep the transmission losses (absorption and scattering) down to a practical figure—provisionally set as a target of 20dB per kilometre of waveguide.

What is envisaged at present is a waveguide consisting of a $5\mu\text{m}$ -diameter oxide glass central core surrounded by a $100\mu\text{m}$ -diameter cladding of similar material

but of different refractive index. Optical waves of $600\text{--}1,000\mu\text{m}$ (the red end of the visible spectrum) would be launched into this guide by a solid-state laser (e.g. gallium arsenide), propagated in the HE_{11} mode, and received by a solid-state diode (e.g. silicon). At intervals along the transmission path there would be repeaters, each containing a diode receiver, a solid-state amplifier and a laser transmitter. The bandwidth available would be several GHz for distances of about 1km between repeaters.

Waveguide of this kind should not be confused with the fibre-optic "light-pipes" used in punched-card readers and other viewing applications: these are very much thicker and have thousands of different modes of wave propagation; consequently, because of interference effects, their bandwidth is less than 1MHz for a 1km length of material.

Amateur cloud-cover pictures

In 1967 Ivor le Mercier (4S7LM), president of the Radio Society of Ceylon, set about designing and building a receiver to enable him to record cloud-cover pictures transmitted by the satellite Nimbus-2.

The receiver line-up was as follows: two r.f. stages (AF139), mixer (OC171), crystal oscillator (OC170), tripler (OC171), four 10.7MHz i.f. stages (OC171), two a.f. stages (OC71) and an output stage (OC810). The receiver functioned well and required 0.8 μV for 27dB quieting.

The aerial consisted of a 6-turn helix supported as a wooden boom 3.5m (11.5ft) long and a 1.9m square (6ft) ground plane of galvanized mesh. The aerial was mounted in gimbals, firstly being roughly aligned with the satellite's orbit and then swung by hand to track the satellite. A monitor loudspeaker



One of the pictures recently received by Ivor le Mercier

mounted near the aerial facilitated this process.

Synchronization was achieved using a phase locked oscillator at 2400Hz, divided down to 20Hz, based on a circuit by W. G. Andersen which appeared in the November 1965 issue of *QST*.

Unfortunately by the time the equipment was completed Nimbus-2 was out of commission; however, in June 1968 pictures from ESSA-6 were received and recorded satisfactorily.

To produce complete cloud-cover pictures, signals from the receiver's discriminator are recorded on tape and "played back" through an oscilloscope fitted with a 35mm camera.

Student paper contest

Kenneth Gray, a research assistant at Woolwich Polytechnic, has been chosen to represent the United Kingdom and Republic of Ireland Section of the I.E.E.E. at the Institution's regional student paper contest in Morieux, Switzerland, on 23rd May.

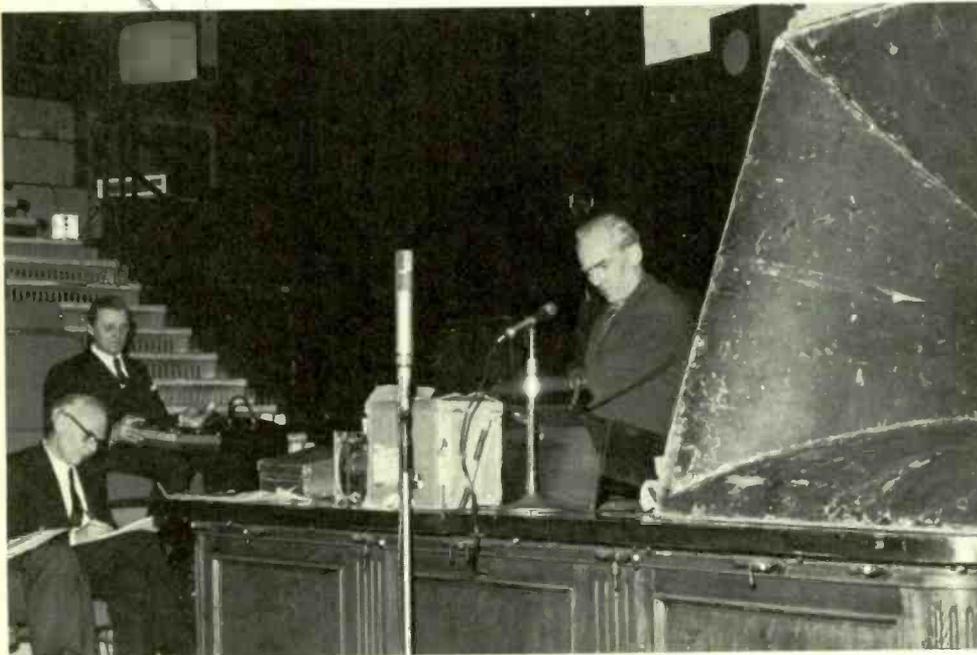
The Regional winner will later compete with other Regional winners in New York to determine the overall winner.

Mr. Gray's paper describes a Fourier method of investigating transient acoustic spectra and its application to human speech and is relevant to the problem of speech communication with computers.

New recording process ?

A member of *Wireless World's* staff recently received some literature from *Reader's Digest* inviting him to buy a set of gramophone records ("Mood Music for Listening and Relaxation") made by RCA engineers using an amazing new process called "Cyclophon Sound". The RCA people in Britain were unable to discover anything about it. Fallir back on etymology, one finds that "cyclo" from the Greek, means circular, or perhaps in this case, rotating; while "phonic", also from the Greek, means relating to sound. The word "Sound", one must assume means sound—though perhaps a different kind of sound, not quite the same as the "phonic" sound. From this analysis one deduces that the new process involves something that is circular, perhaps rotating, and produces sounds. What could it possibly be?

Paul Voigt's contributions to audio were the subject of a meeting of the British Kinematograph, Sound and Television Society at the Royal Institution of Great Britain on March 26th. His work in sound recording was discussed and demonstrated and here Ralph West is shown demonstrating an early Tractrix horn from which Voigt developed his famous corner horn. On the left is Peter Walker who chaired the meeting. Paul Voigt, who is 67 and now lives in Canada, sent a recorded message.



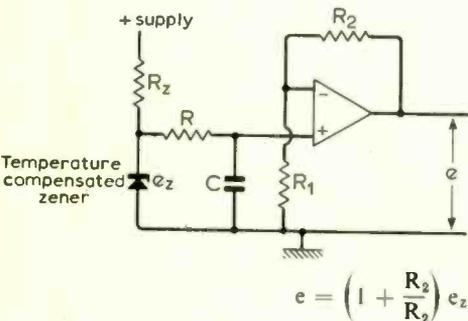
Operational Amplifiers

4. Applications

by G. B. Clayton,* B.Sc., A.Inst.P.

In instrumentation a need sometimes arises for a precise d.c. voltage reference or for a variable direct voltage that can be set accurately with a calibrated potentiometer. In such cases it is necessary to avoid loading the voltage standard if its stability is to be ensured. Also, a potentiometer must not be loaded if its dial calibration is to be accurate. The high input impedance and low output impedance of an op. amp. used as a voltage follower makes it valuable as a buffer in such

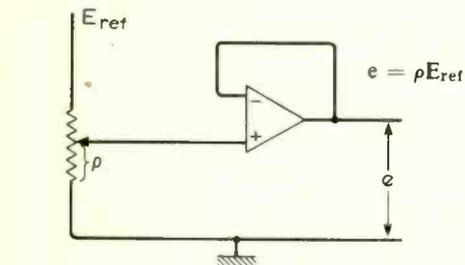
Voltage Reference.



$$e = \left(1 + \frac{R_2}{R_1}\right) e_z$$

cases. In the circuit shown R_z is used to set the current through the reference zener at that value for which the temperature coefficient of the zener is a minimum. R_2 and R_1 are adjusted to compensate for tolerance in the zener voltage and so obtain the precise voltage required at the output. The RC filter may be added to attenuate noise and pick up.

Calibrated Potentiometer Voltage.



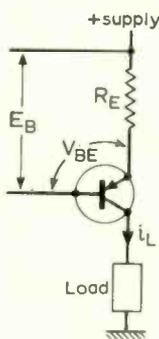
The high input impedance of the follower above does not load the potentiometer and therefore does not affect its calibration.

*Liverpool College of Technology

Current Sources

A requirement that sometimes arises is that a load be supplied with a constant direct current that is linearly related to some input voltage. A single transistor used in the manner shown is often employed to supply a relatively constant current.

Single Transistor Current Source.

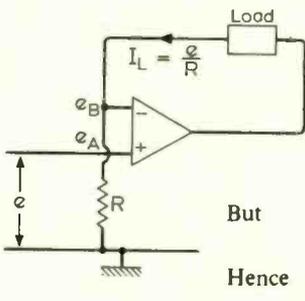


If $E_B \gg V_{BE}$ and if the transistor current gain is high the load current

$$I_L \approx E_B/R_E$$

In applications requiring a higher degree of precision than is possible with the single transistor circuit, op. amps. may be used to advantage as current output devices. In cases where the output current capability of the op. amp. is insufficient a booster amplifier may be added.

Current Source. Follower Connection (Floating Load).



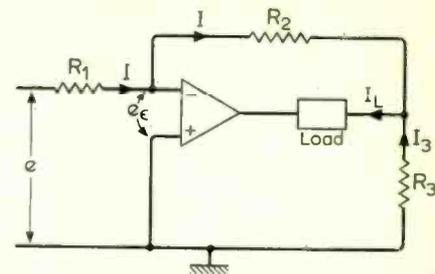
$$e_B = I_L R$$

But $e = e_A = e_B$

Hence $I_L = \frac{e}{R}$

Features. The circuit is similar to the follower with gain with the load replacing the feedback impedance. The load must not be earthed. All follower connections are of course subject to common-mode limitations; in this case the input voltage e represents a common-mode signal and it must not be allowed to exceed the rated maximum for the amplifier.

Current Source. Inverting Connection (Floating Load).



With the error voltage $e_e \rightarrow 0$ the voltage across R_2 and R_3 must be the same

$$I R_2 = I_3 R_3 \quad \text{and} \quad I = \frac{e}{R_1}$$

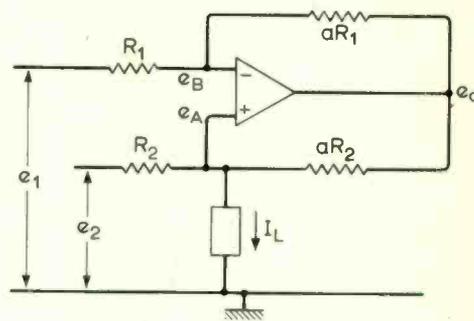
The load current

$$I_L = I + I_3$$

$$I_L = I \left(1 + \frac{R_2}{R_3}\right) = \frac{e}{R_1} \left(1 + \frac{R_2}{R_3}\right)$$

Features. The circuit uses a form of the inverting amplifier and draws an input current $I = e/R_1$. The load is above earth as before; it may be a complex load. The circuit can be used as a deflection coil driver.

Current Source (Earthed Load).



$$\frac{e_1 - e_B}{R_1} = \frac{e_B - e_0}{a R_1}$$

$$e_0 = e_B (1 + a) - a e_1$$

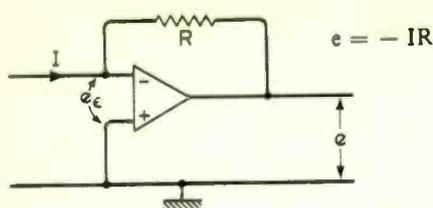
$$I_L = \frac{e_2 - e_A}{R_2} + \frac{e_0 - e_A}{a R_2}$$

$$I_L = \frac{e_2 - e_A}{R_2} + \frac{e_B (1 + a) - a e_1 - e_A}{a R_2}$$

But $e_A = e_B$, hence $I_L = \frac{e_2 - e_1}{R_2}$

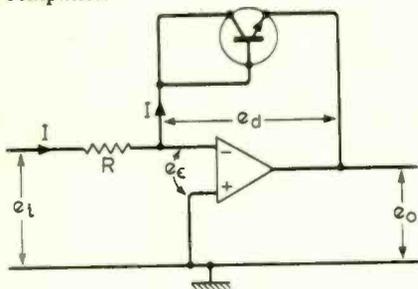
Features. In addition to the negative feedback applied to the inverting terminal of the amplifier, the circuit uses a positive feedback loop to the non-inverting terminal to achieve a very high effective load impedance and thus a constant load current. One side of the load is conveniently at earth potential. Two input voltages may be used, both referred to earth. If only one input signal is used and it has the appropriate polarity, it is preferable to earth the e_2 terminal and use the e_1 terminal as the current determining input. The input current drawn from the source e_1 is determined by the resistor R_1 which can be made quite large to limit the input current. If e_2 is made the current determining input the short-circuit load current is drawn directly from e_2 through R_2 .

Current to Voltage Transducer.



Features. The circuit is essentially the inverting amplifier configuration with the input resistor omitted. It represents a simple but convenient method of current measurement. With the error voltage $e_e \rightarrow 0$ the circuit introduces negligible input voltage drop but the output voltage is developed at the low-impedance, high energy capability output terminal of the amplifier. The high current sensitivity of the circuit makes it useful as a null detector. Null detectors are often used off null, and under these circumstances this simple circuit would saturate and give little indication as to how far off null it was. When used as a null detector it is convenient to arrange a modified non-linear response characteristic (see right).

Log. Amplifier.



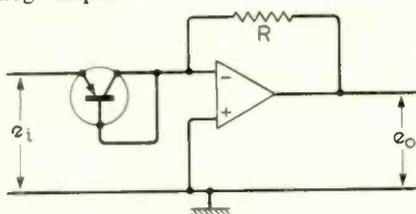
$$e_d = \text{const.} \log_{10} \frac{I}{I_0}$$

With $e_e \rightarrow 0$, $I = \frac{e_i}{R}$ and $e_d = e_o$

This gives $e_o = \text{const.} \log_{10} \frac{e_i}{R I_0}$

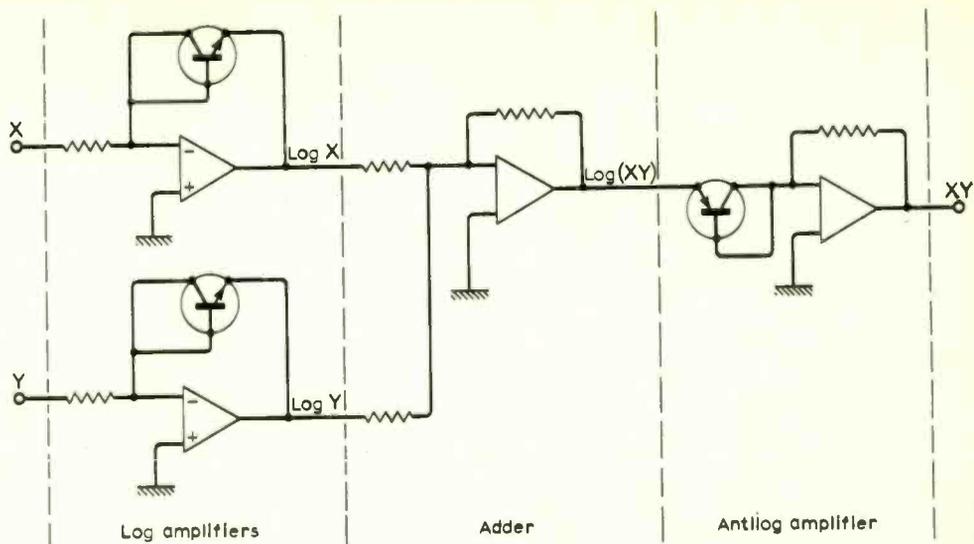
Features. The inverting amplifier is used with the feedback resistor replaced by a device exhibiting a logarithmic characteristic. Log. amplifiers require particular attention to bias current and input offset adjustment and to choice of logarithmic device if reliable operation is to be achieved over several decades. Interchanging the position of the logarithmic device and the input resistor, as shown below, gives an antilog response.

Antilog Amplifier.

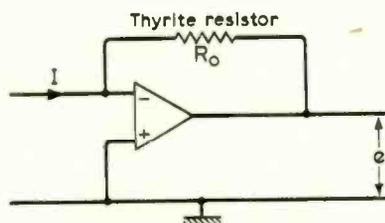


Combinations of log and antilog amplifiers may be used to generate a variety of functions. The principle of operation of a log multiplier is illustrated above.

Log Multiplier.

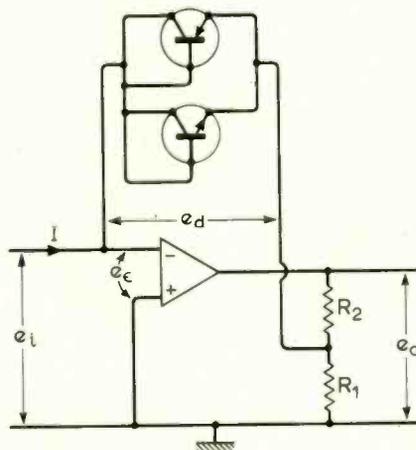


Null detector.



R_0 is a non-linear resistor which decreases for increase in current through it. Sensitivity is maximum near $I = 0$

Null Detector (Log. response).



$$e_d = \text{const.} \log_{10} \frac{I}{I_0}$$

With $e_e \rightarrow 0$

$$e_d = e_o \frac{R_1}{R_1 + R_2}$$

Hence $e_o = \left(1 + \frac{R_2}{R_1}\right) e_d$

$$e_o = \text{const.} \left(1 + \frac{R_2}{R_1}\right) \log_{10} \frac{I}{I_0}$$

Features. The circuit makes use of the approximate logarithmic relationship that exists between current and voltage for a diode-connected transistor.

Corrections

“Simple Class A Amplifier”

Three small errors crept into the article published last month. In Fig. 8, showing the modified circuit for high input impedance the rail-dropping resistor should be 3.9 (2.2k for stereo) not 39k (22k for stereo). In the last line of Table 3 the transistor complement should be 2 x MJ480 and 2 2N697 to correspond with Fig. 9 (b). The photograph on page 152 showing layout of single channel has been wrongly lettered with respect to T_{r1} connections. Reading up from the bottom the correct letter order is e, b,

Although in Fig. 3 the output transistors are boldly marked MJ480, the 15-Ω version requires MJ481s with a 2N1613 driver. This was stated, perhaps a little obscurely, at the end of the third paragraph on page 150.

“Acoustic Absorption Materials”

A printer’s error reversed the meaning of the sentence at the end of the first paragraph on page 173 (April). It should read “It is not easy to ensure . . .”

“Why not angular frequency?”

Mr. Whitehead miscalculated the frequencies for 5,000 and 10,000 rads/sec in the letter on p. 178 (April); they are 796 and 1592 Hz.

Is there a future for the

Television V.H.F. Bands?

A survey of the British television scene as it affects viewers

It has been widely reported in the radio trade press that a large proportion of the viewing public was unaware that when BBC-1 and I.T.A. programmes become duplicated on u.h.f. these programmes will be transmitted in colour. It would be instructive to learn how many people were aware that the programmes were to be duplicated anyway and what advantages they thought it had for them. For someone who is receiving a perfectly satisfactory 405-line picture on v.h.f. (and the broadcasting authorities' figures say that 98 to 99% of the population do) to be told that he will require a new receiver and aerial within the next seven years to receive the same programmes on u.h.f., he may feel that his viewing arrangements are being interfered with unnecessarily and moreover will involve him in additional expense. (The introduction of BBC-2 was different—it was a new programme.) Unless the viewer buys a colour receiver, the picture quality will be only marginally better than before. But to tell the public that the change is being made solely to enable colour programmes to be received would not be quite true, although it is true that without making the change to 625-line u.h.f., colour programmes of any sort cannot be seen. This is because of a Government decision and not because it is technically impossible. It will be recalled that the Independent Television Authority was at one stage leading protagonist for a 405-line colour service and gave some impressive demonstrations in an attempt to prove that the 405-line colour picture quality was of a high order.

If the viewer cannot afford a colour receiver, he can still receive BBC-1 and I.T.A. programmes on 405-lines v.h.f. undisturbed for the next seven years, because it is intended to keep the existing transmitters operational for that period following the start of duplication, and if he has already purchased a dual-standard receiver for the purpose of watching BBC-2, the technical features of the changeover should, in theory, be of no consequence to him. He should already be using a u.h.f. channel group aerial the bandwidth of which is designed to cover the new BBC-1 and I.T.A. u.h.f. channels for his area as well as the existing BBC-2 channel, so that it should merely be a case of tuning to the new BBC-1 and I.T.A. frequencies on the u.h.f. scale.

This may not be quite as straightforward as it sounds. Although all u.h.f. transmitters for any particular area will be co-sited, and of the same order of radiated power (the most far-sighted arrangement made in recent years), the propagation conditions may not be identical on each channel. Whereas the multi-channel u.h.f. aerial was initially aligned and adjusted for optimum reception of BBC-2, it may require re-adjustment for compromise reception of three channels, involving the services of an aerial rigger. In any case, viewers have had no previous standard by which to judge their reception of BBC-2, but it may be a different story when they make the switch from v.h.f. BBC-1 and I.T.A. to u.h.f. BBC-1 and I.T.A.

It should be remembered that while duplication of programmes on v.h.f. and u.h.f. lasts, people with dual-standard receivers will at any time be able to make a direct comparison between them. Those whose BBC-1 and I.T.A. reception is not so good on u.h.f. will feel justifiably aggrieved when v.h.f. 405-line transmissions are eventually switched off. Then again, at some date in the future, after the three programmes are established from his main transmitter for the area, the viewer may find that his particular locality has been provided with a relay transmitter to improve reception (perhaps making it comparable to his v.h.f. reception). This will be on another channel and necessitate a new aerial which will have to be mounted in a different plane to the one used for reception from the main transmitter.

It has been argued that long before the end of the seven-year duplication period the v.h.f.-405-line-only viewer will require a new receiver anyhow, so that it will simply be a matter of his purchasing a replacement receiver which will operate on the new 625-line u.h.f. standard. A complete change from v.h.f. to u.h.f. may still mean a new aerial will be required at a cost of, say, £12.

The whole or part of this cost could be offset by the saving on the single-standard receiver with its simpler circuitry than the dual-standard type. The changeover switch and other components associated with dual-standard operation will be eliminated. The dual-standard receiver has always been regarded as a compromise design not giving of its best on either system, whereas the single-standard version will have a frequency response tailored to give optimum performance on 625 lines only and it will be inherently more reliable. There will still be a need for a v.h.f./u.h.f. tuner unit in some areas perhaps for reasons discussed later, but in the main a u.h.f.-only tuner will be all that is necessary.

Despite this the receiver industry seems to be wary of offering a single-standard u.h.f.-only receiver in advance for those areas where all three existing programmes will be available on u.h.f. and on 625 lines because at the present time no British black-and-white receiver of this type is on sale, and one major manufacturing group is advising its dealers not to stock single-standard receivers this year. This same company predicts that it will still be manufacturing dual-standard receivers in seven years' time. A spokesman for a second major set-making group told *W.W.* that it will be a bold P.M.G. who declares a large number of domestic receivers obsolete by announcing the end of v.h.f. TV broadcasting and his company foresees the continued use of v.h.f. even in ten years' time. It is to be hoped that the single-standard receiver will become a reality in time.

In view of what has been said it may be worthwhile re-examining the question of why the change to 625 lines and at the same time the change to u.h.f. became necessary, and where it is likely to take us in the future.

In 1956, Parliament asked the Television Advisory Com-

mittee (T.A.C.) to say whether the existing 405-line standard was likely to remain adequate for the next 25 years, and whether there was any reason why the 625-line standard, broadcast in u.h.f. Bands IV and V, should not be used for broadcasting in the U.K. if it were recommended by the C.C.I.R. as the European standard. Following large-scale field trials the T.A.C. recommended that 625-line broadcasts on u.h.f. should be adopted if Europe generally adopted this. At a European VHF/UHF Broadcasting Conference in Stockholm in 1961, most countries concerned decided to adopt as standard an 8MHz channel bandwidth which greatly eased the problem of channel sharing with neighbouring countries. It is to some extent because of the variety of channels in the v.h.f. bands in Europe and the varied spacing of sound and vision carriers within them that interference from long-distance stations in these bands is troublesome. The presence of this interference which is due to "Sporadic E" effects is also the reason why 405-line v.h.f. colour transmissions are not considered practicable. Because of the introduction of a colour subcarrier, the visible effects of this type of interference would increase for about nine million viewers during active periods. Should the uniformity of 8MHz channelling agreed at Stockholm be disturbed, a serious interference problem could also arise with colour transmissions, in Bands IV and V, as would be the case in v.h.f.

The T.A.C.'s findings were published as a report in 1960¹. The report stated that 405-line standards would not be adequate for all purposes for the next 25 years and that a 625-line standard would give a definite improvement in picture quality *particularly with larger screens* (our italics). While nobody will dispute that an increase in the number of scanning lines per frame will reduce the visibility of the line structure, the subjective improvement in picture quality should be relatively better irrespective of screen size. Viewing distance plays a part here. Returning to the 1960 report, this pointed out also that the introduction of television broadcasting into Bands IV and V would present the last opportunity the U.K. would have of changing its line standard. In other words, it was a case of now or never. If 625 lines were used in Bands IV and V, then this system would eventually have to be used in Bands I and III. But what of Bands I and III, will they ultimately become available for other programmes? This is a question which remains unanswered.

To advise on the future of broadcasting, the Government set up a committee in 1960 under the chairmanship of Sir Harry Pilkington (The Pilkington Committee) which considered the 1960 T.A.C. Report and weighed the non-technical factors involved in changing the line standard. After deliberating for about two years, this committee finally presented its report² to the P.M.G. on June 5th, 1962. It recommended that the standard be changed to 625 lines and found that the increased costs of transmitting and receiving on the new standard both to the viewer and the broadcaster, were not significant. The committee also recommended the "duplication" method of changeover which virtually puts Bands I and III out of use for some seven years as far as new programmes are concerned. It is interesting to note that had the Pilkington Report recommended the retention of 405-line transmissions, the number of channels which could be used in Bands IV and V would be no greater than on 625 lines in view of the U.K.'s previous undertaking to adopt 8MHz channel spacing. And the number of national programmes possible is related to the number of available channels.

The T.A.C. Report recognized that to produce a u.h.f. replica of the present v.h.f. services is virtually impossible and eventually some of the v.h.f. channels will have to be employed to extend the four u.h.f. programmes to those areas where u.h.f. reception is poor. In order to reach anything like the population covered by Bands I and III with transmissions in Bands IV and V, some 60 main u.h.f. transmitters are planned,

supported by hundreds of relay stations. No one knows at this stage the exact number of relay stations required (the I.T.A. says 400), but unless the countryside is littered with low-power stations, amounting in some places to almost a transmitter to each village, some viewers are bound to find that their u.h.f. reception is inferior to that obtained on v.h.f. The feasibility of using so many stations is only possible by the development of the unmanned station technique, otherwise the number of technical manning staff required would be unreasonable. Poor reception on u.h.f. may not be confined only to remote areas either.

According to estimates the final coverage on u.h.f. will be 95% of the population as compared with 98-99% coverage on v.h.f. This may seem to fall not far short of identical coverage but 1% represents $\frac{1}{2}$ million people. It is at this stage, one is to assume, that use will be made of some of the then redundant v.h.f. channels to complete the coverage of 625-line programmes. This operation together with the institution of two new programmes on 625-line v.h.f. is referred to vaguely by the Pilkington Report as "re-exploitation of Bands I and III" although it is not known what this will entail, pending decision from the Government.

When considering the question of the future use to which the v.h.f. bands should be put it has to be kept in mind that the Pilkington Report recommended that ultimately six television programmes should be planned for: four on u.h.f. and two on v.h.f. Since the 5MHz spacing of the present 405-line channel allows just sufficient number of channels (13) to give national coverage with two programmes, it will be physically impossible to provide the same number of channels with the agreed 8MHz channel spacing unless Band III is widened. If Band III were to be extended from 216 to 222 MHz then Bands I and II together would provide 9 channels which could provide two programmes, although the coverage attainable would be less than that of the existing services on 405 lines. Gaps could be filled in by making use of u.h.f. Whatever use is eventually made of Bands I and III, after the withdrawal of BBC-1 and I.T.A. programmes we shall be left in a few years' time with a network of v.h.f. transmitters which could straight away give national coverage with one additional programme, operating on 9 channels with 8MHz spacing. It is unthinkable that the broadcasting authorities would relinquish their claims for television broadcast facilities in the v.h.f. bands, and remembering that the B.B.C.'s and I.T.A.'s charters expire in 1976 plans for "re-exploitation of Bands I and III" should emerge long before that date.

In the meantime pressure is being exerted by all radio-users for more frequency space in an already overcrowded spectrum and the v.h.f. Bands I and III would, for example, partially fulfil the needs of mobile radio operators if their plea for more space at u.h.f. is rejected. Then again the Conservative party has announced recently that if returned to Parliament they will set up a further 100 radio stations which for part of the time at least, according to the announcement, will be broadcasting on v.h.f., straining further the resources of frequency space. The Government will need to seek advice from the P.M.G.'s Frequency Advisory Committee and although in this country Band V has not yet been wholly allocated and further sectors could be made available for television it would be a pity if the present v.h.f. bands were lost to television broadcasting. In any event, in accepting the Pilkington Report, Parliament has accepted the implications of demands on frequency space required by six television programmes and if this is to be the future pattern, it is now up to Parliament to provide the necessary operating frequencies and authorize the capital expenditure.

J.H.V

References

- ¹Report of the Television Advisory Committee 1967. H.M.S.O. 1968.
²Report of the Committee on Broadcasting 1960. H.M.S.O. Cmd 1753.

Digital Microcircuits

A description of the major logic families

by D. E. O'N Waddington,* M.I.E.R.E.

Microcircuits have been with us for a few years now and the trend in new equipments is to make more and more use of them. This is not entirely because they are small but because they offer very definite advantages in cost and reliability as well as simplifying design procedures. In order to distinguish between the different families of circuits, the manufacturers have found it convenient to describe them by the initial letters of their circuit descriptions. Each family has its own particular characteristics, advantages and disadvantages, and before selecting a family for a particular application it is as well to appreciate the differences. For this reason a glossary of terms and abbreviations is included at the end of the article. This is by no means comprehensive as only the well known logic families are included.

Resistor-transistor logic (r.t.l.)

This was one of the first logic forms to be built into integrated circuits; probably because it is simple and was already in use with discrete components. The basic circuit of a two-input gate is shown in Fig. 1. When either, or both of the inputs is taken positive, the output will go to 0 V—either Tr_1 or Tr_2 , or both, will be bottomed. However, when both of the inputs are held at 0 V, the output will be positive—both Tr_1 and Tr_2 will be cut off. Typically these circuits operate from a low voltage, 3 V being about normal; however, under certain circumstances it is permissible to increase the supply voltage. Two types of r.t.l. are made, a low power type—2 mW/gate with propagation delay of 30 ns and a higher power type—12 mW/gate with a propagation delay of 12 ns. Noise can be a problem with r.t.l. as, with a logic swing of 0.8 V, the noise margin is only 0.3 V.

Diode-transistor logic (d.t.l.)

This type of logic, together with t.t.l., comes under the general heading of "current sinking logic". In practice this means that the switching action at the input to a gate consists of transferring the current holding the gate "on" into the circuit driving it. In other words, sinking the current in the output stage of the driving circuit. Most of the current sinking logic forms are com-

Typical integrated circuit characteristics

logic family	gate delay ns	fan out	mW per gate	toggle rate MHz	noise margin V	power supply V
r.t.l.	12-40	4-5	2-12	3-25	0.3	+3
d.t.l.	8-25	8-25	9-30 ⁽¹⁾	5-25	1	+4 - +5
t.t.l.	6-12	6-15	10-25 ⁽¹⁾	12-30	1	+5
e.c.l.	2-6 ⁽²⁾	25	40-110	20-120	0.35	-5
m.o.s.	50-300	—	5-20	1-5	4-8	24

(1) 1mW types are available but are very much slower in operation.
 (2) gate delays of 0.9ns are now available.

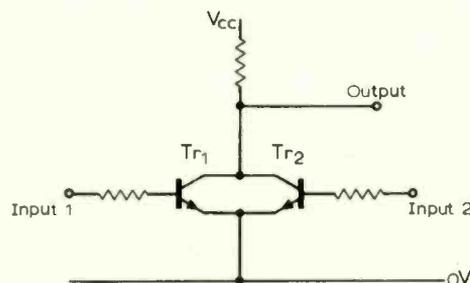


Fig. 1. Basic 2-input r.t.l. gate.

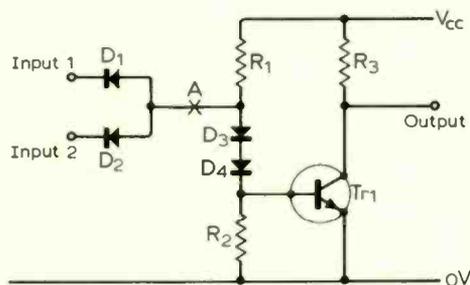


Fig. 2. Discrete component 2-input d.t.l. gate.

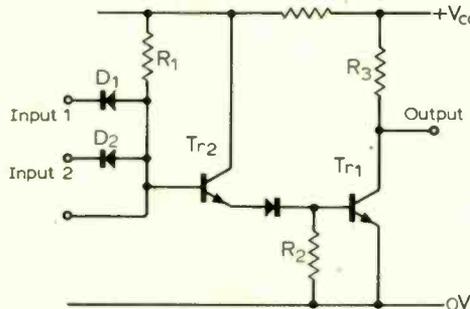


Fig. 3. Basic i.c. d.t.l. gate.

patible and can be interconnected. However, the fan-in and fan-out conditions must be checked as the loads for the different circuit types may be different.

The circuit of a d.t.l. gate in integrated form amounts to an almost direct transfer of the discrete component circuit shown in Fig. 2. The circuit operates as follows:—When the inputs are held positive the diodes D_1 and D_2 are reverse biased so that current flows through R_1 , D_3 and D_4 into the base of Tr_1 keeping Tr_1 bottomed. When either input is connected to earth, the current through R_1 will be diverted through either D_1 or D_2 to earth and Tr_1 will switch-off.

The switch-on noise margin is determined by the voltage required at "A" for base current to flow in Tr_1 . As the voltage drop across a forward biased silicon diode is approximately 600 mV, the voltage must be at least:

$$V_{D_3} + V_{D_4} + V_{BE}(Tr_1) = 3 \times 600 \text{ mV} = 1.8 \text{ V.}$$

This means that the voltage at either input point must be at least one diode forward voltage drop less than that at point "A" if the gate is to change state. Thus this noise margin will be approximately 1.2 V. The switch off noise margin is determined by the power supply and is usually about 2 V.

There is one major disadvantage of translating this circuit into integrated form. The turn-off time depends largely upon how fast charge can be pulled out of the base region of Tr_1 . In discrete component circuits this is achieved either by making D_3 and D_4 slow recovery types so that they provide a transient low impedance path from the base of Tr_1 to earth, or by returning R_2 to a negative supply rail. Neither solution is very good for integrated circuits; the

former because it is not easy to make slow and fast diodes in the same chip and the latter because it is nicer to have only one supply rail. Another approach is to make the value of R_2 relatively low. The disadvantage of this is that it would rob base current from Tr_1 thus reducing fan out. The integrated circuit solution is shown in Fig. 3. D_3 is replaced by an emitter follower, Tr_2 , which gives the necessary current gain so that the value of R_2 can be reduced without affecting the fan out. Sometimes times the point "A" is brought out as a connection to the integrated circuit so that additional diodes can be connected to expand the circuits fan-in capability. The main limitation is one of speed, as each diode adds capacitance across the input, thus increasing the switching time.

It is worth noting that it is often possible to improve the turn-off time of the circuit by using the spare fan-out. For instance, if a circuit has a fan-out of eight and is only driving two loads, there is a six-load capability which can be utilized. Thus, if one load is equivalent to 4 k Ω , the output collector load can safely be shunted by 4/6 k Ω . This will improve the turn-off time at the expense of additional "on" current.

Transistor-transistor logic (t.t.l.)

This logic series is primarily an integrated circuit form which has no counterpart in discrete circuitry. The two features, which are peculiar to t.t.l., are the multi-emitter input transistor and the "totem pole" output. The latter circuit, although recognized as a design feature of t.t.l., has been used both in r.t.l. and d.t.l. circuits.

The basic gate is shown in Fig. 4. If all the emitters of Tr_1 are connected to the positive rail, the base-emitter diodes are reverse biased while the base-collector diode is forward biased thus supplying base current to Tr_2 switching it on and, at the same time, switching Tr_4 on and Tr_3 off. The switching-off of Tr_3 is assured by D_1 (See Fig. 5). When any one (or more) of the input emitters is connected to earth, the corresponding base-emitter diode will conduct and Tr_1 behaves like an ordinary transistor and "bottoms", switching Tr_2 off, Tr_3 on and Tr_4 off. Because the turn-off time of saturated transistors is longer than the turn-on time, there will be a very short period, usually of only a few nanoseconds duration, when Tr_3 and Tr_4 are both conducting. The circuit will, therefore, draw a pulse of current limited only by R_4 from the supply. For this reason adequate supply decoupling must be used. The great advantage of this form of output circuit, over that normally used in d.t.l., is that the turn-on and turn-off times are roughly equal. With d.t.l., the turn-off is generally longer than the turn-on and rapidly becomes longer if the load on the output is capacitive. However, the resistive output has two advantages over the "totem pole" which should not be forgotten. Firstly it is possible to directly connect together the outputs of two or more gates to give a logical "OR" function. "Wired" or "dot OR".) The other advantage is that the

actual output potential, when the output transistor is switched off, is equal to the supply line voltage. With the "totem pole" circuit, however, the output voltage will be at least 0.6 V less than the supply voltage. Some t.t.l. circuits are now being manufactured without the "totem-pole" output so that the wired "OR" function can be achieved.

Emitter-coupled logic (e.c.l.)

Like r.t.l. and d.t.l., e.c.l. was also used in discrete form long before it was incorporated into integrated circuits. However, because transistor matching is possible in integrated circuits, this logic form is very well suited to integration. Unlike all the circuits previously described, e.c.l. is a non-saturating logic form, that is, the logic functions are performed by current steering rather than by saturated switches and, therefore, the delays associated with turn-on, turn-off and hole storage no longer apply. Instead the "switching" time is limited by the speed of the transistors, making e.c.l. one of the fastest forms of integrated circuit logic available.

The basic gate is shown in Fig. 6. Unlike the previous circuits, in which the gates were always of the inverting type, e.c.l. usually provides both output polarities, i.e. output-1 is inverting while output-2 is non-inverting.

If either, or both, of the inputs is taken positive, Tr_1 or Tr_2 , or both will conduct, cutting Tr_3 off. That is, the current through R_2 will be steered through R_1 . This will cause output-1 to go negative and output-2 to go positive. If both of the inputs are taken negative, Tr_1 and Tr_2 are switched-off and the current through R_2 is steered through R_3 . This will cause output-1 to go positive and output-2 to go negative. Saturation is avoided by a proper choice of the ratios of resistors and reference voltage. In practice the logic swing is only about 800 mV with a noise margin of about 200 mV. Despite this low noise margin, e.c.l. is a practical system as the noise generated by the operation of this type of gate is very much less than that generated by any of the saturating logic forms. The main advantage of e.c.l. is that it, and e.c.l., are the fastest logic form available. Propagation delays of less than 2 ns are obtainable and some manufacturers even predict delays of less than 0.5 ns in the future.

Metal-oxide-silicon logic (m.o.s.)

This is very different from any of the other logic forms described. It uses m.o.s.f.e.t.s in place of transistors and resistors, resulting in a very small chip size and making it possible to have more functions per integrated circuit. This means that the main area of application of m.o.s. is where there is a requirement for a large number of logic functions on a single chip.

The basic gate circuits are shown in Figs. 7 and 8. In the circuit shown in Fig. 7, the output goes positive only if both inputs are taken negative, i.e. Tr_1 and Tr_2 are turned on.

In the circuit shown in Fig. 8, the output

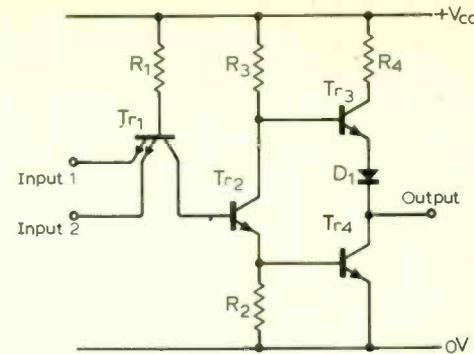


Fig. 4. Basic t.t.l. gate.

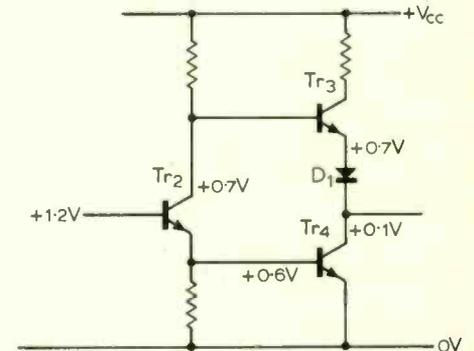


Fig. 5. t.t.l. gate with Tr_4 switched on. The V_{be} and V_{ce} under saturated conditions are assumed to be 0.6 V and 0.1 V respectively. From the voltages shown in the diagram it is easy to see that the base voltage necessary to turn Tr_3 on is 1.3 V thus ensuring that it is turned off. However if D_1 were omitted, there is every likelihood of Tr_3 being turned on.

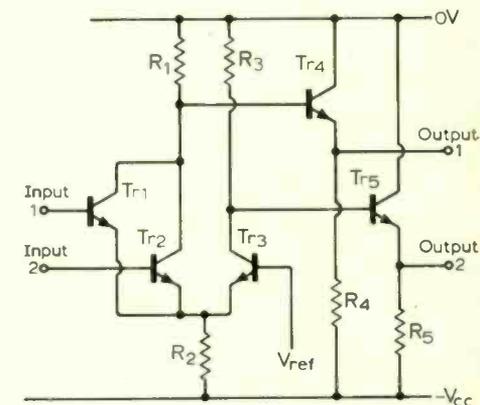


Fig. 6. Basic e.c.l. gate.

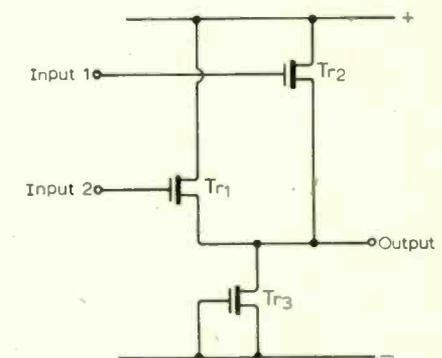


Fig. 7. m.o.s. NAND gate.

May Meetings

is also a fair indication of power output capability as it is usually possible, from a knowledge of what one load is equivalent to, to calculate the available output power.

Tickets are required for some meetings: readers are advised, therefore to communicate with the society concerned

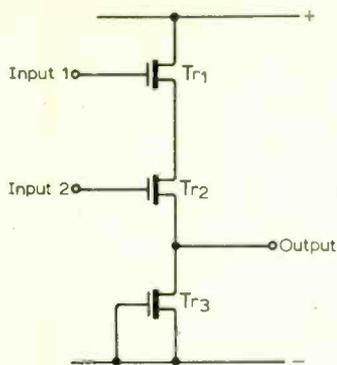


Fig. 8. m.o.s. NOR gate.

oes negative only if *both* inputs are taken positive. i.e. Tr_1 and Tr_2 are turned off. In both circuits the load "resistor" is Tr_3 which is designed to give a suitable resistance value by controlling its g_m . The majority of m.o.s. logic circuits use only n-channel devices but some circuits using p- and n-channel devices are now becoming available. The supply voltages for these circuits is of the order of 20 V and the logic swing is of similar proportions. The speeds of operation are relatively slow, propagation delays being in the region of 50 to 500 ns.

Glossary of terms and abbreviations

The list which follows explains the initials used to describe most of the logic families.

- c.s.l. —compatible current sinking logic
- c.l. —counting logic
- c.t.l. —complementary transistor logic
- d.t.l. —diode-transistor logic
- c.c.s.l. —emitter-coupled current steered logic
- c.l. —emitter-coupled logic
- e.c.l. or e.c.l. —emitter-emitter-coupled logic
- n.i.l. —high noise immunity logic
- h.t.t.l. —high-level transistor-transistor logic
- h.t.l. —high threshold logic
- m.o.s. —metal-oxide-silicon (logic)
- r.c.t.l. —resistor-capacitor-transistor logic
- r.t.l. —resistor-transistor logic
- t.l. or t.l. —transistor-transistor logic

Some terms used in connection with integrated logic circuits are as follows:

Fan-in This is the maximum number of input signals which may be fed into a gate. The gate has four input points the "fan-in" is said to be four. *Note:* In circuits where all the available inputs are not used, it is good practice to connect the unused input points so that they cannot affect the operation of the gate. As a general rule, with r.t.l., unused input points should be connected to the negative rail.

Fan-out This is the maximum number of loads (gate inputs) which the output of a circuit is capable of driving. It is normally quoted as a simple number. (The effective number of loads represented by inputs of integrated circuits are usually quoted as well as they are not necessarily unity). Fan-out

Noise margin This can be defined as the interfering input voltage necessary to cause the gate to change state or start to change state when the input is in either of its normal operating conditions. There are two switching thresholds. (See Fig. 9). One is associated with the turn on and the other with the turn off. The noise margin, quite clearly, is the difference between the specified "0" and "1" states and the respective switching thresholds. The noise margins are not necessarily the same and are usually quoted accordingly. In some e.c.l. gates there is also a further noise margin in that, if the "1" voltage is increased too far, part of the circuit will saturate and a phase reversal will occur as shown dotted.

Power dissipation This is usually expressed as an average value with the gates operating with a 50% duty cycle. However, some manufacturers quote dissipation figures for both the on and off conditions. With saturating logic it is quite usual for the power consumption to increase with frequency.

Propagation delay This is a measure of the speed of operation of a gate. Fig. 10 shows that there are propagation delays associated both with turn-on and turn-off times. The turn-on delay is usually shorter than turn-off delay but this is by no means a fixed rule. However, because the delays are so frequently different, manufacturers usually quote average delay. This is one of the reasons for the very wide propagation delay tolerance in many data sheets.

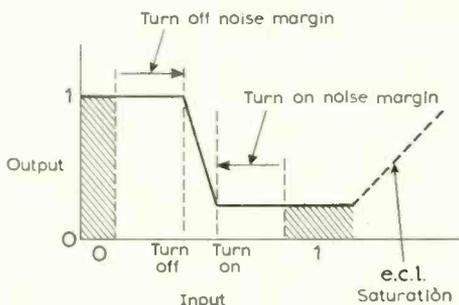


Fig. 9. Diagrammatic representation of the transfer characteristic of a gate.

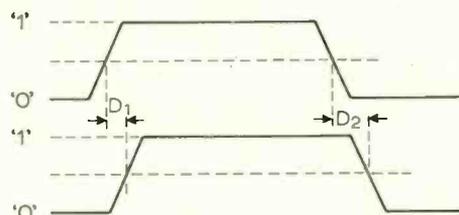


Fig. 10. Waveform showing propagation delay using a non-inverting gate. D_1 is the "turn on" delay and D_2 the "turn-off" time. For convenience it is assumed, in this illustration, that the switching point is at the centre of the transition from 0 to 1. In practice this is very seldom so.

LONDON

- 1st. R.T.S.—Symposium on "Control room design and layout" at 17.00 at the I.T.A., 70 Brompton Rd., S.W.3.
- 2nd. I.P.P.S.—"Acousto-electric effects in semi-conductors" at 10.30 at Imperial College, S.W.7.
- 5th. I.P.P.S.—"Organization and management of research and development" at 10.15 at I.E.E., Savoy Pl., W.C.2.
- 5th. I.E.E.—"V.L.F. navigation" by S.S.D. Jones at 17.30 at Savoy Pl., W.C.2.
- 6th. I.E.E. & I.Mech.E.—"Electronic turbine governing" by P. A. L. Ham and A. A. L. Bental at 17.30 at Savoy Pl., W.C.2.
- 7th. I.E.R.E.—"The Rapier ground-to-air missile system" by S.C. Dunn at 18.00 at 9 Bedford Sq., W.C.1.
- 12th. I.E.E.—"Filters with periodically time-varying parameters" by Dr. W. Saraga at 17.30 at Savoy Pl., W.C.2.
- 14th. I.E.E.—"Large scale integration—why, where and when?" by D. D. Jones at 17.30 at Savoy Pl., W.C.2.
- 14th. S.E.R.T.—"Applications of the unijunction transistor" by G. C. Rayworth at 19.00 at the London School of Hygiene, Keppel St., W.C.1.
- 15th. I.P.P.S.—Symposium on "Optical techniques in acoustics" at 14.30 at the Physics Dept., Imperial College, S.W.7.
- 15th. I.E.E.—"Recent advances in resistor design" by F. J. Wilkins and M. J. Swann at 17.30 at Savoy Pl., W.C.2.
- 15th. I.E.R.E.—"Absolute digital displacement transducers" by A. L. Whitwell at 18.00 at 9 Bedford Sq., W.C.1.
- 19th. I.E.E.—Colloquium on "Cathode-ray tube display" at 10.00 at Savoy Pl., W.C.2.
- 20th. I.E.E. & I.E.R.E.—"Peripheral auditory mechanisms" by Dr. H. A. Beagley at 17.30 at St. Bartholomew's Hospital, E.C.1.
- 21st. S.E.R.T.—"Practical work in technician courses" by A. J. Hymans at 19.00 at the Royal Society of Arts, John Adam St., W.C.2.

CAMBORNE

- 15th. I.E.E.—"The operational aspect of Eurovision" by A. R. Elliott at 14.30 at Cornwall Technical College.

CARDIFF

- 16th. S.E.R.T.—"Tape recorder servicing" by H. W. Hellyer at 19.30 at the Llandaff Technical College.

COLCHESTER

- 15TH. I.E.E.—"Tomorrow's world in tele-communications" by W. J. Bray at 18.30 at Essex University.

HORNCHURCH

- 8th. I.E.R.E.—"Automatic production testing of electronic equipment" by R. Kitchen at 18.30 at the Technical College, 42 Ardleigh Green Road.

MANCHESTER

- 5th. I.E.E.—"Invention as part of education" by Prof. M. W. Thring at 18.15 at U.M.I.S.T.

NEWCASTLE-UPON-TYNE

- 7th. S.E.R.T.—"Colour receiver decoder and c.d.a. circuits" by L. H. Briggs at 19.00 at the Charles Trevelyan Technical College, Maple Terrace.

PLYMOUTH

- 7th. R.T.S.—"Translators and repeater stations" by D. L. Smari at 19.30 at Westward TV Studios.

Personalities

Sir Ian Orr-Ewing, Bart, O.B.E., M.A., F.I.E.E., M.P., is the new president of the Electronic Engineering Association. Sir Ian, who is 57, is chairman of Ultra Electric (Holdings) and of Ultra Electronics which he joined in 1966. After graduating from Trinity College, Oxford, with an honours degree in physics he served a three-year apprenticeship with E.M.I. and then joined the B.B.C. Television Service in 1937 where he stayed (except for war service in the R.A.F.) until 1949. He then served as a director of the Cossor Group of Companies until 1957 when he resigned on being appointed a minister in the Government. Sir Ian served as Un-



Sir Ian Orr-Ewing

der Secretary of State for Air (1957-59) and Civil Lord of the Admiralty (1959-63). At on time during the war he was chief radar officer on General Eisenhower's staff.

Among those recently elected Fellows of the Royal Society were:—**Professor R. L. F. Boyd, Ph.D., B.Sc., F.I.E.E.**, professor of physics and director of the Mullard Space Science Research Laboratory, at University College, in the University of London, "distinguished for his contributions to ionospheric physics and X-ray and ultraviolet astronomy and to the exploitation of space science techniques in these fields"; **Professor C. W. Oatley, O.B.E., M.A., M.Sc., F.I.E.E.**, professor of electrical engineering at the Department of Engineering in the University of Cambridge,

"distinguished for his work on measurements at microwave frequencies, in electron-optics, and in particular for the design and development of a successful scanning electron microscope"; and **Dr. J. H. Wilkinson**, deputy chief scientific officer, Mathematics Division, National Physical Laboratory, Teddington, "distinguished for his contributions to numerical analysis and the development of digital computers, and especially for his work on backward error analysis".

Elizabeth Laverick, Ph.D., B.Sc., F.I.E.E., A.Inst.P., head of research and advanced projects at Elliott-Automation Radar Systems Ltd, has been awarded an honorary fellowship of the University of Manchester Institute of Science & Technology in recognition of her achievements in technology and technological education. Dr. Laverick, who has made major contributions in the field of radar and microwave engineering, gained her B.Sc. at Durham University where she later became the Physics Department's first lady Ph.D. She then joined the microwave aerials department of the GEC Applied Electronics Laboratory. She joined Elliotts in 1954 as a microwave engineer and, in 1959, became head of the Radar Research Laboratory. Since 1967 Dr. Laverick has been a member of the Electronics Divisional Board of the Institution of Electrical Engineers, the first lady member, and is president of the Women's Engineering Society.

W. E. Thompson, B.Eng., M.I.E.E., and **V. J. Cox, M.B.E.**, have been appointed directors of Ekco Electronics Ltd. Joining Ekco in 1949, Mr. Thompson was appointed head of nucleonic development four years later. In 1963 he became technical sales manager—instrumentation, and in 1967 took charge of the Instrumentation Division and will continue to do so. Mr. Cox joined Ekco in 1941 and for many years he has been wholly responsible for avionic design matters. In 1959 he was appointed chief engineer—aviation, and in September last year he became manager of the Aviation Division, a position which he will retain.

John H. Buying, aged 46, who originally joined Marconi Instruments as an X-ray development engineer in 1948, following service with Philips Electrical Ltd, has been appointed sales manager of the Sanders Division of the company. In 1950 he became a service engineer with General Radiological Ltd. In 1954 he rejoined M.I. as a sales engineer in the Export Department, and he was later appointed a distributor manager. The company also announces the appointment of **Renie G. Weston** as sales engineering supervisor. Following service in ground radar in the R.A.F. during the last war, Mr. Weston, who is 46, became a sales engineer with Pye Telecommunications Ltd in 1946. He subsequently became European sales manager. From 1960 to 1964 he was sales director of Storno Southern Ltd, and in 1965 he joined the Specialised Components Division of the Marconi Company, transferring to M.I.'s Sanders Division last October.

John C. W. McCarthy, B.E.M., has joined Racal Communications Ltd as systems consultant. He has spent over 40 years in the Civil Service for 33 of which he was concerned with electronics in the Royal Naval Scientific Service, latterly with the Ministry of Defence (Navy).

R. M. Carroll is now managing director of Eddystone Radio, a member of GEC-Marconi Electronics, on the retirement of H. Cox who had been with the company since its formation in 1927. Richard Carroll, who is 45, joined the Marconi Company's test department at Chelmsford in 1947. He was in the supplies department from 1958 until 1964 when he was appointed marketing manager of the newly formed Microelectronics Division of the company. He was transferred to Eddystone as works manager about a year ago. **Kenneth R. Williams**, who joined Eddystone in 1938, is appointed sales manager. After being in charge of the service department for seven years he took over the professional equipment sales department in 1945.



R. M. Carroll

P. E. Leventhall, B.Sc.(Hons), F.I.E.E., has been appointed division manager of S.T.C.'s Marine Division at Croydon (International Marine Radio Company Ltd). He had previously been technical manager for I.M.R.C. and Hudson Electronics. Mr. Leventhall, who is 41, joined I.M.R.C. in 1966 from Cossor Communications Ltd, where he had been chief engineer.

Dennis C. Flack, Ph.D., B.Sc., F.I.E.E., has been appointed chief engineer of Sifam Electrical Instrument Co. Ltd, of Torquay. D. Flack, who is 44, was with Sangam Controls, a division of Sangam Weston Ltd, from 1960 to 1966. Prior to this he was for twenty years in the aircraft industry at Bristol latterly as chief electrical design with Bristol Aircraft Company.

GEC-Marconi Electronics Ltd announces the formation of a new Mobile Communications Division based at Spon Street Works, Coventry, the manager of which is **I. Alexander, B.Sc., F.I.E.E.**, formerly the technical director of the Communications Division of GEC-A (Electronics) Ltd. **J. E. Hills** is appointed sales and marketing manager and **D. A. S. Dryborough, B.Sc., M.I.E.E.**, chief engineer.

Robin Stephens, who joined Wireless Electronics Ltd, of Bognor Regis twelve months ago as marketing manager has been appointed to the board as marketing director. He graduated in electrical engineering from Bristol University and after serving as sales manager in the Computer Division of Solartr Electronic Group, was later marketing manager of Redifon Astrodata Ltd.

K. G. Thorne, F.I.E.E., F.I.E.R. has joined Epsylon Industries Ltd of Feltham, Middx, as chairman and managing director in succession to **I. D. Cuffe** who has taken up corporate appointment with the Epsylon parent organization, Leigh Instruments, of Ontario, Canada. Mr. Thorne was formerly managing director of Computing Devices Ltd, London.

OBITUARY

John Clarricoats, O.B.E., who has contributed our "World of Amateur Radio" section since its introduction in 1959, died on March 7th aged 71. "Clarr" as he was affectionately known among amateur transmitting fraternity, started his radio career with Standard T. phones & Cables Ltd. and became full-time secretary of the Radio Society of Great Britain in 1932. He retired from this post in 1963 but continued as honorary secretary of the European Regional Division of the International Amateur Radio Union. John Clarricoats also played a major role in the government (particularly in educational matters) and was Major of the London Borough of Enfield.

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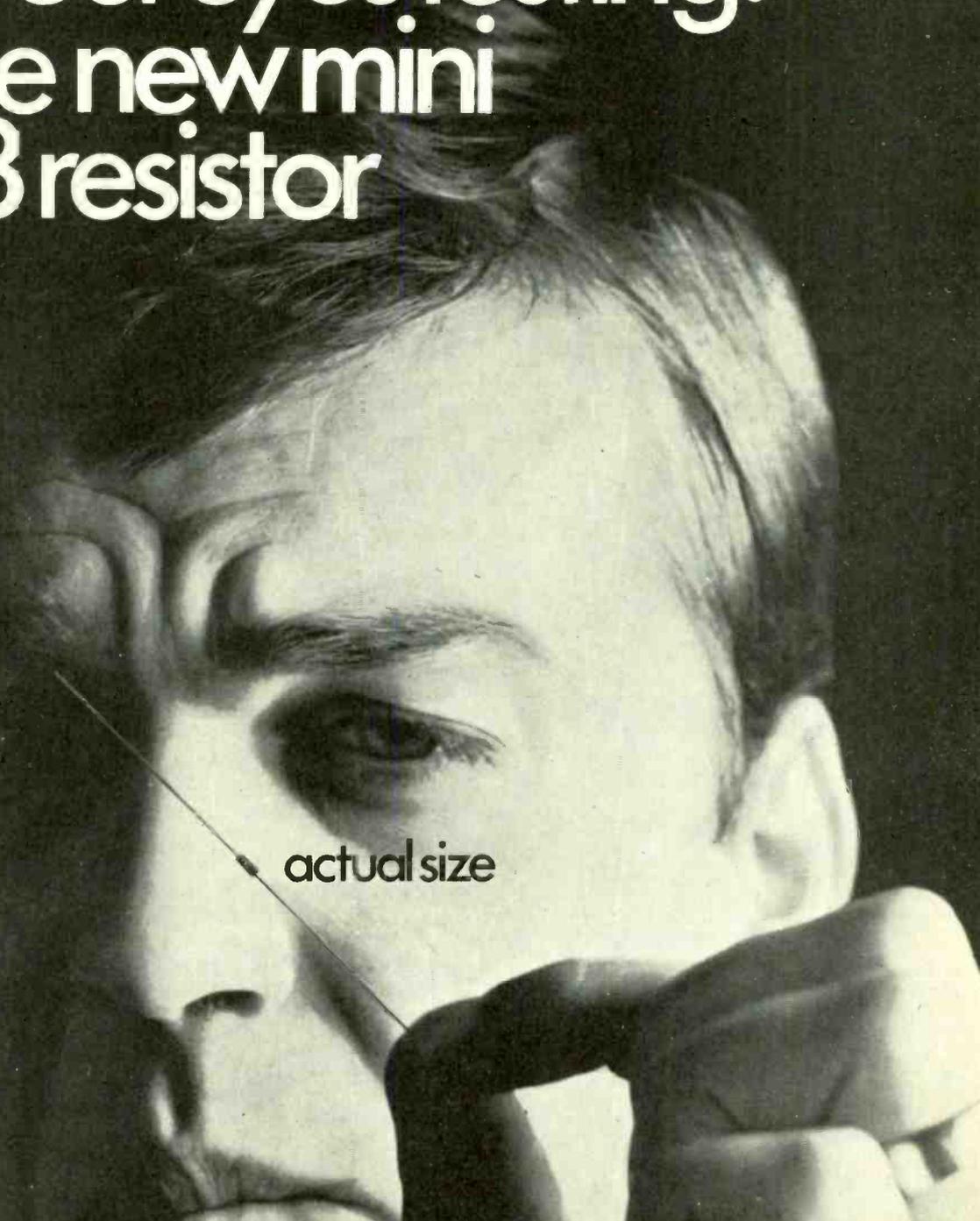
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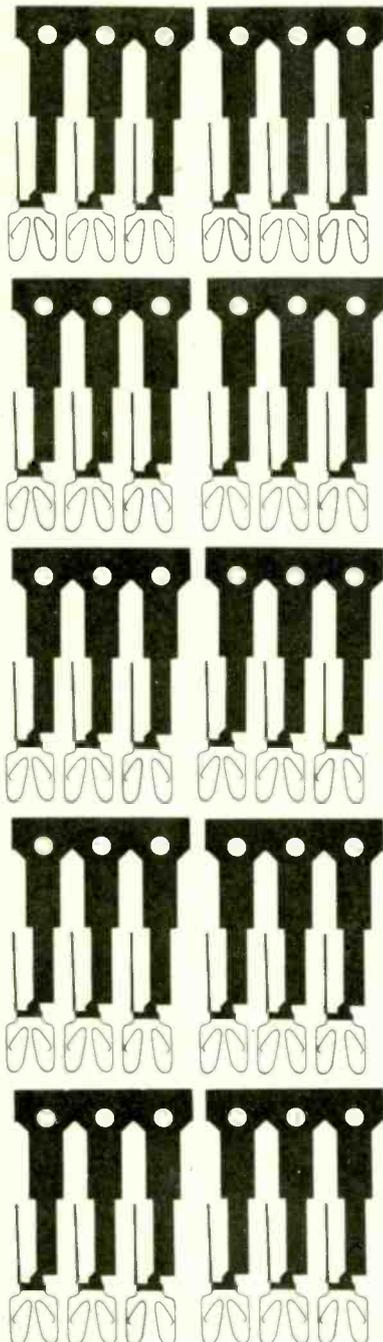
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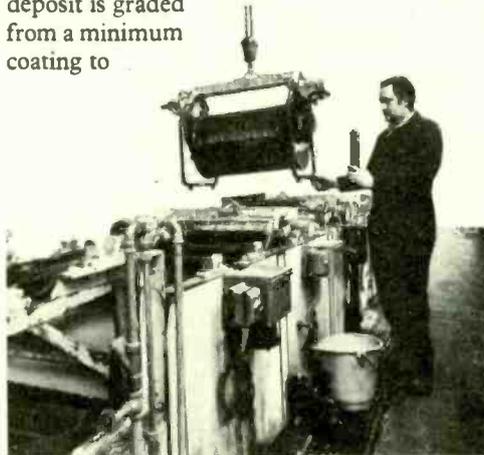


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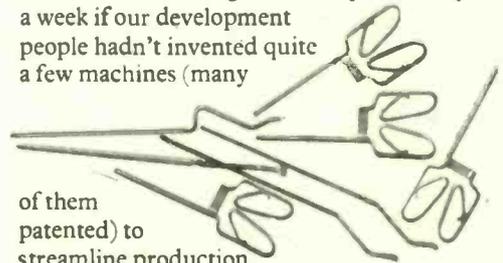
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be very time-consuming – except for the fact that our development boys have devised a little machine that does the necessary test completely automatically. In fact, we'd have a bit of trouble turning out over 25,000,000 parts a week if our development people hadn't invented quite a few machines (many



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WW—107 FOR FURTHER DETAILS

Wireless World Colour Television Receiver

12. Chrominance circuits

Last month details were given of one of the two main boards of the decoder, the board which carries the input chrominance amplifier, the burst amplifier and burst gate, the phase discriminator, the crystal oscillator, the colour killer and the identity circuits. This month the other main board is being dealt with and Fig.1 shows its circuit diagram. As before, the numbers in brackets refer to the sections of the block diagram of Part 10.

The input is applied at P_{12} , which is joined to P_2 in the other board. This signal is the complete chrominance signal plus colour burst. It is applied through C_{35} to a combined attenuator and burst gate (3), the purpose of the gate being this time to remove the burst from the signal.

Saturation control

The attenuator comprises two diodes D_9 and D_{11} connected back to back. Their cathodes are joined to the chassis through the resistors R_{50} and R_{52} , while a variable bias is applied to their anodes. The resistance of the diodes varies with this bias and, therefore, the amount of signal transmitted through them. One resistor, R_{51} , is returned to $-20V$. Another, R_{57} , is taken through R_{58} to the slider of R_{60} to which up to $15V$ can be applied. This control R_{60} is not mounted on the board, but on the front panel, and it forms the saturation control. It is a purely d.c. control and so can safely be connected by leads of any length.

The junction of R_{57} and R_{58} is taken via P_{14} to the luminance amplifier where it is linked with the contrast control. It is connected to the point marked "To saturation control in chrominance units" in Fig.1, Part 6. Adjustment of contrast varies slightly the bias applied to the attenuator diodes and tends to make the saturation independent of brightness.

Another diode D_{10} is connected to the anodes of D_9 and D_{11} . A negative-going line flyback pulse of some $80V$ amplitude from the line timebase is fed to P_{18} by a screened cable. This is reduced to about $3.5V$ by the potential divider R_{63} , R_{62} and applied through R_{61} to the cathode of D_{10} . It renders D_{10} conductive and makes the anodes of D_9 and D_{11} negative, cutting them off. The colour burst, which occurs during the line flyback, is thus prevented from passing through the diodes and the attenuator output at P_{13} is the chrominance signal only at an amplitude which depends on the setting of R_{60} .

This signal is applied to the chrominance amplifier (4) Tr_9 , which has a tuned base circuit comprising L_6 and C_{39} damped by R_{53} and tuned to 4.43 MHz. It has the usual emitter bias network, but the base is taken via P_{20} and P_8 in the other board to the anode of D_8 . When there is no colour signal no bias is applied and Tr_9 is cut-off, thus preventing noise or interference from passing any further through the chrominance circuits to appear on a monochrome picture. With a colour signal a positive

bias is developed by D_8 in the way explained last month and it appears at P_{20} and renders Tr_9 operative.

The amplified chrominance signal at the collector is passed to the next stage Tr_{10} through a trap L_7 , C_{45} tuned to $6MHz$. Tr_{10} is connected as a phase-splitter (5) with both collector and emitter loads. The collector load is the $150\text{-}\Omega$ resistor R_{72} which is connected to the input of the PAL delay line (6) via P_{21} and P_{22} .

At signal frequency the emitter load comprises a fixed component of $86\text{-}\Omega$ provided by R_{76} and R_{77} in series, shunted by a variable component of $39\text{-}\Omega$ to $139\text{-}\Omega$ provided by R_{74} and R_{75} in series. The variable control R_{75} enables the relative amplitudes of the emitter and collector outputs to be adjusted. At d.c. the emitter resistance varies from $159\text{-}\Omega$ to $259\text{-}\Omega$ as R_{75} is adjusted, but this does not vary the operating point of the transistor seriously.

The emitter output is taken from the junction of R_{76} and R_{77} to the centre point of the 1:1 auto-transformer T_7 (7). The two ends of this winding are taken, one each, to the two synchronous demodulators. The centre-point and the R-Y end are taken to P_{27} and P_{28} and thence to the output of the PAL delay line. The $150\text{-}\Omega$ resistor R_{95} produces the proper termination for the line.

Because of the auto-transformer action the signal delayed by the PAL line appears at equal amplitudes but opposite phase at the two ends of the auto-transformer. At the one end it is added to, and at the other end it is subtracted from, the undelayed signal applied at the centre tap. Two things happen as a result. One is that the chrominance signal is separated into its R-Y and B-Y components; the demodulators alone are capable of doing this, and in simple PAL they do, but this pre-separation renders them less critical. The other and main thing is that by combining the signals of one line with those of a previous line, delayed in time by one line, phase errors are largely cancelled.

Reference oscillator inputs

At this point it is necessary to stop following the path of the chrominance signal for a while, because the demodulators require inputs derived from the reference oscillator. For a proper understanding of the demodulators it is necessary to see how these are derived. The output of the reference oscillator at sub-carrier frequency is taken from P_6 in the other board through a $0.002\text{-}\mu F$ capacitor to P_{26} in this board. Notice particularly that this capacitor does not appear in the diagrams because it is connected directly between P_6 and P_{26} and so is not mounted on either board.

The transformer T_4 has four identical windings, and the reference oscillator output is fed to one of them. This winding and one other form a 1:1 ratio auto-transformer and across the whole the voltage is double the oscillator input and is balanced to chassis. This is applied to the phase-shifting (36) circuit C_{57} ,

R_{90} . When the resistance equals the reactance of the capacitance the voltage appearing between their junction and chassis is equal in amplitude to the voltage fed in from the oscillator, but is shifted 90° in phase.

The primary of another transformer T_6 is connected between these points and its secondary feeds a voltage at the frequency of the reference oscillator, but at 90° in phase to it, through R_{93} and R_{94} to the B-Y demodulator.

Returning to T_4 , two secondaries are connected as shown to D_{15} and D_{16} which are arranged to be conductive alternately. When D_{15} is conductive its secondary feeds the oscillator frequency through C_{54} , the primary of T_5 and D_{15} . When D_{16} is conductive the secondary connected to it feeds the primary of T_5 through C_{55} and D_{16} . The outputs of the two secondaries are in opposite phase and so the phase of the voltage fed to T_5 reverses whenever the diodes are switched (35).

PAL switch

This switching is effected by the bistable (34) Tr_{11} and Tr_{12} . This is conventional and needs little or no explanation. The transistors are cut-off and conductive alternately. When one is conductive its collector is nearly at chassis potential and the collector of the other, which is then cut-off, is at about 15V. The collectors are joined through R_{86} and R_{87} to the two diodes D_{15} and D_{16} .

If Tr_{12} is cut-off, for example, the cathode of D_{15} is connected through R_{86} and R_{83} to 15V. The anodes of both diodes are taken to the potential divider R_{88} , R_{89} at about 10V. There is thus about 5V reverse bias applied to D_{15} through some $2k\Omega$. The other diode D_{16} has its anode at about 10V but its cathode is nearly at chassis potential. It thus has nearly 10V applied in the conductive

direction. When the bistable changes state the conditions are reversed and D_{15} conducts while D_{16} cuts-off.

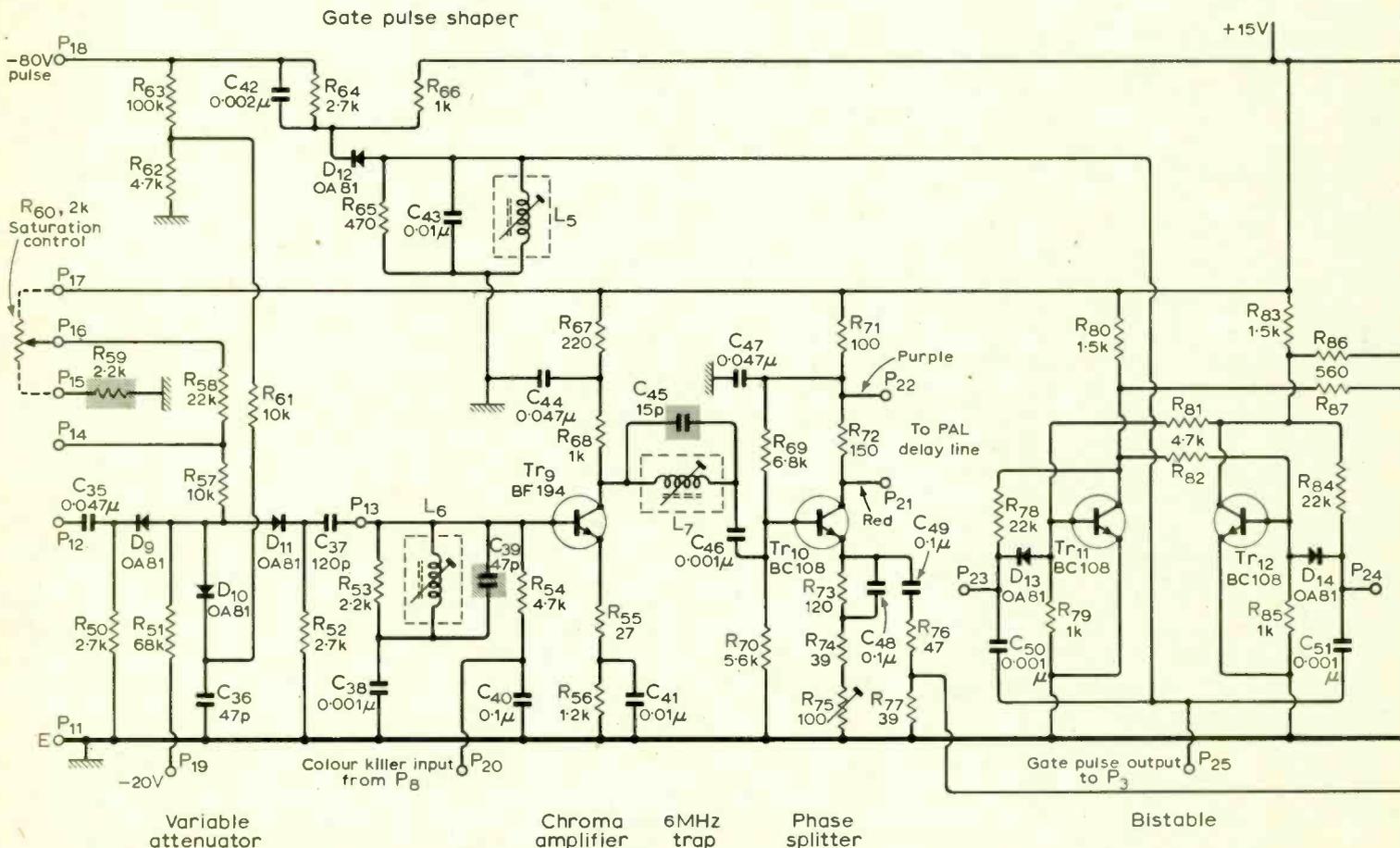
The change of state of the bistable is carried out at line frequency by a pulse derived from the line timebase (33). The $-80V$ pulse occurring on the line flyback at P_{18} is applied through C_{42} shunted by R_{64} to D_{12} and renders it conductive. This diode is normally cut-off by 15V reverse bias applied through R_{66} . The pulse current flows through D_{12} mainly into C_{43} charging it negatively to chassis. When the diode becomes non-conductive again, which it does very shortly after the peak of the flyback pulse, and so about half way through the flyback period, the tuned circuit L_5 , C_{43} , R_{65} is left isolated with C_{43} charged negatively.

It must be pointed out that because of the heavy damping provided by R_{65} , C_{43} does not charge very quickly as one might expect. The voltage waveform during the charging period is nearly a quarter cycle of sinewave.

On the discharge the waveform is a damped sinusoid, which starts at the negative peak and dies away in some two or three cycles. Because of the near sinusoidal voltage during the charging time, however, the charging and discharging parts of the waveform are not really separable when the wave is viewed on an oscilloscope. The waveform looks like a damped sinewave which starts with a negative half cycle of about 5V amplitude and is followed by a positive half cycle of some 3.5V amplitude. Successive half cycles die away rapidly.

It is the first positive half cycle which is used and the circuit has its frequency adjusted by L_5 so that its peak coincides with the centre of the colour burst. The wave is applied through P_{25} to P_3 in the other board where it renders Tr_3 conductive during the burst. It is also applied to the junction of C_{50} and C_{51} and here it is the first negative half cycle which is important.

Fig. 1. Circuit diagram of the second main board of the decoder. It includes the chrominance amplifier, the PAL switch, the synchronous detectors and the first-stage video amplifier and matrix circuit



renders both D_{13} and D_{14} conductive and so carries the basis of both transistors negatively. This has no effect on the transistor which is not conducting, but it reduces the current in the conducting transistor and because of the cross-coupling between the two this starts to turn on the other. The normal regenerative action then causes the bistable to change state. Thus the bistable changes state once every line during the flyback period and this reverses the phase of the oscillator signal applied to T_5 once every line in step with the R-Y reversals of phase in the signal.

While the bistable will change state every line and so reverse the phase of the oscillator signal on T_5 once every line, there is no guarantee that the phase will be in its proper relation with the signal; it may always be 180° out of its proper phase. To prevent this an identity circuit is provided. This was explained last month, when it was shown how a roughly sinusoidal voltage of half line frequency (7.8kHz) is developed and taken through D_6 to P_7 . From there it is brought in to either P_{23} or P_{24} .

Suppose that it is taken to P_{24} . If it happens that Tr_{12} is conductive, the collector potential is very low and so is the potential of P_{24} . If Tr_{12} is non-conductive, however, the collector potential is nearly 15V, D_{14} is cut-off and so is D_6 and the positive half cycle from Tr_8 is not passed by D_6 and the positive pulse from L_5 acts normally on Tr_{12} to initiate a change of state. During the next line Tr_8 produces a negative half cycle which is not passed by D_6 . Thus the identity circuit does nothing.

However, if Tr_{12} is conductive when the positive half cycle of identity signal occurs matters are different. The potential of P_{24} is then near earth, D_6 conducts and allows the positive half cycle to reach P_{24} . It is now Tr_{11} which is conductive and the positive pulse from L_5 makes it draw current as usual. The positive half cycle at P_{24} now holds the base of Tr_{12} positive

and prevents it from moving negatively in response to the change in Tr_{11} . It thus prevents the usual change of state from occurring. It must be noticed that D_{14} is conductive because its anode is held positive by its connection to R_{81} and R_{85} .

The result is that if it happens that the bistable is being triggered in the wrong phase, the identity signal prevents it from triggering, and it remains in the same state for two consecutive lines, and this brings it into the right phase.

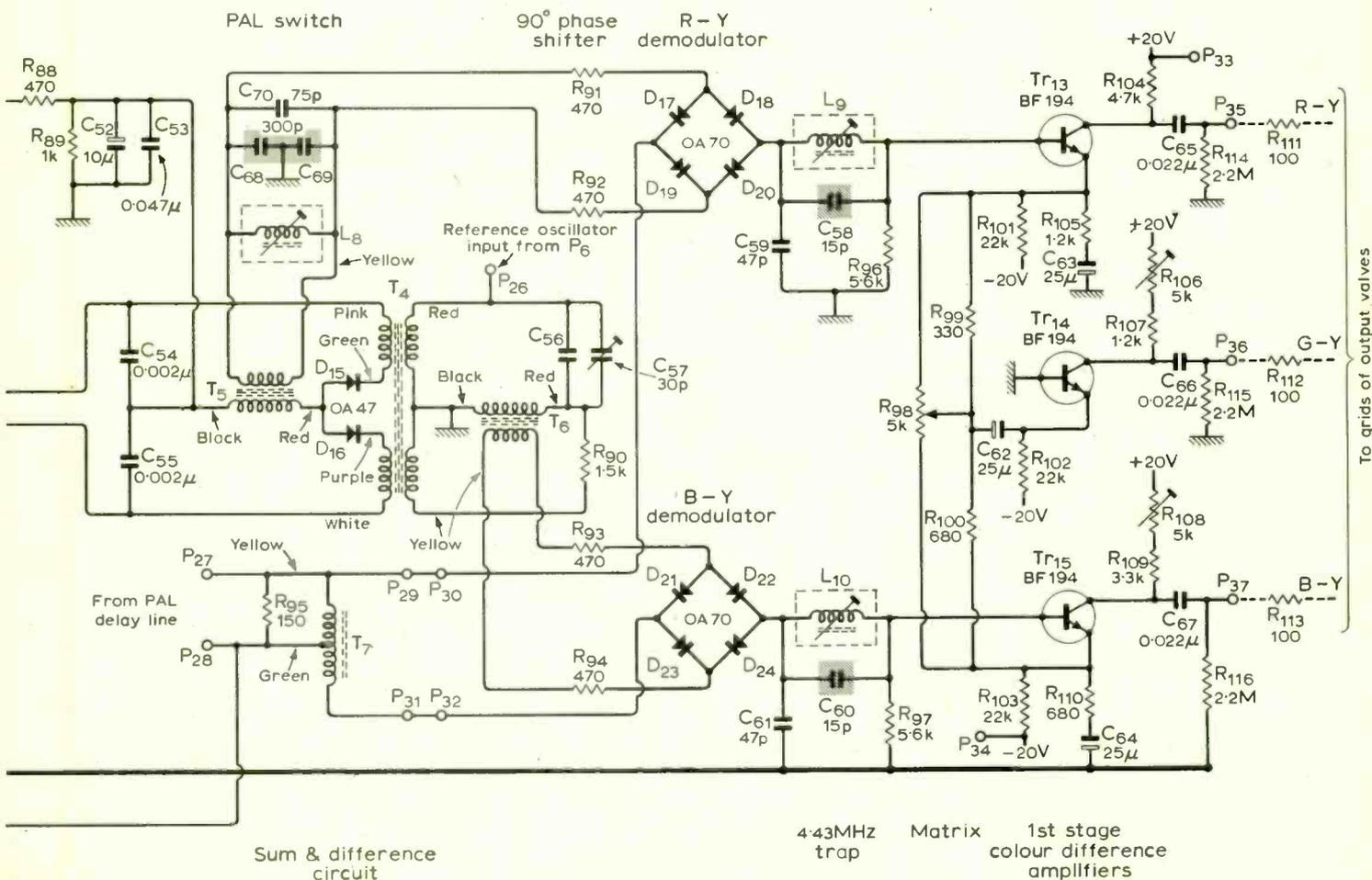
Two points of connection, P_{23} and P_{24} , are provided for the identity signal but, of course, only one is used. The correct phase of the bistable depends on the phasing of some of the transformers. If a mistake is made in one of these, the identity circuit will keep the bistable consistently in the wrong phase. It is usually easier to correct such an error by transferring the identity lead from one pin to another than to find the transformer with the wrong connections and reverse its leads.

This must not be taken to mean that care over the transformer connections is unnecessary. Not all errors of connection can be remedied by changing over the identity lead.

It will now be clear how the reference oscillator signal, reversing in phase every line, is obtained across T_5 . The secondary output is applied to the R-Y demodulator through the resistors R_{91} and R_{92} . A tuned circuit is connected across the secondary, however, in order to suppress harmonics. This comprises L_8 tuned by the combination of C_{68} to C_{70} .

Synchronous detectors

All four diodes of a demodulator conduct during the positive half cycles of the reference signal and so effectively join the input and output terminals and allow the chrominance signals to pass. During the negative half cycles all four diodes are non-conductive and the input and output terminals are isolated.



The outputs are in the form of half cycles of the 4.43-MHz signal waveform and these are smoothed by C_{59} and C_{61} to the R-Y and B-Y video signals. Trap circuits L_9 , C_{58} and L_{10} , C_{60} tuned to 4.43 MHz, remove this component from the signals. The output loads, which are also the base resistors of the following amplifiers, are R_{96} and R_{97} .

Colour difference amplifiers

The chrominance signals now exist in video form and it is necessary to amplify them and also to produce from the R-Y and B-Y signals the G-Y signal. The red (12) and blue (13) channel amplifiers are substantially the same, and are Tr_{13} and Tr_{15} , respectively. In each case there is an emitter load of $22k\Omega$ returned to $-20V$. The collector loads are taken to $20V$, so the transistors operate with a total supply of $40V$. The load of Tr_{13} is a fixed resistor R_{104} of $4.7k\Omega$, but that of Tr_{15} is variable from $3.3k\Omega$ to $8.3k\Omega$ by R_{108} . The blue channel requires higher gain than the red and it must be adjusted to be the right proportion to it.

The emitters have a.c. loads which are virtually provided by R_{105} of $1.2k\Omega$ and R_{110} of 680Ω . This alone makes the red channel have nearly twice the feedback of the blue channel and, hence, makes the gain of the latter nearly double.

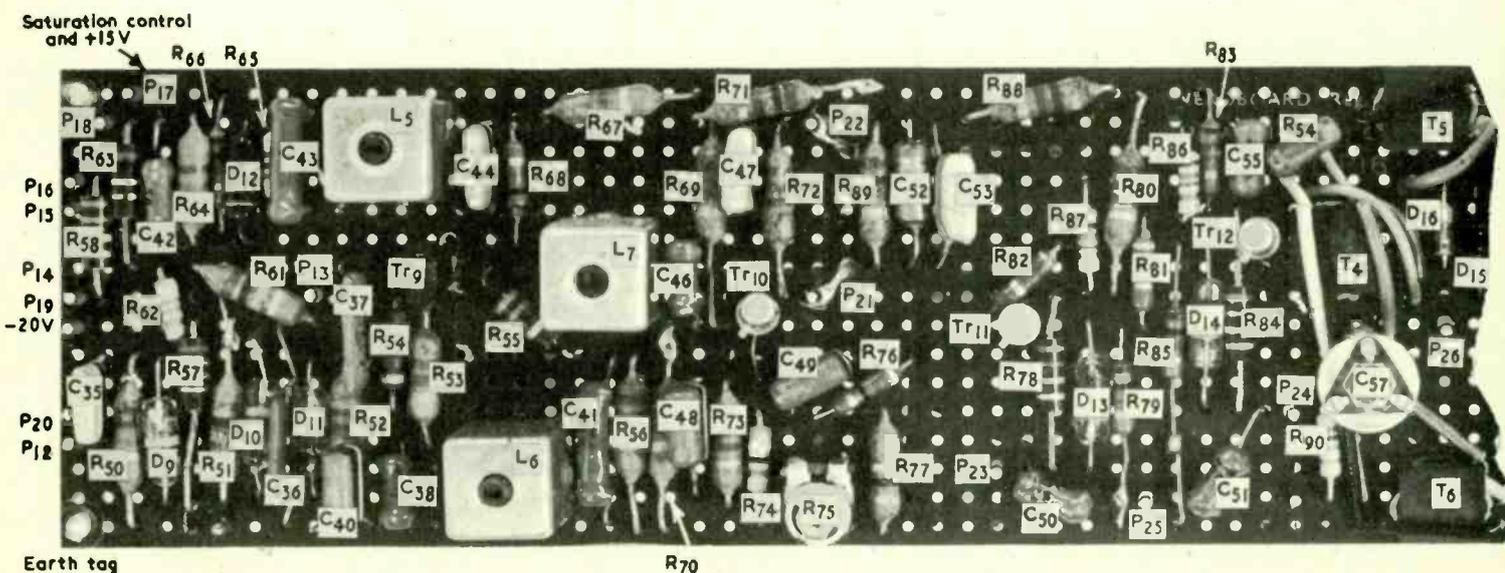
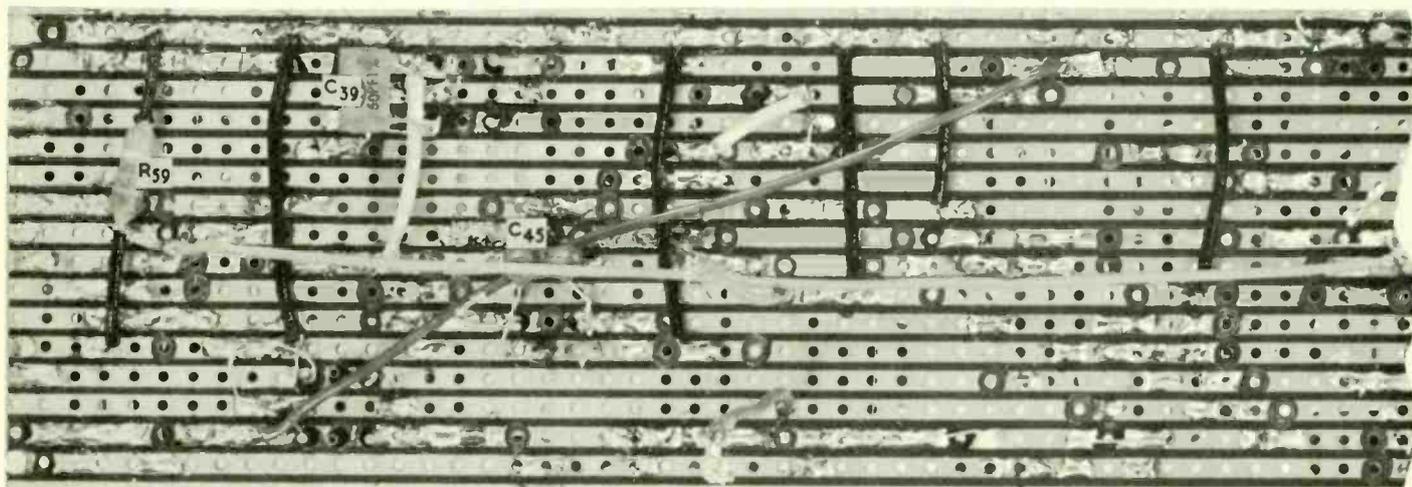
The emitters of these two transistors are joined through R_{99} and R_{100} shunted by R_{98} , which permits the precise ratio of these resistances to be adjusted. The combination of the R-Y and B-Y signals so obtained is applied through C_{62} to the emitter of Tr_{14} and is the G-Y signal. This transistor operates under the same conditions as the other two, and has an adjustable collector load R_{107} , R_{106} to enable the G-Y signal to be set at the proper level.

From the collectors of these three transistors onwards the three channels are identical, so it suffices to describe one of them. The coupling capacitors and grid leaks of the following valves (16)-(21) are mounted on the board and are terminated at P_{35} , P_{36} and P_{37} . The grid stoppers R_{111} , etc., are connected directly between these pins and the grid terminals of the valveholders.

All the parts shown in Fig.1 are mounted on a strip of Veroboard of the same dimensions as that used for the reference oscillator, etc., described last month. Fig.2 shows photographs of both sides of this board.

Details of all the transformers for both boards were given last month. Details of the coils used in both will be given next month. With the exception of L_4 , all the coils are wound on the same type of former and are of the kind used in the i.f. unit. The bases have six pins, of which only two are used for connections. The pin spacing does not fit that of the holes in the

Fig. 2. Photographs of the two sides of the board, showing the component layout. Note that C_{56} does not appear on the board because there was just enough capacitance in C_{57} without it. In some cases, it may be required, but will rarely need to be more than $10pF$



Veroboard and the board cannot be re-drilled for them because of the existing holes. The best thing to do is to cut off the middle pair of pins from the coil bases, leaving only the outer four in the form of a square. Four existing Veroboard holes can then be enlarged with a drill so that the coil base is a tight fit into the four holes, although the individual holes are really very large for the pins. This can just be done without breaking the copper strips, and all four pins are then soldered to the strips, which are broken in the appropriate places. With so many components as in these boards, it is virtually impossible to bring the coil pins just where one would like, and wire connections for the coils are often needed.

The coil L_4 is on a larger former with a larger can. The can is mounted on its side by a pair of self-tapping screws into the side of the can. A small piece of Veroboard has the coil mounted on it and the coil connections made to it, and is held to the fixing lugs of the can by two 6 B.A. screws and nuts. The two tuning capacitors for this coil are mounted on it in the can.

The corner hole of each board is enlarged to 6 B.A. clearance for mounting. Each adjacent hole in the board has the copper removed so that the earthed mounting screws and nuts do not introduce any short-circuits.

The whole of the decoder circuits are mounted in a frame built of brass angle. The horizontal flanges on the board side at the input end each have a $\frac{1}{4}$ -inch hole, through the two of which is passed a length of $\frac{1}{4}$ -inch rod which is fixed vertically to the

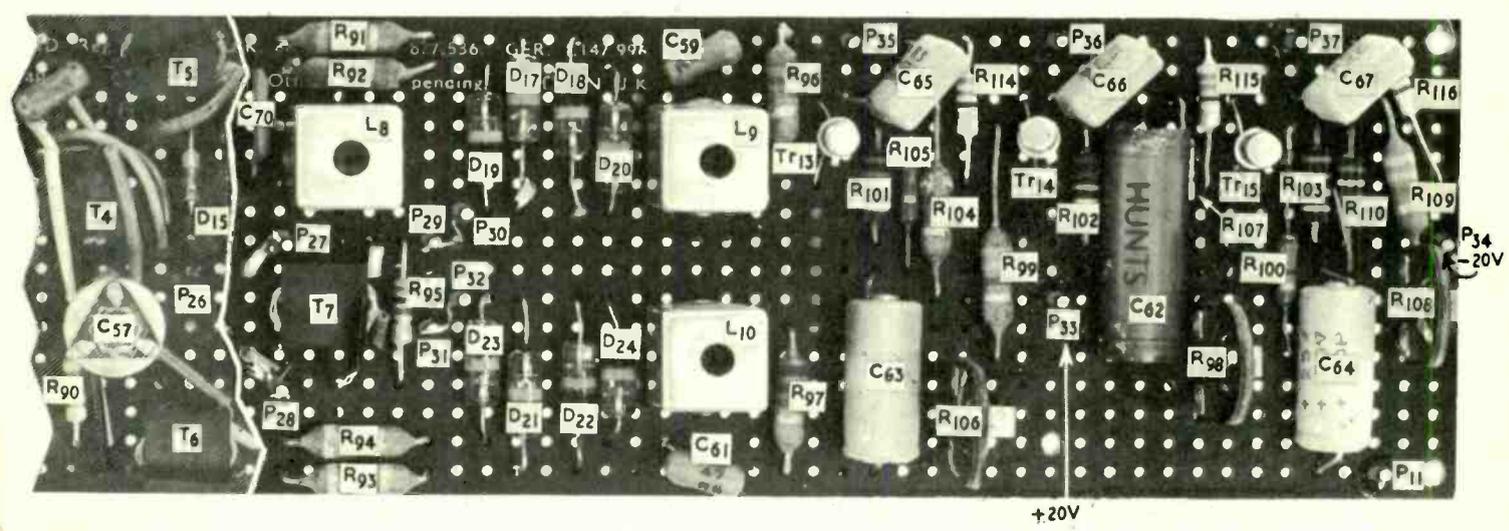
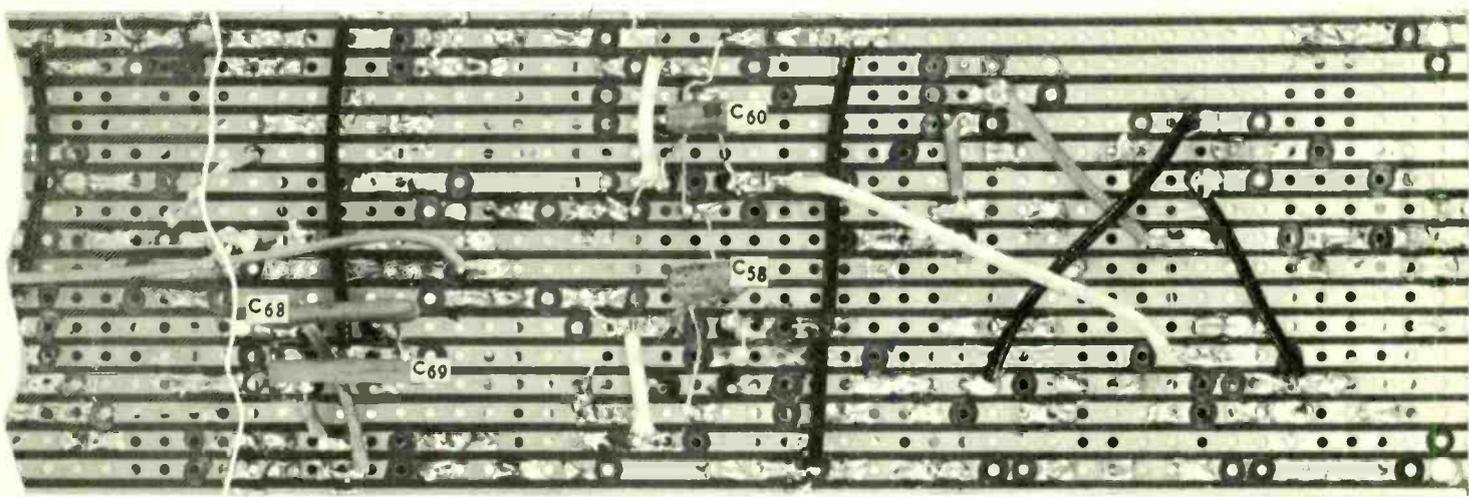
base. The bottom flange rests on the base, and the rod is sufficient to hold the assembly securely and yet enables it to be swung outwards to the rear for access while in operation.

The boards are fixed to the frame by long 6 B.A. screws and nuts. The PAL delay line is attached to a separate board which is screwed to the back of the frame. This is a piece of plain Veroboard with a 0.1-inch matrix of holes; this is necessary to fit the tags and mounting pins of the delay line but, of course, plain board can be used if it is drilled appropriately.

The connections for the delay line are soldered to P_{21} , P_{22} , P_{27} and P_{28} and taken through enlarged adjacent holes to pins on the delay-line side of that board. On the other side the delay line pins are themselves joined to the board pins, and a chassis earth lead is taken to the frame of the line.

In this way the whole delay line with its board is readily disconnected and removed if access is required to the back of either of the main boards. Access at the back is fairly good except at the top of the upper board and the bottom of the lower, where the boards are screened by the flanges of the framework.

The equipment can be operated in the simple PAL mode merely by disconnecting the delay line completely; that is, by making no connection to P_{21} , P_{22} , P_{27} and P_{28} . A few other components are then unnecessary, but their presence does no harm. There are certain advantages in doing this during the initial alignment. This together with details of the output stages will be given in Part 13.



Physics Exhibition

Selected items seen at Alexandra Palace, London, March 10-13

Ultrasonic holography

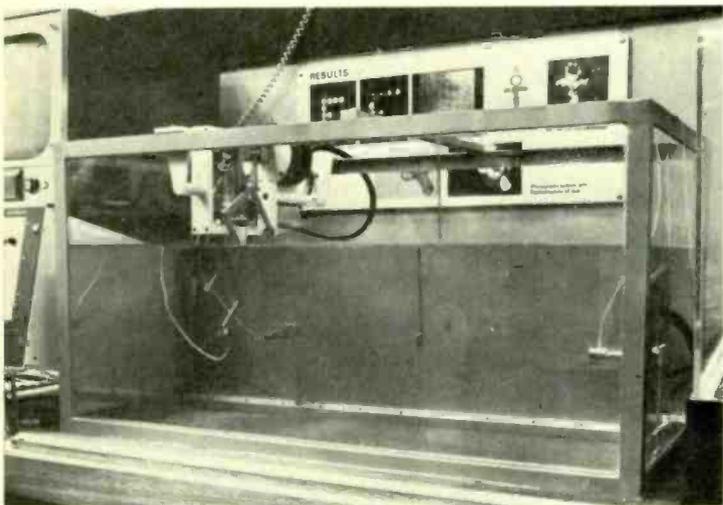
An experimental equipment for making holograms at ultrasonic frequencies was demonstrated on the E.M.I. stand. The demonstration was carried out underwater at 5MHz, although frequencies between 500kHz and 10MHz would have been suitable under these conditions.

The object to be viewed was suspended in a tank of water in the path of a beam from an ultrasonic transducer. Reflected energy from the object was combined with the output of a second transducer which was used to supply the reference signal. The interference pattern so formed was then mechanically scanned, a receiving transducer being used to sense the interference pattern.

The output of the receiving transducer, after suitable amplification, intensity modulated an oscilloscope which was made to scan in sympathy with the receiving transducer. The information on the oscilloscope tube face was then photographically recorded. Instead of being presented on an oscilloscope the output of the receiving transducer could have been used to intensity modulate a light source.

The hologram is viewed in the normal way, the film being illuminated with the output of a laser. On the stand the viewing was done using a closed-circuit television system in order to remove the hazards of viewing laser light with the naked eye.

The resolution obtained using this technique depends upon accurate synchronization, the wavelength used and the size of the scanned area. Unwanted reflections from the side of the tank can be virtually eliminated using suitable gating; however, there is still some break-through of the reference signal. This can be



Ultrasonic holography demonstration apparatus showing, from left to right inside the tank: scanning transducer; transmitting transducer; target; reference transducer. (E.M.I.)

defocused to some extent by critical positioning of the hologram when viewing.

E.M.I. suggest that a possible use for the technique would be to view objects under difficult conditions—in fog, in muddy water or under skin tissue, for instance.

Voice-operated typewriter

Designed as an aid for the disabled, a voice-operated typewriter developed by Standard Telecommunication Laboratories uses a simple electronic recognizer which responds to messages spoken in a modied version of the Morse code. The sounds 'di' and 'dah' (representing the dot and dash of the code) are used, and the machine recognizes these not on a spectral or phonemic basis but purely by their different durations. The spoken message is picked up by a microphone, and the output of this is band-pass filtered and fed to a threshold detector which detects the presence and defines the duration of peaks of voicing in the speech waveform corresponding to the 'di' and the 'dah'. There follow two further duration threshold devices (monostable circuits), one to differentiate between short and long sounds ('di' and 'dah') and the other to discriminate between silences within a code group (letter) and silences separating code groups. The 'di' and



Voice-operated typewriter, showing electronic recognizer on the left. (Standard Telecommunication Laboratories)

'dah' information is then translated into a binary code ('di' = 0, 'dah' = 1) and progressively fills a four-stage shift register (four bistable circuits) as the sounds are uttered. For example, for 'n' (dah-di), the register is altered from its basic state of 0000 to 0100. In addition, an associated two-stage counter (two bistable circuits) counts in binary notation the number of sounds uttered—for 'n' the count is 10. The letter 'n' is thus uniquely identified by the six-digit code 010010.

When the duration threshold device recognizes the end of the uttered group (a long silence) the contents of the shift register and counter are read into a decoder, the output of which actuates the corresponding typewriter key. It is claimed that a person can operate a typewriter accurately by this method at up to 20 words a minute, after a few hours' training. The output of the recognizer can, of course, be used for other functions such as 'dialling' telephone numbers or switching domestic equipment on and off.

Acoustic parametric receiving array

A highly-directional acoustic receiving array, covering a wide bandwidth of response, has been developed at Birmingham University. The system uses the non-linear interaction of a signal wave with a powerful local 'pump' wave.

The 'pump' transducer produces a high-frequency (about 6MHz) acoustic wave, which is well collimated within the Fresnel diffraction region, and a transducer placed along the axis of the first acts as a receiving probe. First-order interaction

between an incoming acoustic plane wave and the locally generated 'pump' column causes sum and difference frequency components to be generated in the water. The magnitude of the pressures at the receiving probe at these interaction frequencies can be shown to depend on the angle between the incoming wave and the pump wave. If the signal frequency is much less than the pump frequency, the device behaves very much like an ordinary end-fire array of the same length operating at the signal frequency.

In the interaction process, energy is transferred from the pump wave into the new frequencies, producing an up-converter type of parametric amplification. This means that a low-level acoustic signal is at least maintained at the same intensity on arrival at the receiving probe (at the new frequencies).

In this way it is possible to make a wide-band receiving device with acceptable directivity even at very low frequencies using two small transducers only.

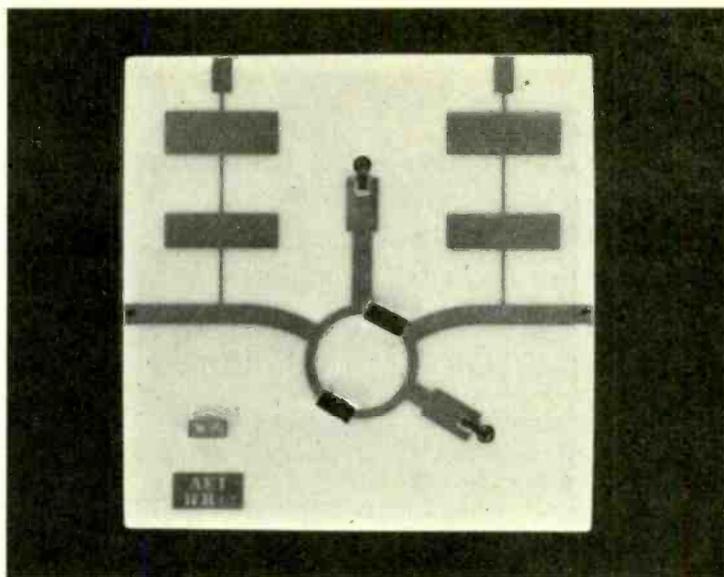
Electromechanical resonator for i.cs

A high-Q resonator that could possibly be used for filters, tuned circuits or oscillators in hybrid integrated circuits is based on the mass and compliance of a small mechanical element. The unusual feature is the use of electrostatic transducers for driving and pick-up. Shown by Standard Telecommunication Laboratories, the device consists basically of a metal beam mounted over conducting plates which form the input and output electrostatic transducers. The variable electrostatic force caused by the incoming signal acts on the metal beam and excites it into flexural vibration corresponding to its natural frequency. This frequency depends on the beam material and on the physical dimensions. The vibration causes small variations in the capacitance of the output transducer which are detected with a high input impedance amplifier. The device is completely passive and is reversible; by variation of the coupling it can be made symmetrical or unsymmetrical. Frequency range is from a few hundred hertz to a few hundred kilohertz, but the most suitable range is 1-20kHz. At low frequencies, below 1kHz, the effect of unwanted external vibrations can be reduced by using a balanced resonant element. S.T.L. say there is considerable choice in the shape and material of the resonant element and in the arrangement of the conducting plates, so a wide range of application should be possible. The vibrating beam can be mass loaded and tuned by removing material from the loaded end. Fine tuning can also be carried out by variation of bias voltage.

Microwave integrated circuits

Applications of microwave i.cs (microstrip) incorporating p-i-n diodes, shown by AEI Semiconductors, included a working circuit of a sideband generator in which two p-i-n phase shifters were included in a ring hybrid. The diodes were modulated in push-pull at a variable frequency up to a few MHz and each changed the phase of the signal by 180°. The fundamental cancelled out and sidebands corresponding to odd harmonics of the modulation frequency were left. Other microstrip circuits shown were a phase-shifting shunt mounted diode, a low capacitance series-mounted diode, a broadband changeover switch and broadband a.m. modulator. Our photograph illustrates a 180° phase-changer using two p-i-n diodes and two chip capacitors for d.c. blocking. The use of integration techniques makes for a tremendous reduction in size and cost of microwave equipment, the switching facility being particularly useful because of the practical difficulties of mechanical switching at microwavelengths.

A practical application of microwave i.cs could be seen in a display by the Admiralty Surface Weapons Establishment, where a microstrip pulsed Gunn oscillator was incorporated in



Microstrip 180° phase-changer incorporating two p-i-n diodes. (A.E.I. Semiconductors Ltd.)

an X-band marine radar beacon. The whole system, aerial, transmitter and receiver, occupied a p.c. board measuring about 152 × 100mm. The transmitter has a peak output power of 100mW and when the radar beacon, or "Racon" as it is called, is fitted to a buoy, it transmits a long identifying pulse on receipt of an interrogating pulse from a ship's radar. The pulse then marks the position of the buoy on the ship's radar. Circuits based on the microstrip transmission line are still being developed, using both thin and thick film techniques.

Motor using piezo-electric effect

A simple reversible linear motor has been designed at the Royal Radar Establishment. This motor moves in steps along a precision track, and the size of step can be varied within the range 0.1-4.0μm, with final adjustments to 0.01μm. The basic structure is very simple. Two electro-magnets, with pole pieces in contact with the horizontal track, are separated by a length of ceramic tube. A voltage applied between the inner and outer surfaces of the tube results, by piezo-electric effect, in a shortening of the tube by an amount proportional to the applied voltage. A single step is taken by de-energizing one magnet to free it from the track, shortening the ceramic tube as described, de-energizing the other magnet, clamping the first magnet, removing the contracting voltage from the tube (causing the free pole pieces to slide along the track), and finally reclamping the remaining magnet.

Integrated circuits are used in a simple logic unit which controls the above cycle and 5V signals are used to start and reverse the motor by remote control. A variable voltage in the range 0-9V determines the step size, by controlling the h.t. generator, and the stepping rate may be controlled by an external oscillator if required.

The distance over which the motor will travel is limited only by the length of precision 'V'-block used as track, and the length of flying leads provided. The ceramic is available in a variety of sizes, a factor enabling motor size and performance to be varied.

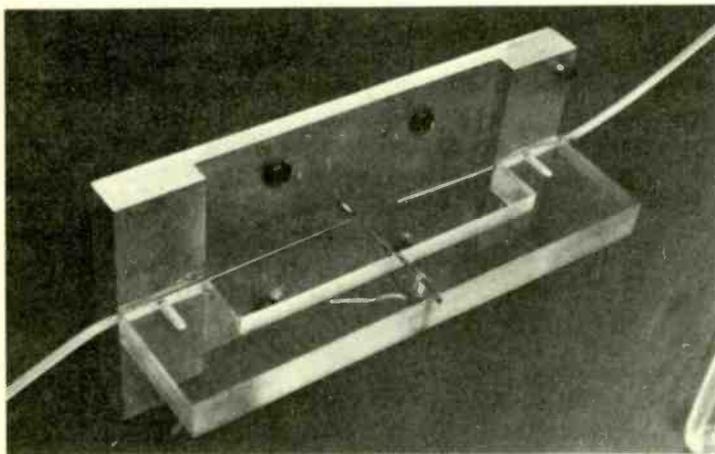
Variations in local force will change the size of step obtained for a given voltage, so that for some applications it would be necessary to use an optical or other highly accurate measuring technique to take full advantage of the motor's capabilities. Possible uses for the motor include: (1) general micromanipulation, (2) moving specimens in microscope work, (3) preparation of photo-masters in microelectronics, (4) manipulation of probes on integrated circuit chips, (5) manipulating micro-electrodes

into nerves—in this application the rapid step action is expected to assist in entering the membrane, (6) microtome sectioning, (7) moving mirrors in laser beams, and (8) grating ruling in conjunction with a laser measuring device.

Using ceramic tube $\frac{1}{2}$ in long, type PZT-5A (made by Brush Clevite Co. Ltd.), a sensitivity of 500V per μm can be obtained.

Electronic-fluidic interface switch

Electrical two-state signals from digital or switching systems can be converted very directly into corresponding air pressure signals by an unusual switching device shown by the University College of North Wales. It works on the principle that a laminar jet of air issuing from a tube can be made turbulent by a small continuous disturbance close to the tube. The disturbing mechanism in this case is the ion wind produced by a corona discharge occurring between a point and a plane electrode, and this forms the electrical input to the interface switch. The fluidic output

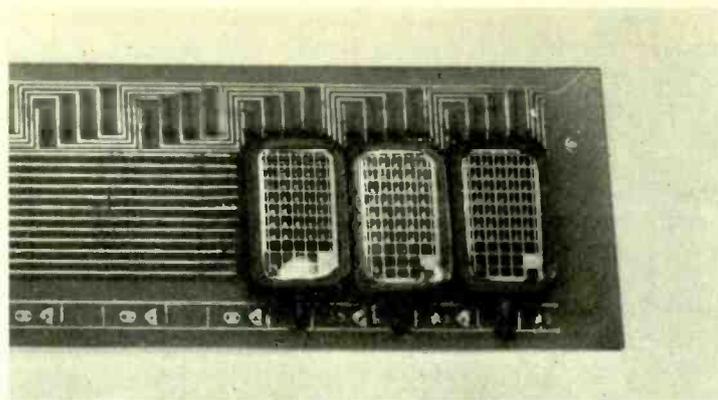


Electronic-fluidic interface switch, showing jet tube on left, discharge electrodes in the middle and collector tube on the right. (University College of North Wales).

signal is obtained by positioning a collector tube coaxially with the air jet so as to sense whether it is laminar or turbulent. The laminar jet diverges slowly and gives a large flow of air into the collector tube, whereas the turbulent jet diverges quickly and only a small flow passes into the collector. The corona discharge therefore switches the fluidic device from a high-output to a low-output state. Tests so far have shown that an electrical signal of 3kV passing a current of $0.1\mu\text{A}$ will give a fluidic signal strong enough to operate commercial fluidic devices. In the demonstration a water gauge tube was used to indicate the pressure signal obtained. The device is said to be suitable for operation over a wide temperature range and in noisy and dirty environments.

Neon matrix display tubes

Glow discharge alpha-numeric display tubes based on the matrix principle were shown by Mullard Research Laboratories. Characters are formed by the selection of dots in a 7×5 array, each dot being the negative glow at a cathode recessed below the glass surface of the tube. The cathodes are arranged in a thin, flat assembly while the common anode, a fine wire mesh, is between the cathodes and the viewing window. The tube is filled with neon gas. Cathodes can be selected to form characters by means of a diode decoding matrix, and, for example, to display the ten numerals a matrix of 40 diodes would be needed. Each neon dot element has a typical breakdown voltage of 170V, a maintaining voltage of 130V and a current consumption of about $150\mu\text{A}$, so a character requiring, say, 16 dots out of the



Glow discharge alpha-numeric display tubes (Mullard Research Laboratories). The picture shows three of the tubes mounted on a printed wiring board.

available 35 would draw about 2.5 mA. The luminance of the display—which is more than adequate for normal room use—is in excess of $2,000 \text{ cd/m}^2$. The tube gives a character size of $10\text{mm} \times 7\text{mm}$ and is made in a form which enables it to be mounted on a printed circuit board.

Camera to computer, direct link

Pattern recognition is becoming of increasing importance in a number of extremely diverse fields. One could almost say that every computer user would find it useful to be able to feed in data by optical means. E.M.I. showed the results of some work they have been doing in this field. A television camera was connected directly to an ICT 1905 computer via a standard interface. The programme was such as to sample the input picture at the 1,600 points in a 40×40 matrix. The signal level, or picture brightness, was measured at each of these 1,600 points and assigned a value between one and 64, which was stored.

In the experiment a graph plotter was programmed to deposit ink in six different density levels. The six density levels were achieved by rather crudely adjusting the amount of shading in a given area.

The 64-level pattern in the computer store was reduced to six levels and fed to the graph plotter. In spite of the rather rough treatment the original signal from the camera had been subjected to, the result at the graph plotter was recognizable. Admittedly all detail had gone but the various areas of dark and light were clearly there. If the graph plotter could have accurately reproduced the six levels of shading the results would have been much better.

All this goes to show that a large amount of information can be rejected and yet the picture can still be recognized. The object of this work is to discover just how much detail machines will require in order to distinguish between different objects. When this has been decided—and the results will depend upon the particular application—we can expect to see special purpose pattern recognition machines on the market that do not require a full-size computer to drive them.

Seismic pattern recognition

A combination of threshold detectors and timing circuits is used in a perimeter alarm system (called AIDA), shown by Elliott's, for detecting human footfalls even when these are masked by other vibrations having similar frequency spectra.

Analogue signals from an array of geophones buried round the perimeter of the protected area are amplified and filtered to remove frequencies outside the spectrum of interest. The filtered signals are then applied to pattern recognition circuits, which measure rise- and fall-time, duration, amplitude and repetition rate, and

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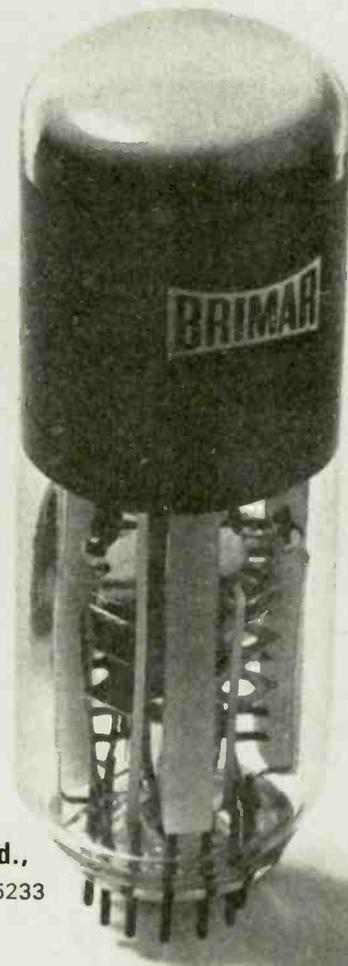
Typical Operation

V_h 6.3V; I_h 0.3A; $V_{a1+a3+a4}$ 1000V.

V_{a2} 100V; V_g (cut-off) -20 to -48V.

S_y 58 to 88 V/cm.

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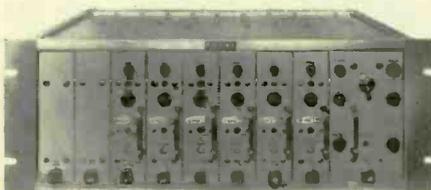


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compare the results with the normal characteristics of human footfalls stored in the equipment. Simultaneous agreement on all measurements for any particular channel will result in the alarm for the particular area being actuated.

Many uses for such alarm systems can be envisaged. For instance, the equipment could be made to recognize the normal vibration pattern of a machine tool and any departure from this pattern could be used to shut down the machine or sound an alarm—and the equipment could function along the clutter normally associated with a shop floor.

Full cycle thyristor firing

The conventional way of using a thyristor to control power in a load is to use phase control. With this method the firing of the thyristor is delayed after the beginning of the half cycle by an amount which depends upon the load power required. Firing late in the cycle gives low power, and early firing gives a high power. Now while current always flows at the end of a half cycle, it seldom does at the beginning, and this gives the effect of a lagging power factor. Also the supply current waveform is poor, containing many harmonics. These harmonics are produced into the MHz region and can cause severe radio interference.

These disadvantages can be overcome to some extent by the adoption of 'burst firing'. Here the thyristor is turned on at the beginning of a half cycle and remains on for several cycles. It turns off for several more cycles before turning on again. The average power is varied by varying the ratio of the number of 'on' cycles to the number of 'off' cycles.

Derby and District College of Technology have designed and built a logic system to control a triac (bi-directional thyristor). A five-bit binary number is the command signal, the triac turning on for as many cycles in a block of 32 as the binary number represents. In general the conducting cycles are spaced reasonably evenly through the 32 cycle period. This is an advantage over normal burst firing methods. The need for a digital command signal may be a disadvantage in many systems but in the case of a computer controlled process a digital signal is produced so that a computer could directly control a heating element in a process control system.

Vibrating wire clinometer

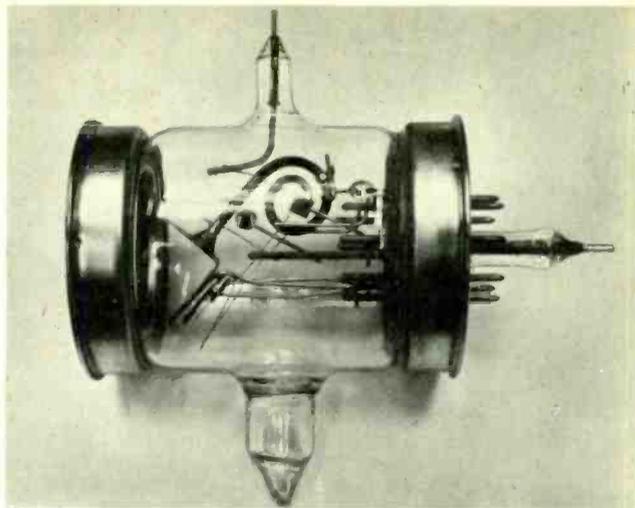
A clinometer employing a rather interesting principle was shown by Smail, Sons and Co. Ltd. (agents for Firma H. Maihak, A.G.). A steel wire is stretched between an oil damped pendulum and a fixed point on the instrument's casing, so that movement of the pendulum with change of slope alters the mechanical tension on the steel wire.

The steel wire is the frequency determining component in an oscillator; any change in the mechanical tension alters the resonant frequency of the steel wire and, therefore, the oscillator frequency.

Any variation in the angle of the instrument's casing results in a change of oscillator frequency, which is measured at a remote point. Using this principle clinometers are available that can measure angle changes as small as 2 seconds of arc.

High sensitivity photoemitter

A photoemitter being developed by Mullard Research Laboratories is claimed to have a sensitivity greater than that of any existing photocathode. It is formed by exposing the surface of single-crystal p-type gallium arsenide to the gases caesium and oxygen. Under optimum conditions the photoemitter has a sensitivity in excess of 500µA per lumen, and it has a response which extends through the visible spectrum and into the infrared as far as 0.9µm. The example on show was one of these photoemitters combined with a channel electron multiplier to form a



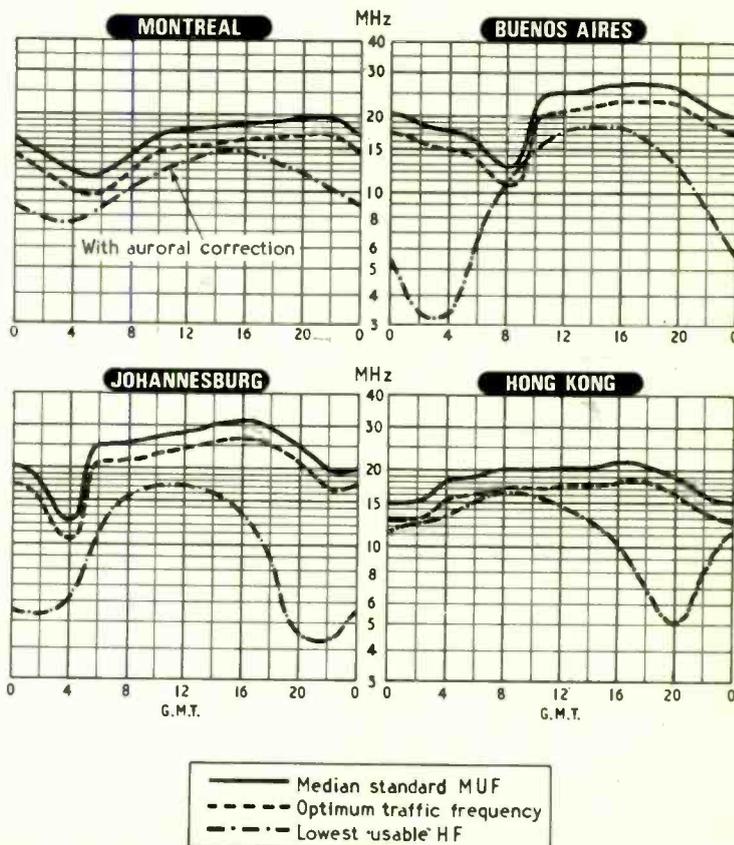
Photomultiplier tube using a new high-sensitivity photoemitter. (Mullard Research Laboratories)

compact, highly sensitive photomultiplier. There is a possibility that the response can be extended farther into the infrared by the use of other chemical compounds.

H. F. Predictions—May

The prediction charts show median standard frequency (MUF), optimum traffic frequency (FOT) and the lowest usable frequency (LUF) for reception in the U.K. Unlike MUF, the LUF is closely dependent upon such factors as transmitter power, aerial gain and type of service. LUFs shown were drawn by Cable and Wireless Ltd, for commercial telegraphy, using several kilowatts and aerials of the rhombic type.

Seasonal changes are most striking on the Hong Kong route; the peaks of recent months are depressed giving an FOT below 20MHz which changes little throughout the 24 hours. The Montreal route shows the same characteristic as it is also an East/West path in the same hemisphere. Daylight FOTs for the trans-equatorial paths continue above 20 MHz.



New Television Camera and Recorder Techniques

Highlights from the National Association of Broadcasters' convention in Washington, U.S.A.

by Aubrey Harris,* M.I.E.E.

The forty-seventh annual convention of the National Association of Broadcasters was held from March 23rd to 26th in Washington, D.C., U.S.A. The convention consists of a large number of equipment exhibits (146 booths) and many programme and engineering meeting sessions. The quality of the technical papers at N.A.B. is seldom worthy of note, whereas the broadcast equipment manufacturers invariably burn their midnight oil in the weeks before the convention in order to be able to show their latest electronic endeavours to the assembled, expectant engineers and station staff. [Incidentally, to give an idea of the size of the industry in the U.S., the F.C.C. has just announced that in 1968 there were 4,203 a.m. stations, 2,198 f.m. and 811 television stations (excluding translators).]

The 1969 show ran true to form, the main highlights being in innovations in colour cameras and videotape recording equipment.

Cameras

There were two major introductions in the colour camera field, one at the high-cost end of the scale and one in the low-cost region. The new Philips PC-100 three-tube (lead oxide) camera at \$84,850 (£35,000) has several striking new features, the most astounding of which is that the camera cable consists of one single triaxial cable (that is, a coaxial cable with two separate, insulated screens). This single cable, about $\frac{1}{8}$ in diameter, carries not only the encoded N.T.S.C. output signal and monitor signals from the camera to the camera control unit, but also sixty digital and sixty analogue control functions, external viewfinder signals, intercommunication, programme sound and camera power (100 volts d.c.) from the c.c.u. to the camera itself.

This not inconsiderable feat is accomplished by three separate multiplexing channels on the cable: a maximum length of 1 mile can be used normally, although this can be extended by the use of repeater amplifiers. The weight of the cable is only about one-tenth of that of the conventional colour camera cable, and this together with its smaller size is bound to have significant advantages in the logistics and costs of outside broadcast operations and studio design.

The camera features a colour bar generator, an encoder and a contour enhancer, all

built into the camera proper. The camera head, without lens, weighs only 70 lb and measures a mere 19½ in. long, 17 in. wide and is 15½ in. high (to the top of the viewfinder)—remarkably compact for a three-tube camera. The viewfinder tilts up and down and has quite a novel feature. It may be turned in a horizontal plane through 90° so that the picture image may be viewed normally from the side of the camera. Those who have attempted to make adjustments on the side of a camera while viewing a picture at the rear will appreciate the advantage of this.

Registration accuracy of 0.2% is claimed for the centre of the scanned image and accuracy of picture geometry within 0.5% of picture height. The peak signal to r.m.s. noise ratio is 50dB.

At the other end of the scale, RCA showed the PK-730, a new single-tube colour camera costing, without viewfinder but with 6:1 zoom lens, \$6,500 (£2,600) and with electronic viewfinder \$9,850 (£4,080). The camera utilizes an 8507A vidicon, in the optical path of which there is a pair of striped colour filters; the spatially shared signals representing the colour analysis of the viewed scan are electronically processed and encoded into an "N.T.S.C.-type" signal for helical scan recording or closed-circuit transmission. The encoded output signal differs from the true N.T.S.C. waveform in that the sub-carrier is not locked to the line frequency, and instead of I and Q signals of different bandwidth being used to modulate the sub-carrier, R-Y and B-Y signals of identical bandwidth are used for the quadrature/colour modulation. This simplified arrangement avoids the need for a delay line and compensating circuitry, although it was not claimed that the signal was up to full broadcast standard; nevertheless the subjective result was very acceptable and this type of system seems bound to find acceptance in many educational, commercial and other less critical uses.

Incidentally, the output can be made to conform to N.T.S.C. (and presumably PAL) standards by the addition of the appropriate encoder.

Video recording

A new entry into the professional videotape market was Westel who showed a new one-inch helical scan recording system in yet

another tape format. This recorder uses a small diameter (2-3 in.) drum guide with an "omega wrap" (200°) two-head configuration. It differs from other helical scan recorders in that only one-sixth of the information in a field is recorded per head sweep (as compared to complete fields in most other helical scan machines and compared to between 10 and 17 lines in transverse scan, quadrature-head type videotape recorders). Either longitudinally oriented or laterally oriented videotape, it is claimed, may be used with little, if any, difference in performance.

Another innovation is a dual-capstan tape device maintaining constant tape tension into, within, and out of the video head recording path. One problem with helical-scan recorders has always been the difficulty of maintaining correct and consistent tape tension around the drum guide; the dual-capstan arrangement, which has previously been used on computer-type, instrumentation and some audio recorders, simplifies the problem of consistent tape tension without external air lubrication. The reel-to-reel tape speed is 15 in. per second and a head-to-tape writing speed of 1260 in. per second is used. A total of five printed-circuit motors is used on the rack-mounted transport, one each for the supply and take-up reels, one for the head drum and one for each of the two capstan motors.

The time-stability of the video signal, directly from the demodulator, is in the region of ± 250 nanoseconds. This brings it well into the capture range of electronic timebase correction devices (such as Amtec) which are used both for "picture-straightening" purposes and also for bringing the signal within the range of colour time-element compensators (such as Colortec) for direct colour signal recovery operation.

Full interchangeability is claimed between the two versions available—the "record-only" WR-250, weighing 37 pounds including batteries, and the rack mounted studio unit WRR-350.

The output video signal-to-noise ratio is said to be 5 to 6dB higher than in other existing studio quality videotape recorders, although no exact figures were quoted. The U.S. price of the studio colour recorder (including the necessary time-element and colour compensation circuitry) is \$58,000 (£24,000); the monochrome version price is \$33,500 (£13,900). The portable, "record-only," versions sell for \$19,500 (£8,300) and

\$17,500 (£7,350), colour and monochrome respectively.

These recorders combine the simplicity of the helical-scan type of recorders with the stability of the broadcast type machine into a low-cost high-quality v.t.r. However, it seems unlikely that broadcasters would wish to be involved in yet another television tape standard, with all its attendant problems, particularly with the likelihood of broadcast E.V.R. (Electronic Video Recording) being introduced in a year or two.

The final step enabling absolute synchronization of two or more videotape recorders seems to have been reached by Ampex, who showed for the first time their RA-4000 Random Access Programmer. This enables tape "addresses" on different portions of different tapes to be selected remotely, automatically cued-up and the machines run synchronously from that point, enabling precise editing to be done by programmed information put into the RA-4000 or by treating the two playback machines as inputs to a video mixer the output of which feeds a v.t.r. in the "record" mode.

To enable this to be accomplished the tapes to be operated on have recorded on the second audio (cue) track digital addresses which indicate hours, minutes, seconds and also individual frames. The address recording may be done prior to, during or after the programme video and audio tracks are recorded. During operation the addresses at which the two machines are required to be run in frame sync are keyed into a control panel, as is also the address of the frame at which the edit from tape A to tape B is to be made.

The machines are started and an automatic search is made for the addresses keyed in, indicating the start of the sections required to be run in picture synchronism. The recorders find these addresses and then back-up to a cue point 150 in. (10 seconds) in advance of these points; the recorder reaching its cue point first waits for the other to cue up. Then both advance at nominally playing speed while the two addresses are continuously compared; any discrepancy is detected and corrected by automatic operation of the capstan tape-speed override circuit on the logging machine. The machines are then in picture synchronism at the desired frame; the tape speed control then reverts to normal intersync operation.

Another departure in the realm of videotape recording, which was likened to a "v.t.r. juke-box", was the RCA colour videotape cartridge recorder/player; this has been designed to record and replay short sequences (up to three minutes long) of video and audio material. The machine can accommodate eighteen enclosed cartridges of 2-in wide videotape, which may be recorded and reproduced by the two tape transport mechanisms within the equipment. Cartridges are reproduced under command of either external signals or signals recorded on the second audio track of a cartridge being played. While one cartridge is being reproduced by one transport the next cartridge is being automatically cued-up ready to play.

The switching signal transfers the signal system input connection from the transport playing the first cartridge to that handling the second cartridge; this gives a virtually

instantaneous picture switch and is ideal for running back-to-back commercial sequences, or other short programme sequences.

Automatic programme control

Both of the two last-mentioned devices seem to lend themselves admirably to incorporation into equipment for automatically controlling the sequence of television programme material being fed to the transmitter or network. Many companies were showing such equipment—General Electric, Ampex, Central Dynamics, RCA, Sarkes-Tarzian, Visual Electronics, to name a few. Details of each company's system vary, but in general these automation systems allow a large number of programme segments to be run, in rapid sequence if required, without manual action by an operator.

For example, film projectors, videotape and audio recorders may be cued-up and started at precise times, slides may be changed, and fading, mixing and cutting between video and audio sources is carried out automatically, although provision is always made for manual override, in case of unforeseen circumstances or because of a change of programme scheduling.

In a typical system each operation is key-punched into an IBM punched card, indicating video source, audio source, type of transition, time of transition, segment duration and brief title description. The cards are then stacked and fed into a card reader which feeds the information in sequence to a control unit, which operates in conjunction with the station clock system. Very often the "next ten" operations are displayed by a character generated display on a picture monitor, enabling the supervisor to check the forthcoming events and change them when desired. Video tape recorder and projector "pre-roll" cues are automatically given to enable these sources to be stabilized by the time the control equipment is ready to switch them to transmission.

Some more sophisticated systems take their input from the station computer, disc file, magnetic tape or remote lines rather than directly from a card reader. A local teleprinter type keyboard is often adjacent to the control equipment for insertion of special commands.

Conferences and Exhibitions

Further details are obtainable from the addresses in parentheses

LONDON

May 6-8 Savoy Place
Power Thyristors and their Applications
(I.E.E., Savoy Pl., London W.C.2)

May 20-23 Olympia
Electronic Component Show
(Industrial Exhibitions, 9 Argyll St., London W.1)

May 20-23 Kensington Close Hotel, W.8
Electronics Exhibition
(T. Jeffrey Burton Associates, 198 Forest Road, Tunbridge Wells, Kent)

May 28-29 Northern Polytechnic
Computer Aided Design Techniques for Electronic Circuits
(Dept. of Electronic and Communications Eng, Northern Polytechnic, Holloway, London N.7)

BIRMINGHAM

May 2 & 3 Grand Hotel
Service—its place in Marketing
(Society of Service Managers, 1 Tichborne Close, Frimley, Surrey)

EASTBOURNE

May 6 & 7 Grand Hotel
Automated Inspection
(Scientific Instrument Research Assoc., South Hill, Chislehurst, Kent BR7 5EH)

OVERSEAS

May 5-7 Ottawa
Electrical & Electronic Measurement
W. J. Moore, 797 Dunloe St., Ottawa 7)

May 5-7 Dallas
Microwave Symposium
(I.E.E.E., 345 E.47th St., New York, N.Y.10017)

May 5-8 Farmingdale
Instrumentation in Aerospace Simulation
(I.E.E.E., 345 E.47th St., New York, N.Y.10017)

May 6-8 Ispra
Nuclear Electronics
(Prof. Luciano Stanchi, C.C.R. Euratom, 21020 Ispra, Italy)

May 6-8 Atlantic City
Frequency Control
(M. F. Timm, Electronic Components Lab., U.S. Army Electronics Command, Fort Monmouth, New Jersey 07703)

May 7-9 Washington
Artificial Intelligence
(British Computer Soc., 23 Dorset Sq., London N.W.1)

May 14-28 Moscow
Automation '69
(Scientific Inst. Mfrs' Assoc., 20 Peel St., London W.8)

May 19-21 Dayton
Aerospace Electronics Conference
(I.E.E.E., 345 E.47th St., New York, N.Y.10017)

May 19-23 Montreux
Television Symposium & Exhibition
(Secretariat, Case-Box 97, 1820 Montreux)

May 21-23 Edmonton
Microwave Power Symposium
(W. R. Tinga, Elect. Eng. Dept., University of Alberta, Edmonton, Alta)

May 21-23 Gaithersburg
Electron, Ion, and Laser Beam Technology
(Dr. L. Marton, National Bureau of Standards, Washington, D.C. 20234)

May 22-23 Washington
Applied Magnetics
(I.E.E.E., 345 E.47th St., New York, N.Y.10017)

May 26-28 Washington
Laser Engineering and Applications
(Lewis Winner, 152 W.42nd St., New York, N.Y.10036)

London Component Show

Provisional list of exhibitors at the international show in May

The biennial Electronic Component Show opening at Olympia, London, on May 20th for four days is the 21st in the series sponsored by the Radio & Electronic Component Manufacturers' Federation. It will be the biggest of the series and will be the first international show sponsored by the Federation.

We list below the manufacturers and agents who have taken space. Indented below the names of U.K. agents are the overseas companies whose products they will be exhibiting. *Wireless World* will again be exhibiting and on our stand we will be demonstrating the Logic Display Aid to be described in the series of articles which begins in this issue. It is planned to include in our July issue a selection of the new components, instruments and materials introduced at the show. On the opposite page are illustrated a few of the new products already announced by exhibitors.

During the last two days of the exhibition a semiconductor symposium is being held in the Pillar Hall at Olympia under the auspices of VASCA, the Electronic Valve and Semi-Conductor Manufacturers' Association. The morning session on the 22nd will be concerned with linear integrated circuits (from basic economics to the latest developments), the afternoon session with digital i.c.s; and the morning session on the 23rd with power devices. Admission to each session is by ticket, costing £1 per session. Details of the programme and also tickets are available from VASCA, Mappin House, 4 Winsley Street, London W1N 0DT.

The show opens from 10.00 to 18.00 daily and admission costs 5s.

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|------------------------------------|------------------------------|--------------------------------------|-----------------------------------|-------------------------------------|
| AB Electronic Components | C.C.L. | Dymar Electronics | Farnell Instruments | M.B. Metals |
| AEI Semiconductors | C.G.S. Resistance Co. | EMI Electronics | Ferranti | M.C.P. Electronics |
| A.K. Fans | C.I. Automation | EMI Sound Products | Filhol, J. P. | McMurdo Instruments |
| AMP Industrial | Cadmium Nickel Batteries | East Grinstead Electronic Components | Fine Wires | Magnetic Devices |
| Air Control Installations | Cambion Electronic Products | Cannon Electric (G.B.) | Flight Refuelling | Magnetic & Electrical Alloys |
| Aladdin Components | Carr Fastener | Cathodeon | Floform Parts | Mallory Battenes |
| Aladdin Electronics | Cathodeon Crystals | Centralab | Formica | Mann Components |
| Alma Components | Chance-Pilkington | Channel Electrical Equipment | Fothergill & Harvey | Mansol (Great Britain) |
| Alston Capacitors | Channel Electrical Equipment | Air-LB | French composite display | Marconi Company |
| Amphenol | Ciba (A.R.L.) | Circuit Integration | G.I. Microelectronics | May Precision Components |
| Ancillary Developments | Circuit Integration | Circuitape | G.K.N. Screws & Fasteners | Metway Electrical Industries |
| Ariel Pressings | Clare, C. P. | Clare-Elliott | Gardners Transformers | Micro Waves Inst. |
| Arrow Electric Switches | Clare, H., & Co. | Coil Winding Equipment Co. | General Instrument Group | Microwave Associates |
| Ashburton Resistance Co. | Clarke, H., & Co. | Cole Electronics | General Instruments | Midland Silicones |
| Astralux Dynamics | Coil Winding Equipment Co. | Aumann, W. (W. Germany) | Girdlestone Electronics | Milton Ross Co. |
| Autronic Developments | Cole Electronics | Kumag A.G. (Switzerland) | Goodmans Loudspeakers | Mitsubishi Electric Corp. |
| Avel Products | Colvern | Kumag A.G. (Switzerland) | Greca Products | Morganite Resistors |
| Aveley Electric | Computer Controls | Siemens A.G. (W. Germany) | Greenpar Engineering | Motorola Semiconductors |
| Avo/Taylor | Computing Techniques | Concordia Electric Wire | Guest Electronics | Mullard |
| BICC-Bumdy | Concordia Electric Wire | Conollys (Blackley) | Haddon, Thomas & Stokes | Muller, Dr. Kurt |
| B. & R. Relays | Corner, G., & Co. | Cosmocord | Haddon Transformers | Multicore Solders |
| Adams & Westlake Co. (U.S.A.) | Counting Instruments | Crouzet England | Hallam, Sleigh & Cheston | Murex |
| Benedict & Jager (Australia) | Crouzet England | cie Petercem (France) | Harrison, A. T., & Co. | N.S.F. |
| Gordos Corp. (U.S.A.) | Electrotherm Engineering | Schmersal, K. A., & Co. (W. Germany) | Harwin Engineers | Newmarket Transistors |
| Minimotor S.A. (Switzerland) | Electrotherm Engineering | Siemens A.G. (W. Germany) | Hawthorn Baker | Newport Instruments |
| Siemens A.G. (W. Germany) | Electrotherm Engineering | Colvern | Healey Meters | O & W Electronics |
| Versa N.V. (Holland) | Electrotherm Engineering | Computer Controls | Heberlein & Co. | Oliver Pell Control |
| BSR | Electrotherm Engineering | Computing Techniques | Hellermann | Oltronix U.K. |
| Bakelite Xylonite | Electrotherm Engineering | Concordia Electric Wire | Hellermann Deutsch | Ospec |
| Barlow-Whitney | Electrotherm Engineering | Conollys (Blackley) | Hengstler, J., & Co. | Oxley Developments Co. |
| Beckman Instruments | Electrotherm Engineering | Corner, G., & Co. | Henry & Thomas | Painton & Co. |
| Bedco | Electrotherm Engineering | Cosmocord | Hesto (Henkels-Stocko) | Palmer Aero Products |
| Belclere Company | Electrotherm Engineering | Counting Instruments | Hewlett-Packard | Palmer, G. A. Stanley |
| Belling & Lee | Electrotherm Engineering | Crouzet England | Heyco Manufacturing Co. | Arco S.p.A. (Italy) |
| Berec International | Electrotherm Engineering | Electrotherm Engineering | Highland Electronics | Collins Radio Co. (U.S.A.) |
| Bird Electronic | Electrotherm Engineering | Enfield Phelps Dodge | Hilger Electronics | Republic Electronics Corp. (U.S.A.) |
| Bonnella, D. H., & Son | Electrotherm Engineering | Engineering Enterprises | Hilger & Watts | Resista GmbH (W. Germany) |
| Bowmar Instruments | Electrotherm Engineering | English Electric Valve Co. | Hinchley Engineering Co. | T.E.C. (France) |
| Bradley, G. & E. | Electrotherm Engineering | Enthoven Solders | Hivac | Park Royal Porcelain |
| Brandauer, C., & Co. | Electrotherm Engineering | Erg Industrial Corp. | Honeywell Controls | Parmeko |
| Uniform Tubes Inc. (U.S.A.) | Electrotherm Engineering | Erie Electronics | Hopt Electronics | Pedoka |
| Brit. Insulated Callender's Cables | Electrotherm Engineering | Erma | Howells Radlo | Perivate Controls Co. |
| British Physical Labs. | Electrotherm Engineering | Ether | Huber, J. J. | Permanoid |
| Brookdeal Electronics | Electrotherm Engineering | Ever Ready Company | Hysol Sterling | Permark |
| Brown, A. G., Electronics | Electrotherm Engineering | Evershed & Vignoles | Imhof, Alfred | Philbrick/Nexus Research |
| Brush Beryllium Co. | Electrotherm Engineering | Dynamic Insts. Corp. (U.S.A.) | Imperial Chemical Industries | Planer, G.V. |
| Bulgin, A. F. & Co. | Electrotherm Engineering | Gossen, P., & Co. (W. Germany) | Insulating Components & Materials | Plannalr |
| Burgess Micro Switch Co. | Electrotherm Engineering | S.F.A.I.R.E. (France) | Instn. of Electrical Engrs | Plasmoulds |
| | | Tettey A.G. (Switzerland) | | Plastronics |
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| | | | | Precious Metal Depositors |
| | | | | Helmut Fischer (W. Germany) |
| | | | | P.M.D. Continentale (France) |
| | | | | Schlottar, Max (W. Germany) |
| | | | | Precision Electronic Terminations |
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| | | | | Pye Switches |
| | | | | Quickdraw Co. |
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| | | | | Redpoint |
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| | | | | SGS (U.K.) |
| | | | | STC/ITT Components Group |
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| | | | | S.T.P. Electronics |
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| | | | | Sarcem Products |
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West Hyde Developments
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 Woden Transformer Co.
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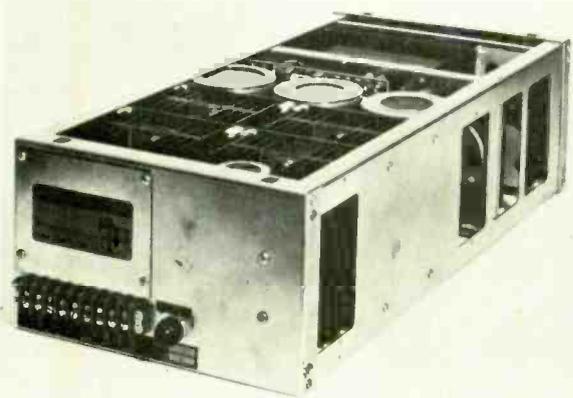
Ultra Electronics (Components)
 Union Carbide UK

Watson, W. & Sons
 Waycom
 Wego Condenser Co.
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Valory Watch Co.
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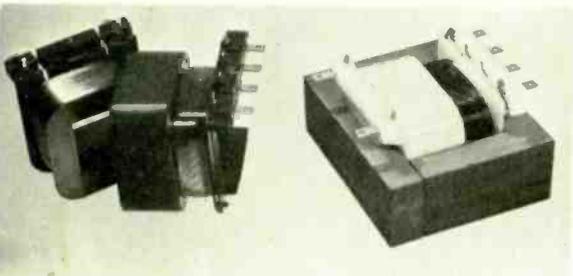
Z & I Aero Services
 Zenith Electric Co.

Typical of the series 40 stabilized power supplies introduced by A.P.T. Electronic Industries, is this 43D10 which provides 50V at 10A. **WW 393 for further details**



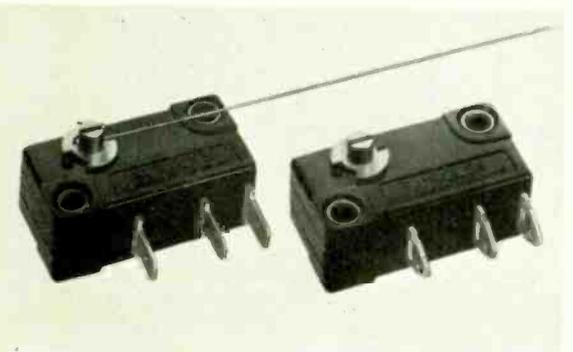
Lyons Instruments new high-power pulse generator (PG 25) provides two outputs of opposite polarity each capable of supplying 1A into 50Ω. Frequency range is 10 Hz to 20 MHz. **WW 391 for further details**

The secondary bobbin in this small mains transformer (Hinckley Engineering) incorporates a moulded skirt which shrouds the primary winding. **WW 394 for further details**



The infinite resolution contactless potentiometer recently introduced by Salford Electrical Instruments is available in various configurations to measure either angular or linear displacements. **WW 392 for further details**

This d.c. multimeter from Levell Electronics measures 0.3 μV to 1 kV in 18 ranges, from 1pA to 1A in 24 ranges and from 0.3Ω to 1000 MΩ in 18 ranges. It incorporates a high-gain, solid-state, chopper-stabilized d.c. amplifier. **WW 396 for further details**



Low torque, rotary-action micro switches (type VII) introduced by Burgess Micro Switch Company for sensing, detection, counting and similar applications where precision coupled with resistance to mechanism derangement is essential. **WW 395 for further details**



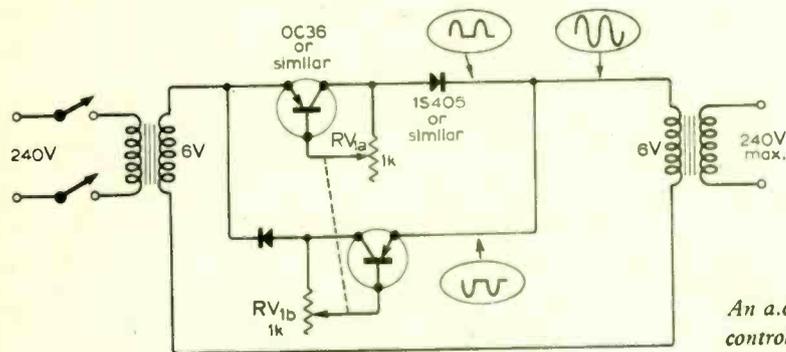
Circuit Ideas

Transistor a.c. mains controller

The circuit shown in Fig. 1 is self-explanatory. The output waveform is approximately sinusoidal. Output power is, of course, dependent on the two transformers and on the allowable dissipation of the transistors. Care will need to be exercised in operating the ganged $1k\Omega$ bias control. As a precaution a suitable

'stopper' resistor can be put in series with each of the two variable resistors to limit maximum dissipation.

J. R. HARRIS,
Woodstock,
Oxon.



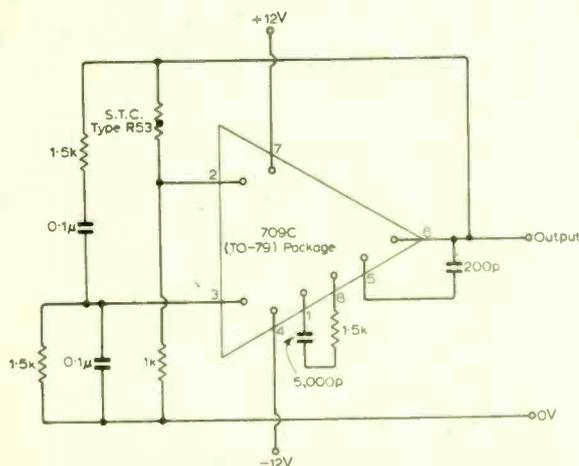
An a.c. mains power controller using transistors.

Oscillator using operational amplifier

A simple Wien bridge audio oscillator can be built using an integrated circuit operational amplifier. The bridge is connected between the output and the non-inverting input of the op. amp. A thermistor and resistor connected between the output and the inverting input limit the output amplitude, producing a sinusoidal output. Two additional capacitors and one resistor are necessary to control the high-frequency gain of the op. amp.

The circuit shown oscillates at about 1kHz with an output of 3.5 volts p-p into a 100 ohm load. The output resistance is very low. Operation from other power supplies or a single supply is possible. The normal audio frequency range can be covered by the usual arrangement of switched capacitors and a two gang potentiometer.

D. W. J. BLY,
Mullard Observatory,
Cambridge.



Mr. Bly's Wien bridge oscillator.

Constant-impedance attenuator

This circuit presents a relatively constant impedance in one direction. It was originally devised as a simple volume control for use with a loudspeaker, as shown in Fig. 1. With VR_1 equal to $3R$ the input impedance varies between 75% R and 120% R . With VR_1 equal to $4R$ it varies between 80% R and 133% R . This circuit can be used, for example, to improve the attenuator of the "Low Distortion RC Oscillator" by P. F. Ridler (*Wireless World*, August 1967). The attenuator originally used (Fig. 2) will only give an output at 600Ω in the 2.2V position if the pot wiper is in the middle of the track, the impedance falling to 350Ω at either end. These variations can be much reduced by replacing the attenuator with the circuit of Fig. 3.

D. AUSTIN,
ATV Network Ltd.,
Birmingham.

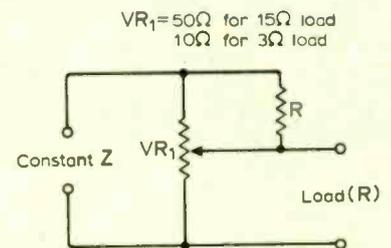


Fig. 1. Constant impedance attenuator.

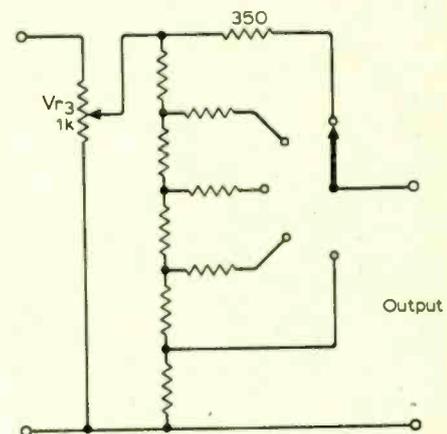


Fig. 2. Attenuator originally used in Ridler's oscillator.

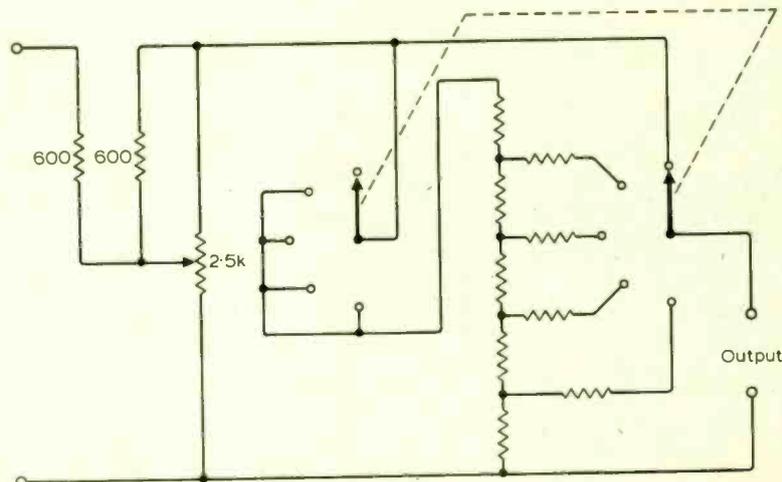


Fig. 3. Improved attenuator for oscillator.

Marconi Radio Telephone Terminal Type H5510

For interconnecting h.f radio circuits with inland telephone networks.

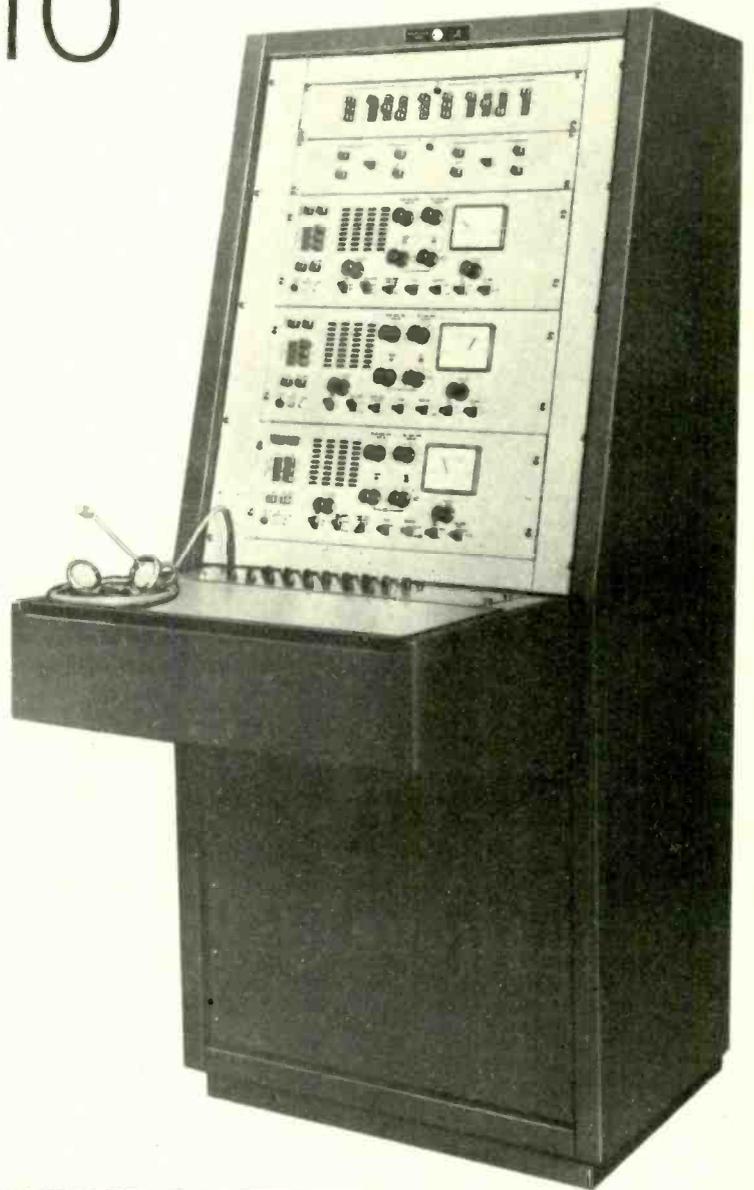
- Eliminates circuit loop instability caused by feedback from the receive-to-transmit path.
- Reduces the effects of fading and high noise level, characteristic of h.f radio propagation.
- Controls outgoing speech so that transmitter loading is maintained at optimum level.
- Channel displacement and privacy equipment can be incorporated.
- Maximum capacity, 4 channels.

Solid-state circuitry

Plug-in modulator book units

Flexible design

Optional built-in tape recorder



Marconi telecommunications systems

Member of GEC-Marconi Electronics Limited

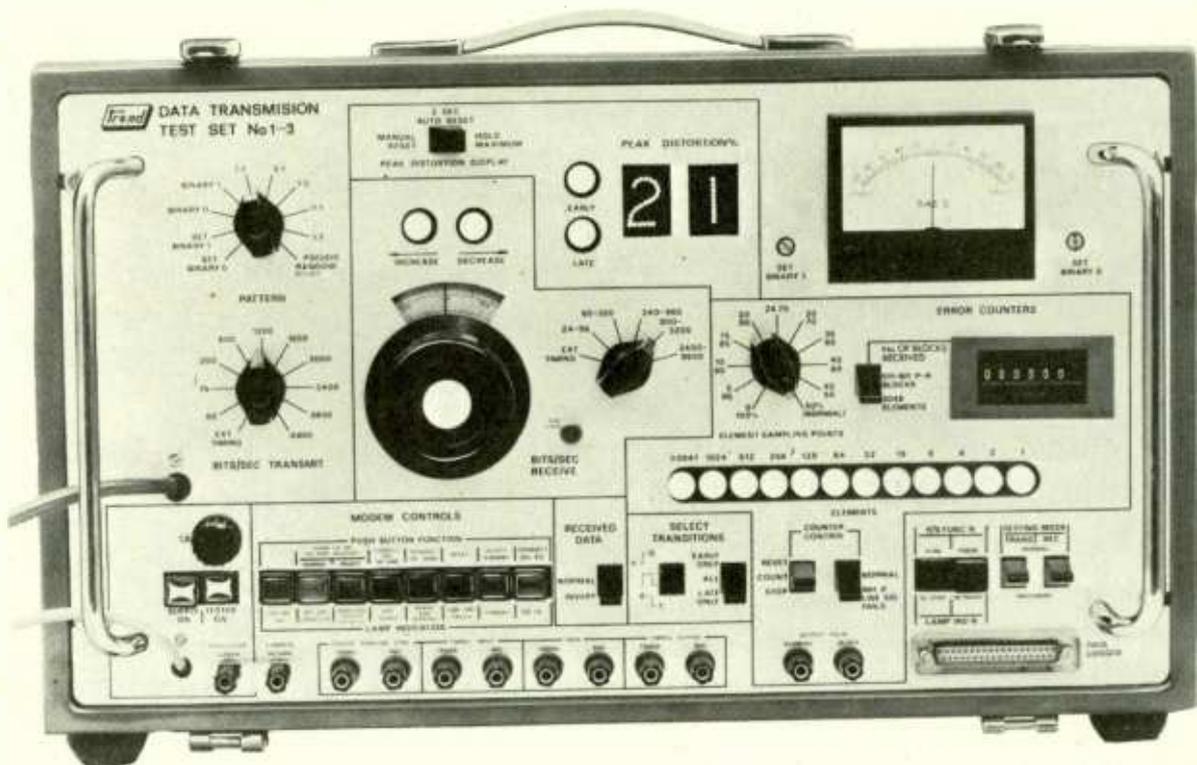
The Marconi Company Limited, Radio Communications Division, Chelmsford, Essex, England

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WW-110 FOR FURTHER DETAILS

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Letters to the Editor

The Editor does not necessarily endorse opinions expressed by his correspondents

Resistance labelling

When resistor values are marked on circuit diagrams in the usual abbreviated way; e.g., 6.8k for 6,800 ohms, errors can arise from the omission of the decimal point. (This can very easily happen if the diagram is a poorly duplicated photocopy.)

The risk of this type of error can be avoided by using the Continental convention whereby the 'multiplier' letter is substituted for the decimal point. Thus, 6.8k becomes 6k8, 3.3M becomes 3M3, and so on. This notation seems to be catching on among British engineers whose work brings them into contact with Continental circuit diagrams, and this encourages me to suggest that the time may be ripe for journals such as *Wireless World* to adopt it.

Naturally, it would look a bit odd at first. Any new notation does. But we don't bat an eyelid at 'kHz' these days, which shows how quickly one gets used to things.

The system appears to break down when one has to indicate fractions of an ohm, as in, say, 3.9 ohms. One could put 'U' for 'units' and write 3U9, but the existing Continental practice seems to be to write '3E9', etc. I don't know what the 'E' stands for (I would guess 'Einheit' though perhaps some better-informed reader can supply the answer) but one could still use the system even it meant nothing in English.

G. W. SHORT,
South Croydon.

Aerial erection

At 40 miles from London I've always found a home-made aerial in the loft quite satisfactory for TV and f.m.-mono transmissions. But now having assembled a stereo version I find I need an outside aerial, and for me at any rate that means a factory built job. I took it for granted that dealers would carry them as a matter of course: they always used to. But not so now. I've been to half a dozen dealers in three sizeable towns and though some are a bit cagey on the subject it appears that (a) aerials are practically not available retail, and (b) there is virtually only one aerial erecting contractor for the greater part of Essex and he is at the other end of the county, which would inevitably put the cost of an erected aerial sky-high.

I am writing to you as Editor of our senior radio magazine because I feel sure your im-

portant advertising links with the trade will not prevent you ventilating a subject of some importance to the majority of your readers. No doubt for dealers it is a great convenience to be able to put this work out to contract, but if as a reciprocal gesture they undertake to refrain from selling aerials retail, it seems to be a gesture at the public expense which the Monopolies Commission should take an interest in. But I shall be much interested to hear your views.

P. J. A. INNES,
Dunmow,
Essex.

Class A versus class B

I was very interested to read J. L. Linsley Hood's remarks concerning subjective differences between class A and class B solid-state amplifiers ("Simple Class A Amplifier", April) since I, too, have recently been performing a series of tests between the two classes of operation.

I feel that the 'slight edginess' referred to in the article is the subjective effect of crossover distortion which, in quite a few of the lower price class B amplifiers, tends to rise in magnitude with reducing power yields and with increasing frequency. High string notes whose harmonics run up to quite high orders, therefore, would be more affected by this sort of distortion than lower frequency signals of greater power (sound intensity). This, indeed, is one of the worst of class B subjective effects and by studying the harmonic yields over the frequency spectrum one would conclude that the crossover effect produces a whole series of odd-numbered harmonics extending to high orders which, of course, are singularly inharmonious to say the least!

The effect is aggravated by the extensive power bandwidth of many recent designs, especially those employing silicon transistors, power not uncommonly being delivered well into the 'radio spectrum' to 40kHz or more. While a passband in excess of the audible spectrum is desirable for maintaining wave-shape and endowing good rise-time features, I feel personally that this power response business is being taken a bit too far. I like to roll-off at a fairly slow rate of 6dB/octave from about 25kHz, and by doing this (not necessarily with a switchable low-pass filter) the rise-time performance is not unduly upset (from the audio aspect) yet disturbing

harmonics are deleted. It seems that although such harmonics might fall above the audible spectrum they can certainly interfere with the complex waveforms of music signals. Rolling-off in that way often minimises the 'listener fatigue', also mentioned by Mr. Linsley Hood, when the amplifier happens to be prone to such symptoms.

It is noteworthy that some listeners are less disturbed by class B amplifiers than others. But those whose ears do 'twitch' to slight high-order odd-numbered harmonic distortion will most certainly discern a difference when rapid A-B testing is made against a well designed class A amplifier and when the comparative material itself carries a high range of overtones and when the listening is performed at relatively low power level. It must be mentioned, though, that there are some class B designs—tailored to reduce crossover distortion—that sound virtually the same as a good amplifier in class A mode; but the price is an important factor that *must* be taken into account when making comparisons like this. From the consumer's point of view a low-cost class A amplifier—assuming that it can produce sufficient audio power and the other audio parameters are as required—must surely be better than a relatively more expensive class B amplifier, the expense of which is the result of the extra design and researches applied to achieve a class A performance, anyway!

GORDON J. KING,
Brixham,
Devon.

Improper oscillations in transistors

Although not a regular reader of your magazine and although I did not see Mr Pitt's original letter on 'improper oscillations in transistors' in the January issue, I am bound to comment on a statement in the reply to this letter by Mr. Vanderkooy in March.

Mr. Vanderkooy asserts that one resistor and one transistor can never cause a transistor to oscillate. It is the experience of the nuclear physics group here that this is far from true. For the past eight years we have been exploiting the fast switching behaviour of transistors when used in the avalanche mode and although there are only a few (2N914 is the best) which can be used reliably as stable pulse amplitude discriminators, we have found that almost all n-p-n transistors can be made to avalanche repeatedly without destroying themselves. These transistors only require a collector load sufficient to limit their dissipation and as the supply voltage is increased beyond the avalanche potential, the transistor bursts into relaxation oscillations analogous to the thyatron. In order to use the device as described the base has to be reverse biased to stop this oscillation and hold the transistor off. When an input pulse applied to the base exceeds the triggering threshold a collector pulse of 15V into a 50Ω load with 0.5 ns rise-time is common with the 2N914.

With regard to decoupling, it is very difficult to completely isolate the device as the radiation from perhaps a 0.5-A pulse

rising in less than 1 ns is not easy to contain, and sealed boxes and elaborate supply filtering are required. Needless to say this transmission can be picked up easily on a small transistor radio.

As for capacitive loading of the collector, this decreases the pulse repetition frequency up to a point and then quenches oscillation.

Unfortunately the means to look at such phenomena are expensive, so might I suggest that one of your regular contributors designs a simple sampling unit to push the use of say a 10 MHz antique scope up to a few hundred MHz. This would not only open up a new domain of amateur investigation but no doubt please the 'Hams' of the 2-metre band.

N. W. BENNÉE,
Dept. of Physics,
Birkbeck College,
London W.C.1.

Surface temperature thermometer

With reference to the temperature measuring instrument described by Mr. L. Nelson-Jones in the April issue, there is a possible source of error which has not been mentioned.

This is when the instrument is used on an item the mass of which, over the contact area, is less than the conducting mass of the probe. In these circumstances the probe will conduct sufficient heat away from the contact area to lower the temperature of the contact area and give a low indication.

It is appreciated that Mr. Nelson-Jones has reduced the conducting mass of his probe to a minimum and that when used, as illustrated, on a large heat sink, errors from this source are negligible. However, if this probe were to be used to measure the temperature of, say, a 0.012in metal skin, the error may well be significant.

As this is so, I feel that this ought to be pointed out so that constructors may be warned of this limitation to accuracy.

H. D. READ,
Yeovil,
Somerset.

The author replies:

I agree that with very small or very thin bodies a surface temperature measurement made with my instrument will be in error. This type of error is common to all such instruments, and the magnitude of the error depends on the relative heat losses of the probe and the body being measured in the case of small bodies. In the case of very thin bodies the error is due to the thermal resistance of the source in supplying heat to the heat losses of the probe. In my design I did try to keep the heat losses to a minimum for this type and size of probe because of this source of error.

I should perhaps have emphasised this aspect more strongly, and the fact that I designed the probe for the larger heat sink rather than for say individual TO5 transistors. The reason for this is that it is normal, for the smaller transistor, to measure the prevailing ambient temperature in the vicinity of the transistor, and then to calculate from the manufacturer's derating curves

whether or not the transistor is in a safe operating temperature region. Whereas for larger heat sinks, due to the many factors involved, it is not as safe to calculate the temperature of the junction, mainly because one does not know the temperature of the heat sink on which the manufacturer's derating curves are usually based.

A useful but not infallible guide is the response time of the probe. If this is fast then the reading should be accurate, but if the pointer is very sluggish to take up a steady reading, then the reading should be regarded with suspicion.

L. NELSON-JONES.

Improving old loudspeakers

Mr. Bennet-Clark's novel theory (March issue) regarding the 'Hookean spring' action of loudspeakers seems strangely at odds with the rest of his text, in the course of which he advocates removal of as much spring as possible from the cone-edges of old loudspeakers.

All loudspeakers have a certain amount of axial restoring-force (spring) in their cone-edge and coil-centring material, and this, whether corrugated paper or not, must be substantially 'Hookean' (strain proportional to stress, up to the elastic limit), if it is to last for any reasonable time.

One feels it is not failure of Hooke's Law which is to blame here, but rather that an oscillating mass attached to a spring has a natural period of vibration, the frequency of which is mainly determined by the mass/spring characteristics of the complete system. The stronger the spring in relation to the mass, the higher the natural frequency, and vice versa.

It follows therefore, that increasing the compliance, i.e., weakening the spring, and/or increasing the cone weight by giving it an extra skin, will both result in the lower fundamental resonance that Mr. Bennet-Clark has found in practice.

T. H. FRANCIS,
High Wycombe,
Bucks.

The author replies:

I quite agree with Mr. Francis' last paragraph and indeed, although I may not have expressed it clearly I appreciate that this was the effect of my treatment to old loudspeakers. The point that I wished to make

about the use of corrugated paper surrounds was that they have elastic properties that are substantially non-linear; that strain is not proportional to stress.

I think that it is fairly generally accepted that either the use of cloth, leather, plastic foam or plastic roll surrounds substantially increases the linearity of movement of a loudspeaker cone. My aim has merely been to achieve this with an existing loudspeaker.

I do not feel, in answer to Mr. Francis' first paragraph, that I have said anything that constitutes a novel theory; all this seems to be accepted practice.

H. C. BENNET-CLARK.

Network neology

There has been much interest in the literature recently in such circuit-elements as the nullator and the norator. The former has been facetiously defined as a one-port which is simultaneously open and short-circuit; the latter is a one-port sustaining arbitrary voltage and current. Combined, they give a two-port, the nullor, which is equivalent to a perfect operational amplifier.

It may be thought by the uninitiated that such elements are the thoroughly un-British products of foreign and fevered imaginations. But can we afford to ignore any part of scientific progress? Who knows but that in a few years the inventing of circuit elements may pass from just a sub-branch of technology to a fully competitive activity, perhaps to be included in some future Olympics. It is in preparation for such an eventuality that the following ideas are offered.

Four new circuit elements are proposed which as far as the writer is aware, have not been previously described. They are the notator, the antiator, the unator, and the disator. Unfortunately no experimental versions have yet been produced. In the case of the first two this is understandable since they are both infinite-ports—a far more advanced concept than a mere one- or two-port element. A notator has an infinite number of input ports and if all carry different currents, the current in the output is *not* equal to any of them. Similarly an antiator has an output current which is the *opposite* of all the inputs simultaneously.

No definitions are provided for the unator and disator and these are offered freely in the hope that British genius can provide a solution. PETER WILLIAMS,
Paisley College of Technology,
Renfrewshire.

John Clarricoats

On behalf of the 160 Meter Radio Amateurs, I wish to convey our sincere regrets and sympathies on the passing of John Clarricoats, G6CL. We shall all miss him greatly, for his enthusiasm and support of 160 Meter Band operations DXwise and propagation research, not only through R.S.G.B. but also recently through *Wireless World*. He was a fine gentleman in every sense of the word, as well as a dedicated radio amateur.

STEWART S. PERRY, W1BB,
Winthrop,
Mass., USA.

Our Next Issue

Amplifier survey. The terms and figures that contribute to the specification sheet of an audio amplifier will be thoroughly investigated by a design engineer accomplished in this field. Tabulated data on commercially available amplifiers will also be presented.

Units converter. As announced on p.202 a *Wireless World* designed "slide rule" for conversions between common electronics and radio units—frequency/wavelength, ratios/decibels etc. (including Imperial/metric SI conversions) will be offered to readers.

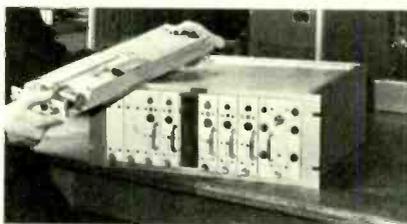
New Products

Gallium Arsenide Light Sources

Five gallium arsenide diode light sources from Texas Instruments Ltd., types OSX 1203, and OSX 1205-1208, emit near-infrared light when forward biased. Radiant output powers range from 20mW for the OSX 1205 to 200mW for the OSX 1208 at 25°C.

Types OSX 1203 and 1205 to 1207 are mounted in hermetically sealed packs with a flat window in the top of the case. The cathode makes electrical contact with the case and adjoining solder lug. The anode is in electrical contact with the stud which is insulated from the case by a glass-to-metal seal. Static forward voltage (V_F) is 2V maximum, spectral bandwidth with $I_F = 2A$, is 450 angstroms and emission band angle is 130°. Diameters of the emitting crystals are 36 mm for the OSX 1203 and OSX 1205 and 72 mm for the OSX 1206 and 1207. The OSX 1208, which is mounted on a copper stud header for efficient heat dissipation has an output of 200mW at 25°C. The anode is in electrical contact with the stud, the cathode lead being a varnished 0.25mm copper wire fastened to the stud by a ceramic insulator. Spectral bandwidth and maximum static forward voltage are identical with the types OSX 1203 and 1207, being 450 angstroms, at half power points, and 2V respectively. Storage temperature of all devices is -55° to +100°C. These devices may be used in communications lines, infrared telescopes and binoculars, and in i.r. intruder detection systems. Texas Instruments Ltd., Manton Lane, Bedford, Bedfordshire.

WW306 for further details



world's foremost receivers. Racal Communications Ltd., Western Road, Bracknell, Berkshire.

WW310 for further details

Versatile Power Supplies

Regulated variable power supplies designed to operate either as a constant voltage source or in a constant current mode are announced by Coutant Electronics. Voltage or current mode of operation is selected by a front-panel switch. The voltage is accurately set by coarse and fine controls and the current is adjusted by two similar but separate controls. Voltage and current levels are indicated on a built-in dual-scale meter. Thus it is possible after setting the supply to two different functions, to switch from constant-current to constant-voltage operation. In the constant-voltage mode



the output voltage remains within $\pm 0.005\%$ or 1mV of the preset level, whichever is the greater, for $\pm 10\%$ mains variation. Output impedance is less than $5m\Omega$ at 100kHz; ripple voltage less than 1mV peak-to-peak and the transient response is such that on switching from no load to full load, the

output recovers to within 10mV of the steady-state voltage in less than $10\mu s$. In the constant-current mode the input current is held to within $\pm 0.01\%$ or 0.1mA of the preset level, whichever is the greater, for a $\pm 10\%$ mains variation. The output current level varies less than 3mA from its setting for a change from zero to maximum output voltage. Operating temperature range is -10° to $+45^\circ C$ and the required input is 105-240V a.c. 45-400Hz. Three models are currently available: types LP.50/50 (0-50V d.c. 0.5A maximum); LP.100/30 (0-30V d.c. 1A maximum); LP.200/15 (0-15V d.c., 2A maximum). Each unit is housed in a case measuring $133 \times 86 \times 282$ mm deep and weighs 3.175kg. Coutant Electronics Ltd., 3 Trafford Road, Reading, Berkshire, RG1-8JR. WW 338 for further details

Hi-fi System

British Radio Corporation are about to enter the hi-fi market with a £200-300 ensemble comprising an f.m. stereo tuner/amplifier, record player and twin cabinet speakers. The usual controls are provided and tuning over the f.m. range 87.5-108.3 MHz is by five station selectors and press-buttons. Solid-state circuitry is used throughout employing 33 transistors and 15 diodes. Varicap diode type tuning is employed. On the audio amplifier side, socket facilities are provided for left- and right-hand speakers of 4-15 Ω impedance, magnetic and ceramic stereo pickup input, tape recorder and auxiliary stereo input. Power output into a 4- Ω load with sinewave input is approximately 15W with better than 1% distortion: into a 15- Ω load, power output is approximately 10W. Frequency response measured at a constant output of 4W with bass and treble controls set level is 40Hz-16kHz ± 1 dB (30Hz-20kHz ± 3 dB). Bass control range at 50Hz with reference to 1kHz is +12dB to -16dB as is the treble control range at 10kHz with reference to 1kHz. Approximate dimensions of the unit are 550mm long, 26mm deep, 100mm high. The record player employs a Goldring-Lenco GL75 transcription unit which has a 4kg turntable driven by a 4-pole constant velocity motor and has low wow and flutter levels. The pickup arm is provided with a hydraulic cueing device and an adjustable bias compensator. Speed adjustment is continuously variable between 15 and 18 r.p.m. and between 30 and 86 r.p.m. with click-stop positions for 16 $\frac{2}{3}$, 33 $\frac{1}{3}$, 45 and 78 r.p.m. A lightweight interchangeable headshell is fitted with a Goldring 800/E magnetic cartridge. The twin speaker system employs Goodmans 305mm long-throw bass units and 102mm sealed back mid- and treble-frequency units fitted in cabinets with front face dimensions of 560 \times 340mm and a depth of 255mm. Crossover is at 1500Hz. Interconnections are made with connectors wired in the DIN configuration. British Radio Corporation Ltd., Thorn House, Upper St. Martin's Lane, London W.C.2. WW 339 for further details

Pulse Current Thyristors

Thyristors specifically designed for pulsed current operation are announced by Motorola. Six types, JAN2N 4199 to 4204 are especially applicable to military equipment such as pulse modulators for magnetrons, radar altimeters, surveillance and ranging radar, satellite systems and phased arrays. They are equally suited to similar civil applications. Forward current rating is 100A with peak forward blocking voltages between 300 and 800V. Maximum turn-on time is 400ns, di/dt rating 5,000A/ μs and pulse repetition as high as 20,000 per second. Switching characteristics are stable over the temperature range -65° to $105^\circ C$ and limits on all critical parameters are guaranteed. Motorola Semiconductors Ltd., York House, Wembley, Middlesex.

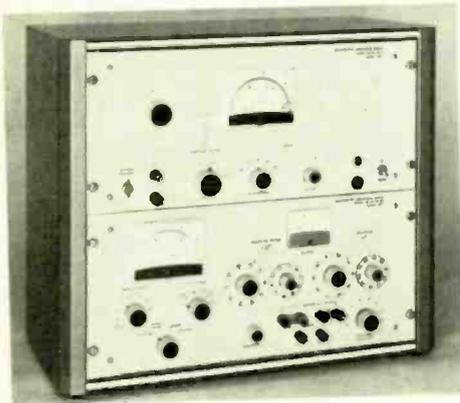
WW 337 for further details

J-band Solid-state Source

A compact J-band solid-state power generator type SSJ9 has been introduced by the M-O Valve Co. It is an electronically-tuned device suitable for local oscillator or test source use. The centre frequency can be pre-selected within the band 12.4 – 14 GHz with a tuning range of 250 MHz. Maximum power output is 5mW. The source operates from a 28V 100 mA supply and has an overall size of 85mm long x 37mm diameter. The M-O Valve Co. Ltd., Brook Green Works, London W.6. **WW 322 for further details**

Capacitor Bridge

A bridge designed for the measurement of all parameters of electrolytic and tantalum capacitors is announced by B.P.L. It is a four-terminal solid-state instrument, model CB154/4, which can be used with varying frequencies up to 20kHz and covers the capacitance range 0.01 μ F to 1F. Leakage current measurement is provided in nine ranges enabling values as low as 0.1 μ A to be detected. Another feature is a facility for the measurement of the voltage across the capacitor under test. Internal switchable bridge frequencies



and three separate panel meters are said to make for accurate reading on all parameters. Two internal bridge frequencies of 50Hz and 100Hz can be selected and an external frequency source up to 10kHz can be fed in. The internal polarizing voltage is fully stabilized over the entire range which is continuously variable up to 600V. Operation is from 115/125 and 200/240V, 50 or 60 Hz, a.c. The CB 154/4 measures 483 x 305 x 457mm and costs £425. British Physical Laboratories, Radlett, Hertfordshire.

WW 309 for further details

Portable Multi-band Receiver

One of the higher priced portable radio receivers now available is the Zenith Trans-Oceanic Royal 7000 which has been announced recently. This receiver carries a recommended retail price of £180 and provides reception on eleven wavebands. Refinements include a b.f.o., calibrated logging scale, and a log chart compartment and time zone indicator. The waveband ranges are: 150–400 kHz, 540–600 kHz, 1.6–9.0 MHz, 9.4–10.1 MHz, 11.4–12.3 MHz, 14.6–15.8 MHz, 17.1–18.5 MHz and 20.6–22.4 MHz. Bandsread tuning is provided on the s.w. bands. Also covered is the 88–108 MHz v.h.f. f.m. broadcast band and in the final position of the selector switch, the receiver is crystal-locked to the American v.h.f./f.m. weather broadcasts on 162.55 MHz. A "Norm-Sharp" i.f. switch modifies the i.f. bandwidth to reduce adjacent interference on s.s.b. and c.w. reception. Semiconductor complement totals 18 transistors (including the voltage regulator) and 9 diodes. A telescopic aerial is built-in for s.w. reception and a



ferrite rod provides for the reception of medium- and long-wave signals. The ferrite rod can be detached from the receiver and extended to a window to improve reception inside buildings. The receiver employs a 150mm elliptical loudspeaker and is powered internally by nine 1.5V cells, or alternatively it can be plugged into the mains supply via a fitted mains unit. The Zenith 7000 measures 240 x 350 x 160mm and weighs 7kg. U.K. distributors: United Mercantile Co. Ltd., Sovereign House, 13-14 Queen Street, Mayfair, London, W1X 8BB.

WW 320 for further details

Press-button Reed Switch

Contact bounce, a feature of press-button key switches which can be troublesome in keyboards associated with business machines and computer peripheral equipment, has been reduced by a new method employed by Starpoint Electrics. In their push-button reed switch, type 1RB1, two circular magnets are fitted; one to the switch housing and the other around the moving plunger. This gives a switching time of less than 1ms on operation. The 1RB1 is specially designed for p.c. boards and has terminals of pure nickel. It is claimed to have a life in excess of 10×10^6 operations. Keys may be mounted individually or in multiple arrays and complete keyboards with solid-state encoding can be supplied. Starpoint Electrics Ltd., 86 Coombe Road, New Malden, Surrey.

WW 321 for further details

Gunn Diode Oscillator

A stable and spectrally pure source of microwaves is provided by MI-Sanders' new Gunn diode oscillator, type 6061. It covers the frequency range 8.0 to 10.5GHz, and comprises essentially a hybrid mode cavity whose resonant frequency may be varied through the X-band by insertion of a micro-



meter spindle, and a Gunn diode which is suitably mounted and shunted across the cavity. When biased between -8 and -16 volts, the diode will oscillate in a cavity-controlled Gunn mode at a frequency that is determined primarily by the micrometer insertion, and to a lesser extent by the characteristic properties of the diode. The tuning rate is approximately linear and an individual calibration chart is supplied with each oscillator. Microwave power (5mW typical) is coupled via an iris in the end wall of the cavity, which is matched at 9GHz by a fixed stub. Power output may be further improved by additional matching stubs in the outer waveguide. The instrument is priced at £70, f.o.b. U.K. A suitable power supply is the type 6590. Marconi Instruments Ltd., Sanders Division, Gunned Wood Road, Stevenage, Hertfordshire. **WW 333 for further details**

Waveform Source

A waveform signal source which may be used in applications such as calibrating or evaluating oscilloscopes, measuring frequency response characteristics of voltimeters, measuring characteristics of low-pass filters etc. is announced by Britec Ltd. This is the Preston X-Mod 135 which provides three switch-selected waveforms: sine, triangle and square. Frequency is variable from 0.001 Hz to 10kHz in seven decades and output impedance is 50 Ω . Output voltages are calibrated and range from 2mV to 10V peak via a 12-way switch and a 20:1 vernier control. Sinewave distortion is less than 1%, triangle linearity less than

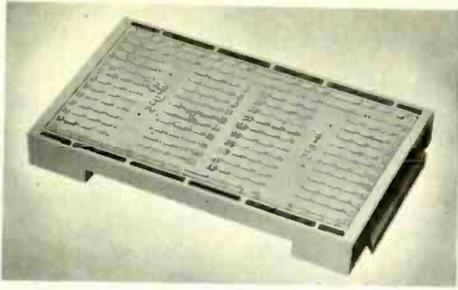


0.5% and squarewave rise and fall time less than 1 μ s. Construction is all-silicon with plug-in printed circuit boards. Price: £209 plus import duty. Britec Ltd., 17 Charing Cross Road, London, W.C.2.

WW 313 for further details

Solderless Breadboards

Latest extension to the range of solderless breadboard systems by S.D.C. Products, are boards designed to accommodate integrated circuits as well as discrete components and to have an increased capacity of 208 contacts per board. One type (called μ DeC) is intended primarily for i.c.s and can accommodate two 16-lead d.i.l. or four 10-lead TO5 packages. The other type (called T-DeC) is for discrete components and can also accommodate one d.i.l. or two TO5 packages. The layout consists of two panels of parallel rows of electrically linked contacts spaced at 5mm which enables short lead devices to be inserted directly into the boards. The new boards may be interlocked to give an area of any desired size and each has slots to accommodate two control panels. Both types of board are supplied



in two packs. A single pack at £2 10s (£2.50) for T-DeC and £2 15s (£2.75) for μ -DeC contains one board, one control panel (with bushes for reducing the diameter of drilled holes in the panel) and a jig (for pre-forming components). A six-board pack contains six boards, six control panels, sets of bushes and jigs, fifty 1mm plugs and eight links for joining power rails in neighbouring boards. These cost £15 for the T-DeC and £16 10s (£16.50) for the μ -DeC. S.D.C. Products (Electronics) Ltd., The Corn Exchange, Chelmsford, Essex.
WW 334 for further details

General Purpose Op. Amp.

Type F1-8 operational amplifier, just added to the Comtec range, features an f.e.t. input. It is epoxy encapsulated in a shell measuring 31.8 × 31.8 × 15.2mm and has standard 7-pin configuration on 5.1mm centres. Operating from $\pm 15V$ supplies, the F1-8 has an input current of 50pA, an open loop gain of 80,000 and an output swing of $\pm 10mA$ at up to 50kHz. Protection is provided against supply reversal and short-circuit of any terminals. Computing Techniques Ltd., Westminster Bank Chambers, Bridge Street, Leatherhead, Surrey.
WW 335 for further details.

Edge Connector

Designed for use with standard 1.6mm thick printed circuit boards having a contact pitch of 0.38mm a new edge connector is announced by Mullard. The bifurcated contacts ensure low circuit resistance and good reliability even when used in conjunction with misaligned or warped boards. Reliability is further enhanced by a heavy gold-plated finish over the whole of the contact spring. The connector, type 036, is available with up to 45 contacts for single-sided or 90 contacts for double-sided boards. The body moulding, of black synthetic resin, is designed so that a connector can easily be cut into shorter lengths for experimental purposes. The loose fixing feet simply clip on the ends of the connector body. Mullard Ltd., Torrington Place, London W.C.1.

WW 336 for further details

Digital Voltmeter

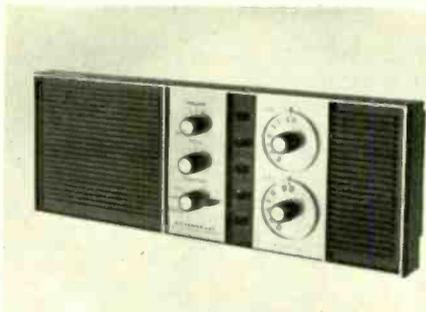
A compact digital voltmeter employing t.t.l. integrated circuits, an f.e.t. input amplifier and quartz crystal clock is announced by Verus Electronics. It is the company's type DC4500 and it features data output, isolated input, remote control and command



ranging. Storage circuitry incorporated into the drive to the neon display tubes ensures a non-flickering display. Decimal point indicators are positioned by the range switch. Readings may be initiated externally, manually or internally at rates up to 20 readings per second. Polarity and magnitude of the input are determined in one measurement, using a single zener reference source. Overload is indicated by a full-scale reading of 4999 with correct polarity indication, the accuracy of subsequent readings being unimpaired. Measurements from 0.1mV to 499.9V d.c. in four ranges are possible with an accuracy of 0.1% and resolution of 0.02%. Input impedance is 10 Ω on all ranges. The instrument measures 228 × 120 × 254mm and weighs 4kg. Price £347. Verus Electronics Ltd., 122-124 Charing Cross Road, London W.C.2.
WW 329 for further details

Small Sound-system

A radio/intercom system kit by Emerson-Rittenhouse comprises a master station (illustrated) with a.m./f.m. radio, three indoor remote stations, and an outdoor remote station, plus an installation kit of 36m of 5-core cable, plaster frame, power transformer, and a.m. and f.m. aerials. The equipment provides two-way communication from any position and it will relay radio programmes, tapes or records. It also enables the door or telephone to be answered remotely. The door-bell push overrides



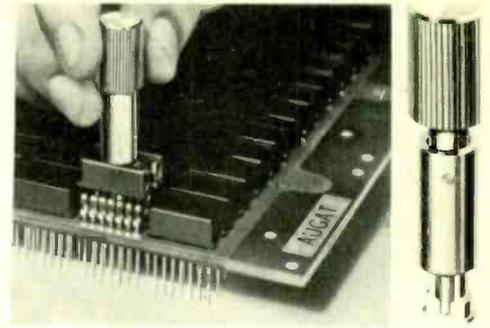
any service in operation with an optional electronic chime. The system is transistorized and can be extended up to a maximum of eight remote stations. U.K. agent: Van den Bosch Ltd., Euro-pair House, Alexandra Road, London S.W.19.
WW 325 for further details

F.E.T. Pairs with S-clip

Matched pairs of field effect transistors type BFS21 and BFS21A from Mullard are now supplied with a new-style "temperature equalizer". This is an S-shaped clip with thermal characteristics similar to those of the rectangular heatsink previously supplied. However, as the transistors in the clip can be easily removed or re-orientated, the new S-clip makes possible greater flexibility in circuit layout. The matched f.e.t.s in each pair have an extremely high input impedance ($10^9 \Omega$), low feedback capacitance (0.75pF), and a very low noise voltage (7.5nV at 10kHz with bandwidth of 5Hz). When in the clip, the transistors are maintained at the same temperature and the differences between their gate-to-source voltages do not change with changing temperature by more than 75 $\mu V/deg C$ (type BFS21) or 150 $\mu V/deg C$ (type BFS21A). Mullard Ltd., Torrington Place, London W.C.1.
WW 326 for further details

I.C. Accessories

Two Augat i.c. accessories being marketed in the U.K. by Electrosil are an i.c. breadboard and test panel, and a socket removal tool. The 8130 series breadboard is for dual-in-line i.c.s and takes up to 50 packages. Solderless interconnection is used



throughout and sockets have large contoured entry holes for easy i.c. insertion. Wiping gold-plated contacts are employed. The removal tool enables socket bodies to be withdrawn from the breadboard panel in order to replace damaged or broken wire wrap contacts. The tool lifts the socket body from the board, and when the damaged contact is replaced, the body can be pressed back into place. Electrosil Ltd., Pallion, Sunderland, Co. Durham.

WW 331 for further details

High Value Capacitors

Sprague announce an extension to their range of 36D "Powerlytic" capacitors in a 76mm diameter × 220mm long can which, they say, gives the highest C/V product available in a single electrolytic capacitor. Values available in this can size range from 650,000 μF at 3V d.c. working with a maximum e.s.r. of 0.0120 Ω and maximum ripple current at 120Hz and 65°C of 26.7A, to 15,000 μF at 150V d.c. working with a maximum e.s.r. of 0.0240 Ω at a maximum ripple current at 120Hz at 65°C of 18.9A. Sprague Electric (U.K.) Ltd., Trident House, Station Road, Hayes, Middlesex.
WW 318 for further details

I.C. Voltage Regulators

Motorola i.c. voltage regulators in a TO-66 package delivering up to 500mA without the use of external power transistors are announced by Celdis Ltd. Using a single external power transistor, the load current can be boosted to more than 10A. Electronic "shut-down" and output short-circuit protection features are built-in. Input regulation is of the order of 0.002%/ V_{IN} and published data sheets specify output impedance. The TO-66 encapsulation has a 10-W power dissipation up to 65°C. Three types available are MC1460G, MC1460R and MC1560G, priced at £2 8s 3d (£2.41), £3 2s (£3.10) and £10 6s 6d (£10.32 $\frac{1}{2}$) respectively. U.K. agent: Celdis Ltd., 43/45 Milford Road, Reading, Berkshire.
WW 314 for further details

Digital Picoammeter

A digital picoammeter by Keithley Instruments, model 445, measures currents over nine ranges from $10^{-9}A$ full scale to $10^{-2}A$ with a resolution of $10^{-12}A$. It features automatic polarity and overload indication and overload protection up to 1000V. Range selection can be manual or automatic. The circuit uses an f.e.t. input followed by a differential transistor amplifier stage and a transistor output stage. The analogue-to-digital converter is a dual-slope integrating

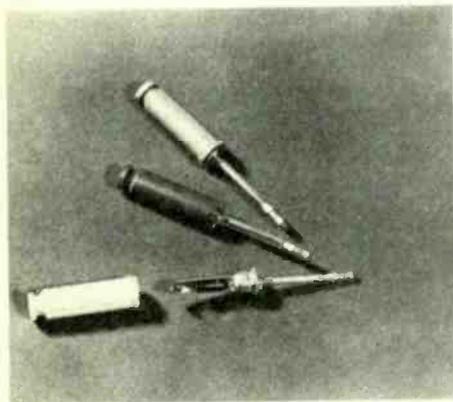


type composed mainly of integrated circuits. Line frequency rejection is 60dB with filter out; 100dB on the 10^{-9} to 10^{-7} A ranges with filter in. Common-mode rejection is such that a 100V d.c. or peak 60Hz a.c. signal will not affect the reading. Time stability is better than 0.5% of full scale per week and temperature stability is better than 0.05% of full scale per deg C. Offset current is less than 10^{-13} A. Display rate may be adjusted from 24 readings per second to one reading per 10 seconds. Isolation of circuit earth from chassis earth is greater than $10^6\Omega$ shunted by 0.02iF. Circuit earth may be floated up to ± 100 V with respect to chassis earth. Accuracy is from ± 0.5 to $\pm 0.2\%$ over the full measurement range. Power requirements are 105-125V or 210-250V a.c. in 50Hz or 60Hz versions, and dimensions are $130 \times 482 \times 254$ mm. U.S. price \$1495. U.K. office: Keithly Instruments Ltd., P.O. Box 43, Reading, Berkshire.

WW 308 for further details

Programme-pin With Integral Diode

Although programming pins are available with provision for wiring-in the diode, Sealectro has now produced a component holder programme pin



which incorporates an integral diode, type 1S920. The diode is rated at 50V p.i.v., 200mA and is connected with cathode-to-tip polarity. A silver-plated stem minimizes contact resistance. Sealectro Ltd., Farlington, Portsmouth, Hants.

WW 311 for further details

Audio Equalizer

Full compensation in broadcast audio channels comprising treble and bass boost and cut together with mid-lift and cut at four spot frequencies is provided by EQ Series equalizers from Elcom. The transistor amplifier which has unity voltage gain is accessible for service on a hinged p.c. board. Input and output impedances are 600Ω unbalanced and output level is $+15$ dBm maximum. Frequency characteristics are as follows: flat position ± 1 dB 30Hz - 20kHz; presence ± 10 dB in 2dB steps at 1.4, 2.8, 4.0 and 5.6kHz; treble -15 dB to $+12$ dB in 3dB steps; bass -15 dB to $+12$ dB in 3dB steps. Noise is -90 dBm and distortion ranges from 0.03% at 0dBm output to 0.3% at $+15$ dBm. Operating voltage required is 24V or 50V at 20mA. The equalizer front panel measures 177×62 mm and it is 190mm deep. Elcom (Northampton) Ltd., Weedon Road Industrial Estate, Northampton.

WW 328 for further details

Digital Tacho-ratiometers

Orbit 70 range of digital tacho-ratiometers by Orbit Controls of Cheltenham comprises a number of twin-channel frequency measuring instruments



with the added facility of measuring and displaying digitally the ratio between two speeds being measured as well as the absolute speeds. Instruments may be 4, 5 or 6 decade with timebase fixed at either 1 or 10 seconds, or with the timebase variable in 1ms steps from zero to 9.9995, allowing the display to be normalized to standard units (r.p.m., ft/sec., etc.). A counting rate of up to 10^6 seconds is possible. Input signals can be taken from any sensor which provides a pulse train of recurrent frequency bearing a direct relationship to the parameters being measured. Suitable sensors, including magnetic pick-offs, photo-electric detectors and photo-electronic tacho-generators are available from the makers. A b.c.d. output can be provided for control purposes or for the operation of printers or data-loggers. Orbit Controls Ltd., P.O. Box 16, The Runnings, Cheltenham, Glos. GL51 9PL.

WW 312 for further details

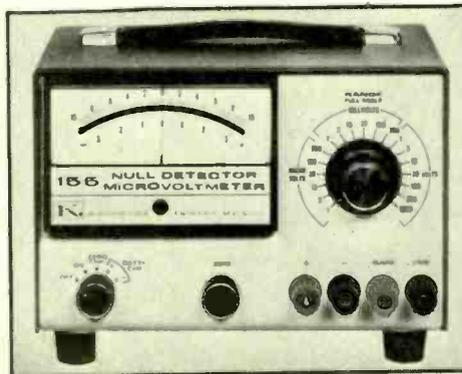
Thick-film D.C. Voltage Regulators

A comprehensive range of thick-film standard circuits has been introduced by Morganite Resistors Ltd. This range includes compatible positive and negative d.c. voltage regulators with output voltages from 3 to 32V. Built-in short-circuit protection and output voltage are adjustable by the addition of external resistors. The units have an operating temperature range from -55° to $+125^\circ$ C with a maximum load capability of 500mA, and a load regulation of $\pm 0.05\%$. Only $25.4 \times 12.7 \times 4.3$ mm high, these units are manufactured using cermet thick-film passive elements fused to an alumina substrate, chip semiconductors are bonded to the substrates and attached to the passive elements by thermo-compression gold lead bonding. The addition of an alumina cover seals the unit. Regulators with a voltage range of 5 to 28 volts, load capability of 750mA and load regulation of 0.003%/mA are also available. Morganite Resistors Ltd., Bede Industrial Estate, Jarrow, Co.Durham.

WW 330 for further details

Null Detector/Microvoltmeter

Sensitivity from 1μ V to 1000V full scale is the main feature of null detector/microvoltmeter

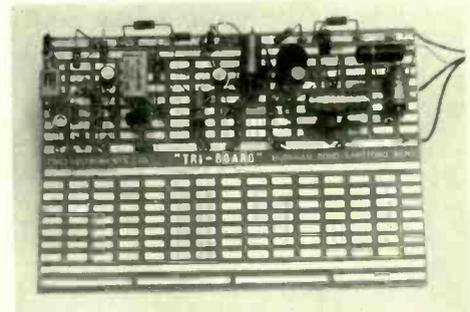


announced by Keithly Instruments, of Ohio, U.S.A. The new transistor instrument, model 155, is battery operated. Input impedance varies from $1M\Omega$ on the most sensitive range to $100M\Omega$ and the makers add that there is "excellent immunity" from a.c. interference. An m.o.s. f.e.t. chopper is employed in the input circuit to provide good zero stability. Accuracy is $\pm 1\%$ of full scale at recorder output, 2% of full scale at the meter. Recorder output is ± 1 V at up to 1mA. An overload feature allows up to 1200V to be momentarily applied to any range. Normal mode rejection is such that an applied 50-60Hz signal 80dB greater than full scale peak-to-peak will not affect the reading. A common mode voltage 120dB greater than full scale will not affect the reading. Operating power is derived from four internally mounted zinc-carbon batteries and a power unit accessory is available which permits operation from a.c. mains supplies. Model 155 measures $133 \times 210 \times 170$ mm and weighs 2.7kg. Price \$325. U.K. office: Keithly Instruments Ltd., P.O. Box 43, Greysfriars Road, Reading, Berkshire.

WW 304 for further details

Designer's P.C. Board

Rapid construction of circuits at the design and prototype stages of development is provided by the "Tri-board" breadboard comprising a copper-clad laminate, etched to leave rectangular lands of copper. Four continuous strips running the length of the board can be used as power supply and earth busbars and large strips at each edge serve for termination of input and output leads. Supplies are in glass fibre and s.r.b.p. laminates in grades suitable for cold punching or cutting.



Board size is 190×140 mm, 1.6mm thick with 28g copper. Roller tinned finish is standard. The makers claim that the Tri-board may be used over and over again. Price: 15s (75p) in glass fibre, 9s 6d (47½p) in s.r.b.p. laminate. Tri Instruments Ltd., "Allington", Dartford Road, Farningham, Kent.

WW 301 for further details

Avalanche Diode Sources

Available over the frequency range 5 - 18GHz, new avalanche diode sources by Interplanetic contain built-in solid-state current control circuit which require a 90V power supply and exhibit an effective source resistance of $50k\Omega$. Additional power drain on the supply is typically 250mW. The benefits of current control are improved amplitude and frequency stability with variations in power supply, protection against reverse polarity and over voltage plus a reduction in incidental a. m. and power output uniformity from unit to unit. An adjustment is provided to change the power output over a moderate range without changing the supply voltage, the resultant frequency change being typically 5MHz/mA. Centre frequency setting hold to within 0.5% over the temperature range -40° to $+70^\circ$ C and second harmonic output in the 20-GHz region is typically 40dB down. Interplanetic, 39-49 Cowleaze Road, Kingston-upon-Thames, Surrey.

WW 332 for further details



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Unitor Pattern 103 DEF-5325-1 reporting for heavy duty!

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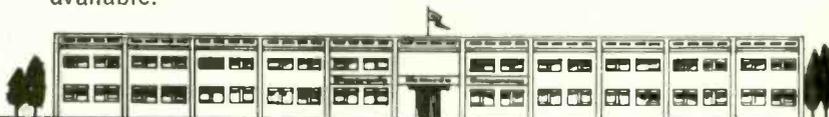
Member of the Louis Newmark Group,
 with access to the combined facilities
 of all other member companies.

Ministry Approval Certificate 1693 was the honour earned by McMURDO Unitor Pattern 103 – the toughened version of the universally trusted Micronector.

With specially treated contacts and D.A.P. moulding the Unitor is ready to do battle with extremes of environmental conditions.

It is polarised for simple, trouble-free connection and is available with a range of covers and masks similar to those supplied for the Micronector range. The full range of 7, 14, 26, 34, and 50-pole versions of the new Ministry of Defence approved Unitor connector are available.

Send for data sheet and further information to:
 The McMURDO Instrument Co. Ltd.
 Rodney Road, Portsmouth, Hants.
 Telephone 35361 Telex 86112



Authorised Stockists: -LUGTON & CO.LTD., 209/210 Tottenham Court Road, London W.1. Tel: Museum 3261. SASCO, P.O. Box No. 20, Gatwick Road, Crawley, Sussex. Tel: Crawley 28700 (also Chipping Sodbury 2641, Cumbernauld 25601 and Hitchin 2242) and agents in principal overseas countries

WW-112 FOR FURTHER DETAILS

TAKE A GOOD LOOK

The Cossor CDU 150 Joint Services CT 531



£470

CDU 150 is a fully transistorised general purpose versatile oscilloscope with many advanced features and extremely high engineering quality.

- **Bandwidth DC – 35 MHz at 5 mV/cm – Dual Channel.**
- **Large (8 x 10cm), bright display.**
- **Measuring accuracy $\pm 3\%$ 'X' and 'Y' all ranges.**
- **Full delayed timebase facilities with gated mode.**
- **Compact, rugged, lightweight.**

The Cossor CDU 150 has been selected, in open competition, from a wide range of commercial oscilloscopes by the Joint Departmental Radio and Electronics Measurements Committee to be the general purpose oscilloscope for use by the British Armed Forces and associated Ministry Departments. The CDU 150 satisfied the exacting requirements of this committee in respect of electrical performance, construction, and ease of operation and maintenance.

Take a good look at the Cossor CDU 150 – send for comprehensive literature.

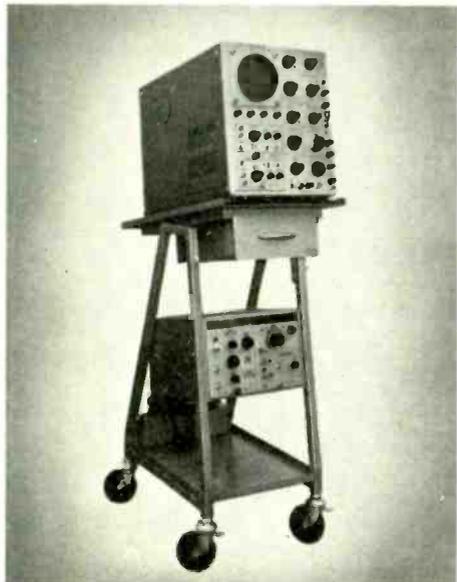
COSSOR

Cossor Electronics Limited, Cossor Instruments (Industrial Products Group)
The Pinnacles, Elizabeth Way, Harlow, Essex, England
Telephone: Harlow 26862 Cables: Cossor Harlow England Telex: 81228

WW-113 FOR FURTHER DETAILS

Oscilloscope Trolley

An instrument trolley made in a variety of versions to suit almost every known make of oscilloscope is announced by Avoncel. It costs £25 and can be ordered by simply stating the make and model number of the oscilloscope for which it is required. Of welded construction, the framework (25.4 x 25.4 mm) is of 14 gauge mild steel with 14 and 16



gauge mild steel shelves. Good stability is claimed with 113kg load. Features include a fail-safe top shelf adjustment which enables the viewing angle to be adjusted from 0-20°. Both top and bottom shelves have lipped edges and the top shelf is fitted with adjustable back stops. Four-inch swivel castors are fitted; the two front castors are equipped with brakes. A four-way 13A power distribution box is fitted. Avon Communications and Electronics Ltd., 318 Bournemouth (Hurn) Airport, Christchurch, Hampshire.

WW316 for further details

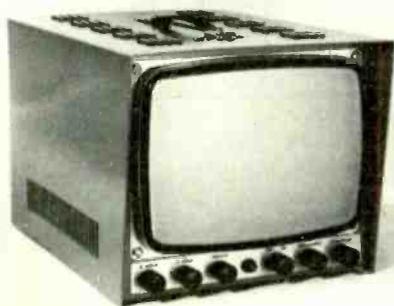
Transient Voltage Suppressors

Two new types, designated the KSA and KSL series, have been added to the range of Klip-Sel transient voltage suppressors by International Rectifier. These units are designed to give protection to electrical equipment and systems which are subject to voltage transients and the new series utilizes a new type of selenium plate offering improved reliability and reduced steady state power loss. International Rectifier, Hurst Green, Oxted, Surrey.

WW319 for further details

11-in Television Monitor

Picture monitors for use in industrial and educational television systems have been introduced by E.C. & S. of Newark. They are models 11T and 11T/S and are especially suitable for mobile duties because of their compactness, light weight

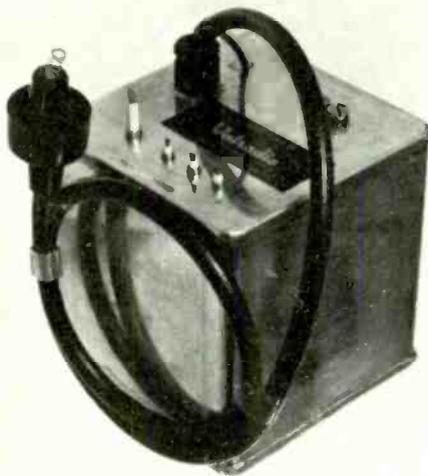


and mechanical rigidity. Silicon transistors are employed throughout and an 11-in ringguard c.r.t. Construction is of four printed circuit panels with heavy components mounted on the unit chassis. Both composite and non-composite video signals will be accepted and these may be bridged or terminated by the operation of toggle switches on the rear panel. Model 11T/S may be fitted with an additional optional circuit module producing random mixed syncs, which are fed from the monitor via a coaxial connector on the rear panel. This facility allows the outputs from several cameras to be fed into a singled monitor via a video switching unit without incorporating an independent synchronizing pulse generator. The random mixed syncs with frame pulses locked to the mains may be used to lock the associated cameras, providing stable displays on camera switching. Prices: £195 (11T) and £205 (11T/S). Electronic Control and Surveillance Ltd., Queens Head Court, Newark-upon-Trent, Notts.

WW 302 for further details

25kV E.H.T. Unit

An e.h.t. unit suitable for providing the 25kV e.h.t. supply to most projection television receivers and for conventional shadowmask tubes when separate circuits are used for line deflection and e.h.t. is announced by Valradio. The circuit recommended for use in conjunction with the e.h.t. unit includes a feedback regulator to provide zero output impedance between no load and the maximum current of 350 μ A. The 25kV is smoothed

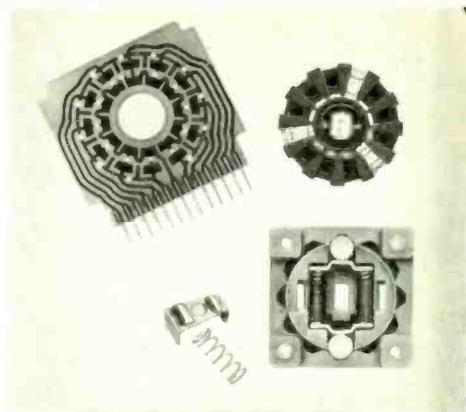


and fed via a 700mm screened cable to an outlet plug to fit Mullard c.r.t. type MW2. Power supply requirement is 350V at up to 70mA at an effective impedance of 400-600 Ω . Size of the e.h.t. can is 107 x 107mm with an overall height of 127mm including the top connections. Valradio Ltd., Browells Lane, Feltham, Middlesex.

WW 305 for further details

Flexible Switch Innovation

Described by Plessey as a "new concept in rotary switch techniques" their new PrintSwitch features a unique printed pattern which enables any contact configuration to be obtained by removal of unwanted inter-connections. Shorting or non-shortng contacts on a single pole can easily be arranged. To this has been added better standards of reliability by the elimination of contact alignment problems associated with conventional clipped wafer switches. The PrintSwitch uses a printed epoxy glass stator assembly and rotor contact pressure is obtained from low-rate coil springs. Dual-compression springs and rollers are used for indexing. All con-



nections are provided in a single plane at standard pitch so that direct insertion into a printed board is possible. Metric spindles and bushes are standard and the usual facilities such as concentric shafts are also available. Professional Components Division, Plessey Components Group, Titchfield, Hampshire.

WW380 for further details

Tunnel Diodes

New miniature tunnel diodes announced by Mullard have a switching time of one nanosecond and are primarily intended for use in the switching circuits associated with ferrite-core memories. The diodes, type AEY25 and AEY26, are in DO-17 encapsulations that are only 2.54mm long and 2.8mm in diameter—small enough to be mounted around the edge of the matrix plane. Consequently, very short connecting leads can be used and high operating speeds are achieved. Operating characteristics are: maximum forward current 50mA; typical peak current 4.7mA (AEY25), 5mA (AEY26); peak voltage 75mV; and valley voltage 330mV. Ratio of peak current to valley current (I_p/I_v) is typically 6. Mullard Ltd., Torrington Place, London, W.C.1.

WW381 for further details

Broadband Miniature Amplifier

A new low-noise transistor amplifier by Electro/Data Inc., U.S.A., covers the entire v.h.f. and u.h.f. frequency bands and is contained in a shielded package no larger than a normal coaxial connector with 7-mm input and output plug-and-socket features. It has input and output impedances of 50 Ω (nominal) and requires only a single negative 18V, 20mA d.c. power source. The amplifier, model A10, has a 10dB gain response from 20-1000MHz and greater than 18dB from 50-850MHz. Increased gain can be obtained by cascading two or more units. Noise figure is 4dB (typical), 5dB (max). Weight of the unit is 21g and the price for single quantity \$300. Electro/Data Inc., 3121 Benton Street, Garland, Texas 75040, U.S.A.

WW315 for further details



Letter from America

Here is a success story that is worth recording. Back in 1939, two electronics engineers decided to go into business for themselves and so they began in a garage with a total capital of about \$500 (then worth about £120). At first they made a few diverse and exotic products but then moved into the instrument business with an audio generator. This was an RC device and eight of these instruments were used by the Disney studios for sound effects in the famous "Fantasia" film. Soon the garage became too small as more and more instruments were added to the range. Such was the phenomenal rate of expansion that by 1956 annual sales had sky-rocketed to \$20 million, reaching the incredible figure of \$200 million by 1966 and \$265 million last year. As you have probably guessed, the two engineers are William Hewlett and Dave Packard. The firm now employs over 13,000 workers all over the world and Dave Packard is now Deputy Secretary of Defense in the Nixon Administration. This appointment has met with some criticism on the basis of HP's large business deals with the U.S. Government. Although Dave Packard has resigned from the company and placed his \$300 million stock in a charitable trust the critics say could he really be impartial to his own firm even if he sold all his stock? On the other hand, his supporters argue that the government should not be denied the services of so talented and experienced an executive just because he is successful!

There are now nearly 20 million American households with colour TV—something like 33% of the total. Sales of colour receivers increased more than 10% in 1968 to 5,771,000 of which 800,000 were imported from Japan. The import situation is even worse in Canada where the influx of Japanese receivers increased from 3.7% in 1965 to more than 25% at present. The president of the Canadian Electronic Industries Association said recently that no less than 56% of all TV sets with 19-inch screens or smaller are imported from Japan. About 190,000 colour sets were sold in Canada last year and the 1969 forecasts are up to 250,000.

Curiously enough, varactor diodes are not used as tuning elements in American television sets. This is in sharp contrast to European practice: if I remember correctly Grundig used them as far back as 1965. The reason is mainly due to technical difficulties

arising from the large number of channels involved. Manufacturers must provide a choice of 12 channels in the v.h.f. band plus another six in the u.h.f. range. So selectivity becomes a problem and there is the added cost of the switches to contend with.

Infra-red systems for night vision (Snooperscopes!) were used in World War II and I believe some are still employed in Vietnam. Now a much better method has been devised using lasers. The complete system comprises a laser diode, optical assembly, infra-red tube, modulator and delay circuitry and a 28-volt battery. Coherent light from the gallium arsenide laser is pulsed to the target and the tube is cut-off until the ray returns to prevent ambient light from entering. The reflected pulse switches the tube on and the viewer sees the target image on the lens. To see moving objects the instrument can be switched to a d.c. mode and then when once located the object can be watched with greater definition by reverting to the pulse mode. Range is said to be up to 300 feet and the weight of the whole outfit is 15 lb. It is priced at \$3,000 (£1,250) and the maker is Laser Diode Laboratories, Inc.

Westinghouse have developed a TV pick-up tube which if not capable of seeing in the dark, will certainly operate with extremely low illumination. It uses the principle of secondary emission (s.e.c.) and has a rated sensitivity of 20,000 microamps per lumen. They are used in the colour cameras for medical purposes, electron microscopes, and industrial and military applications where a good resolution under low lighting conditions is required.

General Telephone & Electronics Corporation are also working with lasers and they disclosed recently that they had evolved what they termed a "technological breakthrough" in the use of lasers for large-screen colour TV. Picture sizes up to 48 by 31 inches have been achieved although it was emphasized that the system is still very much an experimental one. The system uses two lasers to produce three laser beams. A krypton gas laser provides red light and an argon laser gives blue and green light. The beams pass through electro-optical modulating equipment where signals from a standard colour receiver are impressed on them. An arrangement of mirrors then combines the three beams into a multicolour beam which travels to a prism that splits it into a pair of similar full-colour beams. The two full-

colour beams are then directed by mirrors to a rotating 15-sided mirror which scans them in rapid succession, producing the horizontal lines needed for a TV picture. The scanned beams are then reflected to a vibrating mirror that produces vertical motion. From there the light rays are reflected to a large screen where the picture is produced.

Ultrasonics are used for all kinds of things these days and recently I came across ultrasonic bird repellers. These are made by a firm rejoicing in the name Bird-X of Chicago and work in the 20-kHz range. One model uses a transistor oscillator and the other is operated by compressed air with focusing reflectors.

The 59th annual Boat Show held recently in New York attracted a very large attendance and exhibitors were very optimistic about the future. With good reason—sales now top \$15,000 million and there are now more than 8 million boat owners in the U.S. Electronic devices were well in evidence and one of the most interesting was a "wrist range finder" made by Hartmann. This gadget is a micro-miniature depth sounder worn like a wrist watch for skin divers. It has a range of 360 feet and has been tested to withstand submersion to 220 feet. The device can tell the wearer the distance to the bottom, to the surface, to underwater obstructions or to other swimmers. The price? \$129.99 (say £50). Dozens of radio telephones were to be seen but here the situation is complicated by an F.C.C. regulation which states that January 1971 is the latest date for the installation of a.m. transmitters using the 2-3 MHz marine band.

However, sales of the new more expensive f.m. units have been relatively slow and the actual figures show less than 200 f.m. units out of a total number of some 167,000. One of the reasons might be due to some confusion over F.C.C. cut-off dates and also whether amplitude modulated s.s.b. will be permitted. This state of affairs is not entirely due to F.C.C. vacillations but rather to the necessity of co-ordinating with the requirements of the International Telecommunication Union. The manager of Raytheon Marine Product Division said that sales of v.h.f./f.m. radio telephones have yet to capture a mass market because of their higher price and to an understandable inertia on the part of the general public until definite time schedules are announced by the F.C.C. He went on to say that he expected that the final date for the use of a.m. radio telephones except those employing s.s.b. would be 1977 after which only v.h.f./f.m. equipment could be used.

Radar may well be standard equipment on millionaires' yachts, but it is still a luxury item for most boat owners, nevertheless, prices are coming down. For example Kelvin Hughes had a radar system at less than \$2,700 (£1,100) and small boat systems were also shown by Decca and Astaron Birc. Some of the larger, expensive boats were not only equipped with the latest navigation aids but boasted wall-to-wall carpeting, TV stereo and a full complement of washing machines, dishwashers, and other gadgets in the galley—sorry—kitchen! About the only thing missing were Bird-X devices to keep the sea-gulls off!

G. W. TILLET

Public Address Equipment

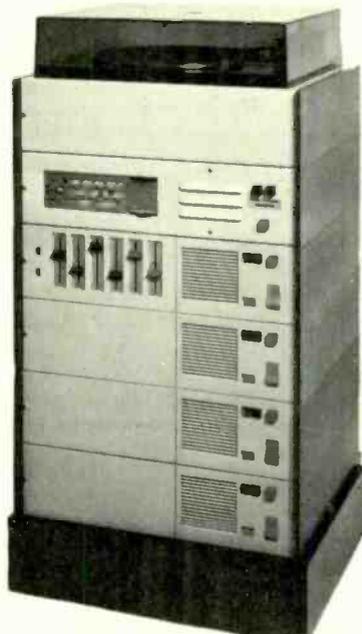
The A.P.A.E's Coming-of-age Show at Harrow

This small but exclusive annual exhibition of public address equipment, arranged under the auspices of the Association of Public Address Engineers, was again held at the King's Head Hotel, Harrow, from March 11th to 13th. This year's show marked the Association's 21st anniversary. The exhibition of equipment which ranged from large custom-built desk console systems to handy personal p.a. kits was supported by a series of lectures giving to the show an atmosphere of an annual swapping of ideas. Transistors and printed circuits have enabled the modular type of construction to be employed almost invariably in new equipment so that versatile installations can be achieved using a minimum of components by exchanging only the significant section of the total circuit. Because of the arduous conditions in which p.a. equipment is expected to operate, most of the housings are robustly constructed, and in some cases speakers were proofed against corrosion and even against flame. Public address work, mobile p.a. in particular, can be an untidy business requiring the plugging and unplugging of ancillary units between installations and "hooking-up" a variety of configurations of microphone and music inputs, speaker outputs and so on, to satisfy the requirements of individual functions. Most manufacturers have commendably adopted the DIN specification for their inputs and outputs but the p.a. equipment handler may be tempted to question the ability of the DIN-type plug and socket to withstand the inevitable rough handling it will receive.

One welcomed innovation at this year's show was the introduction by the A.P.A.E. of a 45 r.p.m. test disc costing 15s (75p). This is the first time that a facility of this sort has been available to the p.a. engineer and with it he can apply a more professional touch to the testing of his installation. Instead of the "one, two, three . . . testing", kind of exercise the installer will simply start the test record then check his equipment for volume levels, speaker phasing, and correct functioning generally. The first side of the record contains three minutes of male speech ending with 30 seconds of talking away from the mic, followed by three minutes of female speech. The second side contains selected test phrases followed by a 1-kHz tone, a warble tone, and pink and white noise.

Of the equipment being shown, the largest

display was a sophisticated desk console by Audix which, although appearing in a standard version, can be varied to accommodate different combinations of sound and control equipment. Consoles are normally custom designed and are intended for lecture theatres, concert halls and the like. Combinations include microphones, tape recorders, gram turntables and radio tuners with the usual level controls on each channel, output metering and circuit switching. The output is suitable for feeding via G.P.O. lines to remote power amplifier and speaker distribution networks. At the other end of the scale there was what might be described as a one-man public address system, the Bouyer Clubflex 201. This is a French import shown by D. A. Lyons and Associates. It comprises a collapsible microphone stand to which is clamped a quadruple unit column-type loudspeaker and reading lectern. The speaker unit contains a 5-W amplifier and eight U2 batteries. The equipment features a dynamic hand microphone which can be removed from the stand and has a reasonable length of connecting cable to allow the talker to move about if required. The Clubflex 201 weighs 3.9kg and costs 64gn (£67.20). Ultra Electronics Ltd. were



Philips stack-unit p.a. assembly

featuring their TAM25 and TAM50 amplifiers which are basically power output stages of 25- and 50-W rating respectively. The amplifiers are designed with a separate section on the chassis containing just six edge connectors for the insertion of plug-in p.c. boards. Individual boards are available for microphones, radio, records, tape, etc., thus enabling the role of the installation to be changed quickly. A further six inputs could be added to the system by means of a separate audio mixer. One permutation of modular assembly is simply to stack units one on top of the other as required, a method favoured by the Philips Division of Pye TVT. The cases are designed to fit one on to the other in building-brick fashion and thus, using three basic amplifiers of 25-, 50- and 100-W output and three types of preamplifier, nine different combinations are possible. For future extension additional units can be added to the stack including a radio tuner, record player, tape recorder or signal switching unit.

Microphones to be seen at the show were many and varied but there was a handful of new types. There was, for instance a Reslo dynamic microphone type SL1 in the high-quality bracket at a cost of £38. It has a frequency response of 100-16000Hz and sensitivity 84dB below 1V/dyne/cm². Available in low- or medium impedance versions, response is omni-directional.

Another new range of microphones was the Series 4 by Lustraphone. Of these the 4-10 and 4-11 are respectively desk and lavalier type using the same microphone head. Frequency response is substantially flat from 200 Hz to 11kHz with an omni-directional pick-up pattern. Output level is -86dB at 50Ω at 1kHz (0dB = 1V/dyne/cm²); high- and low-impedance versions are available. No dramatic developments were to be seen in loudspeaker design but one feature worthy of mention is the use of glass fibre for the construction of re-entrant horns in place of metal. This material is used in the construction of Rola Celestion's model FG and it makes the speaker impervious to salt air on boat decks or chemical atmosphere in some industrial plants. Rola Celestion is not the first speaker manufacturer to use glass fibre construction but it does no harm to be reminded that the electronics industry generally, probably more than any other industry, takes every opportunity to exploit the benefits offered by new materials.

An important aid to audio engineers, particularly in locations where high ambient noise is troublesome, is a new portable sound level meter (model SLM3) by Acos. The SLM3 complies with BS 4142, making it suitable for the measurement of industrial noise nuisance and BS 3425 for measurement of vehicle noise, so that its use could widen the scope of p.a. dealers' activities. Fast and slow meter damping facilities are provided (peak and average levels) and an output socket enables the meter to be connected to a pen recorder. The sound level meter comes in an attache case kit which includes accessories to extend the range and scope of the basic instrument, comprising an amplifier module, calibrator unit, wind-shield, comparator unit (for differential measurements), tripod and extension lead.

Test Your Knowledge

Series devised by L. Ibbotson* B.Sc., A.Inst.P., M.I.E.E., M.I.E.R.E.

12. Acoustics

- At a point in free air carrying a plane travelling sound wave the excess pressure variation with time is observed to be sinusoidal. The particle velocity at this point will
 - be constant
 - be constant in magnitude, but change in direction when the excess pressure changes sign
 - vary sinusoidally with time in phase with the pressure
 - vary sinusoidally with time in phase quadrature with the pressure.
- The velocity of an audible sound in free air depends on
 - the total air pressure
 - the absolute temperature
 - the frequency
 - the intensity.
- A sound source moves towards and away from the observer in a cyclic manner. The observed frequency
 - is unaffected
 - is increased
 - is decreased
 - rises and falls cyclically.
- The overtones produced by a closed organ pipe are
 - inharmonic
 - all harmonics of the fundamental
 - odd harmonics of the fundamental
 - even harmonics of the fundamental.
- On a piano (tuned in equal temperament) middle C is found to have a frequency of 260Hz, the C above it 520Hz. An octave has 12 semitones. The frequency of the note 6 semitones above middle C (F#) will have a frequency
 - $260 \times \frac{3}{2}$ Hz
 - $260 \times \sqrt[6]{12}$ Hz
 - $520 \times \sqrt[12]{6}$ Hz
 - $260 \times \sqrt{2}$ Hz.
- Two pure sound tones, one at 100Hz the other at 1000Hz, sound equally loud. The threshold of audibility is 10^{-12} watt per square metre at 1000Hz, 10^{-9} watt per square metre at 100Hz. The loudness levels of the two signals in phons
 - are the same
 - differ by 3dB
 - are in the ratio 3:1
 - are in the ratio 1000:1.
- The dynamic range of human hearing at frequencies around 1kHz is of the order of
 - 10dB
 - 60dB
 - 130dB
 - 200dB.
- The mechanical response of the moving parts of a loudspeaker or microphone can conveniently be analysed using methods which are analogous to those of electric circuit analysis. If force is regarded as analogous to voltage the mechanical analogue of inductance is
 - inertial mass
 - compliance (the reciprocal of stiffness)
 - viscous friction
 - velocity.
- The moving parts of a loudspeaker have at a given frequency a mechanical impedance Z_m . The extra electrical impedance introduced by the motion of these parts (the motional impedance) is
 - directly proportional to Z_m
 - directly proportional to Z_m^2
 - inversely proportional to Z_m
 - inversely proportional to Z_m^2
- The fundamental resonant frequency of a cone loudspeaker should be
 - below the lowest frequency which it is required to radiate
 - in the centre of the range of frequencies which it is designed to radiate
 - above the highest frequency which it is designed to radiate
 - outside the audio range of frequencies.
- A simple cone loudspeaker becomes increasingly ineffective as the frequency of the sound which it is required to radiate increases above a value corresponding to a wavelength equal to the circumference of the cone. Select the factor below which is not relevant
 - the radiation from the cone becomes increasingly directive
 - there is a fall off of total radiated power
 - the cone "breaks up"
 - cancellation can occur between radiation from the two sides of the cone.
- An exponential-horn loaded loudspeaker can give uniformly efficient energy conversion over the whole of the audio frequency range provided the mouth is sufficiently large. The horn must, however, be long because the taper must not be too sharp. The disadvantage of a short horn with a wide mouth is
 - it exhibits resonances at low frequencies
 - it exhibits resonances at high frequencies
 - it has a high cut-off frequency below which no energy is radiated

(d) it has a low cut-off frequency above which no energy is radiated.

- Of the following types of microphone one requires an applied d.c. potential
 - a crystal microphone
 - a capacitor microphone
 - a moving-coil microphone
 - a ribbon microphone.

14. A ribbon microphone and a crystal microphone (both normal of their type) feed amplifiers which are adjusted so that the output is the same from each when the two microphones are exposed to a plane sound wave in free air. Both microphones are placed in a large tube, which supports a total standing wave of sound, at a pressure antinode. The output will be

- very small from both
 - very large from both
 - large from the ribbon microphone, small from the crystal microphone
 - large from the crystal microphone, small from the ribbon microphone.
- The basic polar diagram of a normal ribbon microphone is
 - figure-of-eight at all frequencies
 - omnidirectional at low frequencies; figure-of-eight at high frequencies
 - omnidirectional at high frequencies; figure-of-eight at low frequencies
 - omnidirectional at all frequencies.

16. It is normally accepted that the optimum reverberation time for a small room in which music is to be reproduced should

- be the same for all frequencies
- decrease uniformly with increasing frequency
- decrease with increasing frequency up to about 1kHz and remain constant for all frequencies above this.
- be constant with increasing frequency up to about 1kHz and decrease with increasing frequency above this.

Answers and comments, page 247

"Test Your Knowledge—11"

I must apologize to readers for question 6 of No.11. The answer which I gave is incorrect, and the alternative solutions given in the question are inappropriate.

R.F. amplifiers of the sort shown are generally designed on an impedance matching basis for maximum power transfer. Thus the input impedance of the next stage will be transformed to such a value that it is presented to the transistor as equal to its output impedance (Losses in the coil can generally be neglected). With the usual values of input and output impedances a parallel tuned circuit connected directly across the transistor would require, to give the optimum bandwidth for amplitude-modulated sound reception, values of inductance and capacitance which are inconvenient; the capacitance value required is very large. A smaller value of C can be used if a larger tapped coil is used in the way shown so that the required values of L and C are presented to the transistor. The transformed impedance of the next stage presented to the transistor must still be the same.

If, with a stage designed in this way, the collector connection were moved to point Q on the diagram, the bandwidth would be too wide, not too narrow, as suggested by my answer.

I am indebted to Mr. M. G. Scroggie for drawing my attention to this fact.

*West Ham College of Technology, London, E.15.

World of Amateur Radio

Famous Contact Recalled

A link with perhaps the most famous amateur contact of all time—the first two-way, short-wave, transatlantic contact of November 28, 1923—has been broken with the death on January 21 of Leon Deloy ex-8AB of Nice, France. It was Deloy, more than any other European, who was responsible for starting the rush to shorter wavelengths. In the Spring of 1923 he began experiments on about 100 metres and soon formed the opinion that these wavelengths could “render immense and unsuspected service in long distance work”. During that summer he visited the United States and arranged with Warner, Schnell and Handy of A.R.R.L. to try such wavelengths in the 1923 transatlantic tests. On his return to France Deloy began a long series of tests with E. J. Simmonds, 2OD of Gerrards Cross. In late November, he cabled A.R.R.L. asking them to listen for him on 100-110 metres. Fred Schnell, 1MO, received strong signals from him on November 27, and the following night two-way contact was made with Schnell reporting 8AB's signals as “U ALSO VY QSA TWENTY FEET” indicating that he estimated the signals were strong enough to be heard 20ft from the headphones! Almost immediately contact was also established with John Reinartz, 1XAM, and the historic three-way contact continued for several hours. As news of this success became known, the great rush by other amateurs and many commercial communications organizations to exploit the shortwaves gained momentum.

New Award Stimulates H.F. Activity

The level of DX activity on the main h.f. bands seems to have been stimulated by a new A.R.R.L. “Five Band DX Century Club Award”. This sets amateurs an extremely tough requirement of contacting 100 different countries on each of five h.f. bands: 3.5, 7, 14, 21 and 28 MHz, and only contacts made after January 1, 1969 are counted. Considerable Commonwealth activity was also noted during the annual B.E.R.U. Contest, organized by the R.S.G.B., during early March and held this year under good propagation conditions. Some of the overseas participants were heard giving contact serial numbers well over 500, and the 14 MHz long and short paths to Australia were open for many hours.

In general, however, many British

amateurs have become concerned at the lower level of h.f. activity apparent in this country in recent years, with a high percentage of licensed amateurs now apparently inactive on these bands. This is believed to be due in part to the continued problem of avoiding causing interference to television reception. It is hoped that more activity will be possible by using such techniques as absorptive low-pass filters (with which v.h.f. harmonic energy is separated from the h.f. power by means of cross-over filters and then dissipated in a resistive load) and various forms of ferrite transformers and baluns to reduce entry of fundamental and harmonic power into television receivers along the outer screen of coaxial feeder cables. Firm hope for the future is based on British television “duplication” plans since u.h.f. TV appears appreciably less susceptible to interference than Bands I and III, with Channel 1 notoriously suffering.

Long-distance V.H.F.

A new 144 MHz record is being claimed for a “moonbounce” contact between the Swedish station SM7BAE and New Zealand ZL1AZR. SM7BAE has also worked California on c.w., and has received s.s.b. from K6MYC. During March, the Rhodesian station, ZE1AZC on 50 MHz has been reported for the first time in the U.K., having been heard by G3JVL probably due to trans-equatorial propagation. Several good aurora DX openings on 144 MHz occurred during March. At an R.S.G.B. meeting, C. Newton, G2FKZ, put forward the view that, during aurora openings, longer east-west paths are possible at the beginning and end of such periods, and advised amateurs to continue operation in these conditions to about 02.00. He believes that “afternoon” auroral openings are produced by a different mechanism and do not give rise to such long distances. D. Hayter, G3JHM, predicted that “double hop” paths would be found feasible during sporadic E conditions, and that this could result in contacts between the U.K. and Middle East on 70 MHz. He announced that the Gibraltar beacon station ZB2VHF will soon be transmitting simultaneously on the 50, 70 and 144 MHz bands. Rhodesian 50 MHz beacons have been reported on a number of occasions in Gibraltar, where the South African beacon ZS6VHF has also been received.

Several v.h.f. and u.h.f. contests organized

by R.S.G.B. will be held during May, including 144 MHz portable (May 3-4); 432 MHz open (May 24-25); and 1296 MHz (May 24-25). G3GZL was winner of Section A of the 144 MHz c.w. contest held during January. G3VPK of Chelmsford led the field in the 70 MHz contest held during February. American amateurs recently regained the 2300 MHz record with a 225-mile contact using pulse techniques. Both stations were at about 1500 ft and it is believed the contact was effected by scatter propagation.

Gift to Mauritius Amateurs

The Johnson Viking Ranger II transmitter donated to the Mauritius Amateur Radio Society by the American Radio Relay League was recently handed over to the chairman of the society Paul Caboche (VQ8AD) during an informal ceremony at the United States Embassy. In making the presentation, William B. Hussey, the Chargé d’Affaires, displayed a real interest in the society’s training programme and disclosed his own earlier interest in amateur radio. News has been received that the construction of the transmitter is finished and the first QSO was made on 20 metres c.w. with station K6QPH/4 in South Carolina. It is hoped to install the transmitter in the society’s clubroom and Region 1 of the I.A.R.U. has agreed to give assistance in providing a companion receiver.

Reciprocal Licensing

The current issue of the I.A.R.U. Calendar lists the names of 41 countries and their amateur societies, together with the names of those countries whose amateurs are accorded eligibility for amateur operating privileges when visiting that country. Information is given regarding the address from which forms and assistance in making application may be obtained. In the case of the United Kingdom, reciprocal licensing agreements have been signed with Austria, Belgium, France, Luxembourg, Netherlands, Morocco, Israel, Finland, Denmark, F.R. of Germany, Portugal, South Africa, Sweden, Switzerland, United States and all Commonwealth countries. Information can be obtained from the Radio and Broadcasting Department of the G.P.O.

In Brief: A special station GB2HRH will operate at Caernarvon from June 28 to July 6 to mark the investiture of the Prince of Wales. . . . Indonesia has notified I.T.U. of the withdrawal of objections to YB amateurs working other countries. . . . An I.A.R.U. Region 1 Conference is being held in Brussels between May 5 and 10. . . . The c.w. section of the U.S.S.R. “Peace to the World” h.f. contest takes place from 09.00 May 3 to 21.00 May 4, on all bands from 3.5 to 28 MHz. . . . R.S.G.B. 1.8 MHz direction finding qualifying events are to be held at Stratford-on-Avon on April 27, Grimsby on May 18, Oxford on June 29, Salisbury on July 20, and High Wycombe on August 3. The national final is to be held at Rugby on September 21. . . . An American amateur was recently given a six-months prison sentence for transmitting obscene, indecent and profane language.

Literature Received

and how the construction of this rectifier (251UL) differs from normal rectifiers. Typical applications are also given. International Rectifier, 233 Kanas St., El Segundo, California 9024S, U.S.A. **WW 415** for further details.

Digital-to-analogue converters for 4- to 10-bit words are described in application note 00011D/A from Sprague Electric (U.K.) Ltd., Trident House, Station Rd., Hayes, Middlesex. **WW 416** for further details.

"Parameters . . . Circuit Analysis and Design" is an 87-page application note (No.95) consisting of seven articles devoted to the description of high-frequency design (<100MHz) using "S" parameters. A description of "S" parameters is included. Hewlett Packard Ltd., 224 Bath Road, Slough, Bucks. **WW 417** for further details.

Also from Hewlett Packard, of the above address, application note 920, "Harmonic Generation Using Step-recovery Diodes". **WW 418** for further details.

PRODUCT LITERATURE

A **dry-joint locator** manufactured by Davian Instruments Ltd. is described in a leaflet available from Techmation Ltd., 58 Edgware Way, Edgware, Middlesex. **WW 419** for further details.

Solderless wrapped "Barb" connectors are the subject of a leaflet from Oxley Developments Ltd., Priory Park, Ulverston, Lancs. **WW 420** for further details.

Data on a 110-MHz **digital frequency meter** is given in a leaflet produced by Venner Electronics Ltd., Kingston By-pass, New Malden, Surrey. **WW 421** for further details.

A leaflet from Coutant Electronics Ltd., 3 Trafford Rd., Reading, Berks. gives details of a **digital voltmeter** (CDV200) with 0.05% accuracy and 100 μ V resolution. **WW 422** for further details.

Performance details of a range of **voltage reference valves** (QS1200 to QS1213) and voltage stabilizers (OA, OB and QS series) are given in a brochure available from the English Electric Valve Co., Ltd., Chelmsford, Essex. **WW 423** for further details.

Toroidal inductors from Control Technology Ltd., 44 Meeching Rd., Newhaven, Sussex, are the subject of a leaflet we have received. **WW 424** for further details.

"President" **panel instruments**, which are manufactured by Ferranti Ltd., Moston, Manchester M10 0BE, are described in a brochure that is now available. **WW 425** for further details.

A **y.i.g. tuned microwave receiver** (1.8 to 25 GHz) designed for use, as a plug-in, with the Tektronix series 560 and letter-series oscilloscopes is described in a leaflet. The receiver can cover the whole band in one-sweep to display received signals on the tube face. Electro/Data Inc., 3121 Benton Street, Garland, Texas, U.S.A. **WW 426** for further details.

For low-level measurements Tektronix have produced a **10 μ V/div. plug-in** (Type 3A9) for the 560 series oscilloscopes which is described in a leaflet received. Tektronix U.K. Ltd., Beaverton House, Harpendon, Herts. **WW 427** for further details.

GENERAL INFORMATION

"**Equivalents Index 1969**" lists the English Electric equivalents for a variety of valve types. English Electric Valve Co. Ltd., Chelmsford, Essex. **WW 428** for further details.

"**Mullard Data Book**". The 1969 edition of this popular publication is now available at 3s 6d per copy from Mullard House, Torrington Place, London, W.C.1.

Details of a **components brokerage service** are available from GDS (Sales) Ltd., Michaelmas House, Salt Hill, Bath Rd., Slough, Bucks. **WW 429** for further details.

Details of the **services offered** by the National Research Development Corporation are given in a nicely produced brochure, called a "Service to Industry", we have received. N.R.D.C., 34 Bouverie St., London E.C.4. **WW 430** for further details.

BS4410:1969, "Specification for the Connection of Flexible Cables and Cords for Appliances" is now available, price 6s, from the British Standards Institution, British Standards House, 2 Park St., London, W.1.

CP 1016: Part 1:1968 "The Use of Semiconductor Devices" is also available from the above address, price 12s.

CATALOGUES

Sub-miniature, miniature and standard **lamps** from Vitality Bulbs Ltd., 64 Marylebone Lane, London W.1, are described in catalogue no.69. **WW 401** for further details.

Supplement no.2, dated February 1969, is available for the ITT (S.T.C.) **Electronic Services Catalogue**. ITT Electronic Services, Edinburgh Way, Harlow, Essex. **WW 402** for further details.

Telemetry equipment for a wide range of applications and remote control systems are described in a brochure produced by Sound Diffusion Ltd., Datum Works, Hove, Sussex BN3 1RZ. **WW 403** for further details.

Data on **test and measuring equipment** from B & K Laboratories Ltd., Cross Lances Rd., Hounslow, Middlesex, is given in a new short-form catalogue. **WW 404** for further details.

Precision measuring apparatus (standard cells, potentiometers, galvos etc) are listed, complete with performance data, in a catalogue from H. Tinsley and Co. Ltd., Werndee Hall, South Norwood, London S.E.25. **WW 405** for further details.

An enlarged **components catalogue**, on the same lines as earlier editions, is now available from Home Radio (Components) Ltd., London Road, Mitcham, Surrey, price 8s 6d.

Redifon Ltd., of Broomhill Road, London S.W.18, have produced a catalogue which describes military and commercial **communication equipment**, **broadcasting equipment** and **navigational aids**. **WW 406** for further details.

Catalogue of **used scientific equipment** from V. N. Barrett and Co. Ltd., 1 Mayo Road, Croydon, CRO 2QP, lists a wide range of items from vacuum pumps to electronic equipment. **WW 407** for further details.

The 1969 **Transistor Catalog** of the Raytheon Company, Components Division, Semiconductor Operation, 350 Ellis Street, Mountain View, California, U.S.A., gives data on and physical details of a large number of transistor types. **WW 408** for further details.

"Econoline", a moulded series of **plastic encapsulated transistors** from the Semiconductor Division of the Sprague Electric Company, Trident House, Station Rd., Hayes, Middlesex, are described in a short-form catalogue (CN200B). **WW 409** for further details.

High-power rectifiers (50kV p.i.v. at 1A) are listed in a catalogue from Solitron Devices Inc., 256 Oaktree Road, Tappan, N.Y. 10983, U.S.A. **WW 410** for further details.

Croydon Precision Instrument Co. of Hampton Road, Croydon CR9 2RU, give details of a range of **precision components**, potentiometers, bridges, switches etc., in their latest catalogue. **WW 411** for further details.

APPLICATION NOTES

From Sprague Electric, Trident House, Station Rd., Hayes, Middlesex: TP.66.11 "Microcircuit digital to analogue converter", (**WW 412** for further details); TP 68.24 "Series 5400/7400 integrated circuit application guide", (**WW 413** for further details); and 25200 "More efficient logic design with multiple function series SE100 integrated circuits", (**WW 414** for further details).

"Application and Characterization of a 250A **Fast Recovery Rectifier**" (AN-B-4) explains how the recovery time of a high-power rectifier is measured

Answers to "Test Your Knowledge"—12 Questions on page 244

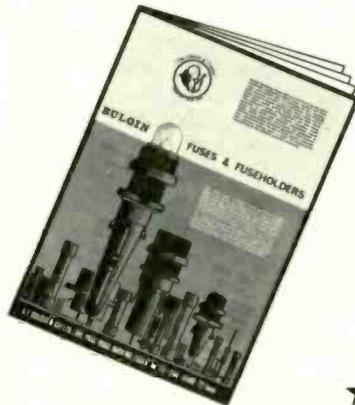
1. (c). It is the *particle displacement* which is in phase quadrature with the excess pressure. A useful analogy can be drawn between excess pressure and particle velocity in a sound wave and electric and magnetic field strengths respectively in an electromagnetic wave. Thus we can define acoustic wave impedance as p/v and the instantaneous wave intensity can be shown to be $p \cdot v$ watts per square metre.
2. (b). The velocity is proportional to the square root of the absolute temperature. At frequencies above the audible range the velocity varies with frequency; at intensities well above the threshold of pain the velocity varies with intensity.
3. (d). This is an example of the Doppler effect and can give rise to a form of non-linear distortion in a cone loudspeaker which is simultaneously radiating a low and a high frequency tone.
4. (c).
5. (d). The musical interval between two notes depends on the ratio of their frequencies. Hence the frequency of $F \#$ must be $260 \times r$. Since $260 \times r \times r$ must = 520, $r = \sqrt{2}$.
6. (a). The definition of the loudness level of a sound in phons is the intensity, in dB above threshold, of a pure 1kHz reference tone which *sounds equally loud*.
7. (c). This is the approximate range between the threshold of audibility and the threshold of pain.
8. (a).
9. (c). For a normal moving coil loudspeaker the back e.m.f. (E) induced by the motion of the coil is $B l v$ where v is the phasor velocity. The force on the coil is $B l i$ (i being the phasor current in the coil) and this must equal $Z_m v$. Motional impedance = $E/i = (B l)^2 / Z_m$.
10. (a). Provided the cone is fitted into a suitable baffle the acoustic power radiated does not change significantly as the frequency is increased from just above the fundamental mechanical resonance to at least a value giving a wavelength equal to the cone circumference. Below the mechanical resonance the power radiated falls off very rapidly with decreasing frequency.
11. (d). This effect is only significant at low frequencies.
12. (c). The horn exhibits a cut off frequency which increases if the rate of taper with distance is increased. Below this frequency there is no appreciable sound transmission through the horn.
13. (b).
14. (d). At a pressure antinode in a standing wave we have a velocity node. The crystal microphone, being pressure operated, will give a large output; the ribbon microphone is a velocity microphone and therefore will give very little.
15. (a).
16. (c). A recommended range of reverberation times for rooms between 1000 and 3000 cubic foot volumes is 0.6 to 0.8 seconds above 1kHz rising to 1.2 to 1.6 seconds as the frequency drops to 30Hz.



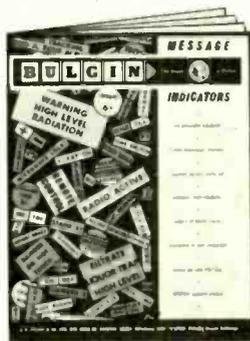
BULGIN COMPONENT BROCHURES

Bulgin publish over 12 Brochures which give full technical information on the vast range of over 15,000 Bulgin Precision Electronic Components. The six Brochures illustrated below are as follows:

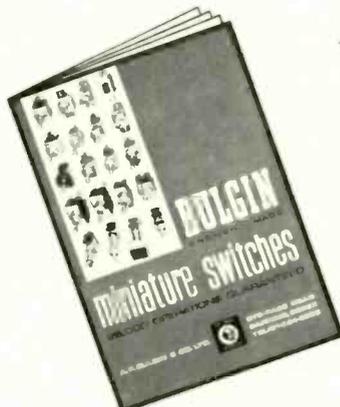
- Brochure No. 1532/C.** Six informative pages detailing our complete range of Fuses and Fuseholders and including Time/Current Characteristics.
- Brochure No. 1500/C.** Twelve pages containing Illustrations and dimensions of our range of over 300 Instrument Control Knobs.
- Brochure No. 1512/C.** Message Indicators are listed with complete technical and ordering information in this eight-page Booklet.
- Brochure No. 1501/C.** Full Electrical and Mechanical Data of our range of Micro Switches is contained in these eight papers.
- Brochure No. 1509/C.** Ten pages of Electrical and Mechanical Data on our complete range of Moulded and laminated Switches.
- Brochure No. 1502/C.** Ten colourful pages containing the information required to decide which Signal Lamp suits your requirements.



FUSES & FUSEHOLDERS
Brochure No. 1532/C



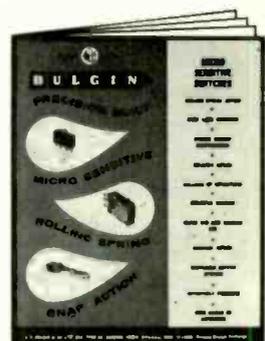
MESSAGE INDICATORS
Brochure No. 1512/C



MINIATURE SWITCHES
Brochure No. 1509/C



INSTRUMENT CONTROL KNOBS
Brochure No. 1500/C



MICRO SWITCHES
Brochure No. 1501/C



SIGNAL LAMPS
Brochure No. 1502/C

Many other component brochures are available, in addition to those illustrated and described above. All contain List Numbers, Illustrations and the relevant Technical Data concerning the various components in the range described. A list of these brochures are given below. Please give both title and number when ordering.

- ★ **PLUG AND SOCKET**
Brochure No. 1506/C
- ★ **CROCODILE CLIP**
Brochure No. 1510/C
- ★ **JACKS AND JACK PLUGS**
Brochure No. 1516/C
- ★ **DESK-TO-DESK SIGNAL KIT**
Brochure No. 1519/C
- ★ **SUD-INTER SWITCH**
Brochure No. 1524/C
- ★ **NEW SWITCH LEGEND INDICATOR**
Brochure No. 1534/C
- ★ **NEW EIGHT-POLE CONNECTOR**
Brochure No. 1533
- ★ **NEW MOULDED INSULATION D.P.C.O. SWITCHES**
Brochure No. 1531/C

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Real and Imaginary

by "Vector"

"In the day of adversity, consider"

Wireless World readers, as a race, are not given to writing letters to the journal unless some hapless author or the printer has mucked up an equation. Their reluctance is understandable, for in all probability most of their working week is spent writing reports which nobody reads. Such circumstances generate a certain disenchantment with penmanship to the point where the Christmas letter to Aunt Mary represents the total spare-time effort. I am therefore particularly grateful to the many readers who have been stirred to write to the editor or to me personally regarding my comments on take-overs and business structures in general. Many thanks for your most interesting letters, which have provided food for the thoughts which follow.

It does no harm at times to try to establish first principles. So let's think for a minute or so in general terms about the electronics industry; and in particular its importance in the scheme of things in the world today.

Of the last there can be no doubt. Electronics has so woven itself into the fabric of civilization that if all electronic devices simultaneously ceased to function the world would be in complete chaos. Communication services (both radio and line) would cease completely; aircraft would be grounded; manufacture and commerce disrupted—you name it, electronics plays a part in it. And, to complete the picture, try to imagine the demoralization of the public bereft of its sound radio set and its "goggle box"! *

This, then is something of the measure of the latent power of the electronics engineer. He has only to withdraw his services, his skills and his experience to overset the world.

I mention this because Professor D. A. Bell, in his thoughtful letter in the February issue, expresses doubts as to whether the learned societies could operate on the lines of the British Medical Association in protection of their engineers and technicians. You may remember, one point he made was that the electronics engineer does not carry the life-and-death image which is attached to a doctor. This of course is very true. We don't carry much of an image at all with the public because, with the exception of the domestic radio servicing fraternity, we don't come into direct contact with them. Everyone knows, either at first or second hand, pretty well what goes on inside a hospital; nobody, when making a telephone call from

London to Glasgow, thinks for a single moment of the complex electronic devices which come into operation when he does so. He doesn't even know they exist. But this doesn't mean that he wouldn't care if they ceased to function. He would care very much. Similarly with broadcasting. Nobody thinks of the engineers manning the studios and stations but if they withdrew their services the whole matter would be at parliamentary level within hours.

So much for the *potential* strength of the electronics engineering profession. In reality, however, it is pitifully weak. It is weak to the point of impotence because, as a generalization, we are individualists. We don't want to be dragooned by a militant trade union. We want to think our own thoughts, make our own decisions, take our own executive action. This is fine—provided that the premium doesn't rise too high.

In the post-war years, until the fairly recent past, the premiums were, on the whole, small. Immediately after peace broke out there was a famine of electronics engineers. We were lured, cajoled and cossetted by every blandishment known to the personnel recruitment boys; as Robert Browning *nearly* put it, "God was in His heaven, all was right with the world!" The firm for which we worked was smallish, but making a profit; moreover it was stable. Job-wise, the ambitious could confidently look forward to promotion; the others to security of tenure, provided the daily task was well done.

The one big mistake we made was to imagine that we had reached the millenium. The idea of building an electronic engineering profession defence mechanism, which had always been an unpalatable thought, was now ludicrous. No lab. stewards for us!

Then came the first rumblings of the storm. We read of small electronics firms being taken over by a big boy. So what? If there was a certain amount of redundancy, the unfortunate could easily get a job somewhere else. So we ignored the cloud on the horizon and concentrated on the clear blue sky overhead.

Now, with storms all around us, we are bewildered and aggrieved. The financial jugglers, with no interest in electronics other than the profits that can be wrung out of the industry, have moved in. Today there is no company or group, however large, which cannot be toppled into takeover. But even in adversity we are completely divided among ourselves. There is, for instance, the 'up

ladder, I'm aboard" school of thought adopted by some engineers in cases where the situation hasn't caught up with them and (they piously trust) it never will. Then there is the young, ambitious element who see in every enforced retirement a greater opportunity to further their own careers. And of course there are the redundants themselves, humiliated, bitter at being thrown prematurely on the scrap-heap, but alone and completely powerless to do anything about it. Lastly there is a core of engineers who take thought beyond mere self-preservation and the short-term future, but feel equally helpless to do anything constructive. It is upon the last-mentioned that the future status of the professional electronics engineer will depend.

Make no mistake about it, we are now paying an intolerably high premium for our individuality of outlook. We are discrete small sticks, easily snapped, whereas, if we had had the sense we were born with, we should have bound ourselves together for strength while the going was good. The financial jugglers know this and this is why the electronics industry is such an attractive fishing pond.

All right, then. Let's admit we were stupid. What to do about it?

If an opinion poll was taken I doubt whether many of us would opt in favour of a *trade* union. I can't readily see us coming out on strike because of a dispute as to which union man should be responsible for applying the solder to the bit. It still seems to me that the logical move would be to coerce the learned societies into throwing their formidable aggregate of weight in on our side. (I say "coerce" with intent because the institutions are not noticeably receptive to innovation. Official comment on the original suggestion was conspicuously absent.)

Clearly, there would be problems. A "best way" to go about it would have to be found—perhaps a committee to study the B.M.A. mechanism would be one promising approach. The question of costs would also have to be solved and here again the B.M.A. model seems to provide a basis for study. One particular headache which would arise concerns the large body of engineers and technicians who are not members of any learned society. One can also foresee that those who regard a learned society as an exclusive club would curl up at the thought of being associated with those who, for one reason or another, cannot put the magic letters after their names. Yet I know many such who possess neither university degree nor learned society membership, but who are nevertheless very able—and in one or two instances, distinguished engineers. What to do about them? Debar them and a singular injustice would be done. Admit them and you *could* be opening the door to all the quacks and incompetents.

No, it isn't going to be simple. But it can be done; indeed, to my mind, it must be done. From here on, the road forks three ways; towards a united front bonded together by the learned societies; towards a militant trade unionism; or to continue as we are, as extras in a twentieth century Uncle Tom's Cabin, with Simon Legree played by the Stock Exchange.

Think on, as they say up North.

* Vector has not seen my mail!—ED.

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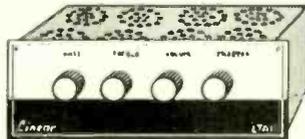
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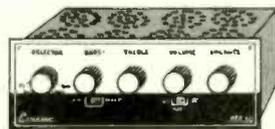


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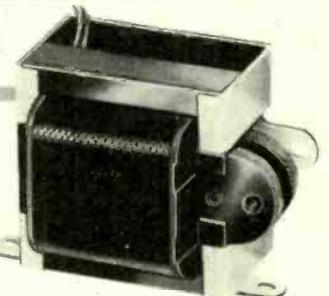
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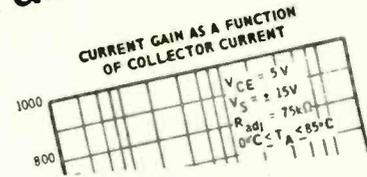
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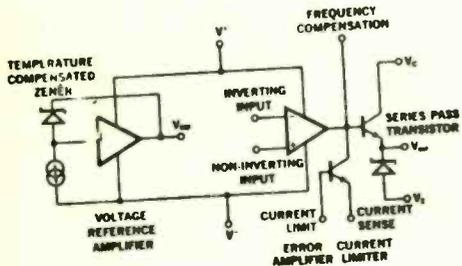
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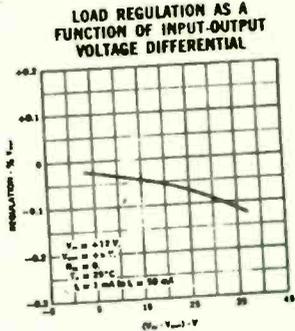


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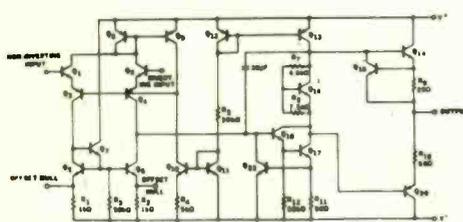
CHARACTERISTICS. $T_{amb} = 25^\circ C.$



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SCHEMATIC DIAGRAM



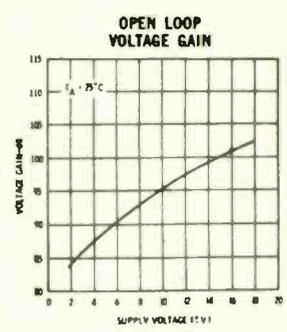
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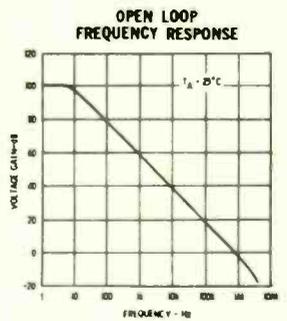
Supply Voltage	± 18	V.
Differential Input Voltage	± 30	V.
Input Voltage	± 15	V.
Total Power Dissipation	500	mW.
Operating Temperature Range	0°C. to 70°C.	

CHARACTERISTICS ($V_+ = 15 V.$ $V_- = 15 V.$ $T_{amb} = 25^\circ C.$)

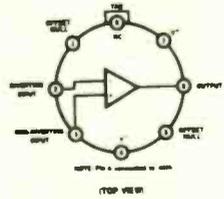
Input Offset Voltage $I_{DS} \leq 10K\Omega$	min.	typ.	max.	
do. 0-70°C.		2.0	6.0	mV.
Input Offset Current		20	200	nA.
do. 0-70°C.			300	nA.
Input Bias Current		200	500	nA.
Input Resistance		0.3	1.0	M Ω .
Large Signal Voltage Gain $R_L = 2K\Omega$		20,000	100,000	
do. 0-70°C.		15,000		
Common Mode Input Range		± 12		V.
Output Voltage Swing $R_L = 10K\Omega$		± 12	± 14	V.
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Supply Voltage Rejection			30	150 $\mu V/V.$
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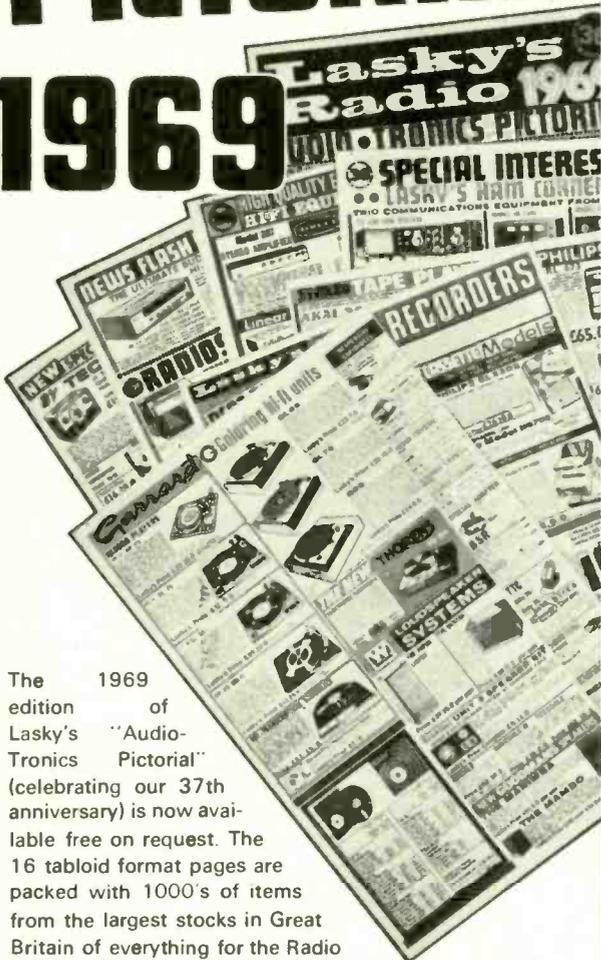
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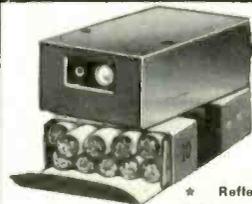
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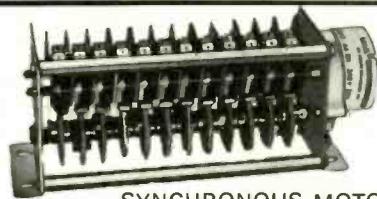
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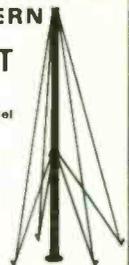
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FULL F1 12 INCH LOUDSPEAKER. This is undoubtedly one of the finest loudspeakers that we have ever offered. Produced by one of the country's most famous makers. It has a die-cast metal frame and is strongly recommended for Hi-Fi load and Rhythm Guitar and public address. Flux Density 11,000 gauss—Total Flux 44,000 Maxwells—Power Handling 15 watts. E.M.F.—Cone Mounted fibre—Freq. response 30-10,000 c.p.s.—specify 3 or 15 ohms—Main resonance 60 c.p.s.—Chassis Diam. 12in.—12 mounting lugs—Baffle hole 11in. Diam.—Mounting holes 4, holes—1/2in. diam. on pitch circle. 1 1/2in. diam.—Overall height 5 1/2in. A 26 speaker offered for only 23.9.8 plus 7/6 p. & p. Don't miss this offer.



PROCESS TIME CONTROLLER

Made by Smiths, motorised and mains driven, enables 15A circuit to be started up to 18 hours in advance and to stay on for a period from 15 minutes to 3 hours. Totally enclosed in metal box with glass front and chrome surround. 49/6 plus 4/6 post and ins. Similar instrument by Hortamund, 14 hrs delay, 4 hrs on-time, 30-amp switch, 69/6.



NICAD RECHARGEABLE BATTERIES

3-6V 500mA size 1 1/4 x 1 1/2in. dia. really powerful will deliver 1 amp for 1/2 hour. Regular price 32/6 our price 17/8 each. New and guaranteed. Other voltages available, single cell 1.2V 6/6. 5 cell 6V 29/6.



Where postage is not stated then orders over £3 are post free. Below £3 add 2/9. Semi-conductors add 1/- post. Over £1 post free. S.A.E. with enquiries please.

TELESCOPIC AERIAL

for portable, car radio or transmitter. Chrome plated—six sections, extends from 7 1/2 to 47 in. Hole in bottom for 6BA screw. 7/6.

MOVING COIL METER BARGAIN

Panel meters are always being needed and they are jolly costly when you have to buy them in a hurry—so you should take advantage of this offer: 2in. moving coil flush mounting meters only 9/8. These are actually R.F. meters and cost about £3 each but if you don't want them for R.F. then all you have to do is to remove the thermocouple and you will have a 2-3 ma. meter which you can make into almost anything by adding shunts or series resistor. New and unused.

MAINS TRANSISTOR POWER PACK

Designed to operate transistor sets and amplifiers. Adjustable output 6v., 9v., 12 volts for up to 500mA (class B working). Takes the place of any of the following batteries: PP1, PP3, PP4, PP6, PP7, PP9, and others. Kit comprises: mains transformer rectifier, smoothing and load resistor, condensers and instructions. Real snip at only 18/6, plus 3/6 postage.

REED-SWITCH

Suitable for dozens of different applications, such as burglar alarms, conveyor-belt switching. These are simply glass-encased switches which can be operated by a passing permanent magnet coil. A special by enables us to offer these at 2/6 each, or 24/- a dozen. Suitable magnets are 1/- each.

SPRING COIL LEADS

as fitted to telephones, 4 core 2/6 each, 3 core 2/- each.



MINIATURE RELAY

American make—630 ohm coil 20-30 volt operation—2 pole change over 4/8 each. 48/- doz.



5A 3-PIN SWITCHED SOCKETS

An excellent opportunity to make that bench dis board you have needed or to stock up for future jobs. This month we offer 6 British made (Heraclit) bakelite flush mounting shuttered switch sockets for only 10/- plus 3/6 post and insurance. (20 boxes post free.)

Rotary Cam Operated Switch. 4 positions: 1st position all contacts open; 2nd, contact 1 closed; 3rd, contacts 1 and 2 closed; 4th, contacts 1, 2 and 3 closed. Contact rated 250 v., 16 amps, 8/6 each.
Circular Fluorescent. 22 watt, 9in. diam. tube complete with choke, starter, holders and chrome clips, 29/8, post, etc., 4/6.
Midjet Relay twin 250 ohm coils, size approx. 1 1/2in. x 1in. x 1in. 4 pairs changeover contacts, 7/6 each.

ELECTRONICS (CROYDON) LTD

Dept. WW, 266 London Road, Croydon CRO-2TH
Also 102/3 Tamworth Road, Croydon

TRANSISTOR D.C. CONVERTORS

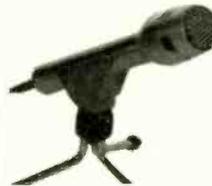
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LONDON microphones

Quality sound—at low cost

The London Microphone range offers you quality microphones, good characteristics—and good looks, too, at remarkably little cost. Made in Britain.



NEW to the range: LM300 dynamic cardioid microphone incorporating top-quality moving-coil capsule. Gives maximum front-to-back ratio over a frequency range of 50-15,000 Hz. Elegant styling, robust metal case, natural anodised finish.

	Low imp.	Dual imp.
LM 300 (Cardioid)	£11 10 0	£12 10 0
LM 200S "	£5 19 6	£6 15 0
LM 200 "	£4 19 6	£5 15 0
LM 100 (Omni)	£3 3 0	£3 18 6

Home or overseas trade enquiries welcome. Write or ring for details

LONDON MICROPHONE CO. LTD.
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WW-126 FOR FURTHER DETAILS

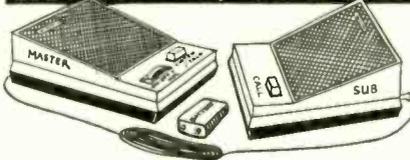
4-STATION INTERCOM



Our Price Only
£7/15/0

Solve your communication problems with this new 4-Station Transistor Intercom system (1 master and 3 subs), in de luxe plastic cabinets for desk or wall mounting. Call/talk/listen from Master to Subs and Subs to Master. Operates on one 9 v. battery. On/off switch. Volume control. Ideally suitable to modernise Office, Factory, Workshop, Warehouse, Hospital, Shop, etc., for instant inter-departmental contacts. Complete with 3 connecting wires, each 66ft. and other accessories. Nothing else to buy. P. & P. 7/6 in U.K.

INTERCOM/BABY ALARM



OUR PRICE ONLY
65/-

Same as 4-Station Intercom for two-way instant conversation from MASTER to SUB and SUB to MASTER. Ideal as Baby Alarm and Door Phone. Complete with 66ft. connecting wire. Battery 2/6. P. & P. 4/6.

7-STATION INTERCOM

(1 MASTER & 6 SUB-STATIONS) in strong metal cabinets. Fully transistorised. 3 1/2in. Speakers. Call on Master identified by tone and Pilot lamp. Ideally suitable for Office, Hotel, Hospital and Factory. Price 27 gns. P. & P. 14/6 in U.K.

Transistor TELEPHONE AMPLIFIER



59/6

Why not increase efficiency of Office, Shop and Warehouse with this incredible De-Luxe Portable Transistor TELEPHONE AMPLIFIER which enables you to take down long telephone messages or converse without holding the handset. A useful office aid. A must for every telephone user. Useful for hard of hearing persons. On/off switch. Volume Control. Operates on one 9 v. battery which lasts for months. Ready to operate. P. & P. 3/6 in U.K. Add 2/6 for Battery.

Full price refunded if returned in 7 days.

WEST LONDON DIRECT SUPPLIES (W.W.),
169 Kensington High Street, London, W.8

R.S.C. SENSATIONAL HIGH FIDELITY STEREO PACKAGE OFFERS

Matching as recommended for optimum performance. Compare prices with equipment and cabinets purchased individually.

'Package 3' 30 Watt Output

- ★ Goldring Transcription Turntable on Plinth.
 - ★ Shure Magnetic Pick-up Cartridge.
 - ★ Super 30 Amplifier in veneered housing.
 - ★ Pair of Stanton Loudspeaker Units.
- Special total price. Four fully wired units ready to "plug-in".
- 85 Gns.** Plus small P.T. surcharge

Illustrated with TFM1 Tuner fitted.

'Package 2' 30 Watt Output

- ★ Garrard SP25 Mk. II Turntable on Plinth.
 - ★ Goldring CS90 Ceramic P.U. Cartridge.
 - ★ Super 30 Amplifier in veneered housing.
 - ★ Pair of Stanton Loudspeaker Units.
- Special total price. Four fully wired units ready to "plug-in".
- 75 Gns.** Carr. 25/- Plus small P.T. surcharge
- Extremely Attractive and Versatile Plinths finished in Teak or Afrormosia veneer. Tinted Perspex "roll over" cover with satin chrome handle.

'Package 1' 13 Watt Output

- ★ Garrard SP25 Mk. II 4-speed Player Unit, on plinth.
 - ★ Goldring CS90 Ceramic P.U. Cartridge.
 - ★ TA12 Amplifier in veneered housing.
 - ★ Pair of Dorchester Loudspeaker Units.
- Special total price. Perspex cover 3 gns extra. Or Dep.
- 49 1/2 Gns.** Plus small P.T. surcharge
- £10. and 9 mthly. pmts. £5.4.0. (Total £58.18/6) Carr. 25/-

BLACKPOOL AGENT APPOINTED

AUDIOTRINE HIGH FIDELITY LOUDSPEAKERS

Heavy construction. Latest high efficiency ceramic magnets. Treated cone surround giving low fundamental resonance. "D" indicates Tweeter Cone providing extended frequency range 40-15,000 c.p.s. Impedance 15 ohms. Exceptional performance at low cost.

Prices include carriage. PLEASE STATE IMPEDANCE

HF 510L 8" 10W 57/9 HF 120 12" 15W 89/9
 HF 801D 8" 8W 57/9 HF 120D 12" 15W 79/9
 HF 811D 8" 10W 24/4.0 HF 126 12" 15W 89/9
 HF 102D 10" 8W 59/9
 HF 100D 10" 15W 25/15 HF 126D 12" 15W 5 Gns.

AUDIOTRINE HI-FI SPEAKER SYSTEMS

Consisting of matched 12in. 12,000 line 10 watt 15 ohm high quality speaker, cross-over unit and tweeter. Smooth response and extended frequency range ensure surprisingly realistic reproduction.

Or Senior 15 watt kit. HF 126 **5 Gns.**
 15,000 line speaker 6 Gns. Carr. 6/6. Carr. 5/9

HI-FI 'SPEAKER ENCLOSURES

Teak or Afrormosia veneer finish. Modern design. Acoustically lined and ported. Prices inc. carr.

JES Size 16 x 11 x 9in. Pressurised. Gives pleasing results with any 8in. Hi-Fi speaker. **4 Gns.**

SES For optimum performance with any 8in. Hi-Fi speaker. Size 22 x 15 x 9in. **5 Gns.**

SE10 For outstanding results with any 10in. Hi-Fi speaker. Size 24 x 15 x 10in. **£5.10**

SE12 For high performance with 12in. Hi-Fi speaker and Tweeter. Size 25 x 16 x 10in. **6 Gns.**

R-S-C TA12 13 WATT STEREO AMPLIFIER

FULLY TRANSISTORISED. SOLID STATE CONSTRUCTION HIGH FIDELITY OUTPUT OF 6.5 WATTS PER CHANNEL

Designed for optimum performance with any crystal or ceramic Gram P.U. cartridge. Radio tuner. Tape recorder. 'Mike' etc.

- ★ 3 separate switched input sockets on each channel
- ★ Separate Bass and Treble controls
- ★ 8kilo Switch for mono use
- ★ Speaker Output 3-15 ohms
- ★ For 200-250V A.C. mains
- ★ Frequency Response 20,000 c.p.s.—2dB
- ★ Harmonic Distortion 0.3% at 1000 c.p.s. Hum and Noise —70dB
- ★ Sensitivities (1) 300 mV (2) 50 mV (3) 100 mV (4) 2 mV
- ★ Handsome brushed silver finish Facia and Knobs. Output rating I.H.F.M. Complete kit of parts with full wiring diagrams and instructions. **12 Gns.** Carr. 7/9. Factory built with 12 mth. gntee. **16 Gns.** Or Dep. £4/18/- and 9 mthly. pmts. **3/18** (Total £18/18/6) Or In Teak or Afrormosia veneer housing **19 Gns.** Or Dep. £4/19/- and 9 mthly. pmts. **3/9** (Total £22/10/0)

HIGH FIDELITY LOUDSPEAKER UNITS

Cabinets of latest styling Satin Teak or Afrormosia veneer. Acoustically lined or filled with woollen damping material. Ported where appropriate. Credit terms available.

DORCHESTER

Size 16 x 11 x 9in. Appr. Range 45-15,000 c.p.s. Rating 8-10 watts. Fitted High Flux 13" x 8in. **£8.19.9**

Dual cone speaker. Impedance 3 or 15 ohms. Inc. carr.

STANTON IIIS

Size 18 x 11 x 10in. Rating 10 watts. Incorporating Pass 803b speaker with roll rubber cone surround and 10,000 line magnet. High flux tweeter. Handsome Scandinavian design cabinet. **16 Gns.**

GLOUCESTER

Size 20 x 16 x 10in. 12in. High flux 12,000 line speaker. Cross-over unit and Tweeter. Rating 19 watts. Frequency range 40-20,000 c.p.s. Impedance 15 ohms. **12 1/2 Gns.**

R.S.C. TA6 6 Watt HIGH FIDELITY SOLID STATE AMPLIFIER

200-250V. A.C. mains operated Frequency Response 30-20,000 c.p.s.—2dB. Harmonic Distortion 0.3% at 1,000 c.p.s. Separate Bass and Treble controls. 3 input sockets for Mike, Gram, Radio or Tape. Input selector switch. Output for 3-15 ohm speakers. Max. sensitivity 5mV. Output rating I.H.F.M. In fully enclosed enamelled case. 9 1/2 x 2 1/2 x 5 1/2in. Brushed silver finish. Facia plate 19 1/2 x 3 1/2in. and matching knobs. Complete kit of parts with full wiring diagrams and instructions. Carr. 7/9 Or factory built with 12 months' guarantee. **£8. 19. 9**

R.S.C. COLUMN SPEAKERS

Covered in two-tone Resin/Vinyl. Ideal for vocalists and Public Address. 15 ohm impedance. Type C27 15 watts inc. five 7 x 4in. spkrs. **£7/10/11. Type C485 30 watts.** Fitted four 8in. high flux 8 watt speakers. Overall size approx. 42 x 10 x 5in. **16 Gns.** Or deposit 65/- and 9 mthly pmts. **24/9** (Total £18/17/9). Carr. 10/-

Type C412a, 50 watts. Fitted four 12in. 11,000 lines 15 watt speakers. Overall size 56 x 14 x 9in. approx. **24 Gns.** Or deposit **£24/19/6** and 9 monthly payments Carr. 15/- of £2/6 (Total £28/5/-)

R.S.C. TFM1 SOLID STATE VHF/FM RADIO TUNER

★ High-sensitivity 200-250V. A.C. Mains operation. ★ Sharp A.M. Rejection. ★ Drift-free reception. ★ Output ample for any amplifier (approx. 500 m.v.). ★ Simple alignment instructions. ★ Output available for feeding into meter. ★ Output for feeding Stereo Multiplexer. ★ Teak or veneer housed siltion Planar Transistors. ★ Designed for standard 80 ohm coaxial input.

Visually matching our Super 15 and 30 amplifiers and of the same high standard of performance and reliability. The pre-wired tuning head facilitates speed and simplicity of construction. Printed circuitry. Only high grade transistors and components used. A quality product at considerably less than the cost of comparable units. Stereo version. All parts 20 gns. Inc. Carr. Assembled 22 1/2 gns. Inc. Carr.

14 Gns.

Or factory built 18 1/2 gns. Or in Teak finished cabinet as illustrated 19 gns. Terms: Deposit £5 and 9 monthly payments 22. Total £23.

THE 'YORK' HIGH FIDELITY 3 'SPEAKER SYSTEM

Moderate size approx. 25 x 14 x 10 in. *Range 30-20,000 Complete kit. c.p.s. Impedance 15 ohms. * Performance comparable with units costing considerably more. Consists of (1) 12in. 15 watt Bass unit with cast chassis, Roll rubber cone surround for ultra low resonance, and ceramic magnet. (2) 3-way quarter section series cross-over system. (3) 8" x 5in. high flux middle range speaker (4) High efficiency tweeter (5) Measured weight of wood and damping material. (6) Teak veneered cabinet. (7) Circuit and full instructions. HEAR IT AT ANY BRANCH. **19 Gns.**

R.S.C. A10 30 WATT ULTRA LINEAR HI-FI AMPLIFIER

Highly sensitive. Push-Pull high output, with Pre-amp./Tone Control Stages. Performance figures: Hum level—70dB. Frequency response ±3dB 30-20,000c.p.s. Sectionally wound output transformer. All high grade components. Valves EF86, EF89, ECC83, 607, 807, GZ34, separate Bass and Treble Control. Sensitivity 38 millivolts. Suitable for High Impedance mike, or pick-ups. Designed for Clubs, Schools, Theatres, Dance Halls or Outdoor Functions, etc. For use with Electronic Organ, Guitar, String Bass, etc. Gram, Radio or Tape. Reserve L.T. and H.T. for Radio Tuner. Two inputs with associated volume controls so that two separate inputs such as Gram and 'Mike' can be mixed. 200-250 v. a.c. mains. For 3 and 15 ohm speakers. Complete Kit parts wiring diagrams, instructions. Twin-handled perforated cover 27/6 or factory built with EL34 output valves and 14 Gns. 12 months' guarantee for 17 gns. Tech. figs. apply to factory built units. Carr. 12/6

TERMS: Deposit £5/14/- and 9 monthly payments of 31/3 (Total £19/15/3) Send S.A.E. for leaflet.

R.S.C. BATTERY/MAINS CONVERSION UNITS

Type BM1. An all-dry battery eliminator. Size 5 1/2 x 4 1/2 in. approx. Completely replaces batteries supplying 1.5 v. and 90 v. where A.C. mains 200/250 v. 50 c/s. is available. Complete kit with diagram **49/11** or. Ready to use. **59/11**

SELENIUM RECTIFIERS

F.W. Bridged 6/12V. D.C. Or Input Max. 18v. A.C. Ia. 3/11. 2a. 6/11. 3a. 9/9. 4a. 12/9. 5a. 15/9.

R.S.C. MAINS TRANSFORMERS

FULLY GUARANTEED. Interleaved and Impreg. materials. Type 21 21 x 21 in. Screened MIDGET CLAMPED TYPE 21 x 21 x 21 in.

250 v., 60 mA, 6.3 v. 2a. 15/11
 250-0-250v., 60mA, 6.3v. 2a. 16/11

FULLY SHROUDED UPRIGHT MOUNTING

250-0-250V. 100mA. 6.3v. 2a. 0-5-6.3v. 3a. 21/9
 250-0-250V. 100mA. 6.3v. 2a. 0-5-6.3v. 3a. 37/9
 300-0-300V. 100mA. 6.3v. 2a. 0-5-6.3v. 3a. 37/9
 300-0-300V. 130mA. 6.3v. 2a. c.t. 0-5-6.3v. 3a. 45/9
 For Mullard 510 Amplifier. 45/9
 350-0-350V. 100mA. 6.3v. 2a. 0-5-6.3v. 3a. 37/9
 350-0-350V. 150mA. 6.3v. 2a. 0-5-6.3v. 3a. 47/9
 425-0-425V. 200mA. 6.3v. 2a. c.t. 0-5-6.3v. 3a. 69/9
 425-0-425V. 200mA. 6.3v. 2a. 0-5-6.3v. 3a. 75/-
 480-0-480V. 250mA. 6.3v. 2a. c.t. 0-5-6.3v. 3a. 87/9

TOP SHROUDED DROP-THROUGH TYPE

250-0-250V. 70mA. 6.3v. 2a. 0-5-6.3v. 2a. 21/9
 250-0-250V. 100mA. 6.3v. 2a. 0-5-6.3v. 3a. 28/9
 250-0-250V. 100mA. 6.3v. 2a. 0-5-6.3v. 3a. 27/9
 300-0-300V. 100mA. 6.3v. 2a. 0-5-6.3v. 3a. 37/9
 300-0-300V. 130mA. 6.3v. 2a. c.t. 0-5-6.3v. 3a. 47/9
 Suitable for Mullard 510 Amplifier. 45/9
 350-0-350V. 100mA. 6.3v. 2a. 0-5-6.3v. 3a. 37/9
 350-0-350V. 150mA. 6.3v. 2a. 0-5-6.3v. 3a. 45/11

FILAMENT or TRANSFORMER POWER PACK Types

6.3 x 1.5a. 7/9; 6.3v. 2a. 8/9; 6.3v. 3a. 10/9; 6.3v. 6a. 21/9; 12v. 1a. 8/9; 12v. 3a. or 24v. 1.5a. 21/9; 250v. 1.5a. 17/9; 0-15-250v. 2a. 39/9

CHARGER TRANSFORMERS 0-9-150V. 1a. 14/11; 2 1/2a. 17/9; 3a. 19/11; 5a. 23/9; 6a. 27/9; 8a. 33/9

AUTO (STEP UP/STEP DOWN) TRANSFORMERS

0-110-120V. 200-230-250V. 50-80 watts 15/9
 50-100-250V. 250-250V. 40-80 watts 19/9

OUTPUT TRANSFORMERS

Standard Pentode 5,000Ω or 7,000Ω to 3Ω 8/9
 Push-Pull 8 watts EL84 to 3Ω or 15Ω 12/9
 Push-Pull 10 watts 6V6 EL84 to 3, 5, 8 or 15Ω 22/9
 Push-Pull EL84 to 3 or 15Ω 10-12 watts 21/9
 Push-Pull Ultra Linear for Mullard 510 etc. 35/9
 Push-Pull 15-18 watts sectionally wound 6L6 KT66, etc. for 3 or 15Ω 39/9
 Push-Pull 20 watt high quality sectionally wound EL34, 6L6, KT66, etc. to 3 or 15Ω 59/9

SMOOTHING CHOKES

150mA. 7-10Ω. 250Ω 12/9; 100mA. 10Ω. 200Ω 10/9; 80mA. 10Ω. 350Ω. 8/9; 60mA. 10Ω. 400Ω 4/11.

INTEREST CHARGES REFUNDED

On Credit Sales settled in 3 months.

R.S.C. SUPER 15 HI-FI AMPLIFIER

FULLY TRANSISTORISED 200/250V. A.C. Mains. OUTPUT 10 WATTS R.M.S. continuous into 15 ohms. 15 WATTS R.M.S. continuous into 3-4 ohms. TRANSISTORS. 9 current types of high quality by leading manufacturers. 5 POSITION INPUT SELECTOR SWITCH EQUALISATION to Standard R.I.A.A. and C.C.I.R. Characteristics for Gram and Tape Heads. FULL TAPE MONITORING FACILITIES SENSITIVITIES: Magnetic P.U. 4 mV. Crystal or Ceramic P.U. 400 mV. Microphone 4.5 mV. Tape Head 2.5 mV. Radio/Aux. or Ceramic P.U. 110 mV. FREQUENCY RESPONSE: ±2dB 20-20,000 c.p.s. TREBLE CONTROL: +10dB to -14dB at 10 Kc/s. NEG. FEEDBACK: 52dB. BASS CONTROL: +17dB to -15dB at 50 c/s. HUM LEVEL: -70dB. HARMONIC DISTORTION at 10 watts 1,000 c.p.s. 0.2% Complete Kit of parts with full constructional details and point to point wiring diagrams. Carr. 12/6. Supplied factory built, 15 1/2 Gns. Carr. 12/6. Terms: Deposit 4 Gns. and 9 monthly payments 31/1 (Total £18/3/9). Or in Teak or Afrormosia veneer housing as illustrated. 19 Gns. COMPONENTS ETC. ARE OF A HIGH STANDARD AND SUPPLIED BY LEADING MANUFACTURERS.

R.S.C. A11T 15 WATT HIGH FIDELITY AMPLIFIER

DUAL PURPOSE P.A. or HI-FI SOLID STATE CIRCUITRY. 3 input sockets. 2 vol. controls for mixing purposes. ★ Input Selector. ★ Output for speakers between 3 and 15 ohms. ★ Separate Bass and Treble Controls. Suitable for Gram, Radio, Tape, Microphone, or Guitar P.U. For Vocal and Instrumental groups. Frequency Response 20-40,000 c.p.s.—3dB. Hum level—80dB. Harmonic Distortion 0.2% at 10 watts R.M.S. Operation on 200-250V. A.C. mains. Output rating I.H.F.M. Size 9 1/2 x 2 1/2 x 5 1/2in. Complete Kit of 9 Gns. 9/6 Or Factory built with 12 mth. guarantee 13 Gns. Carr. 9/6. Terms: Deposit £4 and 9 monthly payments 25/6 (Total £15/9/6)

12in. High Quality LOUDSPEAKERS

In teak veneered cabinets. 15 Watt Model, Gauss 11,000 lines. 3 or 15 ohms. **£5/15/-** Carr. 7/6

20 Watt Model, 15 ohm. Size 18 x 18 x 18in. Gauss 10,000 lines. Resine **£8/19/9** Carr. 8/9

COVERED 10/- extra

TWO-WAY 'PHONE AMPLIFIER

Listen and speak with both hands free. Handsome black case. Battery operated. **59/9**

R.S.C. SUPER 30 STEREO AMPLIFIER

A DUAL CHANNEL VERSION OF THE SUPER 15. Employing Twin Printed Circuitry. High quality Ganged Pots. Matched components. CROSS TALK: -52dB at 1,000 c.p.s. CONTROL: 5 position Input Selector, Bass Control, Treble Control, Volume Control, Balance Control, Stereo/Mono Switch, Tape Monitor Switch, Mains Switch, INPUT SOCKETS (Matched Pairs). (1) Magnetic P.U. (2) Ceramic or Crystal P.U. (3) Radio/Aux. (4) Tape Head/ Microphone. Operation of the Input Selector Switch assures appropriate equalisation. Rigid 18 s.w.g. Chassis. Size approx. 12in. wide, 5in. high and 8in. deep. Neon Panel Indicator. Attractive Facia Plate and Spun Brass Knobs. Above facia plate, etc. except for Ganging and Balance control, apply also to Super 15.

THESE UNITS ARE EMINENTLY SUITABLE FOR USE WITH ANY MAKE OF PICK-UP OR MICROPHONE (Crystal, Ceramic, Magnetic, Moving Coil, Ribbon) CURRENTLY AVAILABLE. SUPERB SOUND OUTPUT QUALITY CAN BE OBTAINED BY USING WITH FIRST RATE ARCILLARY EQUIPMENT. All required parts, point to point wiring diagrams and detailed instructions. Carr. 15/-

Unit factory built 28 Gns. or deposit 27/5/- and 9 monthly payments 56/3 (Total £32/13/9). Or in Teak or Afrormosia Veneered housing. 31 Gns. Carr. 16/- or Deposit 27/3/6 and 9 monthly payments. 64/- (Total £35/19/6) Send S.A.E. for leaflet

12 1/2 Gns.

R.S.C. SUPER 30 STEREO AMPLIFIER

These units are eminently suitable for use with any make of pick-up or microphone (Crystal, Ceramic, Magnetic, Moving Coil, Ribbon) currently available. Superb sound output quality can be obtained by using with first rate ancillary equipment. All required parts, point to point wiring diagrams and detailed instructions. Carr. 15/-

Unit factory built 28 Gns. or deposit 27/5/- and 9 monthly payments 56/3 (Total £32/13/9). Or in Teak or Afrormosia Veneered housing. 31 Gns. Carr. 16/- or Deposit 27/3/6 and 9 monthly payments. 64/- (Total £35/19/6) Send S.A.E. for leaflet

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Unit factory built 28 Gns. or deposit 27/5/- and 9 monthly payments 56/3 (Total £32/13/9). Or in Teak or Afrormosia Veneered housing. 31 Gns. Carr. 16/- or Deposit 27/3/6 and 9 monthly payments. 64/- (Total £35/19/6) Send S.A.E. for leaflet

Record Playing Units

MONEY SAVING UNITS Ready to plug into Amplifier

RP2 Consisting of Garrard SP25 Mk. II (with heavy turntable) fitted with Goldring CS90 high compliance ceramic Stereo/Mono cartridge with diamond stylus. Mounted on plinth. Perspex Cover **22 Gns.** included. Carr. 15/-

Plus 8/7 P.T. surcharge.

RP3 As above but with Goldring Lenco G168 Transcription unit and CS90 Cartridge. Cover included. Inc. P.T. surcharge. Carr. 21/- ONLY **£28**

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Total dissipation (in free air, $T_{amb} = 25^{\circ}\text{C}.$).....100mW. Derating Factor.....2mW/ $^{\circ}\text{C}.$
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Power dissipation*.....600mW. Derating factor for T_{amb} greater than $25^{\circ}\text{C}.$7.5mW/ $^{\circ}\text{C}.$
Reverse voltage V_R max 1-0V.

*When mounted on an aluminium heat sink 1 in. x $\frac{1}{2}$ in. x $\frac{1}{2}$ in.

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Epoxy sealed $\frac{1}{2}$ in. diam. x $\frac{1}{8}$ in. thick. Resistance at 100 Lux — 700 to 3,000 ohms. Maximum voltage 200 A.C. or D.C. Maximum current 500 mW. 12/6 post free



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These have a higher dark resistance in a given period than Cadmium Sulphide Cells, indicating much faster response. Suitable for all CdS applications plus applications in chopper, electronic musical instruments, computer and other sophisticated circuitry. Time response shown in megohms is dark resistance measured 10 secs. after 400 Lux light intensity is intercepted.



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Hermetically metal sealed. $\frac{1}{2}$ in. diam. x $\frac{1}{8}$ in. thick. Time response 100 megohms. Resistance at 1,000 Lux — 100 ohms to 1,000 ohms. Resistance at 10 Lux — 1 Kohm to 10 Kohms. Maximum voltage 50 A.C. or D.C. Maximum current 80 mW. Continuous 30 mW. 16/6 post free

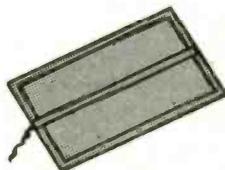
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Selenium cells in which light energy is converted into electricity directly measurable on microammeter or used with amplifier as light trigger for alarm and counting devices, luminous fluxmeters, exposure meters, colorimeters, etc., etc. Spectral response covers visible light range.

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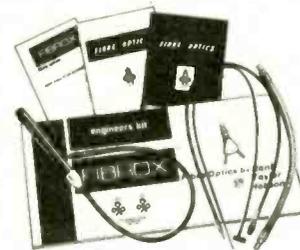
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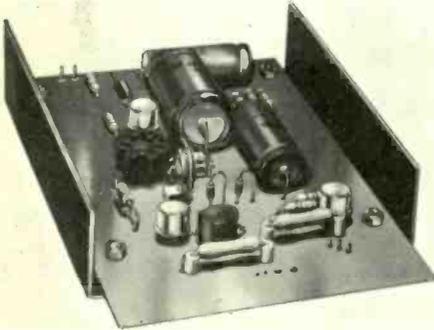
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25
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RMS
INTO
15Ω

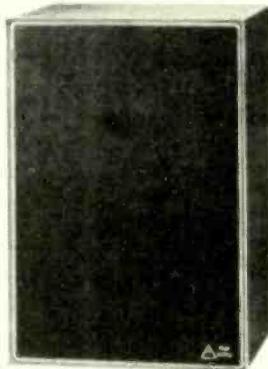
A superb specification

Output at 1 KHz into 15 ohms—26.6 watts R.M.S. ■ Acceptable to speakers from 8 to 15 ohms ■ Frequency response at 1 watt—20 Hz to 120 KHz (−3dB) ■ Power bandwidth for −1dB at 20 watt at less than 0.25% distortion—20 Hz to 20 KHz ■ Input sensitivity for 26.6 watts output—500 mV into 500 K ohms ■ Signal to noise ratio better than −80dB ■ Power requirements—68 volts DC.

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5 in. x 2½ in.	0-15 matrix	3/11	5 in. x 2½ in.	0-1 matrix	4/7
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1μF	20 volt	5μF	6 volt	25μF	25 volt		
1-25μF	16 volt	6μF	6 volt	30μF	6 volt		
2μF	3 volt	8μF	3 volt	30μF	10 volt		
2μF	350 volt	8μF	12 volt	50μF	6 volt	All at 1/- each.	
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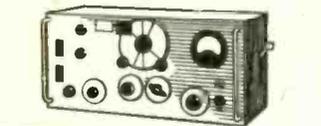


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Y amp. Sensitivity. 1v p-p/CM. Bandwidth 1.5 cps—1.5 MHz. Input imp. 2 meg Ω. 25 PF. X amp sensitivity. .9v p-p/CM. bandwidth 1.5 cps—800 KHZ. Input imp. 2 meg Ω. 20 PF. Time base. 5 ranges 10 cps—300 KHZ. Synchronization. Internal/external. Illuminated scale. 130 x 215 x 330 MM. Weight 15 1/2 lbs. 220/240 V. A.C. Supplied brand new with handbook. £35/-/. Carr. 10/-.

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 4 band receiver covering 500 Kc/s to 30 Mc/s, continuous and electrical bandspread on 10-15, 20, 40 and 80 metres. 8 valve plus 7 diode circuit, 4/8 ohm output and phone jack. 885-CW ● ANL ● Variable BFO ● 8 meter. ● Sep. Bandspread dial ● 1F 455 Kc/s ● audio output 1.5 w. ● Variable BF and AF gains controls. 115/250 v. A.C. mains. Beautifully designed. Size 7 x 15 x 10in. With instruction manual and service data. £42.10.0. Carriage paid Trio Communication Type Headphones. Normally £5.19.6. Our price £3.15.0 if purchased with a valve receiver.

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High quality ceramic construction. Windings embedded in vitreous enamel. Heavy duty brush wiper. Continuous rating. Wide range available ex-stock. Single hole fixing. 1in. dia. shafts. Bulk quantities available.
 25 WATT. 10/25/50/100/250/500/1000/1500/2500 or 5000 ohms. 14/8. P. & P. 1/6.
 50 WATT. 10/25/50/100/250/500/1000/2500 or 5000 ohms. 21/- P. & P. 1/6.
 100 WATT. 1/5/10/25/50/100/250/500/1000 or 2500 ohms. 27/8. P. & P. 1/6.

MULTIMETERS for EVERY purpose!

LAFAYETTE DE-LUXE 100 KO/VOLT "LAB TESTER" Giant 6 1/2 in. scale. Built in meter protection. 0.5/2.5/10/50/250/500/1,000 v. D.C. 0.3/10/50/250/500/1,000 v. A.C. 0.1/10/100 μA/10p/100/500 MA/2.5/10 Amp. 0.1k/10K/100K/10M/1000 Ω. —10 to 49.4 dB. £18/18/- P. & P. 5/6.

LAFAYETTE 57 Range Super 50K Ω/V. Multimeter. A.C. volts 120mv—1000v. D.C. volts 15v—1000v. D.C. Current 25 μA—10 Amp. Ohms 0—10 Meg Ω. D.B.—20 to +81 db. Overload protection. £12/10/- P. & P. 3/6.

PROFESSIONAL 20,000 Ω P.V. LAB TYPE MULTIMETER. Automatic overload protection. mirror scale. Ranges 1/10/50/250/500/1,000 v. D.C. and A.C. 0-500 μA. 10mA. 250mA. Current: 0.20K, 200K, 2megohm, Decipels: —20 to +22db. £5/19/6. P. & P. 2/6.

MODEL TE-90 50,000 Ω P.V. Mirror scale overload protection. 0.3/12/60/300/600/1,200 v. D.C. 0.6/30/120/600/1,200 v. D.C. 0.3/6/60/600 MA. D.C. 16K/160K/1.6/16 MEG Ω. —20 — + 63db. £7/10/0. P. & P. 3/6.

TE-10A. 20k Ω/Volt 5/25/50/250/500/2,500 v. D.C. 10/50/100/500/1,000 v. A.C. 0.50 μA/2.5 mA/250 mA D.C. 0.6K/6 meg. ohm. —20 to +22 dB. 10-8, 100 mfd. 0.100-0.1 mfd. 89/6. P. & P. 2/6.

MODEL TE-70. 30,000 Ω P.V. 0.3/15/60/300/600/1,200 v. D.C. 0.6/30/120/600/1,200 v. A.C. 0.30 μA/3/30/300MA. 0.16K/160K/1.6M/16 Meg Ω. £5/10/- P. & P. 3/6.

MODEL TE-12. 20,000 Ω P.V. 0.9/6/30/120/600/1,200/3,000/1,000 v. D.C. 0.9/30/120/600/1,200 v. A.C. 0.60 μA/6/60/600 mA. 0.8K/600K/6M/60 Meg Ω. 50 PF. 2 MFD £5/19/6. P. & P. 3/6.

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 Nearly 200 pages giving full details of a comprehensive range of COMPONENTS, TEST EQUIPMENT, COMMUNICATION EQUIPMENT and HI-FI EQUIPMENT. Each section greatly enlarged and fully illustrated. Thousands of items, many at bargain prices. FREE DISCOUNT COUPONS VALUE 10/-.
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 Call into your nearest shop—Edgware Rd. for all Equipment—Lisle Street for all Equipment and Components.

TE111 DECADE RESISTANCE ATTENUATOR
 Variable range 0-111 db. Connections. Unbalanced T and Bridge T. Impedance 600 ohms. Range (0.1 db x 10) + (1 db x 10) + 10 + 20 + 30 + 40 db. Frequency: DC to 200 KHZ (—3db). Accuracy: 0.05 db. + indication db x 0.01. Maximum input less than 4 watts (50 volts). Built in 600 Ω load resistance with internal/external switch. Brand new £27/10/- P. & P. 5/6.

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 Wonderfully comfortable. Lightweight adjustable vinyl headband, 6ft. cable and stereo jack plug, 25-17,000 cps., 8 Ω imp. £7/8. P. & P. 2/6.

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 19 transistors, 8 diodes, IHP music power 30 watts at 8 ohms. Res. 30-20,000 ± 2 dB at 1 v. Distortion 1% or less. Inputs 3 mV and 250 mV. Output 3-16 ohms. Separate L and R volume controls. Treble and bass controls. Stereo phone jack. Brushed aluminium, gold anodised extruded front panel with metal case. Size 10 1/2 in. x 7 1/2 in. Operation 115/230 volt A.C. £28. Carr. 7/6.

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 High quality instrument with 28 ranges. D.C. volts 1.5-1,500 v. A.C. volts 1.5-1,500 v. Resistance up to 1,000 megohms. 220/240v. A.C. operation. Complete with probe and instructions £17/10/0. P. & P. 3/6. Additional Probes available: E.F. 35/- H.V. 42/6.

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 10 meg. input 10 ranges: .01/.03/.1/.3/1/3/10/30/100/300 v. R.M.S. 4 cps-1.2 Mc/s. Decibels —40 to +80 dB. Supplied brand new complete with leads and instructions. Operation 230 v. A.C. £17/10/- Carr. 5/6.

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 1 μwatt to 6 watts. £20. Carr. 20/-.

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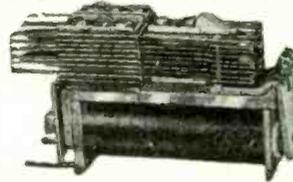
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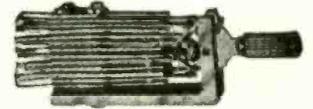


Contacts up to 8 changeover

- ★ QUICK DELIVERY
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KEY SWITCHES

3 POSITION Type 212 2C lock/
 2C lock 12/6. Type 198 4C lock/
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 Other types available. Knobs 8d.



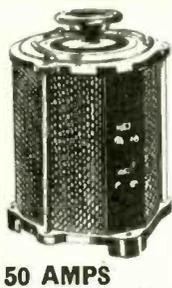
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OIL FREE ROTARY COMPRESSORS & EXHAUSTERS, with continuous Air Flow. Cooper type ED 12 coupled to 3 phase 1 h.p. 400/440 volt motor, 50 cycles, 1450 r.p.m., complete with Vokes fittings £35 ea.
ONE HOLE FIXING SWITCHES S.P.D.T. 3 amp, 250 volt A.C., can be used as on/off or changeover switch, 18/- per dozen, 130/- per 100, post 3/- for doz., 6/- for 100.

RESISTORS EX STOCK IN QUANTITY WIRE WOUND, HIGH STABILITY CARBON, ETC., BEST MAKES AT LOWEST POSSIBLE PRICES

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INPUT 230 v. A.C. 50/60

BRAND NEW. Keenest prices in the country. All Types (and spares) from 1/2 to 50 amp. available from stock.

0-260 v. at 1 amp.	£5 10 0
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20 DIFFERENT TYPES AVAILABLE FOR IMMEDIATE DELIVERY.

Double Wound Variable Transformers

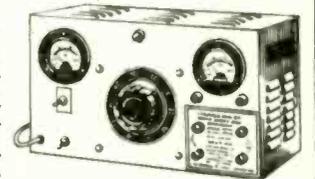
Fully isolated, low tension Secondary winding. Input 230 v. A.C. **OUTPUT CONTINUOUSLY VARIABLE 0-36 v. A.C.**

0-36 v. at 5 amp. £9.12.6—
p. & p. 8/6
0-36 v. at 20 amp. £21.0.0—
15/- p. & c.

These fully shrouded Transformers, designed to our specifications, are ideally suited for Educational, Industrial and Laboratory use.

5 Amp. AC/DC VARIABLE VOLTAGE OUTPUT UNIT

Input 230 v. A.C.
 Output 0-260 v. A.C.
 Output 0-240 v. D.C.
 Fitted large scale ammeter and voltmeter. Neon indicator, fully fused. Strong attractive metal case 15in. X 8 1/2in. X 6in. Weight 24 lb. Infinitely variable, smooth stepless voltage variation over range.



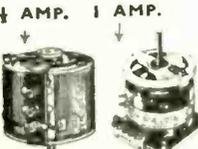
Price £30 P. & C. £2.

7 Amp. A.C./D.C. Mk. II Variable Output Power Unit
 Input 230 v. A.C. Output continuously VARIABLE from 0 to 260 v. A.C. OR 0 to 230 v. D.C. at 7 a. Robustly constructed in metal case, complete with safety fuse, neon indicator, voltmeter and ammeter. Size 17in. X 12in. X 7in. Weight 36 lb. Price £39/10/-. Carriage 40/-.

OPEN TYPES

Designed for Panel Mounting.
 Input 230 v. A.C. 50/60
 Output variable.

0-260 v.	
1/2 amp.	£3 10 0
1 amp.	£5 10 0
2 1/2 amp.	£6 12 6
P. & P. 7/6	
1 AMP. 1 AMP.	



PORTABLE VARIABLE VOLTAGE TRANSFORMER

Input 230 v. A.C. Output variable 0-260 v. A.C. at 1.5 amp. Fitted in beautifully finished steel case. Complete with voltmeter, pilot lamp, fuse, switch, carrying handle. £9/5/-. P. & C. 10/-. Also 2.5 amp. as above. £11/7/6. P. & C. 10/-.

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 LT constant voltage Transformer Input 102/127V 2 ohm 205/255. Output 6.3 volts. RMS Load 7-10 amps. £3 6/6 p.p.

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Input 185-250 v. A.C. Output constant at 230 v. A.C. Capacity 250 watt. Attractive metal case. Fitted red signal lamp. Rubber feet. Weight 17lbs. Price £11/10/-. P. & P. 10/-.



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Ideal for lighting and heating circuits, compact panel mounting. Built in fuse protection. **CONTINUOUSLY VARIABLE.**
 Input 230v AC output 25-230v AC
 5 amp model £8. 7. 6
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 Test to I.E.E. Spec. Rugged metal construction, suitable for bench or field work, constant speed clutch. Size L. 8in., W. 4in., H. 6in. Weight 6lb. 500 volts, 500 megohms. Price £22 carriage paid. 1,000 volts, 1,000 megohms, £28 carriage paid.

36 volt 30 amp. A.C. or D.C. Variable L.T. Supply Unit

INPUT 220/240 v. A.C.
 OUTPUT CONTINUOUSLY VARIABLE 0-36 v.

Fully isolated. Fitted in robust metal case with Voltmeter, Ammeter, Panel Indicator and chrome handles. Input and Output fully fused. Ideally suited for Lab. or Industrial use. £55 plus 40/- p. & c. Similar in appearance to above illustration.

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Kit and parts including ORP.12 Cadmium Sulphide PhotoCell. Relay Transistor and Circuit. Now supplied with new Siemens High Speed Relay for 6 or 12 volt operations. Price 25/-, plus 2/6 P. & P. ORP 12 and Circuit 10/- post paid.



220/240 A.C. MAINS MODEL

incorporates mains transformer rectifier and special relay with 3 X 5 amp. mains c/o contacts. Price inc. circuit 47/6, plus 2/6 P. & P.

LIGHT SOURCE AND PHOTO CELL MOUNTING

Precision engineered light source with adjustable lens assembly and ventilated lamp housing to take MBC bulb. Separate photo cell mounting assembly for ORP.12 or similar cell with optic window. Both units are single hole fixing. Price per pair £21/5/0 plus 3/6 P. & P.



VAN DE GRAAF ELECTROSTATIC GENERATOR

fitted with motor drive for 230 v. A.C. giving a potential of approx. 50,000 volts. Supplied absolutely complete including accessories for carrying out a number of interesting experiments, and full instructions. This instrument is completely safe, and ideally suited for School demonstrations. Price £7/7/-, plus 4/- P. & P. L't. on req.



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2 on/off every 24 hrs. at any pre-set time. Fitted in metal case 36 hr. spring reserve. Used but fully tested. Fraction of maker's price. £31.9/6 plus 4/6d. post and pack. Available with solar dial on request.



LATEST TYPE SELENIUM BRIDGE RECTIFIERS

30 volt 3 amp., 11/-, plus 2/6 P. & P. 30 volt 5 amp., 16/-, plus 2/6 P. & P.

NICKEL CADMIUM BATTERY

Sintered Cadmium Type 1.2 v. 7AH. Size: height 3 1/2 in., width 2 1/2 in. x 1 1/2 in. Weight: approx. 13 ozs. Ex-R.A.F. Tested 12/6. P. & P. 2/6.

DRY REED SWITCHES

2 x lamp Dry Reeds (makes contacts) mounted in 870 ohm 9-18v coil. Size 3 in. x 3 1/2 in. x 1/2 in. New. Price 8/6 per pair. Post Paid. 6 of the above mentioned units (12 Reeds) fitted in metal box. Size 4 in. x 3 1/2 in. x 1 1/2 in. Mfg. by Elliott Bros. New 45/- each. Post Paid.

Telephone Dials (New) 14/6d. Post Paid.

SOLAR OIL-FILLED CONDENSER

240 mfd. for 230 V.A.C. 600 volt D.C. Overall size 14 in. x 9 in. x 5 1/2 in. plus feet. Weight 46 lb. Guaranteed perfect. Manufacturer's packing. Price £7/10/- Carriage 15/-.



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Step up, step down. 110-200-220-240 v. Fully shrouded. New. 300 watt type, £3 each. P. & P. 4/6. 500 watt type, £4/2/6 each. P. & P. 6/6. 1,000 watt type, £5/5/- each. P. & P. 7/6.

LEVER MICRO SWITCH

Brand new lever operated micro switch. 20 amp. A.C. Price 4/6 each plus 1/6 P. & P. 5 for £1 post paid.



MOVING COIL HEADPHONE AND MIKE

Soft rubber ear-pieces with M/C Mike fitted 5-way plug as on No. 19 set. New, in maker's packing, 16/6, plus 3/6 C. & P.

SEMI-AUTOMATIC "BUG" SUPER SPEED MORSE KEY

7 adjustments, precision tooled, speed adjustable 10 w.p.m. to as high as desired. Weight 2 1/2 lb. £4/12/6 post paid.



NEW MODEL HIGH FREQUENCY TRANSISTORISED MORSE OSCILLATOR

Adjustable tone control. Fitted with moving coil speaker, also earpiece for personal monitoring. Complete with morse key. 45/- plus 3/6d. P. & P.

34R SILICON SOLAR CELL

4 x .5 volt unit series connected, output up to 2 v. at 20 mA. in sunlight, 30 times the efficiency of selenium. As used in power Earth Satellites, 45/- P. & P. 1/6d.

CONDENSERS

New at a fraction of maker's price. 2,500 mfd. 100 v... 12/6 4,000 mfd. 25 v... 10/- 10,000 mfd. 35 v... 15/- 4,000 mfd. 50 v... 15/-

220/240v. A.C. COOLING UNIT

2,300 r.p.m. 6in. blade size. Smooth powerful motor. All metal construction. Continuously rated. Individually tested. Offered at fraction of maker's price, £21/5/- P. & P. 7/6.



100 WATT POWER RHEOSTATS

(NEW) Ceramic construction, winding embedded in Vitreous Enamel, heavy duty brush assembly designed for continuous duty. AVAILABLE FROM STOCK IN THE FOLLOWING 11 VALUES:

- 1 ohm 10a., 5 ohm 4.7a., 10 ohm 3a., 25 ohm 2a., 50 ohm 1.4a., 100 ohm 1a., 250 ohm 7a., 500 ohm 45a., 1,000 ohm 280mA., 1,500 ohm 230mA., 2,500 ohm .2a. Diameter 3 1/2 in. Shaft length 1 1/2 in. dia. 1 1/2 in., 27/6. P. & P. 1/6.
- 50 WATT 1/5/10/25/50/100/250/500/1,000/1,500/2,500 ohm, 21/-, P. & P. 1/6.
- 25 WATT 10/25/50/100/250/500/1,000/1,500/2,500 ohm, 14/6, P. & P. 1/6.

Black Silver Skirted knob calibrated in Nos. 1-9. 1 1/2 in. dia. brass bush. Ideal for above Rheostats, 3/6 each.

STROBE! STROBE! STROBE!

★ TWO EASY TO BUILD KITS USING XENON WHITE LIGHT FLASH TUBES. SOLID STATE TIMING + TRIGGERING CIRCUITS. PROVISION FOR EXTERNAL TRIGGERING. 230-250v. A.C. OPERATION. ★ The Strobe is one of the most useful and interesting instruments in the laboratory or workshop. It is invaluable for the study of movement and checking of speeds. Many uses can be found in the psychiatric and photographic fields, also in the entertainment business. It is used a great deal in the motor industry and is a real tool as well as an interesting scientific device. ★ EXPERIMENTERS "ECONOMY" KIT. 1 to 36 Flash per sec. All electronic components including Veroboard S.C.R. Unijunction Xenon Tube + instructions £5.5/0 plus 5/- P. & P. ★ INDUSTRIAL "ADVANCED" KIT. 1 to 80 Flash per sec. IDEAL FOR LABORATORY OR SCHOOL USE. Fully isolated from the mains supply by specially wound transformer. 500v. FLASH CIRCUIT and stabilised timing circuit. Higher output flash tube. Price £8.8/0 plus 7/6 P. & P. ★ 6 INCH POLISHED REFLECTOR. Ideally suited for above Strobe Kits. Price 8/6 post paid. ★ Regret not sold separately.

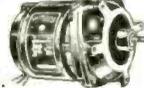
PARVALUX TYPE SD19 230/250 VOLT AC REVERSIBLE GEARED MOTORS

30 r.p.m. 40 lb. ins. Position of drive spindle adjustable to 3 different angles. Mounted on substantial cast aluminium base. Equipment. Tested and in first-class running order. A really powerful motor offered at a fraction of maker's price. 6 gns. P. & P. 10/-.



BODINE TYPE N.C.1 GEARED MOTOR

(Type 1) 71 r.p.m. torque 10 lb. in. Reversible 1/70th h.p. 50 cycle .38 amp. (Type 2) 28 r.p.m. torque 20 lb. in. reversible 1/80th h.p. 50 cycle .28 amp. The above two precision made U.S.A. motors are offered in 'as new' condition. Input voltage of motor 115v A.C. Supplied complete with transformer for 230/240v A.C. Input. Price, either type £2.17.6 plus 6/6 P. & P. or less transformer £2.2.6 plus 4/6d. P. & P. These motors are ideal for rotating aerials, drawing curtains, display stands, vending machines etc.



230/250 v. A.C. SOLENOID

Heavy duty type. Approx. 3lb. pull. 17/6 plus 2/6 P. & P.



12/24 v. D.C. SOLENOID

Approx. 8 oz. push, 8/6 plus 1/6 P. & P.

A.C. CONTACTOR

2 make and 2 break (or 2 c/o) 15 amp. contacts. 230/240 v. A.C. operation. Brand new. 22/6 plus 1/- P. & P.



CT82 NOISE GENERATOR

Ideal for alignment of all types of communication and VHF receivers. Self contained audio output meter and mains power supply. 100Kc/s to 160 Mc/s Frequency range 43 ohm or 75 ohm impedance. Noise figure range to 20 db. In rugged alloy case with instructions for use. Offered untested but in excellent condition, less mains lead. £7/19/6, P. & P. 10/-.



Latest American. New. Plastic THYRISTOR

400 P.I.V. 8 amp. Data sheet. 19/6 post paid.

COPPER LAMINATE PRINTED CIRCUIT BOARD

Large sheet 15 1/2 x 5 1/2 in. 3 for 10/- post paid. (3 minimum order).

MINIATURE UNISELECTOR



3 banks of 11 positions, plus homing bank. 40 ohm coil. 24-36 v. D.C. operation. Carefully removed from equipment and tested. 22/6, plus 2/6 P. & P.

UNISELECTOR SWITCHES

NEW 4 BANK 25 WAY

25 ohm coil, 24 v. D.C. operation. £5/17/6, plus 2/6 P. & P.



8-BANK 25-WAY FULL WIPER

24 v. D.C. operation, £7/12/6. Plus 4/- P. & P.

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BULK PURCHASE ENABLES US TO OFFER THE FOLLOWING NEW SIEMENS PLESSEY, etc. MINIATURE PLUG IN RELAYS COMPLETE WITH BASE, AT A FRACTION OF MAKER'S PRICE



COIL	WORKING VOLTAGE	CONTACTS	PRICE
280	6-12	2 c/o	14/6
280	9-18	4 c/o	15/6
700	12-24	2 c/o	12/6
700	16-24	4 c/o	15/6
700	16-24	4M 2B	12/6
1250	20-40	2 c/o Heavy Duty	12/6
2500	30-50	2 c/o Heavy Duty	12/6
5800	50-70	4 c/o	10/-
9000	40-70	2 c/o	10/-

POST PAID

SEALED RELAY

230 VOLT AC COIL Two c/o 5 amp contacts. Plug-in I.O. Base. Price 14/6d. incl. base. Post Paid. Three c/o 5 amp contacts. 17/6. incl. base. Post Paid.



SANGAMO WESTON

Dual range voltmeter. 0-5 and 0-100 v. D.C. FSD 1 mA. In carrying case with tests prods and leads. 32/6. P. & P. 3/6.



A.C. AMMETERS 0-1, 0-5, 0-10, 0-15, 0-20 amp. F.R.

2 1/2 in. dia. All at 21/- each.

A.C. VOLTMETERS 0-25 v., 0-50 v., 0-150 v. M.I.

2 1/2 in. Flush round all at 21/- each. P. & P. extra.

0-300 v. A.C. Rect. M-Coil 2 1/2 in. 29/-

0-300 v. A.C. Rect. M-Coil 3 1/2 in. Type W23 55/-

'AVO' METER MODEL 7

Supplied fully checked and tested on all ranges and in excellent condition. Complete with batteries and leads. Price £13/10/- P. & P. 7/6d. Avo Leather Carrying Case 30/- (Regret not sold separately)



'AVO' METER MODEL 47A

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	Q81202 18/-	U801 19/6	X76M 7/6	5B285M40/-	6B8G 2/6	6F62 2/6	30PL39 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B286M40/-	6B8G 2/6	6F63 2/6	30PL40 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B287M40/-	6B8G 2/6	6F64 2/6	30PL41 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B288M40/-	6B8G 2/6	6F65 2/6	30PL42 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B289M40/-	6B8G 2/6	6F66 2/6	30PL43 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B290M40/-	6B8G 2/6	6F67 2/6	30PL44 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B291M40/-	6B8G 2/6	6F68 2/6	30PL45 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B292M40/-	6B8G 2/6	6F69 2/6	30PL46 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B293M40/-	6B8G 2/6	6F70 2/6	30PL47 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B294M40/-	6B8G 2/6	6F71 2/6	30PL48 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B295M40/-	6B8G 2/6	6F72 2/6	30PL49 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B296M40/-	6B8G 2/6	6F73 2/6	30PL50 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B297M40/-	6B8G 2/6	6F74 2/6	30PL51 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B298M40/-	6B8G 2/6	6F75 2/6	30PL52 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B299M40/-	6B8G 2/6	6F76 2/6	30PL53 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B300M40/-	6B8G 2/6	6F77 2/6	30PL54 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B301M40/-	6B8G 2/6	6F78 2/6	30PL55 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B302M40/-	6B8G 2/6	6F79 2/6	30PL56 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B303M40/-	6B8G 2/6	6F80 2/6	30PL57 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B304M40/-	6B8G 2/6	6F81 2/6	30PL58 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B305M40/-	6B8G 2/6	6F82 2/6	30PL59 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B306M40/-	6B8G 2/6	6F83 2/6	30PL60 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B307M40/-	6B8G 2/6	6F84 2/6	30PL61 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B308M40/-	6B8G 2/6	6F85 2/6	30PL62 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B309M40/-	6B8G 2/6	6F86 2/6	30PL63 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B310M40/-	6B8G 2/6	6F87 2/6	30PL64 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B311M40/-	6B8G 2/6	6F88 2/6	30PL65 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B312M40/-	6B8G 2/6	6F89 2/6	30PL66 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B313M40/-	6B8G 2/6	6F90 2/6	30PL67 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B314M40/-	6B8G 2/6	6F91 2/6	30PL68 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B315M40/-	6B8G 2/6	6F92 2/6	30PL69 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B316M40/-	6B8G 2/6	6F93 2/6	30PL70 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B317M40/-	6B8G 2/6	6F94 2/6	30PL71 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B318M40/-	6B8G 2/6	6F95 2/6	30PL72 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B319M40/-	6B8G 2/6	6F96 2/6	30PL73 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B320M40/-	6B8G 2/6	6F97 2/6	30PL74 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B321M40/-	6B8G 2/6	6F98 2/6	30PL75 14/-
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	Q81202 18/-	U801 19/6	X76M 7/6	5B325M40/-	6B8G 2/6	6F102 2/6	30PL79 14/-
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	Q81202 18/-	U801 19/6	X76M 7/6	5B327M40/-	6B8G 2/6	6F104 2/6	30PL81 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B328M40/-	6B8G 2/6	6F105 2/6	30PL82 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B329M40/-	6B8G 2/6	6F106 2/6	30PL83 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B330M40/-	6B8G 2/6	6F107 2/6	30PL84 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B331M40/-	6B8G 2/6	6F108 2/6	30PL85 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B332M40/-	6B8G 2/6	6F109 2/6	30PL86 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B333M40/-	6B8G 2/6	6F110 2/6	30PL87 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B334M40/-	6B8G 2/6	6F111 2/6	30PL88 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B335M40/-	6B8G 2/6	6F112 2/6	30PL89 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B336M40/-	6B8G 2/6	6F113 2/6	30PL90 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B337M40/-	6B8G 2/6	6F114 2/6	30PL91 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B338M40/-	6B8G 2/6	6F115 2/6	30PL92 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B339M40/-	6B8G 2/6	6F116 2/6	30PL93 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B340M40/-	6B8G 2/6	6F117 2/6	30PL94 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B341M40/-	6B8G 2/6	6F118 2/6	30PL95 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B342M40/-	6B8G 2/6	6F119 2/6	30PL96 14/-
	Q81202 18/-	U801 19/6	X76M 7/6	5B343M40/-	6B8G 2/6	6F120 2/6	30PL97 14/-
	Q81202 18/-	U801 19/6	X76M				

1. ULTRASONIC CLEANERS



(Burndept B.E.352) 60 watt model. Supplied Brand New complete with stainless steel tank 9½ x 6½ x 4½ in. £60. Carr. 20/-.

2. FAST NEUTRON MONITORS (Burndept 1407C) for measuring neutrons in the energy range 0.15-15 meV. £100.

3. Radiation Monitors (Burndept BN 110 MK. V) 0-5/50/500/5k c.p.s. Brand new. £100. Alpha and Beta Gamma probes available at extra cost.

4. PORTABLE RADIATION MONITORS (Burndept BN 132) 0-5/50/500/5k c.p.s. With built-in Gamma probe. Brand new. £50 complete with carrying harness.

S.A.E. for literature. 10% discount for Educational Authorities.

LARGE CAPACITY ELECTROLYTICS. 2,000 µF. 30v.; 2,500 µF. 25v.; 2,500 µF. 50v.; 4,000 µF. 90v.; 5,000 µF. 25v.; 7/6 ea. 5,000 µF. 50v.; 10,000 µF. 30v.; 16,000 µF. 10v. 10/- ea. p.p. 1/-.

SPEAKER BARGAINS. E.M.I. 13x8 in. with double Tweeters 15 ohm, 65/-, P.P. 5/-. As above less tweeters 3 or 15 ohm, 45/- ea., P.P. 5/-.

FANE 12 in. 20 watt (Dual Cone), 95/-, P.P. 5/-.

CAR RADIO SPEAKER 7 x 4 in. 3/5 ohm. 15/- ea. P.P. 2/6

EXTRACTOR/BLOWER FANS (Papst)



100 c.f.m. 4½ x 4½ x 2 in.
2800 r.p.m. Wonderful buy at 50/- ea. 240v. A.C.

SPEAKER SYSTEM (20x10x10 in.). Made to spec. from ½ in. board. Finished in black leathercloth. 13x8 in. speaker with twin tweeters complete with cross-over. 50c/s-20k/c. £7.10. P.P. 10/-.

PHOTOMULTIPLIERS 6262 and 6262b. £15 ea.

RELAYS H.D. 2 pole 3 way 10 amp. contacts. 12v.w. 7/6 ea.

LIGHTWEIGHT RELAYS (with dust-proof covers) 4 c/o contacts. 12v. 100 ohm. or 24v. 500 ohm. 7/6 ea.

RE-SETTABLE HIGH SPEED COUNTER (3x1x½ in.) 3 digit. 12/24/48v. (state which), 32/6 ea. P.P. 2/6.

HIGH SPEED MAGNETIC COUNTERS (4x1x1 in.) 4 digit. 6/12v. 24/48v. (state which), 6/6 ea. P.P. 1/-.



MINIATURE KEY SWITCHES. (P.O. Lever Type 1000), centre off. 2 c/o each way. 7/6 ea.

DEAC BATTERY PACKS (5x4½x1½ in.) containing 3 cells giving 4 volts at 5a.h. 35/-, P.P. 5/-.

SOLARTRON PULSE GENERATORS (OPS 100C) 50c/s-1m/c. £60 each. Carriage 50/-.

WOBBULATORS TYPE 210 (Matrix) 0-220 M/c. Sweep width 1/2/5/10/20 m/c. £40. Carriage 30/-.

THYRISTOR LIGHT DIMMERS

500 watt Module 45/-
1000 watt Module 60/-

These modules may be fitted into standard socket boxes and made up into banks as required.

5 kW DIMMERS in metal cabinet £20 ea.



TRANSFORMERS

H.T. TRANSFORMER (Parmeko 'Neptune') Prim. 200/250v. Sec. 350-0-350v. 150 m.a. 6.3v. @ 1/2/6 amp. 35/-, P.P. 5/-, Matching Choke 10h 180 m.a. 12/6.

E.H.T. TRANSFORMER (Parmeko 'Neptune') 3,000v. 280 m.a. £12/10/0. P.P. 50/-.

L.T. TRANSFORMERS Prim. 200/250v. Sec. 0-1/0-3/0-9/0-27v. 30 amp. £7.10. 15 amp. £5. P.P. 15/-.

L.T. TRANSFORMER Prim. 200/250v. Sec. 0/25/35v 30 amp. £7.10. P.P. 20/-.

STEP-DOWN TRANSFORMERS Prim. 200/250v. Sec. 115v. 1.25 amps, 25/- ea. P.P. 5/.

L.T. TRANSFORMERS Prim. 240v. Sec. 8/12/20/25v. 3.5 amp models 20/-; 5 amp model 25/-, P.P. 5/6.

L.T. TRANSFORMERS Prim. 240v. Sec. 14v. 1 amp 10/- ea. P.P. 2/6.

ELECTRIC SLOTMETERS (1/-) 25 amp. L.R. 240v. A.C. 85/- ea. P.P. 5/-.

QUARTERLY ELECTRIC CHECK METERS, 40 amp 240v. A.C., 20/- ea. P.P. 5/-.

COPPER LAMINATE PRINTED CIRCUIT BOARD (8½ x 5½ x ¼ in.), 2/6 sheet. 5 for 10/-, Also 11 x 9 in. 4/- ea., 3 for 10/-.

BULK COMPONENT OFFERS

100 Capacitors (latest types) 50pF to .5µF.
250 Resistors ½ and ¼ watt.
250 Resistors ¼ and 1 watt.
150 HI-Stab Resistors. ½, ¼ and 1 watt.
25 Vitreous W/W Resistors. 5%.
12 Precision Resistors .1% (several standards included).
12 Precision Capacitors 1 and 2% (several standards included).
12 Electrolytics (miniature and standard sizes).
ANY ITEM 12/6. ANY 5 ITEMS 50/-.

TELEPHONE DIALS (New) 20/- ea.

Amplified TELEPHONE HANDSET (706) 27/6. P.P. 2/6.

EXTENSION TELEPHONE (Type 706) Black or 2 tone Grey. 65/-, P.P. 5/-.

UNISELECTORS (Brand new) 25-way 75 ohm. 8 bank ½ wiper 65/-, 10 bank ½ wiper 75/-.



REED RELAYS 4 make 9/12v. (1,000 ohm.) 12/6 ea. 2 make 7/6 ea. 1 make 5/- ea. Reed Switches (1½ in.) 2/- ea. £1 per doz.

CONTINUOUS LEVEL MONITORS (Burndept BE307) complete with Sensing Probe. £25.

Transistorised PROXIMITY SWITCHES (Burndept BE315) sensing speed 120 per min. £16.

LEVEL CONTROLLER (Burndept BE305). £8.

LIGHT SWITCH. COUNTER. (Burndept BE290) 750 Interruption per min., comprises: Light Source, Sensing Head, Control Unit. £15.

S.A.E. Literature.

COLD CATHODE TUBES (Hivac XC25) 2/- ea. Quantity quotations on request.

PATRICK & KINNIE
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LATEST RELEASE OF
RCA COMMUNICATION RECEIVERS AR88



BRAND NEW and in original cases—A.C. mains input. 110V or 250V. Freq. in 6 bands 535 Kc/s-32 Mc/s. Output impedance 2.5-600 ohms. Complete with crystal filter, noise limiter, B.F.O., H.F. tone control, R.F. & A.F. variable controls. Price £87/10/- each, carr. £2.

Same model as above in secondhand cond. (guaranteed working order), from £45 to £60, carr. £2.

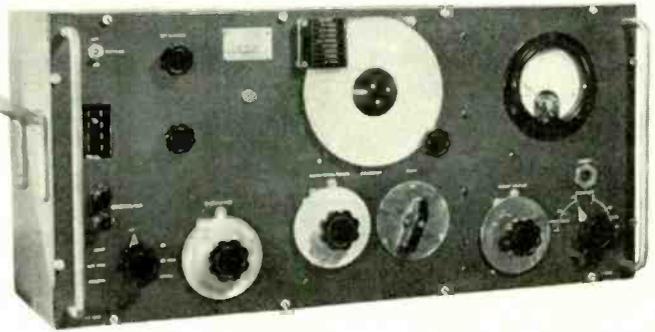
***SET OF VALVES:** new, £3/10/- a set, post 7/6; **SPEAKERS:** new, £3 each, post 10/-; ***HEADPHONES:** new, £1/5/- a pair, 600 ohms impedance. Post 5/-.

AR88 SPARES. Antenna Coils L5 and 6 and L7 and 8. Oscillator coil L55. Price 10/- each, post 2/6. RF Coils 13 & 14; 17 & 18; 23 & 24; and 27 and 28. Price 12/6 each. 2/6 post. By-pass Capacitor K.98034-1, 3x0.05 mfd. and M.980344, 3x0.1 mfd., 3 for 10/-, post 2/6. Trimmers 95534-502, 2-20 p.f. Box of 3, 10/-, post 2/6. Block Condenser, 3x4 mfd., 600 v., £2 each, 4/- post. Output transformers 901666-501 27/6 each, 4/- post.

* Available with Receiver only.

S.A.E. for all enquiries. If wishing to call at Stores, please telephone for appointment.

MARCONI SIGNAL GENERATORS
TYPE TF-144G



Freq. 85Kc/s-25Mc/s in 8 ranges. Incremental: +/— 1% at 1Mc/s. Output: continuously variable 1 microvolt to 1 volt. Output Impedance: 1 microvolt to 100 millivolts, 10 ohms 100mV-1 volt-52.5 ohms. Internal Modulation: 400 c/s sinewave 75% depth. External Modulation: Direct or via internal amplifier. A.C. mains 200/250V, 40-100 c/s. Consumption approx. 40 watts. Measurements: 19½ x 12½ x 10 in. The above come complete with Mains Leads, Dummy Aerial with screened lead, and plugs. As New, in Manufacturer's cases, £40 each. Carr. 30/-.

DISCOUNT OF 10% FOR SCHOOLS, TECHNICAL COLLEGES, etc.

W. MILLS 3-B TRULOCK ROAD, TOTTENHAM, N.17
Phone: Tottenham 9213

HRO RECEIVER. Model 5T. This is a famous American High Frequency superhet, suitable for CW, and MCW, reception crystal filter, with phasing control. AVC and signal strength meter. Freq. range 50 kc/s. to 30 mc/s., with set of nine coils. Complete HRO 5T SET (Receiver, Coils and Power Unit) for £30, plus 30/- carr.

COMMAND RECEIVERS; Model 6-9 Mc/s., as new, price £5/10/- each, post 5/-.

COMMAND TRANSMITTERS, BC-458: 5.3-7 Mc/s., approx. 25W output, directly calibrated. Valves 2 x 1625 PA; 1 x 1626 osc.; 1 x 1629 Tuning Indicator; Crystal 6,200 Kc/s. New condition—£3/10/- each, 10/- post.

(Conversion as per "Surplus Radio Conversion Manual, Vol. No. 2," by R. C. Evenson and O. R. Beach.)

AIRCRAFT RECEIVER ARR. 2: Valve line-up 7 x 9001; 3 x 6AK5; and 1 x 12A6. Switch tuned 234-258 Mc/s. Rec. only £3 each, 7/6 post; or Rec. with 24 v. power unit and mounting tray £3/10/- each, 10/- post.

ROTARY CONVERTERS: Type 8a, 24 v D.C., 115 v A.C. @ 1.8 amps, 400 c/s 3 phase, £6/10/- each, 8/- post. Converter 12 v D.C. input, 110 v A.C., 60 c/s @ 2.73 amps, 0.300 Kva, £15 each, carr. £1. 24 v D.C. input, 175 v D.C. @ 40mA output, 25/- each, post 2/-.

CONDENSERS: 150 mfd, 300 v A.C., £7/10/- each, carr. 15/-, 40 mfd, 440 v A.C. wkg., £5 each, 10/- post. 30 mfd, 600 v wkg. D.C., £3/10/- each, post 10/-, 15 mfd, 330 v A.C. wkg., 15/- each, post 5/-, 10 mfd, 1000 v, 12/6 each, post 2/6, 10 mfd, 600 v, 8/6 each, post 5/-, 8 mfd, 1200 v, 12/6 each, post 3/-, 8 mfd, 600 v, 8/6 each, post 2/6, 4 mfd, 3000 v wkg., £3 each, post 7/6, 2 mfd, 3000 v wkg., £2 each, post 7/6, 0.25 mfd, 32,000 v, £7/10/- each, carr. 15/-, 0.25 mfd, 2Kv, 4/- each, 1/6 post. 0.01 Mfd. MICA 2.5Kv. Price £1 for 5. Post 2/6.

AVO MULTIRANGE No. 1 ELECTRONIC TEST SET: £25 each, carr. £1.

OSCILLOSCOPE Type 13A, 100/250 v. A.C. Time base 2 c/s.-750 Kc/s. Bandwidth up to 5 Mc/s. Calibration markers 100 Kc/s. and 1 Mc/s. Double Beam tube. Reliable general purpose scope, £22/10/- each, 30/- carr.

COSSAR 1035 OSCILLOSCOPE, £30 each, 30/- carr.

RELAYS: Relay Unit (with 9 American relays) 24 v. D.C., 250 ohm coils, heavy duty, M. & B. 30/- each, 4/- post. GPO Type 600, 10 relays @ 300 ohms with 2M and 10 relays @ 50 ohms with 1M., £2 each, 6/- post. 12 Small American Relays, mixed types £2, post 4/-.

CALIBRATION TACHOMETER Mk. II: Maxwell Bridge Type 6C/869, £25 each, £2 carr.

ROTAX VARIAC & METER UNIT: Type 5G.3281. Reading 0-40 v., 0-40 mA and 0.5 amps., all on 275 deg. scales, £30 each, £2 carr.

HEWLETT PACKARD TYPE 400C: 115 v./230 v. input 50/60 c/s. Freq. range 20 c/s-2 Mc/s. Voltage range: 1mV-300 v. in 12 ranges. Input impedance 10 megohms. Designed for rack mounting, £30 each, carr. 15/-.

TCS MODULATION TRANSFORMERS, 20 watts, pr. 6,000 C.T., sec. 6,000 ohms. Price 25/-, post 5/-.

AUTOMATIC PILOT UNIT Mk. 2. This complex unit of diodes and valves, relays, magnetic clutches, motors and plug-in amplifiers, with many other items, price £7/10/-, £1 carriage.

FOR EXPORT ONLY: B.44 Transceiver Mk. III. Crystal control, 60-95 Mc/s. **AMERICAN EQUIPMENT:** BC-640 Transmitter, 100-156 Mc/s., 50 watt output. For 110 or 230 v. operation. ARC 27 transceivers, 28 v. D.C. input. Also have associated equipment. BC-375 Transmitter, BC-778 Dinghy transmitter. SCR-522 transceiver. Power supply, PP893/GRC 32A; Filter D.C. Power Supply F-170/GRC 32A; Cabinet Electrical CY 1288/GRC 32A; Antenna Box Base and Cables CY 728/GRC; Mast Erection Kits, 1186/GRC; Directional Antenna CRD 6; Comparator Unit, CM.23; Directional Control CRD.6, 567/CRD and 568/CRD; Azimuth Control Units, 260/CRD. Test Set URM.44, complete with Signal Generator TS.622/U.

VARIABLE POWER UNIT: complete with Zenith variac 0-230 v., 9 amps.; 24in. scale meter reading 0-250 v. Unit is mounted in 19in. rack, £16/10/- each, 30/- carr.

SOLENOID UNIT: 230 v. A.C. input, 2 pole, 15 amp contacts, £2/10/- each post 6/-.

CONTROL PANEL: 230 v. A.C., 24 v. D.C. @ 2 amps., £2/10/- each, carr. 12/6.

AUTO TRANSFORMER: 230-115 v.; 1,000 w. £5 each, carr. 12/6. 230-115 v.; 300VA, £3 each, carr. 10/-.

OHMITE VARIABLE RESISTOR: 5 ohms, 5½ amps; or 2.6 ohms at 4 amps. Price (either type) £2 each, 4/6 post each.

POWER SUPPLY UNIT PN-12B: 230 v. A.C. input, 395-0-395 v. output @ 300 mA. Complete with two x 9H chokes and 10 mfd. oil filled capacitors. Mounted in 19in. panel, £6/10/- each, £1 carr.

TX DRIVER UNIT: Freq. 100-156 Mc/s. Valves 3 x 3C24's; complete with filament transformer 230 v. A.C. Mounted in 19in. panel, £4/10/- each, 15/- carr.

POWER UNIT: 110 v. or 230 v. input switched; 28 v. @ 45 amps. D.C. output. Wt. approx. 100 lbs., £17/10/- each, 30/- carr. SMOOTHING UNITS suitable for above £7/10/- each, 15/- carr.

DE-ICER CONTROLLER MK. III: Contains 10 relays D.P. changeover heavy duty contacts, 1 relay 4P C/O. (235 ohms coil). Stud switch 30-way relay operated, one five-way ditto, D.C. timing motor with Chronometric governor 20-30 v., 12 r.p.m.; geared to two 30-way stud switches and two Ledex solenoids, 1 delay relay etc., sealed in steel case (4 x 5 x 7 ins.) £3 each, post 7/6.

ALL GOODS OFFERED WHILST STOCKS LAST IN "AS IS" CONDITION UNLESS OTHERWISE STATED

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3-B TRULOCK ROAD, TOTTENHAM, N.17

Phone: Tottenham 9213

ADVANCE TEST EQUIPMENT: VM76 Valve Voltmeter, £78 each; VM78 A.C. Millivoltmeter (transistorised) £55 each; VM79 UHF Millivoltmeter (transistorised) £125 each; J1B Audio Signal Generator £30 each; TT1S Transistor Tester (CT472) £37/10 each. 10 per cent Discount for schools, colleges, etc. on the above items. Carr. 10/-, extra per item.

INDICATOR UNIT TYPE CRT.26: complete with CV1526 Cathode Ray Tube (3EG1). (3 x CV138; 3 x CV329; 1 x CV858; 2 x CV261; 6 x Crystals). Complete with brilliance and focus controls. Suitable for converting into a small oscilloscope (10 x 8 x 6 in., wt. 15 lb.) £5 each. Post 10/-.

NIFE BATTERIES: 6 v. 75 amps., new, in cases, £15 each, £1 carr.; 4 v. 160 amps, new, in cases, £20 each, £1 10/- carr. **L.R.7 Cells,** only 1.2 v. 75 amps., new, £3 each, 12/- carr. The above batteries are low resistance designed to give a heavy surge for starting and can be stored for long periods without any effect to their performance.

FUEL INDICATOR Type 113R: 24 v. complete with 2 magnetic counters 0-9999, with locking and reset controls mounted in a 3in. diameter case. Price 30/- each, postage 5/-.

UNISELECTORS (ex equipment): 5 Bank, 50 Way, 75 ohm Coil, alternate wipe, £2/5/- each, post 4/-

FREQUENCY METERS: LM13, 125-20,000 Kc/s., £25 each, carr. 15/-, TS 175/U, £75 each, carr. £1. TS323/UR, 20-450 Mc/s., £75 each, carr. 15/-, FR-67/U. This instrument is direct reading and the results are presented directly in digital form. Counting rate: 20-100,000 events per sec. Time Base Crystal Freq.: 100 Kc/s. per sec. Power supply: 115 v., 50/60 c/s., £100 each, carr. £1.

CT.49 ABSORPTION AUDIO FREQUENCY METER: freq. range 450 c/s-22 Kc/s., directly calibrated. Power supply 1.5 v.-22 v. D.C. £12/10/- each, carr. 15/-.

CATHODE RAY TUBE UNIT: With 3in. tube, colour green, medium persistence complete with nu-metal screen, £3/10/- each, post 7/6.

APNI ALTIMETER TRANS./REC., suitable for conversion 420 Mc/s., complete with all valves 28 v. D.C. 3 relays, 11 valves, price £3 each, carr. 10/-.

GEARED MOTORS: 24 v. D.C., current 150 mA, output 1 r.p.m., 30/- each, 4/- post. Assembly unit with Letcherbar Tuning Mechanism and potentiometer, 3 r.p.m., £2 each, 5/- post.

Actuator Type SR-43: 28 v. D.C. 2,000 r.p.m., output 26 watts, 5 inch screw thrust, reversible, torque approx. 25 lbs., rating intermittent, price £3 each, post 5/-.

SYNCHROS: and other special purpose motors available. British and American ex stock. List available 6d.

MARCONI NOISE GENERATOR TF-987/1: Used to determine noise factor of a.m. and f.m. receivers. Designed for 230 v. a.c. operation. In used condition, £20 each, carr. £1.

MARCONI TF-956 (CT.44) AUDIO FREQUENCY ABSORPTION WATTMETER; Large clear 6in. scale. 1 microW. to 6W. £25 each. Carr. 15/-.

MARCONI DIVERSITY RECEIVERS; Consisting of 2 x CR.150's and associated equipment. £175 each. Carr. £5.

MARCONI DEVIATION TEST SET TF-934: Freq. 2.5-100Mc/s. Can be extended to 500Mc/s. Deviation range 0-5, 0-25 and 0-65 Kc/s. £35 each, carr. £1.

CANADIAN C52 TRANS/REC.: Freq. 1.75-16 Mc/s on 3 bands. R.T., M.C.W. and C.W. Crystal calibrator etc., power input 12V. D.C., new cond., complete set £50. Used condition working order £25. Carr. on both types £2/10/-, Transmitter only £7/10/- (few only) Carr. 15/-, Power Unit for Rec., new £3/5/-, Used power units in working order £2/5/-, Carr 10/-.

AVOMETERS: Model 47A, £10 each, 10/- post. Model 7, £12/10/- each, 10/- post. Excellent secondhand cond. (Meters only—batteries and leads extra, at cost.)

DECADE RESISTOR SWITCH: 0.1 ohm per step. 10 positions. 3 Gang, each 0.9 ohms. Tolerance ±1% £3 each, 5/- post. 90 ohms per step. 10 positions, total value 900 ohms. 3 Gang. Tolerance ±1% £3/10/- each, 5/- post.

COAXIAL TEST EQUIPMENT: COAXWITCH—Mnfrs. Bird Electronic Corp. Model 72RS; two-circuit reversing switch, 75 ohms, type "N" female connectors fitted to receive UG-21/U series plugs. New in ctns., £6/10/- each, post 7/6. CO-AXIAL SWITCH—Mnfrs. Transco Products Inc., Type M1460-22, 2 pole, 2 throw. (New) £6/10/- each, 4/6 post. 1 pole, 4 throw, Type M1460-4. (New) £6/10/- each, 4/6 post.

TERMALINE RESISTOR UNITS: type 82A/U, 5000W, freq. 0-3.3 KMC Max VSWR 1.2 Type "N" female connectors, etc. Brand new, £30 each, carr. 15/-.

PRD Electronic Inc. Equipment: STANDING WAVE DETECTOR: Type 219, 100-1,000 Mc/s. (New) £65 each, post 12/6. FREQUENCY METER: Type 587-A, 0.250-1.0 KMC/SEC. (New) £75 each, post 12/6. FIXED ATTENUATOR: Type 130c, 2.0-10.0 KMC/SEC. (New) £5 each, post 4/-. FIXED ATTENUATOR: Type 1157S-1, (new) £6 each, post 5/-.

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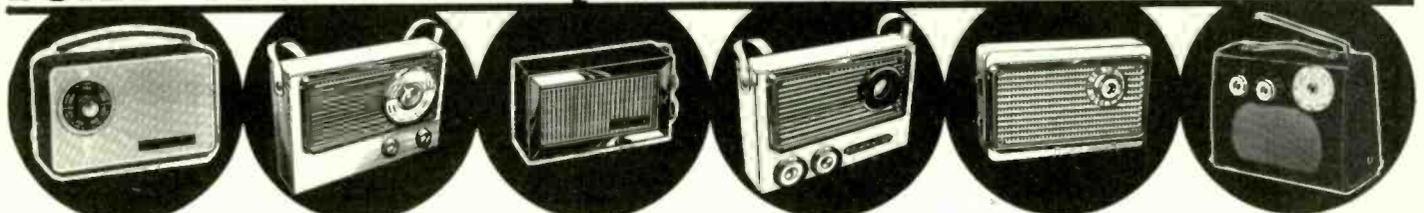
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Bulk Purchase. Famous manufacturer. Must have cost nearly £40 each. Input 200/250 volts 50c/a.c. Output 250 volts d.c. at approx. 170mA. 6.3/12 volts at approx. 4 amps a.c. Robust metal rack mounting cabinet, size approx. 19 x 15 x 8in. Price only 85/-, carriage and insurance 15/-. All units are fully fused and metered.

SMOOTHING UNITS

Beautifully made pieces of equipment. 12 volts or 24 volts d.c. input gives a fully smoothed fully regulated d.c. output. Worth £30 each. Robust metal cabinet with provision for standby battery. Brand new in maker's cartons. Price 65/-, p. & p. 10/-.

MORSE PRACTICE OSCILLATOR SET

Complete with "Hints on Learning Morse" manual. Fully Transistorised. 19/6. p. & p. 3/6.

COMMUNICATIONS RECEIVER

TYPE T.R.G.D.X/20.C.

Brand new fully transistorised and fully portable Communications Receiver. Specifications: 4 complete ranges 550 K/ca. to 30 Mc/a, covering all amateur bands, shipping and trawler bands, and broadcast band. A highly efficient double tuned superhet, comprising R/F aerial tuning section, A.V.C. and built in B.F.O. Ideal for fixed or mobile reception. With speaker and headphone output. Hammer finished robust steel case of pleasing modern design. Size approx. 9 x 7 x 6in. British manufacture. Due to bulk purchasing we can offer these excellent receivers at less than half their normal worth. Complete with handbook. £18.10.0. carriage and insurance 15/-. Headphones £ required 17/6 extra. 2/6 p. & p.

SURPLUS BARGAINS

HEAVY DUTY ACCUMULATORS

Type 1 (6 volt) 40A.H. In metal cabinet. Size approx. 10 x 9 x 6in. Complete with output socket, carrying strap. Brand new and unused. Worth £10 each. Our price 55/-, carriage and insurance 15/-. Type 2 (6 volt) 16A.H. In sturdy wooden cabinet with carrying strap. Worth £7 each. Brand new and boxed, only 32/6 each, p. & p. 12/6.

FIELD TELEPHONES

Type F. Housed in a portable wooden case. Ideal for indoor/outdoor communication up to 10 miles. Absolutely brand new. Price only £5.19.6 per pair, carriage and insurance 15/-.

19 Set Headphones and Mike. Not new but in working order. Only 7/6 per set, p. & p. 4/6.

Tanny Mikes. As new, 9/6 each, p. & p. 3/6. (Heavy duty, ideal for P.A. work.)

High Quality moving coil headphones and mike. Brand new, only 17/6. p. & p. 5/6. Suitable for most applications (cost approx. £3 per pair).

AIRCRAFT-PLUS GENERAL TELECOMMUNICATIONS BAND REC.

Listen to the thrills of Aircraft, Pilots, and Airports at work. Also Civil Depts., Fire and Ambulance services. Gas and Electricity Depts. Ideal for receiving 2 metre amateurs. Gives super reception within the range of all transmissions. A fully transistorised receiver covering 37-150mc/a V.H.F. broadcast. Robust attractive finished metal cabinet size approx. 7 x 4 x 4ins. Operates from a 9 volt internal battery. Speaker or earphone output. Simple to use. Available from us at the pre-devaluation price of £8.19.6. carriage and insurance 10/6. CWG or COD.

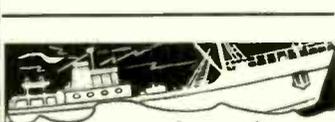
BATTERY ELIMINATORS AND STABILISED POWER PACKS

The most economical method of running transistorised equipment from A.C. mains. Power radion, record players, etc. Mark 1 model: replaces all 9 volt batteries. Price only 35/-, p. & p. 5/-. Mark 2 model: output 6.7 and 9 V. STABILISED, making it ideal for running Hi-Fi and test gear and cassette type tape recorders. Price only 85/-, p. & p. 5/-.
LOUDSPEAKER UNIT SALE
 Famous manufacture 8in. Moving Coil 10 watt Loudspeakers. In Wooden Cabinet. Not brand new but in good condition. Only 50/- each, p. & p. 10/-. Two speakers for £4.10.0. post free.

LOUDSPEAKER UNIT SALE

Famous manufacture 8in. Moving Coil 10 watt Loudspeakers. In Wooden Cabinet. Not brand new but in good condition. Only 50/- each, p. & p. 10/-. Two speakers for £4.10.0. post free.

10 Henry (60 m.a.) SMOOTHING CHOKES. Only 3/6 each, p. & p. 1/-. Four for 15/-, post free.



SHIPPING/S.O.S. BAND RECEIVER

Now incorporates the full coverage of 80/160 meters amateur bands. Listen to the world's shipping, Hams at work. Covers the complete Maritime and Trawler Band. Plus Top Band and 90 m. Attractive hammer finish case, size approx. 7 x 5 x 5in. A neat little superhet. Fully transistorised, works from 9 volt battery. Speaker or earphone output. Brand new from makers. Price £9.10.0. carr. & insur. 10/-.

RUN YOUR 19 SET TX/RX FROM AC MAINS.

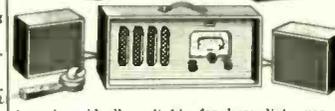
We manufacture a brand new unit ready to operate all 19 set Trans/Rec. direct from the mains. Complete ready to plug in with full connecting instructions. Contained in an attractive steel cabinet. Price £8.10.0. carr. & insur. 10/-. Receiver version only, £4.10.0. carr. & insur. 5/-.

12v. MULTI-PURPOSE Switching Relay



One of the most versatile relays ever made. Operates from 6 volt or 12 volt A.C. or D.C. Consists of one pair of heavy duty D.P.D.T. contacts which are ideal for switching up to 20 amps. Plus many low current switching contacts. Metal base-plate. Eboutie terminal block. Ideal for aerial changeover units. Car or house burglar alarms, model railways etc. Worth nearly £3 each. Size only 3 x 2 1/2in. approx. Special price of 17/6 each, p. & p. 2/6. Two for 30/-, post free.

FACTORY RADIO PLUS STAFF INTERCOM



A system ideally suitable for immediate use in factories, workshops, garages, schools and hospitals. Incorporates Radio, covering M.W. broadcasts plus staff communication amplifier. The master unit is contained in a robust cabinet with full controls. Two slave units are supplied, additional ones may be added if required. Press/Talk microphone supplied for staff messages. Operates from 240v A.C. mains. A 6v input model for portable use is also available. As used in Government departments. Worth over £25. Our price, in excellent condition, £13.10.0. carriage and insurance 30/-.

RADIATION METERS. Dosimeter type. Q.F. No. 4. Mk. 3. Brand new in maker's cartons. 55/- each, carriage 5/-, Two for £5.10.0. post free.

G.P.O. TELEPHONE HANDSETS. Brand new with lead, in maker's cartons. 25/- each, p. & p. 5/-.

AIR/SEA TRANS/REC. RESCUE

Compact V.H.F. Trans/Rec. Fits in the pocket. Consists of Mike/Speaker, amplifier, aerial, transmitter and receiver. Were made to operate up to 100 miles depending on terrain. Operates from dry batteries. Completely self-contained. Cost Govt. over £50 each. Regulations state must not be operated in UK so please mention "For Dismantling purposes only" when ordering. Price £2.10.0 each, p. & p. 10/-. Two sets for £5.0.0. post free. Four sets £8, carriage free. Bulk sale of 10 sets £2.5, carriage £1. Export enquiries invited.



MINIATURE MOVING COIL SPEAKERS

1 1/2in. diameter. Only 3/6 each, p. & p. 1/6. Two for 8/6 post free. Four for 15/- post free.

MATCHING P.S.U. For R1132 and 1392 Receivers. Only £3.10.0 each, carriage 10/-. Absolutely brand new in maker's cartons.

HANDY MAINS POWER SUPPLY UNIT

Input 240 volts A.C. Output 250 volts 80 mA. D.C. 0.5V. at 2 amps plus 12 volts at 2 amps. Built on a robust compact chassis. Containing double isolated transformers, smoothing chokes, capacitors and Silicon rectifiers. Built up with full instructions. Only 25/-, plus 5/- carriage.

WHIP AERIALS. One foot interlocking sections. Only 2/6 each. Four for 7/6. p. & p. 2/6. Eight for 15/-, post free.

CAR BATTERY CHARGER PLUS ELECTRONIC FAULT TRACING UNIT

A good start in 1969. Heavy Duty charger for 6/12v. batteries. Combines circuit tester, ignition checker and faultfinder. Cuts repair costs, easy view ammeter, calibrated 0-7, with overload indicator, full accessories plus free faultfinding guide. Insulated, fused and earthed for safety. Ideal home/industrial use. Robust metal cabinet, functional control panel. Should be 6 gns. Genuine bankrupt stocks. Now offered at 22/6 each, p. & p. 7/6. Trade enquiries invited.

ROBUST METAL BOXES

These Superb 20 SWG steel cases are complete with hinged lid and clasp. Made to rigid Govt. specifications. Cost over £3 each to make. Size approx. 7 x 7 x 6in. Hammer finished. Complete with carrying handle. Ideal for Bait Boxes, Tool Boxes, Instrument Cases, Lunch Boxes. Huge purchase of 7,500 enables us to offer them at only 8/6 each, carriage 3/6. Three for 25/- post free. Six for £2 carriage 5/-. One dozen £4 carriage free. Special prices

TRANSISTOR SALE

OC44 1/6 each, p.p. 4d. Three for 5/- post free.
 OC72 1/6 each, p.p. 4d. Three for 5/- post free.
 OC71 1/3 each, p.p. 4d. Three for 4/8 post free.
 OC45 1/3 each, p.p. 4d. Three for 3/6 post free.
 OC81 2/- each, p.p. 4d. Three for 5/- post free.
 BCY 95a 3/6 each, p.p. 4d. Three for 10/- post free.
 BC108/107 4/6 each, p.p. 4d. Three for 12/6 post free.
 2N706 2/6 each, p.p. 4d. Three for 6/6 post free.
 2N2926 2/- each, p.p. 4d. Three for 5/- post free.
 BSV27 300 m/cs silicon 7/6 each, p.p. 4d. Three for £1 post free.

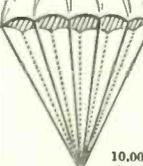
RECTIFIER SALE

6/12 volt full wave bridged, 4 amps. Brand new manufacturers surplus, only 4/6 each, p. & p. 1/6. Two for 10/-, post free. Four for 15/-, post free. £2 per dozen, post free.

NEW SHOP NOW OPEN at

38 Bridge End, Meadow Lane, Leeds 1. Open 9 p.m. to 6 p.m. weekdays and Saturdays. All goods advertised available for inspection and demonstration. The North's newest walk-round Scientific and Electronic Store.

PARACHUTES



Again we have pulled off another scoop purchase. Brand new parachutes direct from the War Dept. Must have cost over £25 each. Highest quality manufacture. Lift. dia. giving over 100 sqft. in area. Complete with cords, etc. Thousands of uses. Over 10,000 already sold. Unobtainable elsewhere at the ridiculous price of 50/- each, p. & p. 10/-. or two for £5. post free. Five for £12.10.0. post free. £22.10.0 a dozen, post free.

RECEIVE MORSE C.W./SSB ON ANY RECEIVER

This miniature fully transistorised tunable B.F.O. will be a valuable addition to any receiver. A compact unit with single hole fixing that will fit anywhere. Ideal for all Ex-Govt. and commercial receivers. Complete with installation instructions. 49/6 post free.

COLLAPSIBLE AERIAL IN 5 SECTIONS CLOSED 13' OPEN 5' 6"

A fully adjustable highly efficient whip aerial. Made to exacting specifications. Copper plated sections. Brass base. An ideal aerial for TX/RX use. Easily adaptable for cars, scooters, walkie talkies, etc. Only £1 each, post and packing 2/6. Two aerials for 35/-, post free.

RUN TELEVISION-LIGHTING DRILLS ETC-ETC from a 12 VOLT CAR BATTERY



A superbly designed POWER CONVERTER (de-luxe model). A 12-volt INPUT gives a 200/240 volt OUTPUT. Enables you to run up to 220 watt AC/DC TELEVISION lighting and equipment. Thousands of uses. Indispensable to caravaners, Workshops and Garages. The unit is contained in a compact louvered steel case. Complete with connecting leads, battery clips and full instructions. Ready to connect up and use. Our price while stocks last £6/19/6, carriage 12/6. C.O.D. 3/6 extra.

VALVE SALE

807-8/- each, three for 18/-, 6V6-3/- each, three for 7/-, 6K7-2/- each, three for 5/-, 6K8-5/- each, three for 12/6, EP50-1/8 each, three for 5/-, 6H6-2/6 each, three for 6/-, 0Z4-9d, each, three for 2/-. Three valves post free, otherwise 9d. P. & P. All Valves guaranteed and insured in transit.

SCOOP PURCHASE TRANSFORMER SALE

Bulk purchase enables us to offer the following transformers at a ridiculously low price. Made by a famous manufacturer and fully tested and guaranteed. CHARGER TRANSFORMERS, 0-9.15 volts, 2 amp. 9/6 each, p.p. 2/6. Two for 17/6 post free. TRANSISTOR POWER PACK TYPES, 6.3v. at 2 amps. 5/6 each, p.p. 2/-. 12 volt at 2 amp. 12/6 each, p.p. 2/6.

All Mail Orders to
GLOBE SCIENTIFIC LTD
 DEPT. WW24, CAWOODS YARD,
 MILL STREET, MARSH LANE, LEEDS 9.

P. F. RALFE

Please Note our New Address is Now

10 Chapel St London N.W.1 Phone 01-723 8753

SPECIALISED EQUIPMENTS

MARCONI TF 890A/4. Of special interest to microwave engineers, the instrument comprises several X-Band measuring functions for checking 3 cm equipments. It combines in one compact unit a C.W.-F.M. Klystron Signal Generator, a Wave Meter, a Power Meter, and Spectrum Analyser. With C.R.T. display. This equipment is complete with all accessories, in functional order and offered in nearly new condition. List Price over £1,000. Our Price £275.

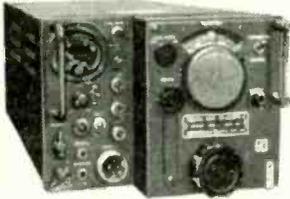
HEWLETT PACKARD RF. POWER METER—Type 431B

Measures RF. power in 7 ranges, from 0.01 MW to 10 MW. This instrument is fully completely solid state, small portable, current series equipment. Mains or battery powered C/W thermistor mount either 478A 10 Mc/s to 10 K.Mc/s. Supplied in good used condition at £60. Extra for the thermistor mounts.

SPECTRUM ANALYSER TS-148/UP

This instrument is a portable unit used in testing the over-all system performance of micro wave systems, it also checks the frequency of TR cells and RT boxes, signal generators, local oscillators and magnetrons, also pulse width, RF. spectrum width and the Q of resonance cavities. For 115 volts A.C. 50 c/s. Mains transformer supplied. Price £125.

AN/APR4 VHF COMMUNICATIONS AND SEARCH RECEIVERS



Frequency range 38-1,000 Mc/s. Accuracy 1%. Five I.F. stages. Output impedance 600 or 4,000 ohms. Power supply 115 volts A.C. (internal). Price complete with three tuning units £90. All tuning units have Auto Tune Mechanism.

WAVE ANALYSER—AIRMEC Type 853

Frequency range 300 Kc/s-30 Mc/s. This instrument particularly suitable for the evaluation of harmonics and components of a complex waveform, also suitable for field strength and interference measurements, insertion loss, and as Heterodyne Wave-meter. Offered in excellent condition at 50% of List Price.

F.M. MONITOR TYPE 1170 GENERAL RADIO

This monitor gives a continuous indication of centre-frequency and percentage modulation of F.M. receivers, also output for measuring distortion and noise, and 600 ohm output for audio monitoring. The monitor is designed to operate between 30 and 900 Mc/s, 100% mod corresponds to ± 25 Kc deviation. Input 1 volt R.F. or better. I.F.: 150 Kc, 140 Kc or 160 Kc. Centre frequency indication -6 Kc to +6 Kc. Good used condition. Price £95.

MARCONI DOUBLE-PULSE GENERATOR Type TF 1400

This instrument is offered as new with TM6600 plug-in at £155. Original price £335.

MARCONI DUAL TRACE PLUG-IN Type 6456

For use with Marconi oscilloscope TF 2200 etc. As new. Price £38.

MARCONI V.T.V.M.—Type 1041C

These highly sensitive and well known instruments are offered in first-class operative condition. Specification is seven A.C. ranges, 300 Mv to 300 volts f.s.d.; eight D.C. ranges, 300 Mv to 1,000 volts f.s.d.; eight resistance ranges, 50 ohms to 500 Mohms. Multipliers for 2 Kv A.C. and 30 Kv D.C. Frequency response 20 c/s to 1,500 Mc/s. Price, C/W leads, etc.£45

BRADLEY RF MILLIVOLTMETER Type 112

A precision instrument, fully transistorised and portable with dual input facility. Specification is: direct measurement of RF voltage between 0.5 Mv and 300 Mv. RMS source impedance matched to 50 ohms. The instrument can also be used as a sensitive null detector. Battery powered, offered in as new condition at£30

Goodman's Industries POWER OSCILLATOR Type D120

Frequency range 10 c/s to 100 Kc/s in three directly calibrated ranges, power output 1,000 watts, supply 240 volts A.C., as new condition. Price £125, carriage at cost.

INDUSTRIAL POWER AMPLIFIERS

Output 175 watts can be supplied with variable frequency oscillator 10 c/s to 14 Kc/s. C/W all usual facilities for 19in. rack mounting, supply volts 250 volts A.C. Price.....£49/10/0
HIVOLT PORTABLE E.H.T. GENERATOR Variable output from 0 to 10 Kv D.C., Megohms range 200 to 10⁵. A small modern completely portable instrument. Fully transistorised C/W batteries. Weight complete 21 lbs. New condition£35

ENGLISH ELECTRIC INSULATION TESTERS

Type TD5443/2-0-10 Kv with variable current control and ionisation amplifier. Small portable unit for A.C. mains operation. Price£30

DIGITAL VOLTMETERS!



Digimeter Type B.I.E. 2123 is a fully transistorised multi-range instrument possessing the following distinctive features:

Electrical Characteristics:
D.C. Ranges: 10 Mv to 400 volts in four ranges (1,000 volts for positive voltages). Accuracy: the greater of $\pm 0.1\%$ of ± 1 digit.
A.C. Ranges: 100 Mv to 250 volts RMS in three ranges.
Brand new with handbook£92/10/0

REFLECTOMETERS BY A.T.E.

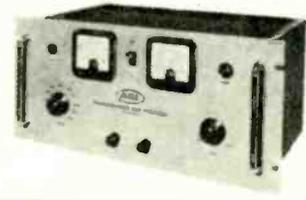
This equipment consists of reflectometer suitable for VSWR measurements at frequencies from 5 to 500 Mc/s and as a power output meter incorporating a non-inductive dummy load for RF measurements up to 200 watts, impedance 50 ohms; all stages are interconnected by "N" type connectors. These units are mounted on a 19in. rack fully equipped and no extra fixings are necessary. Offered at a fraction of original cost, brand new, boxed. Price, only£17

PLEASE NOTE

MOST EQUIPMENT ADVERTISED IN PREVIOUS MONTHS STILL AVAILABLE

A.E.I. HIGHLY STABILISED P.S.U. R2240

This fully transistorised unit is variable between 3-30 volts D.C. with a maximum load of 2 amps. Supplied brand new at only £22/10/0, carriage 20/-. List price £73.



AT LAST. Surplus to Requirements

Pairs of 4 x 250 series valve bases. The bases are of the forced-air type, heavily silver plated, insulation is P.T.F.E. Supplied as new, fitted to base plate. Price 69/6 per pair, post/packing 3/6.

"PERISTALTIC PUMPS" HR FLOW INDUCER TYPE MHRE 72 L WATSON MARLOW LTD.

These very versatile pumps have facilities for two feed lines. The pumps are standard type but less variable speed control. Ideally suitable for highly corrosive liquids. Offered as new for A.C. mains operation, at the greatly reduced price of £24/10/0. Post/packing 10/-.

G.E.C. PRECISION CIRCSCALE IMA METERS Type 2E1

These meters are of the very latest design, clearly scaled 0-10 with over 280° of deflection. Black numerals, white scale. Supplied brand new at 59/6 for panel mounting. Size 3 x 3 x 2 1/2 in. depth. C/W special mounting clamp.

RF ATTENUATORS—ADVANCE TYPE A38

These attenuators are contained in a screened cast case and are suitable for the audio to V.H.F. range up to 300 Mc/s. Input level 0.5 watts max. Impedance 75 ohms. Attenuation 80 dB in steps of 20 dB. Weight 9 oz. Panel mounting. List price £10. Special offer price 85/- post paid.

LEVELL TRANSISTOR A.C. VOLTMETER TM2A

Price, only£16/10/0

LEVELL TRANSISTOR A.C. VOLTMETER TM2B

Price, only£18/10/0

LEVELL TRANSISTOR MULTITESTER TM1

Price, only£12/10/0

DOUBLE BEAM OSCILLOSCOPES TYPE 13A

A general purpose instrument suitable for most applications, i.e., radio and TV service, audio-amplifiers, demonstrations, voltage and frequency measurements, etc. Bandwidth 2 c/s to 5.5 Mc/s, sensitivity 33 Mv/CM. Both amplifiers can be worked in cascade. C/W all leads, circuits, operating instructions. For A.C. mains operation. Price only £22/10/0. Carriage 25/-.

BURNDIPT RF PLUGS

These difficult-to-obtain plugs, suitable for the Londex aerial c/o relay and many other types of equipment, are offered new, ex. equipment at 4/6 each, post/packing 6d.

BRADLEY 148A

General purpose miniature scope. Battery or mains. Fully transistorised, band width D.C., 6 Mc/s. Price, as new£55

Rhode & Schwartz Model SDR-41022 300-1,000 Mc/s, little used condition, £125.
Advance B4A2 100 Kc/s-70 Mc/s, as new, £18. Advance Q1 7.5-250 Mc/s, £20. Advance EI 100 Kc/s-60 Mc/s, £15.
General Radio U.S.A. 605B 500 Kc/s-30 Mc/s, £35. General Radio 804B 7-330 Mc/s, £22.
AVO Ltd. CT378 2-225 Mc/s, as new, £40. All the above generators have internal mains power supply units.

SPECIAL OFFER AVO LTD. TRANSISTOR ANALYSER MODEL TA

These extremely versatile instruments are offered in first-class and serviceable condition. Incorporates all facilities for transistor testing. List price £115only £40

Portable non-spillable 12 volt 4 amp hour Lead Acid Batteries. These are a very modern type battery fully sealed but not dry charged, they are terminated with screw terminals, brand new and guaranteed, with full instructions. The size is about the same as the Perdio portable TV type batteries and you know how much they were. Our price is 45/-. If you are still guessing, the size is roughly 4in. square. Post/packing 2/6.

COMMUNICATIONS RECEIVERS

Redifon R50 13.5 Kc/s-32 Mc/s.
Hammerlund SP600 550 Kc/s-54 Mc/s.
CR150 1/2 10-60 Mc/s.
Murphy B40 640 Kc/s-30 Mc/s.
Marconi Electra 260 Kc/s, 25 Mc/s.
Halicraters SX28 550 Kc/s, 42 Mc/s.
All receivers in first class condition.

EDDYSTONE DIE-CAST BOXES

Contains sensitive amplifier originally intended for amplification of P.E. cells. C/W input socket, fuse, signal lamp. P.S.U. (mains) amplifier, fully transistorised. Brand new 32/6. Post/packing 2/6.

L.S.T. ELECTRONIC COMPONENTS LTD.

SEMI-CONDUCTORS, BRAND NEW AND FULLY GUARANTEED

IN914	2/-	2N4255	8/6	BC211	10/4	OC19	5/-	
5113	3/-	2S018	8/6	BD121	19/6	OC20	33/-	
5100	2/6	2S024	25/-	BD123	22/6	OC22	13/-	
5130	2/6	2S034	15/-	BD124	11/-	OC23	15/-	
C131	2/6	AC107	14/6	BF152	13/6	OC24	10/-	
1S132	2/6	AC126	6/6	BF154	9/-	OC25	6/8	
2G301	4/-	AC127	6/-	BF159	18/-	OC26	12/-	
2G302	3/9	AC128	4/-	BF163	9/-	OC28	12/-	
2G339A	5/-	AC176	7/6	BF167	6/6	OC29	15/-	
2G374	5/-	AC187	12/-	BF173	7/6	OC30	7/-	
		AC188	12/-	BF181	7/-	OC35	9/6	
2G371	3/-	AC117	5/8	BF184	7/6	OC36	13/-	
2N305A	15/-	AC118	3/4	BFW52	7/4	OC41	3/6	
2N188A	15/-	AC119	4/4	BFW58	7/4	OC42	4/-	
2N496	6/-	AC120	3/8	BFW55	6/6	OC44	3/-	
2N497	6/-	AC121	4/-	BFW60	6/6	OC45	3/-	
2N498	4/6	AC122	2/4	BF133	4/4	OC71	3/-	
2N706	3/6	AD140	15/-	BFK29	6/5	OC72	4/6	
2N706A	6/6	AD149	11/8	BFY50	6/-	OC73	3/-	
2N708	4/-	AD161	6/6	BFY51	6/-	OC75	5/-	
2N711	7/6	AD162	6/-	BFY52	6/-	OC76	2/6	
2N711A	7/6	AD163	12/6	BFY53	6/-	OC77	6/8	
2N929	5/6	AF102	18/-	BSX20	3/3	OC810	3/-	
2N930	6/6	AF114	4/4	BSX21	8/-	OC82	4/6	
2N1131	9/6	AF115	4/4	BSY27	4/-	OC82D	3/-	
2N1132	7/6	AF116	4/4	BTX39	400	120/-	OC201	10/6
2N1102	4/6	AF117	4/4	BUY11	15/-	OC84	4/-	
2N1303	4/6	AF118	16/6	BSY55A	3/4	OC123	7/-	
2N1304	5/-	AF124	6/-	BY100	5/-	OC139	8/-	
2N1305	5/-	AF127	6/-	BYX10	4/9	OC140	12/-	
2N1306	6/6	AF139	15/-	BYZ10	9/-	OC169	6/6	
2N1307	6/6	AF186	11/-	BYZ12	6/-	OC170	4/-	
2N1308	8/-	AF219	12/-	BYZ13	5/-	OC171	6/-	
2N1309	8/-	AF212	11/9	GE1102	6/-	OC200	6/-	
2N1613	4/6	AS236	5/8	GET103	4/8	OC201	10/6	
2N1247	17/-	AS227	5/8	GET113	5/-	OC202	16/6	
2N1248	12/6	AS230	4/4	GETS73	7/6	OC203	8/-	
2N2160	14/6	AS239	4/4	GMO378B	6/-	OC204	8/-	
2N2368	6/6	AS221	11/-	MPF102	9/-	OC205	9/6	
2N2369	5/6	AU110	2/8	MPF103	9/-	OC206	10/6	
2N2369A	7/6	BA115	2/8	MPF104	9/-	OC207	7/6	
2N2646	10/-	BA130	3/6	MPF105	9/-	ORP60	8/-	
2N2696	6/6	BAY31	2/6	NKT216	10/5	ORP61	8/-	
2N2924	5/6	BC107	2/9	NKT217	10/5	ORP63	9/-	
2N2925	5/6	BC107	2/9	NKT261	4/3	5X631	7/4	
2N2926	2/-	BC108	2/9	NKT262	4/3	5X636	10/8	
Green	2/-	BC109	2/9	NKT264	4/3	5X638	12/-	
Yellow	2/-	BC113	5/-	NKT271	4/3	5Z30C	15/-	
Orange	2/-	BC114	18/-	NKT272	4/3	5CC1	17/4	
Red	2/-	BC115	13/6	NKT274	4/3	CA26	8/3	
2N3053	8/-	BC118	5/-	NKT275	3/6	P346A	6/-	
2N3054	15/-	BC125	14/-	NKT276	2/6	P346A	9/3	
2N3055	15/-	BC126	14/-	NKT281	5/6	EC401	5/-	
2N3702	4/6	BC134	5/-	NKT403	15/-	EC402	4/8	
2N3703	4/6	BC147	6/-	NKT405	15/-	CI11E	18/-	
2N3704	4/6	BC148	4/-	NKT713	5/6	C400	9/-	
2N3705	4/6	BC149	4/-	NKT773	5/6	CC111	45/9	
2N3706	3/6	BC154	12/-	NKT774	5/4	2C425	32/6	
2N3707	4/6	BCY30	7/-	OAS	3/8	EA403	3/6	
2N3708	3/6	BCY31	9/-	OA47	1/6	EB383	3/6	
2N3709	3/6	BCY32	16/-	OA70	1/6	MJ481	27/3	
2N3710	4/6	BCY33	4/4	OA73	1/6	MJ481	27/3	
2N3711	4/6	BCY34	6/4	OA79	1/6	40361	13/3	
2N3819	8/-	BCY38	8/-	OA81	1/6	40362	16/3	
2N3820	23/6	BCY39	22/6	CA85	1/3	CA2341	3/6	
2N4058	7/6	BCY40	13/4	DA90	1/6	OA2242	3/6	
2N4059	6/6	BCY54	15/3	CA91	1/6	OA2269	3/6	
2N4060	6/6	BCY70	8/4	OA95	1/6	OA2270	3/6	
2N4061	6/6	BCY71	8/4	OA200	2/-	OC971	18/3	
2N4062	4/6	BCY72	4/6	CA202	2/6	5T140	3/-	
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CHEAPEST EVER SOLID-STATE SALE

BEST VALUE IN BRITAIN

40 Silicon Planar Transistors TO-18 case. NPN & PNP mixed. Similar V405A, P346A, etc. Not tested or coded. Guaranteed minimum 50% good. 10/-

40 Silicon Planar Transistors TO-18 case. NPN type similar 2N706, BSY55A, etc. Not tested or coded. Guaranteed minimum 50% good. 10/-

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16 Silicon Rectifiers. Top-Hat case. 750mA @ 100 - 1000 piv. Guaranteed minimum 80% good. 10/-

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2G371B and SD19 are Manufacturers' tested devices. Other uncoded stock are given type numbers as a guide only. Money refunded if not satisfied.

All above packs post free in UK.

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Signal neons for many types of circuit. type "N" Price 1/6 each or 16/- dozen.

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Suitable for 2 x OC35, etc. As used in commercial equipment. Type 10D ... 6/-

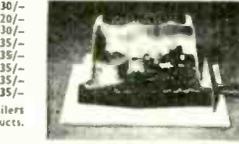
ALUMINIUM CHASSIS

6 x 4 x 2 1/2" with reinforced corners 6/9 each (P & P. 1/6). Alloy panel to fit 1/6. Passolun panel to fit 2/6. Many other sizes in stock up to 12 x 8 x 2 1/2" (see catalogue).

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MODULES YOU CAN OPEN!

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50	6d	1/-	2/3	—
100	9d	1/6	2/3	4/6
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400	2/-	2/6	4/-	8/-
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800	3/-	3/9	5/-	11/3
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PIV	1A	3A	10A	30A	100A
50	7/6	9/-	7/6	—	20/-
100	—	10/-	10/-	—	22/-
200	8/6	—	12/6	42/-	35/-
300	—	11/-	—	—	—
400	9/6	12/6	15/-	60/-	45/-
600	—	—	20/-	84/-	120/-
800	—	—	—	—	—

ZENER DIODES

1 Watt 10% Tolerance—

Voltages:

3.0	4.7	7.5	12	ALL
3.3	5.1	8.2	13	ONE
3.6	5.6	9.1	15	PRICE.
3.9	6.2	10	16	3/6
4.3	6.8	11	—	each

See IR Panel for 1 Watt types Full range 5 Watt also in stock.

BC107/8/9 NPN 2/9

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1-6 7-11 12+

uL900 11/- 9/6 8/4

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Five Page Data and Circuits article 2/6

Larger quantity prices (100+ and 1,000+) on application.

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CA3020 1/2 Watt output 9 volt supply 30/6 (Price includes free circuit for Guitar/PA Amplifier !!)

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CA3012 Wide band with built-in regulation 27/6

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FREE: With each pair our complete transmitter and receiver circuit.

PRICE £5.18.0 Pair (Sold only in pairs)

IR

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B2M 0.2-0.4 volts @ 2mA Selenium type 12/6

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EP50A Runs from sunlight activity on S4M cells (above) 39/6

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CS120 20v 0.4 Watts Dark Res 110k ohms Min. R @ 10FC = 7.2k R @ 100 FC = 800 ohms 19/8

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ZENER DIODES

Available in the following voltages with a dissipation of 1 watt and tolerance on 10%. All supplied with free manual describing many interesting projects

3-9v. 5.6v. 6.8v. 8.2v. 10v. 12v. 15v. 18v. 22v. 27v

ALL ONE PRICE 7/11

ZENER KIT

DD170 Bargain pack—contains 5 popular 1 Watt diodes plus free project manual 19/6

TRANSISTOR SUBSTITUTION

Our TR01-C to TR10-C range are universal replacements for over 700 JEDEC (2N—) types. Prices in our FREE Catalogue.

FULL SEMICONDUCTOR CENTRE LISTINGS.

DOZENS OF INTERESTING DEVICES IN OUR CATALOGUE.

COMPONENTS

RESISTORS 1/2 or 1 Watt 5% LOW NOISE CARBON FILM 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 ohms and decades (x10, x100, x1,000, x10,000) 1 Meg etc. to 2 Megohms (10% tolerance). PRICES: 1-25 4d. 26-99 3d. 100+ 2d (your selection) 1/2 and/or 1/2 Watt mixed).

SKELETON PRESET POTS. 20% Tol. Linear. Low noise. Available in sub-miniature or standard size, horizontal or vertical. 100, 250, 500, 1k, 2.5k, 5k, 10k, 25k, 50k, 100k, 250k, 500k, 1 Meg, 2.5 Meg, 5 Meg. NEW PRICE: 1/- each or any selection of 12 pieces 10/-.

ELECTROLYTIC CAPACITORS (Mullard). —10% to +50% tol. Subminiature (all values in µF)

4V	4	32	64	125	250	400
6-4V	6.4	25	50	100	200	320
10V	10	20	40	80	125	200
16V	16	32	64	125	250	400
25V	25	50	100	200	400	800
40V	40	80	160	320	640	1280
64V	64	125	250	500	1000	2000
Price 1/4	1/3	1/2	1/1	1/1	1/1	1/1

MIN. POLYESTER CAPACITORS. Printed circuit type 250 Vdc working: 0.01, 0.015, 0.022, 7d each: 0.033, 0.047, 8d each: 0.068, 0.10, 9d each.

VEROBOARD 015" Matrix FLUX COATED 2 1/2 x 3 1/2, 3 1/2 x 5, 3 1/2 x 3 1/2, 3 1/2 x 5, 5/6

ELECTRONIC BROKERS

MARCONI VALVE VOLTMETER TF 428B/1.



Frequency response on probe 10 c/s to 3-100 MA/a. Five separate Voltage Ranges. Overload Protection 1 0 0 - 2 5 0 A.C.I.P. Input

1 MΩ Acc. ±2% or 00.2 v. Size: 10 x 16 1/2 x 9 in. —15 lbs. £419.6.

TRANSFER FUNCTION ANALYSER OS103/VP 253



Frequency range 0.1 c/s to Kc/a covering electro-mechanical applications and servomechanisms. Resolves network response signals simultaneously into in-phase or

quadrature components. Permits direct polar diagram plotting of a servo system frequency response using cartesian co-ordinates. Establishes data for Nyquist diagram, attenuation phase response and other servo characteristics. Gives network phase/amplitude response from 0.1 c/s to 1 K c/s. Deflection sense of two centre zero meters gives immediate identification of vector quadrant involved. 40 db rejection on amplitude. High sensitivity 50 mV/fd. High accuracy measurement of true R.M.S. volts. List price £1,600. Our price £595.

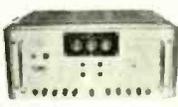
V.P.253 available separately £149.

AC CARRIER CONVERTER JX 671A

Provides modulation and demodulation to adapt transfer function analyser for use with A.C. carrier systems. Frequency: 50 c/s, 60 c/s, 200 c/s, 400 c/s. Carrier supply 0-230 R.M.S. Our price £95.

TRANSFER FUNCTION ANALYSER REFERENCE RESOLVER JX 746

for use with Transfer Function Analyser. On T03/VP253 provided digital display of phase angle. Three decade digital 0-180; with lead/lag switch. Our price £125.



SOLARTRON AS 562 KLYSTRON POWER UNIT.

Suitable for supplying low voltage Klystron valves. Sine wave, Square wave and triangular wave modulation facilities provided. Precision reflector supply. L.T. 6.3 V. D.C. up to 1 amp adjustable output. Resistor supply 250-400 V at 50M/A (Positive). Reflector supply 0-400V (Negative) Switched. Modulation internal 50 cycle symmetrical triangular. 3 Kc/s - 50 cycles) sq. wave, 3 Kc/s (-50 cycles) sine wave. List price £220. Our price £85.

SERVO TEST SET JX 563

Enables Testing of Servo Units and Systems by unskilled personnel. The unit consists of an L.F. amplitude-stabilised oscillator feeding the servo unit under test via a preset attenuator, the output from the servo being compared within the instrument against preset reference signals at chosen frequencies. Oscillator output: 10 volts R.M.S. unbalanced, or 20 volts R.M.S. balanced. Maximum current in load: 5MA. Oscillator frequencies any four from 0.5 cycles-500 cycles. Servo output limits: Minimum 30MV to maximum 100 volts. List price £450. Our price £150.

SANGAMO WESTON LABORATORY STANDARD AC/DC VOLTMETER S 92

Accurate to 0.1 per cent of full scale. 12 inch Vernier scale magnetically shielded. Self-contained thermometer. Spirit level, range 0.75, 150, 300. List price £150 approx. Our price £45.

PRECISION POTENTIOMETERS

TEN TURN 3600° ROTATION

BRAND NEW



Res. Ohms	Linearity Per cent	Manufacturer	Model	Price
100/100/100		Beckman	A	160/-
100	0.5	Beckman	A.8	60/-
200	0.5	Beckman	A	60/-
500	0.1	Beckman	S	70/-
500		Colvern	2501	45/-
500		Foxes	PX 4	40/-
2K		Colvern	2610	50/-
2K	0.5	Beckman	8A1101	60/-
2K		Beckman	7216	60/-
2K		Reliance	GPM15	40/-
10K	0.5	Beckman	A	60/-
10K	0.1	Beckman	A	70/-
10K	0.05	Beckman	A	95/-
15K		Foxes	GPM15	50/-
18K		Beckman	A	60/-
20K	0.5	Beckman	A	60/-
20K	0.05	Beckman	8A1244	70/-
30K		Colvern	2402	30/-
30K		Beckman	8A 95C	60/-
30K	0.1	Beckman	A.88	70/-
30K	0.5	Beckman	8A 1692	60/-
30K	0.25	Beckman	8A 1692	65/-
50K		Reliance	07.10	70/-
50K		Colvern	07.5	45/-
50K		Colvern	2503	45/-
50K	X	Foxes	PX 4	45/-
50K	0.5	Beckman	A	70/-
50K	0.1	Beckman	A	70/-
100K/100K		Ford	A	100/-
100K	0.1	Beckman	A	70/-
100K	0.5	Beckman	A	60/-
100K		Colvern	2501	45/-
100K		Colvern	2610	50/-
298K	0.1	Beckman	8A 3902	70/-
300K	0.1	Beckman	A	70/-

THREE TURN 780° ROTATION

100/100	0.5	Beckman	A	60/-
300		Beckman	9303	45/-
10K	0.5	Beckman	A	35/-
10K	0.5	Beckman	C.88	45/-
10K	0.1	Beckman	C	55/-
20K/20K	0.1	Beckman	C.8	60/-
10K/10K	0.1	Beckman	C	60/-
50K	0.5	Beckman	C.8	35/-

FIFTEEN TURN 5400° ROTATION

25K/25K	Beckman B	10 watts	£6.10s.
46K/46K	Beckman B	10 watts	£6.10s.

TWENTY TURN 7200° ROTATION

250 ohms. General Controls. PX M130. 80/-
1 Meg. General Controls. PX M130. 80/-
50K Reliance. 40/-

156 TURN 56,160° ROTATION

460 ohms. Kelvin Hughes. KT P0701 £9.10s.

FIVE TURN 1800° ROTATION

500 ohms. Colvern. CLR 2505 40/-
1.5K. Colvern. CLR 2605 40/-

SINE COSINE

Colvern 8601. 10K. £12.10s.
Colvern 9501. 11K C.T. £16.10s.
CLR 9604—Cam Corrected 25K. £20.
9101/A 20K. £16.10s.

PRECISION BECKMAN 40 TURN 14,400° ROTATION

Wirewound Precision Potentiometer. SE 107A 20 watts at 40°C. 3 1/2" Diameter. Servo Mounting. 200K. Brand New £12.10s. List Price £30.

TRIMPOTS 990 GB—Wirewound Micropot

Potentiometer. Low noise. Brand new, by well known manufacturer. 1 watt @ 70°C. 100 ohms and above ±5%. Available in the following values: Ohms: 5, 15, 25, 50, 100, 250, 400; 1K, 2K, 2.5K, 10K, 25K, 10/- each.

FERRANTI PRECISION CONTINUOUS WIRE-WOUND POTENTIOMETER, TYPE P4A

Size 15. Seven Sections. Ganged, giving seven different predetermined values. £9.10.0.



COLVERN 10-TURN INSTRUMENT DIALS 10/6

RECORDING INSTRUMENTS AND MOTORS

FOUR CHANNEL HIGH SPEED PEN RECORDER

by Kelvin Hughes, with four channel amplifier, giving a frequency range of 0-100c/s. The Recorder consists basically of a magnet carrying in its poles four stiffly suspended moving coil units, each with a stylus arm attached. The stiffness of the coil unit suspension enables the instrument to withstand the effects of vibration and acceleration. Mains operated. Pen deflection ± 7.5 m.m. 6 chart speeds—0, 5; 1; 2; 4; 8; and 16 cm/sec. Excellent condition. £195 N.B. Two channel version available, giving ± 16.5 m.m. deflection.

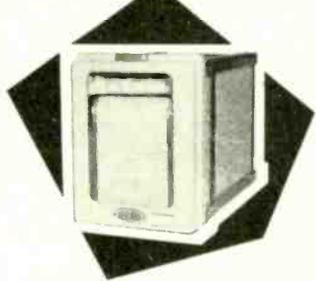
FIVE CHANNEL PEN RECORDER

Complete with five channel amplifier. Chart width 9in. Maximum trace width of ± 2 cm. per channel. Frequency response flat to 60 c/s. Mains operated, complete in free standing console. Fully overhauled cost £1200+ Our price £450

HYSTERESIS CLUTCH MOTOR

with integral clutch allowing the motor to drop out of engagement with the gear train, thereby facilitating easy resetting when used in timers or in conjunction with a light spring. 6 oz. torque at 1 r.p.m. 240 v., 50 c/s. L—left, R—right, 15 r.p.m. L, 8 r.p.m. R & L, 6 r.p.m. L, 4 r.p.m. L, 4 r.p.m. L/1/5 r.p.m., 1/6 r.p.m., R & L, 1/10 r.p.m., 1/12, 1/15 r.p.m. L. Also 120 v., 50 c/s 2, 1/6, 1/12, 5/12, 4/11, 1/10 r.p.m. 25/-.

PORTABLE SINGLE PEN RECORDER BY RECORD ELECTRICAL



(illus.). 3 in. chart, sensitivity 500 micro amps. Coil res. 1.5kΩ. Fully interchangeable gears available to make a wide range of chart speeds. 200/250v. Size: 8 x 11 x 6 in. Brand new—complete with chart and ink. List over £100. Our price £49.10.0.

TRANSITROL 2 POSITION INDICATING TEMPERATURE CONTROLLER BY ETHER

TYPE 990



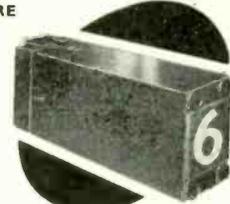
Completely transistorised self-contained direct deflecting units for indicating and controlling temperature accurately over a wide range. Suitable where a signal can be converted into D.C. Sensitivity 10 ohms per M.V. Minimum F.S.D. 8 M.V. protection. Copper compensation. Calibrated scale length, 6.5 in., 0-800 degrees centigrade accuracy ± 1%. Front panel size 10 x 5 1/2 in., weight 11 lb. Mains supply 100-260 v. Control switching and Thermocouple connections all at back of case. Our price £22.10.0. List price £49. New condition.

MAGNETIC FLUX MEASURING SET TS 13A

Range 1,500-9,900. Gauss—Bohr. Pole face diameter of magnets 1/2 in. Air gap 550 in. 1.51 in. Powered by U2 1.5V cell. Our price £18.10.0.



MINIATURE DIGITAL DISPLAY



Operates on a rear projection 6.3 pilot lamp. The lamp projects the corresponding digit on the condensing lens through a projector lens, on to the viewing screen at the front of the unit. 1 in. width. 3 1/8 in. deep. 1 1/8 in. high. Weight 3 1/2 oz. Character size 1/2 in. high, 0-9 with 8 right hand decimal point and degree. Available to special order, words and other characters or colour, at cost of artwork or plates. List price 6 gs. Our price 49/6.

EAC DIGIVISOR Mk. II DIGITAL READ-OUT DISPLAY



Ideally suitable for use in conjunction with transistorised decade counting devices. No need for amplifiers or relays as only a few milliwatts of power are required to charge the digits. The DIGIVISOR incorporates a moving coil movement which moves a translucent scale through an optical system and the resultant single plane image is projected on a screen. The translucent scale is made to represent digits 0-9. Specifications: 6.3 volt, 250 microamp. Image height 1 in. Size 4 9/16 x 2 39/64 x 1 1/4 in. Our price 3j Gus. List price 8j Gus.

LOW TORQUE HYSTERESIS MOTOR MA23



Ideal for instrument chart drives, extremely quiet; useful in areas where ambient noise levels are low. Having a high starting torque a relatively high inertia load can be driven. 6 oz./in. at 1 r.p.m. 240 volts 50 cycles. 10 r.p.m. R, 1/10 r.p.m. R & L, 1/12 r.p.m. L, 1/15 r.p.m. R, 1/10 r.p.m. R, 1/12 r.p.m., 1/20 r.p.m., 1/40 r.p.m., 1/60 r.p.m., 1/180 r.p.m., 1/360 r.p.m.; 1/6 r.p.m. hour, 1/12 r.p.m.; 1 r.p.m., 1/4 r.p.m. 25/-.

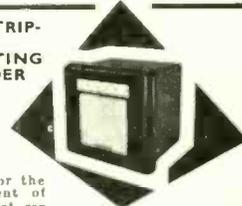
HYSTERESIS REVERSIBLE MOTOR.

Incorporating two coils. Each coil when energized will produce opposite rotation of the output shaft. 240 volt 50 cycle. 1 r.p.m., 1/10 r.p.m., 1/5 r.p.m., 1/10 r.p.m., 120 volt 60 cycles 1/10 r.p.m. 80/-, reduced to 30/-.

POTENTIOMETRIC 6 POINT STRIP CHART RECORDER BRAND NEW

For use with thermocouples, pyrometers and other e.m.f. sources. 6 point. Range (—100) —(+100) mV; 0—1,600 deg. C. 6 1/2 in. chart width; pen speed 8 sec. Accuracy ±0.5%; 10 chart speeds 20-720mm/hr. Tropicalised. Including tools and spares listed at over £200! Our price £79.10.0. 12 point version available £99.10.0.

KENT STRIP-CHART INDICATING RECORDER



Suitable for the measurement of anything that can be measured in terms of an electrical signal. Chart width 9 1/2 in. 10 mV. 2 v. Sensitivity ±0.17 of full scale. Speed of operation 33 sec. for full-scale travel. Chart speeds 1/2 in., 3 in., 6 in. per hour. Single point £49.10.0.

TORQUEMOTOR 225 BY ELLIOTT

Originally designed to operate hydraulic valves or hydraulic motor under extreme conditions of temperature, altitude and vibration. The torque-motor is practically unaffected by vibration or sudden shock, i.e. consists of a moving iron rotor with a travel of 7 degrees either side of centre. MIN TORQUE (gm-cm) 500 at zero at 6 degree. 70 gm cm. Total hysteresis at 0°C. 0-58 degree current 45 M/A. £9.10.0.

FERRANTI HIGH SPEED 5 HOLES 20 CHARACTERS per second reader. £29.10.0.

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LOW COST ELECTRONIC AND SCIENTIFIC EQUIPMENT AND COMPONENTS

DIGITAL MAGNETIC DATA STORAGE DECK

Seven track record replay heads

These machines originally ex-computers, but lend ideally for use as audio stereo multi-track recording units or data storage. Record and Playback Heads encased in one common unit. This unique close spacing of Record and Playback Head will enable the operator to monitor instantly while recording, crosstalk between tracks absolute minimum. Head Resistance 40 ohms and 7 ohms. Freq. Response approx. 30 c.p.s.—30 Kc/s with a good response to 50 Kc/s. Deck driven by one synchronous capstan motor and two variable-speed rewind motors. Electro-pneumatic capstan take-up mechanism. Speed 37 1/2 L.p.m. (Note: Capstan Head can be easily removed and any diameter Capstan Head corresponding to any speed can be fitted.) All deck function push buttons are illuminated and are brought out to separate multi-core leads which can be wired to any deck function or auxiliary equipment. Finished in brush-aluminium and matt-black. Size: 27 x 26 x 8 in. Weight 90 lb. 230v-280v. A.C. Capstan motor speed 1,500 r.p.m. Must have cost £1,000. Our price **£65**. New condition but ex-equipment. **VACUUM ASSEMBLY** required for computer and data use. **£7.10** extra. Seven Track record replay head, ex-computer, complete with guides, little used. **£12.10.0**. 4 in. Tape. 2,400 ft. **£8.10**, new. Empty reels 25/-, in cassettes 45/-.



MEMORY PLANES

Ferrite core memory planes with wired Ferrite cores. Used for building your own computer or as an interesting exhibit in the demonstration of a computer. Mounted on plastic material, frame 5" x 8". Consisting of matrices 40 x 25 = 1000 core store planes. Price **£8.10.0**.

PROGRAMME BOARDS BY SEAELECTRO

These boards are basically a multi pole multi throw switch device consisting of a X-Y Matrix with two contact decks in the Z Plane running at 90 degrees to each other. Contact in made by either, shorting or plugging in pins. Ideal for prototype work, etc. Boards available in 16 x 16 2 plane **£4.5.0**. 24 x 60 2 plane **£12.10.0**. Pins available 1/3 each.

MINIATURE RELAY COIL

REMOVING SHIS

By Bangama Weston, suitable for D.C. circuit. A high sensitivity relay more sensitive than the electro-magnetic type. Single Coil Resistance 2K. 50 - 0 - 50 Micro-Amp. List price **£4.10**. Our price **20/-**.

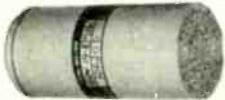


BRAND NEW S.E. LABORATORIES TRANSDUCER

complete with encapsulated Amplifier/demodulator S.E. 441/2 Frequency D.C.—60 c.p.s. Available in the following ranges:
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 0 - 25 p.s.i. 0 - 350 p.s.i. 0 - 2000 p.s.i.
 0 - 50 p.s.i. 0 - 500 p.s.i. 0 - 3000 p.s.i.
 0 - 200 p.s.i. 0 - 750 p.s.i. 0 - 4000 p.s.i.
 Also available differential types ± 5 p.s.i., ± 10 p.s.i.
 List price **£70+** Our price **£15**

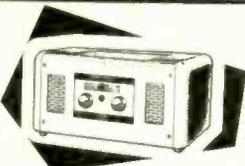
BURROUGHS 101 DESK SIZE

electronic digital computer with 220 word store 10 digit word length E101 Tape reader for electronic computations of small complex or repetitive calculating problems. Little used. **£485.0.0**.



"V" SCAN DIGITAL SHAFT ENCODER BY MOORE REED TYPE 18 DV-19-EP 116 3 discs.

Brand new. Counts 524288 in 1024 revolutions of shaft in V Scan. Brand new in maker's original sealed tins. List price **£75** approx. Our price **£22.10**.



SPEECH INVERTER MI-7181-A

The R.C.A. Speech Inverter is a device intended for use in radio-telephone installations where privacy is a prime consideration. The equipment when used in conjunction with the R.C.A. MI-7182 Hybrid Transformers enables parallel two-way conversations on a single telephone pair line at each terminal of the communications system. With inversion, speech fed into the transmitting inverter circuit will feed the radio transmitter with unintelligible signals. These signals will remain unintelligible until they pass through a receiving inverter circuit at the other end of the communication channel. (Used only under Licence in U.K. P.O.A.) **£12.10.0**.



HYBRID UNIT MI-7182

The Hybrid Unit is designed for use with the Speech Inverter where it is desirable to operate the output of a receiving circuit and the input of a transmitting circuit from a single pair of telephone wires whose electrical characteristics are essentially constant. When the Hybrid Unit is properly connected and balanced to the line, high attenuation will be provided between the receiver output circuit and the transmitter input circuit. **£10.10.0**.

EVERSHED BRIDGE MEGGER

250 volt, 50 meg. Insulation tester with built-in four decade bridges with ratio arms giving ratios of 100-1, 0.1 + 0.01 and Selector switch for insulation, resistance and variety measurements. **£29.10.0**. 500 volt 0-100 meg. with Varley Loop. **£89.10.0**.



VACTRIC 144-WAY HIGH SPEED MINIATURE SAMPLING SWITCHES

consisting of 24 segments in six bank. 8000 samples per second can be obtained from these switches. Ideally suitable for data logging application. Low inherent noise and contact resistance permitting high speed sampling of the most difficult transducers. Pulse generator for digital counting. Brand new. **£25**.

DIFFERENTIAL PRESSURE TRANSDUCERS

by Sifam Ltd. O.B. Type E33 Range ± 900 MB Resistance 942 ohms. Our Price **£19.10.0**

HOLLERITH 80 COLUMN CARD READER

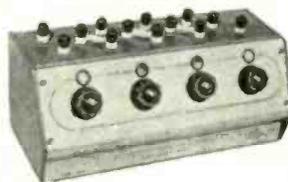
Complete with Verifier By ICT, Type No. H 129/2489. Good condition **£95**.

Carriage extra on all equipment.

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LABORATORY TEST EQUIPMENT PURCHASED DIRECT FROM LEADING MANUFACTURERS & DISTRIBUTORS

HIGH VALUE RESISTANCE BOX TYPE R.7003



Specification. Range: 0.01-11.10 Megohm in 0.01 Megohm divisions. Accuracy: 0.05%. Maximum power rating: 0.1W per step. Case: Hammer finished stove enamel. List price **£80**. Our price **£22/10/-**.

DECADE CAPACITANCE BOX TYPE R.7004



Specification. Range: 0.00002uF-1uF in 0.00002uF steps. Accuracy: 0.05%. Frequency Range: 40 c/s-10 Kc/s for all decades except X1=40 c/s-5 Kc/s. Case: Hammer finished stove enamel. List price **£80**. Our price **£22/10/-**.

MUTUAL INDUCTANCE BOX TYPE R.7005

Specification. Range: 0.1-110mH in 0.002 mH divisions. Accuracy: $\pm(0.3 \times \frac{0.012}{M})\%$ where M = value of mutual inductance in mH set on the box. Frequency range: 0-2.5 Kc/s for all decades except X1=0-15 Kc/s. Maximum current: 0.5A for decades 1A for variometer (both primary and secondary windings). Case: Polished teak. List price **£65**. Our price **£26/10/-**.



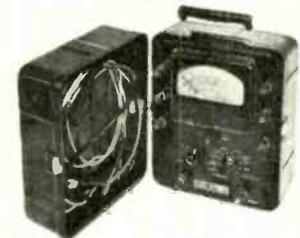
MUTUAL INDUCTANCE COIL TYPE R.7006

Specification. Value: 0.01 H. 0.001 H. Accuracy: $\pm 0.3\%$. Operating Frequency: 5 Kc/s, 10 Kc/s. Maximum current: 1A. 5A. Resistance of coils: 4 ohm, 1 ohm. Case: Moulded plastic. List price **£8** gns. Our price **50/-**.



★ A special price of **£65** is offered if the following equipment is ordered together: High Value Resistance Box, Decade Capacitance Box, Mutual Inductance Box, Mutual Inductance Coil.

PORTABLE MULTIRANGE METER



PORTABLE WHEATSTONE BRIDGE



Specification. Type: Moving Coil Galvanometer. Ranges: 1. 0.05 to 5 ohms. 2. 0.5 to 50 ohms. 3. 5 to 500 ohms. 4. 50 to 5,000 ohms. 5. 500 to 50,000 ohms. Scales: Switched. Slidewire: 0.5 to 50. Galvanometer Scale: 10-0-10. Case: Moulded plastic. Internal Source: 4V. Dry battery. Operating Temperature: $+10$ to $+35$ deg. C. Operating Humidity: Up to 80% R.H. Dimensions: 200 x 110 x 65mm. Weight: 0.9 kg. List price **£25**. Our price **£9/10/6**.

SET OF MEASURING INSTRUMENTS



Specification Type: Moving Coil D.C. Ranges: 0-75mV, 0-3V, 3-15-150V, 3-150-450V, 0.3-0.75A, 1.5-7.5A, 15-90A. Scale Length: 82mm. Accuracy: 1.0%. Shunts: 1.0-0.75 amps, 2.1-5.75 amps, 3.15-30 amps. Case: Moulded plastic. Carrying Case: Stove enamelled metal. List price **£30**. Our price **£12/10/6**.

★ ILLUSTRATED LEAFLETS AVAILABLE ★

PORTABLE RECORDING MILLIAMMETER



Specification. Type: Moving Coil, D.C. Range: 0-500 milliamperes. Chart Width: 100mm. Scale Length: 127mm. Chart Speeds: 20, 60, 180, 600, 1800 and 5400 mm/hr. Precision: 1.5%. Shunts: 75mV (Internal). Operating Temperature: $+5$ to $+50$ °C. Dimensions: 180h x 165 w x 245mm. Weight: 3.5kg. Complete with: 10 chart rolls, gears, ink, pipette, scale template and component case. List price **£65**. Our price **£35**. Illustrated leaflets available.

ADVANCE CONSTANT VOLTAGE TRANSFORMERS—Brand New.

15 watt 190-260 CV15 35/- 150 watt 190-260v. **£8/10/-**
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SOLA CONSTANT VOLTAGE TRANSFORMERS

210-250-600 watts. **£25**.

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NEW RANGES FOR THE AMATEUR AND PROFESSIONAL USER

***QUALITY PANEL METERS**

38 Series. Face size 42 x 42mm (1 1/2 in x 1 1/2 in). 50µA, 37.6; 100µA, 35/-; 200µA, 32/6; 500µA, 27/6; 1mA, 5mA, 10mA, 50mA, 100mA, 500mA, 25/- each; 10V, 20V, 50V, 100V, 300V and 500V, 25/- each; 1A and 5A, 25/- each. "S" meter, 1mA, 29/6. VU meter, 37/6.

65 Series. Face size 50 x 50mm (2 in x 2 in). 50µA, 62/6; 100µA, 52/6; 200µA, 47/6; 500µA, 45/-; 1mA, 5mA, 10mA, 500mA, 37/6 each. "S" meter, 1mA, 42/6. Other ranges and sizes available. List on request.



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Recommended quality instrument with mirror scale and overload protection. 0 to 30 (12), 60/120, 300, 600/1200V d.c. (50KΩ/V); 0 to 30 (12), 60/120, 300, 600/1200V a.c. (10KΩ/V); 0 to 30 (12), 60/300mA, 0.12A resistance, 0.10kΩ/10/100MΩ. Meter movement 20µA. Polarity reversing switch. Complete with batteries, leads, and instructions.

AF105 Price £8.10.0 p.p. 2/6
Leather case 28/6



***SINE SQUARE WAVE AUDIO GENERATOR**

Provides audio output on 4 bands. Sine wave 20c/s to 200kc/s, output up to 7V; square wave 60c/s to 30kc/s, 7V p-p. Distortion under 2%. Output impedance 1kΩ. Variable output amplitude control. Supplied with leads and instructions. A.C. mains operated.

TE22 Price £16.10.0. p.p. 8/6

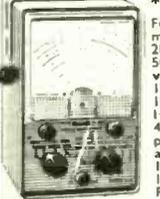


***VACUUM TUBE VOLTMETER**

Features low price for such an instrument. Large 6in full view scaled meter. 28 ranges. D.C. volts: 0.1/1/5/15/50/150/500/1500. A.C. volts: 0.1/1/5/15/50/150/500 r.m.s.; 0.1/4/4/14/40/140/400/1400/4000 p-p. Resistance: R x 10-100-1k-10k-100k-1M-10M. Range 0.2 ohm to 1000MΩ dB

scales: -10 to +65dB. Complete with instructions and leads.

MODEL TE65
£17.10.0 p.p. 7/6
HV Probe 50/-
R.F. Probe 42/6



20KΩ/V MULTIMETER

Popular model but with extra scale range. 20,000 ohms per volt. 0.5/25/50/250/500/2500V d.c., 0.1/10/50/100/500/1000V a.c.; 0.50µA, 0.2/1/250mA. Resistance 0-6kΩ and 6MΩ. Also dB scales or capacitance.

Model 200H 77/6
(Leather case, Price 15/-)



***PORTABLE OSCILLOSCOPE**

Features 3in clear view tube, easy to use controls and good stability. Y amp. Sensitivity, -1V p-p/CM. Bandwidth 1.5 cps-1.5 MHz. Input imp. 2 meg Ω. 25 PF. X amp sensitivity, -9V p-p/CM. Bandwidth 1.5 cps-800 KHz. Input imp. 2 meg Ω. 20 PF. Time base. 5 ranges 10 cps-300 KHz. Synchronization: Internal/external. Illuminated scale. 140 x 215 x 330 MM. Weight 15lbs. 220/240V. A.C. Supplied brand new with handbook.

TO3 Price £35 p.p. 10/-



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***TRANSISTOR POWER AMPLIFIERS**

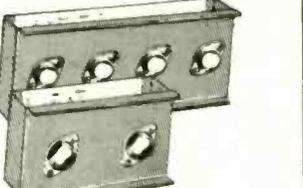
12 watt 3 ohm 100mV Input 24 volt supply. Model MPA 12/3 £4.10 p.p. 3/-

12 watt 12-16 ohm 100mV Input 40 volts supply. Model MPA 12/15 £5.5 p.p. 43/-

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Power Supplies 24-40 volt 90/- p.p. 3/6
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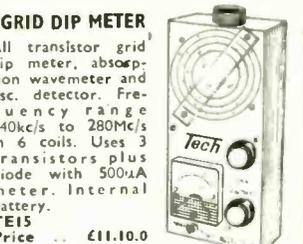
Model P.97 7 watt Amplifier 3 ohms C/P. 7mV Input, operates 12-18 volts D.C. Price 72/6 p.p. 2/6



***GRID DIP METER**

All transistor grid dip meter, absorption wavemeter and osc. detector. Frequency range 440kc/s to 280Mc/s in 6 coils. Uses 3 transistors plus diode with 500µA meter. Internal battery.

TE15 Price £11.10.0



DC POWER SUPPLIES

220/250 volt A.C. Input LA1D5 9 volt-500mA 45/- p.p. 2/6

PA12 o/p 6-9-12 volts lamp switched. Price £6.5.0

RP215 Stabilised 8-15 volts 0.2 amps 3mV PP Ripple. Two Panel Meters. Price £17.10.0 p.p. 7/6

RP216 as above but 0-15 volt 2 amp. Price £21.10.0 p.p. 7/6

All Meters Brand New.

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Covers 1-250Mc/s. Switches for model control and any application requiring peaking of transmitters and oscillators. 100µA meters. Complete with aerial.

FS1 Price £25.0 p.p. 2/6



***POCKET DOSIMETER**

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***SIGNAL INJECTOR**

New model for checking all audio and RF up to VHF. Simple to use. Battery operated. Output approx. 1kc/s, 1-4V pp. Harmonics up to VHF.

SE250B Price 35/- p.p. 1/6



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Complete kit with punches 1in, 3in, 3in. lin, 1 1/2in for metal, plastics; etc., up to 16 gauge.

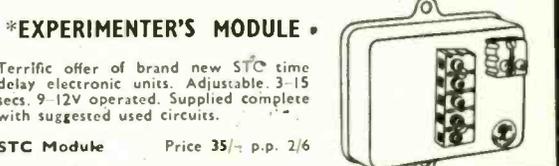
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***EXPERIMENTER'S MODULE**

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STC Module Price 35/- p.p. 2/6



MEC, BORG PRECISION PRESETS

Complete Range in stock of these Precision W/W Presets.

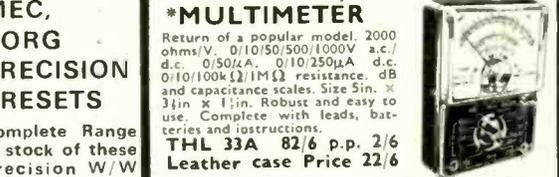
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Return of a popular model. 2000 ohms/V. 0/10/50/500/1000V a.c./d.c. 0/50µA, 0/10/250µA d.c. and capacitance scales. Size 5in. x 3 1/2in x 1 1/2in. Robust and easy to use. Complete with leads, batteries and instructions.

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***SWR ALIGNMENT METER**

Ideal for all transmitter alignment. Built-in field strength meter 100µA. Complete. Ready to use. SWR 1:1 to 1:3.

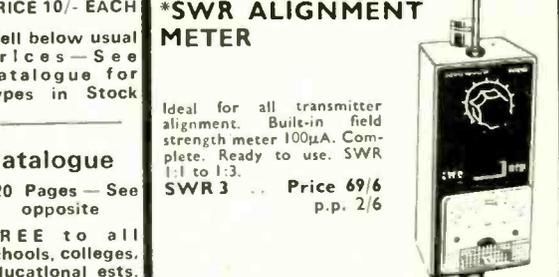
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Catalogue

320 Pages—See opposite

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BRAND NEW SPECIAL OFFER 75/- p.p. 2/-



***SPECIAL OFFER OF EMI TWEETERS**

● 2 1/2in units 6/8W, 3kc/s to 15kc/s. 8 ohms (suitable for 3-8 ohms). Price 12/6, p.p. 1/6.

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ALL ITEMS OFFERED ARE BRAND NEW STOCK ALWAYS IN STOCK

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the MA7 or MA66 will FILL THE BILL.

for complete listening satisfaction choose either the—

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POST 18/-

SPARE BATTERIES 12/- PAIR. POST 5/-



NEW MODELS NOMBREX TRANSISTORISED Test Equipment

MODEL	£	s.	d.	No.
22 Power Supply	14	0	0	22
30 Audio Generator	19	10	0	24
31 R.F. Generator	12	10	0	25
32 C.R. Bridge	10	10	0	26
33 Inductance Bridge	20	0	0	29

Send for descriptive illustrated Brochure.



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The Detector Unit consists essentially of a highly sensitive 931A photo-electric cell combined with a firing circuit, incorporates a single cold cathode electronic relay, capacitors and resistors designed to fail to safety if external wiring is open or short-circuited. Encapsulated in a resin which fully insulates the unit electrically and provides a high degree of mechanical and thermal shockproofing. Original price £74. OUR PRICE, BRAND NEW £6 each, with data sheet. Limited quantity available.

SIZE 4 X 3 X 2 1/4 in.



MULLARD 1 WATT AMPLIFIER

PORTABLE TRANSISTOR UNIT with volume control. Many uses. Intercoms, Baby Alarms, Guitar Practice, Telephone or Record Player Amplifier. Optional Roxine covered Wood cabinet 12 x 9 x 4. 12/6. 7 x 4 in. speaker, 17/6. Uses PP9 battery.

45/- pp. 3/6d.

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2 Track 36 gns. P.P. 22/6 either model
Kit comprises: Deck, Amplifier, Cabinet and speaker, with MICROPHONE 7 in. 1,200 It. tape, spare spool. ALL UNITS AVAILABLE SEPARATELY. Today's ASK FOR BROCHURE 6. Value £60.

4 Track 39 gns.



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* 6 MULLARD TRANSISTORS & 4 DIODES * 300 Mc/s BANDWIDTH * PRINTED CIRCUIT CONSTRUCTION * HIGH FIDELITY REPRODUCTION MONO AND STEREO

A popular VHF FM Tuner now used throughout the country for quality reception of monophonic and, with the decoder stereophonic broadcasts. There is no doubt about it—VHF FM gives the real sound. Excellent stability economically priced. TOTAL COST £6.19.6. DECODER £5.19.6. (CABINET 20/- EXTRA) ASK FOR LEAFLET 3

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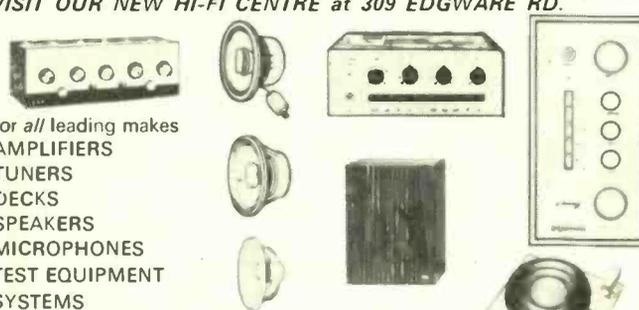


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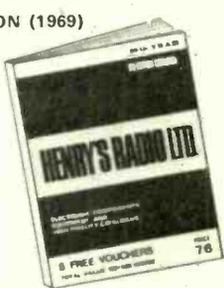
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PC103	45/-	PC97	10/6	UP98	7/3
PC104	45/-	PC98	10/6	UP99	7/3
PC105	45/-	PC99	10/6	UP100	7/3
PC106	45/-	PC100	10/6	UP101	7/3
PC107	45/-	PC101	10/6	UP102	7/3
PC108	45/-	PC102	10/6	UP103	7/3
PC109	45/-	PC103	10/6	UP104	7/3
PC110	45/-	PC104	10/6	UP105	7/3
PC111	45/-	PC105	10/6	UP106	7/3
PC112					

CURRENT RANGE OF BRAND NEW L.T. TRANSFORMERS. FULLY SHROUDED (*excepted) TERMINAL BLOCK CONNECTIONS. ALL PRIMARIES 220/240v.

No.	SEC. TAPS	AMPS	PRICE	CARR.
1A	25-33-40-50	15	£9 10 0	10/6
1B	25-33-40-50	10	£6 19 6	8/6
1C	25-33-40-50	6	£5 19 6	8/6
1D	25-33-40-50	3	£3 12 6	7/6
2A	4-16-24-32	12	£6 10 0	7/6
2B	4-16-24-32	8	£4 17 6	7/6
2C	4-16-24-32	4	£3 5 0	6/-
2D	4-16-24-32	2	£2 2 6	5/-
3A*	25-30-35	40	£14 17 6	15/-
3B*	25-30-35	20	£9 7 6	9/6
3C	25-30-35	10	£6 10 0	7/6
3D	25-30-35	5	£3 15 0	6/6
3E	25-30-35	2	£2 15 0	6/6
4A*	12-20-24	30	£11 15 0	10/-
4B	12-20-24	20	£7 10 0	8/6
4C	12-20-24	10	£4 15 0	7/6
4D	12-20-24	5	£3 5 0	6/6
5A	3-12-18	30	£8 15 0	7/6
5B	3-12-18	20	£6 10 0	7/6
5C	3-12-18	10	£3 17 6	6/6
5D	3-12-18	5	£2 12 6	6/6
6A	48-56-60	2	£3 5 0	5/6
6B	48-56-60	1	£2 7 6	5/6
7A*	6-12	50	£9 7 6	9/6
7B	6-12	20	£5 10 0	7/6
7C	6-12	10	£3 10 0	6/6
7D	6-12	5	£2 10 0	5/6
8A	12-24	1	£1 9 6	5/6
9A	17-32	8	£5 12 6	5/6
10A*	9-15	2	£1 5 0	5/6
11A	6-3	15	£2 5 0	5/6
12A	30-25-0-25-30	2	£3 5 0	5/6

Note: By using the intermediate taps many other voltages can be obtained.

Example: No. 1, 7-8-10-15-17-25-33-40-50V.
 .. 2, 4-8-12-16-20-24-32V.
 .. 5, 3-6-9-12-15-18V.

GUARANTEED SURPLUS L.T. TRANSFORMERS

- No. 1. Twickenham Transformer Co. Pri: Tapped 110-220-235-250v. Sec: 55v. 24A., 14v. 10A., 60v. 2A. All windings very conservatively rated. Tropically finished. Terminal connections. Size H9 x W7 1/2 x D7 ins. Wt. 65lbs. Fraction of maker's price. £10.19.6d. Carr. 15/-
- No. 2. Gresham. Pri: 230v. Sec: 70-75-80v. 4A. Conservatively rated. Totally enclosed. Oil filled. 79s. 6d. Carr. 8/6
- No. 3. Redcliffe 'C' core. Pri: Tapped 200-240v. Sec: 3 x 17.5v. 1A. Tropically rated. 27s. 6d. P. & P. 4/6
- No. 4. Gardners. 'C' core. Pri: Tapped 200-240v. Sec: Tapped 2 x 2.5-5.6-4v. 2A., 2 x 2.5-5.6-4v. 1A. 25s. 0d. P. & P. 4/6
- No. 5. Gardners. 'C' core. Pri: Tapped 200-240v. Sec: Tapped 4-5-6-3v. 4A. 12s. 6d. P. & P. 3/6
- No. 6. Gresham. 'C' core. Pri: Tapped 200-240v. Sec: 6-3v. C.T. 5A., 2 x 6-3v. 3A. 29s. 6d. P. & P. 4/6
- No. 7. Redcliffe 'C' core. Pri: Tapped 200-240v. Sec: 6-3v. 3A., 6-3v. 2A. 15s. 0d. P. & P. 4/6
- No. 8. Redcliffe 'C' core. Pri: Tapped 200-240v. Sec: 2 x 125v. 260 m/A. Conservatively rated. 32s. 6d. P. & P. 5/-
- No. 9. Redcliffe 'C' core. Pri: Tapped 200-240v. Sec: 45v. 25 m/A., 1v. 0-5A. Conservatively rated. 15s. 0d. P. & P. 3/6
- No. 10. Parmeko. Pri: 230v. Sec: 65v. 85 m/A., 6-3v. 5A., 6-3v. 1A. Tropically rated. 25s. 0d. P. & P. 5/-
- No. 11. Gresham 'C' core. Potted type. Pri: 6-3v. Sec: 2-0-2v. 4A. 5kv. Wkg. 17s. 6d. P. & P. 3/6
- No. 12. Pri: 200-240v. Sec: 30v. 0-5A. Open type. Tag connections. 8s. 6d. P. & P. 2/6

SEND 6D. STAMP FOR LATEST PRICE LIST OF TRANSFORMERS, CHOKES, RECTIFIERS, CAPACITORS AND ELECTRONIC COMPONENTS.

HEAVY DUTY L.T. TRANSFORMER

Pri: 240v. Sec: 12v. 90A. Flying leads. Size 7 1/2 x 6 1/2 x 6 ins. £13.19.6d. Carr. 15/-

FOSTER VOLTAGE REGULATOR TRANSFORMER

Double wound. Pri: 200-240v. Sec: 0-270v. 20A. continuous. Built into metal case on wheels. Overall size 11 x 9 1/2 x 19 1/2 ins. Perfect conditon. ONE ONLY. £35 ex warehouse

AUTO TRANSFORMERS

240v.-110v. or 100v. Completely Shrouded fitted with Two-pin American Sockets or terminal blocks. Please state which type required.

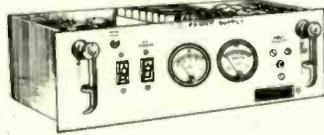
Type	Watts	Approx. Weight	Price	Carr.
1	80	2 1/2 lb	£1 17 6	4 6
2	150	4 lb	£2 7 6	5 0
3	300	6 1/2 lb	£3 7 6	6 0
4	500	8 1/2 lb	£4 15 0	6 6
5	1000	15 lb	£6 12 6	7 6
6*	1750	25 lb	£13 10 0	10 6
7*	2250	30 lb	£16 10 0	12 6

*Completely enclosed in beautifully finished metal case fitted with two 2-pin American sockets, neon indicator, on/off switch, and carrying handle.

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(ELECTRONICS) LTD.

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AMERICAN HIGHLY STABILISED POWER SUPPLY UNIT



Regulation between 7-15 volts D.C. at 20 amps. Fitted 0-30 D.C. ammeter, 0-15 D.C. voltmeter and overload protection switch. Built to a very high specification. Bench or rack mounting. Size 19 x 8 x 17 ins. A.C. input 110v. 50 cycles. Ex equipment but guaranteed in perfect condition. Maker's price in excess of £200. Our price £25. Carr. 30/- 240/110 volt, 400 watts, Mains Transformer available if required. £3 extra.

HIVOLTRONIC LTD. High Rate Discharge Capacitors

0-25 mfd. 20kv. wkg. 1 1/2 x 7 1/2 x 9 ins. Brass strip contact connections. Unused. Fraction of maker's price. £6 10s. Carr. 15/-

TEDDINGTON REFRIGERATION THERMOSTATS. Type QJ with control knob. 15/- P.P. 3/6.

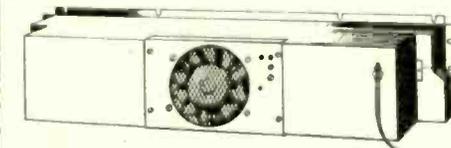
CRAMER CONTROLS SYNCHRONOUS GEARED MOTORS. 220-240v. A.C. 6 revs per minute. 17/6. P.P. 2/6.

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Manufactured by Papst. A.C. 220-240 volts. Complete with fibre-glass filter. Ex equipment. Guaranteed in perfect order. Size: 28 x 5 x 5 in., 59/6. Carr. 8/6.



FANS ONLY



Mounted on metal plate. Size 13 x 5 x 3 in. 45/- Carr. 5/-

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BERCO CERAMIC POTS. 1:5 KΩ 1 1/2 in. dia., 7/6. P.P. 2/-

BRAND NEW PANEL MOUNTING METERS

2-inch Square. 0-150 m/A. 15s. 0d. 0-1 m/A. 25s. 0d. 0-500 micro/A. 35s. 0d., 0-100 micro/A. 39s. 6d., 0-50 micro/A. 47s. 6d.
 2 inch Round. 1-0-1 m/A. Scaled. 150-0-150. 19s. 6d., 250-0-250 micro/A. 25s. 0d., 0-500 micro/A. 19s. 6d.
 2 1/2 inch Round. 50-0-50 m/A. 25s. 0d., 0-50 m/A. 17s. 6d., 0-100 m/A. 17s. 6d., 0-15v. A.C. 17s. 6d., 0-70 Amps, less shunt. 10s. 0d.
 1 1/2 inch Square. Level meters. 0-1 m/A. 17s. 6d.
 All meters by famous makers and guaranteed in perfect condition. Please add 2/- for Packing & Postage on all models.

SANGAMO WESTON

Special offer 3 1/2 inch Round Panel Meters. Double reading, 0-50 and 0-100 micro/A. Scaled 0-8 and 0-16 Kilovolts. Brand new in maker's cartons. List price over £5. Our price 25s. 0d. P. & P. 2/-

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Switch contacts, 15 amps., 250 volts A.C. Control knob can be set between 30 secs. and 6 mins. Complete with chrome bezel and knob. Brand new 17/6. P.P. 2/6.

AMERICAN WILLARD, miniature accumulators 6v. 1-2 A.H. size 2 x 1 1/2 x 4 ins. wt. 4.25s. 7/6 + 1/6.

SCOTCH MAGNETIC TAPE. Type 3M 459. 1/2 in. 3,600 feet. Suitable for video. Brand new in maker's sealed cartons. List Price £18/10/- Our Price £3/19/6. P.P. 5/-

DIGITAL HOUR METERS

6 figs inc. 1/10ths, 1/100ths 40v. A.C. but complete with transformer for 240v. A.C. operation. All in plastic case. Size 6 1/2 x 6 1/2 x 3 1/2 in. Condition as new 45/- P.P. 5/-



WE HAVE SEVERAL THOUSAND TRANSFORMERS ALWAYS IN STOCK—L.T., H.T., AUTO, VARIABLE, CONSTANT VOLTAGE, HEAVY DUTY, ETC. LET US KNOW YOUR REQUIREMENTS.

SPECIAL OFFER HIGH GRADE H.T. TRANSFORMERS

- No. 1. Woden 'C' core. Pri: Tapped 200-240 volts. Sec: 315-0-315v. 110 m/A., 175-0-175v. 25 m/A., 5v. 1-9A., 6-3v. C.T: 4A., 6-3v. 3-1A., 6-3v. 2A., 6-3v. 1A. Tropically rated. Table top connections. 50s. 0d. P. & P. 7/6
- No. 2. Redcliffe 'C' core. Pri: Tapped 200-240v. Sec: 400v. 290 m/A. Tropically rated. Table top connections. 59s. 6d. P. & P. 7/6
- No. 3. Redcliffe 'C' core. Pri: Tapped 200-240v. Sec: 300v. 300 m/A. Tropically rated. Table top connections. 39s. 6d. P. & P. 5/-
- No. 4. Gardners 'C' core. Pri: Tapped 200-240v. Sec: 300-0-300v. 66 m/A., 6-3v. 4A. Tropically rated. Table top connections. 30s. 0d. P. & P. 4/6
- No. 5. Gardners Potted type. Pri: Tapped 200-240v. Sec: 2 x 300v. 37-5 m/A. 4kv. wkg., 4v. 1A. 4kv. wkg., 4v. 0-3A. 29s. 6d. P. & P. 4/6
- No. 6. Gardners. Pri: Tapped 200-240v. Sec: 350-300-0-350v. 50 m/A., 0-4-6-3v. 3A. 1kv. wkg., 0-4-6-3v. 4A., 0-4-5v. 3A. Table top connections. 35s. 0d. P. & P. 6/6
- No. 7. Gresham 'C' core. Pri: Tapped 200-240v. Sec: 0-170-200v. 350 m/A., 200v. 350 m/A., 2 x 130v. 185 m/A. Tropically rated. Table top connections. 47s. 6d. P. & P. 7/6
- No. 8. Gardners. Pri: Tapped 200-240v. Sec: 450-0-450v. 180 m/A., 2 x 6-3v. 3A., 5v. 3A. Open type. Table top connections. 55s. 0d. P. & P. 7/6

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Neptune Series.
 50 H. 25 m/A. 10s. 6d. P. & P. 4/6. 15 H. 50 m/A. 10s. 6d. P. & P. 4/6. 10 H. 180 m/A. 17s. 6d. P. & P. 5/- 10 H. 120 m/A. 12s. 6d. P. & P. 4/6. 10 H. 75 m/A. 10s. 0d. P. & P. 4/6. 5 H. 150 m/A. 12s. 6d. P. & P. 5/- 5 H. 60 m/A. 8s. 6d. P. & P. 4/6. 0-7 H. 450 m/A. 12s. 6d. P. & P. 5/-
 Jupiter Series Swinging Chokes.
 34 H. 60 m/A. 70 H. 35 m/A. 2-8kv. D.C. wkg. 29s. 6d. P. & P. 6/6.

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Type 9000/39. Atlantic Series. Pri: 5 H. 12 m/A. Sec: 500 m/V. 15-5:1. 4-5:1. 8s. 6d. P. & P. 2/-

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180v. D.C. Approx. 1/2 in. pull. Size 1 1/2 x 1 1/2 x 1 1/2 ins. 5s. 0d. P. & P. 1/6. 50v. D.C. 7s. 6d. P. & P. 1/6.



ELECTRO METHODS 2-3v. A.C. CONTACTORS

1 Heavy Duty Change-over Contact. Size 2 1/2 x 1 1/2 x 1 ins. 7s. 6d. P. & P. 2/-



MAGNETIC DEVICES 6v. D.C. CONTACTORS

1 C.O., 1 H/D Make contacts. Size 2 x 1 1/2 x 1 ins. 7s. 6d. P. & P. 2/-



MICRO SWITCHES

Burgess Type CRK2-524. Lever operated. Make or break (3 tags). Three for 12s. 6d. P. & P. 2/- Many other types available.



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1004 ohms. 1 amp. Single tube slider 55s. 0d. P. & P. 7/6. 30 ohms. 1 1/2 amps. Single tube slider. Right angle geared drive. 17s. 6d. P. & P. 4/6. 758 ohms. 0-7 amp. Double tube. 55s. 0d. P. & P. 7/6.

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Max. A.C. input 36v., D.C. 8 amps, 29/6. P. & P. 3/6. Max. A.C. input 18v., D.C. 8 amps, 22/6. P. & P. 2/6. 4 amps 15/- P. & P. 2/- 2 1/2 amps, 9/6. P. & P. 2/- Supplied new and guaranteed. Not to be confused with surplus types.

TWIN TERMINAL BLOCKS

Air Ministry Type 5 C/430. Cartons of 50, 17/6. P. & P. 2/6.

T.C.C. VISCONOL TUBULAR CAPACITORS

1 mfd. 2.5 kv. D.C. wkg. at 60° C., 15/- 0.1 mfd. 8 kv. D.C. wkg. at 60° C., 7/6. 0.1 mfd. 5 kv. D.C. wkg. at 60° C., 5/6. 0.05 mfd. 10 kv. D.C. wkg. at 60° C., 7/6. 0.02 mfd. 12 kv. D.C. wkg. at 60° C., 7/6. P. & P. all types 2/- each.

HIGH CAPACITY TUBULAR ELECTROLYTICS

25,000 mfd. 12v. wkg., 12/6. 6,300 mfd. 63v. wkg., 8/6. 4,000 mfd. 60v. wkg., 7/6. 1,250 mfd. 180v. wkg., 7/6. P. & P. all types 2/- each.

AMERICAN OIL-FILLED CAPACITORS

8 mfd. 1,000v. D.C. wkg., 15/- P. & P. 2/6. 8 mfd. 600v. D.C. wkg., 8/6. P. & P. 2/- 4 mfd. 1,000v. D.C. wkg., 8/6. P. & P. 2/- 3 mfd. 1,000 mfd. 1,000v. D.C. wkg., 7/6. P. & P. 2/-

A.C. CAPACITORS

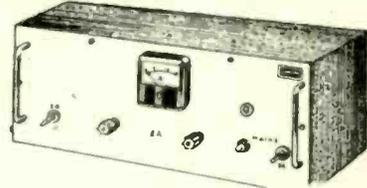
60 mfd. 275v. wkg., 37/6. P. & P. 5/-
 18 mfd. 300v. wkg., 12/6. P. & P. 3/-
 13 mfd. 250v. wkg., 7/6. P. & P. 2/-
 12 mfd. 250v. wkg., 7/6. P. & P. 2/-
 5 mfd. 400v. wkg., 6/6. P. & P. 2/6.

SPECIAL OFFER. BLOCK CAPACITORS

G.E.C. 8 mfd. 600v. D.C. wkg. Six for 29/6. Carr. 7/6. Dubliner. 1 mfd. 600v. wkg. Six for 9/- P. & P. 3/6. T.C.C. 2 mfd. 500v. wkg. Three for 7/6. P. & P. 2/6. T.C.C. 0.1 mfd. 500c. wkg. Six for 6/6. P. & P. 2/6.

L.T. SUPPLY UNITS TYPE S.E.S.

A.C. input 220-240 volts. D.C. output 12 or 24 volts 1.0 amp. rating. Selenium full wave bridge rectification. 3 inch scale ammeter, neon indicator, housed in strong metal case. Size 17 x 7 x 6 1/2 in. £14/10/-
L.T. SUPPLY UNITS TYPE S.E.6
 As above, but 50 volts 6 amps. £14/10/- Carr. 15/-



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BOX NUMBERS: Replies should be addressed to the Box number in the advertisement, c/o Wireless World, Dorset House, Stamford Street, London, S.E.1.

No responsibility accepted for errors.

Advertisements accepted up to MAY 9 for the JUNE issue, subject to space being available.

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BRISTOL TECHNICAL COLLEGE

Applications invited for the following vacancies, duties to commence as soon as possible:

Ref. No. T698/7/2 SENIOR TECHNICIAN (Grade T.3) in PHYSICS.

Ref. No. T698/10/2 TECHNICIAN (Grade T.2) in PHYSICS (2 posts).

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T.2 £765-£895

Starting salary dependent upon age, qualifications and experience. £50 or £30 p.a. extra payable to Candidates with appropriate National Certificate and C. & G. qualifications.

Applicants should be over 21 and preferably have some qualifications and experience of laboratory work.

38-hour, 5-day week with usual holiday and sick pay schemes. Opportunities for evening work with additional pay. Permanent pensionable posts; medical.

Further particulars and application forms (to be returned within fourteen days) from Registrar, Bristol Technical College, Ashley Down, Bristol, BS7 9BU.

Please quote appropriate reference number in all communications.

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Please state briefly, in writing, how each requirement is met. Nothing will be disclosed, unless you give permission after a confidential interview.

Development Engineer

radio telecommunications (Ireland)

This Irish company, employing about 200 but part of a major international electrical and electronic group, specialises in the design, development and quantity production of radio telecommunications and specialised peripheral test equipment, much of it unique.

The company seeks two radio communications development engineers who must have had experience in taking a project from initial specification through the design and development stages to final quantity production. They must be professionally qualified, either graduates or AMIERE and should have had some actual quantity production experience. Ideal age about 30. Salary £2000. Location Dublin. Please send details of age, qualifications and experience to P. J. H. Fryer quoting ZH.80552.

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OXFORD AIRPORT • KIDLINGTON**

**Electrician
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It you are one of these, a job awaits you at C.S.E. (Aircraft Services), Kidlington. The work covers the preparation of Wiring and Components and the Installation into modern aircraft (including the Jetstream), of Radio and Electronic Systems Equipment.

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C.S.E. (AIRCRAFT SERVICES) LTD.
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OXFORD**

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ELECTRONIC TEST ENGINEERS

Our Test Department is responsible for testing and fault finding on a wide range of Marconi equipment; airborne communication and navigation aids; radar; broadcasting; and space, radio and line communications. There are excellent career prospects both within the Test Department and in other areas of the expanding Marconi Company.

We wish to hear from men with a proven career record in the electronics industry who, preferably, should have gained qualifications to at least C & G Telecommunications Intermediate standard.

Members of H.M Forces in the electronic fitter category would find these positions of particular interest.

Marconi



Please write for brochure to Mr. M. J. Shepherd, Personnel Officer, Chelmsford Works, The Marconi Company Limited, Marconi House, Chelmsford, Essex, quoting reference WW/E/61.

Member of GEC-Marconi Electronics Limited

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THE WORLD'S FINEST
PROFESSIONAL PORTABLE TAPE RECORDER

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GOOD SALARY AND CONDITIONS.

EXISTING HOLIDAY ARRANGEMENTS HONOURED.

Please send full details in writing to:—

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UNIVERSITY OF SOUTHAMPTON

Department of Electronics

An EXPERIMENTAL OFFICER experienced in digital techniques required to take charge of the day-to-day running of several research and teaching projects. A number of the projects are linked to a Honeywell 516 computer and familiarity with a computer or similar system is essential. Applicants should be graduates or hold associate membership of a relevant professional institution.

A JUNIOR TECHNICIAN is required to work in the field of microelectronics. Some knowledge of chemistry or photography is desirable for this post, but full training will be given. Four G.C.E. 'O' levels required.

Salary scale for Experimental Officers rises to £1,930 per annum plus F.S.S.U.

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Applications, giving details of age, qualifications, experience and the names of two referees, should be sent to the Deputy Secretary, The University, Southampton, SO9 5NH, quoting reference WW.

Government of ZAMBIA

REQUIRES

RADAR ENGINEER

for the Department of Meteorology, Ministry of Transport, Power and Works, on contract for one tour of 36 months in the first instance. Commencing salary according to experience in scale Kwacha 2,736 (£Stg. 1,596) rising to Kwacha 3,216 (£Stg. 1,876) a year, plus an inducement allowance of £Stg. 568 - £Stg. 615. Gratuity 25% of total salary drawn. A direct payment of £Stg. 268 - £Stg. 291 is also payable direct to an officer's U.K. bank account. Both gratuity and direct payment are normally TAX FREE. Free passages. Quarters at low rental. Children's education allowances. Liberal leave on full salary or terminal payment in lieu. Contributory Pension Scheme available in certain circumstances.

Candidates between 22 and 35 years of age, must

1. Have served a five years apprenticeship in radio and radar engineering, or
2. Possess a service Trade Certificate, or
3. Possess a City and Guilds Intermediate Certificate in Telecommunications Engineering or its equivalent.

Preference will be given to candidates experienced with

1. H.F. R/T transceivers radio-facsimile and radio-sonde,
2. S and X-band radar equipment.

Duties include:—

- a. Repair and maintenance of all radar sets and communications equipment for which he is responsible, plus the
 - b. Care and Maintenance of appropriate spares and stores.
- He may also be required to assist in installation work.

Write to CROWN AGENTS 'M' Dept., 4 Millbank, London, S.W.1, for application form and further particulars, stating name, age, brief details of qualifications and experience and quoting reference MzK/690222/WF

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ELECTRONICS

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Vacancies at RAF Sealand, near Chester
RAF Henlow, Bedfordshire
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Interesting and vital work on RAF radar and radio equipment for:

TELECOMMUNICATIONS TECHNICAL OFFICERS GRADE 3

Minimum qualification, ONC in electrical engineering or equivalent qualification.

Starting pay according to age, up to £1347 p.a. (at age 28) rising to £1521 p.a. with prospects of advancement to higher grades with pay scales up to £2,500 p.a.

RADIO TECHNICIANS

Minimum qualification, 3 years' training and practical experience in radio engineering.

Starting pay according to age, up to £1130 p.a. (at age 25) rising to £1304 p.a. with prospects of promotion to T.T.O. Grade 3 (above).

5 day week—good holidays—help with further studies—opportunities for pensionable employment.

Write for further details to: Ministry of Defence, CE3h(Air), Sentinel House, Southampton Row, LONDON, W.C.1, stating post required.

Applicants must be U.K. residents.

OXLEY 

**CHIEF
DRAUGHTSMAN**

A senior man is required to take charge of the Drawing Office of an expanding wholly British privately owned company engaged in the invention, design and manufacture of electronic components.

The modern factory, ideally situated in the Lake District, employs a very wide variety of talents and offers unequalled opportunities to a competent, educated, inventive and level headed man, preferably with a wide peripheral knowledge of physics and chemistry

The usual advantages of superannuation etc., are offered, and applicants, who are asked to send us a curriculum vitae including present salary, in confidence, will be considered and offered remuneration according to their merit.

OXLEY DEVELOPMNETS COMPANY LIMITED,
Priory Park, Ulverston, North Lancashire

TELEVISION ENGINEERS

for outside servicing with experience in closed circuit medical, scientific, or allied applications required. A knowledge of 1" Helical scan V.T.R.s and colour television would be an added advantage. Company car provided. Salary according to experience. Any further information and interview.

SIEREX LIMITED,
15/18 Clipstone Street, London W1P 8AE.
Telephone: 580 2464.

THE UNIVERSITY OF SUSSEX
SCHOOL OF BIOLOGICAL SCIENCES

**TECHNICIAN OR
JUNIOR TECHNICIAN**

Applications are invited for the post of Technician to build and maintain systems for the automatic control and recording of animal behaviour. Work will involve integration of electromagnetic and computer systems with simple mechanical and hydraulic equipment. Preference will be given to applicants with interests in either elementary programming, analysis or behavioural records, or running the experiments.

Salaries are in accordance with age, qualifications and experience within the ranges:

£373 to £575 for Junior Technicians
£692 to £1007 for Technicians

In addition, qualification allowances are paid for approved qualifications. Three weeks paid holiday plus University Closures. Applications should be sent in writing to: Laboratory Superintendent, School of Biological Sciences, The University of Sussex, Falmer, Brighton, BN1 9QH, quoting ref. no. 135/2.

MEDICAL RESEARCH COUNCIL
Laboratory of Molecular Biology,
Hills Road, Cambridge

which makes extensive use of on-line computer control requires **ELECTRONICS ENGINEER** holding HNC, or equivalent qualification, for design, construction and maintenance of electronic equipment.

The applicant should have experience of computer technology or digital electronics, or related fields.

Apply to the Administrative Secretary.

**Commissioning Engineers
and Installers**

TRANSMISSION DIVISION

In spite of an excellent response to our recent advertisement a continuing expansion projecting into the foreseeable future demands that we seek additional staff.

Opportunities exist for commissioning and installation staff with experience of carrier systems to join a well established team working on transmission contracts both in the U.K. and overseas.

The Transmission Division's growth and its heavy commitments also create openings for less experienced engineers with a good transmission background who would be prepared to accept responsibility after a period of field training.

If you meet any of the above mentioned requirements we shall be pleased to hear from you. Please telephone V. S. Klein, Installation Manager or write stating age and giving details of qualifications and experience quoting reference number BEE/393/E to the Personnel Officer, Personnel Department, The Plessey Company Limited, Beeston, Nottingham NG9 1LA tel. Nottm. 254831 Ext. 4497.

PLESSEY ELECTRONICS



ELECTRONIC TECHNICIANS

Marconi

Can offer you

NON-TIED HOUSING IN A NEW TOWN
ATTRACTIVE SALARY
ANNUAL SALARY REVIEWS
GOOD WORKING CONDITIONS
37-HOUR WORKING WEEK

At Basildon we have a number of vacancies for technical test staff to work on advanced aeronautical electronic systems, maintenance and building of test equipment and other major projects. These positions will be of particular interest to men with experience of transmitters; receivers, aerials, closed circuit T.V. or digital systems.

Please telephone or write for an application form to:—

Mrs. B. Bridgen, Personnel Officer, The Personnel Dept., The Marconi Company Limited, Christopher Martin Road, Basildon, Essex. Phone: Basildon 22822.

It's Racal 'quality year'

And we are looking for good quality
Service Engineers
 to help us maintain our standards of
 Test Equipment service.

Specification:-

Wide general experience
 Good knowledge of circuit applications
 Experience with H.F. S.S.B.
 Communications Test Equipment.

Optional Extras:-

City & Guilds or O.N.C. or H.N.C.

Power Consumption:-

£1100 - £1300

Applications in writing please to:-

RACAL

THE RACAL GROUP

Mr. P. Cousins,
 Group Personnel Manager,
 Racal Electronics Limited,
 Western Rd., Bracknell, Berks.



REDIFFUSION

REDIFFUSION VISION SERVICE LTD
 ST. HELENS AUCKLAND. BISHOP AUCKLAND Co. DURHAM.

Senior TEST ENGINEER— TELEVISION RECEIVER MANUFACTURE

Due to a promotion, Rediffusion Vision Service Limited, which is a large scale producer of Television Receivers, now require an experienced Test Engineer. He will be responsible to the Production Manager for taking charge of all fault-finding staff engaged in manufacture. Duties will include training and instruction of test staff and liaison with the Group Engineering Department.

EXPERIENCE AND QUALIFICATIONS

Full familiarisation with monochrome television techniques including the use of transistors is essential. Knowledge of colour techniques and experience in a similar position is desirable. H.N.C. or equivalent preferred but lack of formal qualification will not debar a suitable applicant.

SALARY

Subject to negotiation with a minimum of £1,500 per annum. Housing assistance and removal expenses are available.

Applications in confidence to:

**Mr. J. W. Lunken, Manager,
 Rediffusion Vision Service Limited,
 Trading Estate, St. Helens Auckland,
 Bishop Auckland, Co. Durham.**

*A Member Company of the Rediffusion
 Organisation*

SERVICE TECHNICIANS

Experienced Electronic Engineers, minimum qualifications O.N.C./City and Guilds or 2/3 years' Bench experience, to service and repair a wide range of electro-acoustic instruments. Driving experience essential. Excellent salary and opportunities for advancement.

Write or telephone for immediate interview:

Personnel Department,
Amplivox Limited,
Beresford Avenue,
Wembley, Middlesex.
Telephone 902-8991.

BROADCAST RELAY ENGINEERS

required for the

ISLAND OF MASIRAH

(Off the Coast of MUSCAT and OMAN)

For an unaccompanied tour of duty of 1 year preceded by about a month in U.K. for familiarisation, documentation and medical clearance.

Total emoluments in the range £2,436-£3,079

for service on the Island. Actual level within range will depend on experience and marital status.

Engineers experienced in the operation and maintenance of high-power broadcast transmitters and who are of Third Year City and Guilds Telecommunications Technical standard are invited to apply for full particulars to:

The Personnel Officer,
Diplomatic Wireless Service,
Hanslope Park, Wolverton, Bucks.

COMMUNICATION & CALL SYSTEMS

Speech & Visual

Our steadily increasing volume of business, at home and overseas, now creates a requirement for additional engineering staff. We have immediate vacancies for Senior and Junior engineers with good practical experience in any of the following aspects of the work:

- System design.
- Planning and Estimating.
- Installation control.
- Test and commissioning.

The work is varied and interesting, with frequent opportunities for travel, and for contacts with other organisations. Applications, which will be treated in strict confidence, should be sent to:

BRITISH RELAY

The General Manager,
Special Services Division,
British Relay House,
41 Streatham High Road, S.W.16.

UNIVERSITY OF NOTTINGHAM

THE LANGUAGE CENTRE

PROGRAMME ASSISTANT

(male or female)

The Programme Assistant will be responsible for providing multiple copies of master tape recordings for use in the language centre. The ability to organise his or her own work to meet the programme time table will be expected. Some typing ability is necessary, and an interest in tape recording would be an advantage.

Salary will be on the Technicians Scale of £692 to £1,057 per annum.

Applications in writing quoting the names of two referees to the Staff Appointments Officer, University of Nottingham, University Park, Nottingham.

TECHNICIAN

required, for work in laboratories and in connection with use of visual and aural aids, at CITY OF LONDON COLLEGE, Moorgate, E.C.2.

Interesting and varied duties.

Salary within range £750-£1,115 p.a. according to age (minimum 21) and qualifications. Local government pension scheme.

Further details and application form from the Secretary.

PORT OF LONDON AUTHORITY

Radio Technicians

The Authority operate a complex telecommunications network which includes position fixing survey systems, V.H.F. and U.H.F. radio (both marine and shore-based), U.H.F. and micro-wave telemetric links, message switching and tape relay systems and low power real time digital computers. Staff are required to maintain this equipment at maximum efficiency and applications are invited from men interested in work which plays an important part in the smooth functioning of the Port.

Vacancies exist at Gravesend and King George V Dock, and successful candidates will be offered salaried positions on the Authority's permanent pensionable staff.

SALARY: £910 to £1,210 per annum. There are opportunities for promotion to a senior grade with salary up to £1,355 per annum. Commencing salaries will be in accordance with qualifications and experience. To ensure adequate coverage, a two-shift system is operated, for which an additional allowance is payable.

Applicants should have a sound basic knowledge of electronics and experience of installation and servicing in at least one of the following fields:

- ★ V.E.F., U.H.F., FM and AM (transmitters and receivers)
- ★ Radar and Microwave Links
- ★ Digital and Telemetry

Possession of ONC Electrical Engineering, City and Guilds Intermediate Certificate in Telecommunications plus Radio II, or an equivalent standard of technical training in civil or service fields is desirable but not essential, and the ability to drive would be an asset. Practical training on specialist equipment will be provided where necessary.

Application forms may be obtained from:

The Chief Engineer (Personnel), Port of London Authority, P.O. Box 242, Trinity Square, London, E.C.3.

TECHNICAL AUTHORS

Additional authors are required for important projects at our London and Portsmouth offices, including on-site opportunities, in the following fields:

- | | |
|---------------------|------------------------------|
| ■ Data processing | ■ Solid state radar |
| ■ Servo systems | ■ Telecommunications |
| ■ Navigational aids | ■ Electronic instrumentation |
| ■ Sonar systems | ■ Electro-mechanical systems |

Generous salaries are being offered, according to qualifications and experience.

Formal qualifications to H.N.C. or equivalent, and a minimum of three years in the engineering industry, will be an advantage.

Please apply in writing to:

The Technical Publications Manager,
Irwin Technical Limited,
109-123 Clifton Street, London, E.C.2.

SALES ENGINEER CO-AXIAL CONNECTORS

Precon is growing rapidly and we are making new appointments to handle the already wide range of co-axial connectors for the electronics and communications industries. New models are being introduced—we have a vigorous expansion policy and the prospects for advancement are excellent.

Fringe benefits include car, pension scheme, and 3 weeks holiday.

Applicants should have experience in selling electronic components but be ready to become involved in wider commercial duties.

Apply in confidence to:

Director and General Manager
Precision Connectors Ltd.
56-58 Green Street,
Forest Gate, London, E.7.
Telephone: 01-552 3405.



TRANSMITTER ENGINEERS

£1,485 - £2,365

We are looking for keen Engineers to join the Transmitter Section of our Station Design and Construction Department to assist with the heavy programme of work already under way to establish an extensive UHF network suitable for colour television. Most of our projects consist of three main stages:

PLANNING—this involves consideration of specification requirements, tender appraisals, discussions with manufacturers and production of suitable layout drawings for transmitters and ancillary equipment.

CONSTRUCTION—during this stage it is necessary to hold regular meetings to ensure that the work is progressing in accordance with the planned programme, and to agree many detailed points not covered in the specification.

Finally there is the **COMMISSIONING** stage, when comprehensive works and on site acceptance tests are carried out to ensure the specification has been complied with before the station is handed over to our operations and maintenance engineers.

The work will cover all the above aspects. The appointment is based at our Knightsbridge, London, Headquarters but a considerable amount of travelling throughout the United Kingdom will be necessary for which appropriate allowances will be paid.

The successful applicants will need to have had some relevant experience with RF circuitry and television techniques. They should also have the ability to write clear and concise reports and to work on their own initiative. An HNC or equivalent qualification would be an advantage.

Salary in above grade depending on qualifications, experience, etc. Excellent conditions of service.



Application forms from:—

The Personnel Officer
INDEPENDENT TELEVISION AUTHORITY
70 Brompton Road, LONDON, S.W.3

Quote reference no. WW/1136/H.69/70.

Closing date for completed application forms: 7th May, 1969

BBC

LABORATORY TECHNICIANS

required by BBC in the Test Laboratory of Equipment Department, Chiswick, W.4.

The duties include the inspection, alignment and performance checking of equipment used in the Television and Radio Services. Applicants should have experience in a development laboratory, or be familiar with the problems encountered when new designs of electronic equipment, made by small batch production methods, are being tested. Preference will be given to applicants who have an H.N.C. or equivalent qualification in electrical engineering, but for those who have made some progress toward one, day release facilities will be given to complete their studies to this level.

Salaries on appointment will be between £1,215 p.a. and £1,550 p.a. in grades having maximum salaries of £1,560 p.a. and £1,775 p.a. Technicians lacking qualifications or sufficient experience may be appointed at a lower grade.

Request for application form to Engineering Recruitment Officer, Broadcasting House, London W.1A 1AA, quoting reference 69.E. 2081. W.W.

RANK PRECISION INDUSTRIES

test equipment calibration engineer

Skilled in the comprehensive calibration and minor fault correction of the usual range of commercial test equipment. Salary from £1,250—£1,400 per annum according to experience, etc.

Apply to:



Personnel Manager
Rank Precision Industries Ltd.
Great West Road,
Brentford, Middlesex.
Tel: 01-560 1212

The Rank Organisation

Holders of The Queen's Award to Industry for 3 successive years.

ELECTRONIC ENGINEERS

Service Engineers required for Offices, throughout the United Kingdom, of well-known Company manufacturing Electronic Desk Calculating Machines. Applicants should possess a sound knowledge of basic Electronics with experience in Electronics, Radar, Radio and T.V. or similar field. Position is permanent and pensionable. Comprehensive training on full pay will be given to successful applicants. Please send full details of experience to the Service Manager, Sumlock Comptometer Ltd., 102/108 Clerkenwell Road, London, E.C.1.

REDIFFUSION

COLOUR TELEVISION FAULTFINDERS & TESTERS

We have a number of vacancies in our Production Test Departments for experienced faultfinders and testers.

Knowledge of transistor circuitry and experience with Colour Receivers together with R.T.E.B. Final Certificate or equivalent qualifications required.

These will be staff appointments with all the expected benefits.

Applications to:

**Works Manager,
Rediffusion Vision Service Ltd.,
Fullers Way South,
Chessington, Surrey (near Ace of Spades).
Phone: 01-397 5411**

Pye Telecommunications Ltd.
OF CAMBRIDGE

The largest exporters of VHF/UHF radiotelephone
equipment in the world require

ENGINEERS AND DESIGN DRAUGHTSMEN

Type of work and experience: We require electronic engineers and design draughtsmen to join teams engaged in the design and development of fixed mobile and portable UHF and VHF transmitters and receivers. These teams are responsible for all aspects of designing and development through to the production line.

Applicants should have experience in economic design for quantity production in the same or similar field of activity.

Education. Appropriate degree or diplomas preferred or proven experience of comparable level will be considered.

Age: 20-40 years.

Company contribution Pension Scheme.

Applications should be submitted to PERSONNEL MANAGER

Pye Telecommunications Ltd

Newmarket Road, Cambridge. Tel: 0223 61222



An immediate vacancy occurs at
**THE WIRELESS COLLEGE,
COLWYN BAY, NORTH WALES**
for an additional Instructor to assist in preparing students for P.M.G. examinations. The primary responsibility will be the theoretical instruction on the technical electricity section of the syllabus. Applicants must hold a P.M.G. Certificate and should have a sound theoretical knowledge. Recent Marine operating and/or teaching experience is desirable, but not essential.
Write in the first instance to The Principal.

TECHNICAL AUTHORS

A Technical Publications Contractor has vacancies in their Home Counties offices and on site for personnel to be engaged in the preparation of manuals for a wide range of electronic and allied equipment to Ministry and Commercial requirements. Applications are invited from practising or aspiring authors with relevant experience. Box No. 5056.

BATH UNIVERSITY OF TECHNOLOGY
School of Chemistry and Chemical Engineering

EXPERIMENTAL OFFICER IN ELECTRONICS

Applications are invited for the above post. Duties include the design and construction of special purpose electronic equipment for research projects and the maintenance of electronic equipment within the School. The School has an on-line PDP8/K70 computer and it is intended to use this in conjunction with undergraduate teaching and post-graduate research projects. Although candidates should have an interest in computer systems, previous experience with on-line computers is not essential, since training in relation to PDP8 computer maintenance can be arranged. The School also has several other facilities including Nuclear Magnetic Resonance, Mass Spectrometry, Infra-red and Ultra-violet Spectrometry, Electron Spin Resonance Equipment and Chromatography.

Experience in solid state electronics and modern construction and wiring techniques is essential.

Starting salary will be within the range £1,435-£1,715 per annum, for suitably qualified candidates.

Application forms from Registrar (S), The University, Claverton Down, Bath, quoting reference 69/20.

RADIO TECHNICIANS

Vacancies to be filled by October, 1969

A number of suitably qualified candidates are required for unestablished posts, leading to permanent and pensionable employment (in Cheltenham and other parts of the UK, including London). There are also opportunities for service abroad.

Applicants must be 19 or over and be familiar with the use of Test Gear, and have had practical Radio/Electronic workshop experience. Preference will be given to such candidates who can also offer "O" Level GCE passes in English Language, Maths and/or Physics, or hold the City and Guilds Telecommunications Technician Intermediate Certificate or equivalent technical qualifications. A knowledge of electro-mechanical equipment will be an advantage.

Pay according to age, e.g. at 19—£869; at 25—£1,130.

Prospects of promotion to grades in salary range £1,217-£2,038. There are a few posts carrying higher salaries.

Annual Leave allowance of 3 weeks 3 days rising to 4 weeks 2 days. Normal Civil Service sick leave regulations apply.

Application forms available from:
**Recruitment Officer (RT 3),
Government Communications Head-
quarters,
Oakley, Priors Road,
CHELTENHAM, Glos, GL52 5AJ.**

CENTRAL MIDDLESEX GROUP HOSPITAL MANAGEMENT COMMITTEE

NEW POST—ULTRA-SONIC TECHNICIAN

This is the first post of its kind and will attract a man with a strongly developed interest in electronics who wishes to consider the application of ultra-sonics to medical examinations.

The successful candidate will be required to work on his own initiative, be capable of handling patients and prove able to conduct ultra-sonic examinations single-handed on occasions. He will also be required to develop, under supervision, new electronic apparatus.

Possession of a car is essential and a car user allowance will be payable.

Further details and application forms available from: Group Secretary, Central Middlesex Hospital, Park Royal, N.W.10.

ELECTRONICS DESIGN ENGINEERS SENIOR DESIGN DRAUGHTSMEN

are required to work on a variety of challenging problems in a rapidly expanding company. An ability to assume a large degree of individual responsibility as part of integral design team is required or will be encouraged and developed.

Our design projects include micro-electronics, digital computers, static inverters, power supplies and complete Systems Designs both Ministry and Commercial. Realistic salaries will be proportional to general ability. For further details and interview for either position please reply in writing to:—



Personnel Officer,

GRESHAM LION GROUP LIMITED,
TWICKENHAM ROAD,
HANWORTH, MIDDLESEX.

RADIO ENGINEERS

required by the GOVERNMENT OF ZAMBIA, Department of Civil Aviation, Ministry of Power, Transport and Works, on contract for one tour of 36 months in the first instance. Commencing salary according to experience in scale Kwacha 2736 (£Stg.1596) rising to Kwacha 3216 (£Stg.1876) a year, plus an Inducement Allowance of £Stg.568-£Stg.615. A Direct Payment of £Stg.268-£Stg.291 is also payable direct to an officer's U.K. bank account. Both gratuity and direct payment are normally TAX FREE. Free passages. Quarters at low rental. Children's education allowances. Generous leave on full salary or terminal payment in lieu. Pension scheme available under certain circumstances.

Candidates must be under 55 years of age and should possess 8 years relevant experience following:—

- (i) an apprenticeship of 5 years, or
- (ii) possession of a Service Trade Certificate, or
- (iii) possession of an A.W.O.A. or I.C.A.O. certificate of competency or its equivalent.

In addition, candidates must have a sound knowledge of the theoretical principles of and experience in the maintenance of at least FOUR of the following groups of Communications, CMA Navigational and Surveillance Systems.

1. Medium powered H.F. Transmitters and associated Receivers: Frequency Shift Keying, S.S.B. and D.S.B.

Equipment, Medium Frequency Non-Directional Radio Beacons.

2. Low and High powered V.H.F., A.M. Equipment.
3. V.H.F. Omni range: Automatic VHF Direction Finders. Distance Measuring Equipment.
4. Instrument Landing System.
5. Radar X and S Band Terminal and P.P.1 Talk Down Equipment.
6. Audio and Remote Control Equipment; Public Address Equipment; Airport Magnetic Tape Recorders; Inter Office Communication; Underground Control Cables; Impulse and D.C. Switching Systems.
7. Teleprinter Telegraphy (torn tape) and associated Page Printers; Tape Recorders (autoheads); Printing Reproformers and Associated Switching Equipment.

Duties include the maintenance, overhaul and installation of ground terminal radio communication equipment and navigational aids at Airports and Flight Information Centre. Possession of a valid driving licence will be an advantage.

Apply to CROWN AGENTS, M. Dept., 4, Millbank, London, S.W.1., for application form and further particulars, stating name, age, brief details of qualifications and experience and quoting reference M2Z/690315/WF

**UNITED SHEFFIELD HOSPITALS
ROYAL INFIRMARY, SHEFFIELD S6 3DA
ELECTRONICS TECHNICIAN**

Applications are invited for the position of Electronics Technician, to work on a research project in the University Department of Surgery in association with the Regional Medical Physics Department. The Technician will work in an electronics laboratory on design and development of equipment to be used in the clinical research. Applicants are expected to have O.N.C. or H.N.C. in Applied Physics or Electrical Engineering or equivalent qualifications, with some practical experience in electronics. Salary will be on the Medical Physics Technician Scale V or IV (£711 to £1,050) depending on qualifications and experience. Applications giving names and addresses of two referees, to the Superintendent quoting Ref. 137.

**Independent Specialist Radio,
Television, Audio,
Tape, etc., dealer**

requires a young engineer, preferably minimum C. & G. Inter., to reinforce staff of increasingly busy Service Department. A conscientious and adaptable extrovert able to make good use of a comprehensive range of test gear and having a clean driving licence will be rewarded on a five-day week basis and will have the pleasure of working with similarly orientated colleagues.

Write in confidence to Managing Director, The Studio (Abingdon) Ltd., The Square, Abingdon, Berkshire, giving full background details and indicating availability for interview. All applications will be answered. [169]

Technical Author

A vacancy within the Publicity Department of the Radio Systems Division has arisen for a Technical Author.

Applicants, whose minimum qualifications should include O.N.C. or equivalent, will ideally have a knowledge of radio and electronic engineering. The successful applicant will be required to assist in the writing of technical sales proposals on the systems and equipment manufactured by the Division. Assistance in this task will be given by a creative team of engineers, artists and printers.

Generous salaries according to experience and qualifications will be negotiated and there are excellent staff benefits within this progressive Company.

Applications, giving a brief career history, and quoting Ref. ILF/755/E to: The Technical Staff Manager, The Plessey Company Limited, Ilford, Essex

PLESSEY ELECTRONICS



**ELECTRONICS DESIGN
DEVELOPMENT ENGINEERS**

Needed for work on advanced systems for voltage and current regulation at large power levels. Applicants should have H.N.C. as minimum qualification, and preferably some industrial experience. Assistance with housing is available if needed.

LABORATORY TECHNICIAN

Needed to assist in the development of voltage regulating and allied equipment. The successful applicant will have at least O.N.C. in Power Electrical Engineering (or an equivalent qualification), and will find some familiarity with simple electronics and closed loop control principles useful. As a member of a small but enthusiastic team, working in a rapidly changing technology, he will need to show drive and initiative which he will find well rewarded both by job interest and by a salary properly matched to his qualifications and abilities. Housing assistance is available.

Write with career details to:—

**The Technical Director,
BRENTFORD ELECTRIC LIMITED,
Manor Royal, Crawley, Sussex.**

**PRODUCTION TEST
ENGINEERING**

Due to our successful Research and Design work many exciting new projects are entering a production phase and we require Engineers and Technicians to participate in this work.

Minimum qualifications required are a basic understanding of Transistor circuitry enabling testing to specification to be carried out on our Data Processing and Servo Control Systems, etc.

Electrical Engineering Certificates an advantage, but not essential if experience in a similar activity can be offered.

Apply:

**Personnel Officer
RECORDING DESIGNS LTD.
Blackwater Station Estate
Blackwater, Camberley, Surrey
Telephone Camberley 24622**





We have vacancies for
EXPERIENCED TEST ENGINEERS

in our Production Test Department. Applicants are preferred who have experience of Fault Finding and Testing of VHF and UHF Mobile Equipment. Excellent opportunities for promotion due to expansion programme.

Please apply to Personnel Manager

PYE TELECOMMUNICATIONS LTD.

Cambridge Works, Haig Rd., Cambridge. Tel: Cambridge 51351 Ext. 355

ARE YOU EXPERIENCED..... in

Circuit Design or Systems Development—earning £1,200 to £2,500 and considering relocation?

Are you a Technical Sales Engineer, Test Engineer or Production Engineer perhaps unrecognised or poorly rewarded in your present position?

Have you special skills which are not fully utilised on your present job?

Then do you know that Electronics Appointments is constantly in touch with almost 800 companies in the electronics field, covering all aspects of electronic engineering at all levels.

Unique opportunities exist for you to obtain the best available job, with excellent prospects, in the area of your choice.

The service is free and confidential, you need only telephone or write for full details.



**ELECTRONICS
APPOINTMENTS LTD.**

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SEISMIC OBSERVERS

with analogue or digital field experience required for overseas service on land or sea, by

**GEOPHYSICAL SERVICE
INTERNATIONAL**

who offer a good salary and foreign bonus, ample leave on full pay and foreign bonus, medical insurance scheme, life insurance, profit sharing and a pension plan. Those interested please write to:

The Personnel Manager

Geophysical Service International Ltd.

Canterbury House, Sydenham Rd.,

Croydon, Surrey

quoting ref. 12/68, or telephone

01-686 6511



THE EUROPEAN SPACE RESEARCH ORGANISATION (ESRO)

requires for its Sounding Rocket Launching Range (ESRange) at Kiruna (Sweden)

Head of Operations Division

The holder of this post is expected to be a qualified engineer with univ. degree or equivalent (preferably in electronics or aeronautics) and with 5 to 10 years' experience in sounding rocket operations or missile testing.

His activities will cover: launching forecasts, technical information and liaison with users of the Range, preparation, co-ordination, checking, and reporting of launching procedures, maintenance and preparation of launching facilities and rockets, and directing recovery.

He will be in charge of app. 10 engineers and technicians and directly responsible to the Head of ESRange.

For the Instrumentation Division

2 electronic engineers with univ. degree or equivalent and appropriate prof. experience.

1. Head of Division

Responsible to the Head of ESRange for utilisation, maintenance and planning of a £2m. installation and in charge of a staff of 40 electronics engineers and technicians. He must have relevant experience in management and of electronic equipment systems including:

- telemetry receiving station
- tracking radar with digital computer
- timing and time-code systems
- line and radio communications
- riometer, magnetometer, ionosonde, photometer, etc.
- calibration and maintenance laboratory

2. Head of Communication and Timing Section

Candidates for this post must have had experience with modern systems of radio communication, frequency monitoring, payload recovery, timing systems with atomic clock, etc. They will also be responsible for a low altitude wind measurement system.

All candidates for the above posts must be fluent in at least one of the two official languages of the Organisation (English and French) and have a working knowledge of the other.

Attractive salary, special post allowance and leave according to international contract terms.

For application form and further information please apply to: **The Head of Personnel, ESOC, D-61 Darmstadt, Robert-Bosch-Str. 5, Germany.**



**RADIO & TELEVISION SERVICING
RADAR THEORY & MAINTENANCE**

This private College provides efficient theoretical and practical training in the above subjects. One-year day courses are available for beginners and shortened courses for men who have had previous training.

Write for details to: The Secretary, London Electronics College, 20 Penywern Road, Earls Court, London, S.W.5. Tel.: 01-373 8721.

WEST HAM COLLEGE OF TECHNOLOGY

ROMFORD ROAD, STRATFORD, LONDON, E.15

Telephone: 01-534 4545 ext. 599

**SECOND SYMPOSIUM ON
FIELD EFFECT TRANSISTORS**

Papers on:

Technology, Design, Measurements and Applications of MOS and Junction devices, in discrete and integrated form.

6th and 7th MAY, 1969

Fee: £6.6.0 (including lunch)

**NEWCASTLE UPON TYNE
POLYTECHNIC (Designate)**

RUTHERFORD COLLEGE OF TECHNOLOGY

B.Sc. ELECTRICAL AND ELECTRONIC ENGINEERING
(Honours and Ordinary)

B.Sc. PHYSICAL ELECTRONICS (Honours and Ordinary)

M.Sc. ADVANCED EXPERIMENTAL PHYSICS

Further details of these and other courses and of residential accommodation available, may be obtained from Administrative Officer, Rutherford College of Technology, Ellison Place, Newcastle upon Tyne, NE1 8ST quoting WW 693

**TELEVISION RECEIVER
MAINTENANCE—ZAMBIA**

The leading television hire service organisation in Zambia invites applications from suitably qualified service engineers for appointment as Service Manager (designate). Qualifications required for this post are eight years in an approved post, plus a City & Guilds certificate in electronics or an equivalent technical qualification. Consideration will be given to applicants, preferably single, who can submit evidence of a high standard of theoretical knowledge, and practical experience which would enable them to undertake the duties attached to the post, including ability to assist with the training of local nationals in the skills of television receiver maintenance. A contract for an initial tour of three years will include a salary not less than K4,000 p.a. (£2,320 equivalent Sterling p.a.), company accommodation at subsidised rental or an allowance in lieu, 30 days paid leave p.a., accumulative up to 90 days, passages paid, free medical, contributory provident fund. An appointment to a station on the Copperbelt will be made subject to issue of a Zambia Immigration Work Permit.

Applications, stating age, availability and briefly how the above requirements are met should be addressed to "Zambia, Ref: GM/050/69/JRDS, c/o Bush Murphy Export Limited, Shanowen Road, Whitehall, Dublin 9, Ireland." Those ultimately selected for interview in Dublin or London will be asked to complete a formal application.

SITUATIONS VACANT

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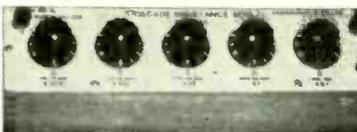
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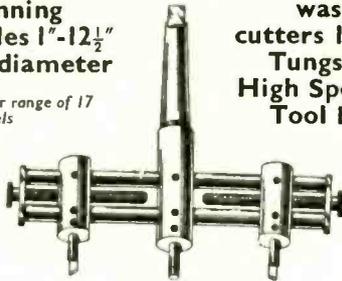
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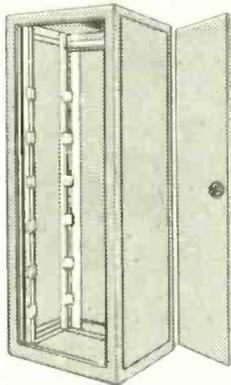
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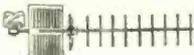
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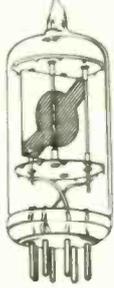
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