

**Radio Frequency Bridge** with its Low Impedance Adaptor reads a wide range of L, C and R values at frequencies from 15kHz to 5MHz, generally to 1%. Special Adaptors, Q601 series, for measuring transistor parameters. Two or three-terminal connections, balanced or unbalanced.

B 601



**VHF Admittance Bridge** covering 1MHz - 100MHz measures conductance from 0 - 100 millimhos and susceptance from -230pF to +230pF, with an accuracy of 2%. Two or three-terminal connections, balanced or unbalanced. Adaptor Q801A for transistor parameters.

B 801 B



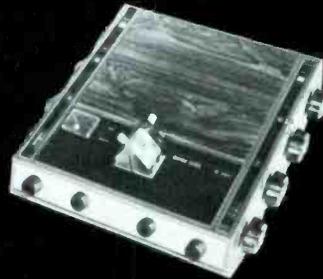
**Universal RF Bridge** measures real and quadrature terms of any immittance to 1%, without frequency dependence, from 100kHz to 10MHz. Includes standards of R, C and L. Unique magnetic potentiometers give exceptional linearity and stability.

B 602



**Source & Detector** has single-knob tuning from 100kHz to 100MHz, with push-button attenuators for output level and input sensitivity. Ideal for B602, B601, B801B and B201. Available as SR268L, covering 46.5kHz to 46.5MHz.

SR 268



**Precision RF Bridge** measures capacitance to 0.1% accuracy, conductance to 0.2%. Operation centred on 1MHz but high performance is maintained from 100kHz to 5MHz. Plug-in source/detector units. AC or battery operation.

B 201



**Adaptors** are available to convert the block terminals or coaxial sockets of the B201 to the 14mm International Standard connectors, GR900. These permit the B201 calibration to be referred to internationally recognised standards.

AB 201

## High-frequency Bridges

The RF and VHF Bridges produced by Wayne Kerr are designed on the transformer ratio-arm principle.

This gives stable performance and makes available a third measurement terminal, thus overcoming most of the problems associated with the connection of an Unknown to a bridge at high frequency. All models read the real and quadrature terms simultaneously.

### WAYNE KERR

THE WAYNE KERR COMPANY LIMITED,  
Roebuck Road, Chessington, Surrey. Tel: 01-397 1131. Cables: Waynkerr, Chessington. Telex 262333

WW-001 FOR FURTHER DETAILS

Designers specify them for their reliability and modern styling.  
Buyers choose them for their competitive prices and delivery.

# Taylor panel meters

are selected by equipment manufacturers everywhere.



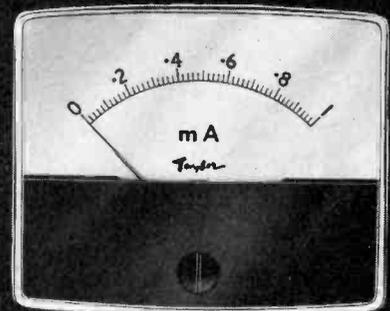
### Vista Series

Popular, reliable panel meters with robust phenolic mouldings and scale lengths from 1 3/4 in to 4 1/2 in. This range combines compact functional styling with easy readability and excellent performance. Mechanically interchangeable with the Fyneline range.



### Edgewise Series

Here's the latest in the range of three Edgewise panel meters, the Model 330 with a 2 1/4 in scale length. Ideal for today's crowded instrument panels, other scale lengths are 1 1/8 in (Model 11) and 1 3/4 in (Model 220).



### Fyneline Series

Adaptable versatile series with scale lengths from 1 3/4 in to 4 1/2 in. Contemporary styling and clear shadow-free readings ensure maximum readability. This modern range maintains the Taylor reputation for reliability and sensitivity.

Taylor offers a comprehensive range of moving-coil and moving-iron panel meters. The moving-coil meters feature the proven Taylor centre-pole movement with practically friction-free operation, inherent magnetic shielding

and high torque/weight ratio. They are sensitive, accurate instruments that conform generally to BS 89/54 with contemporary or conventional styling. Ask for the Panel Meter Shortform Catalogue.

### Taylor makes test equipment too!

Two typical models are Taylor Model 88B, a robust, wide-range multimeter with automatic cut-out and polarity reversal facility, and the



popular Taylor Type 127A, a pocket-sized multimeter for the service engineer and hobbyist. Ask for the Instrument Shortform Catalogue.



## Taylor Electrical Instruments Limited

- remember we're now at Dover! -

Archcliffe Road, Dover, Kent. Tel: Dover 2634 Telex: 96283



T 4 U

WW-066 FOR FURTHER DETAILS

TUBE TYPE	UNIT PRICE DM	UNIT PRICE US \$	TUBE TYPE	UNIT PRICE DM	UNIT PRICE US \$	TUBE TYPE	UNIT PRICE DM	UNIT PRICE US \$
GY 802	2.76	—49	PY 81 (17Z3)	1.24	—31		3.40	—85
GZ 32 (5V4)	1.72	—43	PY 202	1.32	—33		1.40	—35
GZ 34 (5AR4)	2.92	—73	PY 301	1.24	—31		2.00	—50
GZ 37	1.72	—43	PY 500	1.72	—43		2.00	—50
GZ 41	2.40	—60	PY 800	5.60	1.40		1.40	—35
HAA 91 = 12AL5			UABC 80 (28AK8)	5.44	1.36		1.20	—30
HABC 80 = 19T8			UAF 42 (12S7)	1.72	—43		1.80	—45
HBC 90 = 12AT6			UBC 41 (14L7)	1.68	—42		1.80	—45
HBC 91 = 12AV6			UBC 81 (15BD7)	2.56	—64		1.80	—45
HCC 85 = 17EV			UBF 80 (17C8)	2.36	—59		1.40	—35
HF 93 = 12BA6			UBF 89 (19DC8)	1.72	—43		1.28	—32
HF 94 = 12AU6			UBL 1	1.80	—45		1.80	—45
HK 90 = 12BE6			UBL 3	1.60	—41		2.48	—62
HL 90 = 19AQ5			UBL 21	3.28	—82		1.40	—35
HL 92 = 50C5			UC 92 (9AB4)	3.60	—90		1.60	—40
HL 94 = 30A5			UCC 85 (26AQ8)	2.08	—52		1.32	—33
HY 90 = 35W4			UCF 41	2.72	—68		1.20	—30
KY 80	4.00	1.00	UCF 81 (19D8)	2.08	—52		1.20	—30
LC 900 (31M5)	1.80	—45	UCH 11	2.72	—68		1.20	—30
LCF 80 (6LX8)	1.80	—45	UCL 11	1.64	—41		1.20	—30
LCF 801 (5G4)	1.80	—45	UCL 81	2.40	—60		2.60	—65
LCF 802 (6LX8)	2.64	—66	UCL 82 (50BM8)	1.84	—46		2.12	—53
LCL 82 (11BM8)	2.20	—55	UEL 51	3.60	—90		1.32	—33
LCL 84 (10DX8)	2.00	—50	UEL 71	2.08	—52		1.20	—30
LCL 85 (10GV8)	2.40	—60	UF 5	1.80	—45		1.20	—30
LF 183 (4EH7)	1.76	—44	UF 9	3.60	—90		1.20	—30
LF 184 (4EJ7)	1.76	—44	UF 41 (12AC5)	1.80	—45		2.60	—65
LL 86 (10CW5)			UF 80 (19BX8)	1.68	—42		2.12	—53
LY 88 (20AQ3)			UF 85 (19BY7)	1.68	—42		1.32	—33
LFL 200 (11Y9)	1.76	—44	UF 39 (12DA6)	1.60	—40		1.20	—30
PABC 80 (9AK8)	1.76	—44	UL 41 (45A5)	2.48	—62		1.20	—30
PC 86 (4CM4)	2.68	—67	UL 84 (45B5)	1.60	—40		2.60	—65
PC 88 (4DL4)	2.92	—73	UM 11	2.00	—50		2.12	—53
PC 92 (3AB4)	1.28	—32	UM 34/35	2.00	—50		1.60	—40
PC 96	1.28	—32	UM 80 (19BR5)	3.12	—78		1.60	—40
PC 97 (4FY)	1.28	—32	UY 1 (N)	1.76	—44		2.44	—61
PC 900 (4H)	1.28	—32	UY 11	1.20	—30		2.80	—70
PCC 84 (7A)	1.76	—44	UY 41	2.40	—60		2.08	—52
PCC 85 (9AQ8)	1.76	—44	UY 42	1.60	—40		2.24	—56
PCC 88 (7DJ8)	2.32	—58	UY 82 (55N3)	1.60	—40		1.76	—44
PCC 89 (7FC7)	3.60	—90	UY 85 (38A3)	1.60	—40		1.60	—40
PCC 189 (7ES8)	2.32	—58	UY 89	1.60	—40		1.60	—40
PCF 80 (9A8)			U 50 = 5Y3GT	1.64	—41		1.60	—40
PCF 82 (9U8A)			U 52 = 5U4GB	1.24	—31		1.60	—40
PCF 86 (7HG8)			U 70 = 6Y5GT	1.24	—31		2.08	—52
PCF 200 (8X9)			XC 900 (2HA5)	1.64	—41		2.24	—56
PCF 201 (8U9)			XCC 82 (7AU7)	1.64	—41		1.44	—36
PCF 801 (8GJ7)	2.20	—55	XCF 80 (4BL8)	2.24	—56		2.88	—72
PCF 802 (9JW8)	2.16	—54	XCF 82 (5U8)	1.76	—44		2.00	—50
PCF 805 (7GV7)	3.28	—82	XF 104 (3L7)	1.76	—44		2.64	—65
PCH 200 (9V9)	2.40	—60	XL 84 (8BQ5)	1.76	—44		1.20	—30
PCL 81	2.40	—60	XL 86 (8CW5)	1.68	—42		3 C 4 = DL 96	1.20
PCL 82 (16X6)	2.40	—60	XT 88 (16AQ3)	1.92	—48		3 CB 6	1.20
PCL 83	2.40	—60		2.40	—60			
PCL 84 (15X3)	1.76	—44						
PCL 85 (18GV8)	1.92	—48						
PCL 86 (14GW8)	2.08	—52						
PCL 200	3.64	—91						
PCL 805	2.08	—52						
PD 5								
PF 81								
PFL								
PL 31								
PL 81								
PL 82								
PL 83								
PL 84								
PL 91								
PL 31								
PL 51								
PL 51								
PL 51								
PL 51								
PL 511	5.68	1.42	1 AD 2	2.16	—54		3 JD 6	2.36
PM 84	1.84	—46	1 AH 5 = DAF 96				3 JH 6	1.36

# Tubes

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Whatever your language is, we understand that you ask for quality. Our SQ-Series of Television tubes gives you safety at no extra cost.

Since 1955 we offer a complete line of European and American type receiving & industrial tubes for worldwide export with off-the-shelf-service.

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# From L to X-band for marine, airborne and ground radar

The standard range of EEV duplexer components covers applications from L to X-band marine, airborne and ground radar systems. TR cells, TB cells, pre-TR cells, solid state limiters, monitor diodes . . . whatever your requirement, in narrowband, broadband or tunable types, EEV have it. Or, if it's a 'special' you need, we can almost certainly make it.

The precision manufacture of duplexers forms only part of EEV's massive experience in the whole field

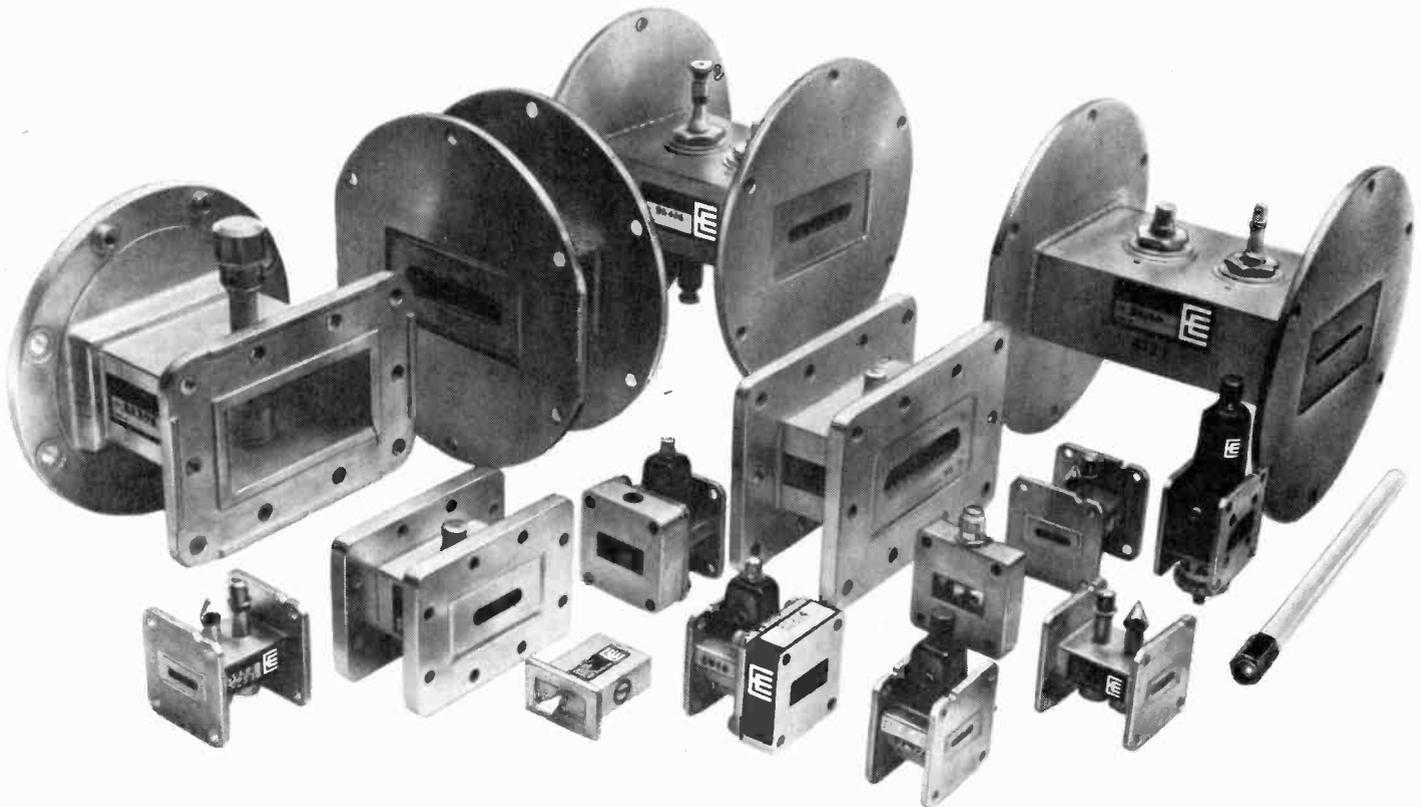
of radar. And we have delivery and service to match our capability.

If you would like a copy of the EEV guide 'Duplexer Devices'—or if you are interested in a particular component—then please post the coupon.

English Electric Valve Co. Ltd. Chelmsford, Essex  
 England. Telephone: 0245 61777. Telex: 99103  
 Grams: Enelectico Chelmsford



## see EEV's duplexer devices.



Product	Type No.	Band	Frequency range (MHz)	Peak power (kW)
Pre TR cells	BS834	—	2000–12000	2500
	BS870	L	1240–1370	2500
TR cells	BS456	S	2850–3050	1250
	BS824	S	2700–3100	250
	BS856	C	5300–5700	250
	BS156	X	9000–9600	200
	BS452	X	9310–9510	100
	BS810	X	9250–9550	75
TB cell	BS310	X	9375	5–200
TR Limiter cell	BS814	X	9000–9700	200
Solid state microwave switches	BS392	S	2925–3075	0.5
	BS460	X	any 100 MHz	0.5

To: English Electric Valve Co. Ltd., Chelmsford, Essex, England.  
 Please send a copy of 'Duplexer Devices'.  
 I am interested in a device with the following parameters:

Frequency \_\_\_\_\_ Power \_\_\_\_\_ Type \_\_\_\_\_

Name & Position \_\_\_\_\_

Company \_\_\_\_\_

Address \_\_\_\_\_

Tel. exchange or code \_\_\_\_\_

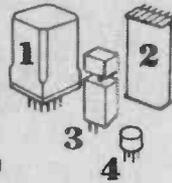
Number \_\_\_\_\_ Ext. \_\_\_\_\_

ENGLISH ELECTRIC VALVE CO LTD



## FOUR NEW COMPONENTS FROM ASSOCIATED AUTOMATION

**1 Industrial Relay Type MR**  
A.C. or D.C. operation. Panel mounting or plug-in to octal type socket. Will last for up to 5 million operations with 1, 2 or 3 poles switching up to 10 amps. Compact, lightweight and cheap.



**2 Dry Reed Relay Type ERTN**  
Range of up to 12 poles. Switching capabilities up to 50 VA breakdown voltages up to 1500 V.A.C. Life expectancy at contact rating 7.5 VA,  $100 \times 10^6$  operations. Cheap to buy, capable of fast action with low power consumption and stable operation.

**3 Miniature Dry Reed Push Button Switch Series 500**  
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**4 Hermetical Saalec Commercial Relay Type TPC**  
A.T.O.5 transistor can envelope giving high isolation switching. Resists shock and vibrations, operates on power down to 40mW. Switching capacity 1 amp at 23 V.C. to low voltage (single and double pole). Economical price though comparable with any military equivalent.

Three relays and a switch, designed by Associated Automation to cut your switching costs. Built to the highest standards of engineering, these components join the already comprehensive range of switches and relays for all communication and control purposes. All economically priced and backed by Britain's most outstanding engineering service. Send in the coupon and we'll let you have all the information you require

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Electromagnetics  
70 Dudden Hill Lane, London, N.W.10.

Please send me your fully illustrated literature on (tick box applicable)

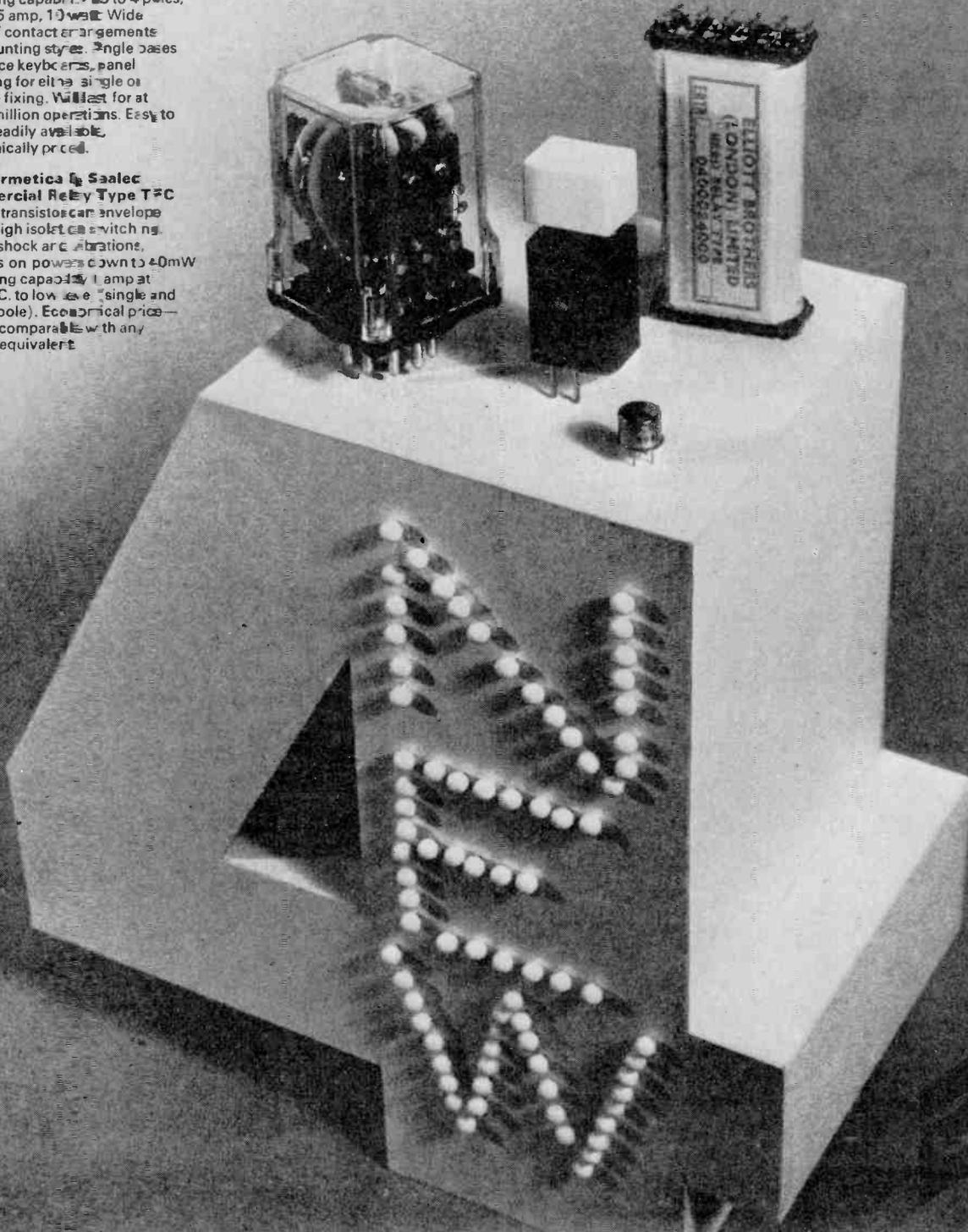
1  2  3  4

NAME \_\_\_\_\_

COMPANY \_\_\_\_\_

ADDRESS \_\_\_\_\_

W 43/71



WW-009 FOR FURTHER DETAILS

# UHF klystron efficiency? You can rely on it with EEV.

For reliable UHF klystron performance choose from the largest range available today. The EEV range. 40kW, 25kW, 10kW, 7kW and 5kW.

Each one offers economy and ease of use, solid-state compatibility and, above all, efficiency—even at low drives.

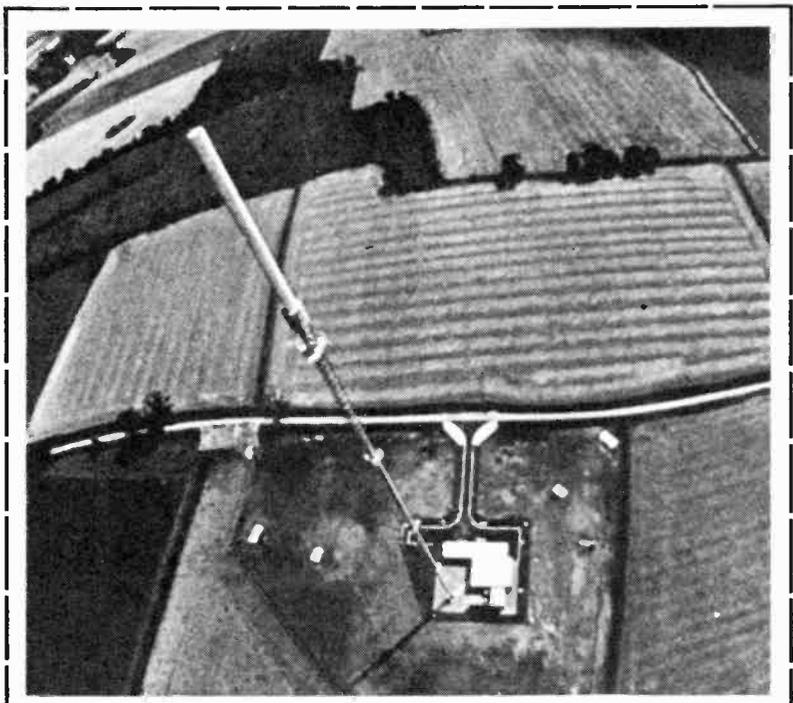
Broadcasting authorities around the world are using



EEV klystrons for UHF television – proving their operational flexibility, reliability and efficiency in climatic conditions as varied as those of Australia and Finland.

To get the full facts about the tube *you* need, please post the coupon.

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To: English Electric Valve Co Ltd, Chelmsford, Essex, England

Please send EEV data on UHF television amplifier klystrons.

I am interested in a klystron with the following parameters:

Frequency \_\_\_\_\_ Bandwidth \_\_\_\_\_ Power \_\_\_\_\_

Name & position \_\_\_\_\_

Company \_\_\_\_\_

Address \_\_\_\_\_

Tel. exchange or code \_\_\_\_\_

Number \_\_\_\_\_ Extension \_\_\_\_\_

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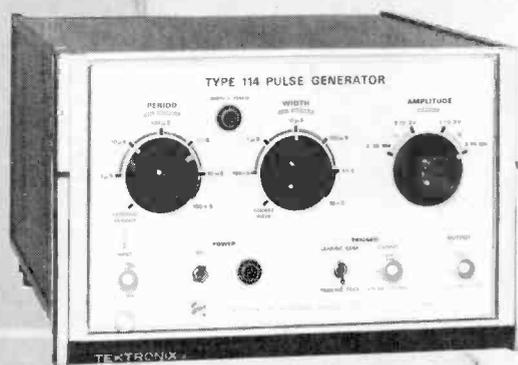


WW-010 FOR FURTHER DETAILS

# Tektronix Pulse Generators

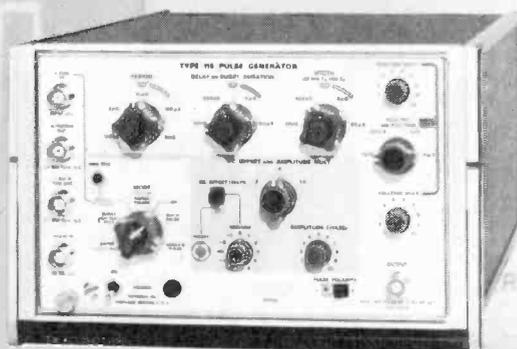
**The Type 114** is a general-purpose pulse and squarewave generator designed for laboratory and production test facilities. The broad operating range of the Type 114 makes it well suited for applications such as studying network response to changes in pulse period and/or width, or determining the step response of systems.

Price: £164 plus £19 duty



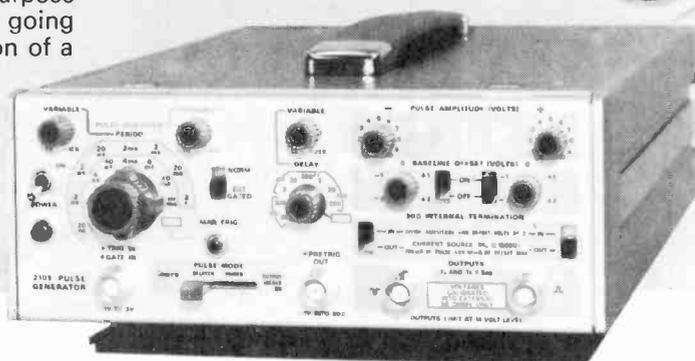
**The Type 115** is a 10-MHz, 10-volt, general-purpose pulse generator with separately variable risetime, falltime, width, delay, period, amplitude and baseline offset. It is intended for use in applications where a variety of pulse amplitudes, polarities, shapes and other characteristics are required.

Price: £412 plus £47 duty



**The Type 2101** is a compact, 25-MHz, 10-volt, general purpose generator with SIMULTANEOUS positive and negative going pulse outputs. Switch positions are provided for selection of a specific pulse period, duration and delay, within the calibrated range of the respective control. Weighs only 8½ lb.

Price £334 plus £38 duty



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committed to progress in waveform measurement

Please fill in Reader Reply Card or write, telephone or telex:

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## Experience:

Since the beginning of industrial r.f. heating, EEV have been the pace-setters. With this experience, backed by our equal know-how in the transmitter valve field, is it any wonder that we are so well known for power triodes?

EEV make power triodes for industrial heating applications from 1kW up to 250kW. They are all conservatively rated and realistically designed to give good length of life. Whatever your application—for drying paper, baking biscuits, welding plastic,

treating metal—r.f. heating the EEV way is economical and dependable.

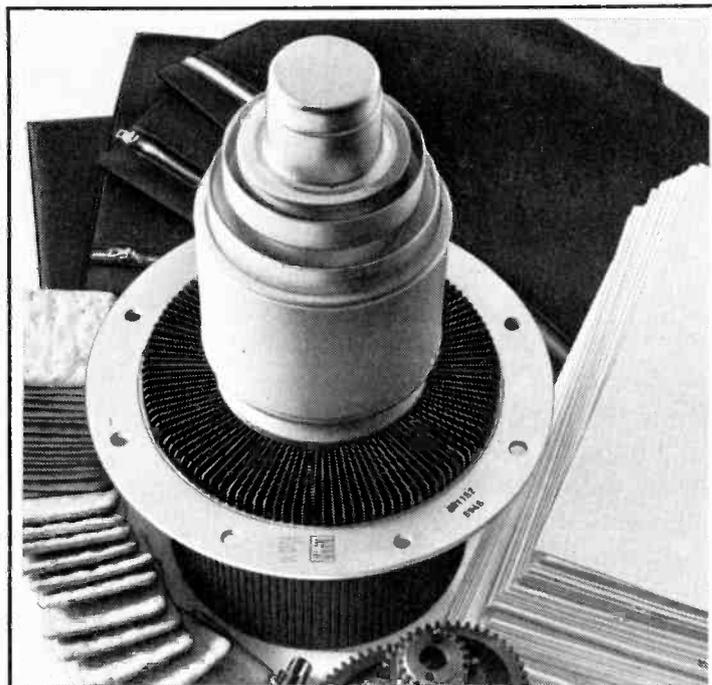
Our sales engineers are at your service to discuss designs and to recommend the best tube or combination of tubes for your particular application.

For full details just post the coupon or telephone Mr. M. J. Pitt.

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## the vital factor of EEV's industrial r.f. heating power triode range



To: English Electric Valve Co Ltd, Chelmsford, Essex, England.

Please send full data on power triodes for industrial heating.  
Please recommend triodes for an equipment with these ratings.

Output power (kW) \_\_\_\_\_ Anode voltage max. (kV) \_\_\_\_\_ Frequency (MHz) \_\_\_\_\_

Name & Position \_\_\_\_\_

Company \_\_\_\_\_

Address \_\_\_\_\_  
\_\_\_\_\_

Telephone exchange or STD code \_\_\_\_\_

Number \_\_\_\_\_

Extension \_\_\_\_\_



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## "ASTRONIC" LTD.

FIRST IN THE FIELD WITH A COMPLETE  
RANGE OF MODULAR AMPLIFIERS

THE RESULT OF THIRTY YEARS  
EXPERIENCE IN SOUND  
AMPLIFICATION,

NOW ANNOUNCE THEIR  
**RESPONSE SELECTOR TYPE A 1888**



**A MUST IN ACOUSTICALLY  
DIFFICULT SITUATIONS SUCH AS  
CHURCHES, HALLS, THEATRES etc.**

This unit, the result of three years research, can be built into a new, or added into an existing sound system and provides a simple but effective means of adjusting the overall response to suit the particular location.

Eight calibrated thumb wheel controls enable each section of the audio band to be adjusted to reduce troublesome building resonances etc., thereby allowing microphone levels to be increased before "howl back" occurs.

The unit is available in two forms: Type A 1888 is a portable instrument and Type A 1781 is a module to be used in conjunction with our Series 1700 units.

Further information from :

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# ADCOLA Soldering Instruments add to your efficiency

## ADCOLA 64

for Factory Bench  
Line Assembly

A precision instrument—supplied with standard 3/16" (4.75 mm) diameter, detachable copper chisel-face bit\*.

Standard temp. 360°C at 23 watts.

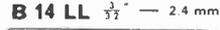
Special temps. from 250°C—410°C.

\*Additional Stock Bits  
(illustrated) available

### COPPER

-  **B 38**  $\frac{1}{8}$ " — 3.2 mm CHISEL FACE
-  **B 14**  $\frac{3}{32}$ " — 2.4 mm CHISEL FACE
-  **B 24**  $\frac{3}{16}$ " — 4.75 mm SCREWDRIIVER FACE
-  **B 12**  $\frac{3}{16}$ " — 4.75 mm EYELET BIT
-  **B 58**  $\frac{1}{4}$ " — 6.34 mm CHISEL FACE

### LONG LIFE

-  **B 42 LL**  $\frac{3}{16}$ " — 4.75 mm CHISEL FACE
-  **B 38 LL**  $\frac{1}{8}$ " — 3.2 mm CHISEL FACE
-  **B 14 LL**  $\frac{3}{32}$ " — 2.4 mm CHISEL FACE
-  **B 44 LL**  $\frac{3}{16}$ " — 4.75 mm SCREWDRIIVER FACE



Don't take chances. We don't. All our ADCOLA Soldering Instruments are of impeccable quality. You can depend on ADCOLA day after day. That's why they're so popular. You get consistent good service... reliability... from our famous thermally controlled ADCOLA Element and the tough steel construction of this ideal production tool.

# ADCOLA

(Regd Trade Mark)

\* Write for  
price list  
and  
catalogue

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Telephone: 01-622 0291/3 · Telegrams: Soljoint London Telex · Telex: Adcola London 21851

WW-014 FOR FURTHER DETAILS

# Why do so many industries rely on EEV tubes?

## Because they're so reliable.



You can specify each and every EEV tube with confidence. Whatever your industry, when it involves electronics you can be sure that EEV's expertise will provide the performance, the length of life and, above all, the reliability you want.

**For industrial heating:** EEV r.f. power triodes range from 1kW up to 250kW, and mercury vapour rectifiers are available with capabilities up to 30 amps at 21kV. All are conservatively rated, realistically designed and economical.

**For TV monitoring:** EEV vidicons are ideal for any closed-circuit TV application. They can be used in any position and are available with a choice of photosurfaces,

**For power supplies:** EEV make voltage stabilisers and voltage reference tubes to fit more than 80 different sockets.

**For high-speed switching:** EEV glass and ceramic hydrogen thyratrons provide greater accuracy and precision.

**For motor control:** EEV industrial thyratrons provide the degree of precision needed for motor speed control and similar applications. Both mercury vapour and xenon thyratrons are available,

**For industrial welding:** EEV ignitrons have long-life ignitors, and robustly constructed envelopes and water jackets of unique design giving supreme reliability.

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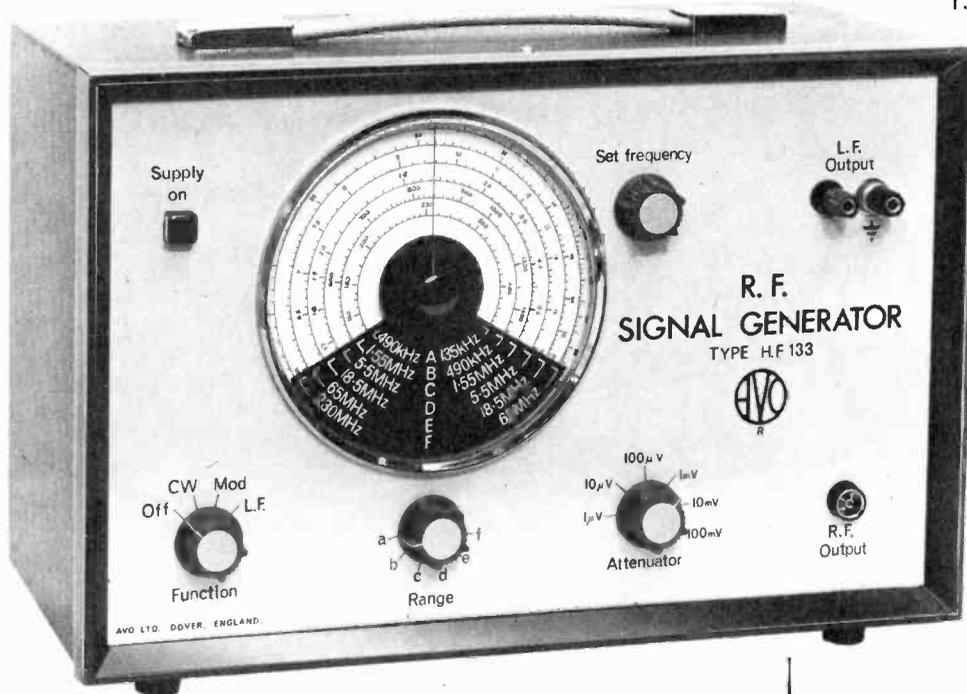
### ENGLISH ELECTRIC VALVE CO LTD

# stop searching for a signal

Find it easily with Avo's inexpensive, easy-to-operate HF133 Signal Generator, which covers the complete r.f. spectrum from the long-wave broadcasting to the VHF television band.

The six separate ranges were carefully chosen to make range switching unnecessary when operating in most transmission bands. Get full details of this versatile tool for the service engineer from

Avo Ltd, Avocet House, Dover, Kent; telephone 2626, telex 96283.



WW—016 FOR FURTHER DETAILS

Frequency range: 135kHz-230MHz \* R.F. Calibration Accuracy:  $\pm 1\%$  \* Amplitude Modulation: 17% at 1kHz (35% highest range) \* R.F. Output:  $1\mu\text{V}$ -100mV (continuously variable) into  $75\Omega$  — wider variation on highest range.

## TRANSIPACK<sup>®</sup> INDUSTRIAL RANGE

( $\frac{1}{2}$ —100 Kilowatts)

REGULATED AC-DC  
POWER UNITS

DC-AC STATIC  
INVERTERS

AC-AC FREQUENCY  
CHANGERS

STATIC EMERGENCY  
POWER SYSTEMS

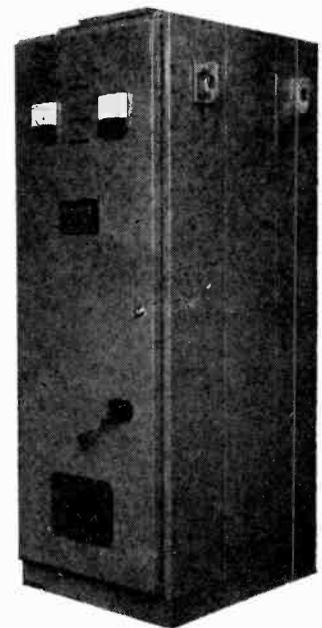


INDUSTRIAL  
INSTRUMENTS  
LIMITED

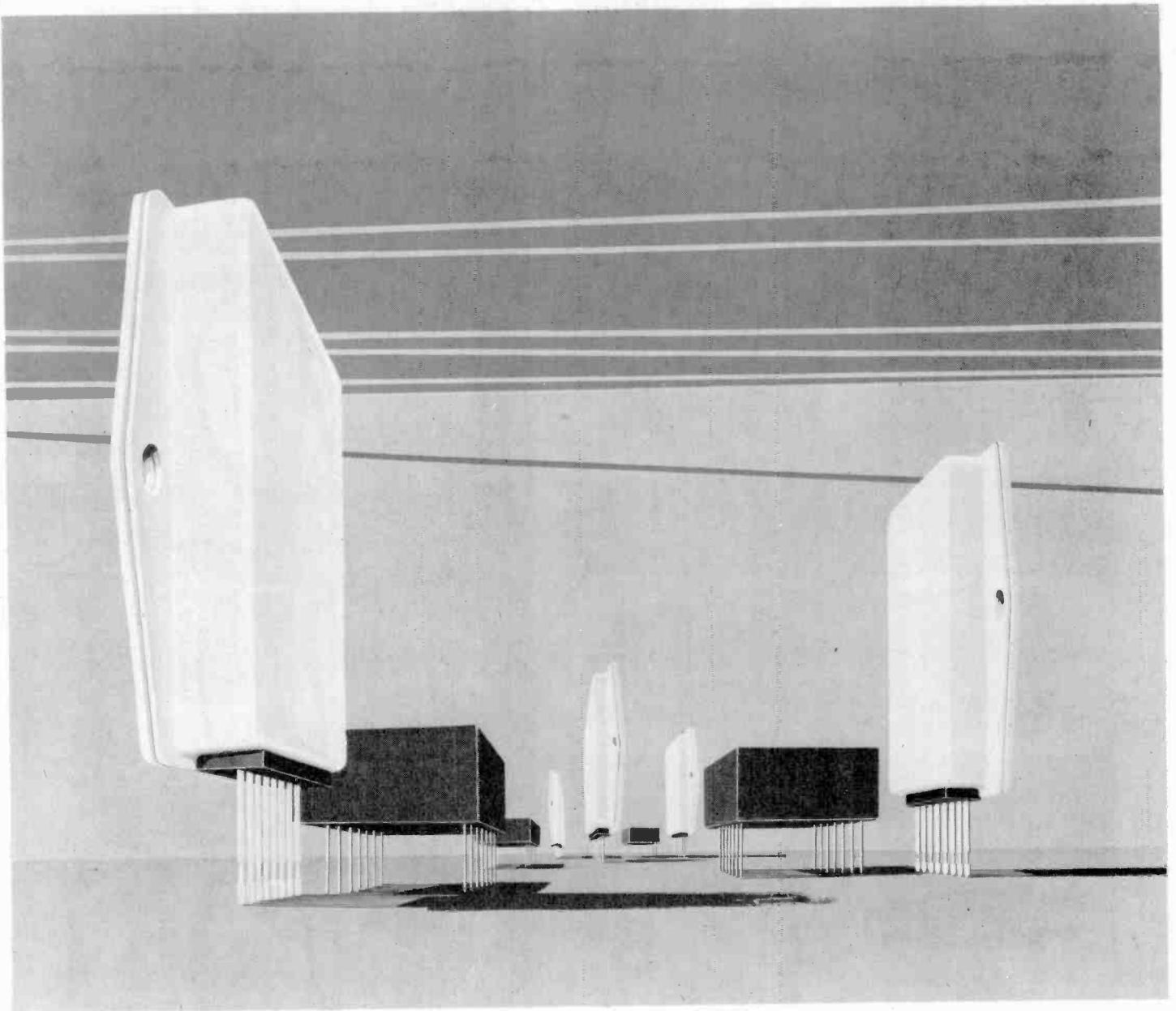
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## ERIE

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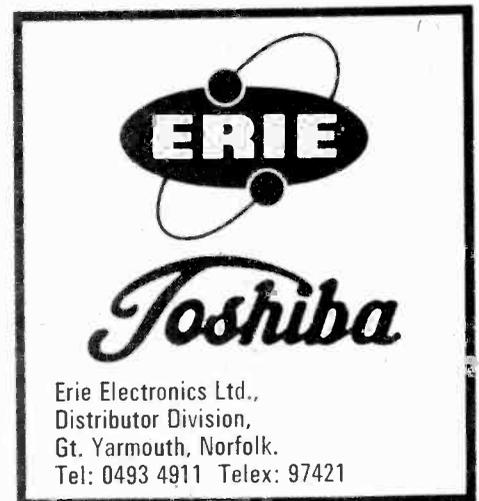
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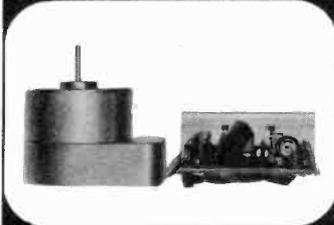


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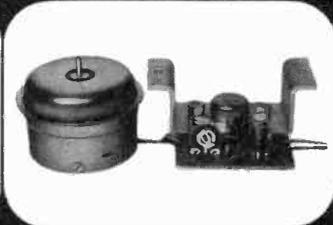
T1/71

*Micro Motors*  
*Level Meters*  
*Magnetic Heads*

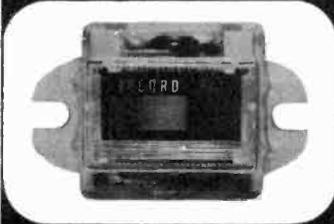
**Sankyo's  
GLEESOME THREESOME  
SALE TO MAKERS  
OF TAPE RECORDERS,  
OTHER PRODUCTS.**



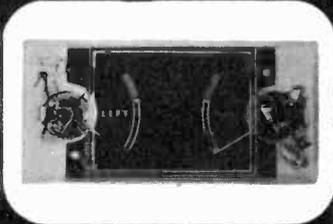
• **Micro Motor ZF-900**  
A transistorized motor for portable dictating machines and tape recorders.



• **Micro Motor BF207R**  
A transistorized governor motor for cassette tape recorders and record players.



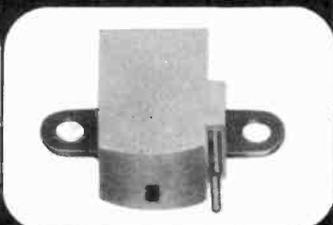
• **Level Meter Model-08**  
For cassette tape recorders and record players.



• **Level Meter Model-15**  
Dual level meter for stereo tape recorders and record players.



• **Magnetic Head 07-03**  
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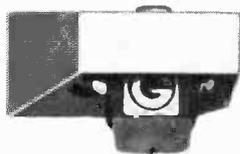
## GOLDRING SERIES 800 and 850 STEREO MAGNETIC CARTRIDGES

Our famous '800 Series' True Transduction cartridges, developed on the 'Free Field' principle, allow the most delicate groove-stored signals to be accurately relayed and re-created with uncompromising precision. And the

G.850 Free Field stereo magnetic cartridge, intended primarily for 'budget' hi-fi systems, offers all the advantages of a good quality magnetic cartridge at a very attractive price.



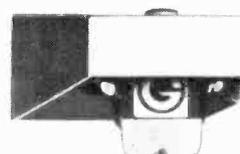
**800 Super E** For those aiming at perfection—extra low mechanical impedance for ultimate tracking is achieved by a duo-pivoting arrangement membrane-controlled to avoid longitudinal or torsional modes blemishing performance. Each cartridge supplied with individual curve and calibration certificate.



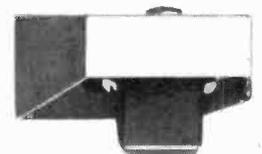
**800/E** Designed for transcription arms, a micro-elliptical diamond is fitted to a fine cantilever, end-damped against natural tube resonances, accurately terminated in a special conical hinge to give pin-point pivoting.



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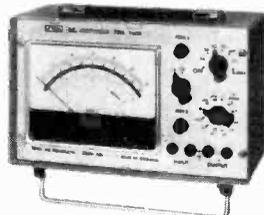
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**VOLTAGE & dB RANGES:** 15µV, 50µV, 150µV... 500V f.s.d. Acc. ± 1% ± 1% f.s.d. ± 1µV at 1kHz. - 100, - 90... + 50dB scale - 20dB/+ 6dB rel. to 1mW/600Ω.  
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 TM3A TM3B



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**CURRENT RANGES:** 3pA, 10pA, 30pA... 1mA (1A for TM9BP) Acc. ± 2% ± 1% f.s.d. ± 0.3pA. LZ & CZ scales.  
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 TM9A TM9B TM9BP  
**BROADBAND VOLTMETERS**  
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**L.F. RANGES:** As TM3 except for the omission of 15µV and 150µV.  
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# The Gerry



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Once upon a time Gerry Adler worked a 25 hour day making and selling valve filament testers. And very efficient they were too.

But at that time the Japanese could make them for about half the price, and sent Gerry one to prove it. It was as good as the ones he was making, so he sold it. And every other one he could get into the country.

After a time Gerry decided to go one step further. He designed some electronic equipment and had it built to his specification in Japan. Then he sold it here under the brand name 'Eagle'. Nothing particularly remarkable about that. But Gerry couldn't stand the idea of a barrier between him and his manufacturers. So he went to Japan. He poked his nose into all the electronics factories to find out how the Japanese worked. And when he got back he started to learn Japanese, and to study their history, culture and way of life. That way he had fewer communication problems and could get what he wanted.

That's what matters to Gerry. He's very fussy about what goes out under the Eagle banner. Because Eagle aren't in the filament testing business any more. They make just about everything electronic: amplifiers, test equipment, PA systems, intercoms, old uncle substation and all. Eagle is now twelve years old, and has opened offices in New York, Tokyo and Brussels.

This isn't just so much chest expansion on Gerry's part. He puts his money where his mouth is. If you think one of his products is not as good as a rival's, or it's faulty, or it's not all it should be, Gerry wants to know.

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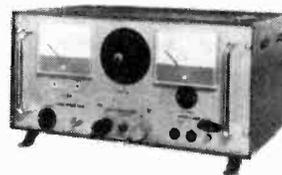


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WW-028 FOR FURTHER DETAILS

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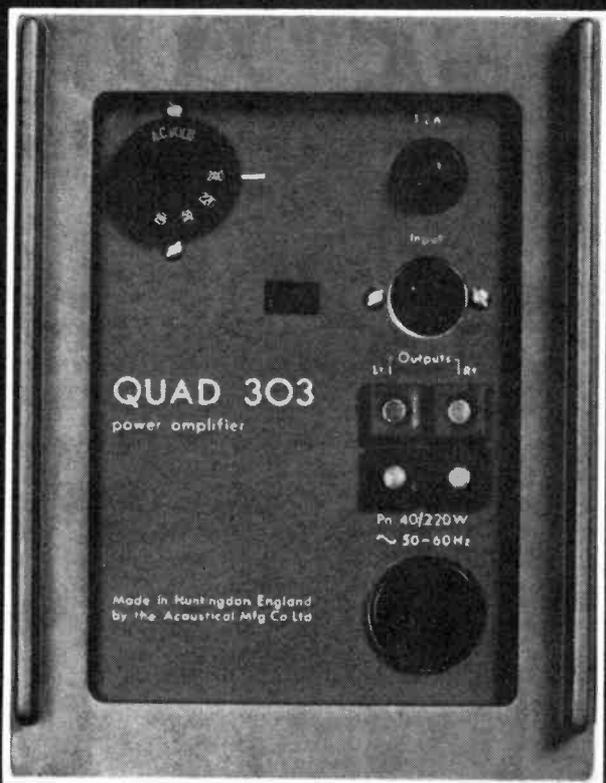
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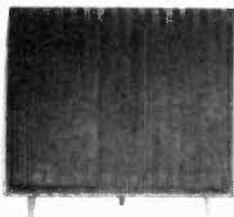
wireless



It has been suggested that a perfect amplifier would be equivalent to a piece of wire with gain.

A piece of wire? First of all it would hum, so we'd have to screen it. This would increase the input capacity so we'd have to make the screening large or the conductor small. Then we would have output resistance and, if of appreciable length, we'd have inductance and termination problems as well. All in all a 303 power amplifier would be much easier.

The funny thing is; even if we had our perfect piece of wire with gain and compared it with a 303, the two would sound *exactly* the same no matter how carefully we listened.



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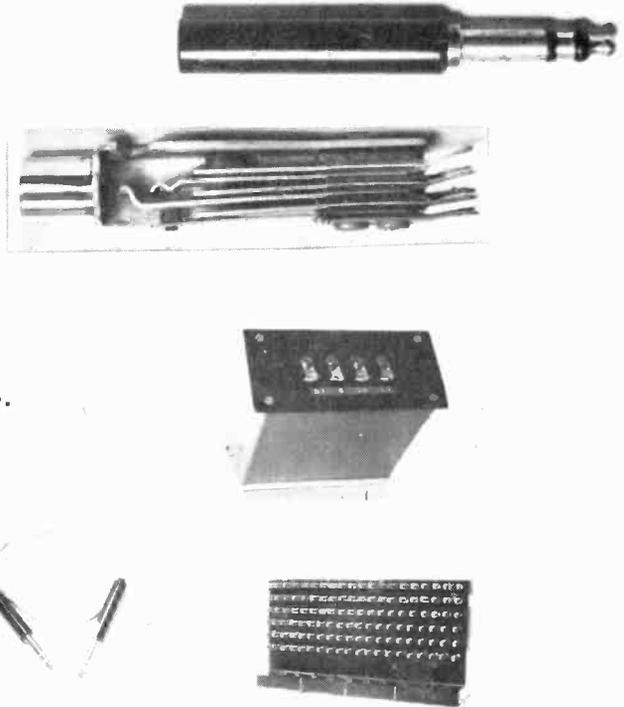
Polymite capacitors scorn conventional housings. You buy them stripped for action. Because Polymites use a thin polyester metallised film, they offer high capacitance values, small physical size, much less weight; plus the high mechanical strength of Erie's special way of applying terminal connections. All *without* a 'can'. And all with the properties of recovery from humidity that Erie Polymites alone can offer.

Scan the specification :	<i>Type M310</i>	<i>Type M312</i>
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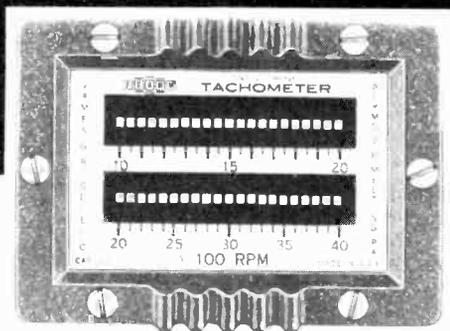
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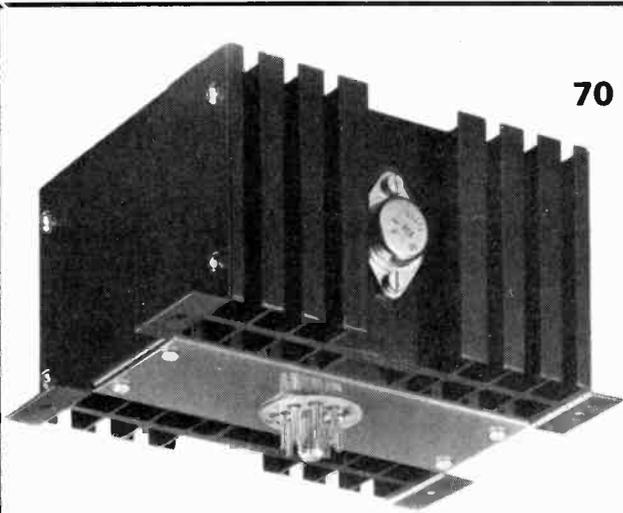
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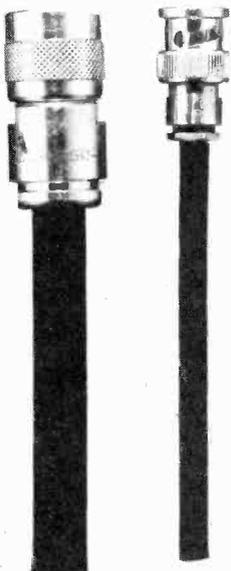
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"BNC"

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### CABLE-CONNECTOR ASSEMBLY



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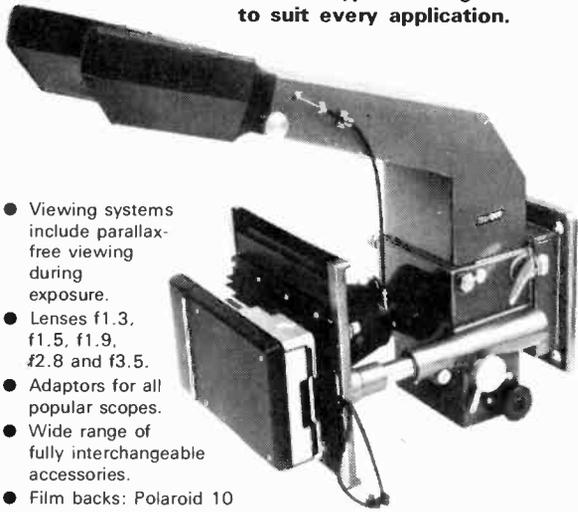
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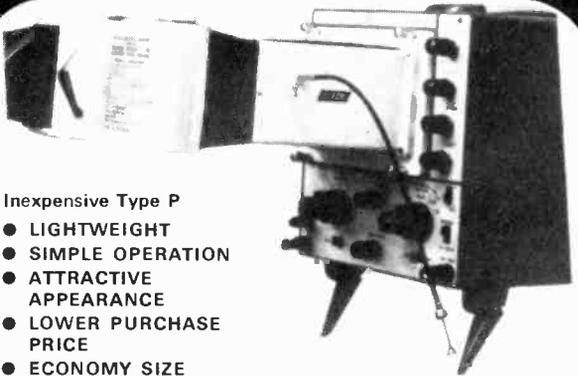
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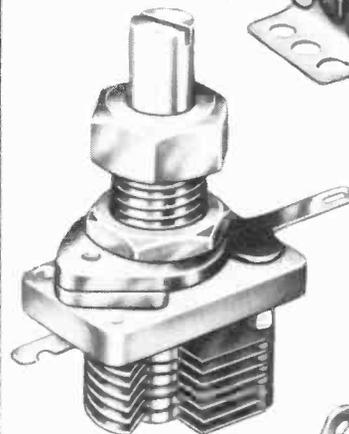
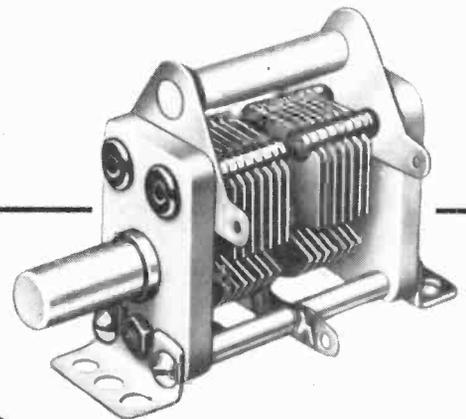
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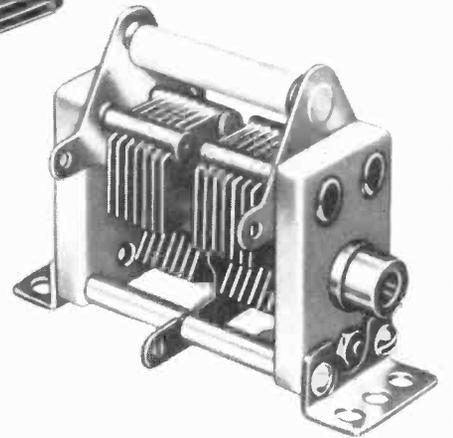
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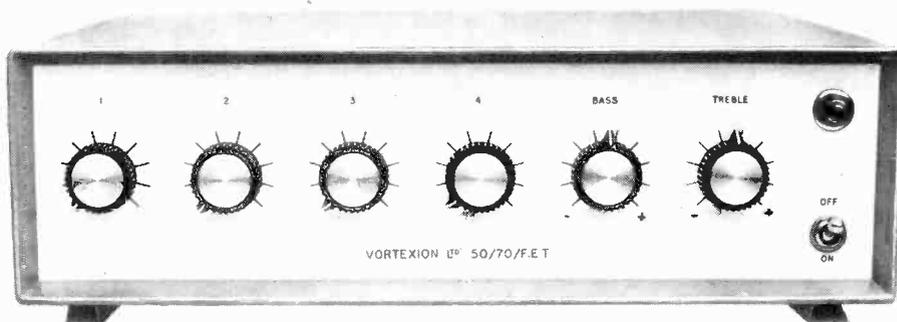
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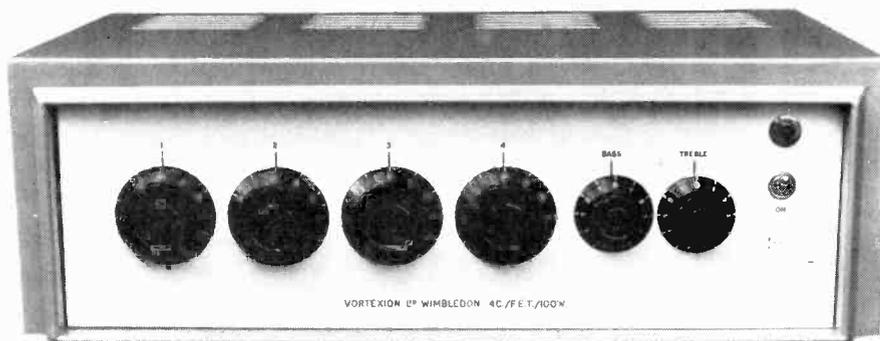
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This is a high fidelity amplifier (0.3% intermodulation distortion) using the circuit of our 100% reliable—100 Watt Amplifier (no failures to date) with its elaborate protection against short and overload, etc. To this is allied our latest development of F.E.T. Mixer amplifier, again fully protected against overload and completely free from radio breakthrough. The mixer is arranged for 2-30/60 $\Omega$  balanced line microphones, 1-HiZ gram input and 1-auxiliary input followed by bass and treble controls. 100 volt balanced line output or 5/15 $\Omega$  and 100 volt line.

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**100 WATT ALL SILICON AMPLIFIER.** A high quality amplifier with 8 ohms—15 ohms or 100 volt line output for A.C. Mains. Protection is given for short and open circuit output over driving and over temperature. Input 0.4 V on 100K ohms.



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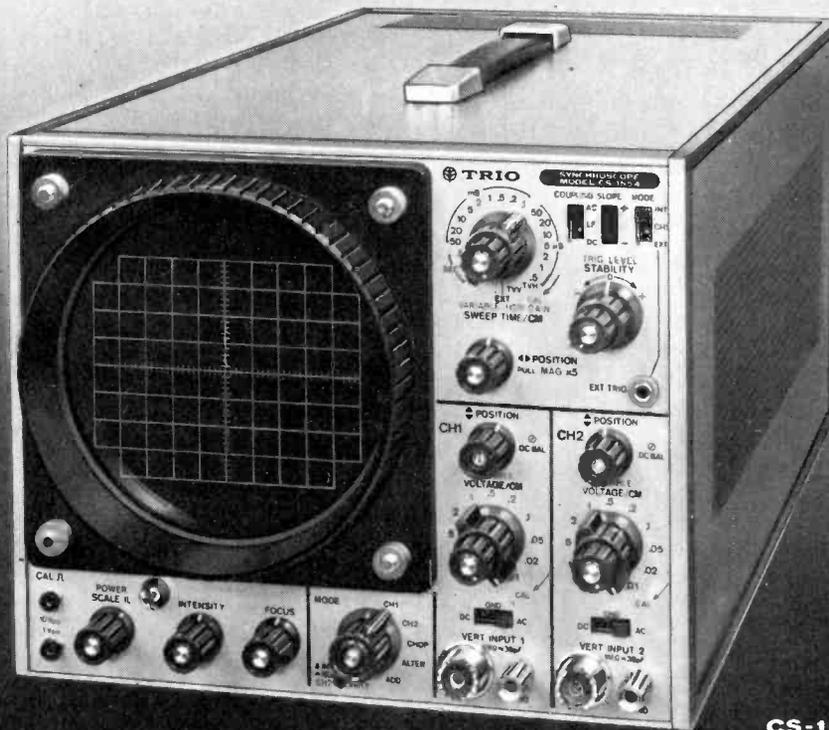
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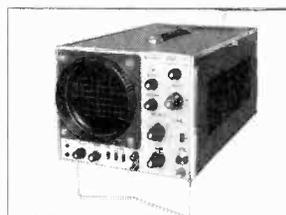
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**CS-1554**  
130mm Dual Trace Oscilloscope

## TRIO's CS-1554 Passes The Most Rigid Testing Requirements

Waveform analysis and other electrical equipment and electronic installation testing is performed at the highest possible peak of efficiency with TRIO's CS-1554. This wide-band dual trace triggering oscilloscope operates at ultra-high sensitivity while also offering an over-all expansive range of test capabilities. Lightweight because of its all-solid state construction, this completely dependable instrument is remarkably versatile. For example, dual trace waveform analysis with very wide synchronization capabilities is possible from DC-10MHz. It has no equal for speedy analysis efficiency.



**CS-1553**  
130mm Oscilloscope  
An essential device for signal waveform analyses and TV alignment and servicing. Complete solid state circuitry. Trigger sweep and automatic sweep potential. Very high sensitivity with wide frequency response from DC to 10MHz extremely versatile.



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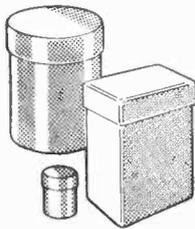
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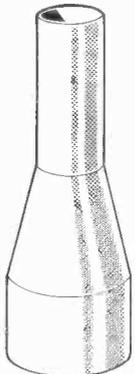
### Standard shields

Telcon Metals offer an extensive standard range of high efficiency Mumetal shields, which fit most cathode ray, photo multiplier and radar tubes, together with a selection of boxes and cans for microphones pick-ups, transistors and transformers. These are normally supplied stove enamelled in hammer grey externally and matt black internally. Other finishes can be supplied by arrangement.



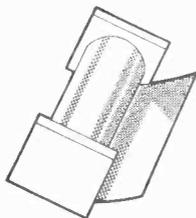
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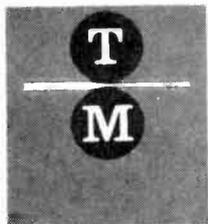


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'Telshield' is an easy to use, ferromagnetic shielding foil, which can be cut with scissors, wound into cylinders, cones, etc., and fixed with adhesive tape, clips or spot welds, to provide a permanent efficient shield. It is economical to use, especially for research, development and short-run applications which do not merit the tooling involved in the production of fully fabricated shields. 'Telshield' is supplied in a standard thickness of 0.05 mm, in widths of 150, 50 and 25 mm in convenient packs costing approximately £5. Other thicknesses and widths are available by arrangement.



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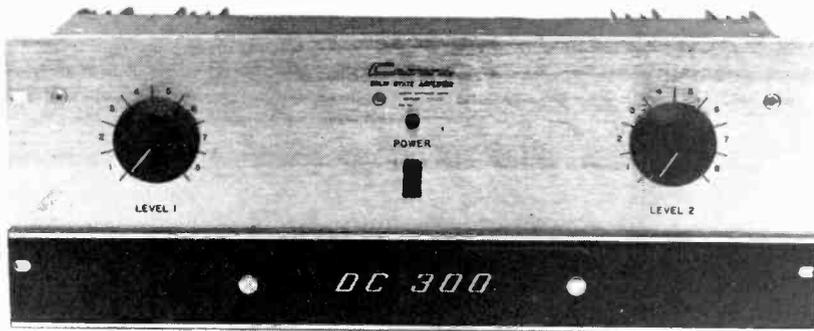
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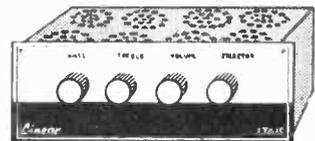
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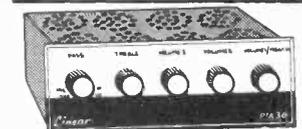
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 Output 30 watts.  
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 Three individually controlled inputs for mixing purposes.  
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**AN IDEAL UNIT FOR VOCAL AND INSTRUMENTAL GROUPS SUIT. ABLE FOR ANY KIND OF 'MIKE' AND INSTRUMENT PICK-UP, ALSO FOR RADIO, TAPE, OR GRAM.**



Recommended Retail price **£24**  
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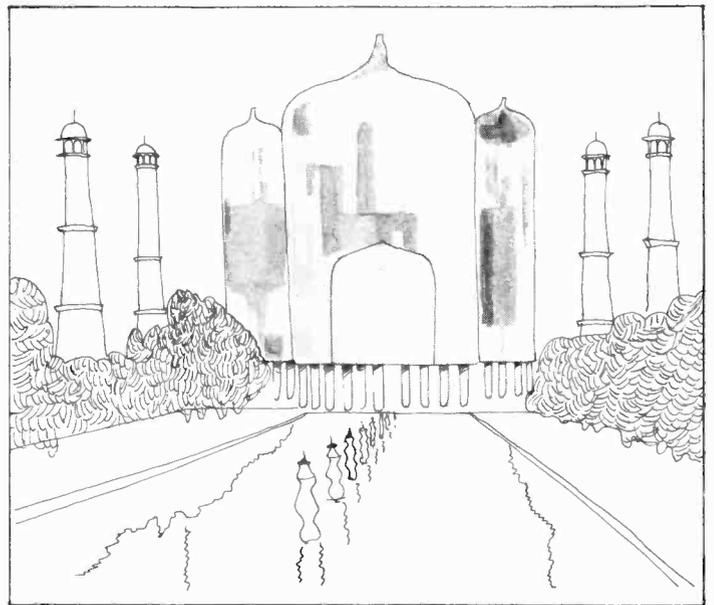
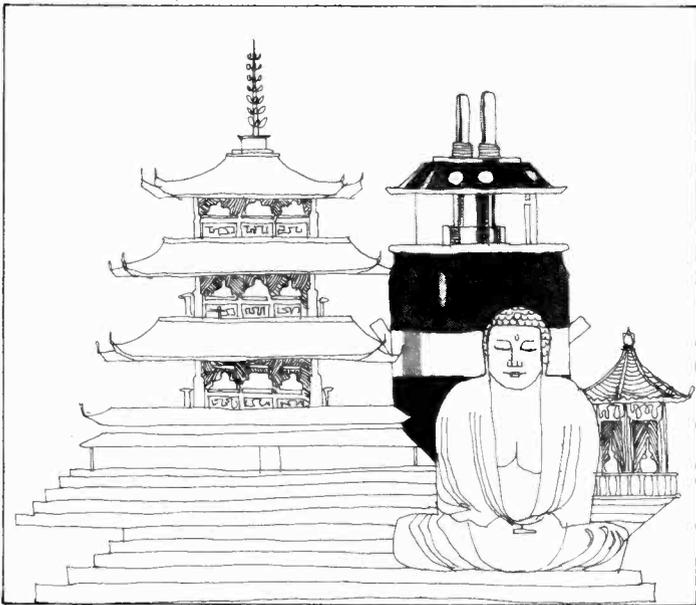
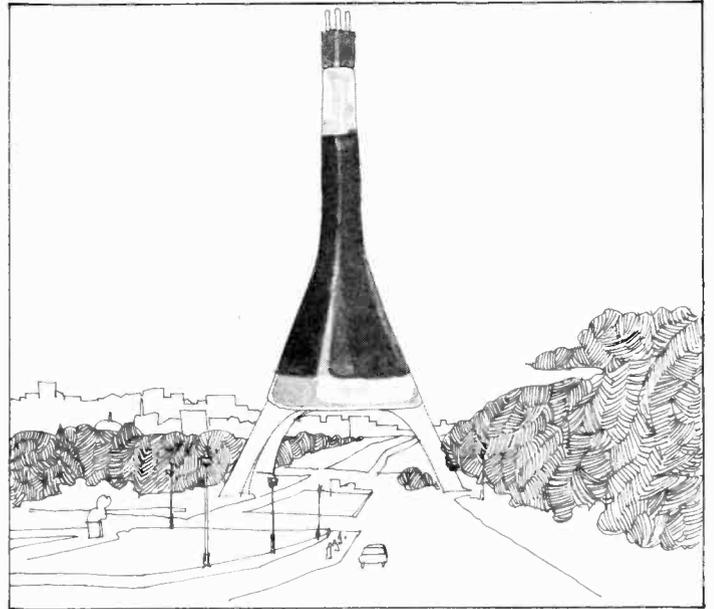
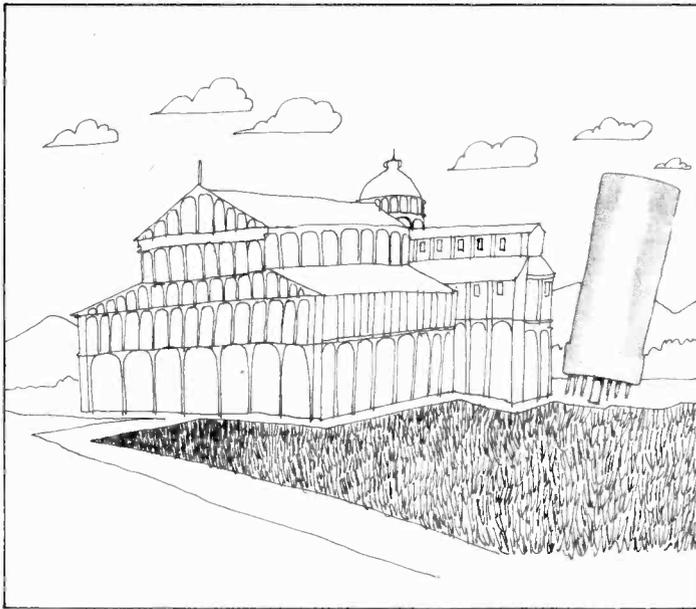
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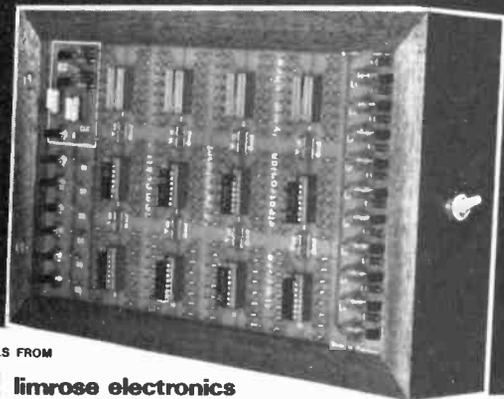
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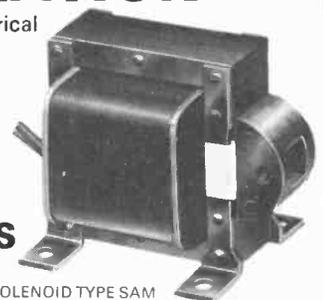
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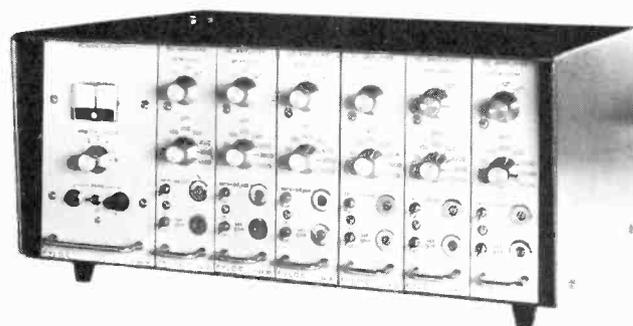
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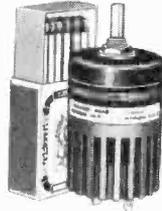
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## DMM2 DIGITAL MULTIMETER

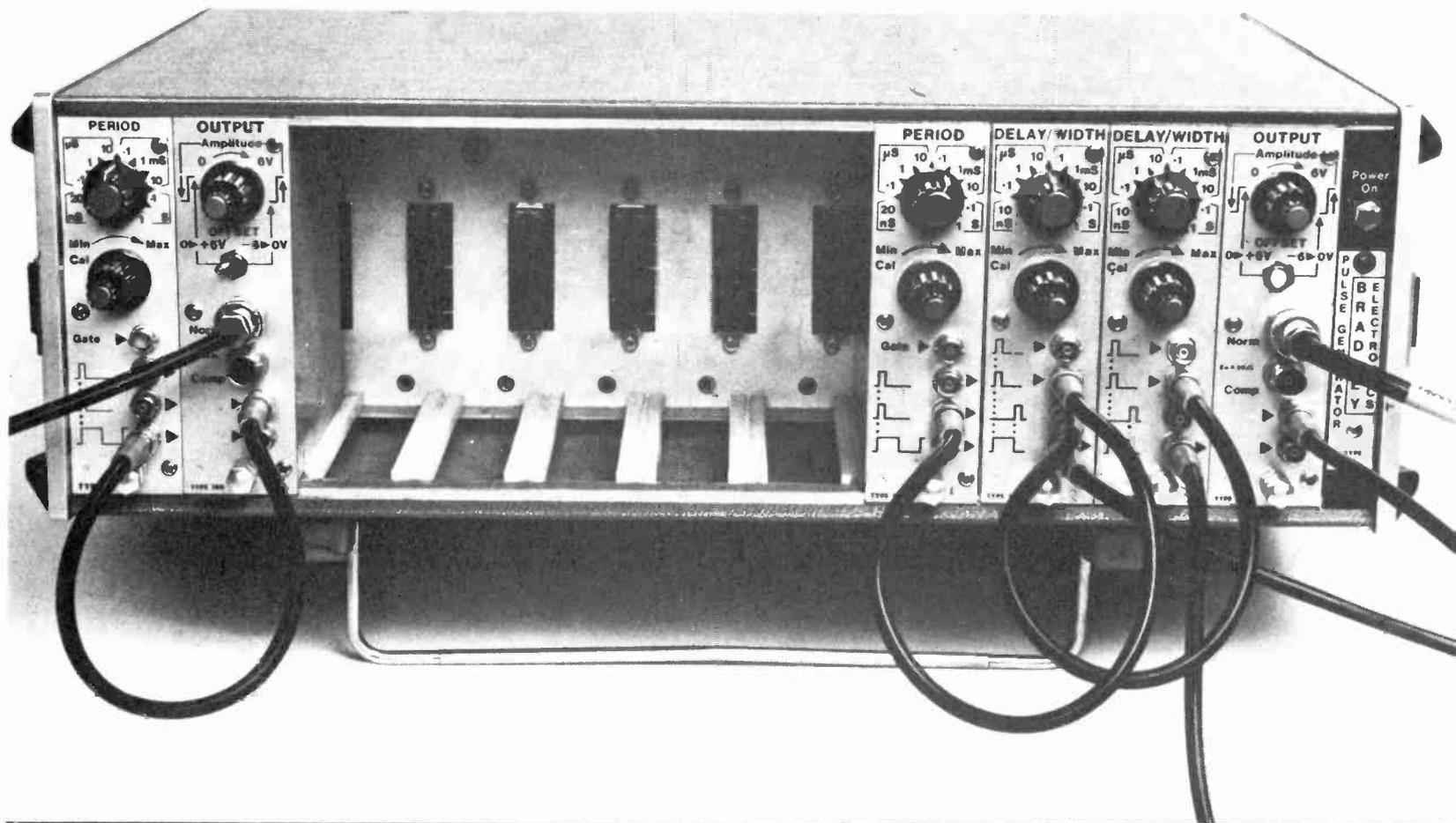
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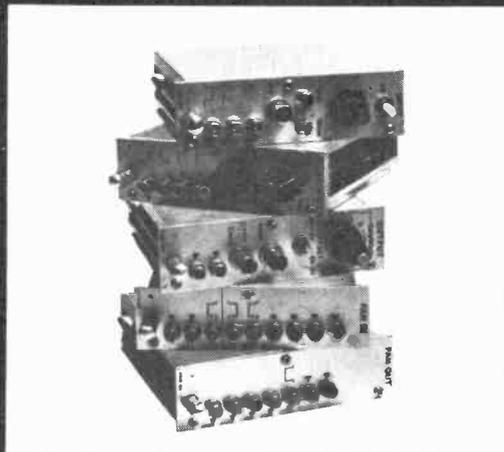
# From Bradley. A Modular Pulse Generator

The two modules on the left form a complete square wave generator giving outputs up to 6V into 50ohms, over the range 1 Hz to 50 MHz

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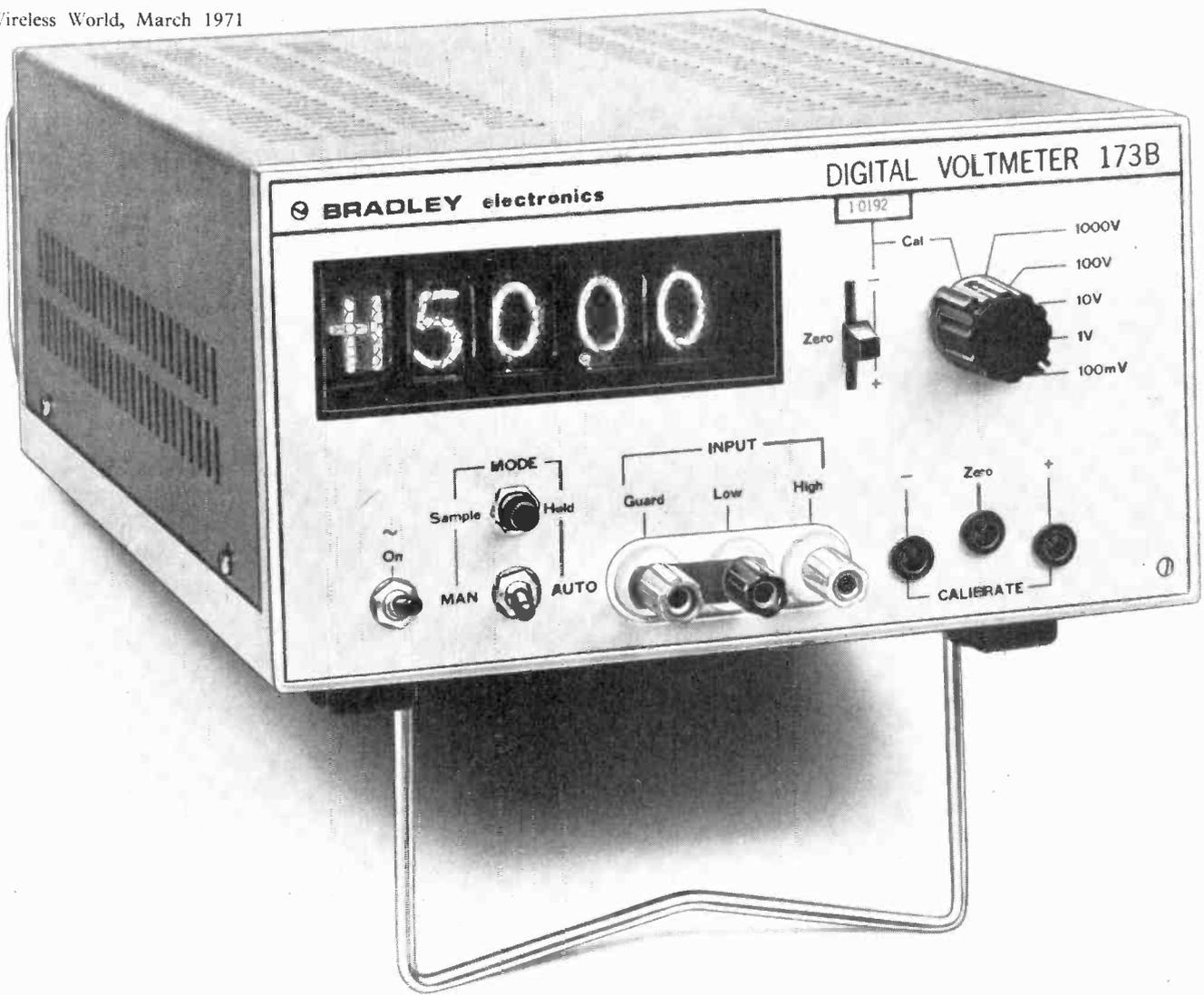
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Bradley's compact 173B Digital Voltmeter will cost you only £360 in the U.K.

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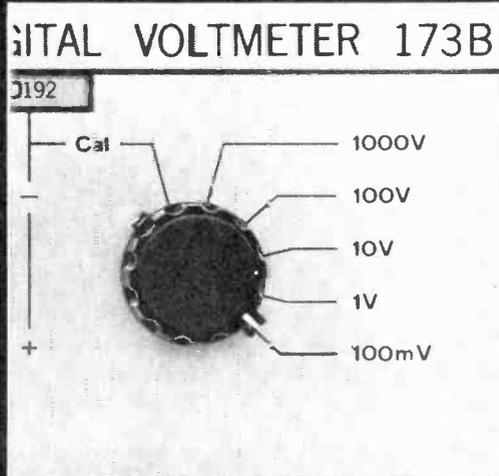
There's guarded input giving high common mode rejection > 140 dB at line frequency.

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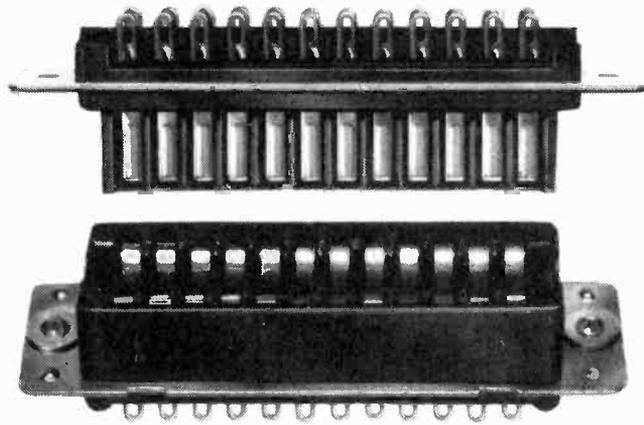


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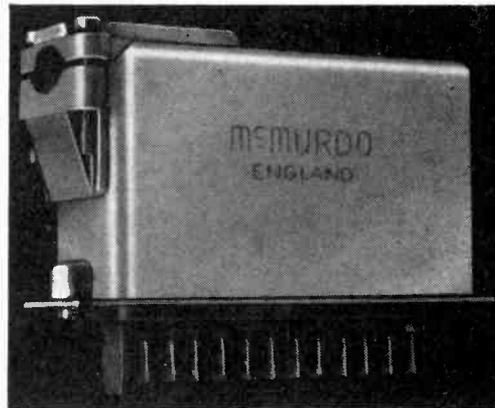
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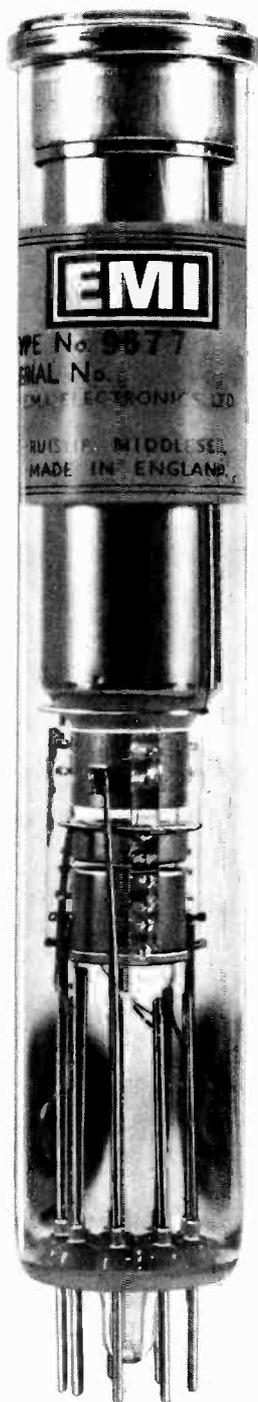
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**Versatility** Designed for use in a wide range of colour and monochrome broadcast and closed-circuit cameras, both live and film pick-up.

**2**

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**3**

**Uniform Quality** Every EMI vidicon tube is produced to uniform standards for complete reliability.

**4**

**5**

**Economy** EMI technology, quality control and production techniques provide tubes at realistic prices.

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South Wales Wireless Installation Co. Ltd.  
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An instrument of high stability providing very pure sine waves, and square waves, in the range of 5 Hz to 500 kHz. Hybrid design using valves and semiconductors.

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A sensitive instrument for the measurement of total harmonic distortion, designed for speedy and accurate use. Capable of measuring distortion products as low as 0.002%. Direct reading from calibrated meter scale.

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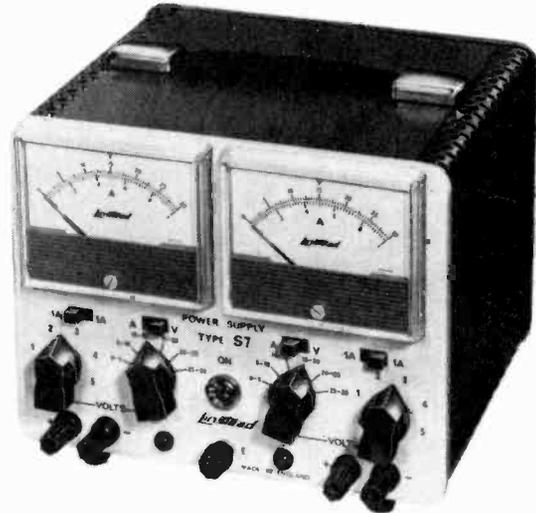
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WW-062 FOR FURTHER DETAILS

## Your choice in Linstead low cost twin stabilised power supplies



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- ★ 2 x 0 to 20 V, 0.5 A each.
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current  $\pm 2\%$  F.S.D.
- ★  $\pm 10\%$  supply voltage gives  $\pm 0.1\%$  output change.
- ★ Ripple: 300  $\mu$ V r.m.s.
- ★ Can be used in series for 40 V, 0.5 A.
- ★ Can be used in parallel for 20 V, 1 A.
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- ★ Indefinite shorting without damage.
- ★ Size: 8¼ x 6½ x 6½ in (21 x 17 x 17 cm).
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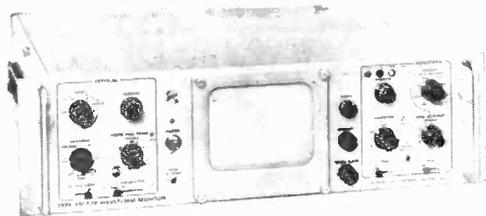
To: Linstead Electronics, Roslyn Works, Roslyn Road, London, N. 15.  
 Please send me full details of your twin stabilised power supplies.

Name .....

Address .....

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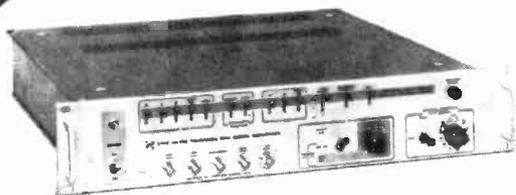
# Tektronix instruments serve worldwide television



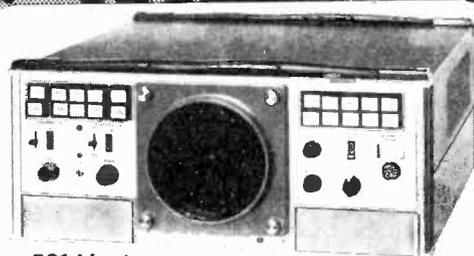
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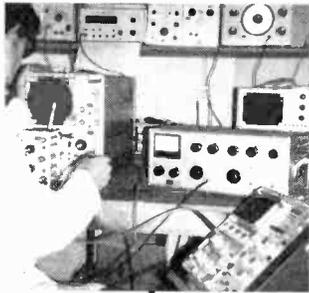
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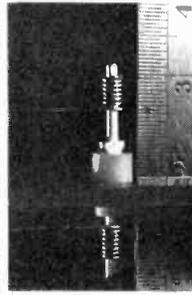
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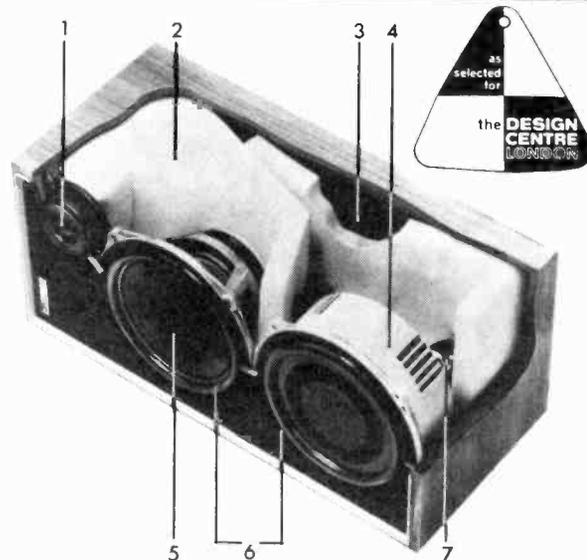
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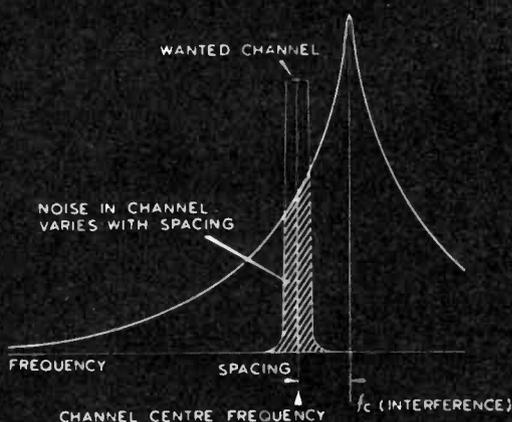
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New Low Noise UHF FM Signal Generator permits >70dB adjacent channel rejection measurements



The TF 2012 is the first of 'the quiet ones' - a series of signal generators designed to embody all the features needed for the accurate evaluation of narrow band mobile FM receivers. It is a signal generator with sufficiently low sideband noise to permit - with ease - the exacting two and three signal generator tests required by the licensing authorities on advanced mobile equipment. It has extremely low microphony and its frequency

stability specification is entirely consistent with this type of measurement. TF 2012 covers the frequency range 400 to 520 MHz and a swept frequency output of 200 kHz excursion is available by application of an external low speed voltage. Measurements and test capability includes: sensitivity; modulation acceptance bandwidth; adjacent channel selectivity; AF power output; AF response characteristic; hum and noise;

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**mi Marconi Instruments Ltd**

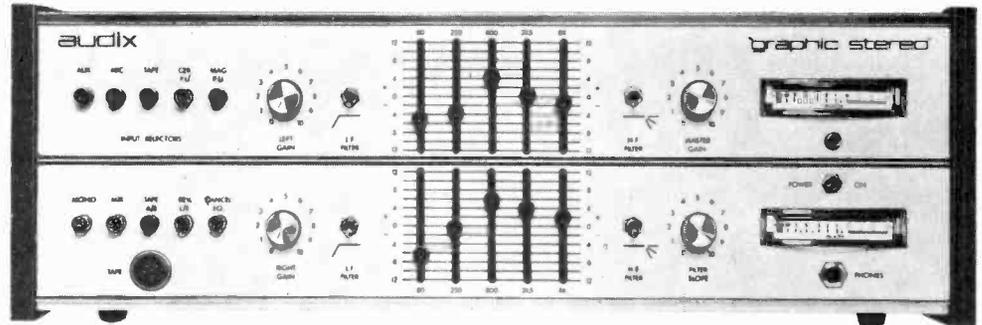
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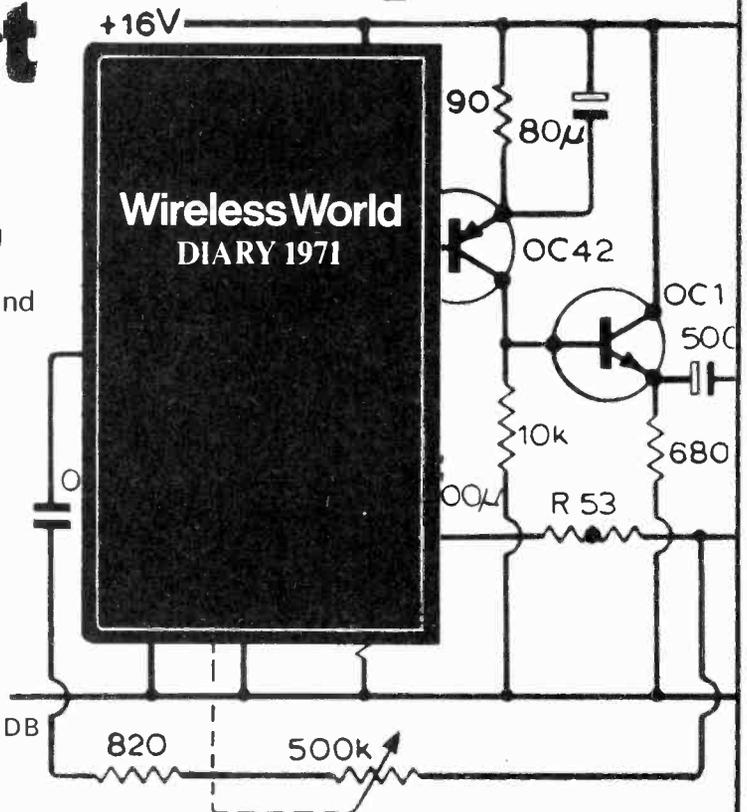
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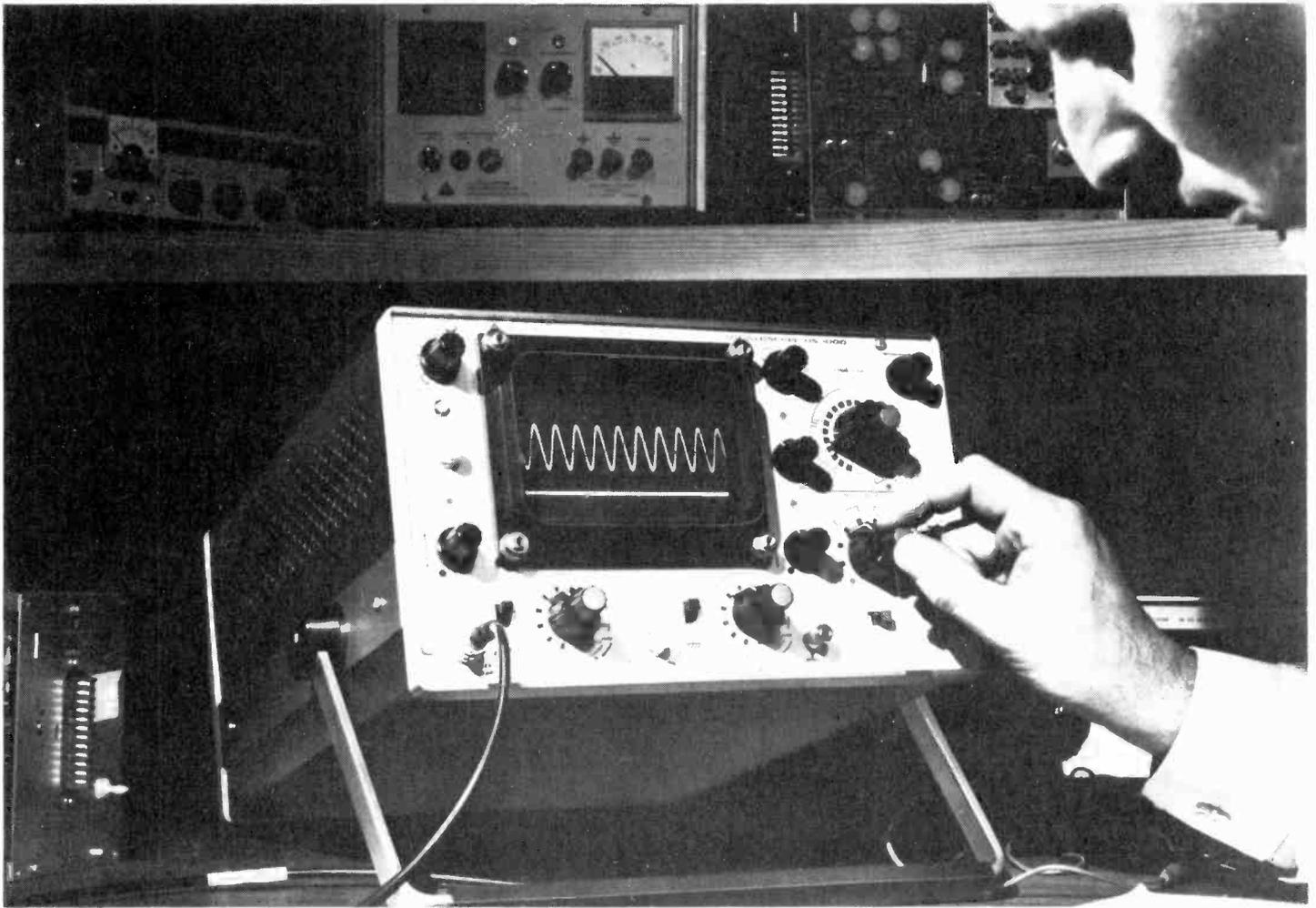
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 5mV/cm dual trace display.  
 Signal Delay.  
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 with T.V. sync separator.  
 Switched X-Y operation.  
 Bright line auto free-run.  
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*Advance OS1000 — £185*

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## OS1000 OSCILLOSCOPE

from the **ADVANCE** range



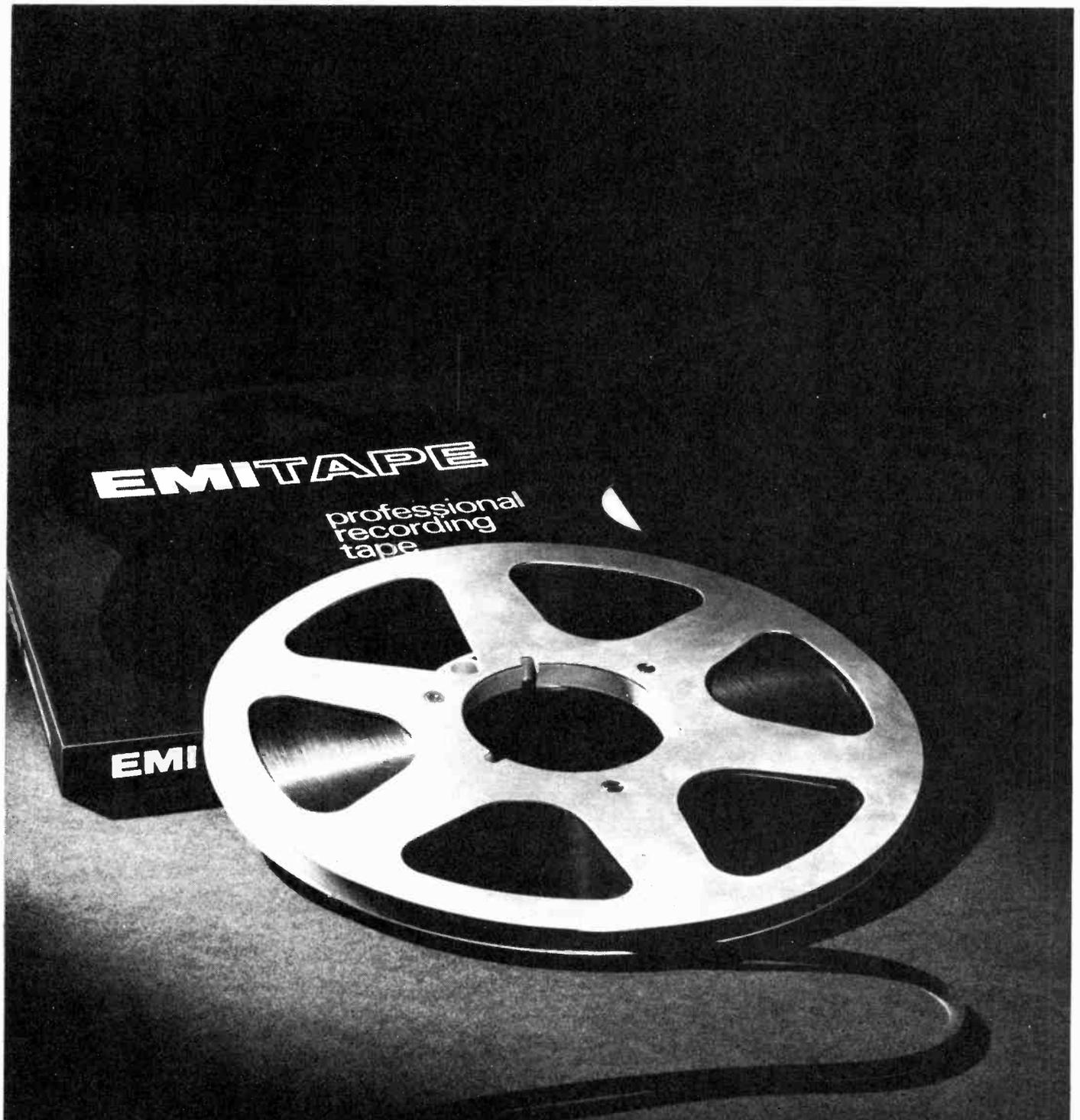
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## Just add sound

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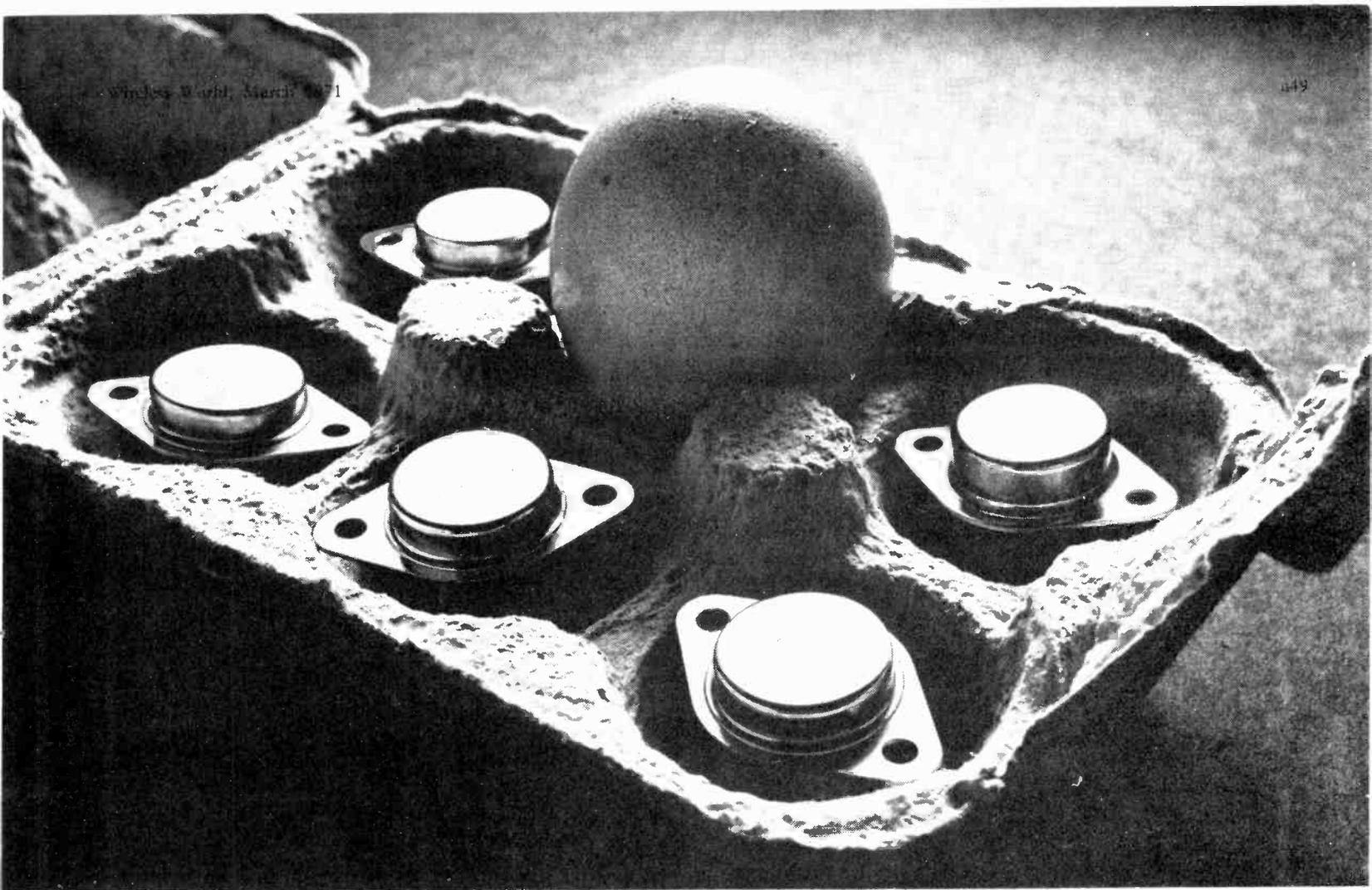
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### EMITAPE 815

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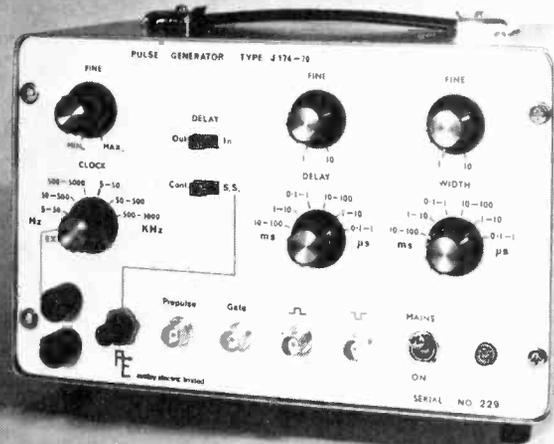
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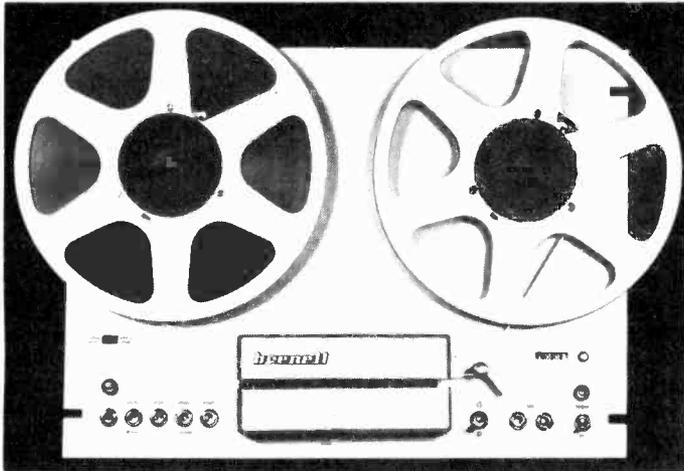
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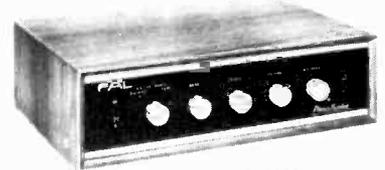
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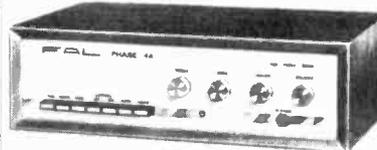
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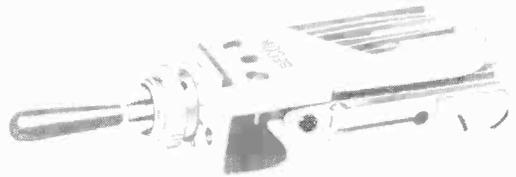
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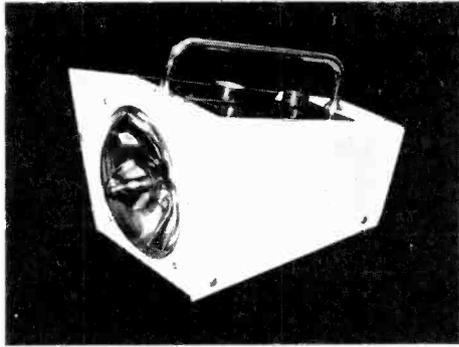
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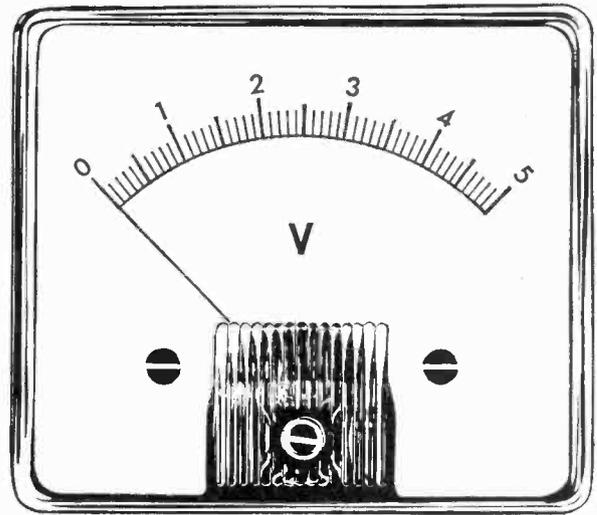
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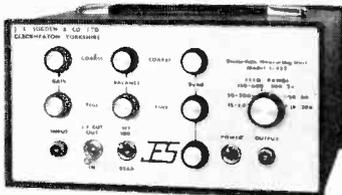
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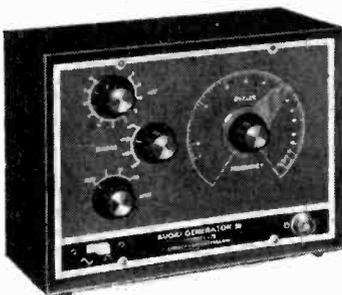
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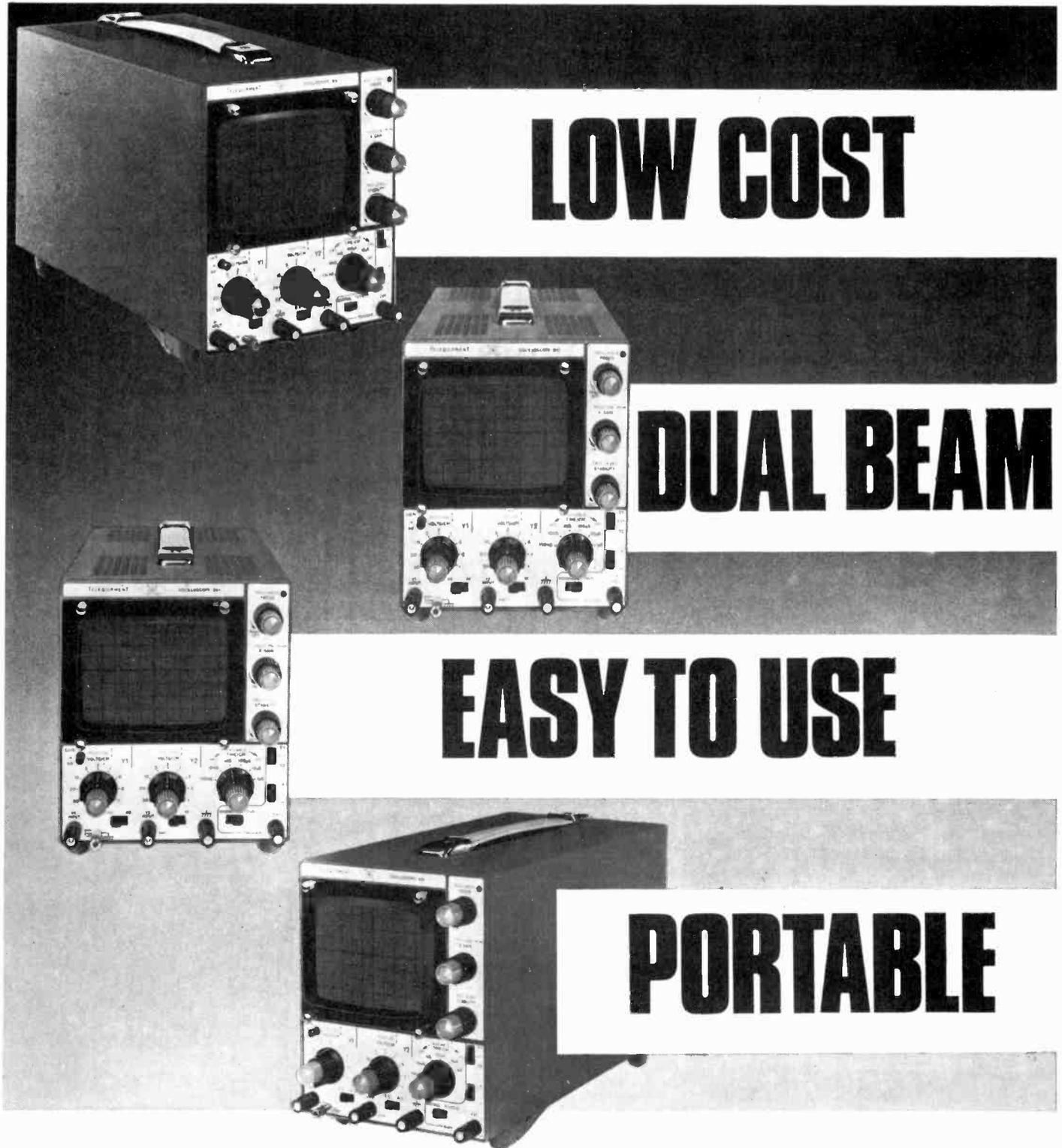
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# Wireless World

Electronics, Television, Radio, Audio

Sixtieth year of publication

March 1971

Volume 76 Number 1425



**This month's cover.** A simulated emergency at Standsted airport to demonstrate the use of rescue vehicles equipped with AVOID radar described in this issue.

## IN OUR NEXT ISSUE

The first of two articles describing a sensitive f.m. tuner using dual-gate m.o.s.f.e.t.s, ceramic i.f. filters and integrated circuits.

Low-cost logic teaching aid enabling the Karnaugh map of combinational logic circuits to be displayed on an oscilloscope.

Further details of special articles in this our 60th birthday issue are given on p.113.

## Contents

- 103 **Concepts and Reality in Electronics**
- 104 **Wein Bridge Audio Oscillator** by A. J. Ewins
- 107 **Demonstrating Multivibrator Action** by T. Palmer
- 108 **News of the Month**
- 110 **AVOID—Short-range High-definition Radar** by K. L. Fuller
- 113 **Wireless World's 60th Birthday**
- 113 **H.F. Predictions**
- 114 **Elements of Linear Microcircuits—6** by T. D. Towers
- 119 **Electronic Voltmeter for 2 to 50kV** by A. M. Albisser & N. F. Moody
- 122 **Circuit Ideas**
- 123 **Letters to the Editor**
- 126 **Electronic Building Bricks—10** by James Franklin
- 127 **New Approach to Class B Amplifier Design** (concluded) by P. Blomley
- 132 **Multiple-array Loudspeaker System** by E. J. Jordan
- 134 **Announcements**
- 134 **Conferences & Exhibitions**
- 135 **Choosing a Vidicon** (concluded) by D. J. Gibbons
- 139 **Diode Switching using Charge Analysis** by B. L. Hart
- 143 **Letter from America**
- 144 **World of Amateur Radio**
- 145 **New Products**
- 149 **Personalities**
- 150 **Literature Received**
- 151 **March Meetings**
- 152 **Real & Imaginary** by "Vector"
- A100 **APPOINTMENTS VACANT**
- A112 **INDEX TO ADVERTISERS**



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## Concepts and Reality in Electronics

One of the difficulties in studying electronics is to know what conceptual level a lecturer or writer is on when he is explaining or describing something. Even if one is familiar with all the technical terms and symbols, and has crossed the first hurdle—that the meaning is not simply the sum of the facts—there is still this slight worry about where exactly the meaning lies on the scale of reality, a scale that stretches from the groundrock of sense data to the stratosphere of abstract notions.

One sees such a scale in logic systems. At the top (for the sake of a reference point) there is the level of abstract logical relationships which can be expressed in words or some other kind of symbolism. Next down, and seemingly more “real”, is the functional or black-box level concerned with states (on, off, up, down etc.), which are usually represented by voltages or currents. Below this is the hardware level, of interconnected devices and components with electrical energy shunted about among them, which is describable in engineering terms without any reference to logic as such. Lower down, and hardly recognizable as logic, is the level of tangibles: the materials and electricity, which one can experience directly without being an engineer. (Of course the reality of even this level is dubious, based as it is on complementary concepts of waves and particles, so it might equally well be placed at the top of the scale of abstractness.)

For the student the middle of this conceptual scale is the most tricky because the terms and symbols used can have various degrees of abstractness. If we see a NOR gate symbol, do we think of the pure logical function or of a familiar circuit configuration? It must depend on the context. At this level, more or less, we have those shifty characters voltage and current. Owing to their long history in electrical power engineering, and their common usage by the layman, these variables have acquired the reputation of being the real stuff of electricity. As a result when we hear such terms as voltage drive, voltage gain or voltage feedback we might easily come to think that the drive, gain or feedback takes place solely by voltage alone and that current doesn't enter into the process. This may lead us into all sorts of confusion in trying to understand what is going on. It is only when we come to examine voltage or current more closely that we see the will-o'-the-wisp nature of these apparently solid citizens. Apart from being concepts they exist only as instrument readings. Thus something that we may think of as comparatively “real”, such as voltage gain, turns out to be more in the nature of an indicator of the real thing—an indicator that has been invented mainly because voltmeters are readily available and we therefore like to use voltage for design and specification purposes. To see the full picture we must know what are the input and output impedances across which the voltages are measured.

The practical experimenter tends to blame mathematics for many of the conceptual difficulties met in studying electronics. It is true that mathematical concepts, such as the mysterious square-root-of-minus-one, have taken hold in electronics pretty extensively. But this is not to be considered as some sort of infestation. If mathematics had not provided ready-made concepts we would have had to invent our own, and it is doubtful whether even these would have helped to dispel the slight confusion we are bound to feel when encountering different aspects of reality.

# Wein-bridge Audio Oscillator

Provides 10Hz to 100kHz in eight  $\sqrt{10}$  steps and uses a m.o.s.f.e.t. as the input device

by A. J. Ewins

In the 'good-old-days' before the invention of the transistor, an audio oscillator designed on the Wein-bridge principle used a double-gang variable capacitor for fine control of the frequency and fixed resistors to determine the frequency range. Because of the lower input impedance of transistor circuits, Wein-bridge audio oscillators employing them have reversed the roles of the variable capacitor and fixed resistors to fixed values of capacitors with variable resistors. Some excellent oscillators have been designed on this basis\* but good double-gang variable resistors and accurate fixed capacitors tend to be rather expensive. Now that the m.o.s.f.e.t. is available, with its extremely high input impedance, it is possible to revert to the original design using variable capacitors and fixed resistors should it be considered desirable to do so. The author thought that the design of such an oscillator was worth the attempt.

One possible solution to using a m.o.s.f.e.t. as the input device would be to place a 'source-follower' circuit in front of a good existing transistor design. However, the author's approach has been to start at the beginning and arrive at a m.o.s.f.e.t. input stage with exceptionally high voltage gain.

## Design procedure

Neglecting the frequency selective positive feedback and the voltage stabilizing negative feedback loops the design of a high-gain amplifier with a m.o.s.f.e.t. as the input device is first considered.

Fig. 1 shows the typical transfer characteristic of the RCA 40468A m.o.s.f.e.t. used by the author. This device was chosen because of its low cost and high value of transfer conductance (7.5mA/volt). With a drain current of about 5mA the transfer characteristic is fairly linear and the transfer conductance is at a maximum of about 7.5mA/V for source-to-drain voltages in excess of about 10V. As will be seen from the transfer characteristic, the gate-to-source bias voltage at a drain current of about 5mA is typically -1V. As this bias voltage may vary between samples of the m.o.s.f.e.t., it was thought advis-

able to bias the gate with a positive voltage, as for a conventional n-p-n transistor, and use a suitable value of source resistor to obtain the correct source voltage at the chosen value of drain current. With the voltage on the gate chosen to be 5V, the expected source voltage is 6V. With a drain current of 4.5mA, a value for the source resistor of 1.33k $\Omega$  is obtained. A 1k $\Omega$  resistor was used in series with a 330 $\Omega$  resistor; the 330 $\Omega$  resistor forming part of the negative feedback loop. With this biasing arrangement, the drain current will be within  $\pm 10\%$  of its design value (assuming precise values of resistance) for variation in the gate-to-source bias voltage of  $\pm 50\%$  (i.e.  $\pm 0.5V$ ).

With a positive supply of 22.5V, the source voltage set nominally at 6V and a drain-to-source voltage of at least 10V, the maximum value of resistance that may be placed in the drain line of the m.o.s.f.e.t. is  $(22.5 - 6 - 10)/4.5$  which equals 1.45k $\Omega$ . Thus, since the voltage gain of a m.o.s.f.e.t. stage is proportional to the load on its drain, the maximum voltage gain attainable from the circuit would be approximately 7.5mA/volt  $\times$  1.45k $\Omega$  which equals 11. (This is assuming, of course, that the source resistor is decoupled.) The voltage gain of this stage could be improved by increasing the value of the drain resistor, necessitating an increase in the positive supply voltage. However, in view of the fact that the absolute maximum drain-to-source voltage is 20V for this particular type of m.o.s.f.e.t. it would not be advisable to increase the supply voltage by any appreciable amount.

One way of making the drain load appear

high while maintaining a low supply voltage is to replace the drain resistor with the collector circuit of a transistor which has a fixed emitter resistor and a constant base voltage (i.e. a constant current circuit). The variation of collector current with varying collector voltage is negligible for such a configuration, giving an output impedance in the collector line in excess of 100k $\Omega$ . Thus, with the constant current matched to the drain current of the m.o.s.f.e.t., the voltage gain of the m.o.s.f.e.t. stage is potentially increased to a value in excess of  $100k\Omega \times 7.5mA/V = 750$ .

Having decided on a constant current circuit as the load for the m.o.s.f.e.t. stage the problem arises as to how to match the constant current to the chosen value of drain current and to stabilize the voltage on the collector and drain of the constant current transistor and m.o.s.f.e.t. By means of d.c. negative feedback from the collector/drain junction, either the f.e.t.'s drain current may be controlled by varying the bias voltage on its gate, or the constant current may be controlled by varying the voltage on the transistor's base. Figs. 2(a) and 2(b) illustrate these two possible methods. The drawback of both these methods is that the d.c. feedback line imposes an unwanted load on the drain of the m.o.s.f.e.t. stage, reducing its voltage gain. The second method having a more drastic effect than the first. The first method was attempted using feedback resistors with values in the megohm region. However, it proved unsuccessful in that low-frequency instability resulted when an input signal was applied to the circuit.

At this stage, thought was given to the second stage of amplification and having decided on a p-n-p transistor an obvious solution presented itself. With the base of the second stage transistor directly coupled to the drain of the first stage, the d.c. voltage developed across its emitter resistor could be tapped to provide the base of the constant current transistor with just the correct amount of d.c. voltage to produce the required value of constant current, thus stabilizing the d.c. voltage at the collector/drain junction (see Fig. 2(c)). In doing this no unwanted load is placed upon the drain of the m.o.s.f.e.t. stage

Using this method of matching the constant current load to the chosen value of drain current results in an extremely stable

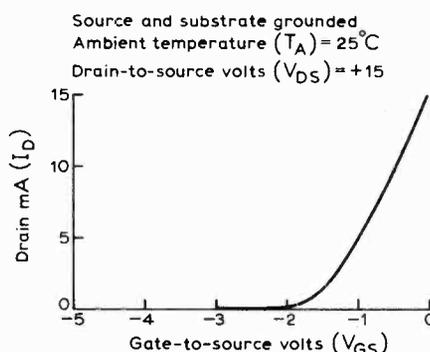


Fig. 1. Characteristics of the R. C. A. 40468A m.o.s.f.e.t.

\* Ridler, B. E., "Low-distortion R. C. Oscillator". *Wireless World*, August 1967.

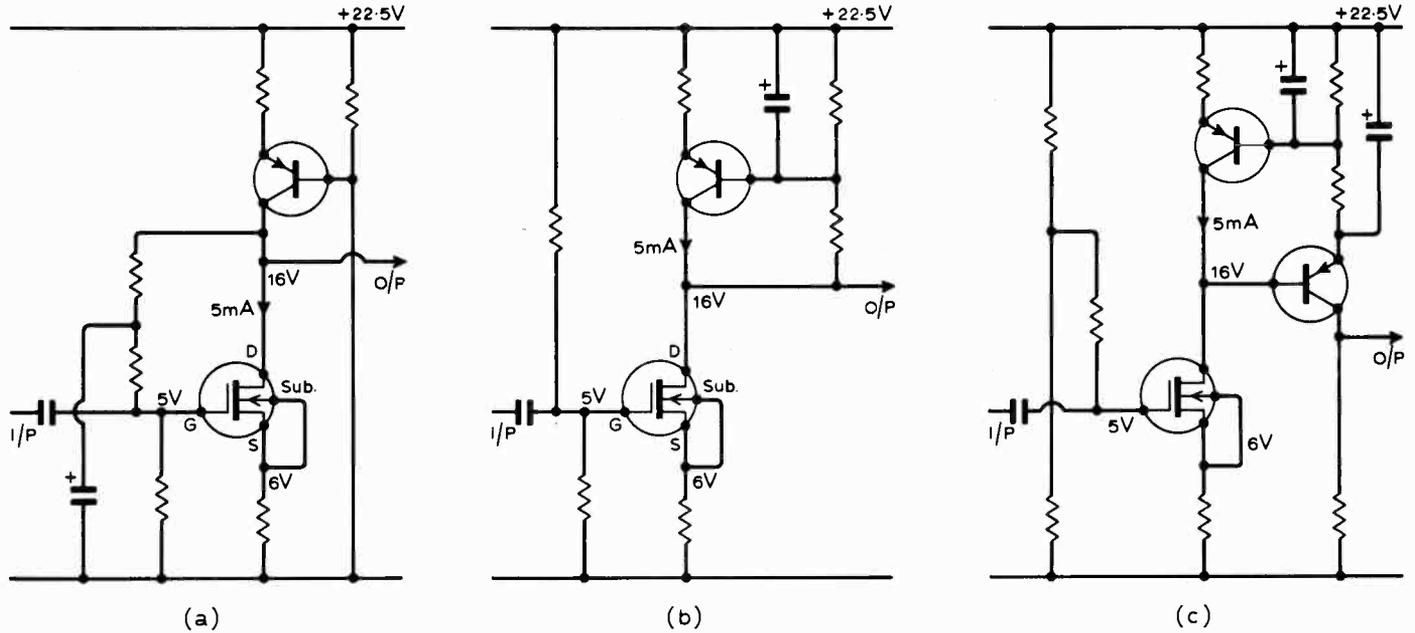
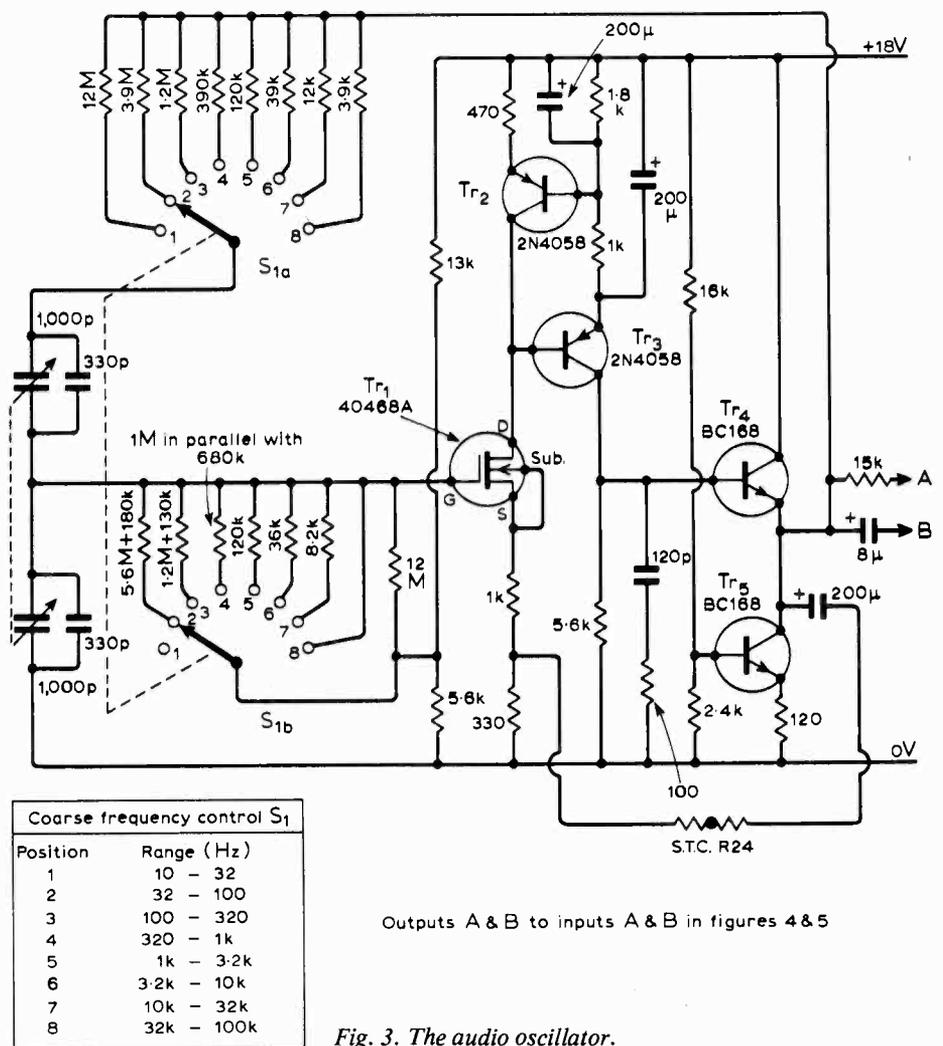


Fig. 2. (a and b) Two ways of stabilizing the voltage on the collector and drain of the constant current transistor and m.o.s.f.e.t. (c) the solution employed.

working point d.c. voltage at the collector/drain junction of the first stage. For variations in the bias voltage of the m.o.s.f.e.t. of  $\pm 50\%$  about the design value of  $-1V$ , a variation in the d.c. voltage of the collector/drain junction of as little as  $\pm 2\%$  is achieved (assuming that all resistors are their precise values).

The design of the second stage of amplification (the p-n-p transistor,  $Tr_2$  in Fig. 3) is conventional, as is the output stage, which is an emitter follower. A constant current was used as the emitter load of the output stage in order to reduce the load on the emitter of this stage. If the output from the oscillator is to be connected to the output attenuator circuit of Fig. 4, or if the load applied to the output from the oscillator is not likely to be less than  $1k\Omega$ , the constant current circuit may be replaced by a resistor of about  $470\Omega$  without any detriment to the oscillator's performance. As shown in Fig. 3, the minimum value of resistance that may be applied to the output from the oscillator is  $220\Omega$ .

Fig. 3 shows the circuit diagram of the audio oscillator as described. It will be seen that the frequency selective, positive feedback is a conventional Wein-bridge circuit. The frequency ranges (coarse control) are provided by means of switched selected fixed resistors, the double-gang variable capacitor providing the fine frequency control. Using values for the resistors and capacitors as shown in Fig. 3 gives frequency coverage over the range of 10Hz to 100kHz in eight  $\sqrt{10}$  steps. i.e. 10 to 32Hz, 32 to 100Hz, etc. The double-gang, 1000pF, variable capacitor is a four-gang, 500pF, tuning capacitor with its four sections divided into two pairs; the two sections in each pair being connected in parallel. The tuning capacitor used by the author is an expensive item and rather upsets the argument of a cheap, fine-frequency control. However, a double-gang, 500pF tuning capacitor, which may certainly be obtained for less than 10s, may



Coarse frequency control $S_1$	
Position	Range (Hz)
1	10 - 32
2	32 - 100
3	100 - 320
4	320 - 1k
5	1k - 3.2k
6	3.2k - 10k
7	10k - 32k
8	32k - 100k

Fig. 3. The audio oscillator.

alternatively be used, providing frequency coverage over the range of 20Hz to 200kHz, again in eight,  $\sqrt{10}$  steps. i.e. 20 to 63Hz, 63 to 200Hz, etc.

The voltage stabilizing, negative feedback is achieved by means of a thermistor as shown in Fig. 3. The type specified is an S.T.C. R24 which gives an output of about

1.4V r.m.s. The S.T.C. types, R53 and R54 may be used, providing outputs of 1V and 2.2V, respectively. Some alteration to the feedback resistor in the source line of the m.o.s.f.e.t. ( $330\Omega$ ) may be necessary with these other types.

The only capacitors in the circuit, other than the frequency selective capacitors, are

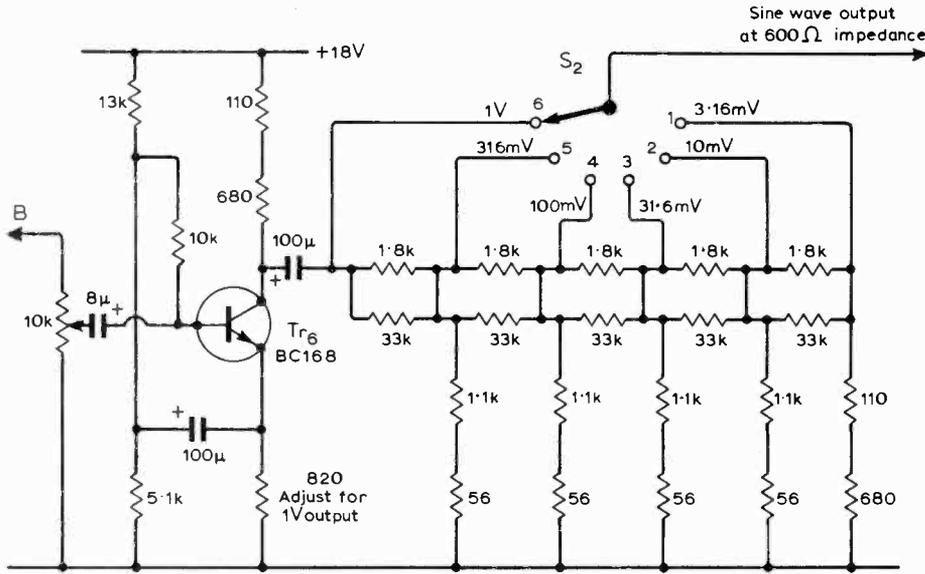


Fig. 4. Output attenuator circuit.

those in the output, in the negative feedback line and the two for decoupling around the emitter circuit of  $Tr_3$ . The role that these two decoupling capacitors play is worthy of comment. Neglecting, for the moment, the decoupling capacitor across the base of  $Tr_2$ , the capacitor decoupling the emitter of  $Tr_3$  produces maximum voltage gain in the second stage of amplification. However, its presence reduces the input impedance of the second stage, increasing the load on the drain circuit of the m.o.s.f.e.t. and hence reduces the voltage gain of the first stage. If only the  $1.8k\Omega$  resistor in the emitter circuit of  $Tr_3$  is decoupled, leaving  $1k\Omega$  undecoupled, the input impedance of the second stage is raised, increasing the voltage gain of the first stage but at the expense of a drastically reduced second stage voltage gain. Perhaps not surprisingly, completely

decoupling the emitter of  $Tr_3$  produces the greatest overall, open loop gain of the two alternatives. It may be worth experimenting with the amount of resistance left undecoupled in the emitter of  $Tr_3$  since maximum open loop voltage gain of the two stages is not necessarily achieved when the emitter of  $Tr_3$  is totally decoupled.

Returning now to the decoupling capacitor on the base of  $Tr_2$ ; it was found necessary to have this in order to maintain the high gain of the amplifier down to low frequencies. The open loop gain of the amplifier as shown in Fig. 3 was found to be in excess of 5,000 at 1kHz. The 120pF capacitor connected in series with the 100Ω resistor across the collector load of  $Tr_3$  tailors the high-frequency response of the amplifier and prevents any unwanted high-frequency oscillations from occurring. For

this reason also, the  $1k\Omega$  resistor in the source line of the m.o.s.f.e.t. was left undecoupled.

The circuit of Fig. 4 provides a means of varying the output voltage from 0 to 1V in six,  $\sqrt{10}$  steps with a constant output impedance of  $600\Omega$ . The  $820\Omega$  resistor in the emitter of  $Tr_6$  may be adjusted, if required, so that, with the variable control set at maximum, the output from the attenuator in position six is exactly 1V. The resistors used in the constant output impedance attenuator were of 5% tolerance, being perfectly adequate for the author's requirements. Resistors of 1 or 2% tolerance may, of course, be used if a greater degree of accuracy is required.

Readers will notice that, although the audio oscillator was originally designed to operate from a supply of 22.5V, the circuits of Figs. 3 and 4 are shown as operating from an 18V supply. After the initial design was made the author reasoned that a supply of 18V would be more convenient should battery operation be preferred. Consequently, after initial experimentation with the circuit, a prototype and final model were constructed for use with an 18V supply. All performance data given is for an oscillator operating from an 18V supply.

The author does not have ready access to harmonic distortion measuring equipment and, as a result, was unable to check the overall performance of the oscillator until it had been completed. The total harmonic distortion of the oscillator, which was discovered to be predominately second harmonic, was measured at the output of the output attenuator circuit at a level of 1V and was found to be less than 0.15% over the range of 25Hz to 25kHz. The author was able to employ the services of Brunel University's electronics department for this measurement and wishes to thank its staff for their co-operation.

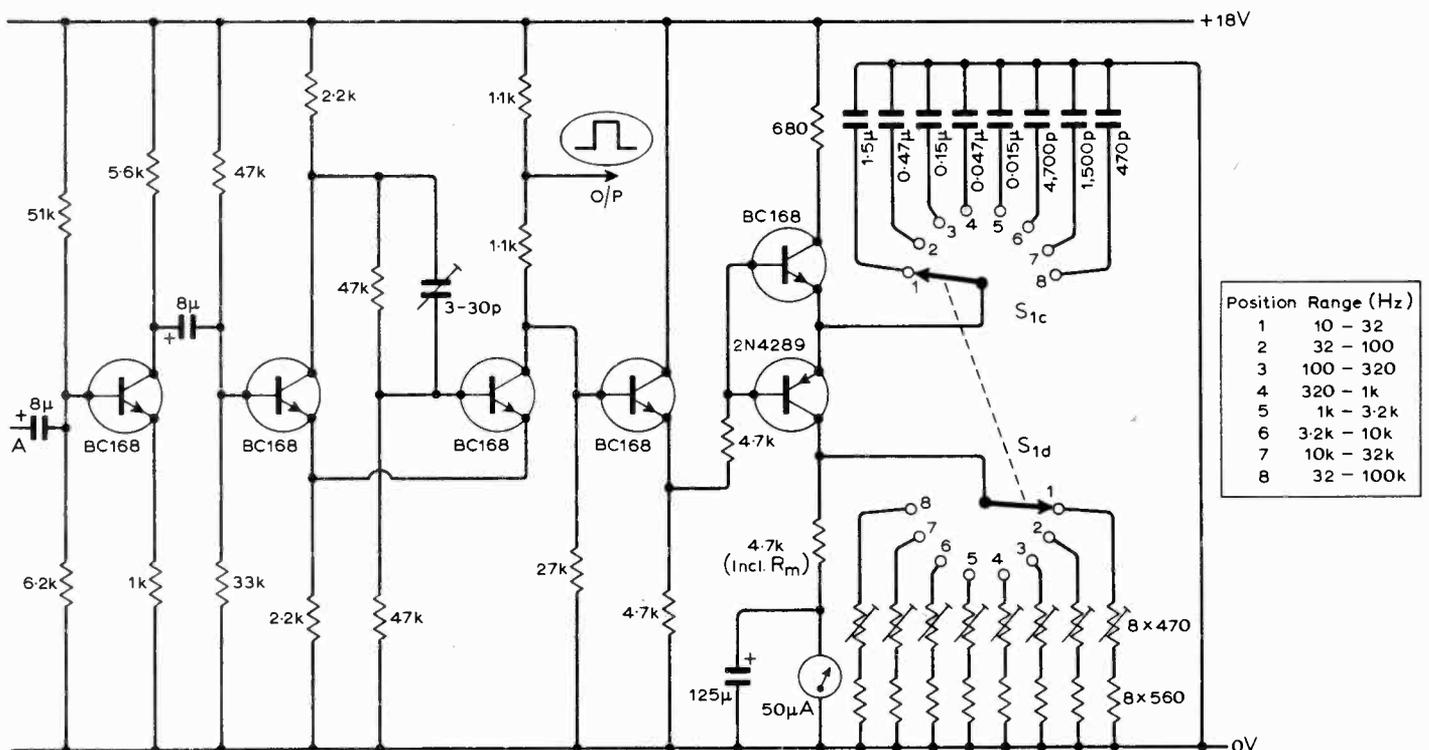


Fig. 5. Frequency meter and square-wave shaper.

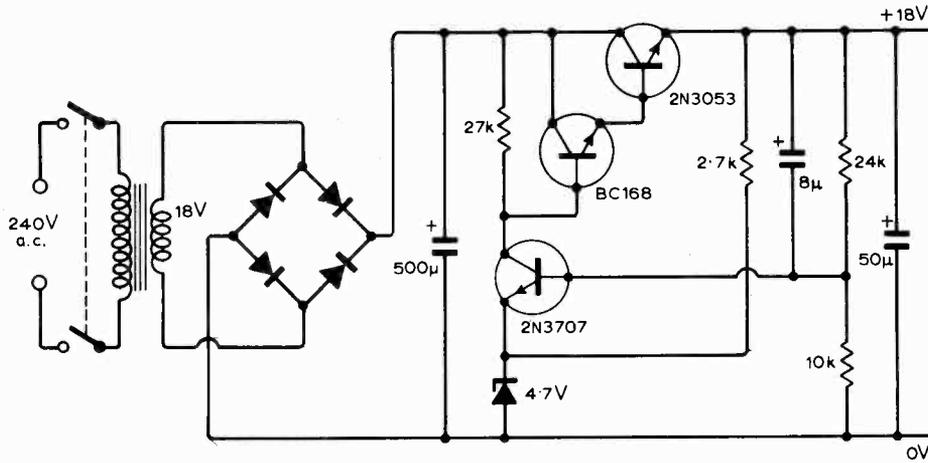


Fig. 6. The circuit of the power supply unit.

Because the design of the oscillator was very much by rule-of-thumb, it is to be expected that it is capable of refinement with, perhaps, an improvement in the distortion figures.

**Calibration**

As with all test instruments, calibration of the oscillator poses a problem and is best achieved with the aid of a digital frequency meter. Calibration of two adjacent ranges, e.g., the ranges 100 to 320Hz and 320Hz

to 1kHz, is all that is necessary, provided that 1% tolerance resistors are used for the construction of the coarse frequency control, as the relationship between alternate ranges will hold good for all the ranges covered by the oscillator. The author, however, used 5% tolerance resistors, having decided to build-in a frequency meter to the completed oscillator. For those readers who may be interested the circuit of the author's frequency meter is shown in Fig. 5. The same switch that selects the frequency range of the oscillator was used to select

the frequency range of the meter. As part of the frequency meter is a square-wave shaper, a square-wave output was made available with a peak-to-peak voltage of approximately 4V. The rise time of the square-wave was less than 0.2µsec at a frequency of 100kHz.

**Performance**

No tests were carried out as to the frequency or output voltage stability of the oscillator with variations in room temperature or supply voltage. However, there is no reason to expect these to be any different from other oscillators of a similar design. Typical values that may be expected are: frequency stability; better than 2% for ±10°C variation; less than 1% for ±5% variation in supply volts. Output voltage stability; less than 3% for ±10°C variation; less than 1% for ±5% variation in supply volts.

The output voltage variation with frequency was found to be less than 1% over the entire range of the oscillator.

The distortion figures of the oscillator are not exceptional and are, as previously mentioned, less than 0.15% over the frequency range of 25Hz to 25kHz.

As the circuit of the frequency meter used by the author is sensitive to changes in supply voltage, he used a mains operated, stabilized power supply capable of delivering up to 100mA at 18V. Fig. 6 shows circuit of the author's power supply.

# Demonstrating Multivibrator Action

T. Palmer\*, B.A., Assoc.I.E.R.E.

When teaching the action of an astable multivibrator to students, there is the difficulty that, no matter at what point in the cycle we begin, the action is determined by what happened in a previous period. If the important feature at a certain moment is that a capacitor is discharging, we have to go back in time to explain how it became charged. These difficulties can be avoided by starting at a certain point, which I call stage 1, and for which the circuit is shown below.

**Stage 1.** With switch  $S_1$  open,  $A_1$  reads zero,  $A_2$  reads 6mA, and  $A_3$  reads 6mA. When  $S_1$  is closed,  $A_1$  immediately gives a reading of 6mA. The reading on  $A_2$  falls to zero and stays at zero for a certain time. It then rises to 6mA. When the reading on  $A_2$  rises to 6mA, that on  $A_3$  falls to zero and stays at zero for some time; eventually it rises to 6mA. All the meters continue to read 6mA.

The moral to be drawn from the demonstration so far is that when any transistor starts to pass current, its neighbour on the right stops passing current for a certain period. If  $C_1$  and  $C_2$  are banks of 100µ F capacitors it is easy to show, by varying  $C_1$  or  $C_2$ , how the

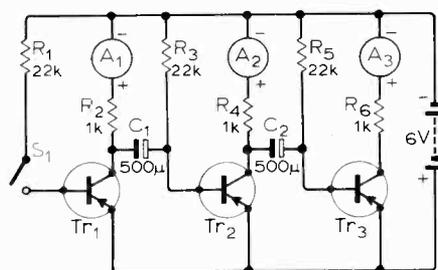
delay is related to the value of capacitance (100µ F for a short delay, 800µ F for a long delay).

**Stage 2.** Switch  $S_1$  is open; the lead from  $C_2$  which previously was connected to the base of  $Tr_3$ , is now connected to the base of  $Tr_1$ . Initially,  $A_1$  reads zero,  $A_2$  reads 6mA, and  $A_3$  reads 6mA. When  $S_1$  is closed,  $A_1$  immediately reads 6mA and  $A_2$  reads zero, because of the action illustrated in stage 1. Eventually the reading on  $A_2$  rises to 6mA and now  $Tr_1$  behaves in the same way as  $Tr_3$  in stage 1. Whereas  $Tr_3$  could not affect  $Tr_2$ ,  $Tr_1$  can. Whenever either of the transistors starts to

pass current, the other one is switched off. The pattern continues indefinitely.

If the transistors and resistors are mounted on an S-DeC†, it is not necessary to have a switch for  $S_1$ : simply insert the leads of  $R_1$  in the appropriate holes. The circuit can easily be changed from that of stage 1 to that of stage 2 by plugging the lead from  $C_2$  in a hole associated with the base of  $Tr_1$ .

Students often have difficulty understanding that in an astable multivibrator of this type the base can swing appreciably positive to the emitter. It is instructive to improvise a voltmeter out of a centre-zero 25µ A meter in series with a 1MΩ resistor. Such a voltmeter connected between base and emitter of  $Tr_2$ , for instance, shows that immediately after  $Tr_2$  has stopped passing current, the base is momentarily 6V positive with respect to the emitter. Students can see that it is not until the base is slightly negative to the emitter that collector current starts to flow in  $Tr_2$ . Eventually some of them may be persuaded to have some faith in the statements made to them about RC circuits. Even if they are not, the demonstration keeps them out of mischief.



Circuit for demonstrating astable multivibrator action. Meters are 0-10mA types.

† S-DeC. is available from SDS Electronics Ltd, 34 Arkwright, Astmoor Industrial Estate, Runcorn, Ches.

\* Acton Technical College, London

# News of the Month

## Sony defies PAL patents

A colour television receiver is to be introduced in April which is unlike any other on sale in this country. Instead of using the three-electron-gun shadow-mask tube Sony, who produce the receiver, are employing a tube of their own design which they have called the Trinitron. In the tube a single electron gun produces three beams which are magnetically deflected to provide the scan and electrostatically deflected for convergence purposes. Unlike the shadow-mask tube, which has the three beams arranged in a triangle, the Trinitron employs a 'horizontal-in-line' beam geometry. This arrangement, claims Sony, means that in optical terms one is using a large lens with a small aperture giving very high definition. Certainly on receivers viewed by *Wireless World* the definition was very good although the convergence arrangements were such

that a slight colour fringing on black and white pictures was visible at the extreme corners of the picture. Incidentally convergence has to be carried out in one plane only and therefore the controls are few and simple.

In place of the shadow mask the Trinitron employs a metal plate with vertical slits running the height of the tube face. The phosphors are also applied in stripes.

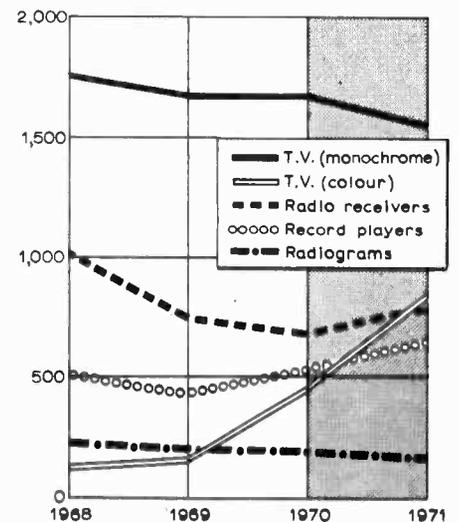
Sony have not a licensing agreement with AEG-Telefunken who developed the PAL television system and who hold the patent rights. Sony say that their 'system employs a completely new concept of reception for the British colour TV broadcasting standard'. Just how different the circuitry is we were unable to establish as Sony will not release any details at this stage. All we were able to find out was that no valves are used.

Sony must be very sure of their position because, although their set receives and processes PAL colour television signals (and the make-up and format of these signals are covered by AEG-Telefunken patents), they claim that they are not infringing any of the patent rights. It will be interesting to follow Telefunken's reaction to the announcement.

The new set has a 13in screen (in line with Sony's earlier preference for small sets); it weighs 39lb, and has a recommended retail price of £199.75.

Another Japanese firm who will soon be launching a range of PAL colour television sets, this time with a licensing agreement with AEG-Telefunken, is Hitachi.

## Domestic radio and TV deliveries



The graph shows the deliveries of U.K. manufactured radio and television receivers and record playing equipment to the trade (multiply by one thousand) as released by the British Radio Equipment Manufacturers' Association. We have projected the curves into 1971 although we may perhaps have erred on the side of optimism. The colour TV market will almost certainly increase its rate of growth but it would be very difficult to say what sort of impression imported colour receivers are going to make and the share of the market they are going to win. We feel that the radio receiver market will start to pick up because public interest in v.h.f. receivers will be aroused by the discussions on local and commercial radio that will take place during the year.

## Touring Exhibition

During 1971 a series of 'Electromation Exhibitions' will be held throughout the country. Some of the firms taking part will be: Cannon Electric, Watford Electric, Elite Engineering, Gresham Lion Electronics, Seiga Electronics, Mullard, Bowthorpe Hellerman, Rowband Electronics, Coutant



*The photograph shows a portable position indicating unit which operates in conjunction with the U.S. Navy's navigational satellite system and a master station which may be hundreds of miles distant. As the satellite rises over the horizon both the master and portable stations record the satellite's signals and the portable station then transmits this information to the master station. The master first computes its own position using the doppler shift of the satellite's signals and then computes the portable station's relative position. This information is then transmitted to the portable station. The portable station weighs 27lb and was built by Honeywell.*

Electronics, S.D.S., Interface Components, Stabletron, Integrated Photomatrix, Avdel, Excel Electronics, Murex, G.D.S. Sales, Highland Electronics, Electrical Remote Control, Chemical Processes, Vero Electronics, Craig & Derricott, Membrain, and Hallam Sleigh & Cheston. The exhibitions will be held at the following places.

Feb. 23-25 Guildhall, Plymouth

April 6-8 Excelsior Hotel, London Airport

20, 21 Station Hotel, Newcastle

22, 23 Grand Hotel, West Hartlepool

June 9, 10 Central Hotel, Glasgow

11, 12 Caledonian Hotel, Edinburgh

22, 23 Hotel Leofric, Coventry

24, 25 North Stafford Hotel, Stoke-on-Trent

July 6, 7 Adelphi Hotel, Liverpool

8, 9 Midland Hotel, Bradford

20, 21 Grand Spa Hall, Bristol

22, 23 Rank Banqueting Suite, Swansea

Sept. 7, 8 Queen Hotel, Leeds

9, 10 Royal Victoria Hotel, Sheffield



*The traffic control room at the Dartford tunnel. S.T.C. have recently installed a single-channel u.h.f. communication system which allows contact with service control vehicles. The use of u.h.f. has overcome the problems of receiving the signal inside the tunnel itself and no dead spots exist at the tunnel mouths due to cancellation effects.*

## BBC-2 trade test transmissions

During the following transmissions the sound sequence will be: four-mins 440Hz tone, one-min no sound and fifteen-mins of recorded music.

### Monday to Friday

09.00 Test card F	14.28 Caption
09.58 Caption	14.30 Service information
10.00 Service information	14.35 Colour film
10.05 Test card F	15.00 Test card F
11.00 Colour prog. or film	15.30 Colour film
11.20 Test card F	16.00 Test card F
11.28 Caption	16.10 Colour bars
11.30 Service information	16.15 Test card F
11.35 Colour film	16.30 Colour film
11.55 Colour bars	17.00 Test card F
12.00 Test card F	17.10 Colour bars
12.10 Colour film	17.15 Test card F
12.25 Colour bars	17.30 Colour film
12.30 Test card F	18.00 Test card F
14.00 Colour film	18.15 Colour film
14.20 Test card F	18.40 Test card F

### Saturdays

As Mondays to Friday except for:

14.50 Test card F	16.35 Test card F
15.00 Saturday cinema	17.00 Colour film

## T.E.M.A. awards

The annual awards to the winners of the competition for technologists and technicians were made at the annual dinner of the Telecommunication Engineering & Manufacturing Association on February 2nd. The entrants from member companies submitted essays on some aspect of their studies or training. The winner in the technologist grade (confined to graduate trainees or those in

the final year of their studies) was Jack Roberts, B.Sc. (Hons.), of Creed & Co, and the runner-up was Richard P. Edwards of the Marconi Company. Winner in the technician class was Peter J. Walters of GEC-AEI Telecommunications.

## Emley Moor again

The new aerial at Emley Moor is now operational and it is hoped that about 1.75M more viewers will be able to receive programmes than with the temporary aerial, which has been in use since the collapse of the original mast.

The lower portion of the new mast is a 900ft high concrete tower, 80ft in diameter at the base, and weighing 14,000 tons. The top 180ft of the mast (the total height is 1,080ft) is a steel lattice structure containing the various aerials. The main companies who have built the new mast for the I.T.A. are Ove Arup and Partners (consultants), Tileman and Co. (main contractors for the tower) and E.M.I. (aerials).

The I.T.A. have also recently announced that a £1M contract has been awarded to Marconi for 15 television transmitters to be installed in various parts of the country from 1972 onwards.

## The Physics Exhibition

The Physics Exhibition will again be held at the Alexandra Palace, London (19th to 22nd April). There will be an increased number of exhibitors from overseas including France, Hungary and Israel, as well as a large stand which will be organized by the Federation of Scientific and Technical Associations of Italy.

An important change has been made in

the regulations relating to equipment and instruments in production. In the past to qualify for the exhibition instruments, or other apparatus, had to show 'substantial advances on or differences from existing apparatus, instruments or techniques'. The eligibility of each item was assessed by a committee. This process will continue for the 1971 exhibition but in addition, for every experimental or new item the committee consider suitable for the exhibition the exhibitor may also exhibit one item, or in some cases two, from production. The organizers, the Institute of Physics and the Physical Society, say that by this change in the regulations 'it is hoped to restore the interest in scientific instrumentation and careful measurement which was a feature of the early Physical Society Exhibitions and that a balanced exhibition of interest to physicists, both pure and applied, will result.

While appreciating the reasons for this change in the regulations we sincerely hope that this new licence to exhibitors will not be abused. It would be very sad to see the exhibition become a happy hunting ground for the salesmen.

In place of the open forum which has been a feature of the last two exhibitions there will be a joint meeting of the Education and Electronics Groups of the Institute (2.30 p.m., 21st April). The lectures that will be held during the exhibition are as follows: 'The Impact of Electronics in the Medical Field', Professor Vito Svelto, University of Panavia (3.30 p.m., 19th); 'Science Teaching at the Open University', Professor M. J. Pentz, dean and director of studies in science at the Open University (3.30 p.m., 20th); and 'Holography, Industry and the Rebirth of Optics', J. W. C. Gates, division of optical metrology, the National Physical Laboratory (3.30 p.m., 22nd).

# AVOID -Short-range High-definition Radar

by K. L. Fuller\*

**An experimental short-range radar has been built for detecting airfield vehicles. Using a c.w. frequency modulation ranging technique in conjunction with a frequency-sensitive steerable aerial, it achieves azimuth scan from the same frequency modulation. The radar also has marine and military applications.**

With the growing use of fully automatic landing systems at airfields there is an increasing need to drive vehicles on the airfield at fairly high speeds in conditions of poor or zero visibility. After a successful automatic landing it is necessary to guide the aircraft from the end of the runway via the taxi-track to the main terminal building. This could be done with buried cables in the taxi-tracks, but would have the disadvantage that considerable installation work would be required and the system would not be flexible. Further, although following the cable would keep the aircraft on the correct route, there would be no guarantee that the route was free from obstacles. In the case of an unsuccessful automatic landing in fog resulting in a crash, it is obviously essential that fire tenders and ambulances should be able to reach the scene as soon as possible, without colliding with obstacles and survivors en

\*Mullard Research Laboratories, Redhill, Surrey.

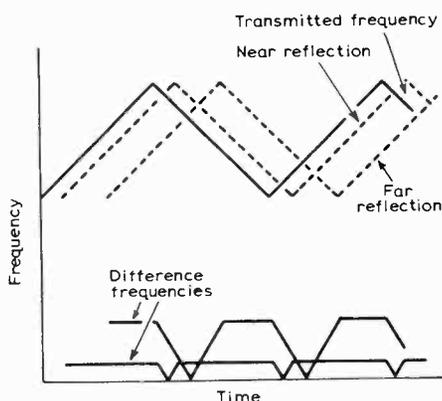


Fig. 1. Transmitted and received signals in an f.m.-c.w. radar. Near target produces low difference frequency and a distant target a higher difference frequency.

route, and here a really effective aid to vehicle navigation in zero visibility is required.

It has therefore been decided that a radar which looks over a sector of about  $60^\circ$  ahead of the vehicle and with a maximum range of perhaps 160 metres is the most practical solution. To produce a useful picture such a radar would need a short-range performance and range resolution performance about an order of magnitude better than current radar systems. In addition it is desirable that the radar has a rapid angular scan to avoid picture flicker and present a high information rate. In the AVOID radar system this is done with an electronic scan, giving 25 complete pictures per second. (AVOID is an acronym for airfield vehicle obstacle indication device.)

## Range measurement

To achieve a two-metre resolution over the range 3 to 160 metres would require a pulse length of 10ns if conventional pulse techniques were used, which would present almost insoluble problems of bandwidth, generation and T/R switching.

An alternative approach which seemed attractive at first sight was the use of an ultrasonic radar system because the velocity of propagation is much lower, so the range resolution can be obtained with more reasonable pulse lengths and bandwidths. When this was tried several major difficulties arose. First, the attenuation of ultrasonics in air is high and hence it is extremely difficult to obtain ranges in excess of 20 metres with a reasonable transmitter power. Second, due to the low velocity of propagation, the information rate from the radar is insufficient to produce a useful up-to-date picture. Third, the ultrasonic radar is very sensitive to interference generated by jet engine noise.

It was therefore decided to use conventional microwave radar but to measure range by applying a linear frequency modulation to a continuous transmission (Fig. 1). The transmitter frequency, shown by the solid line, increases linearly with time until it reaches the end of the frequency range of the device and then decreases. A return signal from a close target (broken line) will have

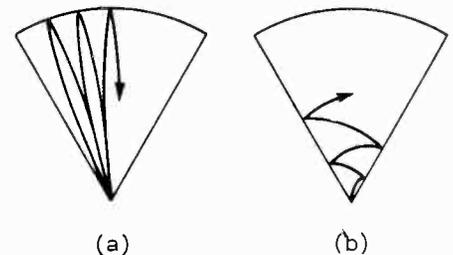


Fig. 2. Two azimuth scanning systems (a) mechanical and (b) electronic. In the electronic system scanning is achieved by using an aerial whose radiation pattern changes with frequency.

the same shape but delayed slightly in time, and the return signal from a more distant target will again be the same shape but delayed more in time. If these return signals from the targets are mixed with a sample of the transmitter output, and the difference or beat frequencies extracted, the close target will produce a low difference frequency and a more distant target will produce a higher difference frequency. In general there will be targets at all ranges, so a spectrum of difference frequencies will be produced with frequency proportional to range. These frequencies will momentarily go down to zero and return to their normal value at the turn-round points on the main frequency sweep. If the time for this turn-round is kept short compared with the sweep time, this effect can be neglected.

One major advantage of this method is that the transmitter is running continuously and that the effective power is the mean or continuous power of the transmitter, and this therefore lends itself ideally to solid-state microwave generators. Unfortunately it is not possible at this time to produce a solid-state generator with enough output power frequency-modulated over a sufficient frequency range, but it is expected that these will be available in the very near future. At present the transmitter is a backward-wave oscillator frequency modulated from 8 to 11.5GHz and producing 100mW output.

If the return signals from the targets are to be used efficiently, they should be fed into a bank of filters where the energy

corresponding to each range element is integrated. Ideally there should be one filter for each range element and with a time constant equal to the 'illumination' time of that particular target. In the experimental radar the complexity of a bank of filters was too great, and instead a single swept superhet filter is used which scans through the range spectrum and converts the parallel returned information into a more conventional serial range scan. The resultant loss of sensitivity is not serious in a short-range system. To have good range resolution a linear frequency sweep is needed. For example, if it is required to resolve to one part in a hundred of the maximum range, the linearity of the sweep has to be approximately 1%.

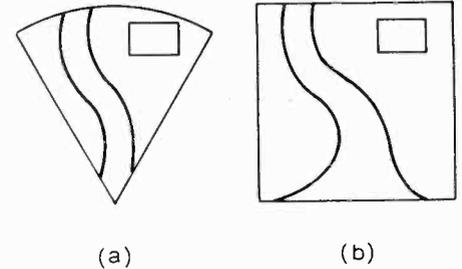
**Azimuth scan**

In a conventional pulse radar the range scan rate is determined by the velocity of propagation, but in AVOID the range scan obtained from the superhet just described can be carried out at any rate convenient to the system. If the range is scanned from minimum to maximum and back again in a triangular form, and at the same time the aerial is slowly scanned in azimuth, the picture will be built up in a petal form shown in Fig. 2(a).

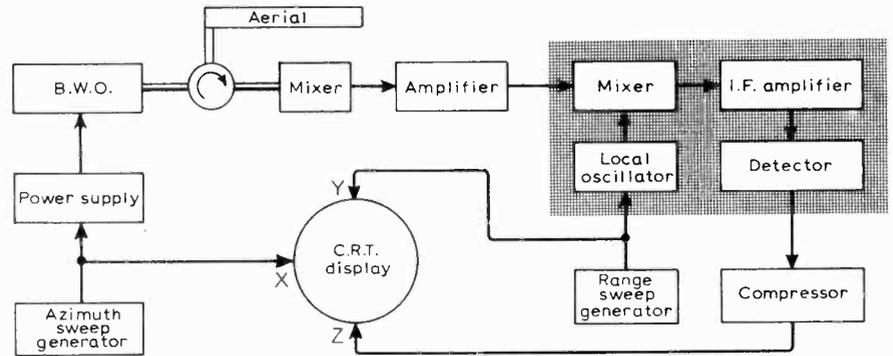
Because it is not desirable to have a mechanical scan for various reasons an electronic scan was used. The method chosen uses an aerial whose angle of radiation depends on the frequency of the signal fed to it, and it is possible to use the same frequency sweep used for range measurement to produce the angular scan. Examination of the parameters of the system shows that the angular scan must be fast and the range scan slow in comparison, so the picture is built up as shown in Fig. 2(b).

The first aerial to achieve this result consisted of a piece of waveguide 1.2 metres long with circular holes cut in the broad face. These holes were spaced a half-wavelength apart, and on alternate

(Right) Fig. 4(a). Plan view of typical scene. A radar representation of this would bear little relation to what the driver would see. Perspective view using a B scan (b) gives a truer picture.



(Below) Fig. 5. Complete system block diagram. Part enclosed by shaded box is a swept superhet receiver.



sides of the centre-line of the broad face to bring them into phase. At the centre frequency where the half-wavelength spacing was exact, the aerial radiated broadside, and the beam steered from left to right as the frequency was lowered or raised from this value. The waveguide was mounted in a vertical horn to restrict the vertical beamwidth and to give extra gain.

There were two main difficulties with this aerial. First, despite the fact that the holes were as large as possible with diameter extending from the centre-line to the outside edge, insufficient power radiated from them and 80% of the input power was dissipated in the load at the end. This loss occurred similarly on reception. Second, two spurious beams were produced at 45° in error in elevation and azimuth, and these caused low efficiency due to the wastage of power in the beams and also confusing results due to signals being returned from these

directions. These beams were attenuated heavily on the experimental model by the addition of resistive loading to the horn, but this was not a completely satisfactory solution.

The second aerial built used the travelling-wave principle, and consisted of a similar piece of waveguide, this time with a slot cut along the centre of the broad face of the guide. This slot tapers in width along the guide and is covered by a piece of dielectric material to assist radiation from inside the guide to outside. The direction of radiation is determined by the relative velocity of the wave inside and outside the guide, and as there is a velocity change within the guide according to frequency, the radiation direction changes also with frequency. This aerial has two advantages over the former aerial—it produces only one beam, and it has a much higher efficiency, about 7dB greater. It does have two disadvantages of its own. It cannot produce a beam broadside by definition, and so it has to be mounted at an angle. Also for the same frequency range the angular scan is reduced—to just over 20°.

The present aerial system is a return to the principle of the first aerial, but uses dielectric loading inside the guide. The dielectric constant and the hole spacing have been chosen to eliminate grating lobes; to obtain better radiation from the holes there is a dielectric layer on the outside. Vertical beamwidth is defined by a parabolic reflector. To remove problems at the broadside frequency, where small mismatches at the holes add in phase to produce a poor v.s.w.r. at the input, the aerial is designed to have a 35° offset, seen in Fig. 3, so that it scans from 5° to 65°.

**Display**

There are various methods of displaying the radar information to the driver. The most desirable is the provision of a



Fig. 3. Poor v.s.w.r. at the broadside frequency, caused by small mismatches at the aerial holes adding in phase, are avoided by offsetting the aerial by 35° so that it scans from 5 to 65°.

head-up display which would produce a perspective view of the scene ahead and which would superpose itself on the scene as viewed through the windscreen. This would be a very costly proposition as the head-up display mechanism is expensive, and would mean that the driver's head would have to be fixed accurately in one position. It is preferable therefore, in the experimental stage at least, to produce a display on a cathode-ray tube which the driver can look at by glancing slightly at one side. The form of the display was arrived at as follows.

Fig. 4(a) shows a plan view of a road and building. By suitable X and Y time-base generation, it would be possible to reproduce the radar version of this plan view on the screen, but this would bear little relation to what the driver sees through the windscreen. So it seems more obvious to use a radar B scan, which is range plotted versus angle, and in this case the picture would look like Fig. 4(b)—a perspective view. If the vertical range scale is linear, the picture is not in true perspective as seen by the eye but is

distorted, so a shaped range scan is used to give a more correct presentation. The B scan display is easy to produce as the two triangular scanning waveforms are already present in the circuitry of the system.

#### Experimental system

A block diagram for the complete experimental radar system is shown in Fig. 5. The backward-wave oscillator is frequency modulated over the range 8 to 11.5GHz by the azimuth sweep generator which feeds the power supply. The law of voltage versus frequency for a b.w.o. is exponential, and the power supply has a complex correction circuit to produce a linear frequency sweep. Unfortunately backward-wave oscillators also exhibit a very fine structure on their voltage/frequency curve which cannot be compensated, and is at present affecting the range resolution capabilities. The output from the b.w.o. goes via the broadband circulator to the aerial and a small amount leaks directly into the mixer to provide the local oscillator signal.

Return signals from targets go via the

circulator into the diode mixer and the difference frequencies are extracted and amplified. High difference frequencies corresponding to long range targets are amplified more than low difference frequencies corresponding to short range targets. The next four blocks on the diagram comprise the swept superhet receiver which scans through the range spectrum as determined by the range sweep generator. The output from the swept superhet is compressed in dynamic range and fed to the bright-up amplifier of the display. The X and Y signals for the display are obtained from the azimuth and range sweep generators.

One azimuth sweep takes  $400\mu\text{s}$  and one complete range sweep 20ms, i.e. the complete picture scan rate is 50Hz. The target resolution for this system is  $2^\circ$  in azimuth over a  $60^\circ$  scan, i.e. 30 elements, and two metres in range over a maximum range of 160 metres, i.e. 80 elements. Thus the complete picture is  $80 \times 30 = 2,400$  elements. An optional alternative picture rate of 25 per second has been added recently; this doubles the number of lines on the screen without changing the resolution. The effect is to produce a picture which appears to have much better definition, but at the expense of some flicker.

The experimental equipment built for laboratory evaluation has recently been installed in a vehicle, with a modified portable television receiver as the display. Fig. 6 shows a driver's view and Fig. 7 a view ahead with its radar representation.

An extensive programme of trials has shown that a short period of familiarization is necessary, after which the radar picture is found very useful.

Blind driving, with the windscreen completely obscured, has been tried in two locations; a fenced car park (empty!) and a deserted airfield. Although the driver completely lost his sense of direction, having no visual or compass information, the vehicle did not collide with any of the numerous obstacles, and it was easy to drive through a route marked by corner reflectors.

Further blind driving was undertaken during a simulated emergency at Stansted



Fig. 6. Modified television receiver acts as display in this experimental set-up.

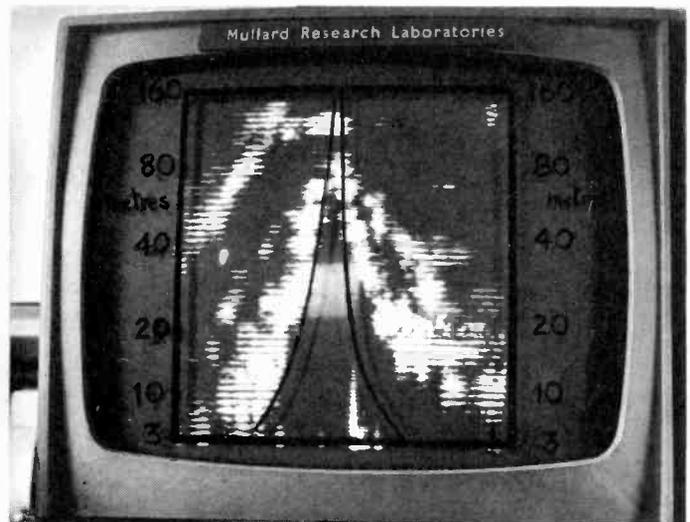


Fig. 7. View of scene and its radar equivalent.

airport in which an aeroplane and 2000 gallons of fuel were ignited. The radar vehicle, with the front and side windows blacked out, was driven successfully at about 40 mile/h over a complex course approximately 500m long, leading four fire engines to the burning aircraft.

More conventional tests and demonstrations, with a filmed record of the radar picture and the outside view, have been made at Heathrow, Gatwick and Farnborough airfields, and on the M4 motorway.

The advantages of this radar over existing conventional radar systems are

- it is cheap
- resolution and near-range performance are an order of magnitude better than conventional systems.
- it has no moving parts
- it produces a daylight-viewing flicker-free picture.
- it is simple
- it does not require high-power or high-voltage supplies
- it is unlikely to interfere with, or receive

interference from, other radars already in use on an airfield

- it is possible to alter the perspective of the display with simple circuitry changes.

It has applications other than those already suggested; for example as a harbour radar for small ships, a radar for launches in rivers and crowded waterways, as a forward-looking radar for military vehicles, or as a manpack battlefield radar. It is especially versatile if used in conjunction with a moving map display giving the direction and location of the vehicle.

Much thought has been given to the use of an alternative frequency for transmission; X-band was chosen for the experimental model for economy, because the resolution in azimuth appears adequate and performance in rain and fog known to be satisfactory at this frequency.

The design, construction and testing was carried out by K. Holford on the system and A. J. Lambell on the aerial. Much of the work was supported by the M.E.L. Equipment Company Ltd, Manor Royal, Crawley, Sussex.

## Our 60th Birthday

Eleven years before broadcasting began in this country, *Wireless World*, the world's first radio journal, made its appearance under its original title of *The Marconigraph*. The first issue was in April 1911. We plan, therefore, to celebrate our 60th birthday with a special April issue.

We have invited two former editors (H. S. Pocock and F. L. Devereux) and several other contributors to survey developments in various areas of our technology—sound reproduction, receiver techniques, communications, radio-wave propagation, basic theory etc.

These articles will be in addition to the normal quota of material so the

issue will be considerably larger than normal.

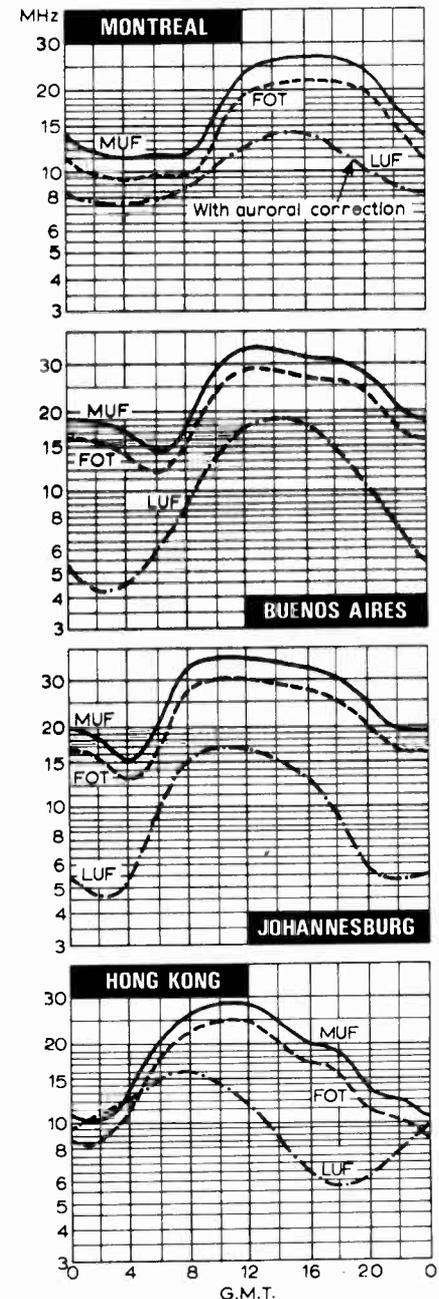
Complete constructional details are given, in the first of two articles, of a sensitive f.m. tuner design for stereo reception. Using dual-gate m.o.s.f.e.t.s, ceramic i.f. filters and integrated circuits, the tuner has a sensitivity of  $0.75\mu\text{V}$  for 20dB quieting, a capture ratio of 2dB, an image rejection of -70dB and spurious response of -94dB.

Constructional details are also given for a low-cost logic teaching aid which enables the Karnaugh map of combinational logic circuits to be displayed on an oscilloscope.

## H.F. Predictions—March

The prediction charts, drawn by Cable and Wireless Ltd, show standard median MUF, optimum traffic frequency (FOT), and lowest usable frequency. MUFs and FOTs apply in both directions. LUFs apply for reception at good sites and in the U.K. only as they are affected by local noise level.

MUF is, by definition, the frequency at which communication should be possible for 50% of the time. The FOT is usually taken as 85% of the MUF.



# Elements of Linear Microcircuits

## 6: Audio amplifiers

by T. D. Towers,\* M.B.E.

If you need an audio amplifier you could design a circuit yourself using discrete transistors. Alternatively you might use a standard off-the-shelf 'packaged circuit' (i.e. amplifiers already assembled on printed circuit boards). But nowadays you are most likely to turn to one of the commercially available integrated circuits.

In the i.c. field most of the linear amplifier circuits available that could be used for audio requirements are general purpose op-amps. To get the gain and frequency response needed for this type of op-amp you have to connect it into a network of resistors and capacitors (as discussed in previous articles in this series).

However, i.c. manufacturers have recognized that some people may not want to play about with discrete components and they have come up in recent years with 'special function' audio amplifiers.

These incorporate in the package as many as possible of the passive components that would normally have to be used externally with a general purpose op-amp. Thus there has grown up the breed of audio amplifier integrated circuits discussed in this article.

As yet, specific audio amplifiers form only a small part of the total linear amplifier microcircuits on the market. A count at the beginning of 1971 showed about 150 a.f. amplifier types against about 1500 general purpose op-amps. Another interesting feature that emerged from the count was that while the U.S.A. was the leader in general purpose op-amps., Western Europe appears to have established a powerful position out in front in monolithic a.f. amplifiers and Japan in hybrid.

Commercially available audio amplifier microcircuits fall readily into three categories, (1) pre-amplifiers (low level up to 50mW output); (2) amplifiers (mid-level with from 50 to 500mW output); and (3) power amplifiers (high level from 0.5W output upwards).

Because of the power dissipation handling difficulties in a very small chip, monolithic integrated circuits tend to be limited to pre-amplifiers and amplifiers. Power amplifiers (and certainly high-power amplifiers above about 5W) are usually thick film hybrid assemblies.

As yet there is no standardization of integrated circuit audio amplifiers. Each company engaged in their manufacture has its own special versions. In addition, while the market is settling down to some standardization, companies may produce models which subsequently go off the market or are superseded by new versions (as, for example, the PA122 of G.E., U.S.A., now superseded by the PA234). If you look at the circuits given later in this article you will see as yet little in common between the different manufacturers except that most use class A at low level and class AB complementary push-pull at high levels. So far, little use has been made of class D, although it has many features that suits it to monolithic or hybrid integration.

Table 1 lists audio amplifier microcircuits fairly readily available in the U.K. The list is still a short one, but over the next few years it will lengthen appreciably.

### Monolithic low level

Of all the various linear functions, the audio circuit is probably the most difficult to integrate because conventional audio circuits usually require large-value capacitors, which are not easily produced in monolithic form. Even so there is quite a choice from a variety of manufacturers and a circuit might have anything from two to six stages of amplification.

One of the simplest circuits is the TAA320 shown in Fig. 1(a) in a 100V, 2W amplifier. You will see that the TAA320 itself comprises an input n-channel insulated-gate f.e.t. driving an n-p-n transistor through a separate base-emitter resistor. In the external circuit, the 180 and 3.3 $\Omega$  resistors in the feedback from the loudspeaker fix the overall amplifier gain. The voltage dependent resistor suppresses potentially damaging voltage spikes across the output transistor, BD115. The circuit has a sensitivity of about 85mV input for 2W output.

Three stages of gain are found in monolithic configurations such as the TAA263, shown in Fig. 1(b). This is widely used as a basic amplifier with the addition of a load resistance between terminals two and three, and a d.c. feedback resistance between terminals three and one to set the output at the required mid-voltage. The TAA263 is designed for a 7/8V rail supply, but, in the

TABLE 1

### Microcircuit directory—a.f. amplifiers

CA3007	RCA	A.	100mW
CA3020	RCA	A.	500mW
CA3048	RCA	P.	(X 4), * 12V
CA3052	RCA	P.	(X 4), 16V
MC1302	Motorola	P.	(X 2), 12V
MC1303	Motorola	P.	(X 2), 26V
MC1306	Motorola	A.	200mW
MC1454	Motorola	A.	1W
MC1554	Motorola	A.	1W
MFC4000P	Motorola	A.	
MFC8010P	Motorola	A.	1W
MFC8040P	Motorola	P.	
MFC9000P	Motorola	A.	4W
MFC9010P	Motorola	A.	2W
OM200	Philips	P.	1.3V
PA222	GE (U.S.A.)	A.	1W
PA230	GE (U.S.A.)	P.	12V
PA234	GE (U.S.A.)	A.	1W
PA237	GE (U.S.A.)	A.	2W
PA239	GE (U.S.A.)	P.	(X 2) 24V
PA246	GE (U.S.A.)	A.	5W
PA263	GE (U.S.A.)	A.	3.5W
SI-1020A	Sanken	A.	25W
SI-1050A	Sanken	A.	50W
SL402A	Plessey	A.	1.5W
SL403A	Plessey	A.	2.5W
SL630C	Plessey	P.	12V
TAA103	Philips	P.	6V
TAA111	Siemens	P.	4.5V
TAA121	Siemens	P.	4.5V
TAA141	Siemens	P.	3V
TAA151	Siemens	P.	7V
TAA1515	Siemens	P.	12V
TAA263	Philips	P.	6V
TAA293	Philips	P.	6V
TAA300	Philips	A.	1W
TAA310	Philips	P.	7V
TAA320	Philips	P.	m.o.s.t.
TAA370	Philips	P.	1.3V
TAA420	Siemens	P.	7.5V
TAA435	Philips	D.	14V
TAA480	Philips	P.	7V
TH9013P	Toshiba	A.	20W
$\mu$ A716	Fairchild	P.	21V
$\mu$ A745	Fairchild	P.	6.3V

P—pre-amplifier; A—power amplifier;

D—driver amplifier.

\* X followed by a number indicates the number of amplifiers contained in a single package.

form of the OM200, the same circuit is available for use on the 1.3 to 1.5V supply for hearing aids.

The TAA310 of Fig. 1(c) illustrates a more complex four-stage monolithic audio pre-amp.  $Tr_1$ ,  $Tr_2$  form a d.c.-coupled input feedback pair;  $Tr_3$ ,  $Tr_4$  a long-tailed pair with the signal fed into  $Tr_3$  and the feedback into  $Tr_4$  via the 100k $\Omega$  and 150k $\Omega$  resistors for d.c. and via the 0.027 and 25 $\mu$ F capacitors from the 4.7k $\Omega$  and 270 $\Omega$  resistors for a.c. The four diodes at the input of  $Tr_5$  carry out the level shifting which is necessary to set the output at half rail voltage. The TAA310 can be used in many practical circuits by the addition of suitable external components. In Fig. 1(c) it is shown with a compensation network for a high-gain tape-replay pre-amplifier.

\*Newmarket Transistors Ltd.

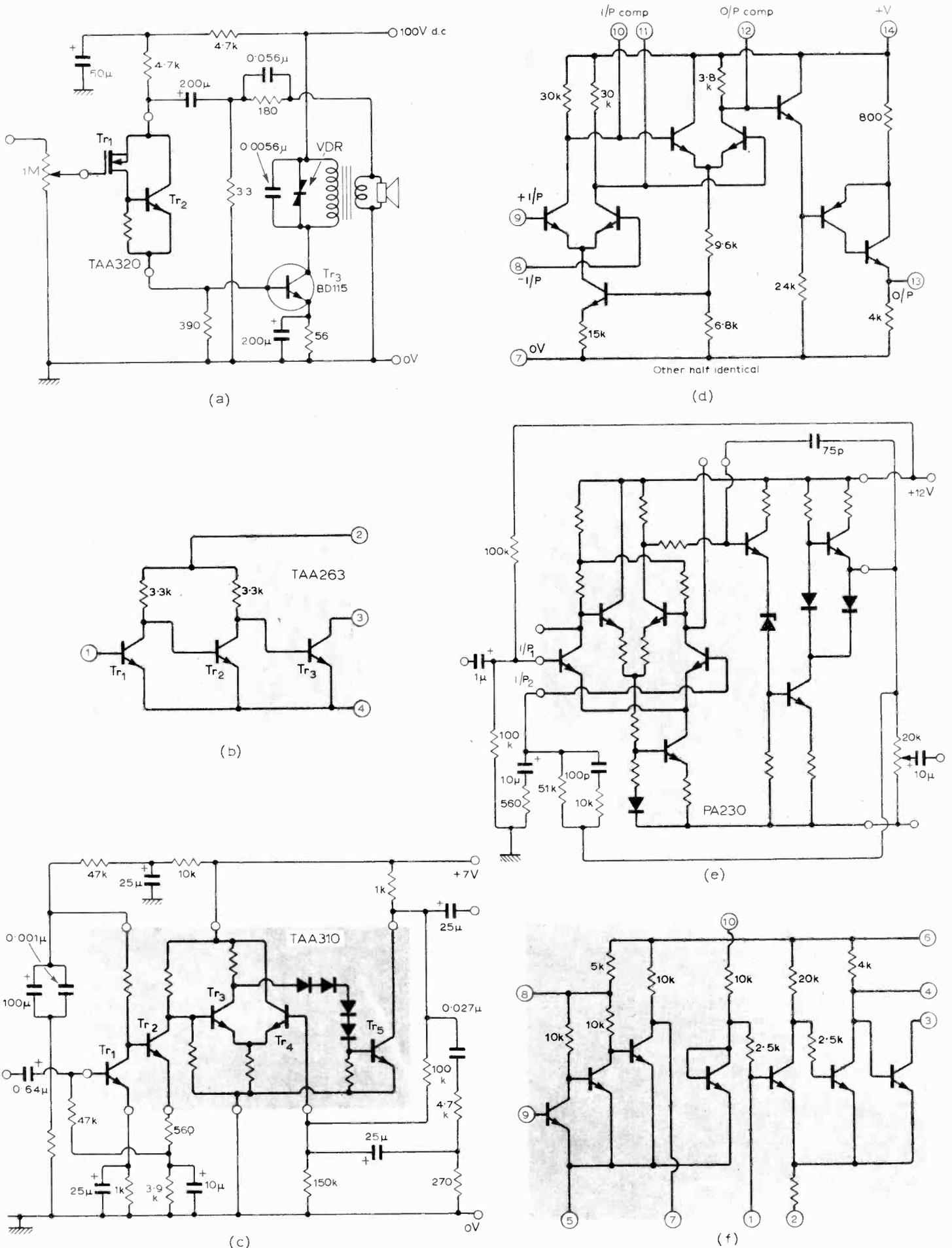


Fig. 1. Typical commercial a.f. low-level amplifier monolithic microcircuits: (a) TAA 320 two-stage m.o.s.f.e.t. input pre-amplifier in 2W crystal pickup record player; (b) TAA 263 three-stage general purpose 7V pre-amplifier; (c) TAA 310 four-stage high-gain pre-amplifier in tape playback system; (d) MC 1303P five-stage dual pre-amplifier; (e) PA 230 four-stage low-level amplifier in 'flat' pre-amplifier; (f) TAA 370 five-stage high-gain pre-amplifier.

Five stages of amplification are to be found in the MC1303P whose internal circuit is shown in Fig. 1(d). The package contains two identical amplifiers as shown. If you have followed the earlier articles in this series, you will recognize that it is very much a derivative of the 'standard' monolithic op-amp. which comprises a series of d.c.-coupled long-tail pairs with some form of d.c. level shifting to set up the output at mid-rail voltage. In use, the input signal is applied to the '+' input and suitable d.c. and a.c. feedback networks inserted between the output and the '-' input. The MC1303 has been widely used to provide front end pre-amplifiers for stereo audio systems, with different equalizing feedback networks switched in for tape replay, magnetic pickup, ceramic pickup, microphone, etc. The dual amplifier comes in a fourteen-lead dual-in-line package.

One example of a monolithic low-level amplifier that has been widely used is the PA230 shown in a typical overall circuit arrangement in Fig. 1(e). The internal circuit of the monolith (inside the shaded area) can be seen to be a conventional op-amp. with balanced input stages followed by level shifting to a single-ended push-pull output. The pair of 100kΩ resistors across one input hold the output at half rail voltage, and the d.c. feedback from the output to the

other input via the 51kΩ resistor clamps the output at virtually the same voltage. The overall gain is set by the ratio of the 51kΩ resistor to the 510Ω resistor connected via a 10μF to earth across the second input. The 10kΩ resistor and 100pF capacitor in series across the feedback resistor cuts the high-frequency response, while the 75pF capacitor from the output at the top of the diagram is designed to prevent h.f. oscillation.

As a last example of monolithic low-level a.f. amplifiers, Fig. 1(f) shows the circuit of the TAA370, a six (2 × 3) stage arrangement for very high-gain hearing aid requirements. Various terminals are brought out that give flexibility of circuit arrangements. Normally the microphone is connected to (9) with the usual feedback from (7). Terminal (8) is decoupled with a 2.2 to 10μF capacitor. The output from (7) is fed via a volume control of about 25kΩ to (1) through suitable 1μF isolating capacitors. An adjustable resistance from the positive 1.3V supply at (6) to terminal (10) enables the setting up of the output d.c. level. Terminals (5) and (2) are connected to the negative supply. The earpiece is connected from terminal (3) to (6). The whole amplifier comes in a TO-89, 10-lead flat pack. Although primarily intended for hearing aid use it is versatile and has been

widely used for other types of audio circuits within the limits of its 5V supply rating.

**Hybrid low level**

A glance at the circuits in Fig. 1 will show you that to make practical a.f. systems with monolithic i.c.s you still have to use many discrete external components, particularly capacitors. The latest progress towards doing away with external components and providing complete systems in microcircuit form has been in the field of hybrid (particularly thick film hybrid) circuits. The Japanese seem to be out ahead in this field and are providing a range of hybrids which are complete functions in themselves. They avoid the limitations of the monolithic technology by mounting subminiature capacitors, etc. inside the package.

Fig. 2 gives three examples of these thick film hybrid audio low-level amplifiers to show how the number of external components is drastically reduced.

Fig. 2(a) shows the Marconi D2009 two-stage amplifier connected in an arrangement to give 62.5dB voltage gain flat from 30Hz to 20kHz with a 100kΩ input resistance. By varying the feedback network compensation can be obtained for tape replay, record play, etc.

In Fig. 2(b) there is an interesting microcircuit, the D2011, which is a single-stage tone-control amplifier. In this integration has advanced to the level where only two potentiometers and one capacitor are needed externally to give a complete treble boost/cut and bass boost/cut unit, with input and output d.c. isolation and with a high input impedance secured by bootstrapping.

Complete three-stage amplifiers are also available in thick film hybrid, as for example the D2100 equalizer shown set up for a magnetic pickup in Fig. 2(c).

In all the hybrids of Fig. 2, there are still a few external components, but the technology is such that ultimately we should find available completely self-contained a.f. amplifiers which have just to be wired in between input and output and connected between the positive and negative supply rails.

**Medium-level monolithic**

Above about 50mW power levels in an amplifier chain, the signal line impedances begin to fall rapidly (and capacitor values correspondingly begin to climb). The very small size of the silicon chip in monolithic amplifiers limits the power that can be handled without special heat sinking arrangements.

Quite a number of manufacturers have produced linear monolithic a.f. amplifiers capable of handling up to 500mW of power, and a selection of these is given in Fig. 3 to show the circuitry adopted.

Fig. 3(a) shows the well-known RCA 500mW amplifier, CA3020. The general lines of the circuit are an emitter follower,  $Tr_1$  capable of feeding a long-tailed phase splitter driver pair,  $Tr_2, Tr_3$ , followed by emitter followers,  $Tr_4, Tr_5$ , feeding into isolated output transistors  $Tr_6, Tr_7$ . The

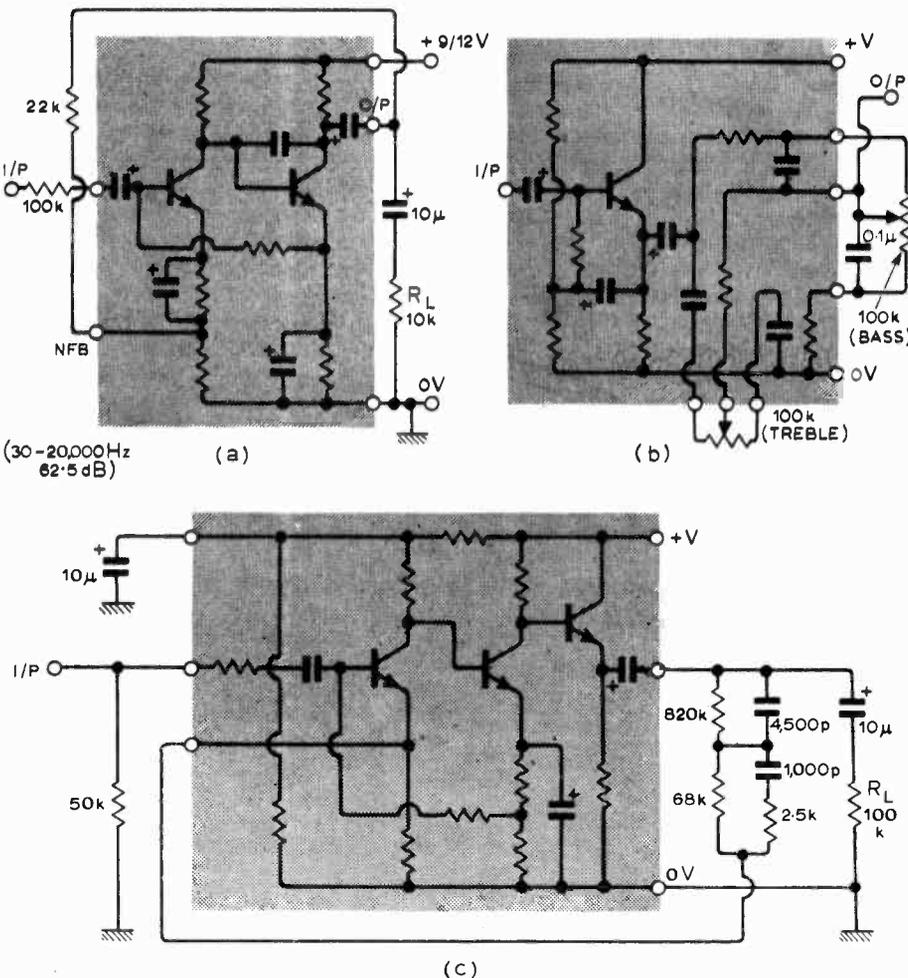


Fig. 2. Typical low-level amplifier circuit configurations now commercially available in hybrid microcircuit form and requiring minimal external components to

give practical amplifier systems: (a) 'flat' pre-amplifier; (b) tone control pre-amplifier; (c) equalizer pre-amplifier for a magnetic pickup.

multiple terminals and isolated input and output devices offer many circuit arrangement options.

Fig. 2(b) is the circuit of the Motorola MFC4000P, 9V, 250mW amplifier. This can be seen to be more complex than the CA3020 and does not follow conventional op-amp circuitry. It uses 14 transistors and 5 diodes, which may seem lavishly extravagant to the circuit man used to economizing on discrete semiconductors, until he remembers that many active semiconductor devices are produced at the one time on the silicon chip. Fourteen transistors in the monolith might not be more than twice as costly as producing one conventional transistor.

While the internal circuitry of these mid-level monoliths might be of interest to an advanced circuit man, the ordinary user is not really much involved. He usually only wants to know what discrete components he should connect round the monolith to get the results he wants. Fig. 3(c) gives such information for the TAA435, a 14V 250mW driver stage for a higher power amplifier. The external circuitry is shown to give 4W output from an AD161/162 complementary germanium transistor pair on a 14V supply rail, with a 15mV input to give full output.

Oddly, in this area, where you would expect hybrid microcircuits to start taking over from monoliths, there is still a dearth of commercial hybrid products. However, thick film technology is such that it seems very likely that commercial hybrids will begin to emerge as they have done in the lower level applications.

**Monolithic power**

Despite the difficulty of getting rid of the heat from monolithic chips, the technology has been pushed at present to the point where up to 5W audio output can be handled. Fig. 4 shows two well known examples, the MC1554 and the PA246.

From the internal circuitry of the MC1554, shown in Fig. 4(a), you can see that this is basically a long-tailed pair  $Tr_1, Tr_2$ , followed by an emitter follower,  $Tr_3$ , feeding into a buffer emitter follower,  $Tr_4$ , connected to an output transistor,  $Tr_5$ . The whole microcircuit is packaged in a ten-lead TO-5 can. In the circuit, the 39pF capacitor  $C_1$  is a compensation capacitor to prevent instability; the network  $R_1, C_2$  across the d.c. supply rail removes high-frequency spikes and the 10Ω resistor and the 0.1μF capacitor series network  $R_2, C_3$  across the output is a 'Zobel' network to prevent high-frequency oscillation when a partially inductive loudspeaker load is used.

The GE (U.S.A.) PA246 shown in Fig. 4(b) in a 5W amplifier set-up is another very well known monolithic power amplifier. The internal circuitry will be seen to

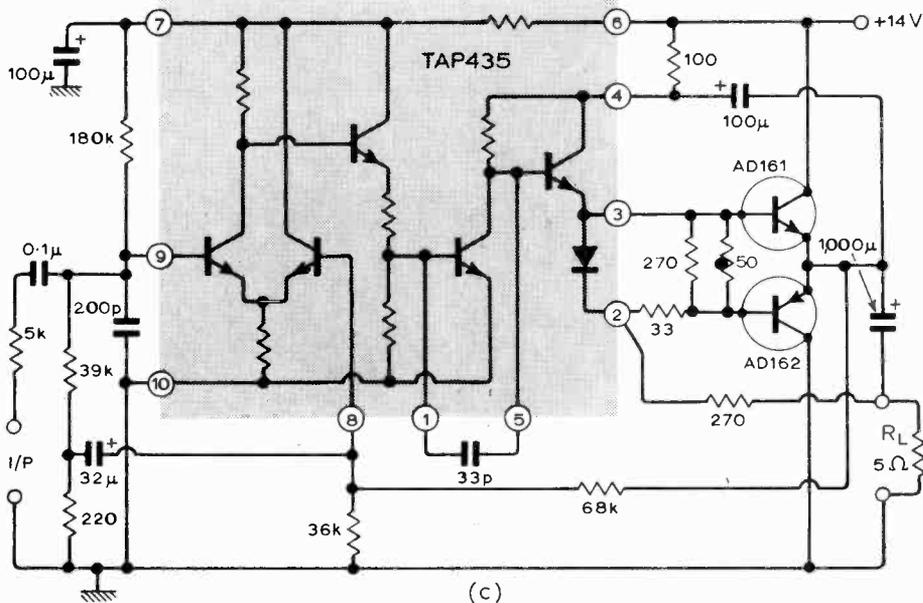
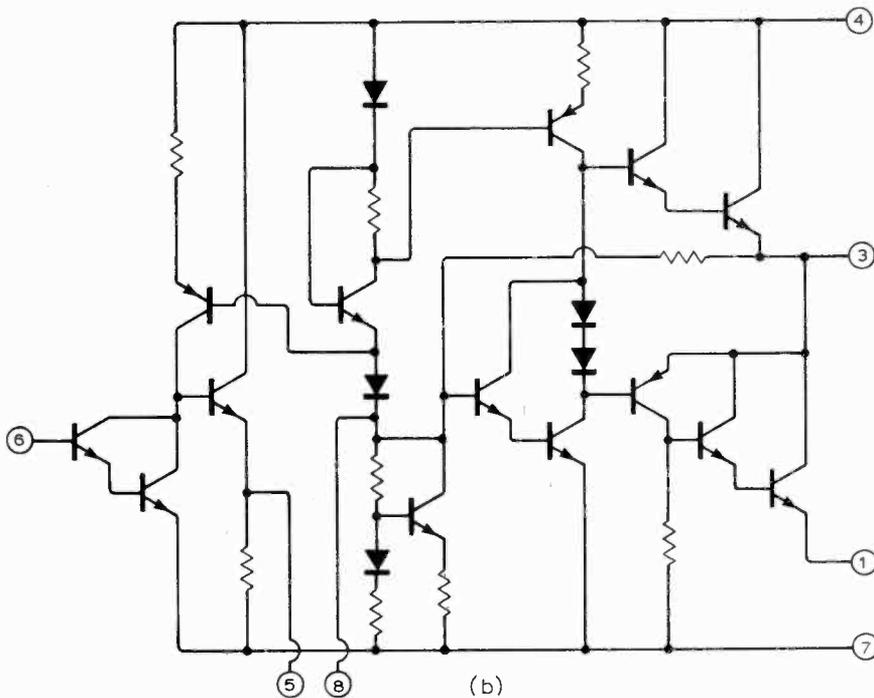
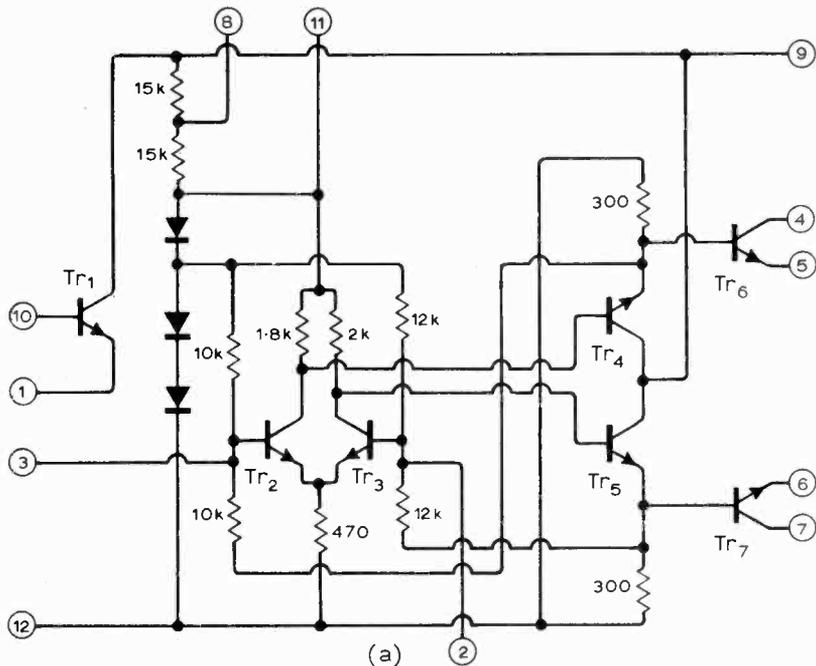
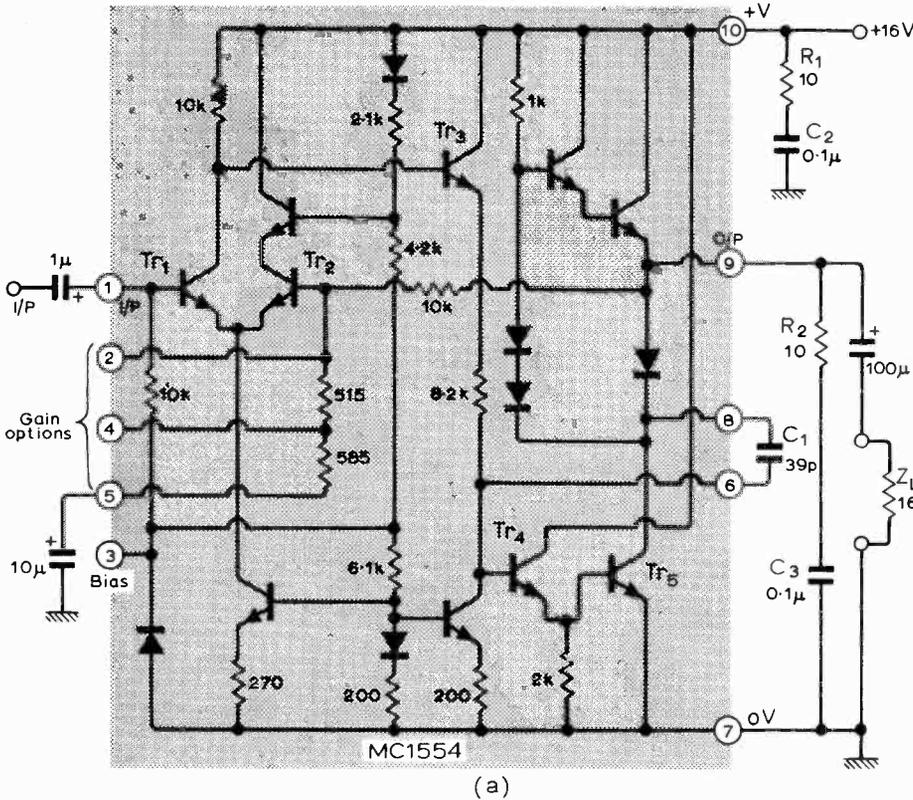


Fig.3. Typical off-the-shelf a.f. mid-level monolithic amplifier microcircuits: (a) CA3020, 9V, 500mW; (b) MFC4000P, 9V, 250mW; (c) TAA435, 14V, 250mW driver stage connected in a 15mV for 4W amplifier.



be simpler than the MC1554 (certainly more easy for the less experienced circuit man to work out). Here  $Tr_1, Tr_2$  make a long-tailed pair input stage, with  $Tr_2$  feeding a p-n-p compound transistor  $Tr_3, Tr_4, Tr_5$  as the lower; an n-p-n compound  $Tr_6, Tr_7$  as the upper of an output complementary pair driving the 15Ω load through a 500µF capacitor. The d.c. setting up of the amplifier is done with the potentiometer  $R_4$  in combination with the d.c. feedback from the output through  $R_1, R_2$  into the base of  $Tr_2$ . The a.c. feedback is set by the ratio of  $R_1$  to  $R_3$ .

**High-power hybrid**

In the power amplifier field, most of the commercial units so far have been monolithic. Thick-film hybrids do not yet feature widely in this area. However, when you get above about 5W (r.m.s.) output power, the hybrid appears up till now to be the only viable integrated circuit.

Thick-film hybrids capable of handling up to 100W of audio power have been developed. Technologies that have had to be developed for producing these include as many as nine separate screen printings, extensive use of crossover dielectric glazes, adequate thermally conductive adhesive bonds of the ceramic substrates to heat sinks, and plastic encapsulations that can withstand heavy thermal stresses. A particularly difficult problem has been the mounting of the output transistor chips to provide adequately low thermal resistance to the heat sink, and adequate thermal capacity to prevent excessive short term rise in their junction temperature.

One commercially available hybrid high-power amplifier that can be taken as typical of the breed is the Toshiba TH9013P which in the circuit arrangement of Fig. 5 gives 20W output into an 8Ω speaker on a 45V d.c. rail voltage.

The internal circuitry of the TH9013P would make conventional circuit men heave a sigh of relief as it follows standard discrete component practice. The hybrid consists of a long-tail input pair which feeds a driver stage which in turn drives a double complementary pair output stage. In fact the circuit could be just another of the discrete component audio amplifier variants that has appeared in the literature over the last ten years. A glance at Fig 5 shows that the number of external components required has been reduced to six including the loudspeaker and the fuse!

When using audio amplifier microcircuits one must not forget that many of them still have gain in the r.f. region so the user should position additional components and wiring accordingly. This point has been stressed many times in this series and cannot be overstated. Before using any of the microcircuits obtain a data sheet, most component distributors will supply you with one, and use it. If you are using a microcircuit for the first time what will you learn if you merely copy someone else's arrangement?

(To be continued)

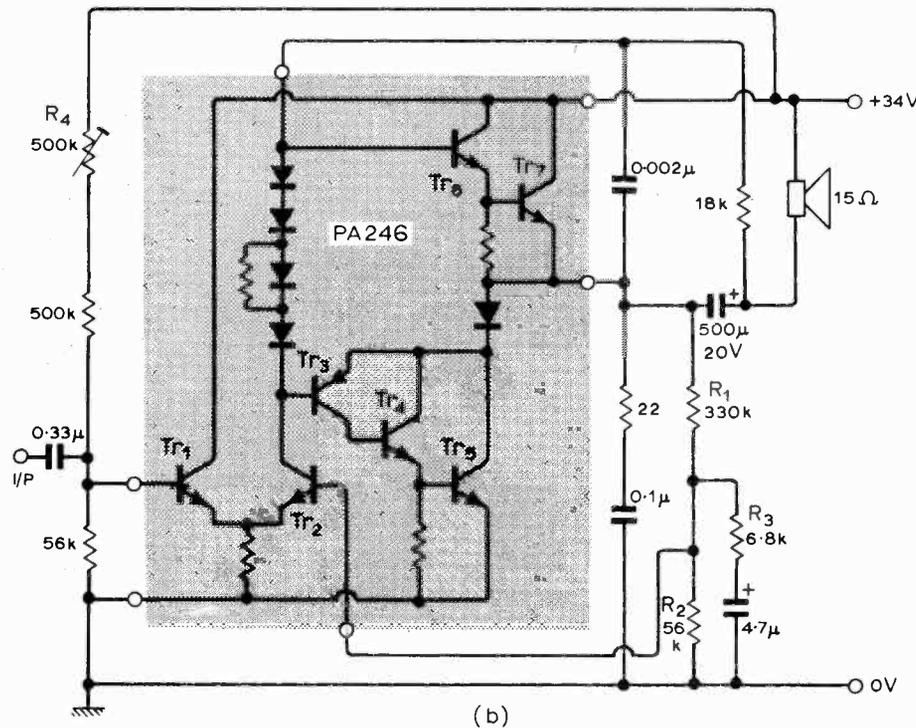


Fig. 4. Typical monolithic a.f. power amplifier microcircuits: (a) MC1554, 1.8W/16V/15Ω in a circuit with 20dB voltage gain, 10kΩ input resistance, 100Hz to 20kHz; (b) PA246, 5W/34V/15Ω arrangement.

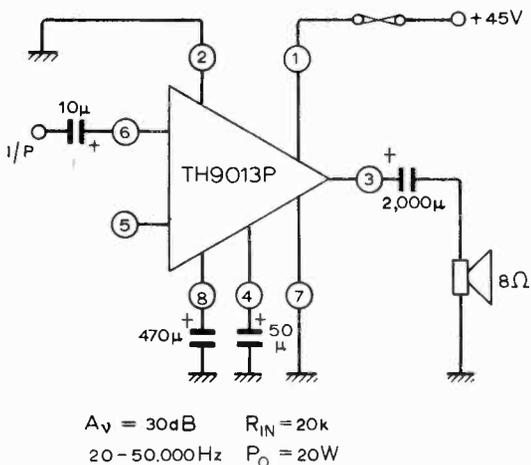


Fig. 5. Example of hybrid microcircuit a.f. high-power amplifier, Toshiba TH9013P, 20W/45V/8Ω; (a) internal circuitry; (b) typical practical circuit arrangement.

$A_v = 30dB$   $R_{IN} = 20k$   
 $20 - 50,000Hz$   $P_O = 20W$

# Electronic Voltmeter for 2 to 50kV

## An instrument which employs a triode valve as well as semiconductors to achieve a 10MΩ/V sensitivity

by A. M. Albisser\* and N. F. Moody†

We were recently faced with the need to employ a 40 kV image intensifier but found that our laboratory had no suitable voltmeter for setting the various electrode voltages. The resistance chains which supply these interelectrode voltages often have values as high as 1000 MΩ, and the load which the voltmeter may impose must be small indeed.

The voltmeter here described covers the range ±2-50 kV d.c. and also measures the peak value of an a.c. waveform to the same scale. The instrument is linear to 1% and contains internal calibrating facilities. The load imposed by the voltmeter is in the form of a constant current, normally set to 0.1 μA, so that a full scale reading the 'movement sensitivity' is effectively 10<sup>7</sup> Ω/V. Means are provided for choosing an alternative 1 μA loading factor and, as will be shown, thereby correction can be made for the small meter loading upon the measured circuit. This inexpensive instrument is mains operated, hermetically sealed and drossicated, more robust and with a wider scale range than an electrostatic voltmeter.

### Principle

The design of the voltmeter is based upon the use of a thermionic triode in an 'inverted' # form, in which the anode voltage is made the independent variable and the grid voltage the dependent variable. Thus, in Fig. 1, if the voltage to be measured,  $E_{ac}$ , is applied between anode and cathode, the grid bias  $E_{gc}$  needed to set a given anode current  $I_b$  is a measure of  $E_{ac}$ . By choice of a suitable valve,  $E_{gc}$  may well be as little as (1/2000)  $E_{ac}$  and so is easily and safely measured. In the instrument to be described, a variant of this principle is employed; furthermore,  $E_{gc}$  is made to set itself automatically and thereby drive the voltmeter movement. These matters will be best understood a little later: to begin with it may prove helpful to review that part of thermionic triode theory which is to be exploited.

Consider a valve operating within the region described by the extension of Langmuir-Child's law,

$$I_b = K(E_{ac} + \mu E_{gc})^{\frac{3}{2}} \quad (1)$$

in which,

$I_b$  is the anode current in amperes,

$K$  is the permeance of the triode, a constant that depends on the size and shape of the three electrodes,

$E_{ac}$  is the anode to cathode potential in volts,

$\mu$  is the dimensionless amplification factor, a constant determined mainly by the anode, grid, cathode geometry and,

$E_{gc}$  is the grid to cathode potential in volts (including contact potential).

We may rearrange equation (1) to give

$$E_{ac} = \left(\frac{I_b}{K}\right)^{\frac{2}{3}} - \mu E_{gc} \quad (2)$$

This equation, with parameter  $(I_b/K)^{\frac{2}{3}}$ , represents a family of straight lines with slope  $-\mu$  and intercept  $(I_b/K)^{\frac{2}{3}}$ . In other words, a linear relationship, the constant current voltage transfer characteristics of the triode, holds between  $E_{ac}$  and  $E_{gc}$  when  $I_b$  is held constant. Two of these characteristic curves of the high voltage beam triode used, the 6 BK4A,† are sketched in Fig. 2.

### Caution!

Above a potential of 16 kV, X-rays are emitted from the anode of the triode. Although some attenuation occurs in the glass envelope, care should be exercised when operating the voltmeter.

Since an ideal voltmeter measures potential without drawing any current, we may employ equation (2) as a basis upon which to design a voltmeter whose deviation from this ideal simply depends on the magnitude of the anode current  $I_b$ . By defining this current, we ensure the linearity of the instrument, according to equation (2); and by reducing the magnitude of this defined current  $I_b$ , we approach the properties of the ideal voltmeter.

With  $I_b$  held constant,  $E_{gc}$  is precisely related to the voltage to be measured,  $E_{ac}$ , by the parameter  $\mu$ . Since  $\mu$ , itself, is domi-

†This valve is of the type used as an e.h.t. voltage regulator in colour TV receivers.

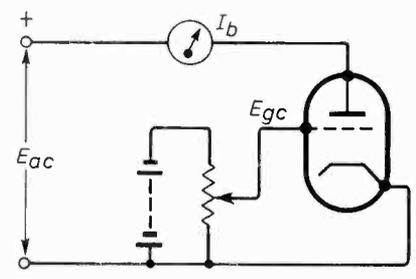


Fig. 1. Basic circuit diagram showing the principle of the voltmeter.

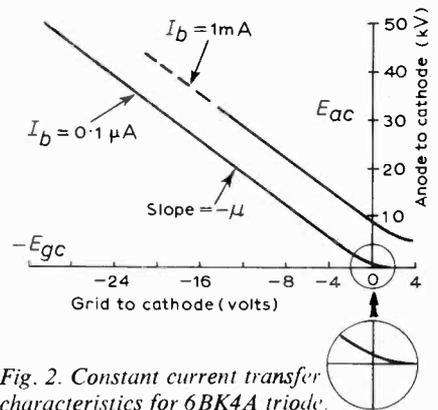


Fig. 2. Constant current transfer characteristics for 6BK4A triode.

nantly controlled by electrode geometry it should remain sensibly constant throughout the life of the valve. The voltage  $E_{ac}$  does include contact potential, whose variation could introduce a source of error. However, the heater supply is stabilized (as will be seen) and a zero control is provided to compensate for drifts due to valve ageing.

### General outline

Block diagram of the valve voltmeter is given in Fig. 3. It illustrates both the operational blocks and the two-compartment aspects of the mechanical design. Outside the voltmeter the mains is converted to a d.c. voltage to supply for a 50 kHz oscillator. The peak amplitude of this oscillator voltage is regulated, and remains constant despite changes of the mains voltage. An isolation transformer, designed to withstand a d.c. stress of more than 50 kV between primary and secondary windings, couples a.c. power from the oscillator into the second compartment of the voltmeter. It provides both filament power for the triode and bias for the automatic balance

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#The term "inverted" has been applied elsewhere to a triode with a negative anode voltage thereby controlling grid current. This mode is not used here, though it was tried unsuccessfully.

circuits. As a result of this isolation, either the negative or the positive terminal of the voltmeter may be grounded and voltages of either polarity can be measured.

In the first compartment, the operation of the automatic balance circuits is as follows: For any given voltage applied to the anode of the triode, the constant-current sink draws a fixed current of either 1 or 0.1  $\mu\text{A}$  (selected by a switch), and the resulting cathode-to-grid voltage is transferred, via the voltage sensing amplifier, to a differential voltmeter. Here, this voltage is displayed on a meter calibrated to read 50 kV full scale.

The second compartment contains only the triode, the element across which all the voltage stress is exerted during a measurement. For convenience, the triode is operated in the earthed grid configuration; we can say that its cathode-to-grid potential regulates the cathode current. Now, when an anode potential is applied and the resulting cathode-to-grid potential is a few volts positive, the portion of the anode current intercepted by the grid is negligible. Thus, the anode current is the same as the cathode current in the operating range of the triode.

In this configuration, equation (2) becomes

$$E_{ag} = (I_b/K)^{\frac{1}{\mu}} + (\mu + 1)E_{cg} \quad (3)$$

This equation, as before, represents a family of straight lines with slope  $(\mu + 1)$  and the same intercept as in equation (2). The details of the circuit, which automatically generates the corresponding  $E_{cg}$  for any  $E_{ag}$  over the operating range, is described below.

**Automatic balance circuit**

The circuit diagram sketched in Fig. 4 shows the automatic balance circuit. To measure the unknown potential difference  $E_{ag}$ , applied across the anode and grid electrodes of the triode, the cathode-to-grid potential  $E_{cg}$  must be sensed when the cathode current is held at the desired value of (say) 0.1  $\mu\text{A}$ . A transistor  $Tr_1$ , in the common base configuration, draws this constant current, and the voltage on its collector,  $E_{cg}$ , is sensed by

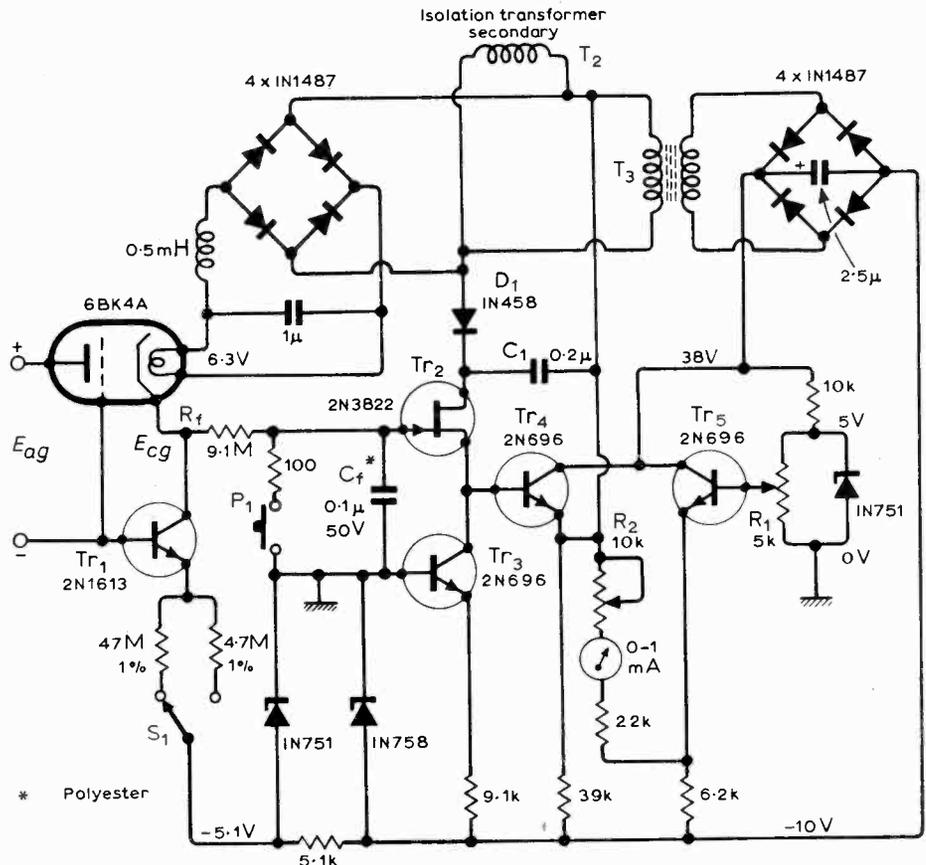


Fig. 4. Diagram of the automatic balance circuit.

a differential voltmeter  $Tr_4$ ,  $Tr_5$ , using an f.e.t. source follower,  $Tr_2$ , to present a high input impedance to the triode cathode. The reading is indicated on a 1mA f.s.d. meter. Thus, if the source follower and differential voltmeter are linear, the millimeter reading is related to  $E_{ag}$ , according to equation (3). A zero adjusting potentiometer  $R_1$ , used in conjunction with the bush-button  $P_1$  at the gate of the f.e.t., permits balancing for a zero reading on the millimeter. This adjustment does not completely balance out the effects of the intercept term of equation (3). However, for small anode currents of 10  $\mu\text{A}$  or less, and for anode potentials of above 2 kV, the difference is negligible, as

illustrated by the linearity of the curve in Fig. 2.

The f.e.t.  $Tr_2$  is operated at both constant source current (by use of  $Tr_3$ ), and constant drain-to-source voltage by the boot-strap consisting of diode  $D_1$  and filter capacitor  $C_1$ . In this configuration, the small leakage current of the gate-to-channel junction is not altered by changes in the gate voltage. Thus, the f.e.t. source-follower imposes a small, but constant, loading on the cathode current of the triode.

To prevent changes in the leakage current between the filament and cathode of the triode at different cathode-to-grid voltages, the filament power supply is also boot-straped to the cathode via both the source follower and the emitter follower actions of  $Tr_3$  and  $Tr_4$ , respectively.

A low-pass filter  $R_f C_f$  isolates the gate of the f.e.t. from the cathode of the triode, thereby assuring that accidental current surges do not damage the junction f.e.t. The resistor  $R_f$  also serves to protect the triode from drawing excess anode current should the zero button be accidentally pushed when high voltages are impressed across the tube; while the capacitor  $C_f$  also provides the additional function of making the voltmeter a peak-reading instrument when the measured voltage is a.c.

Initial calibration of the instrument is performed by adjusting the 'full scale calibrate' potentiometer,  $R_2$ , so that full-scale meter deflection corresponds to 50 kV. However, because the instrument is linear, this calibration voltage need not be 50 kV: any convenient d.c. or peak a.c. voltage within the range of the instrument is adequate. Thereafter, recalibration should not be necessary.

It has been seen that the voltmeter draws

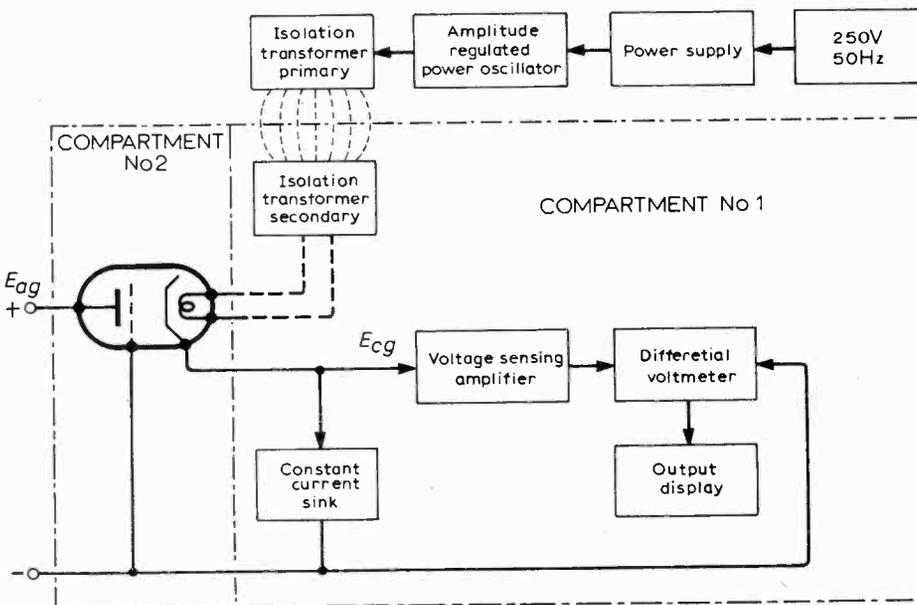


Fig. 3. Block diagram of the valve voltmeter, showing the two internal compartments.

a normal current of  $0.1 \mu\text{A}$  from the source where voltage is being measured. By setting  $S_1$  to the other position, the loading is increased to  $1 \mu\text{A}$ . Thereby the voltage drop due to a source impedance may be determined, for any voltage change  $\Delta V$  due to the increased current is simply divided by 9 and added to the reading taken at  $0.1 \mu\text{A}$ . Evidently the source impedance is also given as

$$R_{\text{source}} = 0.9 \Delta V \text{ M}\Omega$$

Accuracy of the voltmeter depends principally on three factors; the  $\mu$  of the triode, the  $\alpha$  of the transistor in the constant current circuit, and the linearity of the differential voltmeter. For the triode, the amplification factor at constant current, is determined dominantly by the geometry of the electrodes and is affected only slightly by ageing and deterioration. The constancy of the cathode current depends on the  $\alpha$  of the transistor in the current sink, also relatively constant. To ensure the linearity of the source follower, it is operated at constant bias, as mentioned above. Finally, the differential voltmeter proportionally converts, by emitter follower action, the voltage at its input to a corresponding current registering on the milliammeter. Thus the voltmeter is inherently accurate.

In practice, the stability is found to be excellent and the relative precision is within  $\pm 1\%$  of full scale.

**Power oscillator**

The diagram in Fig. 5 shows the circuit of the power oscillator. Briefly, a Colpitts oscillator,  $Tr_6$ , operating at 50 kHz excites a self-biasing driver stage,  $Tr_8$ , via an emitter-follower transistor,  $Tr_7$ , inserted for isolation. The phase-splitting transformer in the collector circuit of  $Tr_7$  couples power to a class-B biased push-pull amplifier,  $Tr_9, Tr_{10}$ . In order to regulate the peak

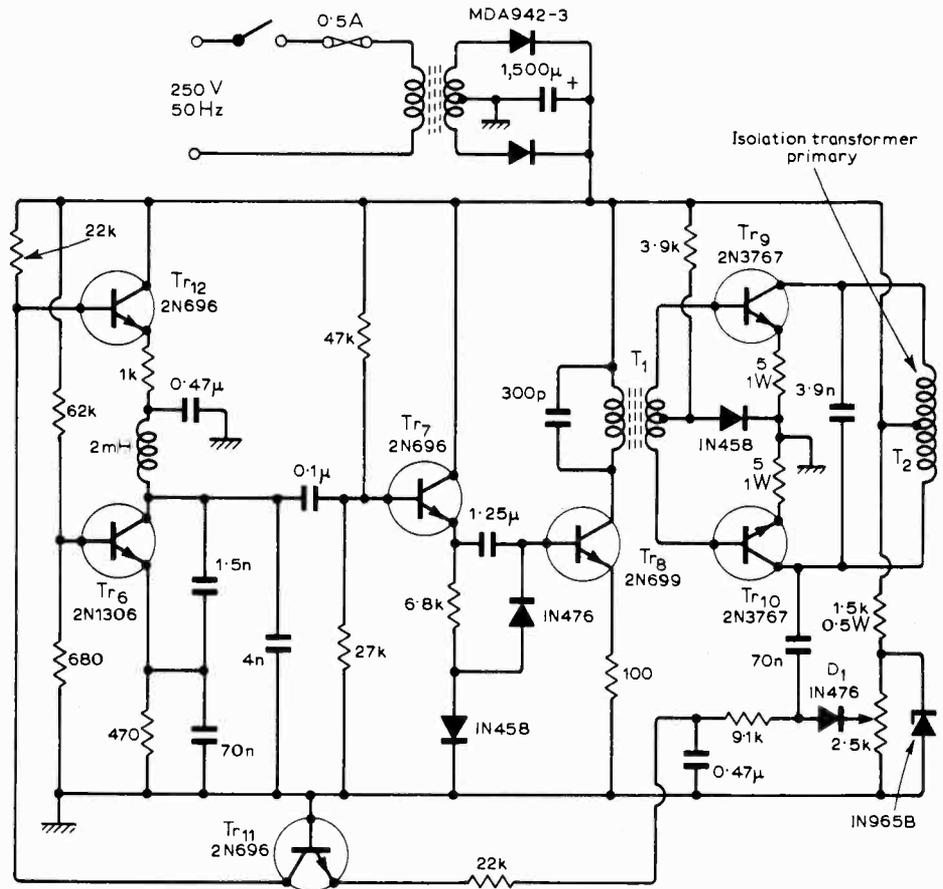


Fig. 5. Circuit diagram of the power oscillator. The 70nF capacitor is  $C_1$ .

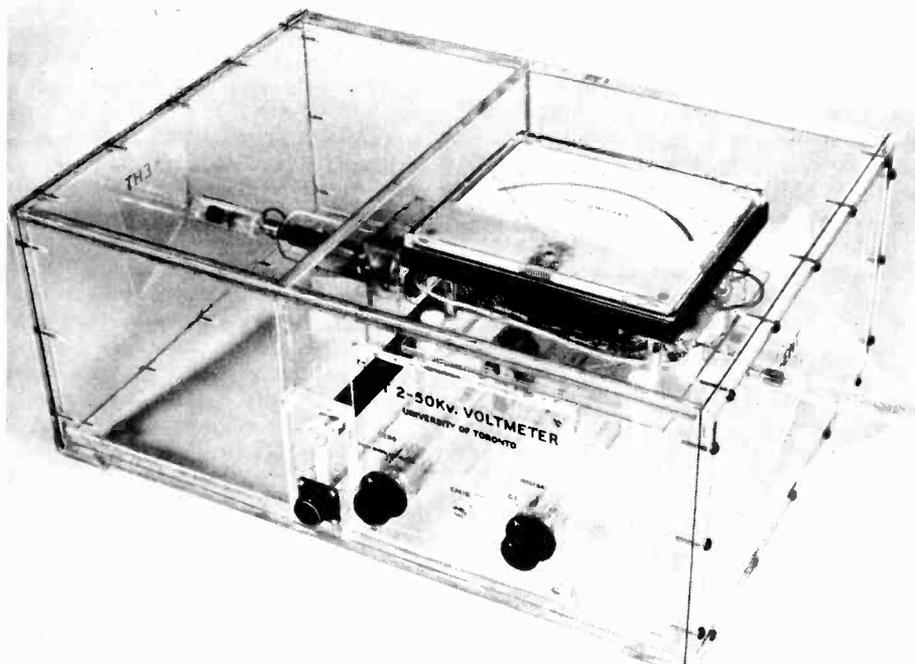
amplitude of the oscillating voltage impressed on the primary of the special isolating transformer, a capacitor and diode circuit,  $C_1, D_1$ , clamps the positive peaks of the a.c. voltage to a reference level. The mean value of this clamped signal biases a common-base and a common-collector transistor,  $Tr_{11}, Tr_{12}$ , in such a way that increases in the peak-to-peak amplitude of the oscillating voltage impressed across the isolating transformer results in lowering the collector voltage of the Colpitts oscil-

lator,  $Tr_6$ . In this way, negative d.c. feedback ensures that the amplitude of the a.c. voltage remains fixed in spite of changes in the components and variations in the d.c. power supply voltage.

**Isolating transformer**

The transformer used to couple both filament power to the valve and bias power to the automatic balance circuit is made as follows: its primary winding consists of two overlapping layers of 36 s.w.g. enamelled copper wire (33 a.w.g.)§, symmetrically wound about a four-inch length of  $\frac{3}{8}$  in diameter ferrite rod. While the inner layer contains 100 turns to the centre tap: the outer has 108 turns to provide a balanced primary inductance of 2.64 mH with a  $Q$  of 7.3 at 1 kHz. The secondary winding simply consists of one layer: 60 turns of 27 s.w.g. enamelled copper wire (26 a.w.g.), symmetrically wound about the outside diameter of a  $1\frac{1}{2}$  in length of Lucite pipe (transparent Acrylic plastic) with  $\frac{1}{2}$  in internal diameter and  $\frac{3}{4}$  in outside diameter. When the primary winding on the ferrite rod is properly placed at the centre of the Lucite pipe, the inductance of the secondary winding is 0.23 mH with a  $Q$  of 2.5 measured at 1 kHz. The breakdown strength of the  $\frac{1}{8}$  in wall of the Lucite pipe is roughly 55 kV. To further enhance this breakdown strength between the windings of the transformer, the primary winding is first centrally located about the axis of the Lucite pipe,

§In the manuscript the author's used the American standard B & S or a.w.g. gauges. We have converted to the nearest s.w.g. figure putting the specified American standard gauge in brackets. Ed.



Note the prototype's twin compartment construction.

then the tubular space formed between the outer diameter of the primary winding and the inner diameter of the Lucite pipe is filled with Sylgard 185 potting and encapsulating resin (Dow Corning) with a breakdown stress of 550 V per mil. This encapsulating procedure also ensures that the geometry of the transformer remains fixed.

**High voltage compartment**

The thermionic triode is the circuit element across which is placed all the potential stress during a measurement. If the loading effect of the voltmeter is to be defined as either 0.1 or 1  $\mu$ A, then it is mandatory that this flow of charge, defined by the current-sink transistor, pass wholly through the active volume of the triode. Otherwise, erratic readings would be registered, for the cathode-to-grid potential would be incapable of controlling all the components of current appearing at the cathode. To minimize this source of error, which results mainly from surface leakage currents, the following procedure is followed. Before enclosure in the high-voltage compartment, the triode is carefully washed with water and a degreasing detergent, and rinsed thoroughly with distilled water. Then, taking care to avoid placing finger marks or other dirt on the glass envelope, the tube is thoroughly rinsed with pure methanol. After it is dry, a layer of Dri-film (General Electric U.S.A.) is sprayed on the glass in order to reduce even further the surface-creepage of charge. A similar procedure is employed to clean the two compartments of the voltmeter.

**Mechanical construction**

Briefly, the side panels of the box are cut from a  $\frac{1}{2}$  in Lucite plastic sheet. Offsets are milled along their edges and Tensol 'A' (Imperial Chemical Industries), is used to cement the offset joints so formed. These joints provide 50% more surface area for gluing than a simple butt joint, and correspondingly lengthen the leakage path between the inside and outside of the voltmeter box. The overall dimensions of the box are 19.75 x 14 x 8 inches, to which must be added the dimensions of the mains driven power supply and the power oscillator.

To allow access to the electronic components in the two compartments, the ends of the box (through which the negative and positive terminals pass) are attached with nylon screws. At all locations where electrical or mechanical paths communicate between the inside and outside of the box, a minimum path of 6 in of Lucite plastic assures isolation and a sufficiently long path to prevent the creepage of charge along the surfaces of the intervening plastic.

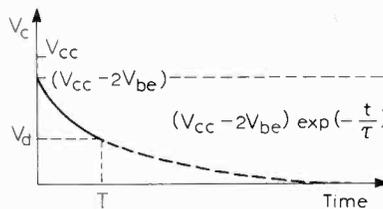
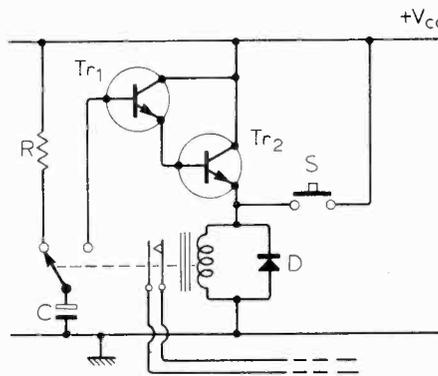
**Transformer details**

Phase-splitting transformer  $T_1$ : Vinkor type LA2316 with a 204-turn primary of 38 s.w.g. (34 a.w.g.) and a 14.5-turn secondary of 22 s.w.g. (21 a.w.g.) centre tapped.  
 Isolating transformer  $T_2$ : see text.  
 Step-up transformer  $T_3$ : Vinkor type LA2216 with a 62-turn primary of 27 s.w.g. (26 a.w.g.) and a 260-turn secondary of 38 s.w.g. (34 a.w.g.).

# Circuit Ideas

**Long-period relay monostable**

There are many examples of systems where a function is excited by an input stimulus and requires to be maintained for a predetermined time, e.g., vending machines, automatic door opening mechanisms etc.



Normally  $C$  is charged to  $+V_{cc}$  until switch  $S$  is momentarily closed. This causes the relay to 'pull-in' and  $C$  is connected to the base of the super- $\alpha$  pair,  $Tr_1, Tr_2$ , which form a very high impedance emitter-follower.  $C$  discharges slowly due to base current, and the voltage at the emitter of  $Tr_2$  falls from  $V_{cc}-2V_{be}$  to  $V_d$ , the relay 'drop-out' voltage, at which point the relay

opens and the circuit reverts to its stable state. The time period  $T$  is given by,

$$T = \tau \log_e \frac{V_{cc}-2V_{be}}{V_d}$$

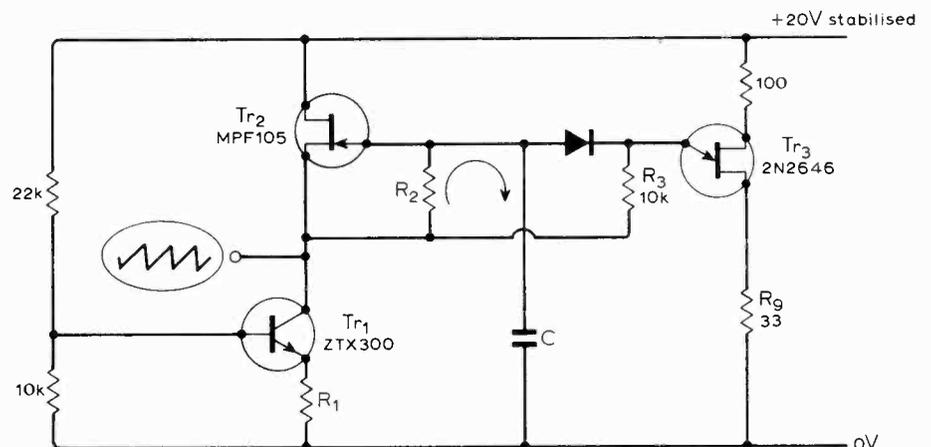
where  $\tau = \beta_1 \beta_2 CR_{relays}$  ( $\beta_1, \beta_2$ , current gains of  $Tr_1, Tr_2$ ). If a high supply voltage is used ( $> 12V$ ) an extra diode should be placed in the emitter lead of  $Tr_2$  to protect against reverse breakdown in the event of  $S$  being closed during a timing period. Time periods of about ten minutes can be obtained with this circuit.

J. F. ROULSTON,  
Edinburgh.

**V.L.F. sawtooth generator**

The circuit shown generates a long-period linear sawtooth at fairly low impedance. The f.e.t. is biased by  $Tr_1$  at its zero temperature coefficient point (calculated from  $I_{dss}$  and  $V_{gs}$ ). By bootstrap action the ramp generated at the gate also appears at the source. The constant current which charges  $C$  is defined by  $V_{gs}$  and  $R_2$ . This current should be sufficiently great to swamp gate leakage current at the working bias point, and variations due to temperature change. The diode is reverse biased by the action of  $R_3$  until the source reaches the trigger point of the unijunction. When the unijunction fires the diode becomes forward biased and the capacitor is discharged.  $R_0$  determines the temperature stability of the firing point. The f.e.t. used required  $R_1$  to be 16k $\Omega$ ;  $R_2$  could be as high as 30M $\Omega$ . With  $C = 4.4\mu F$  (polyester) the period of oscillation was 3 min.

A. J. BARKER,  
Werrington,  
Stoke-on-Trent.



# Letters to the Editor

The Editor does not necessarily endorse opinions expressed by his correspondents

## In praise of C-D ignition

You asked me to let you know my experience with R. M. Marston's C-D ignition unit under cold starting conditions here in Switzerland.

This winter has proved propitious for assessing the effectiveness of the unit, as during the Christmas holidays we experienced at our holiday chalet early morning temperatures in the region of  $-25^{\circ}\text{C}$ . At temperatures down to  $-20^{\circ}\text{C}$  my engine (Citroen DS) started immediately; at lower temperatures I experienced some difficulty due to low cranking speeds, my battery being five years old. When the battery was paralleled with another battery (which had also been exposed to the same low temperatures) I obtained easy starting even at  $-26^{\circ}\text{C}$ .

My unit has now been operating for about six months. I can say that it has been functioning under 'worst conditions' as I installed it under the bonnet above the car heater unit. The only difficulty experienced was the early failure of one of the IN4005 rectifier diodes. I am not sure if this was due to the shorting of the h.t. line or because the rating of these diodes is rather marginal. To be on the safe side I replaced them with BY127s since when the unit has operated correctly.

For me the great attraction of Mr. Marston's unit has been the general improvement in the smooth running of the car, absence of flat spots and no misfiring. I was given to understand that some complaints have been made of misfiring at high engine speeds. On the one occasion when this happened with my car, I withdrew the sparking plugs, which I had deliberately not adjusted when the unit was originally installed and found that the gaps were nearly four times as wide as recommended by the manufacturer!

FRANK GUTTERIDGE,  
Geneva,  
Switzerland.

## "An Equation-solving Aid"

I am sorry that considerations of space led to the deletion of the final paragraph of my paper 'An equation-solving aid' which appeared in the January issue. Perhaps you would kindly allow me some

room to comment a little more fully on the substance of that paragraph.

The procedure outlined in the paper enabled one to determine the value of one of the variables—in the case quoted  $x_3 = -1$ . It may be that one is only interested in this particular variable, but more often than not one would wish to know  $x_1$  and  $x_2$  as well. Referring to the appendix of the article, it will be seen that, after elimination of  $x_1$  and removal of self-loop from  $x_2$ , one is left with the equation

$$x_2 = -\frac{4}{3} - \frac{10}{3}x_3$$

Substitution of  $x_3 = -1$  leads to  $x_2 = 2$ . The initial equations, after removal of the self-loop (no self-loop on  $x_1$  in this case), contained the equation

$$x_1 = 2 + 0.5x_2 + 2x_3$$

Substitution of  $x_3$  and  $x_2$  yields  $x_1 = 1$ . The rule for determining the other variables is thus to note the equations which result after removal of self-loops. These will be in convenient triangular form for substitution.

V. J. PHILLIPS,  
University College of Swansea.

## Sample and hold

I read with interest the article 'Stereo Decoder using Sampling' by D. E. O'N. Waddington in your February issue.

The principle of sampling for a very short duration when  $\sin 2\omega t = +1$  and  $-1$  and the application of a poled network to reduce high-frequency signals in the

output spectrum is indeed interesting.

The price to be paid for sampling with a short duration signal is one of noise. With a sampling interval of 250nsec all noise present at the sample and hold input up to approximately 2MHz will be heterodyned and aliased (i.e. sampling does not occur at at least twice the input signal frequency) into the audio bandwidth. Noise above 2MHz will be aliased into this bandwidth. The amplitude of the individual noise spectra depends, of course, on the harmonic content of the sampling signal. Since the mark-space ratio is high the harmonic spectra of the sampling signal will have amplitudes comparable with the fundamental, e.g. 30th harmonic is  $-3\text{dB}$  and 50th harmonic is  $-6\text{dB}$  (approx.). It follows that the heterodyne noise will have a significant amplitude. Calculations of the noise amplitude would be extremely difficult particularly because it would be unfair to assume a flat noise spectrum at the discriminator output.

In a conventional decoding circuit a 1:1 mark-space ratio is used. The third harmonic is approximately 10dB down, but even so the deterioration in signal-to-noise ratio due to this and the fundamental is some 22dB.

Mr. Waddington's decoder is allowed to 'free run' during mono transmissions. There are two reasons why no decoder should be allowed to do this:—

(1) Signal-to-noise ratio on mono will be reduced considerably.

(2) From some transmitters, Sutton Coldfield included, a 23kHz tone is broadcast in the absence of a pilot tone. An objectionable aliasing beat of 15kHz will be produced between this and the switching fundamental at approx. 38kHz.

With regard to Mr. Waddington's comments on mono and stereo gain, for a sample and hold network the output signal amplitude is substantially the same whether the gate is sampling or is permanently open provided the input signal frequency is below half of the sampling frequency.

I hope that the above comments will prove of interest and that correspondence on the subject of sample and hold analysis may be stimulated.

While on the subject of stereo decoders I would like to mention an addition to the 'Phase Locked Loop Stereo Decoder' by myself and A. J. Haywood published in

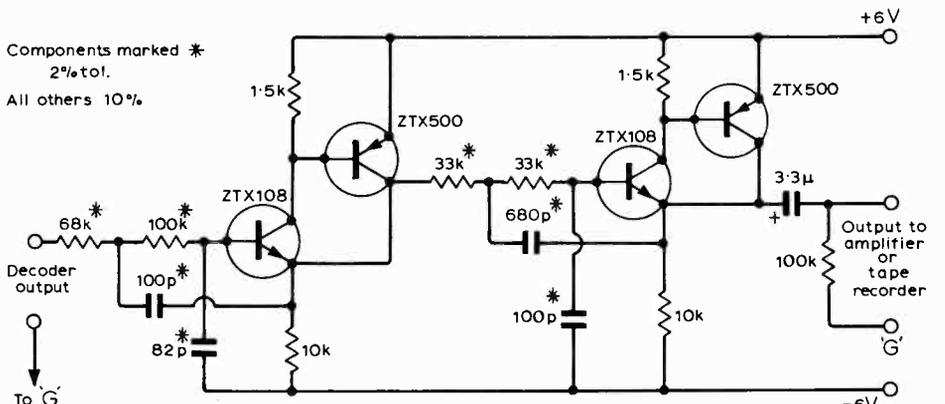


Fig.1 Decoder earth may be 0V or -6V depending on supply rail choice. Filter earth 'G' is independent and therefore may be either.



then the noise improvement will be identical. Thus the two circuits are equivalent in principle and differ only in their input noise sensitive bandwidths.

Mr. Abernethy also mentions that high-speed waveform samplers such as those designed for use in conjunction with oscilloscopes are unsuitable for signal averaging because their fixed gate width does not allow optimum signal recovery conditions to be attained and because their design is aimed at speed of sampling rather than linearity or zero stability. In such samplers the sampling interval is often extremely short, being 350 ps or less, giving them a very large signal bandwidth and correspondingly large noise bandwidths. It is certainly true that this sensitivity may introduce additional unnecessary noise when averaging lower frequency transients. However, this noise can be removed very simply by inserting an ordinary low-pass filter before the sampling gate to match the noise spectrum to that of the signal. In these circumstances the improvement in noise ratio will, in fact, be identical to that given by a conventional boxcar with the same bandwidth and output response time. Thus, while the use of a very narrow sampling window necessitates higher signal gain and causes some increase in open loop sampling non-linearities and zero drift these penalties need not be serious. For instance with an instrument such as the AIM Electronics WSA 114 very adequate results can be obtained without sacrificing the ability to operate at a greatly increased bandwidth allowing averaging of fast transients up to 1GHz, and the ability to time-stretch very fast waveforms and display them on low-frequency oscilloscopes.

R. J. SMITH-SAVILLE,  
AIM Electronics Ltd,  
St. Ives,  
Hunts.

## Loudspeaker enclosures

In the article 'Loudspeaker Enclosures' by E. J. Jordan in the January 1971 issue, a few detail errors have arisen. Using a tapered pipe as a 'quarter-wave transformer', the optimum distance of the drive unit from its throat is given approximately by:

$$d = \frac{l}{2 + (A_t/A_m)^{\frac{1}{2}}}$$

where  $l$  = physical length of pipe;  $A_t$  = cross-sectional area of throat; and  $A_m$  = cross-sectional area of mouth. Hence for a constant cross-sectional area pipe,  $d = l/3$  (not  $1/3$  wavelength as stated, since the loading is very poor beyond the mouth!), increasing to  $l/2$  for a fully tapered pipe of zero throat area, the equivalent of a parabolic pipe of circular cross-section. Far from being 'very popular many years ago' as indicated, I would suggest that its use has become widespread over the past few years, following the publication of my "Paraline" design, (*Hi-Fi News*, April 1963), of which some 20,000 examples are believed to be in use.

The 'quarter-wave' principle was, of course, first used by Paul Voigt in the 1930s in his domestic corner horn and revived by Ralph West in 1949 for the Decca corner speaker.

Regarding horn theory, it is perhaps worth mentioning that the hyperbolic family already includes the conical and exponential cases as respectively limit and central members. In the general expression, the term  $x_0$  is a dimension determining the flare cut-off frequency, not the distance from throat to where  $A = 0$ , since, except for conical horns, the latter is infinitely remote, whilst for the catenoidal horn ( $T = 0$ ) the cross-sectional area is a minimum at  $x = 0$ .

In his closing sentence regarding air displacement, Mr. Jordan echoes the general reluctance of loudspeaker designers to recognize that their devices are usually used in domestic-sized rooms. In these l.f. resonances arise of  $Q$  typically 15-25, so presenting a violently fluctuating load whose predominant component is mostly reactive. Without a conjugate design approach, it would seem that the l.f. performance of a loudspeaker/room/listening position combination must remain quite arbitrary.

R. N. BALDOCK,  
Harrow,  
Middlesex.

## Resistance tolerance code

My attention has been drawn to Mr. Sproxtton's letter in the November issue, in which the tolerance coding for resistors and capacitors is criticized. This code was produced after careful consideration by Technical Committee 40 (capacitors and resistors for electronic equipment) of the International Electrotechnical Commission, of which forty-one countries, including U.S.A., Japan and the whole of Europe, are members. The following points were considered:

1. In matters of this kind it is usually desirable to accept as standard, wherever possible, some widely accepted practice. This particular tolerance code had been used for many years in the U.S.A. and had been adopted by some European countries. These people appear to have used it without confusion.

2. There was not "a whole alphabet available for choice". To have created a new code using the same letters as the existing one but with different meanings would have caused appalling chaos. Leaving out I and O (easily confused with numbers), the thirteen letters of the existing code and the eight letters representing multipliers for capacitance and resistance values, there are three letters left to cover thirteen tolerances. The only reasonable course is to adopt the existing code.

3. If the code is correctly used, as Mr. Sproxtton's examples show, there is little risk of confusion between the letter used for the multiplier and the letter used for the tolerance. His examples were 6800 ohms  $\pm 10\%$  and 4.7 megohms  $\pm 20\%$  which

code respectively as 6K8K and 4M7M. Even with values like 6800 ohms  $\pm 10\%$ , or 0.068 $\mu$ F  $\pm 30\%$ , which code respectively as 68KK and 68nN, the letters still come quite simply in the right order.

The tolerance code may not have been a stroke of genius but it was probably the best choice in the circumstances and it is the first time after a few years of use that anyone has suggested that it is confusing.

G. DAVID REYNOLDS,  
(Chairman of IEC/TC 40)  
Hatfield,  
Herts.

Despite the fact that normally the multiplier for 1000 is "k" the I.E.C. decided that all resistor multipliers (R for unity, K, M, G & T) should be capitals and all capacitor sub-multipliers (p, n,  $\mu$  or u & m) should be lower case.—ED.

## Ganging potentiometers

The Addashaft scheme, whereby either steel or nylon shafts can be cut to length and then inserted into potentiometers has advantages. Risk of damage to the potentiometer during the sawing and filing operation is obviated, and a choice of insulating and conductive shafts is available. Work could be reduced further, and material saved, if a choice of shaft lengths were provided.

An adaptation of the scheme could usefully be applied to twin potentiometers, of which at present only a limited choice of values (usually equal) is available. If one could quickly twin any two potentiometers, the range to be manufactured and held in stock would be reduced, and twin potentiometers, would no longer be "special". For example, if there is a need for  $x$  values of one and  $y$  values of the other, at present one needs to stock  $xy$  different types of twin potentiometer, whereas if any two could be twinned as required, the number of types of single potentiometer needed is only  $(x+y)$ , and any of these can also be used individually. The saving increases rapidly with  $x$  and  $y$ , e.g. for a choice of four values, a stock of 8 single potentiometers replaces a stock of 16 twin potentiometers and so on. The above applies chiefly to ganged potentiometers driven by a single shaft, but it would seem possible also to cater for twin potentiometers which are not ganged but have a central shaft and a coaxial cylinder controlled by separate knobs.

It is at present possible to buy potentiometers with or without d.p. switch, which doubles the amount of stock it is necessary to hold and manufacture. If the switch could be quickly associated with either or both potentiometers at choice, or omitted if not required, this would add further to the advantages.

It appears that both manufacturing and storage costs could be materially reduced by this scheme if widely adopted.

K. J. YOUNG,  
Crowthorne,  
Berks.

# Electronic Building Bricks

## 10. The oscillator

by James Franklin

One of the functional blocks in the television set diagram in Part 1 is labelled "oscillator". According to the dictionary, to oscillate is to swing like a pendulum, move to and fro between two points. This, of course, is a definition of oscillation in visible, mechanical terms. In an electronic oscillator the oscillation cannot be seen because the to-and-fro movement is not of some mechanical part but of electrons in a circuit (Part 5). Although we cannot see this movement directly we can detect, measure and display it by various instruments, and so can discover a good deal about what goes on.

In one type of oscillator the character of this to-and-fro electron movement is similar to that of pendulum movement in a clock, so let us look more closely at a swinging pendulum. Fig. 1 is like a series of frames from a cinematograph film showing the positions of a pendulum at successive instants during its swing. If we take the dead-centre position A as a reference point we see that the pendulum swings first to the right to an extreme position D, back to the dead-centre position G, beyond this to an extreme left-hand position J, then back to the

dead-centre position A'. It then repeats the process through D' G' J' and back to A". . . and so on. This is a cyclic movement which, in the clock, goes on repeating itself as long as mechanical power is applied to the pendulum at the right instants to keep it swinging (e.g. through an escapement mechanism from a spring). One complete cycle of pendulum swing is marked on Fig. 1 as being between reference position A and position A' but a cycle could equally well be defined as between any two corresponding positions, for example between C and C'.

If we plotted a time graph of the displacement of the pendulum bob along its arc of swing it would come out as shown in Fig. 2—a graph which some readers may recognize as simple harmonic motion. In the comparable electronic oscillator, if we plotted a time graph of some variable that indicated electron movement it would be similar to Fig. 2. We cannot easily measure the displacement of electrons from a given point but we can readily measure the rate of displacement of electrons, which is

\*Strictly, only when the angle of swing is very small.

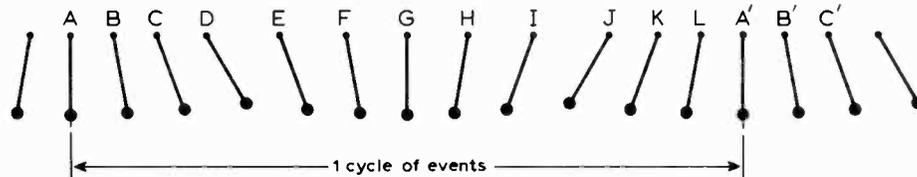


Fig. 1. Sequence of positions of a swinging pendulum—a mechanical oscillator.

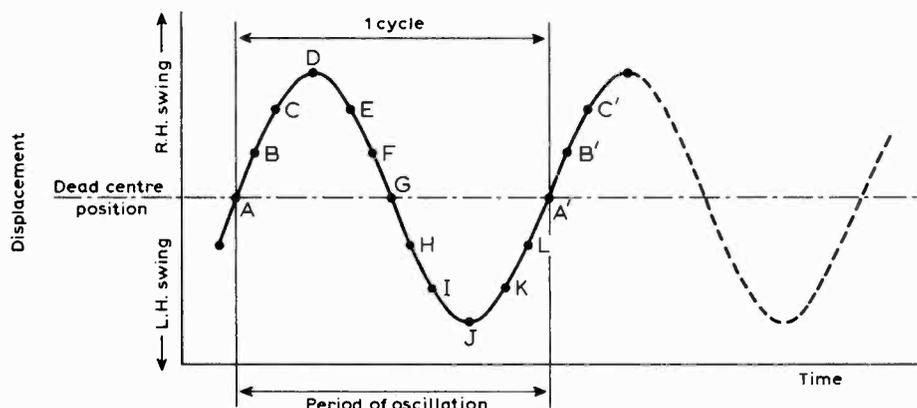


Fig. 2. In this graph the pendulum positions in Fig. 1 are plotted, as displacements from time.

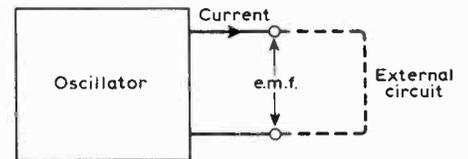


Fig. 3. Output of an oscillator is measurable as an e.m.f.

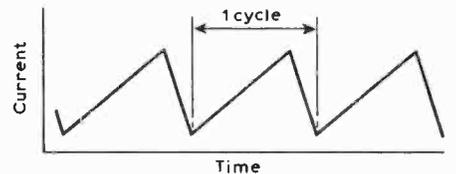
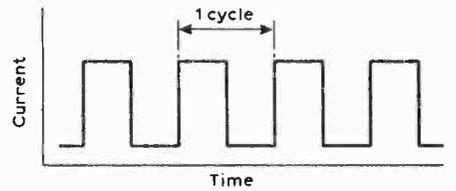


Fig. 4. Two other current/time graphs which are cyclic and are therefore oscillations.

electric current (Part 3). Thus a time graph of current measured at a suitable point in the oscillator circuit would be similar to Fig. 2. This version of simple harmonic motion in electrical form is called a *sinusoidal* oscillation†, or, because of the wave-like character of the graph, a *sine-wave* oscillation. A similar shape would be obtained if we plotted a time graph of potential difference existing across a part of the oscillator circuit; and in fact the output of an oscillator is often measured as an e.m.f. between two terminals (Fig. 3).

The swinging pendulum is analogous to the electronic oscillator for another reason: in both the energy is continually changing between potential form and kinetic form.

As we have hinted, the sinusoidal oscillator is only one of several types available. There are, for example, oscillators generating square waves, pulses of various shapes, and saw-tooth waves (Fig. 4). An oscillator producing pulses is normally called a pulse generator, and one of these appears in the computer block diagram in Part 1. Whatever the wave shape, however, all oscillators have this in common, that they generate a cycle of variation in an electrical quantity which is repeated indefinitely, as long as electrical power is supplied to the oscillator. The length of time taken by one cycle is called the *period* of the oscillation, and the number of periods (or cycles) that occur in a given time is called the *frequency* of oscillation. In practice frequency is measured in cycles occurring per second, and the unit cycle per second is called the hertz (Hz).‡

†The name comes from the trigonometrical function, the *sine* of an angle. A graph of the sine of an angle plotted against the angle in degrees has the same shape as Fig. 2.

‡Named after Heinrich Rudolf Hertz (1857-1894), German physicist.

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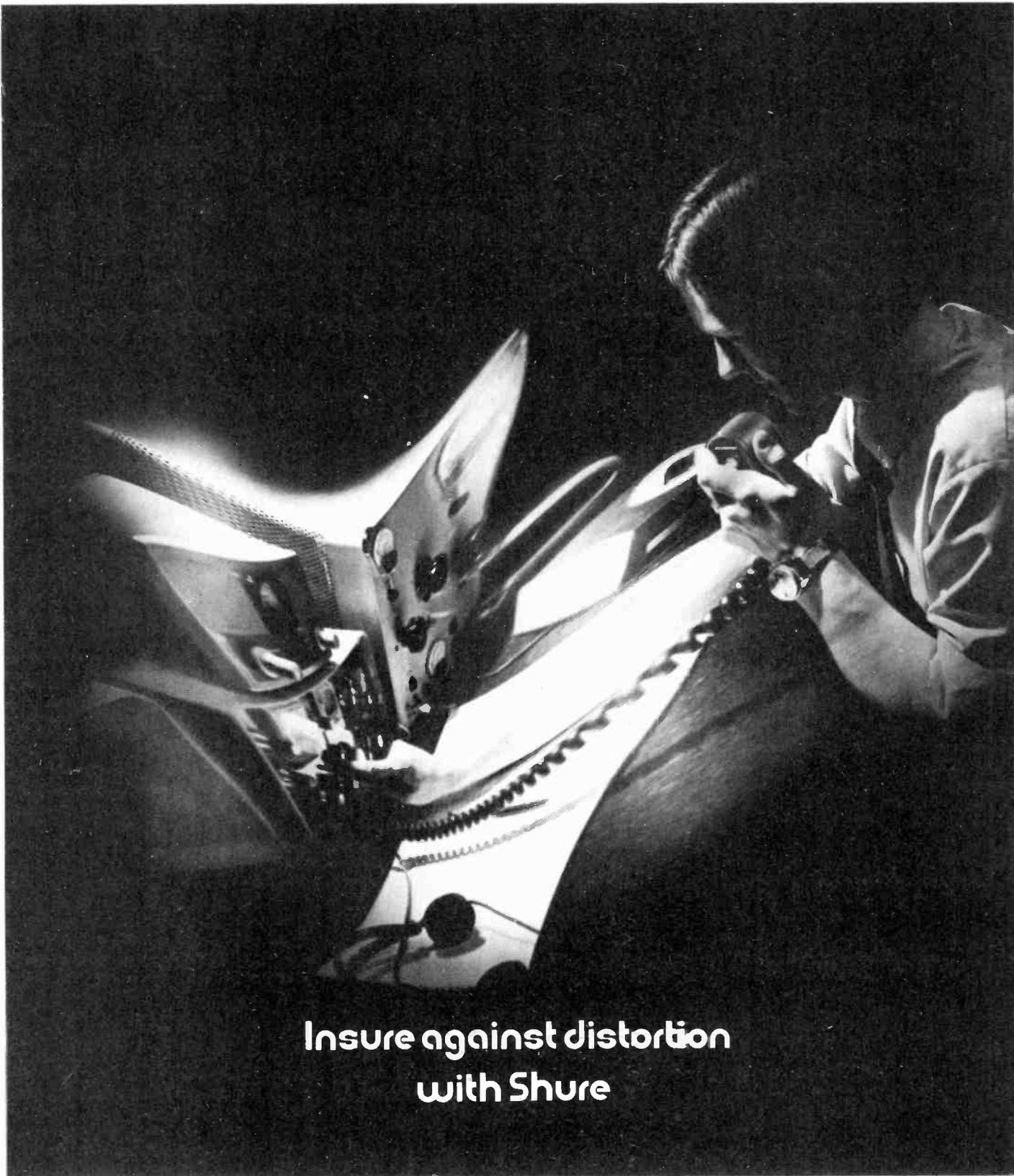


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# New Approach to Class B Amplifier Design

by Peter Blomley\*

(Concluded from February issue)

This article describes a 30-watt amplifier design which embodies the author's approach to class B design, outlined last issue. Although further work on this approach is still needed, the design illustrates the kind of problems involved. The author also discusses the application of integrated components in future designs.

The general design of a complete amplifier using the new approach is relatively conventional except for the inclusion of the signal splitter (described last month). In principle, the design of each half of the output stage is made simpler as there is no cut-off, hence

removing the necessity for predicting the performance in the cross-over region.

Examination of the circuit (Fig. 1) shows that the amplifier consists of three sections, the input amplifier, signal splitter and output amplifier.

**Input amplifier.** This converts the input voltage into a proportional output current

which drives the signal splitter. To enhance the performance of the amplifier as a whole, this section should have a reasonable mutual conductance (1A/V) and good linearity (1%). The latter does not represent a serious problem as the input amplifier is a low-level class A amplifier, but care is needed to control the maximum value of  $g_m$  otherwise frequency compensation problems arise.

**Signal splitter.** As many fundamental details of the signal splitter were described last month, further details are confined to the biasing system. If perfect bipolar devices were available and ideal current sources existed, voltage bias across the emitter-base junction would not be needed, but such situations do not exist and distortions due to conditions falling short of the ideal can be rendered negligible by employing simple bias diodes (Fig. 2). This reduces the voltage excursion at the input to the signal splitter from 1.2V to 300mV pk-pk. The waveform with a sinusoidal output current is shown in Fig. 3.

**Output stages.** This now is one of the easiest to design. As long as the gain remains constant throughout the output cycle all is well. In the initial version, used to evaluate system performance, a compromise was reached between complexity, performance and cost. Thus individual adjustment potentiometers were used instead of the matched devices.

The output sub-amplifiers are similar to the Quad triples, these giving excellent linearity down to very low output currents, coupled with outstanding thermal stability. To compensate for the effect of ambient temperature changes on the quiescent current of the amplifier, diodes  $D_1$  and  $D_2$  cancel  $V_{BE}$  changes in transistors  $Tr_7$  and  $Tr_8$ . It may have occurred to the reader that diodes in the forward path of the amplifier loop could generate appreciable distortion. However, in practice the maximum change in current is about 4:1 and thus almost corresponds to the change in collector current of transistors  $Tr_7$  and  $Tr_8$ . In this way the change in voltage drop across the transistors compensates for the change in the diodes. Even if this did not occur, the resultant gain change for the output sub-amplifier is less than 4% for  $I_{out}$  values between 0 and 2A. The problem can be alleviated by increasing the current into

\*Allen Clarke Research Laboratory (Plessey), Towcester, Northants.

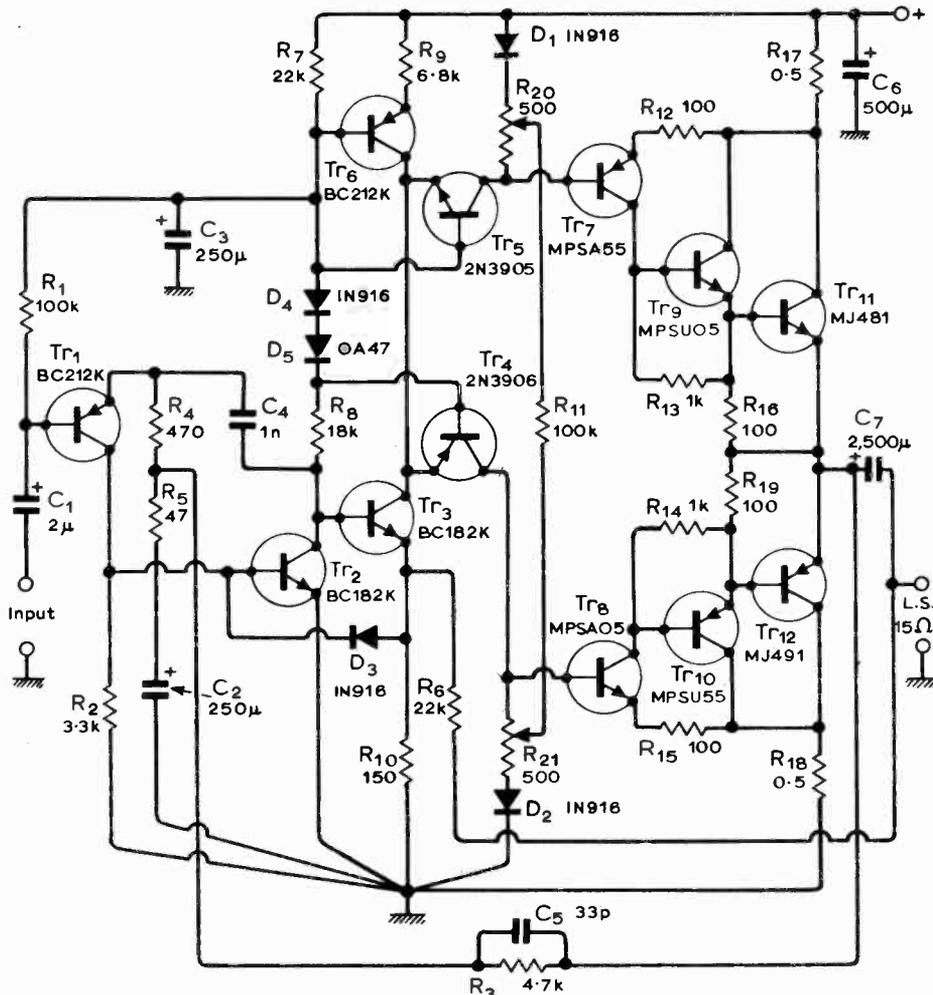


Fig. 1. Complete power amplifier circuit using new approach. Design gives harmonic distortion of 0.01% at all power levels and intermodulation distortion of 0.003%.

diodes  $D_1$  and  $D_2$  and adding one resistor, but the advantages gained from this are negligible.

**Circuit description**

The function of  $Tr_1$ ,  $Tr_2$ , and  $Tr_3$  is to convert an error voltage—the difference between the input and feedback voltage—into a proportional output current. Now to produce the required mutual conductance of this stage (1A/V) without sacrificing either noise performance or linearity, the design in Fig. 1 was used. Starting at the input transistor  $Tr_1$ , this p-n-p type is used mainly as a level shifter. If we assume that the

current gain of  $Tr_2$  was extremely large ( $> 500$ ), then this input stage would have a maximum voltage gain of about five—not very much! If voltage gain was increased to the theoretical maximum of 30 (by decreasing the value of  $R_2$  and  $R_3$ ) problems would arise with the voltage offset at the speaker output due to increased emitter current flowing through  $R_1$  and base current flowing through  $R_1$ .

Assuming for the moment that this first stage gain is a reasonable compromise, it now becomes obvious that the noise and distortion performance is dictated by the next stage. This stage ( $Tr_2, R_8$ ) is a straight-forward class A amplifier with very high

gain (typically 400) and low distortion due to the limited modulation index of the collector current (0.04 max). The peak 2nd harmonic voltage generated is about  $10\mu V$  and, assuming this is referred to the input of the first stage, it represents less than 0.001% 2nd harmonic distortion with feedback. Thus this second stage is the work horse of the input section, the third device  $Tr_3$  being used both as a buffer to reduce the loading of  $R_{10}$  on  $R_8$ , and to convert the voltage changes across  $R_8$  into an output current to drive the emitters of the signal splitter.

Resistor  $R_{10}$  performs two functions in this last stage of the input section. It defines the conversion constant  $Engmen$  for the stage, and it governs the maximum current which can be driven out of the collector of  $Tr_3$ . (This maximum current is defined by using the conducting voltages of  $D_3$  and  $Tr_2$  and the value of  $R_{10}$ .) Therefore this input section seems to have excellent performance during normal operation, but what can happen during an overload?

If the input transient was negative all would be well due to  $Tr_2$  entering saturation. But if the transient was positive  $Tr_1$  would turn off completely, the potential across  $R_{10}$  rising toward that at the end of  $R_8$ . ( $Tr_2$  would also be completely cut off.) This would cause excess currents to flow in  $Tr_3$ , upsetting the bias chain  $R_7, D_1, D_2, R_8$ . After the excessive input signal is removed some time would elapse before recovery would take place, hence diode  $D_3$  clamps the voltage and maintains  $Tr_2$  in full conduction to reduce recovery time and improve amplifier stability.

While discussing the problem of recovery from overload, the charge across the compensation capacitor  $C_4$  has also to be taken into account. The time for the accumulated charge to decay is a function of the amount of charge and the rate of decay. If the rate of decay is constant, the only way to reduce the recovery time is to limit the accumulated charge (in terms of voltage). Diode  $D_3$  performs this function as well as clamping the voltage across  $R_{10}$  at 1V thus limiting drive current into the signal splitter.

The second section is the signal splitter, unique to this approach, and consists of transistors  $Tr_4$  and  $Tr_5$  plus a current source transistor  $Tr_6$ . The signal current into the emitter of  $Tr_4$  or  $Tr_5$  is derived by subtraction of two current levels, one constant and set by the voltage across  $R_9$ , and the other the output current of the input section. This signal current either appears at the collector of  $Tr_5$ —causing a voltage change across  $R_{20}$ —or at the collector of  $Tr_4$ —causing a voltage change across  $R_{21}$ . These voltage changes are converted into positive and negative output currents in the output section, which are then added together to give the final waveform. The current gain of the output sections which are conventional triples are governed by the ratio of  $R_{20}$  to  $R_{17}$  and  $R_{21}$  to  $R_{18}$ , and in this case the gain of 1000 seemed reasonable.

To keep the output triples above the minimum conduction level a bias current is provided by  $R_{11}$ . The procedure adopted for setting the standing current is to first set  $R_{20}$  and  $R_{21}$  to minimum (diode end).

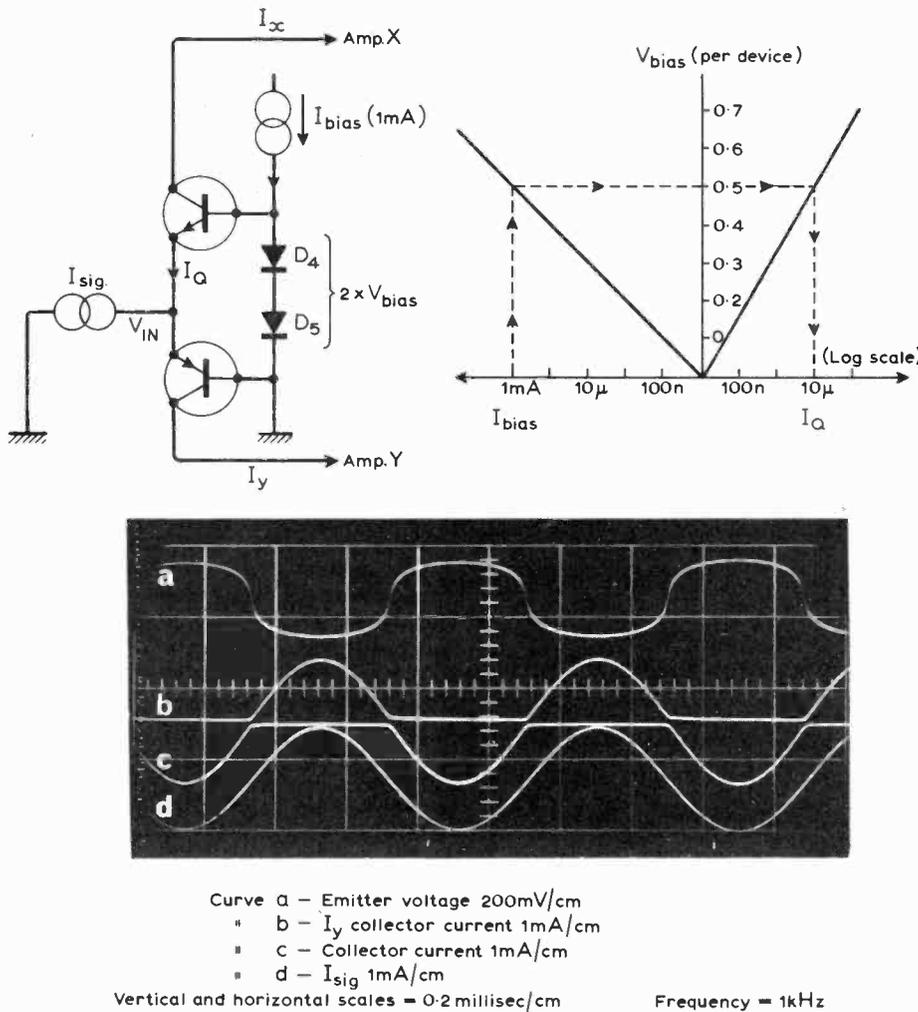


Fig. 2. Input amplifier converts signal voltage to a proportional current to feed transistor signal splitter. Bias diodes reduce voltage excursion from 1.2V to 300mV pk-pk. Bottom trace is current signal input to splitter.

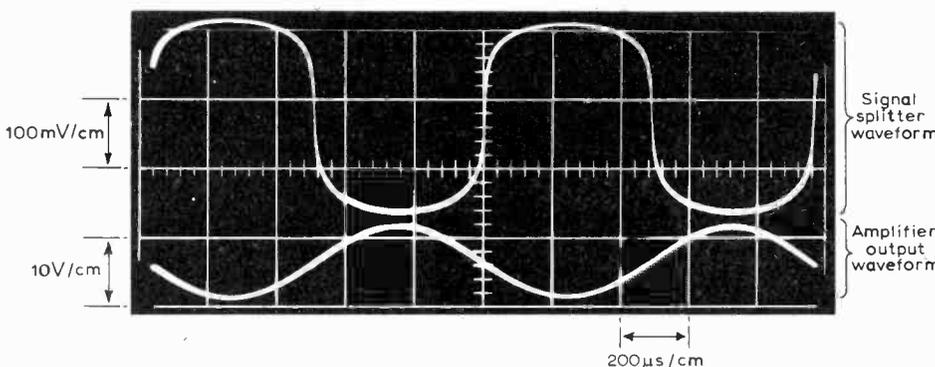


Fig. 3. Voltage excursion at signal splitter input with corresponding sinusoidal amplifier output current ( $R_L=15\Omega$ ).

Set quiescent current with  $R_{20}$  and increase  $R_{21}$  until there is a small increase in current.

The only part still to be described is the biasing chain  $R_7-D_4-D_5-R_8-C_3$ . This provides the half supply voltage for the base of  $Tr_1$  (decoupled by  $C_3$ ), a load for the class A stage  $Tr_2$ , and sets devices  $Tr_4$  and  $Tr_5$  at the minimum conduction level required for good phase response during cross-over—by using the voltage across  $D_1$  and  $D_2$ . By increasing the value of  $C_3$  it is possible to reduce the rate of charging of the speaker coupling capacitor, eliminating 'thump', but capacitor size becomes very large.

Returning for a moment to the input section,  $Tr_2$  is in a similar position to that used in many amplifiers, but instead of driving another stage ( $Tr_3$ ) which only requires a limited voltage swing, it is the prime mover for the output section. To have sufficient drive capability the quiescent current in this stage may well need to be 10mA—instead of the 1mA in mine—and the voltage swing on the collector will be the full supply voltage (50 volts).

It now seems clear why the distortion of many amplifiers rises at low frequencies. The dissipation change of this device during a voltage cycle could be 500mW pk-pk in the case I have quoted giving an emitter-base voltage change at low frequencies of about 100mV. This change, even if we assumed it is basically a linear function of voltage, will cause a non-linear change in the input device and hence a considerable rise in distortion at low frequencies. In my amplifier the maximum dissipation change in  $Tr_2$  will be less than 1mW, thus eliminating this form of distortion and improving intermodulation performance.

**Performance**

The measurement of distortion created some difficulties especially when con-

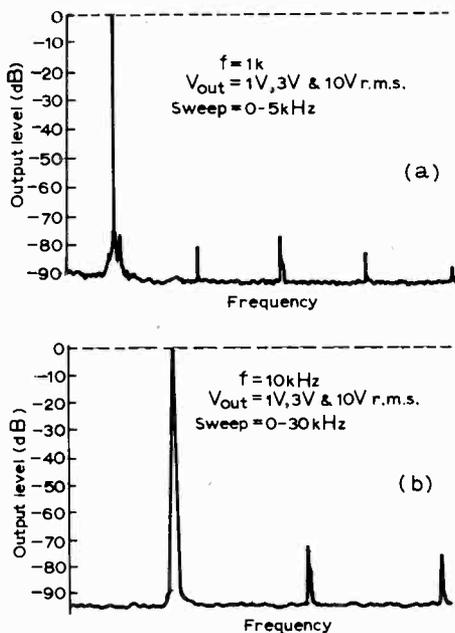


Fig. 4. Spectra made with a wave analyser showed no difference between spectra of outputs from oscillator and amplifier. Plots were made with (a) 1kHz and (b) 10kHz signals and were identical at all three power levels.

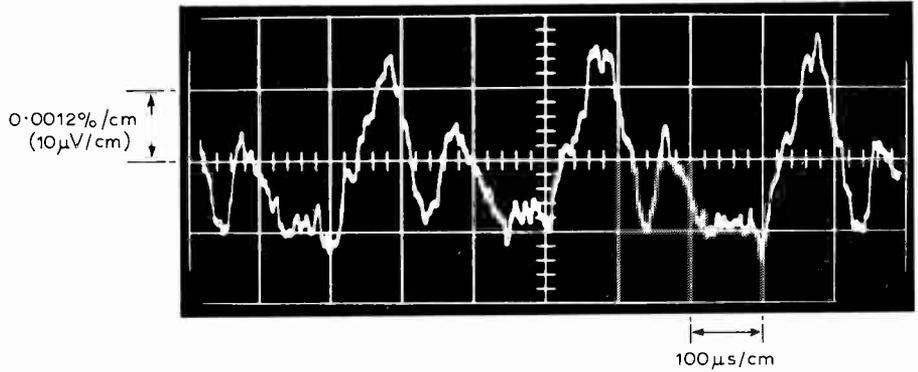


Fig. 5. Null method of assessing amplifier distortion shows distortion products to be well down in the noise. Deflection of 4cm represents 0.003% peak distortion at 10 watts (3kHz, 15Ω load).

sidering the range of frequencies over which this amplifier operates. The methods employed can be separated into two distinct techniques—spectrum analysis and nulling methods. To realize the first technique, an oscillator with a pure, single-line spectrum was needed, but the only one available at the time, approaching a reasonable performance, was the Si 451 produced by J. Sugden & Co, having a range up to 30kHz. This was found (excellent as it is) to be inadequate to permit the measurement of amplifier distortion.

So difficult in fact was the problem that it is impossible to publish distortion curves with any degree of confidence in their truth, but it can be said that using the Hewlett Packard 3590 wave analyser there was no discernible difference between a plot of the distortion of the oscillator and that taken after the oscillator output had been passed through the amplifier. Plots were taken over the frequency range 100Hz to 20kHz and powers of 100mW to 25W. As a matter of interest the spectrum plots of the amplifier are shown in Fig. 4 for 1kHz and 10kHz and at several power levels. The second method attempted was rather more successful but unfortunately does not present information in a usable form because it involves a comparison of output and input signals. It is also not a sequential test as in the previous method and as a result problems were encountered in successfully nulling the output against the input of the amplifier, due to the phasing of the signals and the earth loops generated by the measurement method. After considerable adjustment of the phase compensation and spurious pick-up difficulties the photograph Fig. 5 was obtained. Here the distortion generated is right in the noise (−120dB down from 20V r.m.s.) and the total deflection of 4cm represents 0.003% peak distortion at 10 watts and a frequency of 3kHz, chosen for easiest phase cancellation. The spikes usually evident in the difference waveform with this type of amplifier are completely absent, even with reactive loads, indicating that stability in the cross-over region must be excellent.

**Intermodulation performance**

The use of these two techniques is limited in one way or another to the evaluation of

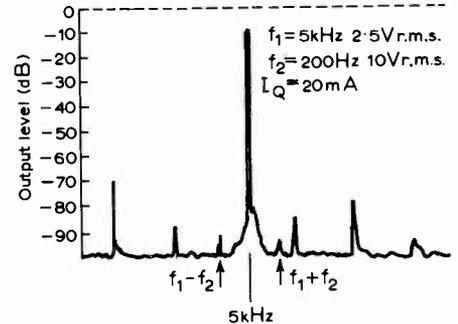


Fig. 6. Result of feeding 5kHz and 200Hz signals in a 16:1 power ratio into amplifier. Intermodulation products  $f_1 + f_2$  and  $f_1 - f_2$  are 90dB below 200 Hz signal. Other spectral lines are due to generator distortion.

amplifier linearity. The main advantage is, of course, that a direct numerical value of distortion is obtained which can be used in comparison with other amplifiers.

The intermodulation test does not rely on low-distortion oscillators of signal cancelling techniques—in fact the only component which limits the measurement accuracy is the wave analyser itself. The real drawback is seen when an interpretation of the results is necessary! The method adopted is to “sweep” the transfer characteristic of the amplifier with a low-frequency signal of large amplitude, and to “measure” the slope of the characteristic with a low-level high-frequency signal. The two frequencies selected were 200Hz and 5kHz in a power ratio of 16:1.

The results not only ease the assessment of the amplifier performance in an absolute sense but also give some form of subjective measurement for comparison with other elements in the system. The results obtained in Fig. 6 indicate an excellent performance, the intermodulation products  $f_1 + f_2$  and  $f_1 - f_2$  are −90dB below the sweeping signal (200Hz) all other spectral lines being due to generator distortion.

**Amplitude-frequency response**

The type of frequency compensation used for this amplifier is unusual, mainly as a result of the system design. The open-loop gain begins to fall off at about 4kHz and continues on a 6dB/octave roll-off to about

500kHz where the second pole of the output section starts to contribute excess phase shift. The choice of the position of the dominant compensation was a difficult one. If it was placed in the output section, as is normally the case, the gain of the input amplifier would have to be restricted at low frequencies, affecting the distortion performance of the amplifier.

Another choice was using the dominant lag to encompass the output section as well as part of the input amplifier. This would lead to instability internal to the loop enclosed by the dominant lag and thus an internal pole would have to be introduced to remedy this condition. The final choice (shown in Fig. 7) gives the single-pole compensation needed for unconditional stability coupled with minimal high-frequency distortion. The inherent pole in the output section is subdued by the feedback resistance  $R_3$  (so far as the main loop is concerned) but gives the required unconditional stability of the output section.

The performance with reactive loads will be spoiled if the output impedance of

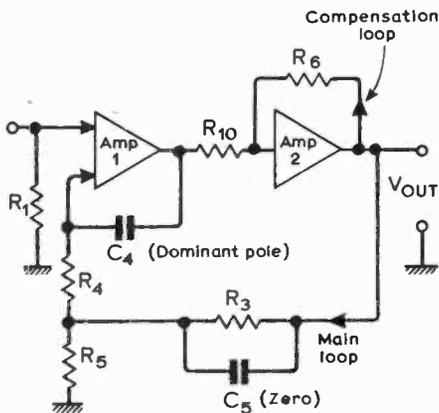
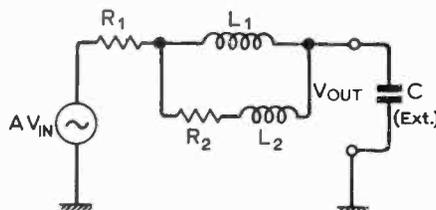


Fig. 7. Single-pole frequency compensation method used gives unconditional stability coupled with minimal h.f. distortion.



$$R_1 = \frac{1}{g_{m1}} \left( 1 + \exp \left( K \cdot \frac{I_{OUT}}{I_{MAX}} \right) \right)$$

$$L_1 = \frac{1}{2 \pi f_2 g_{m1}}$$

$$L_2 = \frac{1}{2 \pi f_3 g_{m2}}$$

$$R_2 = \frac{1}{g_{m2}}$$

Fig. 8. Power amplifier equivalent circuit. Simple analysis shows output impedance is controlled by main feedback loop, but in practice  $R_6$  generates another loop effectively placing a damping resistance across the apparent output inductance.

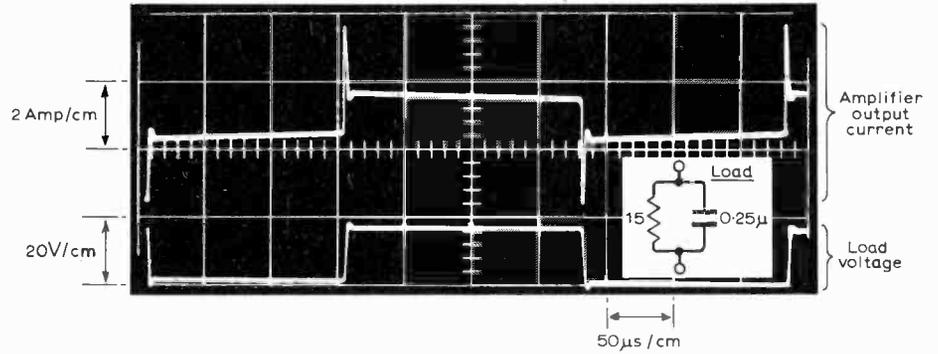


Fig. 9. Performance with a capacitive load. Capacitor in feedback loop effectively reduces maximum rate of change of voltage across load. Overshoot is much less when fed from a pre-amplifier.

	<b>Performance</b> —with 60V regulated supply
output power	20 watts into 15 ohms 30 watts into 8 ohms
power response	30Hz to 100kHz (-3dB)
output impedance	0.1 ohm at 1kHz
total harmonic distortion	< 0.01% throughout audio band and all power levels
intermodulate distortion	< 0.003%
voltage gain	100
noise level	-120dB below full power
maximum peak output current	± 3 amps, approx.

the amplifier is controlled by the overall feedback loop, i.e

$$Z_{out} = \left( 1 + j \frac{f_1}{f_2} \right) / g_m$$

where  $f_1$  is the signal frequency and  $f_2$  the open-loop -3dB frequency. This expression has a simple analogy with a series inductance and resistance, where  $R = 1/g_m$  and  $L = 1/2 \pi g_m f_2$ .

A little more work† shows that if a capacitive load is used the amplifier would have a response given by

$$G = \frac{1}{p^2 T^2 + a p T + 1}$$

This is the equation of a second-order system, where  $a = (1/g_m) \sqrt{C/L}$ , and the natural frequency of oscillation is  $\omega_o = 1/T = 1/\sqrt{LC}$ . If the amplifier has an overshoot it must be due to the overall amplifier having an  $a$ -value approaching zero. If we now assume typical values and examine the worst case condition,  $g_m = 10A/V$ ,  $f_2 = 4kHz$  and  $a = 0.1$  (20dB peak), then  $C = 4\mu F$  and  $\omega_o = 250kHz$ .

If this was a perfect model for the amplifier the overshoot would be excessive, but in practice the output impedance is not only a function of frequency but also of output current. Thus  $a$  gets larger (less overshoot) as the output current increases. The basic assumption of this simple analysis is that the output impedance is controlled by the main feedback loop, but in this amplifier resistor  $R_6$  generates another loop which effectively places a damping resistance across the apparent output inductance (Fig. 8).

The only remaining improvement to the transient performance of the amplifier is by pole-zero cancellation using the feed-

back element. If this term seems somewhat academic, an alternative is to study the overshoot with a second-order system with various inputs. If the input is an ideal step the amplifier will give theoretical overshoots, but if the rate of rise of the input waveform is decreased the overshoot will reduce and eventually disappear. The capacitor (a zero) in the feedback loop is really reducing the maximum rate of change of the voltage across the load and hence the degree of excitation given to this inherently oscillatory system. By using this type of compensation excellent performance with reactive loads has been finally achieved (Fig. 9). The overshoot with capacitive loads, such as  $4\mu F$ , is about 50% with an ideal step input and far less when fed via a preamplifier, thus no difficulties should be experienced with any normal load.

**Electrostatic loads.** The distortion characteristic with this type of load was still insignificant below 10kHz and gave a gradual rise up to 20kHz where it was still less than 0.05% at maximum output ±. Square-wave performance is shown in Fig. 10 at maximum ± output. The ringing is due to the finite output impedance converting the ringing current in the inductance and capacitance of the load into ripples in the output, plus the overshoot of the amplifier itself.

**Future developments**

The amplifier design is hopefully only a source of ideas which may encourage further research into the whole approach to design. So that the trend may be continued, future proposals are outlined in Fig. 11. Here, the main difference is that

† See for instance "Active filters" F. E. J. Girling and E. F. Good, *Wireless World*, vol. 75, Sept. 1969, pp. 403-8.

± Maximum output is dictated by peak current output capability.

the output subamplifiers are oriented toward the use of integrated components. It has become obvious that past problems with class B amplifiers originated with the stabilization of the quiescent current to give zero cross-over distortion. Attempts were made to use diodes to compensate for device  $V_{BE}$  changes with fluctuations in the ambient temperature—the independent variations due to device dissipation could not be eliminated. Most of the time the diode did its job and the voltage defined by the combination of transistor and diode remained constant. This constant voltage was used in conjunction with low-value resistors to set the quiescent current in the output circuits.

If now an integrated component is used both the diode and the transistor are on the same chip and, apart from minor fluctuations, the combination is isothermal. As a result the quiescent current is a function *only* of the setting voltage and not ambient temperature or differential device temperatures. The accuracy with which the current can be set is largely governed by the offset voltage of the transistor pair. Typical values of  $\pm 4\text{mV}$  which would represent a  $\pm 8\text{mA}$  inaccuracy in the quiescent current using 0.5-ohm feedback resistors are readily obtained. With such an arrangement a reasonable quiescent current for the sub-amplifiers would be 30mA, the worst case figures would be 24mA and 38mA. Both of these values are well above the low conductance current level (5mA) which is required for good linearity of the sub-amplifiers.

The advantage of the new approach is fairly evident when it is realized that as long as the amplifiers are above the non-linear region, the spreads introduced in the sub-amplifier quiescent current will not cause the class AB situation of over-biasing (shown last month) characteristic of present designs. It is now possible to design an output stage without the normal trim potentiometers, thus giving a degree of freedom in production not possible with current amplifiers. The performance of the amplifier, once checked at the end of a

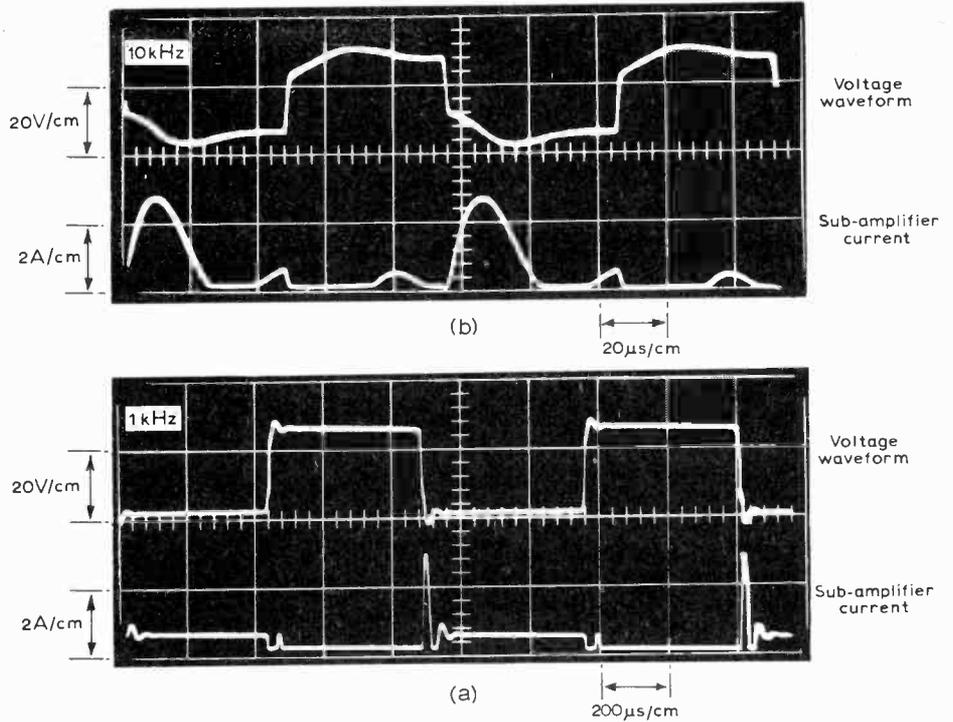


Fig. 10. Square-wave performance when driving electrostatic load at 1kHz (a) and 10kHz (b). Top traces are voltage and lower traces current out of sub-amplifier. Ringing is due to output impedance converting ringing current in  $L_2$  and  $C_2$  into ripples in the output.

production line can be guaranteed for operation in any climate and for any period of time.

**Possible applications**

The performance of an amplifier of this calibre is, in my opinion, wasted in a conventional audio set-up. In most cases, the transducers will be the weakest link.

The approach used in the design of the output sub-amplifiers does not rely on complementary matched devices—in fact, in most cases n-p-n devices are preferred for their superior secondary breakdown characteristics. This represents considerable reduction in amplifier costs especially in the 100-watt region as presently available devices boast a  $V_{CEO}$  of 120V with

100 watts dissipation at a cost of less than 75p.

The ultimate use for this amplifier would appear to lie with the high-power professional market where the performance of cascaded amplifiers in a system would have to be excellent. Use in other fields would be mainly governed by the expected gain in performance or reduction in cost. A possible application would be as a portable standard oscillator, perhaps meter calibration amplifiers, or even high-frequency low-distortion class B transmitter amplifiers. However, these are only inspired guesses which may interest those working in these relevant fields.

Thanks are due to Peter J. Baxandall for his advice and encouragement and to Hewlett Packard and the Plessey Co. for use of their facilities.

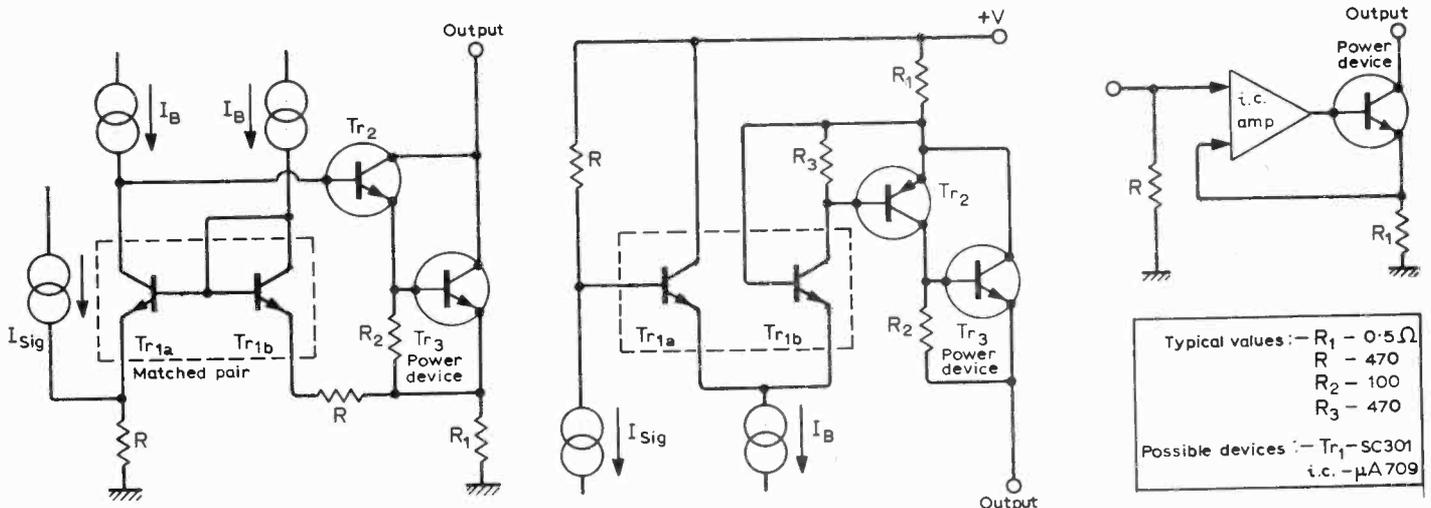


Fig. 11. Proposals for integrated components in output sub-amplifier.

# Multiple-array Loudspeaker System

## How to use an assembly of small units to solve a baffling problem

by E. J. Jordan

In an article in the November 1970 issue (The Design and Use of Moving-coil Loudspeaker Units) I discussed the advantages of the simple single-cone moving-coil loudspeaker, where high-quality wide bandwidth sound reproduction is required. In practice it has been found that for domestic applications in a medium sized lounge, embracing say 2000 cu ft a suitably designed unit having a cone diameter of about 4in correctly loaded will provide more than adequate power bandwidth without difficulty. When it is necessary to provide high-quality sound in rooms considerably larger than this, however, we can either use larger loudspeakers particularly to handle the low frequencies, together with mid-range and high-frequency units and the appropriate cross-over systems or multiple arrangements of the single-cone full-range unit.

The advantages of using a multiplicity of small loudspeakers for high power, wide bandwidth applications are not generally appreciated. In the first place the efficiency of a multiple array can be very considerably higher than that of a large loudspeaker having comparable power handling capacity, and in fact lies somewhere between this and a full horn system. For example typical efficiency for a high-flux 15in direct radiator unit is 3 to 5%. That of a multiple array may be as high as 10-15% at low frequencies. A

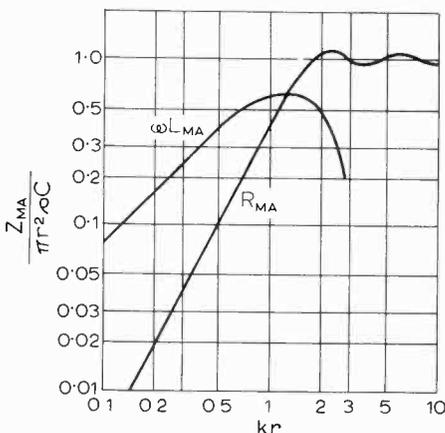


Fig. 1. Mechanical impedance of the air load on a piston surface in an infinite baffle.

large horn-loaded system will be between 30-50% efficient. In comparison with the horn, however, the multiple array can provide a higher standard of quality with considerably less bulk and cost, and further by the use of frequency grading the sound distribution pattern may be 'shaped'. By designing for specific locations a three-dimensional sound field 'tailored' to match the environment may be established. This minimizes adverse effects of the ambient acoustics, and is of particular use where the acoustic environment is difficult. The approach may be extended with considerable success to stereo installations where it is possible to maintain accurate image location throughout large complex areas. Multiple array techniques offer such flexibility in their design that the possible applications are unlimited.

### Efficiency of a multiple array

Consider a single-cone loudspeaker mounted by itself on a flat infinite baffle.

$$Z_{MA1} = R_{MA1} + j\omega L_{MA1}$$

If a number "n" of similar units are mounted close together on the baffle the radiation impedance is

$$Z_{MA_n} = R_{MA_n} + j\omega L_{MA_n}$$

The radiation impedance curves are shown in Fig. 1 and from the work covered in my November article we can say that if the knee of the curve is at  $f_1$  for a single unit it will be  $f_n$  for n units where

$$f_n = \frac{f_1}{\sqrt{n}}$$

For frequencies below  $f_n$

$$R_{MA_n} = n^2 R_{MA1} \text{ and } L_{MA_n} = n^{1.5} L_{MA1}$$

For frequencies above  $f_n$

$$R_{MA_n} = n R_{MA1}$$

The power radiated by a single unit on an infinite flat baffle is given by

$$P_{MA1} \propto \frac{f^2}{Z_{M1}^2}$$

where  $Z_{M1}$  = total mechanical impedance.

We will assume throughout that the loudspeaker(s) is/are working under the condition of mass control then:

$$P_{MA1} \propto \left( \frac{Bli}{L_{Mc} + L_{MA1}} \right)^2 R_{MA1}$$

where  $L_{Mc}$  = mass of moving system.

If the electrical power  $P_1$  fed to one unit is now distributed to n units then the power  $P_n$  received by each unit will be  $P_1/n$ . Assuming that the impedance has been re-matched then if the current supplied to the single unit was  $i_1$  then the current in each of n units will be  $i_1/\sqrt{n}$ . If the length of active conductor in each voice coil is l then the total active length in n units is nl. The flux density B is of course the same as for each individual unit.

Rewriting the power expression for frequencies below  $f_n$  we have:

$$P_{MA_n} = \left( \frac{B(nl)i/\sqrt{n}}{nL_{Mc} + n^{1.5}L_{MA1}} \right)^2 n^2 R_{MA1}$$

$$= \left( \frac{Bli}{L_{Mc} + \sqrt{n}L_{MA1}} \right)^2 n R_{MA1}$$

For frequencies above  $f_n$

$$P_{MA_n} = \left( \frac{B(nl)i/\sqrt{n}}{nL_{Mc}} \right)^2 n R_{MA1}$$

$$= \left( \frac{Bli}{L_{Mc}} \right)^2 R_{MA1}$$

Since the mass of the cone and coil system  $L_{Mc}$  is generally much greater than  $L_{MA1}$  below  $f_n$  the gain in efficiency will tend to approach n but the increase will become progressively less as  $\sqrt{n}L_{MA1}$  approaches  $L_{Mc}$ . Above  $f_n$  the actual efficiency will be independent of n; however there will be a considerable increase in effective efficiency due to the directivity pattern.

### Sound distribution patterns

Fundamentally, the greater the dimensions of a radiating area the more directional it will be. The most familiar example of this is seen in line source loudspeaker systems used for public address or sound reinforcement applications. In this case (Fig. 2) a number of loudspeaker units are mounted vertically in line. The distribution in the horizontal plane is fairly broad, being similar to that of a single unit. Distribution in the vertical plane is however restricted—depending upon the length of the column.

One effect of this is to discourage

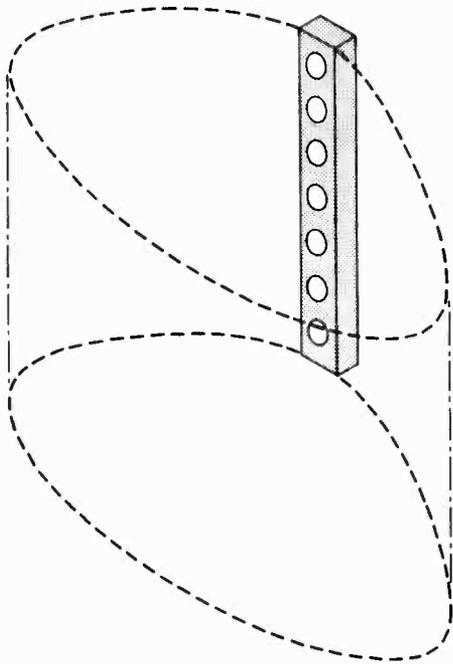


Fig. 2. Idealized distribution pattern for line-source system.

floor-to-ceiling reflections. In practice, due to the fact that the radiating area is not a continuous line but is made up of discrete units, at frequencies where the wavelength is comparable to the physical spacing between the units, the vertical distribution pattern splits up into lobes. The main forward facing lobe becomes excessively sharp and upward and downward secondary lobes appear (Fig. 3). The common method of overcoming this is to grade the electrical power fed to the units so that the centre unit receives the maximum power, the adjacent units above and below receive say  $\sqrt{2}$  of this power and so on. In my view however, a better way of doing this is by *frequency* grading, such that the centre unit receives the full frequency range and the high frequencies are progressively reduced for units away from the centre. This has the effect of reducing the effective length of the line as frequency is raised, thereby maintaining a fairly constant vertical distribution pattern for all frequencies.

The multiple array is an extension of these principles. The basic arrangement consists of close mounted units in square or rectangular formation (Fig. 4). If the same power and frequency response is fed to each unit the mid-frequency sound distribution pattern is given by

$$\frac{\phi_{\theta}}{\phi_0} = 1 - (1.14 \times 10^{-3} fd \sin \theta)$$

where

- $\theta$  = any angle off axis
- $\phi_{\theta}$  = relative pressure at  $L_{\theta}$
- $\phi_0$  = reference pressure on axis
- $d$  = length of vertical or horizontal patterns respectively in metres.

If the pressure is  $-6$  dB at  $L_{\theta-6}$

then 
$$\sin \theta_{-6} = \frac{4.38 \times 10^2}{fd}$$

This basic arrangement will of course be subject to unwanted lobe development as before, and again this may be overcome by frequency grading—this time in both directions away from the centre unit. Here the distribution would tend to be in the form of a rectangular block which by suitable design could be tailored to provide an even distribution throughout a particular location. We can go further however and provide selected areas of higher intensity where required. For certain applications it may be desirable to be able to control the sound distribution at will, this again can be accommodated by providing suitable switching arrangements.

**Circuits for frequency distribution**

It is very desirable that all the units in a multiple array are connected in parallel otherwise there may be inadequate electromagnetic damping on the units. (It may therefore be necessary to fit each unit with its own transformer.) The frequency distribution should be achieved with series air-cored inductors. Sections through multiple arrays are shown in Fig. 5. Two basic circuits are shown with their effect on the vertical distribution. Similar effects can of course be produced in the horizontal plane. More exotic patterns can be produced, where required, with more complex circuits. By combining power grading with frequency grading both the distribution and the frequency response can be controlled and made variable if necessary.

**Applications**

For domestic high-fidelity applications small high-quality, wide-range, units are available. Generally speaking, these are adequate for most domestic locations used

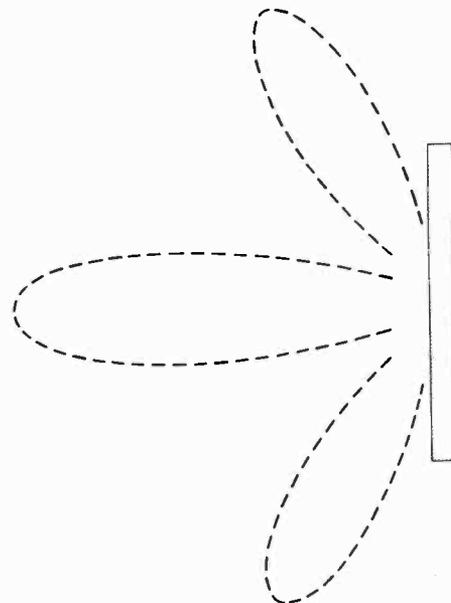


Fig. 3. Example of unwanted lobes due to physical spacing between units.

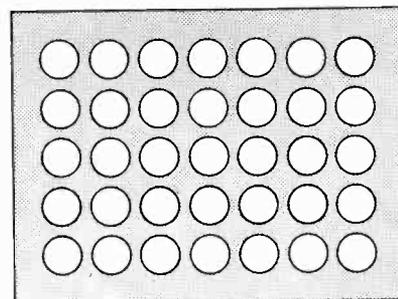


Fig. 4. Basic multiple array.

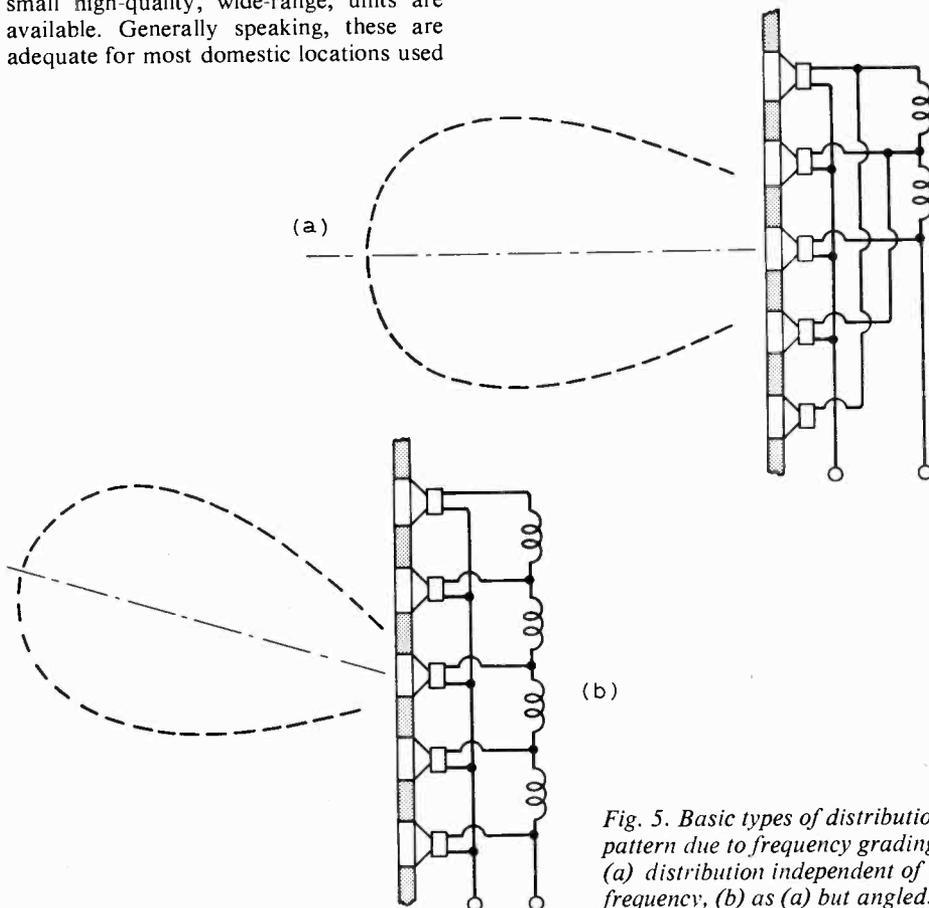


Fig. 5. Basic types of distribution pattern due to frequency grading; (a) distribution independent of frequency, (b) as (a) but angled.

singly. Where required, however, two or four may be used. The units should be mounted vertically in line and frequency grading should be used so that in the case of two units the lower one receives the full frequency range and in the case of four units the third one down should receive the full range: this will ensure that the distribution pattern is displaced upwards. The units should be connected in parallel and frequency grading achieved with air-cored inductors. Inductance values may be specified by the manufacturers of the particular units used.

An extension of this approach is met in the phase-delay stereo techniques described in the February issue. For large sound distribution systems multiple arrays having any number of units may be used, and a point worth noting here is that as the size of the array increases, so the need to provide any form of acoustic enclosure is diminished. When we reach the point where we have a close packed array of 8 or 9 ft square no further form of acoustic loading should be necessary and the system should be 'open-backed'. The 'back-to-front' depth of such an array will be only a few inches (apart from the necessary supports). In a system of this size we would probably be using roughly 150 units. If the highest quality units were used such as those available for domestic hi-fi, the unit cost would be of the order of £1500, which must be considered in conjunction with a power handling capacity of about 2,250 watts, and a low-frequency efficiency of the order of 10%.

In practice it would not be necessary to use units of this quality throughout the entire array and it would therefore not be too difficult to build a very adequate system of similar performance for about a third of this figure. These figures are given only to indicate the order of the 'price per watt' economics of the approach.

When considering the efficiency, a further point is that the sound intensity derived from a multiple array tends to be independent of the distance of the listener from it under normal conditions of usage.

## Summary

The multiple-array system is an approach which renders it eminently suitable for sound reproduction in theatres, halls and auditoria in general. The efficiency is derived basically from the fact that the mass per unit area of diaphragm becomes progressively less for smaller loudspeaker units. The economics are favourable because the manufacturing costs tend to be lowest for 5in-6in loudspeakers. The reproduction quality is favoured by the fact that this size of loudspeaker sits most squarely upon the requirements necessary to reproduce the full audio range, and the relatively low mass per unit area and high values of air load offer very great advantages to transient reproduction. The ability to pre-design the sound distribution pattern makes it possible to tailor both the distribution and the frequency balance to the environment.

# Announcements

The latest Japanese electronics company to sign a licensing agreement with the London based EVR Partnership is Toshiba. The agreement gives Toshiba a non-exclusive licence for ten years to manufacture **EVR teleplayers in Japan** and sell them in all countries except the United States and Canada.

**Plessey Company Ltd** have acquired Arco Societa per L'Industria Elettrotecnica SpA of Italy, manufacturers of specialized electronic components.

**Leavers-Rich Equipment Ltd**, manufacturers of professional audio magnetic recording equipment, has been acquired by Mining and Chemical Products Ltd, the parent company of MCP Electronics Ltd.

**Carlingswitch**, of Watford, have signed a reciprocal sales agreement with **AMELEC**, of Paris, manufacturers of miniature rocker switches. The agreement gives Carlingswitch exclusive sales rights for AMELEC components in the U.K. with the French company having the same arrangement for Carlingswitch products in France.

**Joseph Lucas (Industries) Ltd**, of Birmingham, and **Robert Bosch GmbH**, of Stuttgart, have formed a joint company **Fluggeretechnik GmbH**, with headquarters in Stuttgart. The Bosch holding is 51%.

The **McMurdo Instrument Co. Ltd**, Rodney Road, Portsmouth, Hants, have signed an exclusive agreement with Alliance Technique Industrielle under which they are licensed to manufacture the French company's products in the U.K.

**Euro Electronic Instruments Ltd**, Shirley House, 27 Camden Road, London N.W.1, have been appointed U.K. representatives for **F. W. Bell Inc.**, of Columbus, Ohio, manufacturers of magnetic field measurement and generating equipment.

**Wentworth Instruments Ltd**, North Green, Datchet, Bucks., have been appointed exclusive U.K. and Ireland representatives for the products of Research Incorporated, of Minneapolis, U.S.A., manufacturers of the **Data-Trak programmer**.

**Electrautom Ltd**, 408 Finchley Road, London N.W.2, have been appointed sole U.K. agents by **Qualidyne Corporation** of Santa Clara, California, suppliers of semiconductor products.

For their metallized film capacitors **Advance Filmcap** have appointed Spenco Electronic Services Ltd. as manufacturer's agents for Northern Ireland and Scotland, and G.D.S. Sales Ltd., of Slough as franchised distributors for U.K. and Eire.

**Electronic Component Services (Worcester) Ltd**, of Victoria House, 63-66 Foregate Street, Worcester, have changed the name of the company to **Thorp Electronic Components Ltd**. The company have distribution agreements in the U.K. with The Belclere Co.; Unisem (United Aircraft) U.S.A.; Philco-Ford Microelectronics Division (U.S.A.); Emihus Microcomponents Ltd; AEG (Great Britain) and Semitron Ltd.

**B. Adler & Sons (Radio) Ltd**, Coptic Street, London WC1A 1NR, will in future be known as **Eagle International**. The company has marketed electronic products under the 'Eagle' brand name since 1958.

**Woollett Audiostatics**, 21 Anerley Station Road, London S.E.20, is a new company formed by L. G. Woollett to continue production of electrostatic and dynamic speakers. L. G. Woollett & Co. Ltd is now dissolved and superseded by the new company.

**Teleng Inc.** has been formed in the United States to market Teleng's TV distribution equipment for use in coaxial cable systems in North America.

**Microwave Associates Ltd**, of Luton, have received an order worth approx. £90,000 from the Malaysian Telecommunications Department for the supply of **mobile microwave links**. The MLV7000 equipment

operates in the 7GHz band and employs the heterodyne repeater principle which allows the transfer of information from link to link at a 70MHz i.f.

**GEC-AEI Telecommunications Ltd**, of Coventry, have received an order, worth over £1M, from the Post Office, to supply **microwave radio equipment** to expand the capacity of two radio trunk transmission routes in the national telecommunications network.

The Communications Division of **Redifon Ltd** has received an order valued at £230,000 for **radio beacon equipment** to modernize and extend Indonesia's system of aids to air navigation.

**Eddystone Radio** has received an order, worth over £60,000, to supply EC964 receivers to Televerkets Centralforvaltning, the central agency for supplying and installing maritime radio equipment in Sweden.

# Conferences and Exhibitions

*Further details are obtainable from the addresses in parentheses*

## LONDON

Mar. 16-19 Camden Town Hall

**Sound '71**  
(Assoc. of P.A. Engineers, 394 Northolt Road, South Harrow, Middx HA2 8EY)

Mar. 29-Apr. 2 Earls Court

**LABEX International**  
(U.T.P. Exhibitions Ltd, 36-37 Furnival St., London EC4A 1JH)

Mar. 30 & 31 Grosvenor House

**Training 71**  
(Marketing Exhibitions Ltd, 113/123 Upper Richmond Rd, London S.W.15)

Mar. 31-Apr. 4 Skyway Hotel

**SONEX 71**  
(Fed. of Brit. Audio, 49 Russell Sq., London W.C.1)

## BRISTOL

Mar. 23-26 The University

**EASCON 71—From learning to earning**  
(I.E.E.T.E., 2 Savoy Hill, London WC2R 0BS)

## HARROGATE

Mar. 2-4 Exhibition Hall

**EL-EC 71—Electronic Equip. & Components**  
(Trade News Ltd, Drummond House, 203-209 North Gower St., London N.W.1)

## NOTTINGHAM

Mar. 29-Apr. 2 The University

**Datafair 71**  
(Brit. Computer Soc., 29 Portland Pl., London W.1)

## OVERSEAS

Mar. 9-13 Basle

**MEDEX 71—Medical Electronics**  
(Sekretariat MEDEX 71, CH-4000 Basel 21)

Mar. 9-13 Basle

**INEL—Industrial Electronics**  
(Sekretariat INEL 71, CH-4000 Basel 21)

Mar. 9-14 Bordeaux

**OCEANEXPO 71**  
(Salon International de l'Exploitation des Oceans, 8, rue de la Michodière, Paris 2)

Mar. 14-23 Leipzig

**Leipzig Spring Fair**  
(Leipzig Fair, 701 Leipzig, Messehaus am Markt)

Mar. 22-25 New York

**I.E.E.E. Convention and Exposition**  
(I.E.E.E., 345 E. 47th St., New York, N.Y. 10017)

Mar. 29-Apr. 2 Paris

**Space and Communication**  
(L'Espac et la Communication, 16 rue de Presles, Paris 15<sup>e</sup>)

Mar. 31-Apr. 6 Paris

**Salon International des Composants Electroniques**  
(Fed. Nat. des Industries Electroniques, 16 rue de Presles, Paris 15<sup>e</sup>)

# Choosing a Vidicon

## Concluding the summary of tubes started in February

by D. J. Gibbons\*, M.A., Ph.D.

For many years it was appreciated that size, stability and ruggedness were all in favour of tubes based on the vidicon, in contrast to other types of pick-up tube. The requirements of high-quality colour cameras for live scene broadcasting place severe performance demands on the tube, however, and a number of lead oxide types have appeared (known by the registered trade marks as Plumbicon, Leddicon, Oxycon, etc.); particular characteristics of these types are low lag, low dark current and a linear light transfer characteristic. The special features of these vidicons can be attributed to a target fabricated so that there is a wide region of highly insulating oxide material lying between surface layers doped respectively n-type and p-type. Thus the target is very similar in construction to an array of reverse biased p-i-n photo-diodes. The Oxycon employs a mixture of metal oxides, including PbO, to yield tubes of similar characteristics to the Plumbicon and Leddicon but with shifted spectral response peaks.

### Slow-scan TV and light integration

Occasionally it is necessary to send a television signal over a narrow bandwidth link such as a normal speech telephone wire or a voice radio channel. The picture repetition rate must clearly be reduced under these conditions if detail is not to be lost, and a typical scanning time is between 15 seconds and 2 minutes. Under these unusual conditions the vidicon must be capable of holding the video information in the form of a charge pattern without degradation for considerably longer than normal. Vidicons with high target insulation for these purposes are supplied as 'slow-scan vidicons'. Some idea of their usefulness in such applications is gained from their dark current, because this is a measure of charge leakage within the target.

The high target insulation of these tubes also makes them well suited for light integration. If the light level is very low, then even one of the 'ultimate sensitivity' tubes listed in Table 3 may be incapable of yielding a useful signal because the information rate content of the image is too low. The signal/noise ratio can

TABLE 6 Lead Oxide Vidicons

Type No.	Scanning	Focus	Mesh	Colour response	Max. bulb dia. (mm)	Max. length (mm)	Resolution: modulation @400 TV lines	White light sensitivity $\mu\text{A/lumen}^*$	Applications or Colour channel
<b>Plumbicon Camera Tubes (Philips)</b>									
55875	M	M	I	Fig. 3 H	30.45	220	40%	> 275	L or U
55875R	M	M	I	Fig. 3 H	30.45	220	35%	> 60	R
55875G	M	M	I	Fig. 3 H	30.45	220	40%	> 125	G
55875B	M	M	I	Fig. 3 G	30.45	220	50%	> 32	B
55875-IG	M	M	I		30.45	220	40%	> 275	i, U, e. (c')
55875R-IG	M	M	I		30.45	220	35%	> 60	i, c', e, R
55875G-IG	M	M	I		30.45	220	40%	> 125	i, c', e, G
55875B-IG	M	M	I		30.45	220	50%	> 32	i, c', e, B
55876	M	M	I		30.45	220	30% at 625 lines	> 200	z
55876/01									
XQ1020	M	M	S	Fig. 3 H	30.45	220	40%	> 275	L or U
XQ1020L	M	M	S	Fig. 3 H	30.45	220	40%	> 275	L
XQ1020R	M	M	S	Fig. 3 H	30.45	220	35%	> 60	R
XQ1020G	M	M	S	Fig. 3 H	30.45	220	40%	> 125	G
XQ1020B	M	M	S	Fig. 3 G	30.45	220	50%	> 32	B
XQ1021	M	M	S		30.45	220	40%	> 275	i, e, c
XQ1021R	M	M	S		30.45	220	35%	> 60	i, e, c', R
XQ1021G	M	M	S		30.45	220	40%	> 125	i, e, c', G
XQ1021B	M	M	S		30.45	220	50%	> 32	i, e, c', B
XQ1022	M	M	S		30.45	214	30% at 625 TVL	> 200	z
XQ1023	M	M	S		30.45	220	55%	> 450	S, b, U
XQ1023L	M	M	S		30.45	220	55%	> 450	S, b, c, L
XQ1023R	M	M	S		30.45	220	55%	> 160	S, b, c, R
XQ1024	M	M	S	Fig. 3 J	30.45	220	700 TVL limiting	> 450	i, e
XQ1024R	M	M	S	Fig. 3 J	30.45	220	700 TVL limiting	> 160	c', R
XQ1025	M	M	S	Fig. 3 J	30.45	220	55%	> 450	U
XQ1025L	M	M	S	Fig. 3 J	30.45	220	55%	> 450	S, L, b, c
XQ1025R	M	M	S	Fig. 3 J	30.45	220	55%	> 160	S, b, c, R
XQ1026	M	M	S	Fig. 3 J	30.45	220	55%	> 450	S, i, e, c'
XQ1026R	M	M	S	Fig. 3 J	30.45	220	55%	> 160	S, i, e, c', R
XQ1070	M	M	S		26.6	159	30%	> 275	S, b, e, U, c'
XQ1070/01									
XQ1070L	M	M	S		26.6	159	30%	> 275	S, b, e, L, i, c'
XQ1070L/01									
XQ1070R	M	M	S		26.6	167	25%	> 60	S, c, R, i', b, e
XQ1070R/01									
XQ1070G	M	M	S		26.6	159	30%	> 125	S, c, G, i', b, e
XQ1070G/01									
XQ1070B	M	M	S		26.6	159	35%	> 32	S, c, B, i', b, e
XQ1070B/01									
XQ1071	M	M	S	Fig. 3 H	26	162	30%	> 275	L or U
XQ1071/01									
XQ1071R	M	M	S	Fig. 3 H	26	162	25% @ .2 $\mu\text{A}$	> 60	R
XQ1071/01R									
XQ1071G	M	M	S	Fig. 3 H	26	162	30% @ .4 $\mu\text{A}$	> 125	g
XQ1071/01G									
XQ1071B	M	M	S	Fig. 3 G	26	162	35% @ .2 $\mu\text{A}$	> 32	B
XQ1071/01B									
<b>Leddicon Camera Tubes (English Electric Valve Co.)</b>									
P8000	M	M	S		30.45	220	40%	> 275	S, U, b, c
P8000L	M	M	S		30.45	220	40%	> 275	S, L, b, c
P8000B	M	M	S		30.45	220	50%	> 32	S, B, b, c
P8000G	M	M	S		30.45	220	40%	> 125	S, G, b, c
P8000R	M	M	S		30.45	220	35%	> 60	S, R, b, c
P8000 IG	M	M	S		30.45	220	40%	> 275	c', U, e, r
P8000L IG	M	M	S		30.45	220	40%	> 275	c', L, e, r
P8000B IG	M	M	S		30.45	220	40%	> 32	c', B, e, r
P8000G IG	M	M	S		30.45	220	50%	> 125	c', G, e, r
P8000R IG	M	M	S		30.45	220	35%	> 60	c', R, e, r
<b>Oxycon Tubes (General Electrodynamics)</b>									
8861B	M	M		Fig. 3 G	26		650 TVL limiting	275	
8861E	M	M		Fig. 3 G	26		600 TVL limiting	275	
8861I	M	M		Fig. 3 G	26		550 TVL limiting	240	
8861C	M	M		Fig. 3 G	26		550 TVL limiting	116	

\*Research laboratories of EMI Ltd.

however be increased by exposing a slow-scan vidicon to the image for a few tens of seconds, integrating the charges corresponding to the signal on the target, and then scanning-off in a single shot. Provided that enough signal can be accumulated in this way to yield an output current of  $0.1\mu A$  in a single scan of 17-20ms, the signal/noise ratio will be nearly equal to that in the primary photo-charge; this will be more than 40 dB in a bandwidth of 3 MHz.

Signal integration can also be achieved with the SEC tube and the Ebitron (Tables 3 and 4).

**Integral focus and scanning coil vidicons**

In some specialized applications an advantage of space, ruggedness or power requirements may be achieved through the use of magnetic vidicons with built-in focus and scanning coils. Naturally, most of these advantages exist in the all-electrostatic vidicons but, with the possible exception of the high-resolution all-electrostatic vidicon, the resolving power of these tubes is inferior to that of the magnetic ones. Integral focus and scanning vidicons may consist of integral focus and scanning coils, or integral coils with permanent magnet alignment rings. They are all well suited for such applications as missile and spacecraft guidance, industrial and commercial surveillance systems and very compact cameras.

**Tubes responding outside the visible spectrum**

Choice of a suitable photoconductive target material produces a range of vidicons which are responsive to parts of the electromagnetic spectrum from 200 keV X-rays, through the soft X-ray region, the ultra violet, the visible and up to 2.4 microns in the infra red. Table 9 lists the relevant points for tubes of this type.

**Severe environmental conditions**

Most of the vidicons listed in Table 2 can be operated quite satisfactorily for short periods with faceplate temperatures between 60°C and 80°C. However, despite this capability, it is not recommended by any tube manufacturer that a vidicon camera is designed in such a way that the

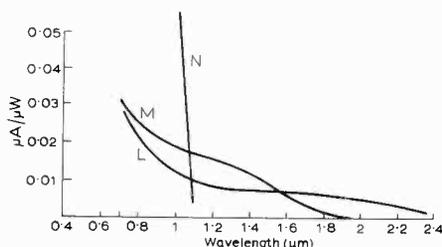


Fig. 5. Spectral sensitivity curves for vidicon targets responding to the infrared. Identification letters L, M and N refer to table 9.

**TABLE 6 Lead Oxide Vidicons—contd.**

Type No.	Scanning	Focus	Mesh	Colour response	Max. bulb dia. (mm)	Max. length (mm)	Resolution: White modulation light @400 TV lines	White light sensitivity $\mu A/lumen^*$	Applications or Colour channel
8865	M	M		Fig. 3 J	26.6	162	47%	153	
<b>Lead Oxide Vidicon (General Electric Co.)</b>									
Z7946	M	E	S	Fig. 3 H	26.1	161	40%		S
Z7869	M	M	S	Fig. 3 H	26.6	165	35%		c. e. S
Z7870	M	M	S	Fig. 3 H	26.6	165	40%		c. e. S
<b>Vistacon Camera Tubes (RCA)</b>									
4592/R	M	M	S	Fig. 3 J	30.45	220	25%	85	R. c
4592/G	M	M	S	Fig. 3 J	30.45	220	30%	140	G. c
4592/B	M	M	S	Fig. 3 J	30.45	220	35%	35	B. c
4592/L	M	M	S	Fig. 3 J	30.45	220	30%	350	L. c
4591/R	M	M	I	Fig. 3 J	30.45	220	25%	85	R. c
4591/G	M	M	I	Fig. 3 J	30.45	220	30%	140	G. c
4591/B	M	M	I	Fig. 3 J	30.45	220	35%	35	B. c
4591/L	M	M	I	Fig. 3 J	30.45	220	30%	350	L. c

Symbols: M—magnetic. E—electrostatic. I—integral. S—separate. R—red. G—green. B—blue. U—unichrome. c—colour. e—educational. S—development tube. L—luminescence. z—for viewing fluoroscope screens. c—industrial colour. b—broadcasting. i—industrial. r—reduced bluish specification.

¶ Identical with the same types without suffix/01 with the exception of having no anti-halation disc.

\* With colour filter in position. No filter is used for monochrome pictures or in the luminance channel.

**TABLE 7 Slow-scan Vidicons**

Type No.	Manufacturer	Scanning	Focus	Mesh	Dark current
E2800	Heimann	M	M	S	—
TH9892	TH-CSF	E	M	S	5nA
WL7290 (WX5424)	Westinghouse	M	M	I	0.2nA
WX4887 (WX4885)	Westinghouse	M	M	I	0.2nA
WX5111 (WX5113)	Westinghouse	M	M	S	0.2nA
WX5115 (WX5117)	Westinghouse	M	M	S	0.2nA
WX4950 (WX5119)	Westinghouse	M	E	S	0.2nA
WX5120 (WX5121)	Westinghouse	M	E	S	0.2nA
WX4384 (WX4871)	Westinghouse	E	E	S	0.2nA
WX4890 (WX5118)	Westinghouse	E	E	S	0.2nA
9728 UV	EMI	M	M	S	0.5nA
(9737)	EMI	M	M	S	less than 1nA at 70°C
9677 UV	EMI	M	M	S	0.5nA
4500	RCA	M	M	I	5nA
(TD1342)	GEC	M	M	S	0.5nA
(TD1368-010)	GEC	M	M	I	0.2nA

Symbols: M—magnetic. I—integral. E—electrostatic. S—separate.

Types in brackets are ruggedized military types with a low wattage heater.

See also tables 3 and 4 for the SEC tubes and the Ebitron which can be used in some slow scan applications.

**TABLE 8 Vidicons having integral focus and scanning coils**

Type No.	Manufacturer	Dia. incl. coils, mm	Bulb dia. mm	Length mm	Resolution* TVL
C23133	RCA	32	26	S	—
F4079A	ITT	32	20	S	104
Z7960	GE	17.8	16	S	700

\* Limiting resolution in centre.

Symbols: S—development type.

**TABLE 9 Vidicons Responding Outside the Visible**

Type No.	Manufacturer	Applications	Long wavelength limit	Short wavelength limit
E2900	Heimann	X-ray		
TH9890	TH-CSF	i.r.	2.4 microns (Fig. 4 L)	
* TH9891	TH-CSF	u.v.	0.7 microns (similar to Fig. 3 E)	240
TH9896	TH-CSF	X-ray	Less than 20keV X-rays **	30-200keV X-rays
9677UV	EMI	u.v.	0.61 microns (Fig. 3 curve E)	210
9728UV	EMI	u.v.	0.61 microns (Fig. 3 curve E)	210
2000	Heimann	i.r.	1.8 microns (Fig. 4 M)	350
P842IR	EEV	i.r.	1.8 microns (Fig. 4M)	
N156	Hamamatsu	i.r.	2.4 microns (Fig. 4 L)	400
*** N157				
† N177				
†† N214				
†*** N248	Hamamatsu	X-ray	Soft X-rays	Hard X-rays
N350				
†† N400				
TD1307—007	GEC	i.r.	1.8 microns (Fig. 4 M)	400

\* Shorter tube than TH9890. \*\* Tubes for hard and soft X-rays are manufactured with differing end-windows.

\*\*\* Shorter tube than N156, N177 & N214. † All electrostatic. †† High resolution. S Provisional; EEV make all their range of vidicons with this photosurface to special order.

N.B. See also the silicon vidicon (Figs. 3J and 4N Table 14), which has a long wavelength cut-off at 1.1 microns.

**TABLE 10 Vidicons Specially for Severe Environmental Conditions**

Type No.	Manufacturer	Scanning	Focus	Mesh	Max. bulb dia. (mm)	Length (mm)	Special features	Applications
9677Q	EMI	M	M	S	26.6	159	Quartz faceplate	f
9738Q	EMI	M	M	S	13	92.8	Quartz faceplate, ruggedized	f, R
9728Q	EMI	M	M	S	26.6	159	Quartz faceplate	f
C74153	RCA	M	M	I	26	132	Radiation resistant faceplate	f, S
TH9808N	TH—CSF	M	M	S	26	165	Non-browning radiation glass	f
TH9813N	TH—CSF	M	E	S	26	165	Non-browning radiation glass	f
TH9813RN	TH—CSF	M	E	S	26	165	Non-browning glass and internal reticule	f
TH9813PN	TH—CSF	M	E	S	26	165	Non-browning; high pressure environments up to 100 bars	f, v
C2316	RCA	M	M	S	26	161	Silicon target	O, S
P864	EEV	M	M	S	26	162	Radiation resistant faceplate	f, S
2255SF	Heimann	M	M	S	26	164	Radiation resistant faceplate	f

N.B. Most manufacturers produce ruggedized vidicons suitable for conditions of high vibration or mechanical shock. These are to be found marked "R" in all other tables except Table 6, where this symbol has a different meaning. Symbols: O—Resistant to over-exposure. f—nuclear radiation. v—high pressures. I—integral. S—separate. M—magnetic. E—electrostatic. R—ruggedized. S—development type.

**TABLE 11 Small Diameter Vidicons**

Type No.	Manufacturer	Scanning	Focus	Max. bulb dia. (mm)	Applications and/or special features
4427	RCA	M	M	13.0	w, i
C23104	RCA	M	M	13.0	S, S
C23134	RCA	M	M	20.3	S, Diameter over integral coils 32 mm.
1135	Heimann	M	M	13.5	—
Z7968	GE	M	E	—	S, R, w, diameter over integral coils 18 mm.
9737	EMI	M	M	13.2	Unity gamma; fine grain target w
9738	EMI	M	M	13.2	S, w
9738Q	EMI	M	M	13.2	Q, w, S
9738N	EMI	M	M	13.2	R, w
9768	EMI	E	E	13.2	w: 15.25 mm. dia. oversheath. Spectral response 3C.
9838	EMI	M	M	13.2	S, w; spectral response 2D
9868	EMI	E	E	13.2	w, S; 9768 but with spectral response 2D.
F4079A	ITT	M	M	20.5	31.7 mm. over integral coils, S
F4079	ITT	M	M	20.5	—
NEC 4427	NEC	M	M	13.0	w, i
8823	Hitachi	M	M	20.3	w, i: spectral curve D

Symbols: i—industrial cameras. M—magnetic. E—electrostatic. w—small lightweight cameras. Q—quartz faceplate (also see Table 10). S—separate mesh. S—development type. R—ruggedized.

**TABLE 12 Developmental Return Beam Vidicons**

Type No.	Manufacturer	Dia. (mm)	Resolution	Lag
C23061A	RCA	52	45% @ 2000 TV lines	extended
C74137A	RCA	115	5000 limiting	low

**TABLE 13 Monoscopes**

Type No.	Manufacturer	Scanning	Focus	Screen
9788	EMI	E	E	Alphanumeric. 64 symbols. ASC11-2 (Fig. 6b)
TH9503	TH—CSF	M	E	Alphanumeric. 64 symbols. or 128
TH9504	TH—CSF	M	M	Alphanumeric. 64 symbols. or 128
TH9505	TH—CSF	E	E	Alphanumeric. 64 symbols
TD1350-001	GEC	* M	M	Linearity pattern
TD1350-002	GEC	* M	M	Registration pattern (& Fig. 6a)
TD1350-003	GEC	* M	M	Resolution burst pattern; white on black
TD1350-004	GEC	* M	M	Resolution burst pattern; black on white
TD1350-005	GEC	* M	M	Slant line burst pattern.

\* Photoconductive target with internal reticule pattern.

In addition to the above tubes, which are intended primarily for generating a television signal from an internal source, RCA, TH—CSF and EEV advertise vidicons with a built-in internal reticule. Various patterns are available, intended mainly for easing any problems of lining-up the tube in special applications.

**TABLE 14 Silicon Target Vidicons**

Type No.	Manufacturer	Length (mm)	Notes
C23136	RCA	161	q, S
VID-136	Texas	121 or 133	S
VID-127	Texas	121 or 133	S
VID-128	Texas	121 or 133	S
VID-129	Texas	121 or 133	S, r
LD 6001	NEC	161	S
P8010	EEV	—	S
P8011	EEV	—	S

Symbols: S—development tube available on sampling basis. q—extra high picture quality. r—relaxed blemish specification.

faceplate temperature rises above 30-35°C, under typical operating conditions. In some cases forced air cooling may be necessary and if a vidicon camera is used to observe furnaces etc. a heat-absorbing or infra red filter should be interposed between the tube and the source of heat. Accidental or short term exposure up to the absolute maximum recommended faceplate temperature will not cause any harm. Lead oxide types should not be operated with the faceplate above 50°C. Corresponding temperatures for slow-scan and infra red types are 45-50°C and 30-35°C respectively. The silicon types will operate up to 200°C and ultra violet vidicons at 70°C.

Under conditions of high vibration, or in a missile or a spacecraft, tube microphony may be troublesome unless one of the special ruggedized vidicons is used. All tubes in Table 2 marked "R" come in this category, as well as a few others to be found in tables elsewhere also marked "R".

Naturally, all vidicons can be used to eliminate human risks, as well as to perform functions which would be impossible for the unaided operator. Some tubes are manufactured specially for use in areas of high nuclear radiation density. These are made with a special 'non-browning' glass or a quartz faceplate, and represent particularly good examples of vidicons which can be employed in conditions which would be very dangerous for a human operator.

Another special vidicon is made to withstand high pressures. All vidicons can be operated in vacuo. The silicon vidicon is remarkably free from risk of damage by accidental exposure to bright objects through the camera, and from damage through underscanning with the electron beam; thus electronic 'zoom' is possible with this tube.

**Small diameter vidicons**

A very important feature of the vidicon is its ability to 'look' into a place where a human operator cannot. There are two ways of doing this; one is to use a flexible fibre-optic 'light pipe' coupled to a fibre-optic tube (Table 3), and the other is to use a small diameter vidicon. The smallest diameter cameras employ the all-electrostatic 13mm diameter tube which needs no bulky scanning and focus coils; at present such cameras have only been proved at an experimental stage. One important use for small diameter vidicons is the detailed examination, without dismantling, of power station boiler pipes for scale formation, but these tubes are useful in all situations where space is at a premium.

**Silicon target vidicon**

A conventional vidicon construction employs in this version a silicon p-i photoconductive diode array, using microcircuit photolithographic techniques to produce a target containing 50,000 or more isolated photo-diodes. Only four companies so far have issued provisional

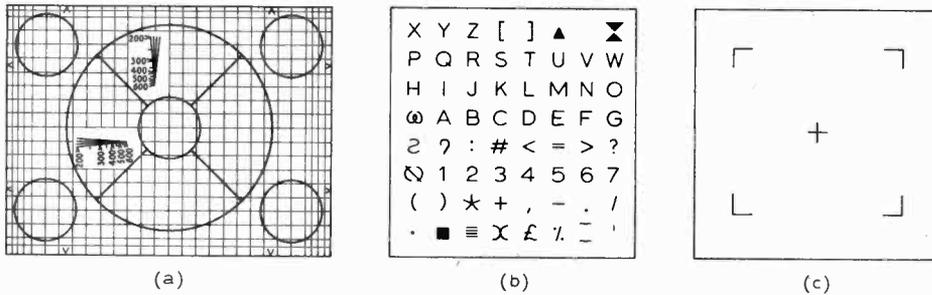


Fig. 6 Representative target patterns of vidicon-based monoscopes and vidicons with permanent internal target patterns: (a) registration chart (GE); (b) Printicon (EMI) or Scriptor (TH-CSF); (c) internal reticule (RCA, EEV or TH-CSF).

specifications for this tube, whose main features are a spectral response extending from 350 or 450 nm to 11,000 nm, a high sensitivity to normal tungsten lighting, and a target virtually immune to damage even when inadvertently exposed to bright sources such as the sun ( $10^8$  lx on the target).

### Return beam vidicons

Utilizing the electron beam for discharging the pattern containing the picture information on the target, and also for its evaluation, invariably leads to a compromise. If the beam current is small, high resolution is possible but picture lag may occur. If the beam current is high, lag is minimized for a given kind of target photoconductor, but a lower resolution results. In the return-beam vidicons a small beam current can be used for evaluation of the charge pattern on the target, and an electron multiplier can be incorporated in a similar way as in the image orthicon, to give virtually noise-free amplification of the video signal before it is passed on to the amplifier. Unlike other vidicons, the 'noise' occurs in the picture blacks. The result of this special design is to yield a tube of remarkably high resolution, as may be seen in Table 12.

### Monoscopes

There are several tubes for generating special patterns. An internal target is used to generate a pre-determined signal, which may be an alphanumeric character for a computer readout monitor (Printicon, or Scriptor), or a pattern for making geometrical accuracy tests for TV system testing. Alternatively the internal pattern is built in on a photoconductive layer (Reticon, or vidicons with an internal reticule). In this type, lens optics are not needed to generate a test pattern but, if necessary, an external test pattern can be superimposed on the internally generated reticule. Fig. 6 gives some idea of the kind of internal patterns which are available in Reticons, Printicons or Scriptor and in vidicons with an internal reticule.

**Acknowledgements.** The author would like to thank all people who provided information for this article. It is a pleasure to thank Mr. S. Taylor for preparing Figs. 2, 3 and 5. The permission of the directors of Electric and Musical Industries for publication is gratefully acknowledged.

### MANUFACTURERS' NAMES AND ADDRESSES

On the left are abbreviations used in the tables. Only the head office addresses are given. All manufacturers have agents or representatives in major countries.

	Amperex Electronics Corp., 230, Duffy Avenue, Hicksville, New York, U.S.A.
EMI	EMI Electronics Ltd., Electron Tube & Microelectronics Division, Hayes, Middlesex, England.
EEV	English Electric Valve Co. Ltd., Chelmsford, Essex, England.
GE	General Electric Co., Imaging Devices Operation, Syracuse, New York, U.S.A.
GEC	General Electrodynamics Corp., 4430 Forest Lane, Garland, Texas 75040, U.S.A.
Hamamatsu	Hamamatsu TV Co. Ltd., 1126, Ichino-cho, Hamamatsu City, Japan.
Heimann	Heimann G.m.b.H., 620 Wiesbaden-Dotzheim, Germany.
Hitachi	Hitachi Ltd., 4, 1-chome, Marunouchi, Chiyoda-ku, Tokyo, Japan.
I.T.T.	I.T.T., Electron Tube Division, 3700, East Pontiac Street, Fort Wayne, Indiana 46803, U.S.A.
	Matsushita Electronics Corp., 1006, Oaza Kadoma, Kadomashi, Osaka, Japan.
Mullard	Mullard Ltd., Mullard House, Torrington Place, London, WC1E 7HD.
NEC	Nippon Electric Co. Ltd., Tokuei Building, 33-7, Shiba Gochome, Minato-ku, Tokyo, Japan.
Philips	Philips Electric Industries Ltd., Electronics Components and Materials Division, Eindhoven, Holland.
RCA	RCA Corporation, Electronics Components Division, 5415, S. 5th Street, Harrison, New Jersey, U.S.A.

R.T.C. La Radiotechnique-  
Compelec,  
51, rue Carnot,  
92—Suresnes,  
France.

Shiba Electric Co. Ltd.,  
Hibiya-Kaidan Building,  
20, 2-chome,  
Uchisaiwai-cho,  
Chiyoda-ku,  
Tokyo, Japan.

Siemens AG,  
8 München 8,  
Balanstrasse, 73,  
Germany.

Texas

Texas Instruments Inc.,  
Dallas, Texas,  
U.S.A.

TH-CSF

Thomson-CSF/DTE,  
Groupement Tubes Electroniques,  
8 rue Chasseloup-Laubat,  
75, Paris 15,  
France.

Thor Electronics Corporation,  
741, Livingston Street,  
Elizabeth,  
New Jersey, U.S.A.

Westinghouse

Westinghouse Electric Corp.,  
Electronic Tube Division,  
Box 284, Elmira,  
New York, U.S.A.

Young Electronique,  
117, rue d'Aguesseau,  
92—Boulogne, Billancourt,  
France.

## Semiconductor Reference Book

The fifth edition of *The Semiconductor Data Book* from Motorola is 'designed to serve four specific functions: 1, to permit quick identification of any semiconductor device having an E.I.A. registered 1N . . . , 2N . . . , 3N . . . , number or special Motorola in house number; 2, to permit quick selection of preferred devices for particular circuit applications; 3, to permit quick selection of preferred devices that best meet a desired set of electrical specifications; and 4, to provide complete design data for all Motorola discrete semiconductor devices.' The book is divided into four sections, the first three covering the above purposes, and the fourth providing the case dimensions of all packages described. Also included in the book are condensed specifications for all Motorola integrated circuits. Pp.2546. Price £3 plus 30p post and packing from Modern Book Company, 19 Praed Street, London W.2.

# Diode Switching Using Charge Analysis

## Explanation of simple charge control model of diode for students and engineers

by B. L. Hart\*, B.Sc., M.I.E.R.E.

**Charge storage models of semiconductor devices allow circuit design work to be done without involved mathematics. The author maintains that an appreciation, and consequent modelling, of the p-n junction is basic to an understanding of transistors and other multi-junction devices. The review develops, and explains the application of, a simple diode charge model for switching circuits. It assumes only an elementary knowledge of calculus.**

In the days when thermionic valves were the workhorse of the pulse circuit engineer there was often little need, or inclination, to "look inside" the device. For most practical applications its behaviour was adequately represented by the d.c. characteristics and a knowledge of (constant) inter-electrode capacitances. The arrival of junction diodes and transistors presented some circuit phenomena not readily explained in terms of d.c. characteristics and capacitances, for example the reverse current flow in a forward biased diode and saturation effects in a transistor. It was then necessary to probe deeper into the physical electronics of device operation for state-of-the art circuit designs. This led to the development of various device models.

For many semiconductor devices the best models—those giving insight into device operation and permitting evaluation of their circuit potentialities with a minimum of mathematical complexity—are those which involve the concept of charge stores. The object of this article is to review the development and application of a simple diode charge model suitable for switching circuits and in doing so to clarify some important concepts in semiconductor device operation which appear to be shrouded in mystery for many practising engineers.

### Basic concepts

In Fig. 1, the p region of the junction has a uniform concentration,  $N_A$ , of fully ionized

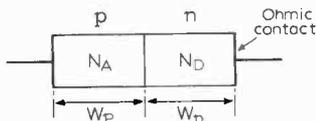


Fig. 1. Basic p-n junction diode. Text explains how charged layer is formed.

"acceptor" impurities whereas the n region has a uniform concentration,  $N_D$ , of fully ionized "donor" impurities. This assumes

$N_A \gg N_D$ , and the transition from one polarity of semiconductor material to the other is abrupt or occurs over a very short distance. Such a structure, with ohmic contacts attached to the p and n regions constitutes a junction diode. When the junction is left open-circuited the free carrier concentration gradient across the junction causes charges (holes) which are in the majority of the p region to diffuse to the n region where they become minority carriers.

Similarly those carriers (electrons) which are in the majority in the n region diffuse into the p region to become minority carriers. The diffusion process leaves some uncovered charges in the crystal lattice structure, either side of the metallurgical junction, where mobile "shadow" charges of majority carriers previously ensured local charge neutrality. As a result a dipole layer of charge is formed.

Associated with this is a "barrier" or

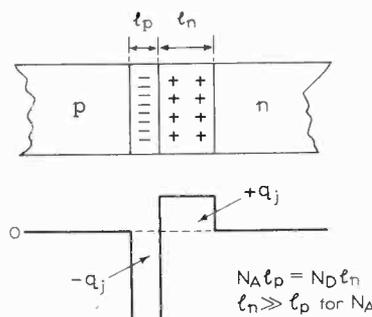


Fig. 2. Charge distribution in depletion region.

built-in potential,  $\phi$ . This causes hole and electron drift currents of such magnitude and direction that the net hole current resulting from drift and diffusion and the net electron current resulting from drift and diffusion are both zero—as must be the case for an open-circuited device. Little conceptual error is involved in assuming that the dipole layer has a rectangular charge distribution—see Fig. 2—sandwiched between the neutral bulk of the p and n

regions. Because of the absence of covering charge the name depletion region is given to the volume bounded by the dipole layer: another description is transition region.

Application of a steady forward bias, i.e. p region made positive with respect to n region, causes two effects. First, a change in the width of the depletion layer to accommodate the applied voltage and second, an enhanced injection of carriers from one region to the other.

### D.C. conditions

In the carrier injection process, the establishment of a forward bias voltage  $V$  causes the minority carrier density in the n region immediately adjacent to the depletion layer to increase from its equilibrium value  $P_{no}$  (a function of  $N_D$ , material type, and temperature) to a value  $P_n(x=0)$  where

$$P_n(0) = P_n(x=0) = P_{no} \exp V/V_T \quad (1)$$

in which  $V_T$  is the thermal voltage, approximately 26 mV at room temperature. Rewriting eqn 1 in terms of the excess minority carrier density,  $P_n'(0)$  gives

$$P_n'(0) = P_n(0) - P_{no} = P_{no} \{ \exp(V/V_T) - 1 \} \quad (2)$$

Eqn 1 may be justified by a thermodynamic argument beyond the scope of this article.

The metal contact has the property of being able to maintain at zero the hole density at  $x = W_N$  however many holes reach it. There will thus be a concentration gradient set up in the n region for holes which therefore diffuse towards the n contact. Some recombine with electrons in the process, the recombination rate, in an elemental volume situated at distance  $x$  from the junction, being proportional to the excess level  $P_n'(x)$  there.

The shape of the  $P_n'(x)$  curve is dependent on the ratio  $W_N/L_H$  where  $L_H$  is the average distance travelled by a hole before recombining. If  $W_N/L_H \gg 1$ , as in the so-called long-base diode, all the excess minority carriers recombine before reaching the contact and the curve is a decaying exponential—see Fig. 3(a). If  $P_n(0) \ll N_D$  the condition known as low-level injection holds and there is no significant field in the n region. Drift can thus be ruled out as a transport mechanism for holes. Since diffusive flow depends on the concentration gradient, the slope of  $P_n'(x)$  at  $x = 0$ , where recombina-

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tion has not yet taken its toll, is proportional to the diode current  $I$  which would be measured on a d.c. instrument connected at the diode terminals. Thus  $I \propto dP_n'(x)/dx$ . The area under the  $P_n'(x)$  curve gives the excess minority carrier charge  $Q$  stored in the diode or the excess minority-carrier charge in transit.

For simplicity the electrons injected from the n to the p region are ignored. The initial choice  $N_A \gg N_D$ —realistic for most usable devices—allows this without introducing any major quantitative error.

Understanding of diode action will not be clear unless the behaviour of the n region majority carriers is considered. In this context the material type and doping levels found in modern semi-conductors is such that the assumption of charge neutrality is a valid approximation independent of the time scale under consideration. Thus the injection of a hole from the p to n region is accompanied by the simultaneous injection of an electron into the n region at the n metal contact.

The increase in excess minority carrier charge to a level  $(+Q)$ , corresponding to a current  $I$ , is matched by the injection of electrons of amount  $(-Q)$  at the n contact. The carrier distributions run parallel, shown

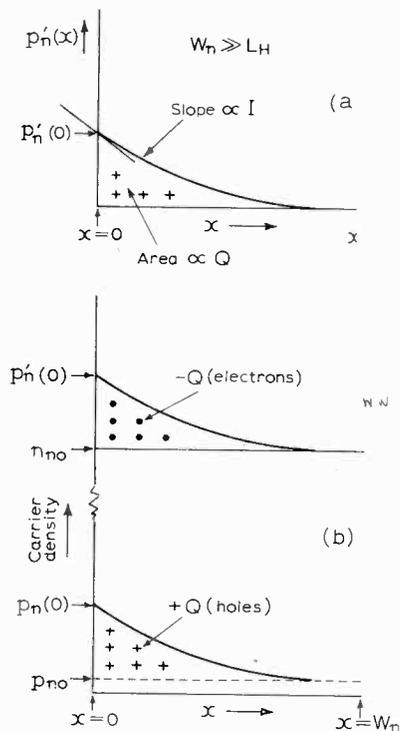


Fig. 3. (a) In long-base diode ( $W_n \gg L_H$ ) excess minority carriers recombine before reaching contact and curve decays exponentially. (b) Injected holes (charge  $+Q$ ) in n region are matched by injection of electrons to amount  $-Q$ .

in Fig. 3(b), and there is no significant voltage drop associated with the two intermingled sets of charges. The word "significant" is important here: there will be a small voltage drop (measured in  $\mu V$  or  $mV$ ) due to the electron drift current flowing through the bulk of the semiconductor lattice. If  $W_n \gg L_H$ , the diode current  $I$  is composed of electron drift current, only, near the n contact. Hence the longer the n

region the greater the voltage drop due to the bulk resistance.

The relationship between  $Q$  and  $I$  is interesting. The bulk minority carrier lifetime,  $\tau$ , is the average time that an excess carrier (in this case a hole) exists before recombining. This is obviously related to  $L_H$ , defined above. A charge  $Q$  would disappear in a time  $\tau$  unless supported by a steady current  $I$ . Hence

$$I = Q/\tau \quad (3)$$

A formal mathematical treatment of the physical ideas discussed yields

$$Q = I_0\tau\{\exp(V/V_T) - 1\}$$

$$\text{or } Q \propto P_n'(0) \quad (4)$$

in which  $I_0$  is the magnitude of the reverse saturation current of the diode. Eqn 4 obviously embodies eqn 2 and is a restatement in charge form of the standard diode equation.

Rewriting eqn 4 gives

$$V = V_T \log_e \{1 + (Q/I_0\tau)\} \quad (5)$$

Under d.c. conditions eqns 3, 4 and 5 tell no more than the normal diode equation and the introduction of charge as a variable might seem to unnecessarily complicate the description. This is not the case with behaviour in the transient state.

**Transient conditions**

A change in diode current is associated with a change in applied voltage. This is accompanied by two effects: a change in the magnitude of  $Q$ , and a change in the width of the depletion layer.

Taking the change in  $Q$  first, a change  $\delta q$  in stored charge in a time  $\delta t$  requires a current component  $\delta q/\delta t$  in addition to  $q/\tau$ , required to combat recombination which is always occurring. Thus if  $i_1$  is the current into the n region then in the limit as  $\delta t$  tends to zero,

$$i_1 = \frac{dq}{dt} + \frac{q}{\tau} \quad (6)$$

This equation is exact, depending only on charge neutrality, and does not depend on the spatial distribution of injected carriers. Obviously eqn 6 reduces to 3 under d.c. conditions.

The depletion layer is narrowed by supplying majority carriers at its edges from the adjacent bulk of neutral semiconductor. The process resembles the charging of a parallel plate capacitor  $C_j$  with plates spaced  $(l_p + l_n)$  apart—see Fig. 4. The current required for this is  $i_2$ , say, where

$$i_2 = \frac{dq_j}{dt}$$

As the two processes are happening at the same time the total instantaneous diode current  $i$  is

$$i = i_1 + i_2 = \frac{dq}{dt} + \frac{q}{\tau} + \frac{dq_j}{dt} \quad (7)$$

We cannot go further, quantitatively, without introducing a fundamental assumption.

It is possible to obtain an exact answer to problems involving transients in semi-conductors by solving the time-dependent diffusion equation for injected minority

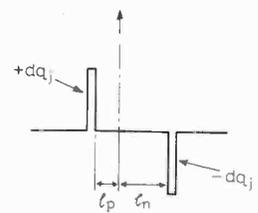


Fig. 4. Depletion layer is narrowed by injecting majority carriers at its edges from adjacent neutral semiconductor, process resembling charging a parallel-plate capacitor with plate separation of  $l_p + l_n$ .

carriers. But the objective here is to derive a simple model giving physical insight into device operation and an accuracy sufficient for circuit calculations.

The basic assumption made is that in changing from one current level to another the curve for  $P_n'(x)$  goes successively through the steady state values which would exist if the change took a (theoretically) infinite time. Thus in Fig. 5 the curve for  $(t + \delta t)$  is

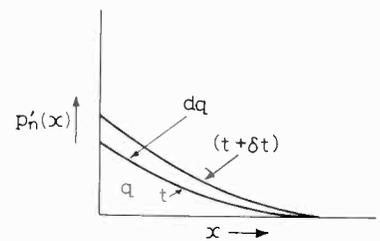


Fig. 5. Shows movement of minority charge during transient, where curves are assumed to be same shape.

the same shape as that for  $t$  irrespective of the magnitude of the time increment  $\delta t$ . Clearly we anticipate trouble with this assumption—in view of the finite velocity of carriers—as  $\delta t$  becomes very small.

The assumption allows eqns 4 and 5 to be generalized for minority carriers so that for  $q > 0$

$$v = V_T \log_e \{1 + (q/I_0\tau)\} \quad (8)$$

Eqn 7 in conjunction with 8 now yields the  $i-v$  characteristic in the transient state.

Before drawing a circuit model for a diode consider further the depletion capacitance  $C_j (= dq_j/dv)$ . This is normally a non-linear function of  $v$  though it is possible to design diodes in which the non-linearity is not very pronounced. Usually

$$C_j(v) = C_j(0)/\{1 - (V/\phi)\}^n \quad (9)$$

where  $C_j(0)$  is the capacitance at zero bias, and  $n \approx \frac{1}{2}$  for abrupt junction,  $\frac{1}{3}$  for a graded junction.

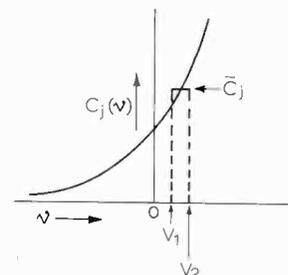


Fig. 6. Non-linearity of depletion capacitance  $C_j$  can be linearized by finding average volume of  $C_j$  graphically.

The non-linearity expressed by eqn 9 can be a nuisance for some purposes and little error is involved in linearizing the capacitance. This is a technique of general use with semiconductor devices and involves finding an average value of  $C_j$ , by calculation or graphically, which displaces the same charge for a specified voltage change as does the non-linear capacitance. Thus

$$\bar{C}_j = \left| \int_{V_1}^{V_2} C_j(v) dv / (V_2 - V_1) \right|$$

This is illustrated in Fig. 6.

**Diode model**

Fig. 7 is the model<sup>1</sup> which summarizes, pictorially, the results of the arguments and associated equations. The network symbol<sup>2</sup>  $S$ , reminds us of the current  $dq/dt$  required when the diode stored charge  $q$  changes: current generator  $q/\tau$  describes the recombination process. There is no voltage drop associated with the store for reasons discussed: all the applied voltage drop  $v$ , given in terms of  $q$  by eqn 8, appears across the depletion layer and is shown on the diagram as a voltage generator. (It could be represented by a conventional diode symbol but this might be confusing as there is no generally accepted symbol for a diode with no inherent stored charge.)

The switch enables use of one model for two conditions of operation,  $q > 0$  (switch closed) and  $q < 0$  (switch open).

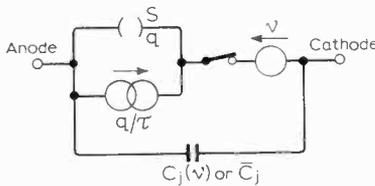


Fig. 7. Charge model of p-n junction diode used to interpret circuit behaviour of diode.

There are four points in using the model which merit specific attention

- for  $q > 0$ , a decade change in  $q$  results, via the logarithmic relationship of eqn 8, in only 60 mV change in  $v$ . Thus in many cases  $C_j(dv/dt) = (dq_j/dt) \ll (dq/dt)$ , and eqn 7 reduces to 6
- for  $q < 0$ ,  $dq_j/dt$ , i.e.  $C_j$ , only need be considered
- a small resistance,  $r_x$ , allowing for bulk drops, may be put in series with the anode or cathode lead
- although a number of seemingly restrictive assumptions were made in the development of the model it has general use subject to our basic assumptions (charge neutrality and instantaneous charge rearrangement so that  $q(t) \propto P_n'(0,t)$ ).

The effects of non-uniform impurity distribution, gold doping (for minority carrier lifetime reduction) and high-level injection are to alter the magnitudes but not position of the components comprising the model.

**Diode circuit behaviour**

The model is now used to interpret circuit behaviour for two drive conditions. A short

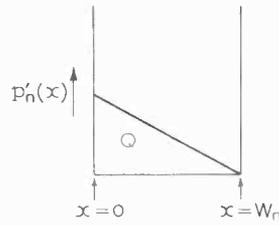


Fig. 8. Excess minority carrier distribution for short-base diode, used in fast switching circuits, interpreted in text with Figs. 9 and 10.

base diode, i.e. one having  $(W_N/L_{II}) \ll 1$ , is frequently used in fast switching circuits and is considered here. The injected minority carrier distribution, shown in Fig. 8 approximates a straight line. For a given diode current (and a corresponding slope at  $x = 0$ ), the stored charge  $Q$  is obviously less than for the case of a long-base diode—Fig. 3(a). The lifetime of the excess minority carriers is no longer the bulk lifetime  $\tau$  but has now a much smaller effective value  $\tau_D$  dependent on  $W_N$  and hole diffusion constant.

Suppose the diode is passing a steady forward current,  $I_F$ , and this is suddenly reduced to zero, by opening the switch in

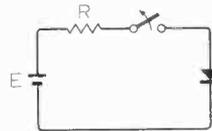


Fig. 9. Behaviour of diode anode voltage when diode forward current is cut off by opening switch can be found from model in Fig. 10.

Fig. 9. The subsequent behaviour of the diode anode voltage may be found from the model shown in Fig. 10, in which  $r_x$  is the diode bulk resistance. As  $I_F$  is instantaneously removed, the anode voltage will fall from its initial value by an amount  $I_F r_x$ . As the diode is open-circuited there is no exit path for excess carriers and these can only die by recombination in the diode, i.e. the store  $S$  is discharged by a current  $q/\tau_D$ , so that ignoring  $C_j$  for reasons already discussed

$$\frac{dq}{dt} = -\frac{q}{\tau_D} \quad (10)$$

This is justified if

$$|C_j(dv/dt)| \ll |q/\tau_D| \quad (11)$$

Now from eqn 8, for  $q/\tau_D I_0 \gg 1$ ,  $v \approx V_T \log_e(q/\tau_D I_0)$ . Hence

$$dv/dt = V_T/q \quad (12)$$

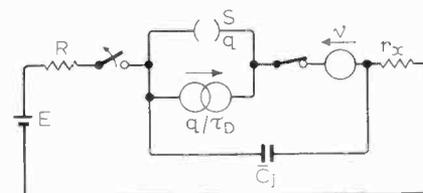


Fig. 10. When switch is opened, anode voltage of diode falls by  $I_F r_x$  and excess carriers stored in  $S$  are recombined in the diode, i.e., discharged by current  $q/\tau_D$ .

From equations 10 and 12

$$\frac{dv}{dt} = \left( \frac{dv}{dq} \right) \left( \frac{dq}{dt} \right) = -\frac{V_T}{\tau_D} \quad (13)$$

Eqn 13 is true for  $\bar{C}_j V_T \ll q$  as may be verified by substituting eqn 13 in 11. Thus a linear fall in  $v$  for  $q/\tau_D I_0 \gg 1$  is expected, after which the fall in  $v$  would cease to be linear.

Fig. 11 shows the practical circuit for tests on a germanium switching diode. Diodes  $D_1$  and  $D_2$  have no significant carrier

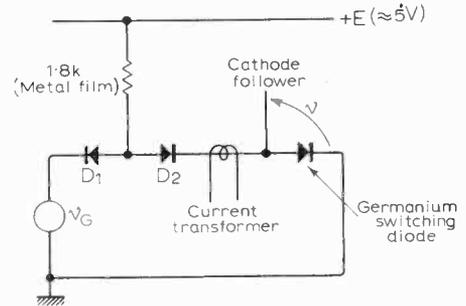


Fig. 11. Practical circuit for open-circuiting test on germanium switching diode. Diode current and voltage waveforms are observed with a current transformer and a high-impedance cathode follower feeding a sampling oscilloscope.

storage. The input gating pulse  $V_G$  is supplied from a pulse generator having a zero offset facility, while the diode current and voltage waveforms are observed using, respectively, a wideband current transformer and a wideband high-impedance, cathode follower feeding a sampling oscilloscope.

Initially  $D_1$  is cut off and the two other diodes conduct a forward current  $I_F$  (chosen in this instance to be 2.5 mA). Subsequently  $D_1$  is switched on and current in  $D_2$ —observed by the current transformer—rapidly falls to zero. The diode voltage waveform is shown in Fig. 12. An initial under-

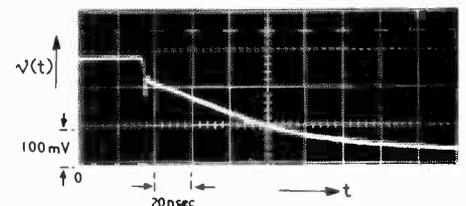


Fig. 12. Anode voltage waveform for diode in circuit of Fig. 11. When  $D_1$  is switched on current in  $D_2$  falls to zero. Undershoot is due to capacitive coupling of gating voltage across  $D_2$ . Voltage step indicates  $r_x$  is 25Ω. Text explains how diode supports reverse current while still forward biased.

shoot is attributed to capacitive coupling of  $V_G$  across  $D_2$ . Ignoring this the voltage step indicates a  $r_x \approx 25\Omega$ . There is a region over which  $dv/dt \approx$  constant and assuming  $V_T = 25$  mV a calculation based on eqn 13 gives  $\tau_D \approx 12.5$  ns.

Now the current in a diode is not usually suddenly reduced to zero but assumes a reverse value, as in some logic gate applications. The reason the diode is able to support a reverse current flow while still forward biased is as follows.

When a step of reverse current  $I_R$  is applied the charge pattern in the immediate vicinity of the junction is disturbed so that the concentration gradient in that region changes its sign—see Fig. 13. Ejection of a

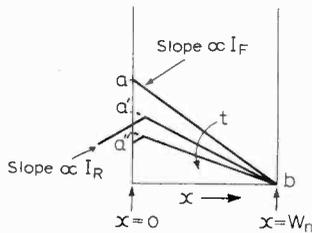


Fig. 13. Minority charge pattern for reverse current drive. Concentration gradient in region of junction changes its sign when step of reverse current  $I_R$  is applied.

hole from the n to p region is accompanied by the extraction of an electron from the body of the diode at the n contact. Now  $v > 0$ , if  $q > 0$ , irrespective of the direction of current flow in the external circuit. Stored charge will disappear more quickly than for  $I_R = 0$  because of the twin processes of extraction and recombination.

The charge model does not account for the backward slope of the  $P_n(x)$  curve, calculations assuming a triangular distribution  $a'b$  at all times. The error is slight if  $I_R \ll I_F$ . From eqn 6

$$\frac{dq}{dt} + \frac{q}{\tau_D} = -I_R$$

Fig. 14 shows the model when  $I_R$  is applied.

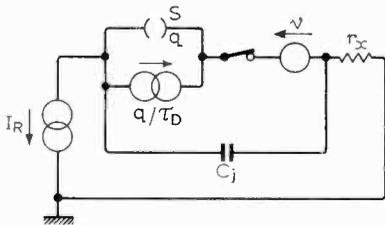


Fig. 14. Charge model with reverse current drive. Charge behaviour is shown in Fig. 15.

Capacitance  $C_j$  is neglected. Fig. 15 illustrates the behaviour of  $q$ .

$$q(0+) = I_F \tau_D$$

$$q(\infty) \rightarrow -I_R \tau_D$$

The switch on the diode model opens at  $q = 0$  corresponding to  $v = 0$ . Thus the diode becomes reverse biased at  $t = t_s$  where

$$t_s = \tau_D \log_e \{1 + (I_F/I_R)\} \quad (14)$$

If  $\tau_D$  is known (e.g. from a photograph such as Fig. 12) the validity of this relationship may be investigated using a test set-up

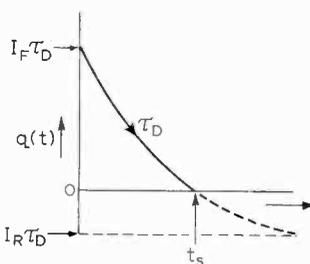


Fig. 15. Variation of excess minority charge with time. Switch opens at  $q = 0$ .

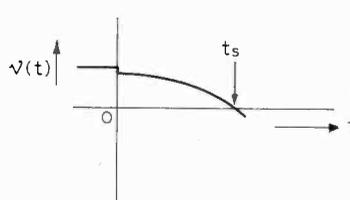


Fig. 16. Diode voltage waveform corresponding to Fig. 13. Small voltage slip is due to current change  $I_F + I_R$  at  $t = 0$

similar to that of Fig. 11 but with  $D_2$  omitted, and a reverse current limiting resistance in series with  $D_1$ . The general nature of the diode voltage waveform is shown in Fig. 16: a small voltage jump due to a current change  $I_F + I_R$  in  $r_x$  at  $t = 0$  (not always clearly defined) is followed during the recovery phase,  $0 < t \leq t_s$ , by a slowly changing anode voltage.

### Limitations of simple charge model

The charge model is based on the assumption that  $q(t)$  and hence  $i(t)$  is proportional to  $P_n'(0)$  for all values of  $t$ . This means regarding the charge as a single, easily accessible, lump and leads to a single time-constant description of the diode for first-order switching calculations. The usefulness of the model is best assessed by comparing its predictions with those obtained from a more exact analysis which does take into account the distributed nature of the device.

- For reverse current switch off the model indicates that all the charge is removed in a time  $t_s$  given by eqn 14. A calculation of the exact value of  $t_s$ —as determined by a solution of the time-dependent diffusion equation<sup>3</sup>—requires a prior knowledge of the ratio  $(W_n/L_n)$ . Thus eqn 14—which gives results erring on the side of pessimism—is a useful approximation for circuit arithmetic.
- The model yields the following result for charge,  $Q_E$ , extracted in the period  $0 < t < t_s$  by a constant reverse current  $I_R$

$$Q_E = I_R t_s \quad (15)$$

Substituting  $t_s$  from eqn 14 into 15, finding the limit as  $I_R \rightarrow \infty$  gives

$$Q_E = I_F \tau_D = Q \quad (16)$$

The value for  $Q_E$  given by eqn 16 is not removed in the time interval  $t_s$ . Actually, the charge is not removed in  $t_s$  and it is just not possible to remove all the stored charge supporting a steady current flow, in a normal diode. Solving the diffusion equation Lindmayer & Wrigley<sup>4</sup> have shown that if a long-base diode initially passing a steady forward current  $I_F$  has its applied voltage instantaneously reduced to zero, the charge,  $Q_R$ , recovered is given by  $Q_R = (I_F \tau_D)/2 = Q/2$ . The expression for a short base diode is  $Q_R = 2Q/3$ .

The recovered charge approach is sometimes useful in logic circuit design<sup>5</sup> and a number of charge recovery test circuits have been described in the literature (see especially ref. 6).

Despite the inaccuracy of eqn 16 it is

useful for rough calculations, the crudest approximation for  $t_s$  being  $t_s = Q/I_R$ .

### Conclusions

This discussion has concentrated on normal or 'classical' junction diodes except for the circuit of Fig. 11 where two diodes used  $D_1$  and  $D_2$  had no significant carrier storage. Hot-carrier diodes<sup>7</sup> have this property. These are metal-semiconductor diodes and in them the current is carried by majority carriers which are not velocity limited in the same way as are minority carriers in p-n junction diodes. At present hot-carrier diodes are relatively expensive, and are only used in those discrete circuits where speed is at an absolute premium (e.g. sampling gates). Their importance will increase as they become incorporated into bipolar integrated circuits.<sup>8</sup> However this does not mean the obsolescence of our charge model for a number of reasons.

Firstly we may wish to investigate storage effects in those instances where its nuisance value cannot easily be avoided, e.g. in power rectifiers working at frequencies much higher than that of the mains. Secondly, we wish to use the model in those applications where storage is purposely exploited. Examples here are the snap or step recovery diode<sup>9</sup> and the choice of a slow diode for diode-transistor logic.

Finally, a very important reason for considering a diode charge model is that an understanding, and consequent modelling, of the basic p-n junction is fundamental to an understanding of multi-junction semiconductor structures. The development of a charge model for a bipolar junction transistor follows quite logically from that of a diode.

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6. General Electric Co. Transistor Manual 1964. Seventh edn., pp. 447-8.
7. Hewlett-Packard Ltd. "Solid-state devices" 1967, pp. 55-87.
8. Turner, M. J., "Advances in integrated circuit technology", Ferranti Ltd electronics symposium, Nov. 1969.
9. See Ref. 7, pp. 1-41.

# Letter from America

As far as the general economic situation was concerned 1970 was a difficult year. Television sales of just over 8.5 million for the first nine months must therefore be considered good although it is a 15% drop compared with the same period in 1969. Radio did not fare too well with a fall of some 14% and record player sales were down about 17%. On the other hand, tape recorder sales were up 25% and both gramophone records and 8-track tapes showed a healthy increase. Here are the yearly figures (millions of \$):

	1969	1970
records	1170	1200
8-track cartridges	300	400
4-track cartridges	21	8
cassettes	75	105
reel-to-reel tapes	21	21

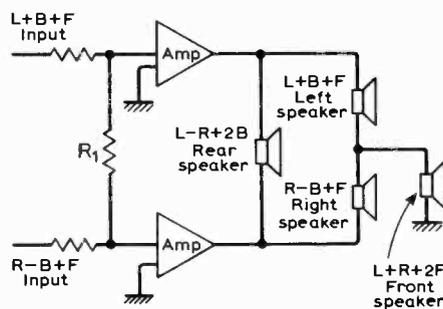
This year will undoubtedly see a further big increase in cassette sales due to the Dolby innovation and the long-awaited appearance of chromium dioxide (Crolyn) tapes. The 8-track format has been mainly used for car systems but it is rapidly becoming quite popular for home use. This trend will continue when more quadraphonic tapes are issued using the quad-eight arrangement. Motorola, RCA, Lear-Jet, Telex, 3M and several other firms have announced new quad-eight playing equipment but at the time of writing very little is actually available. The quadraphonic situation as a whole is still somewhat obscure with all kinds of systems—synthetic, psycho-acoustic, matrix and multiplex vying for attention. The Japanese Record Manufacturers Association recently decided to adopt the JVC (Japanese Victor Company) system as standard but as this is a carrier system involving a bandwidth up to 45 kHz it has obvious disadvantages. CBS have developed a compatible disc system using a switching technique which would involve a minimum expense by the broadcasting stations. Another system, demonstrated successfully at recent hi-fi shows is the Feldman-Fixler, now backed by Electro-Voice. Like the Sansui, Harman-Kardon, Scheiber and at least half-a-dozen others, the Feldman-Fixler is essentially a 'black box' device which can transform any two-channel, or even mono signal, into four. Synthetic of course, but the results are quite impressive for all that. Sceptics—and there are plenty—doubt whether these simulated



*Electro-Voice four-channel decoder which costs \$50.*

4-channel systems can give results that would even *begin* to compare with genuine 4-channel tapes but when such comparisons have been made at demonstrations many of the audience could not tell the difference! On the other hand, contrived demonstrations would not really correspond to home conditions—but none the less they show what *can* be done.

One of the most interesting ideas is due to David Hafler, of Dynaco, whose argument goes something like this: information picked up by microphones pointing to, or at the back of, a hall will have a lag time and part of the information will be out of phase with the front two channels. All you have to do to retrieve this information is to connect another speaker between the two channels on your amplifier and place it somewhere at the rear of the room. This difference signal certainly adds a sense of depth and spaciousness to the overall sound but results will vary widely due to different



*A method of using a derived centre channel to produce four channels (Dynaco patent No. 3,417,203).*

microphone and mixing techniques. Thus a level control is needed to keep some kind of balance. As might be expected, the rarely used, simple M5 microphone placement produces the most rational sound. A further refinement is the connection of a fourth speaker as shown in the diagram. Here we make use of a derived centre channel which produces the sum of both the two channels without crosstalk by simply using a blend resistor  $R_1$ . The effect is to emphasize sound picked up by a centre microphone or from equal pick-up from two side microphones. The beauty of this arrangement is that you can experiment with quadraphonics of a sort without buying another amplifier—a kind of half-way approach to the real thing. It will also be possible to assess feminine reactions which may well be provoked by two extra loudspeakers in the living room!

RCA recently announced a cinema-type television projector for use in the home, school or industry. It employs a special thin film mirror which is deformed electrostatically to modulate a light-beam. The mirror is made of a nickel alloy and is about 5cm square and between 0.2 and 0.6 microns thick. It is mounted on a series of grid supports 50 to 100 microns apart that keep the film some 5 microns from a glass substrate. In operation, a modulated electron beam scans the target as it would the phosphor screen in a conventional TV tube. The beam penetrates the metal film and deposits an electronic charge on the glass substrate in proportion to the intensity of the video picture at each spot. This charge electrostatically attracts and thus deforms the metal film and the projection system converts the amplitude of the deformation into an analogous brightness on the screen corresponding to the video signal. Picture size is 4 by 3 feet and the projection lamp is rated at 500 watts. It was emphasized that much work is needed before the performance is comparable to existing projection systems but the potential low cost justifies further development work.

Through a unique process that combines glass with metal, scientists at Corning have developed a new kind of superconductor. The material used is porous glass impregnated with lead and bismuth which forms about 35% of the total volume. As the text books say, a current will flow in a superconductor for ever without a generating source providing the temperature is kept at absolute zero i.e.  $-273.18^{\circ}\text{C}$  or  $459.67^{\circ}\text{F}$  (would you believe it, Americans still use Fahrenheit!). One of the problems associated with superconductors results from the magnetic field created by the electric current. If it becomes too great, it tends to nullify the superconducting ability. However, when the metal is distributed in glass it forms discrete grains separated by barriers and so the ability of this new Corning material to withstand magnetic fields is considerably increased.

G. W. TILLET

# World of Amateur Radio

## Another amateur satellite

AMSAT—the newsletter of the Radio Amateur Satellite Corporation—reports that work is proceeding on a second AMSAT-Oscar satellite (Oscar 6) designed to be launched as a secondary payload on Thor-Delta or Agena launchings. Priority is being given to the development of active satellites intended for long-lifetime, solar-powered operation and capable of augmenting amateur communications on v.h.f.

A number of satellite repeaters are under development in various parts of the world for use in future amateur satellites. These include a four-channel hard-limiting f.m. repeater being designed in Australia and of the demodulation-remodulation type with frequencies of 145.9 MHz for the up-link and 432.1 MHz for the down-link, the transmitter power being 1 watt. A 50 kHz bandwidth linear repeater is being developed in West Germany for the same frequencies but having a transmitter power of 10 watts and intended for all popular modes of amateur operation. An American group is working on a linear repeater having an input frequency of 145.9 MHz and output on 29.6 MHz.

Many amateurs are hoping that the outcome of the June 1971 World Administrative Radio Conference on Space Matters will be the granting of permission to use space communications techniques on all international bands from 7 MHz upwards. The present Radio Regulations limit operation virtually to the 144 MHz band.

## Harmful interference

In the recent public discussions on frequency allocations affecting amateur radio, there has been a tendency to forget the considerable difficulties that the official administrations have in enforcing the international frequency agreements and the problem presented by the small number of countries which remain outside the International Telecommunication Union. International frequency agreements are effective only when they are adhered to—and nowhere is this basic fact more apparent to radio amateurs than between 7000 and 7100 kHz. For European amateurs, this 100 kHz segment is all that remains of the old '40-metre

band' which for many years was the most popular of all the amateur bands. But the rot set in during the Spanish civil war when a number of amateur stations were pressed into use by both sides for broadcasting, with the result that international broadcasting became firmly established in this part of the spectrum. This was formally recognized in 1947 in the allocations made to broadcasting in some regions above 7100 kHz. But the Radio Regulations continued—and continue—to show 7000 to 7100 kHz as an exclusive world-wide amateur allocation.

Several weeks spent recently operating on this band—with its rewarding mixture of semi-local and long-distance contacts—have underlined the extent of high-power intrusion by some broadcasters. Almost every evening well over half the amateur allocation is rendered unusable by broadcasting, often leaving just a few narrow 'windows' in which amateur stations pile-up several deep. In the past decade, the R.S.G.B. Intruder Watch has reported over 600 intrusions into amateur bands—with some 22 stations persistently causing interference in recent years. Of these, 12 have been broadcast transmitters operated by administrations in four countries in Region 1 and one country in Region 3. One wonders if the countries concerned realize that the operation of these stations within exclusive amateur frequencies far from assisting their external relations, have quite an opposite effect on the very large number of amateurs who nightly suffer from this flagrant disregard of the international Radio Regulations.

## Amateurs in emerging countries . . .

At the recent installation of Fred Ward, G2CVV, as the R.S.G.B. president for 1971, an interesting sidelight was thrown on amateur activities. For the opportunity was taken by Eric Lomax of the Nigerian Amateur Radio Society to make a presentation to Dr Mike Dransfield, 5N2AAF, who, until his recent return to the U.K., had been the mainstay of the society throughout the recent troubled years in that country. For three years no new amateur licences were issued in Nigeria—and this meant a long hiatus in the efforts

of N.A.R.S. to build up the number of licences among the local nationals. Always in the past, the vast majority of amateurs in Nigeria have been temporary residents. Despite the population of about 60 million, only two Nigerian citizens hold licences. Many amateurs, throughout the world, recognize the importance of encouraging more local interest in amateur activities, seeing a potential threat to the hobby posed by the large number of I.T.U. member countries having only a handful of citizens holding licences.

## . . . and in Japan

A very different situation exists in Japan where the number of amateurs now exceeds 100,000. Japan, for some years, has been second only to the United States in numbers of amateurs, and has a far larger growth rate. Between 1965 and 1968, for example, Japanese amateurs increased from 38,000 to 84,000. Bill Hamer, ZL2CD, a recent visitor to Japan reports in *Break-in*, the New Zealand A.R.S. journal, seeing evidence of amateur radio everywhere he went: "DX-band aerials on roof-tops, 50 MHz mobile whips on cars, amateur radio club stations in factories and a thriving electronic components and amateur equipment industry". He believes that the main factor in this increase has been the introduction of a novice licence, although this has not been generally popular with those who have held licences for several years. The novice licence has brought about a serious interference problem and often poor operating standards. Japan has no age limit, and the majority of novices are in the 15 to 20 age group, though he notes there are some boys and girls of about 10 years of age holding licences. Power for novices is limited to 10 watts output and they use all bands except 14 MHz—both c.w. and phone-only novice permits are issued, the c.w. examination being at 5 w.p.m. For the full grade licence, a 10 w.p.m. code examination has to be passed and 100 watts output is permitted. An 'advanced' licence requires amateur experience plus knowledge of the special Japanese morse characters and of monitoring and test equipment. The New Zealander estimates that almost 95% of all Japanese amateurs hold the novice licence.

## In Brief

The next Radio Amateurs' Examination will be held at a number of local centres on May 11 . . . . Many long-distance contacts have been made this winter on 'Top Band' (1.8 MHz) including a number of stations working VK6NK in Australia; another rare station to appear on this band has been PJ2CC in the Netherlands West Indies . . . . An *Electronics* forecast of the amateur market in the United States is: 1970 \$21.6 million; 1971 \$23.2 million, considerably below the figures for 'Citizen's Band' equipment.

PAT HAWKER, G3VA

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WW—096 FOR FURTHER DETAILS

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WW-097 FOR FURTHER DETAILS

# New Products

## M.S.I. high level logic circuit

Designed specifically for high noise environments, the H157 synchronous 8421 b.c.d. decade counter from SGS, has asynchronous preset and reset, and a guaranteed minimum fan-out of 25. It is able to work on a supply voltage of 10.8 to 20V, and has a d.c. noise immunity of 5V with a 15V power supply. Four asynchronous preset inputs are provided which allow the counter to be positioned for whatever counting is desired, from 0 to 9. The circuit operates in the temperature range of 0-75°C, and is mounted in a ceramic 14 lead dual-in-line package. SGS (United Kingdom) Ltd, Planar House, Walton Street, Aylesbury, Bucks.

WW312 for further details

## I.C. unsoldering tool

A portable unsoldering tool has been developed by Marconi to allow damage-free removal of microcircuits and other multi-connection components from printed circuit boards. The unit consists of an electrically heated pot of molten solder with a metal piston floating in it. A vertical hole through the piston is fitted with one of a number of 'nozzles', shaped to accommodate different packages (i.e. dual-in-line packs, TO-5 cans, hybrid solid logic technology devices, valve

holders, relays and even discrete component sub-assemblies). The component to be removed from the board is held in a spring-loaded remover and set over the appropriate nozzle while the piston is depressed. Molten solder wells up through the hole and contacts the pins on the underside of the board before draining back into the pot. The spring loaded remover comes into operation immediately the pins are freed so that removal is practically instantaneous and there is no excessive transfer of heat to damage the component or the board. The oxide layer which invariably forms on molten solder is trapped on its passage up through the piston so that only fresh, clean solder actually touches the joints. Two sizes of pot have already been developed—2in and 3in diameter—both with integral heating elements using a 240V mains supply. The power consumption averages 300W. Marconi Company Ltd, Marconi House, Chelmsford, Essex.

WW324 for further details

## Transmission-line drivers and receivers

A range of five integrated circuits from Motorola are for use as interfaces between coaxial or twisted-pair transmission lines and data transmitters or receivers constructed with r.t.l., d.t.l., t.t.l. or e.c.l. The circuits, types MC1580L to 1584L, have wide input and output ranges (+9 to -3V for the drivers), high input or output impedances (up to 8k $\Omega$ ) and short propagation delays (down to 20ns). The receiver circuits can reject  $\pm 4V$  of noise. Uses of the units other than for data reception or transmission include voltage comparison, waveform generation, high impedance buffering and logic-level translation. Motorola Semiconductors Ltd, York House, Empire Way, Wembley, Middx.

WW311 for further details

## Variable power supply

The Roband Vareco range of variable stabilized supplies for bench use, employs a novel over-voltage protection system, and variable current limit prevents damage to the supply or load under fault conditions

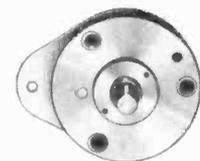
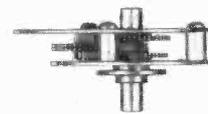


and enables the units to withstand a sustained short-circuit without damage. Stabilization is typically 20,000:1, ripple is less than 2mV, and the dual meter scale enables very accurate setting-up of low voltages in the range 0 to 10V. The units can readily be operated in series or parallel, and remote programming facilities are available. The range consists of the Varex 33-2, giving 0 to 33V at 2A (£55); the 33-10, giving 0 to 33V at 10A (£90); and the 60-5, giving 0 to 60V at 5A (£95). Roband Electronics Ltd, Charlwood Works, Charlwood, Horley, Surrey.

WW313 for further details

## Reduction gear drive

Jackson Brothers (London) have developed a small gear drive with input and output shafts in line, and with provision for mounting a dial or pointer. The reduction ratio between input and



output is 8:1 while that between input and pointer bush is 6:1. The pointer, or dial, will therefore travel 240° while the output shaft travels 180°. The length of this gear drive from back plate to face of pointer bush is only 12.5mm and the front area is 44x54mm. Jackson Brothers (London) Ltd, Kingsway, Waddon, Croydon, CR9 4DG.

WW320 for further details

## Multi-pole high-current connector

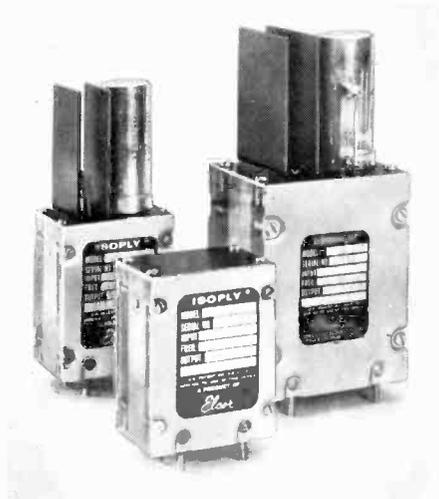
The Fischer type 107A018 circular 6-pin connector available from Sealectro is continuously rated at 25A per pin. The overall diameter is 36mm and versions include free plug, free socket and chassis socket. They can be obtained waterproofed. The free plug and free sockets have a compression type cable clamp tailored to the cable in use while the chassis socket has solder tag connections. Insulation of the



pins to body is p.t.f.e. permitting use in relatively high temperature applications and leaving the insulant unaffected by soldering of connections. Sealectro Ltd, Walton Road, Farlington, Portsmouth PO6 1TB. **WW307 for further details**

## Power supplies with isolated outputs

The Isoplys range of small, isolated-output power supply modules made by Elcor Inc., of Virginia, and available from Aveley Electric use zener diodes to obtain regulation. As inexpensive supplies they are designed to energize various devices that must be well isolated from direct local connection to ground, chassis, case or system common. The units are substantially

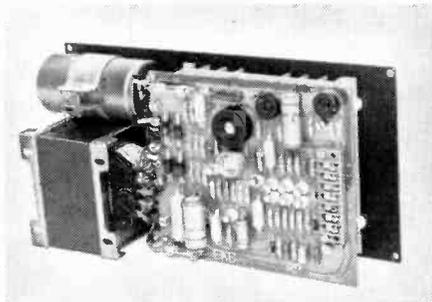


noiseless in floating circuit application. Novel construction of the transformer, and special mounting of the rectifiers, filter elements, and regulator, plus electrostatic shielding, greatly reduce the generation and transference of noise, while providing good isolation between the output circuitry and the combination of input and ground (core case and primary shield). Aveley Electric Ltd, Arisdale Avenue, South Ockendon, Essex.

**WW314 for further details**

## Stabilized power supplies

The RP Series, from EKB, is a range of high performance, low cost, modular power units with output voltages preset in three ranges, 0-7V at 2.5A, 8-18V at 2A, and 19-24V at 1.5A. Potentiometer adjustment is provided to give a  $\pm 1V$  swing about the nominal setting. Overload protection is



provided by a fast-acting re-entrant characteristic which automatically resets on removal of fault conditions. The trip current is adjustable from 25% to 110% of full load. Complete over-voltage protection can be supplied as an optional extra. Units are fused on both mains input and d.c. output lines. Four-terminal sensing is provided to enable regulation to be maintained when long cable runs are unavoidable. The design enables units to be stacked on 75mm centres to form multiple outputs. Units are priced at £19.00 each throughout the complete range; overvoltage protection can be factory fitted for an additional £4.50 per unit. EKB Ltd, Bromham, Chippenham, Wilts.

**WW308 for further details**

## Modular high-voltage power supply

Euro Electronic Instruments, U.K. representatives for Velonex, have announced a precision power supply designed for use with solid-state detectors, photomultiplier tubes and other devices requiring a stable high-voltage source with low noise and ripple content. The power supply—the Velonex Nimpac 105—has an output which is continuously adjustable from zero to 3,000V d.c. at 0 to 10mA with a non-backlash 20-turn control, the output voltage being indicated by four in-line digits accurate to  $\pm(1\% + 3.0V)$ . Ripple and noise are less than 10mV peak-to-peak, including high-frequency components and harmonics, and output voltage is line regulated within 50mV and load regulated within 10mV. Euro Electronic Instruments Ltd, Shirley House, 27 Camden Road, London N.W.1. **WW301 for further details**

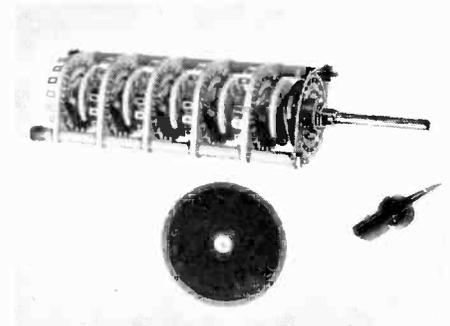
## Impedance meter

The IX704A impedance meter from ITT allows the measurement of any complex impedance in the 50 to 1000MHz bandwidth. The measuring unit consists of a  $50\Omega$  coaxial line incorporated into a standard chassis. Detectors fixed along the length of this line measure the r.f. voltages at different points, and the results are displayed on three independent meters. Three printed discs used in conjunction with a modified Smith's chart form the computing unit. This device establishes the relationship between the three measured voltages and the impedance under test, and also with a  $50\Omega$  standard against which the instrument is calibrated. ITT Electronic Services, Edinburgh Way, Harlow, Essex.

**WW316 for further details**

## Heavy duty wafer switches

A comprehensive range of Centralab wafer switches in various sizes, ratings and configurations, is available from Ultra Electronics (Components). Included among this range is the JV9019, a fifteen-pole heavy duty power switch having from two



to five positions. Contacts are placed  $20^\circ$  apart. Contact springs and terminals are silver plated. Up to 20A can be handled at 12V, and switching life is typically 25,000 cycles minimum. Ultra Electronics (Components) Ltd, Fassetts Road, Loudwater, Bucks.

**WW309 for further details**

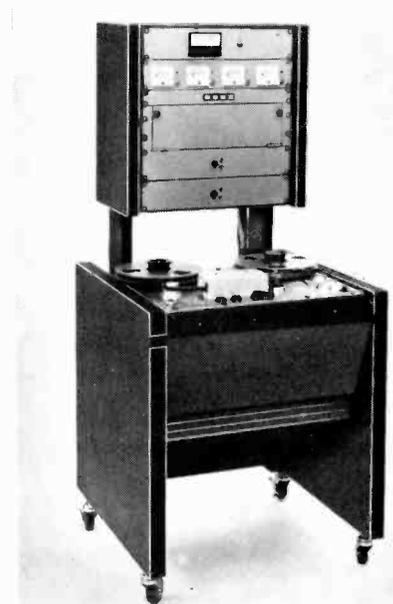
## Subminiature lampholder

A subminiature lampholder made of plated brass is available from WEL Components. The translucent 'windows' are available in blue, green, red, amber, and white. Bulbs are size T2 and type L1123 is recommended for i.c. indication having a rating of 5V 60mA with approximately 100,000 hours life. Price £0.29 each per 100. WEL Components Ltd, 5 Loverock Road, Reading, Berks.

**WW315 for further details**

## Tape duplicator

A master reproducer designed for rapid duplication of cassette, cartridge and reel-to-reel audio tape recordings is available from Ampex. Model RR-200 reproducer can drive up to ten Ampex model 3400 slave units and can duplicate up to 200 copies of a 30-minute-per-side tape in one hour on a 10-slave line. The RR-200 replaces the 3000 series of duplicators. It uses reel-to-reel master tapes and has speeds of 30/60 and 60/120 inches-per-second, plug-in head assemblies, and automatic tape tension control

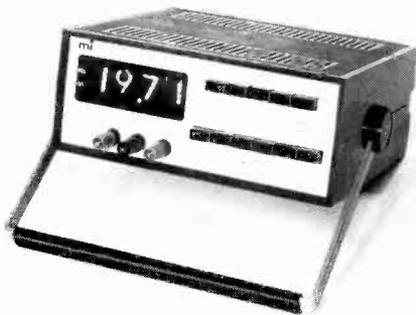


and can accommodate master transport tape widths from  $\frac{1}{4}$ -inch to 1-inch. Four-track and eight-track versions are available capable of duplicating programmes for eight-track and four-track stereo cartridges and two-track stereo or four-channel stereo tapes. The master reproducer has a frequency response equivalent to 50Hz-15kHz at  $7\frac{1}{2}$  i.p.s., a flutter and wow of less than 0.15%, and independent switching is provided for both master and copy equalization. Price from £5,500. Ampex Great Britain Ltd, Acre Road, Reading, Berks.

**WW317 for further details**

### Digital multimeter

The TF2670 from Marconi Instruments measures voltage, current and resistance to an accuracy better than 0.5%. In its basic form it has one current range of  $200\mu\text{A}$  but the addition of a plug-in current shunt unit



extends this to a total of five ranges, both a.c. and d.c., extending from  $199.9\mu\text{A}$  to 1999mA. The instrument has push-button selection of range and function. Price of TF2670 is £105. A rechargeable battery box, which makes TF2670 independent of the mains supply for up to five hours, and the current shunt unit, are available as optional accessories. Marconi Instruments Ltd, St. Albans, Herts.

**WW310 for further details**

### Positive temperature coefficient thermistors

The TG $\frac{1}{8}$ , from Texas Instruments, is a silicon bar thermistor with a positive temperature coefficient of 0.7% per °C (7,000 p.p.m.) and a temperature range of  $-75^\circ$  to  $+150^\circ\text{C}$ . The device is encapsulated in a hard-glass package. There is no hysteresis through its temperature range. It is available in resistance values of 10-2,700 $\Omega$  on a standard decade scale. T.I. Supply, 165 Bath Road, Slough, Bucks.

**WW323 for further details**

### Conductive plastic pots

A range of  $\frac{3}{8}$  inch diameter body, conductive plastic potentiometers has been introduced by Electrautom. The New England C series has a standard linearity of down to 0.25% infinite resolution and longer life than wire-wound models (manufacturers claim by a factor of more than ten). They are available with  $\frac{1}{4}$ in or  $\frac{1}{8}$ in shafts for bush or servo



mounting, and can be supplied with special function angles and taps. Prices for 100-off are £2.80 each for bush-mounted 1% linearity models and £4.25 each for servo-mounted 1% linearity models. Electrautom Ltd, Etom House, Queens Road, Maidstone, Kent.

**WW303 for further details**

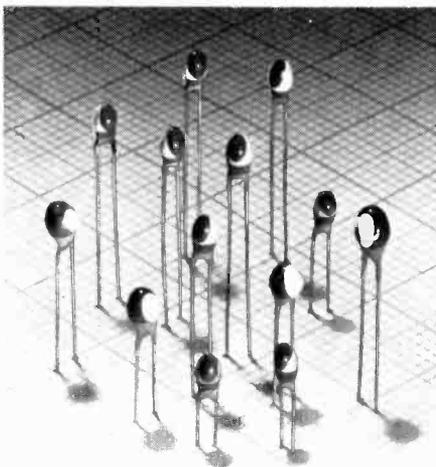
### Capacitor-discharge ignition system

Mobelec are making a range of capacitor-discharge electronic ignition units with specially wound h.t. coils. Three basic units are available in both positive and negative earth versions—model C20 for 4 and 6 cylinder engines up to 12,000 and 8,000 r.p.m. respectively, C40 for 8 and 12 cylinder engines, and model E40, which is a contactless unit, with distributor adaptors for most Lucas, Autolite, Delco and Bosch distributors. Another feature of the system is a low-cost matching unit which permits use of Smith's electronic tachometers. Complete unit prices start at about £13 for the C20 model—which suits the requirements of most British and European cars. Mobelec Ltd, Oxted, Surrey.

**WW302 for further details**

### Miniature tantalum capacitors

A range of miniature resin-dipped solid tantalum capacitors, code-named TAM, is available from ITT. The size is  $5 \times 2.5\text{mm}$  maximum. Capacitance ranges from  $0.015\mu\text{F}$  to  $6.8\mu\text{F}$  with tolerance of  $\pm 20\%$ . Working voltage range is from

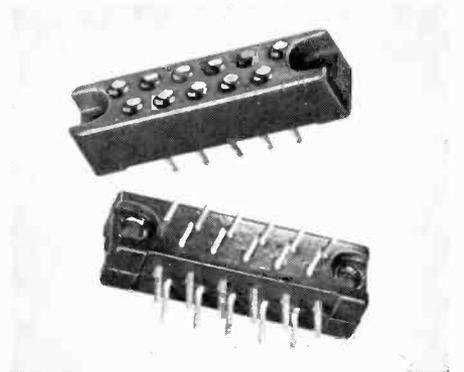


3 to 35V d.c. Prices are from 8p (1s 7d) to 11p (2s 2d) for quantities of 100 up, depending on capacitance and voltage. ITT Components Group Europe. Capacitor Product Division, Brixham Road, Paignton, Devon.

**WW326 for further details**

### Right-angle plug and socket

The Hirose type RA6-11P right-angle plug and socket, from Henry & Thomas, is an eleven pin plug with a 2.5mm (0.098in) contact pitch. The mating socket is designated RA6-11S. The pair have a current rating of 5A at  $20^\circ\text{C}$ , a contact resistance of



$10\text{m}\Omega$  max. and an insulation resistance of  $1000\text{m}\Omega$  at 500V d.c. The body moulding of the connectors is of an epoxy resin. Pins are of gold-plated brass and the sockets are manufactured from gold-plated beryllium copper. Henry & Thomas Ltd, Yeo Street, Bow Common, London E.3.

**WW305 for further details**

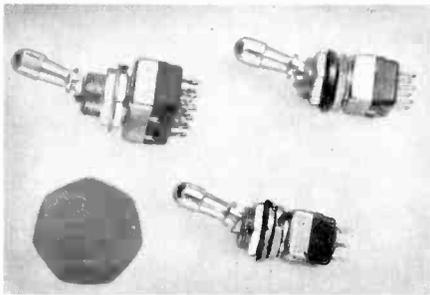
### Range of electrolytic capacitors

The voltage range of new capacitors from Colstar is 3 to 100V d.c., and the capacitance range 1 to  $2500\mu\text{F}$ . The units are small, have low leakage current, and comply to I.E.C.664. The electrodes are of etched aluminium foil and anodes are coated with a very thin oxide film which is the dielectric. The whole capacitor is contained in a hermetically sealed aluminium case insulated by a p.v.c. sleeve. Colstar Ltd, 233-243 Wimbledon Park Road, London S.W.18.

**WW325 for further details**

### Miniature locking toggle switches

In the range of miniature locking toggle switches, available from Guest International, the locking action is achieved through the toggle itself. Once locked, it can be released only if it is axially pulled and then moved to a new position. The length of the toggle is 20mm and standard switches are manufactured in three lockable combinations with the contact arrangements being two-, three- or four-pole. The switch body is available in



either non-sealed or waterproofed versions. Finishes are in chrome or matt-black and contact platings are in gold or silver with a rating of 2A at 250V. Industrial Electronic Components Division, Guest International Ltd, Nicholas House, Brigstock Road, Thornton Heath, Surrey.  
**WW327 for further details**

### High-current switching transistor

A high-current transistor, type BFX34, from Mullard is an n-p-n, silicon planar epitaxial device intended for use as a driver of print hammers and relays. Because of its low saturation voltage (1V or less) the transistor dissipates little power when conducting. It is therefore particularly suitable for use in switching circuits where high efficiency is required. Characteristics include:

max. $V_{CBO}$	120V
max. $V_{CEO}$	60V
max. $I_{CM}$	5A
max. $P_{tot}(T_{case} \leq 25^\circ C)$	5W
$h_{FE}(I_C=2A, V_{CE}=2V)$ min.	40
	max. 150
max. $V_{CEsat}(I_C=5A, I_B=0.5A)$	1V
min. $f_T$	

( $I_C=0.5A, V_{CE}=5V, f=35MHz, T_{amb}=25^\circ C$ ) 70MHz

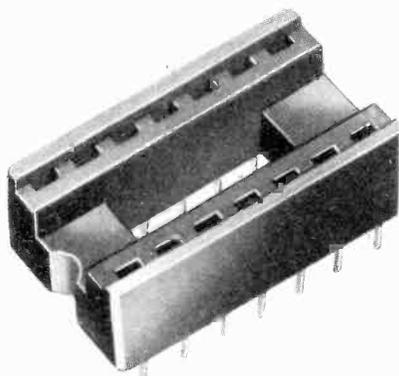
$t_{off}(I_C=5A, I_{B(on)}=-I_{B(off)}=0.5A)$  1.2µs  
 encapsulation TO-39

Mullard Ltd, Mullard House, Torrington Place, London WC1E 7HD.

**WW306 for further details**

### Dual-in-line socket

The A23/2028 dual-in-line socket from Jermyn accepts plug-in packages having 14 leads on 0.1in centres, with row spacing of 0.3in. The glass-loaded nylon body is available with a choice of two contact materials: Z contact—beryllium copper, gold plated over silver; Y contact—



phosphor bronze, gold plated over nickel. Typical contact resistance is 5mΩ for type Z, 10mΩ for type Y. Price range from 15p for 500 up. Jermyn Industries, Vestry Estate, Sevenoaks, Kent.

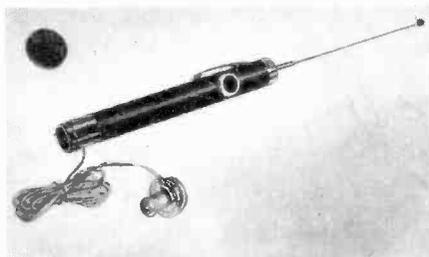
**WW328 for further details**

### Power transistor range

The G.E. (U.S.A.) D44C and D45C series of complementary pairs of power transistors, available from Jermyn, are rated at 30W each with  $V_{ces}$  ratings from 40 to 70V and available in a range of 3:1 maximum gain spreads. They have a low  $V_{ce sat}$  of 0.5V at 1A, typical  $f_i$  around 50MHz and good gain linearity with collector current. The transistors are colour moulded (for ease of identification) and have a heat dissipating plate on one side. The leads may be formed to TO-66 configuration. Jermyn Industries, Vestry Estate, Sevenoaks, Kent.  
**WW321 for further details**

### Miniature v.h.f. radio

Van Dusen have introduced a miniature v.h.f. radio receiver powerful enough to pick up aircraft transmissions over a 25 mile radius. It was developed as an



emergency stand-by receiver intended primarily for pilots. Price £4. Van Dusen Aircraft Supplies Co., Oxford Airport, Kidlington, Oxford.

**WW319 for further details**

### Digital indicator

K.G.M. have announced a digital indicator called the Minitron. It operates from 5V and gives a parallax-free seven-bar presentation. It has a configuration compatible with integrated circuits to the extent of plugging into a standard socket. Life expectancy is 100,000 hours, and current consumption is 8mA per bar. It is capable of time-shared operation. Up to six units can be obtained now at £1 each. K.G.M. Electronics Ltd, Clock Tower Road, Isleworth, Middx.

**WW322 for further details**

### Coaxial reed relays

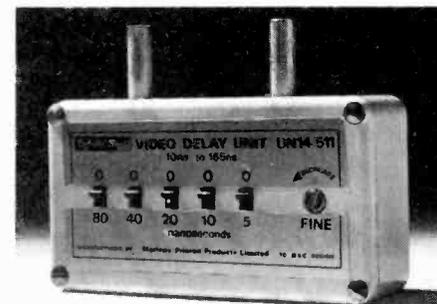
A range of coaxial reed relays is available from Sealectro. The units are designed for use from d.c. to 1GHz and are fitted with gold plated 50Ω subminiature screw-on or snap-on connectors. They will operate from 6, 12 or 24V with an average switching time of 15ms. Isolation between ports is > 30dB with a maximum v.s.w.r. of 1.25.

Typical insertion loss is 0.75dB maximum over the frequency range. The units will handle up to 12W continuous power. RF Components Division, Sealectro Ltd, Walton Road, Farlington, Portsmouth PO6 1TB.

**WW304 for further details**

### Variable delay line unit

Matthey Printed Products are distributing the Silver Star variable delay-line unit UN14/511 as an addition to their existing range of 75Ω equalized delay line modules. Designed to a B.B.C. specification, the plug-in unit offers rapid and accurate selection of any delay time from 10 to 165ns. This facility is particularly useful in colour



television vision mixing equipment when successive special event programmes may require television engineers to re-set temporarily the fine trim of delays in signal trains going to the mixer. The unit measures 114×635×318mm. Matthey Printed Products Ltd, William Clowes Street, Burslem, Stoke-on-Trent, ST6 3AT.  
**WW330 for further details.**

### Low-noise tape on 10½-inch reels

Scotch Dynarange 203 long-play tape is now available in 3,600ft lengths spooled on 10½in NAB metal reels. Designed for use on advanced specification high-capacity recorders, such as those manufactured by Akai and Revox, the new length of tape offers six hours playing time at 3¼ i.p.s (9.5cm/s). Recommended retail price is £6.25 plus p.t. of £0.07. 3M Company, 3M House, Wigmore Street, London W1.

**WW318 for further details**

### Sockets for 24-pin i.c.s

24-pin solder tail i.c. sockets from Texas Instruments can be compactly mounted and the contact positions are numbered. Orientation of contacts is specifically designed to overcome the problem of i.c. lead frame burrs and rough edges, and the solder tail socket will accept any shape of lead frame. The terminations are 0.025in wide by 0.0065in thick with contact plating of 200µin of bright tin plate per MIC-T-10727. Other platings are also obtainable. Socket bodies are of glass-filled nylon. The operating temperature range is from -65 to +125°C. TI Supply, 165 Bath Road, Slough, Bucks.

**WW329 for further details**

# Personalities

**Edgar M. Lee**, B.Sc., F.I.E.E., who founded Belling and Lee Ltd in 1922, has retired from the chairmanship of the company. He has been gradually relinquishing the day-to-day administrative duties since suffering a coronary heart disease in 1955. In recognition of his contribution to the company, which is now part of the Philips organization, he has been appointed founder president. Mr. Lee, a graduate of King's College, London, was a founder member of what is now the Radio and Electronic Component Manufacturers' Federation.

**Gavin Kermack**, B.Sc., D.I.C., F.I.E.E., aged 46, is appointed to the board of Honeywell Ltd as director, industrial products group. Sales & Service Divisions, in succession to **Peter Prior** who recently took up a senior post at the Brussels headquarters of Honeywell's new European marketing organization. Mr. Kermack, who is a graduate of Glasgow University, was managing director, Serck Controls, and latterly group manager, marketing, for Serck Ltd. At one time he was with Ferranti Ltd where he was associated with D. T. N. Williamson (of amplifier fame) on machine tool control.

**J. B. Hodgson**, formerly director and general manager of Centralab Limited and its subsidiary Stability Capacitors Ltd, has been appointed managing director of both companies. He has been succeeded as general manager of Centralab by **A. D. Little**, who was works manager of the Antrim factory.

**Anthony Renton**, B.Sc., D.Phil., has been appointed group technical manager for Highland Electronics Group Ltd. The group recently announced the acquisition of Ardenite Ltd and Ardenite Acoustic Laboratories Ltd (hearing aid manufacturers) from EMI Ltd. Dr. Renton recently returned to this country after 16 years in America where for the latter three years he

was at the NASA Electronics Research Center, Cambridge, Massachusetts, conducting research on power switching components. When he went to America in 1954, he took up a Post Doctoral Fellowship at Penn State University and then spent four years at Bell Telephone Laboratories. In 1960 he joined RCA and from 1962 to 1968 lectured in electrical engineering first at the University of Pennsylvania and later at Northeastern University.

**Peter Wall**, M.Sc., has joined the Rank Organisation as technical manager for Rank Wharfedale Ltd. and H. J. Leak. Immediately prior to joining Rank he was with Redac Software Ltd, the Racal computer-aided design subsidiary. Mr. Wall, who has an honours degree in electrical engineering and an M.Sc. in mathematics, was formerly chief engineer of the Quartz Crystal Division of Standard Telephones and Cables.

**G. S. Innes**, O.B.E., B.Sc., M.I.E.E., A.Inst.P., who retired recently as deputy physicist at St. Bartholomew's Hospital, London, is now consultant on medical physics and engineering to the T.E.M. group of companies which includes T.E.M. Engineering Ltd, who manufacture the Monitron system for patient monitoring and industrial control and the SAMI range of "socially acceptable monitoring instruments". Mr. Innes was appointed an O.B.E. in the New Years' Honours for his services to the hospital and to medical engineering.

**Roger N. Oatley**, formerly a chief technical officer at the British Standards Institution, has gone to Frankfurt a. M., W. Germany, as secretary of the international committee established to introduce the Western Europe harmonized system of quality assessment for electronic components. This committee—CENEL Electronic Components Committee (C.E.C.C.)—is part of the 14-nation European

electrical standards co-ordinating committee (CENEL), which rationalizes electrical technical specifications and procedures in the E.F.T.A./E.E.C. economic groups (Finland is an associated country).

**Stephen Forte**, Ph.D., B.Sc., F.I.E.E., recently joined General Instrument Microelectronics Ltd as marketing director. Since 1955 he had been with Marconi where in 1959 he took charge of a research section investigating parametric amplifiers and microwave solid-state techniques. He then assumed responsibility for the company's microelectronics applications laboratory and on the formation of Marconi-Elliott Microelectronics Ltd was appointed m.o.s. product manager.

**M. P. Mandl** has joined Marconi-Elliott Microelectronics Ltd as a director and general manager. Mr. Mandl has an honours degree in physics from Imperial College, London, and was with English Electric Valve Company from 1958 to 1966. He then joined Raytheon International being latterly the director of their international sales and services.

Cosmocord Ltd announce the following managerial reorganization at their Waltham Cross, Herts, factory. **D. Archer** becomes general manager (technical) and is responsible for all technical and engineering activities, including plant services, engineering services and inspection, development engineering, work study and production engineering; **G. Edwards** becomes general manager (sales) responsible for sales, both home and abroad; and **R. Spence** general manager (manufacturing) responsible for production.

**A. M. Pilbrow**, has joined the staff of the Scientific Instrument Manufacturers' Association (S.I.M.A.) as technical secretary. Following his National Service in R.E.M.E. he joined the G.E.C. Applied Electronics Laboratories as a design engineer and later held positions as a mechanical instrument engineer with S. Davall & Sons and as the senior engineer of the design department of Ultra Electronics (Components) Ltd.

**A. J. Wynroe**, Ph.D., has joined K. J. Bentley and Partners, the Lancashire printed circuit specialists, as technical director. He will have overall responsibility for all technical aspects of Bentley's and its associated companies Portland Electronics Ltd, Bryan Amplifiers Ltd, and Franken Systems & Supply Ltd. Dr. Wynroe was until recently doing research work in nuclear electronics at the

Daresbury Laboratories of the Science Research Council and has been lecturing in physics at Manchester University.

Following the recent appointment of **L. D. Hadfield** as managing director of Plessey, Australia, he is succeeded as general manager of the Automation and Transmission Divisions of Plessey's Electronics Group at Poole, Dorset, by **J. E. Samson**, F.Inst.P. Immediately prior to joining Plessey Mr. Samson was group managing director of Negretti and Zambra Ltd. He is president of the Institute of Measurement and Control.

A number of appointments have been announced by Advance Electronics Ltd, of Hainault, Essex, during the past two months. First, **Gordon C. Pope**, M.Eng., M.I.E.E., who joined the company in 1963, has succeeded **Eric Wakeling**, M.I.E.E., as managing director. Mr. Wakeling, who has been m.d. since 1962 is now executive deputy chairman. **Peter Sidey**, B.Sc., A.R.C.Sc., previously managing director of the company's Instruments Division has been appointed director of new business development. **Rex E. Nelson**, B.Sc.(Eng.), F.I.E.E., A.C.G.I., who joined the company in November last year, is appointed a director and will continue in his executive capacity as marketing director. He joined A.E.I. as a graduate apprentice in 1952 and was marketing director of Thorn Automation, Rugeley, immediately prior to joining Advance. The company has also recently appointed four product marketing managers: **Don Beckman** (instruments), **Tony Skottow** (industrial), **Alan Hutley** (power supplies) and **Mike Briggs** (special projects).

**Harold J. Cooke**, manager of the drawing office handling *Wireless World* drawings since 1939, has retired. He joined the drawing office of the Wireless Press (then our publishers) in May 1921 and has therefore handled the drawings published in the journal for nearly 50 years. Much of the credit for the standard of draughtsmanship displayed in the diagrams published in *W.W.* must go to him.

## OBITUARY

**Harry Faulkner**, C.M.G., B.Sc., F.I.E.E., deputy engineer-in-chief of the Post Office when he retired in 1953 after 40 years' service, died in January aged 78. A graduate of University College Nottingham, Mr. Faulkner was the first engineer-in-charge of the Rugby radio station (1926-29). For ten years following his retirement from the Post Office he was director of the Telecommunication Engineering and Manufacturing Association.

# Literature Received

For further information on any item include the appropriate WW number on the reader reply card

## ACTIVE DEVICES

We have received the following publications from RCA Ltd, Lincoln Way, Windmill Rd, Sunbury-on-Thames, Middlesex.

- HPA-100, 'High-power arrays', very high-power encapsulated circuit modules ..... WW401
- PTD-187B, 'Power transistor directory' ..... WW402
- RFT-700G, 'R.F. power transistors' ... WW403

The 1971 'Abridged valve data booklet' from the English Electric Valve Co. Ltd, Chelmsford, Essex, lists over 600 devices in its 96 pages ..... WW404

'The semicon index' replaces the earlier 'International transistor data manual' although it is still compiled in conjunction with Avo Ltd. The index is well designed and lists data on an enormous number of transistors. Functional Publication Services Ltd, 29 Denmark St, Wokingham, Berks. RG11 2AY ..... price £5.25

If you have facilities for wire bonding the SG3801 quick-chip will be of interest. It contains a variety of active and passive components which may be connected in any way the user requires. The device is made by Silicon General and literature is available from Rastra Electronics Ltd, 275 King St, Hammer-smith, London W.6. .... WW405

The following literature is published by Siemens (U.K.) Ltd, Great West House, Great West Rd, Brentford, Middlesex.

- 'Semiconductor manual 1970/71', 896 pages ..... WW406
- 'Selenium rectifiers for radio and television' WW407
- 'Microwave tubes' ..... WW408
- 'Numeric and symbolic indicator tubes' . WW409

## PASSIVE COMPONENTS

A reed relay catalogue is available from Electro-thermal Engineering Ltd, 270 Neville Rd, London E.7 ..... WW410

We have received the following literature from Vero Electronics, Industrial Estate, Chandlers Ford, Hampshire SO5 3ZR.

- 'Card handles' ..... WW411
- 'D.I.P. boards' ..... WW412
- 'Terminal pins' ..... WW413
- 'Systemized products' (equipment cases and fittings) ..... WW414

A catalogue called 'Cable trunking and cable trays' describes the products of William E. Cary, Sheet Metal Unit, Times Mill, Grimshaw Lane, Middleton, Manchester, M24 2AA ..... WW415

'High fidelity, electronic components, and equipment catalogue' is the title of the latest catalogue of G. W. Smith & Co. (Radio) Ltd, 3 Lisle St, London W.C.2 ..... price 37½p

A leaflet called 'Printed circuits general data' is available from Nevin Electric Ltd, Arkwright Rd, Poyle Trading Estate, Colnbrook, Bucks. . WW416

Illuminated rocker switches (type 900TP) are described in a leaflet available from the Microswitch Division, Honeywell Ltd, Windsor Rd, Slough, Bucks. .... WW417

A wide range of switches, mostly for printed circuit mounting, manufactured by Chicago Switch Inc., is described in a leaflet from Competa International Products, Bye-pass Rd, Barking, Essex ... WW418

Henry's Radio Ltd, Edgware Rd, London W.2, have produced a ninth edition of their catalogue ..... price 37½p

We have received the following literature from Siemens (U.K.) Ltd, Great West House, Great West Rd, Brentford, Middlesex.

- Capacitor catalogue ..... WW419
- Electrolytic capacitor catalogue ..... WW420
- Radio interference suppression catalogue WW421
- Ferrite components and transformers catalogue ..... WW422
- 'Low voltage control equipment' large catalogue listing relays, switches, plugs, sockets, etc. etc. .... WW423

## EQUIPMENT

A brochure describing the MAC-16 small computer system for business use is available from Unidata Ltd, 52 Curzon St, Mayfair, London W.1. . WW429

Details of a range of v.h.f. television transmitters are contained in a booklet from Pye TVT Ltd, Coldhams Lane, Cambridge ..... WW430

A new machine for stripping enamel covered copper wire is described in a brochure from Gardners Transformers Ltd, Christchurch, Hampshire BH23 3PN ..... WW431

Fenlow Electronics Ltd, Whittets Eyot, Jessamy Rd, Weybridge, Surrey, have produced the following literature

- Digital panel meter type DP603 (0 to 1.99V) ..... WW432
- Miniature power unit type PU40 ( $\pm 15V$ , 50mA max.) ..... WW433

'Electrical safety testing equipment to B.S.' is the title of a leaflet from Zenith Electric Co. Ltd, Cranfield Rd, Wavendon, Bletchley, Bucks. .... WW434

Shure Electronics Ltd, 84 Blackfriars Rd, London S.E.1, have produced a leaflet, 'Vocal Master', which describes audio equipment for professional use ..... WW435

We have received the following leaflets from Applied Data Systems Ltd, Station Rd, Belmont, Surrey:

- 100, data collection system ..... WW436
- 200, circuit selection system ..... WW437
- 202, speech privacy equipment ..... WW438
- 300, data matching unit ..... WW439
- 302, data matching unit ..... WW440
- 4,000, store exerciser ..... WW441
- Engine test set ..... WW442
- Telegraph converter units ..... WW443

A six-page brochure is available which describes a three-terminal document reader (Dataterm-3). Data Recognition Ltd, Loverock Rd, Battle Farm Estate, Reading, Berks. RG3 1DX ..... WW444

A low-cost, small, ten-digit desk calculator (Anita 1011) which uses l.s.i. circuits and will add, subtract, multiply and divide is described in a brochure from

Sumlock Comptometer Ltd, 39 St. James's St, London S.W.1. .... WW445

Data sheet 1037 from Honeywell Ltd, Microswitch Division, Windsor Rd, Slough, Bucks, deals with sequential timers ..... WW448

## GENERAL INFORMATION

We have received the following specifications in the BS9000 series for parts of assessed quality. British Standards Institution, 2 Park St, London W1A 2BS

- BS9012:1970, Counter and indicator tubes ..... price 60p
- BS9016:1970, Indicator tubes ..... price 60p
- BS9021:1970, Corona stabilizer tubes . price 80p
- BS9025:1970, Travelling-wave amplifier tubes ..... price £1
- BS9026:1970, Low-noise signal amplifier tubes with integral permanent magnet focusing ..... price 60p
- BS9040: 1970, Gas-filled microwave switching tubes ..... price £1.60
- BS9041:1970, Digital t.t.l. integrated circuits ..... price 60p
- BS9052:1970, G.P. professional c.r.t.s . price 80p

We have also received

- BS4649:1970, 'Miniature circuit-breaker distribution boards for low- and medium-voltage a.c. circuits' ..... price 50p

British Insulated Callender's Cables Ltd, P.O. Box No. 5, 21 Bloomsbury St, London W.C.1, have published a booklet called 'The erection of aerial telephone cables' ..... WW449

## From the Boat Show

Ajax Electronics (1969) Ltd, Southend-on-Sea, Essex.

- 'Leader 100' 100W radiotelephone (£435) WW450
- 'Leader' 75W radiotelephone (£375) ... WW451
- 'A25' 25W radiotelephone (£265) ..... WW452

Marine Electronics Ltd, Ickleford Rd, Hitchin, Herts.

- 'Tasman' echo sounder (£54) ..... WW453
- 'Combined Pacific', combined echo sounder, knot meter and log (£122) ..... WW454
- 'Aqua-log', marine speedometer (£76) . WW455
- 'Pacific 300', echo sounder (£39.5) ..... WW456

Miles Nautical Instruments Ltd, River Bank Works, Old Shoreham Rd, Shoreham-by-Sea, Sussex BN4 5FL.

- Speedometer and course-run indicator (£66.5) ..... WW457
- Depth meter (£82) ..... WW458

Smiths Industries Ltd, Motor Accessory Division, Oxgate Lane, London NW2 7JB.

Catalogue, 'Sport Boat Equipment' ..... WW459

Electronic Laboratories (Marine) Ltd, Cyldon Works, Fleets Lane, Poole, Dorset. (Seafarer range)

- 'Seavista' 3kW small boat radar (£795) . WW460
- 'Seascan' 3kW small boat radar (£450) . WW461
- 'Seafix' radio direction finder (£250) ..... WW462
- 'Surveyor' depth sounder (£200) ..... WW463
- 'Seascribe' depth sounder (£100) ..... WW464
- 'Seafarer Mk II' depth sounder (£28) ..... WW465

The Ferrograph Co. Ltd, The Hyde, Edgware Rd, Colindale, London N.W.9.

- R300 depth sounder (meter—£75) ..... WW466
- G500 depth sounder (chart—£120) ..... WW467
- G180 depth sounder (chart—£85) ..... WW468

S.P. Radio A/S, 9000 Aalborg, Denmark. (Sailor range)

- Catalogue, v.h.f. aerials ..... WW469
- Navigational equipment ..... WW470
- Charge controllers type 76 ..... WW471
- Loops, d.f. (26FA and 26F) ..... WW472
- 56D, 100W telephony transmitter ..... WW473
- 96D, 2W radiotelephone ..... WW474
- 66T, marine receiver ..... WW475
- 56T, marine receiver ..... WW476
- RT141/142, 20W v.h.f. radiotelephone . WW477
- 76D, 35W telephony transmitter ..... WW478
- 86D, 70W telephony transmitter ..... WW479
- Marine radio equipment (short form) ... WW480
- 46T, marine receiver ..... WW481

Derritron Electronics Ltd, Marine Division, 24 Upper Brook St, London W.1.

- DF70, direction finder and marine receiver (£125) ..... WW482
- 'Seaphone', 5W radiotelephone (£175) . WW483
- 'Mayday II' emergency radiotelephone (£125) ..... WW484

# March Meetings

*Tickets are required for some meetings: readers are advised, therefore, to communicate with the society concerned*

## LONDON

1st. IEE—"Telecommunications—new practices, old concepts" by Prof. J. Greig at 17.30 at Savoy Pl., W.C.2.

2nd. IEE—Discussion on "Technical codes of practice in independent television" at 17.30 at Savoy Pl., W.C.2.

3rd. IERE—"Loran C—some recent developments and field observations" by W. F. Blanchard and A. R. Woods at 18.00 at 9 Bedford Sq., W.C.1.

4th. RTS—"Recent developments in colour tubes" by W. Wright at 19.00 at I.T.A., 70 Brompton Road, S.W.3.

8th. IEE—Colloquium on "Recent progress on semiconductor microwave sources" at 14.00 at Savoy Pl., W.C.2.

8th. IEE—"Communication of objectives—reconciling the interests of the organization and the engineer" by Dr. D. Pym at 17.30 at Savoy Pl., W.C.2.

9th. IERE—Clerk Maxwell lecture "Guided electromagnetic waves" by Prof. H. M. Barlow at 18.30 at University College, Gower Street, W.C.1.

10th. IEE—"Aspects of military defence communications, past and future" by J. R. Mills at 17.30 at Savoy Pl., W.C.2.

10th. IERE—"Modernization of short-wave transmitting stations" by C. MacKenzie at 18.00 at 9 Bedford Sq., W.C.1.

15th. IEE—Discussion on "Low cost digital voltmeters" at 14.30 at Savoy Pl., W.C.2.

15th. IEETE—Panel meeting on "Better equipment—by design" at 18.00 at Savoy Pl., W.C.2.

16th. IERE/IEE—Colloquium on "Equipment technology in computer systems" at 14.30 at 9 Bedford Sq., W.C.1.

17th. Inst.Nav.—Discussion on "The relationship between A.T.C. separation standards and navigational capability" at 17.00 at Royal Institution of Naval Architects, 10 Upper Belgrave Street, S.W.1.

17th. IEE—Discussion on "Data communications—studies for a public service" at 17.30 at Savoy Pl., W.C.2.

17th. IERE—"Data logging techniques" by J. T. Kennair at 18.00 at 9 Bedford Sq., W.C.1.

17th. BKSTS—"The development of high-quality audio amplifiers" by J. L. Linsley Hood at 19.30 at I.T.A., 70 Brompton Road, S.W.3.

18th. RTS—"Low light television" by R. J. Core at 19.00 at I.T.A., 70 Brompton Road, S.W.3.

22nd. IEE—Colloquium on "Ferrite microstrips" at 10.30 at Savoy Pl., W.C.2.

24th. IERE—"Engineer to entrepreneur" by T. M. B. Eiloart and J. Langham Thompson at 18.00 at 9 Bedford Sq., W.C.1.

25th. IEE—Discussion on "Techniques for separating biological signals from biological noise" at 14.30 at University College, Gower Street, W.C.1.

31st. IERE—"R.F. standards" at 18.00 at 9 Bedford Sq., W.C.1.

## ABERDEEN

17th. IERE—"Electronics and road safety" by G. J. Glassbrook at 19.30 at Robert Gordon's Institute of Technology, Physics Dept. Lecture Theatre, St. Andrews Street.

## AYLESBURY

11th. IEE—"Stereo transmission" by Dr. G. J. Phillips at 19.15 at the College of Technology.

## BATH

3rd. IEE/IERE—"Data communication" by M. B. Williams at 19.00 at the University.

## BIRMINGHAM

8th. SERT—Colour TV forum at 19.30 at Aston University.

17th. RTS—"Satellite communication in the 70s" by D. I. Dalgleish at 19.00 at ATV Studio Centre, Bridge Street.

## BOURNEMOUTH

4th. IEE—"Application of m.o.s.t. & l.s.i. techniques" at 18.30 at the Technical College.

## BRISTOL

10th. IERE—"Optical character recognition" by Dr. A. W. M. Coombs at 19.00 at School of Chemistry.

## CARDIFF

15th. IERE/IEE—"Electronic control of postal machinery" by H. W. N. Long at 18.00 at University of Wales Institute of Science and Technology.

18th. SERT—"Problems of u.h.f. transmission and reception" by W. Wolfenden at 19.30 at Llandaff Technical College, Western Avenue.

24th. RTS—"U.H.F. transmitters" by D. East at 19.00 at Broadcasting House, Llandaff.

## CHATHAM

25th. IERE—Discussion on "Engineer to manager" at 19.00 at Medway College of Technology.

## CHELTENHAM

16th. IERE/IEE—"Medical electronics" by Dr. D. J. Mahy and M. R. Bullen at 19.00 at Cheltenham Cobalt Unit adjoining General Hospital, Sandford Road.

## COLCHESTER

23rd. IERE—"Direct view storage tube displays" by A. B. E. Ellis at 18.30 at University of Essex.

## EDINBURGH

2nd. IEE/I.Mech.E.—"Complex industrial measurements with simplified electronic presentation" by T. Black and W. Brown at 18.00 at Carlton Hotel.

3rd. Brit. Computer S.—"Character recognition and intelligent machines" by Dr. A. Coombs at 18.00 at the Mountbatten Building of the Heriot-Watt University.

10th. IERE/IEE—"Machine intelligence" by Prof. D. Michie at 19.00 at Napier College of Science and Technology, Colinton Road.

## EXETER

16th. IEETE—"Concorde electrics and electronics" by H. Hill at 19.30 at Imperial Hotel.

## FAREHAM

3rd. IERE/IEE—"Electronics for mass produced cars" by C. F. Rayner at 19.00 at H.M.S. Collingwood.

## FARNBOROUGH

25th. IERE—"Design for maintenance" by Lt. G. Benyon-Tinker at 19.00 at the Technical College.

## GLASGOW

11th. IERE/IEE—"Machine intelligence" by Prof. D. Michie at 19.00 at the Institution of Engineers and Shipbuilders, Rankne House, 183 Bath Street.

## INVERNESS

3rd. IEE—"Instrumentation for oceanography" by B. S. McCartney at 19.30 at the Technical College.

## LEEDS

25th. IERE—"Electronics in cars" by L. G. Cripps at 19.00 at the University, Department of Electrical and Electronic Engineering.

## MANCHESTER

4th. SERT—"Transistor d.c./d.c. converters" by I. McArthur at 19.30 at U.M.I.S.T., Sackville Street.

8th. IEETE—"Technician engineers and technicians—education, training, qualifications and status" by E. A. Bromfield at 19.30 at 113/115 Portland Street.

18th. SERT—"Philips G8 colour receiver" by R. Pratt at 19.00 at Renold Building, U.M.I.S.T.

18th. IERE/IEE—"A fully integrated communications system" by P. L. Dalgleish at 19.15 at Renold Building, U.M.I.S.T., Altrincham Street.

25th. SERT—"Evolution of radio communications and navigation in post war civil aircraft" by D. Allimundo at 20.00 at Renold Building, U.M.I.S.T.

## MIDDLESBROUGH

3rd. IEE—"Instrumentation problems in Polar exploration" by Dr. S. Evans at 18.30 at Cleveland Science Institute.

## NEWCASTLE-UPON-TYNE

3rd. Brit. Computer S.—"The origins of digital computing" by Prof. B. Randell at 19.00 at the University.

10th. IERE—"Engineer to manager—effecting the transition" by M. W. Lauerman at 18.00 at Ellison Building, The Polytechnic, Ellison Place.

## OXFORD

10th. IEE—"Stereophonic broadcasting" by Dr. G. J. Phillips at 19.00 at the S.E.B., 1 Woodstock Road, Yarnton.

## PLYMOUTH

3rd. RTS—"The impact of automation in television transmission" by G. A. McKenzie and R. H. Vivien at 19.30 at the Studios of Westward Television.

## READING

25th. IERE—"Integrated circuits in hi-fi systems" by B. A. Reed at 19.30 at the J. J. Thomson Laboratory, The University, Whiteknights Park.

## ROMFORD

10th. IERE—"The Victoria line" by V. H. Smith at 18.30 at Central Library.

## RUGBY

16th. IERE/IEE—"Digital voltmeters" by J. R. Pearce at 18.30 at College of Engineering Technology.

## SWINDON

2nd. IERE—"Application of protection devices on electricity supply systems" by H. L. Roistein at 18.15 at The College.

## THURSO

4th. IEE—"Instrumentation for oceanography" by B. S. McCartney at 19.30 at the Technical College.

## TREVENSON

9th. IERE—"Global communications—past, present and future" by R. J. Halsey at 19.00 at Cornwall Technical College.

## LATE FEBRUARY MEETINGS

### LONDON

24th. SERT—"Algorithms" by J. H. Robinson at 19.00 at the Manson Theatre, School of Hygiene & Tropical Medicine, Keppel St., W.C.1.

25th. IERE—"Television communication by satellite and conventional systems" by D. J. Whyte at 19.30 at the Medway College of Technology.

26th. Brit. Acoustical Soc.—Meeting on "Scattering phenomena in acoustics" at 14.30 at the Chelsea College of Science & Technology.

# Real & Imaginary

by "Vector"

## Sacred Cows and Other Fauna

The imminence of *W.W.*'s sixtieth birthday sent me scuttling to the back issues to see when 'Vector' first came down like a wolf on the fold. To my surprise I found that it's seven years come September—a mini-anniversary which will no doubt be celebrated by a decor of black crepe in the Editor's Sanctum.\* There is nothing quite so chastening as re-reading one's old copy, so if an aura of gloom envelopes this page, you'll know the reason why.

### Evil eye dept.

My maiden effort was, I see, a send-up of Radiolympia, a time-honoured institution which, by coincidence, folded shortly after, in defiance of my prediction that the next show would be held in a telephone kiosk. The second excursion was a similar exercise on the Farnborough Air Show, which from that time onward has been relegated from an annual to a biennial beanfeast. Was there, I began to wonder, something in this evil eye business after all?

Truly, pride goeth before a fall. I wish I could similarly report the demise of other, and more futile, sacred cows which were subsequently dealt with, but these, alas, have proved to be more resilient. For instance, there is the 'Crow-Bar Effect', a common phenomenon in large companies. This is a condition of self-oscillation using paper-work coupling and the net effect is akin to that produced by a high-power alternator which has had a crow-bar laid across its terminals—namely, a furious display of energy but no useful work done. With the proliferation of control departments to control those departments which control departments, this effect is lamentably on the increase.

Looking on the brighter side, while the heresy is still strongly held that the formation of super-groups will *ipso facto* provide a super-efficient electronics industry, I note with satisfaction that the projected welding of British instrument companies into one mammoth whole, which seemed imminent a year ago, now seems to have folded its tents. And (miracle of miracles) one or two influential voices are now being

raised against that arch-sacred cow, Economic Growth.†

But such trends are not moving fast enough for our health. If, therefore, I have a reader who is well versed in necromancy and would like to help the electronics industry, perhaps he would care to recommend a book, written at amateur level, on "The Do-it-yourself Evil Eye". I should be glad to pick up some tips.

### Physician, heal thyself

According to the *Sunday Telegraph* magazine, a gentleman called Mr. H. Ross Perot, of Dallas, Texas, owns most of a computer company called Electronic Data Systems Corporation. It seems that on April 23rd last, the Company had rather a bad day and Mr. Perot personally dropped just under £200,000,000 (yes, I know that sounds an awful lot of strawberries but that's what it says).

Upon the face of it, it looks as if one of Mr. Perot's computers wasn't really trying on April 23rd. A distinct lack of data transfer, if you ask me.

### Conservation year for television?

I see that in the January issue the Editor has been laying about him on the subject of the frequency allocation accorded to television broadcasting. No doubt his remarks will be hotly debated, but whatever the outcome, surely no-one will dispute that the present television system is woefully inefficient. I am not, in this context, casting aspersions on the programme content (which is a subjective matter anyway). When I say 'inefficient' I mean in terms of information conveyed in relation to bandwidth occupied. If there should be anyone who doubts this, let him try the simple experiment of switching on to a television play, first using vision only and, later, sound only. He will find that the sound channel enables you to follow the plot tolerably well, but with vision only you will be lost in a matter of seconds.

†For example H. V. Hodson "A False God of Growth?"—*Sunday Times*, Jan. 10th.

Necessity being the mother of invention, I hazard a guess that, supposing a goodly part of the television band was wrested for more deserving causes, we should see a great upsurge in technical innovation. Remember, we were quite content to ignore the inefficient and wasteful use of the side-band envelope in the black-and-white era. It wasn't until the exigencies of colour came along that ways and means of packing a colour sub-carrier inside it were developed. Similarly, if need arose, the wasteful areas of the present system, such as frame-to-frame redundancy, would be subjected to a flurry of intensive research and before we knew where we were we should be getting two programmes for the (bandwidth) price of one.

### Sprechen sie Deutsche?

A correspondent who is looking forward to visiting the International Spring Fair at Leipzig, complains that his phrase-book contains little in the way of technical expressions, with the notable exception of 'The wireless operator who grasped the spark gap will be cremated tomorrow,' which might fill a lull in the conversation. Anything to oblige, H.J.G. (Bootle). Here are a few items to help you on your way:—

slide rule . . . . .	gessenstik
computer . . . . .	maschinengessenstik
colour fringing . . . . .	blakrutzonblondenrinse
consonance . . . . .	alphabette mit der wowlz extrakten
convergence . . . . .	autobahn krasherpilup
delay line . . . . .	britischerpuffpufftraken
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gain control . . . . .	neinsalararinisen
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transistor radio . . . . .	skwawkenschreechen
iterative impedance . . . . .	grossenstutter
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microstrip . . . . .	midgetgirlishow
noise generator . . . . .	popgrupkaterwaulen
not-gate . . . . .	achtungderbulle
peak riding clipper . . . . .	rushourtiketinspektor
Poisson's equation . . . . .	einemannzfische = anothermannzpoisson
high pulse repetition . . . . .	longstemzdolifraulein mit der miniminiskirten
quartz . . . . .	zweipinten
store . . . . .	marxundspax
transfer impedance . . . . .	puffpuffdriverstriken

Happy landings, H.J.G., You should have a trip packed with incident.

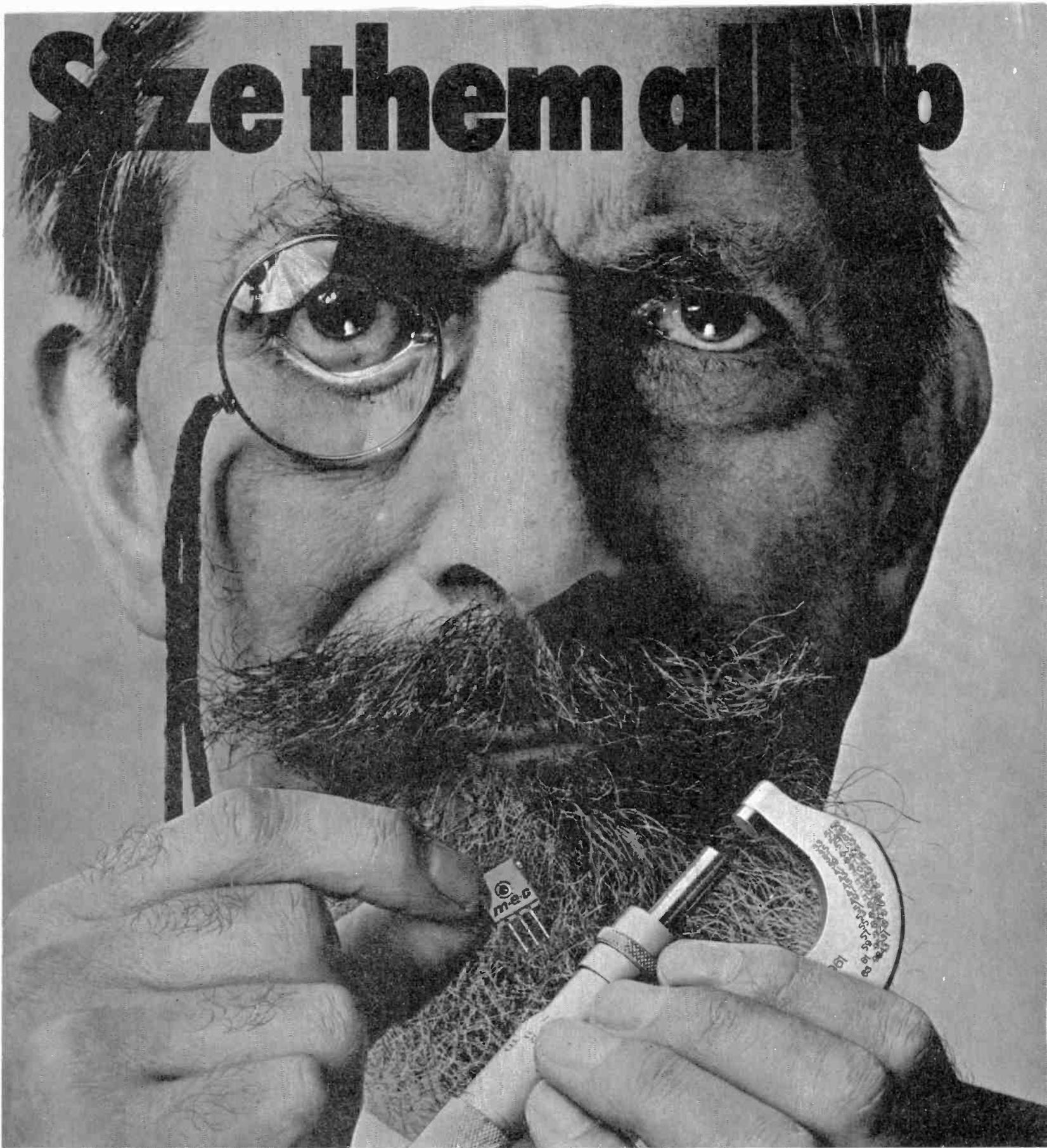
### Quote of the year

"What advice would you give a sixteen-year-old school leaver, with a few O-levels in science and maths, who is interested in electronics as a career?" This question was asked by a staff correspondent of *W.W.*'s sister journal *Electronics Weekly* of a member of the Careers Research Advisory Centre (C.R.A.C.) at the "Opportunity-70" exhibition which was held at Olympia in December.

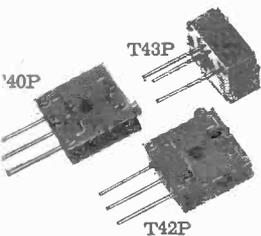
Answer: "Well, we usually send people like that over to Curry's stand in the corner."

\* Don't push your luck—Ed.

# Size them all up



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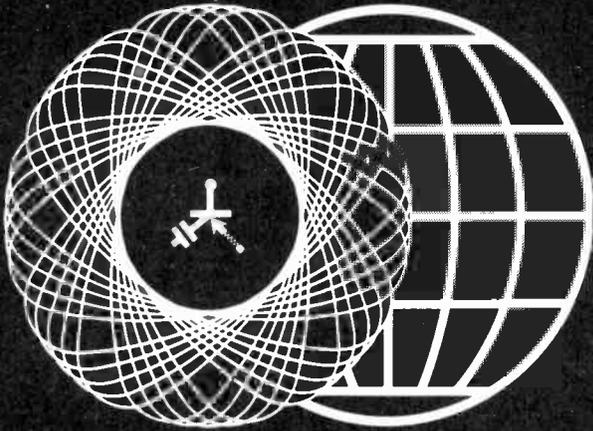
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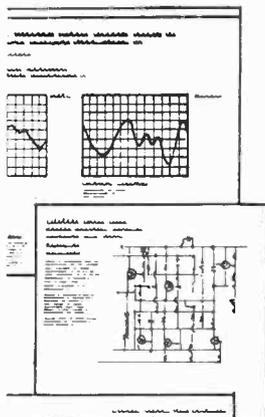
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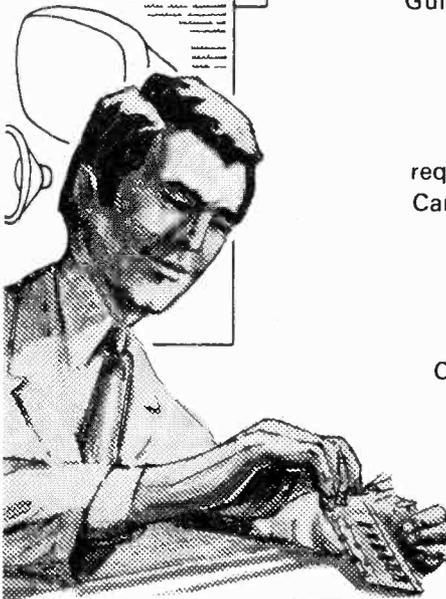
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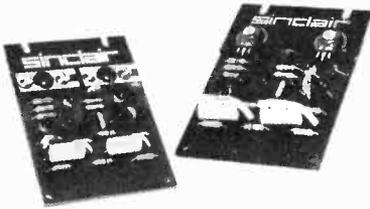
System	The Units to use	together with	Cost of Units
A Simple battery record player	<b>Z.30</b>	Crystal P.U., 12V battery volume control	<b>£9/6</b> (£4.47½)
B Mains powered record player	<b>Z.30, PZ.5</b>	Crystal or ceramic P.U. volume control etc.	<b>£9.9.0</b> (£9.45)
C 20+20 W. R.M.S. stereo amplifier for most needs	<b>2 x Z.30s, Stereo 60, PZ.5</b>	Crystal, ceramic or mag. P.U., most dynamic speakers, F.M. tuner etc.	<b>£23.18.0</b> (£23.90)
D 20+20 W. R.M.S. stereo amplifier with high performance spkrs.	<b>2 x Z.30s, Stereo 60, PZ.6</b>	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	<b>£26.18.0</b> (£26.90)
E 40+40 W. R.M.S. deluxe stereo amplifier	<b>2 x Z.50s, Stereo 60 PZ.8, mains trsfrmr</b>	As for D	<b>£32.17.6</b> (£32.87½)
F Outdoor P.A. system	<b>Z.50</b>	Mic., up to 4 P.A. speakers controls, etc.	<b>£5.9.6</b> (£5.47½)
G Indoor P.A.	<b>Z.50, PZ.8, mains transformer</b>	Mic., guitar, speakers, etc., controls	<b>£17.8.6</b> (£17.42½)
H High pass and low pass filters	<b>A.F.U.</b>	C, D or E	<b>£5.19.6</b> (£5.97½)
J Radio	<b>Stereo F.M. Tuner</b>	C, D or E	<b>£25.0.0</b>

WW—102 FOR FURTHER DETAILS

www.americanradiohistory.com

# Sinclair Project 60

## Z.30 & Z.50 power amplifiers



The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at full output and all lower outputs. Whether you use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and may be used with other units in the Project 60 range equally well.

**SPECIFICATIONS (Z.50 units are interchangeable with Z.30s in all applications).**

**Power Outputs**

**Z.30** 15 watts R.M.S. into 8 ohms using 35 volts; 20 watts R.M.S. into 3 ohms using 30 volts.

**Z.50** 40 watts R.M.S. into 3 ohms using 40 volts; 30 watts R.M.S. into 8 ohms, using 50 volts.

**Frequency response:** 30 to 300,000 Hz  $\pm 1$  dB

**Distortion:** 0.02% into 8 ohms

**Signal to noise ratio:** better than 70dB unweighted.

**Input sensitivity:** 250mV into 100 Kohms.

For speakers from 3 to 15 ohms impedance.

Size  $3\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{2}$  in.

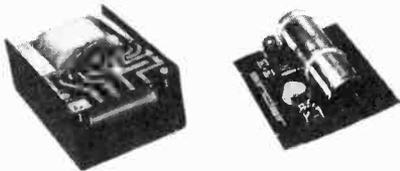
**Z.30**

Built, tested and guaranteed with circuits and instructions manual **89/6** (£4.47 $\frac{1}{2}$ )

**Z.50**

Built, tested and guaranteed with circuits and instructions manual **109/6** (£5.47 $\frac{1}{2}$ )

## Power Supply Units



Designed specially for use with the Project 60 system of your choice.

Illustration shows PZ.5 to left and PZ.8 (for use with Z.50s) to the right. Use PZ.5 for normal Z.30 assemblies and PZ.6 where a stabilised supply is essential.

**PZ-5** 30 volts un stabilised **£4.19.6** (£4.97 $\frac{1}{2}$ )

**PZ-6** 35 volts stabilised **£7.19.6** (£7.97 $\frac{1}{2}$ )

**PZ-8** 45 volts stabilised

(less mains transformer) **£5.19.6** (£5.97 $\frac{1}{2}$ )

**PZ-8** mains transformer **£5.19.6** (£5.97 $\frac{1}{2}$ )

## Guarantee

If within 3 months of purchasing Project 60 modules directly from us, you are dissatisfied with them, we will refund your money at once. Each module is guaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of the purchase date. There will be a small charge for service thereafter. No charge for postage by surface mail. Air-mail charged at cost

## Stereo 60 pre-amp/control unit



Designed for the Project 60 range but suitable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout, achieving a really high signal-to-noise ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.

**SPECIFICATIONS**

**Input sensitivities:** Radio—up to 3mV. Mag. p.u. 3mV; correct to R.I.A.A. curve  $\pm 1$  dB; 20 to 25,000 Hz. Ceramic p.u.—up to 3mV; Aux—up to 3mV.

**Output:** 250mV.

**Signal-to-noise ratio:** better than 70dB.

**Channel matching:** within 1dB.

**Tone controls:** TREBLE + 15 to -15dB at 10KHz; BASS + 15 to -15dB at 100Hz.

**Front panel:** brushed aluminium with black knobs and controls.

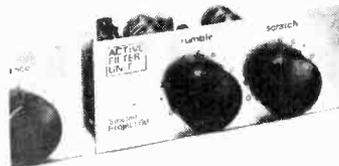
**Size:**  $8\frac{1}{2} \times 1\frac{1}{2} \times 4$  ins.

Built, tested

and guaranteed.

**£9.19.6** (£9.97 $\frac{1}{2}$ )

## Active Filter Unit



For use between Stereo 60 unit and two Z.30s or Z.50s, and is easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is suitable for use with any other amplifier system. Two stages of filtering are incorporated—rumble (high pass) and scratch (low pass). Supply voltage—15 to 35V. Current—3mA. H.F. cut-off (-3dB) variable from 28kHz to 5kHz. L.F. cut-off (-3dB) variable from 25Hz to 100Hz. Distortion at 1kHz (35V. supply) 0.02% at rated output.

Built, tested

and guaranteed

**£5.19.6** (£5.97 $\frac{1}{2}$ )

## Stereo FM Tuner



**first in the world to use the phase lock loop principle**

Before production of this tuner, the phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio over other systems. Now, for the first time, the principle has been applied to an FM tuner with fantastically good results. Other original features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stereo decoder and squelch circuit for silent tuning between stations. Sensitivity is such that good reception becomes possible in difficult areas. Foreign stations can be tuned in suitable conditions and often a few inches of wire are enough for an aerial. In terms of a high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically as the tuning control is rotated, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with any other high fidelity system.

**SPECIFICATIONS:**

**Number of transistors:** 16 plus 20 in I.C.

**Tuning range:** 87.5 to 108 MHz.

**Capture ratio:** 1.5dB

**Sensitivity:** 2 $\mu$ V for 30dB quieting; 7 $\mu$ V for full limiting.

**Squelch level:** 20 $\mu$ V.

**A.F.C. range:**  $\pm 200$  KHz

**Signal to noise ratio:** >65dB

**Audio frequency response:** 10Hz—15KHz ( $\pm 1$ dB)

**Total harmonic distortion:** 0.15% for 30% modulation

**Stereo decoder operating level:** 2 $\mu$ V

**Pilot tone suppression:** 30dB

**Cross talk:** 40dB

**I.F. frequency:** 10.7 MHz

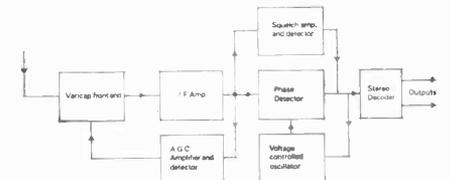
**Output voltage:** 2 x 150mV R.M.S

**Aerial Impedance:** 75 Ohms

**Indicators:** Mains on; Stereo on; tuning indicator

**Operating voltage:** 25-30 VDC

**Size:** 3.6 x 1.6 x 8.15 inches; 91.5 x 40 x 207 mm



Price: **£25** built and tested. Post free

To: SINCLAIR RADIONICS LTD LONDON ROAD ST. IVES HUNTINGDONSHIRE PE17 4HJ

Please send \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

Name \_\_\_\_\_  
 Address \_\_\_\_\_  
 \_\_\_\_\_

for which I enclose cash/cheque/money order.

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WW-103 FOR FURTHER DETAILS

# Sinclair IC10/Q16/Micromatic

## IC10



### The world's most advanced high fidelity amplifier

This is the world's first monolithic integrated circuit high fidelity power amplifier and pre-amplifier. The circuit itself is a chip of silicon only a twentieth of an inch square by one hundredth of an inch thick, having 5 watts RMS output (10 watts peak). It contains 13 transistors (including two power types), 2 diodes, 1 zener diode and 18 resistors, and is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins. This exciting device is more rugged and has considerable performance advantages, including complete freedom from thermal runaway and a very low level of distortion. The IC10 is primarily intended as a full performance high fidelity power and pre-amplifier, for which application it only requires the addition of such components as tone and volume controls and a battery or mains power supply. It may also be used in other applications including car radios, electronic organs, servo amplifiers (it is dc coupled throughout) etc.

### Circuit Description

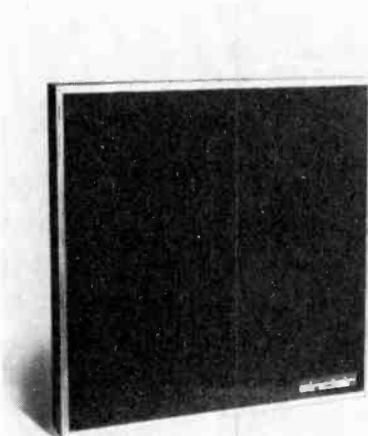
The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class AB output is used with closely controlled quiescent current which is independent of temperature. There is generous negative feedback round both sections and the amplifier is completely free from crossover distortion at all supply voltages, making battery operation eminently satisfactory.

Each IC10 is sold with a comprehensive manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include oscillators, etc. The pre-amp section can be used as an RF or IF, amplifier without any additional transistors.

### Specifications:

Output: 10 watts peak, 5 watts RMS continuous.  
 Frequency response: 5Hz to 100kHz  $1 \pm$  dB.  
 Total harmonic distortion: Less than 1% at full output.  
 Load impedance: 3 to 15 ohms.  
 Power gain: 110 dB (100,000,000,000 times) total.  
 Supply voltage: 8 to 18 volts. (A Sinclair power unit, PZ.7 is available for mains operation).  
 Size: 1 x 0.4 x 0.2 in. plus heat sink and tags.  
 Sensitivity 5 mV.  
 Input impedance: Adjustable externally up to 2.5 Mohms.  
 Price (with manual) **59/6** (£2.97½) post free.

## Q16



### High fidelity loudspeaker

The Q16 employs the well proven acoustic principles specially developed by Sinclair in which a special driver assembly is meticulously matched to the characteristics of the uniquely designed cabinet. In reviewing this exclusive Sinclair design, technical journals have justly compared the Q16 with much more expensive loudspeakers. Its shape enables the Q16 to be positioned and matched to its environment to much better effect than is the case with conventionally styled enclosures. A solid teak surround with a special all-over cellular foam front is used as much for appearance as its ability to pass all audio frequencies.

This elegantly designed shelf mounting speaker brings genuine high fidelity within reach of every music lover.

### Specifications:

Construction: Special sealed seamless sound or pressure chamber with internal baffle.  
 Loading: up to 14 watts TMS.  
 Input impedance: 8 ohms.  
 Frequency response: From 60 to 16,000 Hz, confirmed by independently plotted B and K curve.  
 Driver unit: Special high compliance unit having massive ceramic magnet of 11,000 gauss, aluminium speech coil and a special cone suspension for excellent transient response.  
 Size and styling: 9½ in square on face x 4½ in. deep with neat pedestal base. Black all-over cellular foam front with natural solid teak surround.  
 Price **£8.19.6.** (£8.97½).

## Micromatic



### Britain's smallest radio

Considerably smaller than an ordinary box of matches, this is a multi-stage AM receiver brilliantly designed to provide remarkable standards of selectivity, power and quality for its size. Powerful AGC counteracts fading from distant stations; bandspread at higher frequencies makes reception of Radio 1 easy. The plug-in magnetic earpiece provided matches the Micromatic's output to give wonderful standards of reproduction. Everything including the special ferrite rod aerial and batteries is contained within the minute and attractively designed case. Whether you build a Micromatic kit or buy this amazing receiver ready built and tested, you will find it as easy to take with you as your wrist watch, and dependable under the severest listening conditions.

### Specifications:

Size: 36 x 33 x 13 mm (1¼ x 1⅓ x ½ in.)  
 Weight: including batteries, 28.4 gm (1 oz.)  
 Case: Black plastic with anodised aluminium front panel and spun aluminium dial.  
 Tuning: medium wave band with bandspread at higher frequencies. (550 to 1,600 Hz).  
 Earpiece: Magnetic type.  
 On/off switching: By inserting and withdrawing earpiece plug.  
 Kit in pack with earpiece, case, instructions and solder **49/6** (£2.47½).  
 Ready built, tested and guaranteed, with earpiece **59/6** (£2.97½).

Two Mallory Mercury batteries type RM675 required. From radio shops, chemists, etc.

To: SINCLAIR RADIONICS LTD LONDON ROAD ST. IVES HUNTINGDONSHIRE PE17 4HJ

Please send

\_\_\_\_\_

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\_\_\_\_\_

Name

\_\_\_\_\_

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Address

for which I enclose cash/cheque/money order.

ww3/71

Sinclair Radionics Ltd., London Road,  
 St. Ives, Huntingdonshire PE17 4HJ.  
 Tel: St. Ives (048 06) 4311

**sinclair**

WW-104 FOR FURTHER DETAILS

# BI-PAK=LOW COST I.C.'s VALUE ALL THE WAY SUPER PAKS NEW BI-PAK UNTESTED SEMICONDUCTORS

BI-PAK Semiconductors now offer you the largest and most popular range of I.C.'s available at these EXCLUSIVE LOW PRICES. TTL Digital 74N Series fully coded, brand new. Dual in-line plastic 14 and 16 pin packages.

BI-PAK Order No.	Description	Price	Qty.	Prices 1-24	25-99	100 up
BP00 7400N	Quad 2-Input NAND GATE	33p	27p	23p		
BP01 7401N	Quad 2-Input NAND GATE—OPEN COLLECTOR	33p	27p	23p		
BP04 7404N	HEX INVERTER	33p	27p	23p		
BP10 7401N	Triple 3-Input NAND GATE	33p	27p	23p		
BP20 7402N	Dual 4-Input NAND GATE	33p	27p	23p		
BP30 7403N	Single 8-Input NAND GATE	33p	27p	23p		
BP40 7440N	Dual 4-Input BUFFER GATE	33p	27p	23p		
BP41 7441N	BCD to decimal decoder and N.I.T. Driver	£1.13	£1	87p		
BP42 7442N	BCD to decimal decoder (TTL O/P)	£1.13	£1	87p		
BP50 7450N	Dual 2-Input AND/OR/NOT GATE—expandable	33p	27p	23p		
BP53 7453N	Single 8-Input AND/OR/NOT GATE—expandable	33p	27p	23p		
BP60 7460N	Dual 4-Input—expandable	33p	27p	23p		
BP70 7470N	Single JK Flip-Flop—edge triggered	45p	40p	35p		
BP72 7472N	Single Master Slave JK Flip-Flop	45p	40p	35p		
BP73 7473N	Dual Master Slave JK Flip-Flop	50p	45p	40p		
BP74 7474N	Dual D Flip-Flop	50p	45p	40p		
BP75 7475N	Quad Bistable Latch	55p	50p	47p		
BP76 7476N	Dual Master Slave Flip-Flop with preset and clear	55p	50p	47p		
BP83 7483N	Four Bit Binary Adder	£1.30	£1.13	87p		
BP90 7490N	BCD Decade Counter	£1.13	£1	87p		
BP92 7492N	Divide by 12 4 Bit binary counter	£1.13	£1	87p		
BP93 7493N	Divide by 16 4 Bit binary counter	£1.13	£1	87p		
BP94 7494N	Dual Entry 4 Bit Shift Register	£1.13	£1	87p		
BP95 7495N	4 Bit Up-Down Shift Register	£1.13	£1	87p		
BP96 7496N	5 Bit Shift Register	£1.20	£1.05	87p		

Data are available for the above Series of Integrated Circuits in booklet form. Price 13p.

## TTL INTEGRATED CIRCUITS

Manufacturers' "Fall outs"—out of spec. devices including functional units and part functional but classed as out of spec. from the manufacturers very rigid specifications. Ideal for learning about I.C.'s and experimental work, on testing, some will be found perfect.

PAK No.	Description	Price	Qty.	Prices 1-24	25-99	100 up
UI00	5 x 7400N	50p				
UI01	5 x 7401N	50p				
UI02	5 x 7402N	50p				
UI03	5 x 7403N	50p				
UI04	5 x 7404N	50p				
UI05	5 x 7405N	50p				
UI06	5 x 7410N	50p				
UI07	5 x 7420N	50p				
UI08	5 x 7440N	50p				
UI09	5 x 7441N	50p				
UI10	5 x 7442N	50p				
UI11	5 x 7450N	50p				
UI12	5 x 7451N	50p				
UI13	5 x 7460N	50p				
UI14	5 x 7470N	50p				
UI15	5 x 7472N	50p				

Packs cannot be split but 20 assorted pieces (our mix) is available as PAK UI0X1. Every PAK carries our BI-PAK Satisfaction or money back GUARANTEE.

## LINEAR I.C.'s

Type No.	Case	Leads	Description	Price	Qty.	Prices 1-24	25-99	100 up
BP201C—8L20/c	TO-5	8	G.P. Amp	63p	53p	45p		
BP701C—8L70/C	TO-5	8	OP Amp.	63p	50p	45p		
BP702C—8L70ZC	TO-5	8	OP Amp Direct O/P	63p	50p	45p		
BP702—72702	D.L.L.	14	G.P. O.P. Amp (Wide Band)	53p	45p	40p		
BP708—72708	D.L.L.	14	High Gain OP Amp.	53p	45p	40p		
BP709P—µA709C	TO-5	8	High Gain OP Amp.	53p	45p	40p		
BP741—72741	D.L.L.	14	High Gain OP Amp (Protected)	75p	60p	50p		
µA703C—µA703C	TF-5	6	R.F.—IF Amp	43p	35p	27p		
TAA263	TO-72	4	A.F. Amp	70p	60p	55p		
TAA293	TO-74	10	G.P. Amp	90p	75p	70p		

## RTL FAIRCHILD (U.S.A.) I.C.'s

RTL Micrologic Circuits	Qty.	Prices each
Epoxy case To-5 temp. range 15°C to 55°C	1-11	12-24 25-99 100+
µL900 Buffer	40p	35p 33p 27p
µL 914 Dual two-input GATE	40p	35p 33p 27p
µL 923 J-K Flip-Flop	53p	50p 47p 45p

Full data and circuits for IC's in Booklet form price 7p each.

## GENERAL PURPOSE GERM. PNP POWER TRANSISTORS

Coded GP100. BRAND NEW TO-3 CASE. POSSIBLE REPLACEMENTS FOR OC25-28-29-30-35-36. NKT401-403-404-405-406-450-451-452-453. T13027-3028. 2N250A, 2N456A-457A-458A. 2N511-511A & B. 2G220-222. ETC. SPECIFICATION V<sub>CE0</sub> 80V V<sub>CE0</sub> 50V IC 10A PT 30 WATTS HEE 30-170. PRICE: 1-24 25-99 100+ 43p each 40p each 36p each

## GENERAL PURPOSE SILICON NPN POWER TRANSISTORS

Coded GP300. BRAND NEW TO-3 CASE. POSSIBLE REPLACEMENT FOR 2N3055, BDX20, BDX11. SPECIFICATION: V<sub>CE0</sub> 100V. V<sub>CE0</sub> 60V. IC 15 AMPS. PT. 115 WATTS. Hfe 20-100. FTI MHZ. PRICE: 1-24 25-99 100+ 55p each 50p each 47p each

## SEMICONDUCTOR HANDBOOK

240 PAGES OF SUGGESTED CIRCUITS—TRANSISTOR OUTLINES AND SEMICONDUCTOR SPECIFICATIONS. INTRODUCTION AND EXPLANATION IN 11 LANGUAGES: ENGLISH, DUTCH, FRENCH, GERMAN, INDO-NESEAN, SWEDISH, SPANISH, PORTUGUESE, ITALIAN, ARABIAN, SERBO-CROATIAN. A HANDBOOK FOR ALL SEMICONDUCTOR USERS. (DUTCH PUBLICATION). PRICE £1.43 incl. P. & P.

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Q 4	6	Matched trans. OC44/45/81/81D	50p
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Q 7	4	AC 128 trans. P.N.P. high gain	50p
Q 8	4	AC 126 trans. P.N.P.	50p
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Q 11	2	AC 127/128 Comp. pairs PNP/NPN	50p
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Q 13	3	AF 117 type trans.	50p
Q 14	3	OC 171 H.F. type trans.	50p
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Q 16	2	GBT80 low noise Germ. trans.	50p
Q 17	3	NPN 1 ST141 & 2 ST140	50p
Q 18	4	Madt's 2 MAT 100 & 2 MAT 120	50p
Q 19	3	Madt's 2 MAT 101 & 1 MAT 121	50p
Q 20	4	OC 44 Germ. trans. A.F.	50p
Q 21	3	NPN NPN Germ. trans.	50p
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Q 24	8	OA 81 diodes	50p
Q 25	6	IN914 Sil. diodes 75 PIV 75mA	50p
Q 26	8	OA95 Germ. diodes sub-min.	50p
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Q 30	7	Sil. switch trans. 2N706 NPN	50p
Q 31	6	Sil. switch trans. 2N708 NPN	50p
Q 32	3	PNP Sil. trans. 2 x 2N1131, 1 x 2N1132	50p
Q 33	3	Sil. NPN trans. 2N1711	50p
Q 34	7	Sil. NPN trans. 2N2369, 500MHZ	50p
Q 35	3	Sil. NPN TO-5 2 x 2N2904 & 1 x 2N2905	50p
Q 36	7	2N3646 TD-18 plastic 300MHZ NPN	50p
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U5	60 200mA Sub-min. Sil. Diodes	50p
U6	30 Silicon Planar Transistors NPN sim. B8Y95A, 2N706	50p
U7	16 Silicon Rectifiers Top-Hat 750mA up to 1,000V	50p
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U33	15 Plastic case 1 amp Silicon Rectifiers IN4000 series	50p
U34	30 Sil. PNP alloy trans. TO-5 BCY26, 28302/4	50p
U35	25 Sil. Planar trans. PNP TO-18 2N2906	50p
U36	25 Sil. Planar NPN trans. TO-5 BFY50/51/52	50p
U37	30 Sil. alloy trans. 80-2 PNF, OC200 28322	50p
U38	20 Fast Switching Sil. trans. NPN 400 Mc/s 2N3011	50p
U39	30 RF Germ. PNP trans. 2N1303/5 TO-5	50p
U40	10 Dual trans. 6 lead TO-5 2N2060	50p
U41	25 RF Germ. trans. TO-1 OC45 NKT72	50p
U42	10 VHF Germ. PNP trans. TO-1 NKT667 AF117	50p
U43	25 Sil. trans. Plastic TO-18 AF BC113-114	50p
U44	20 Sil. trans. Plastic TO-5 BC115-116	50p

Code Nos. mentioned above are given as a guide to the type of device in the Pak. The devices themselves are normally unmarked.

TRANSISTOR EQUIVALENTS BOOK. A complete cross reference and equivalent book for European, American and Japanese Transistors. Exclusive to BI-PAK. 75p each.

FREE One 50p Pack of your own choice free with orders valued £4 or over.

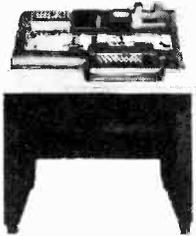
## NEW LOW PRICE TESTED S.C.R.'s

PIV	1A	3A	7A	10A	16A	30A
TO5	25p	25p	47p	50p	53p	£1.15
TO6	25p	25p	50p	53p	58p	£1.40
TO7	25p	25p	50p	53p	58p	£1.40
TO8	25p	25p	50p	53p	58p	£1.40
TO9	25p	25p	50p	53p	58p	£1.40
TO10	25p	25p	50p	53p	58p	£1.40
TO11	25p	25p	50p	53p	58p	£1.40
TO12	25p	25p	50p	53p	58p	£1.40
TO13	25p	25p	50p	53p	58p	£1.40
TO14	25p	25p	50p	53p	58p	£1.40
TO15	25p	25p	50p	53p	58p	£1.40
TO16	25p	25p	50p	53p	58p	£1.40
TO17	25p	25p	50p	53p	58p	£1.40
TO18	25p	25p	50p	53p	58p	£1.40
TO19	25p	25p	50p	53p	58p	£1.40
TO20	25p	25p	50p	53p	58p	£1.40

## SILICON RECTIFIERS—TESTED

PIV	300mA	750mA	1A	1.5A	3A	10A	30A
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**LARGE RANGE OF  
LOW COST  
COMPUTERS &  
PERIPHERAL  
EQUIPMENT  
FROM A SINGLE SOURCE**



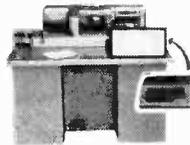
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EQUIPMENT AT  
LOWEST UK PRICES  
AND SHORT DELIVERY**

**IBM**  
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063 077 082 083 084  
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557 etc.

**FROM STOCK, IMMEDIATE DELIVERY**  
PDP8S ASR33 IBM1401 C6 Choice of configurations.  
NCR 400-208 Choice of two.  
ELLIOT 803B Choice of two.  
LITTON 1238 One available.  
FERRANTI ARGUS 400B Four available.

**PLEASE WRITE FOR DETAILS OF  
SPECIFIC EQUIPMENT, DATA PREP.  
—OR COMPLETE SYSTEMS**

**ICT HOLLERITH Type 29.80 column  
Punch.** A well-proven electro-mechanical card punch, with duplicating, spacing, and skipping facilities. Two types of keyboard are available for this model: Alpha/Numeric and Alphabetic Numeric. **FEATURES:** Motor cut-out switch for clearing card jams. Stop Lever for stopping card at the 80th column.

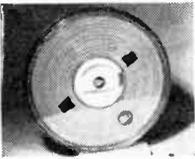


**ICT MODEL 129 VERIFIERS**  
The type 129 programme board verifier is an electronic operated machine which automatically verifies numeric, alphabetic and multiple punchings in standard 80 column cards with rectangular holes. Available from stock.

**REBUILT—DELIVERY FROM STOCK**

**COMPUTER QUALITY ½ in. MAGNETIC TAPE CERTIFIED 550 B.P.1.  
800 B.P.1. ON 2,400-ft. REELS. GUARANTEED  
REPLACEMENT IF FAULTED..... £6.50**

¾ in. Highest grade 2,400 ft..... **£3.00**  
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1 in. metal 10½ in. dia. spool and cassette..... **£2.50**  
¾ in. N.A.B. centres 10½ in. spool only..... **£1.00**



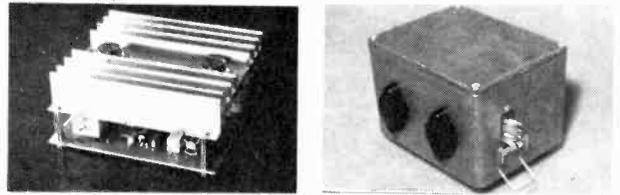
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VERIFIERS 80 COLUMN**  
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WW—106 FOR FURTHER DETAILS

**CAPACITOR DISCHARGE IGNITION SYSTEM**



The popular Wireless World Capacitor-Discharge Ignition system is now available in two versions. The original unit, comprising a printed-circuit board with stand-off heat-sink and separate transformer, or the mechanically re-designed unit with printed-circuits and a transformer contained within a die-cast box; the transistors and thyristor being mounted on the outside of the case and supplied with snap-on plastic covers. This version also includes a plug and socket for ease of connection, together with a conversion plug providing instant change-over to conventional ignition.

Both versions embody printed-circuit boards designed for positive and negative earth ignition systems thus enabling simple conversion to opposite polarity if the vehicle is subsequently changed. A complete complement of components is supplied with each kit together with ready-drilled and roller-tinned printed-circuit board, fully machined heat-sink (or die-cast box) and a custom-wound transformer.

Suitable for 12V. systems only. All components available separately. Wiring details are supplied for both polarity systems. Please state polarity required so that correct semiconductors can be supplied. Complete assembly and wiring manual for boxed version 5/-, refundable on purchase of kit.

**PRICE 'OPEN VERSION' £9.25 plus 50p. Carriage.  
'ENCLOSED VERSION' £11.25 plus 50p. Carriage.  
TRADE ENQUIRIES INVITED. MAIL ORDER ONLY.**

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**COMPUTER MULTI-CORE CABLES**

12, 14/0076 copper cores, each one insulated by coloured P.V.C. then separately screened, the 12 metal braided cores laid together and P.V.C. covered overall making a cable just under 1 in. dia. but quite pliable. Price 38p per ft. Any length out. Other sizes available 7 core 25p ft., 6 core 20p ft., 4 core 18p ft.

**AC FAN**

Small but very powerful mains motor with 5 in. blades. Ideal for cooling equipment or as extractor. Silent but very efficient. 90p, post 23p. Mounts from back or front with 4BA screws.

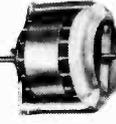


**Double Leaf Contact**

Very slight pressure closes both contacts. 6p each. 60p doz. Plastic push-rod suitable for operating. 5p each. 45p doz.

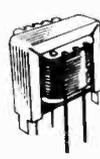
**PAPST MOTORS**

Est. 1/20th h.p. Made for 110-120 volt working, but two of these work nicely together on our standard 240 volt mains. A really beautiful motor, extremely quiet running and reversible. £1.50 each. Postage one 23p, two 33p.



**2 SPEED REVERSIBLE TAPE MOTOR**

230v, 50Hz. Capacitor start. Reversible. Normal construction. Size: 3 1/2 in. dia. x 2 in. deep. Approx. 1/40th h.p. £2 with Condenser, plus 22p post and insurance.



**MIDGET OUTPUT TRANSFORMER**

Ratio 140 : 1. Size approx. 1 1/2 in. x 1/2 in. Primary impedance 450 Ω. Connection by flying leads 23p each. £2.40 doz.

**MIDGET OUTPUT TRANSFORMER**

Ratio 80 : 1. Size approx. 1 1/2 in. x 1/2 in. Primary impedance 192 Ω. Printed circuit board connection 28p each. £3 doz.

**CHART RECORDER MOTOR**

Small (2 in. diameter approx.) instrument motor with fixing flange and spindle (1/2 in. long, 1/4 in. diameter); integral gearbox gives 1 rev. per 24 hours. £1.

**IGNITION (E.H.T.) TRANSFORMER**

Made by Parmeko Ltd. Primary 240v, 50 c.p.s. Secondary 5kV at 23mA. Size approx. 4 1/2 in. x 3 1/2 in. x 2 1/2 in. thick. Price £1.50 + 23p.

**FLUORESCENT CONTROL TIPS**

Each kit comprises seven items—Choke, 2 tube ends, starter, starter holder and 2 tube clips, with wiring instructions. Suitable for normal fluorescent tubes or the new "Grolux" tubes for fish tanks and indoor plants. Chokes are super-silent, mostly resin filled. Kit A—15-20 w. £1. Kit B—30-40 w. £1. Kit C—80 w. £1.20. Kit D—125 w. £1.20. Kit E—150 w. £1.20. Kit F for 8ft, 125 w. tube £1.75. Kit MF1 for 6in., 9in. and 12in. miniature tubes. £1. Kit MF2 for 21in. 13 w. miniature tube. £1. Postage on Kits A and B 23p for one or two kits then 23p for each two kits ordered. Kits C, D and E 23p on first kit then 18p for each kit ordered. Kit F 33p then 23p for each kit ordered. Kit MF1 18p on first kit then 18p on each two kits ordered.

**MAINS TRANSISTOR POWER PACK**

Designed to operate transistor sets and amplifiers. Adjustable output 6v., 9v., 12 volts for up to 500mA (class B working). Takes the place of any of the following batteries: PP1, PP3, PP4, PP6, PP7, PP9, and others. Kit comprises: mains transformer, rectifier, smoothing and load resistor, condensers and instructions. Retail snip at only 85p, plus 18p postage.

**3 DIGIT COUNTER**

For Tape Recorder or other application, resettable by depressing button. Price 28p.



**ISOLATION SWITCH**

20 amp D.P. 250 Volts. Ideal to control Water Heater or any other appliance. Neon indicator shows when current is on. 23p; £2.40 per dozen.



**LIGHT CELL**

Almost zero resistant in sunlight increases to 10 K. Ohms in dark or dull light. epoxy resin sealed. Size approx. 1 in. dia. by 1/2 in. thick. Rated at 500 MW. wire ended. 43p. Suit most circuits.

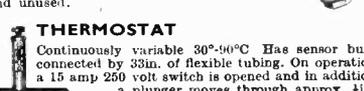
**5A 3-PIN SWITCHED SOCKETS**

An excellent opportunity to make a neat bench or board you may need or to stock up for future jobs. This month we offer 6 British made (Hicraft) bakelite flush mounting shuttered switch sockets for only 50p plus 18p post and insurance. (20 boxes post free.)



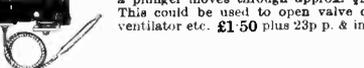
**MOTOR WITH GEARBOX**

Very powerful 7 r.p.m., operates from standard A.C. mains. £1.50, plus 18p P. & P.



**TRANSDUCER**

Made by Acos, reference No. 1.D.1001. For measuring vibration, etc., to be used in conjunction with "G" Meter. Regular price £5. Our price £2.50. Brand new and unused.



**THERMOSTAT**

Continuously variable 30°-90°C Has sensor bulb connected by 33in. of flexible tubing. On operation a 15 amp 250 volt switch is opened and in addition a plunger moves through approx. 1/2 in. This could be used to open valve on ventilator etc. £1.50 plus 23p p. & ins.

**DISTRIBUTION PANELS**

Just what you need for work bench or lab. 4 x 13 amp sockets in metal box to take standard 13 amp fused plugs and on/off switch with neon warning light. Supplied complete with 7 feet of heavy cable. Wired up ready to work. £2 less plug: £2.25 with fitted 13 amp plug: £2.40 with fitted 15 amp plug, plus 23p P. & I.



**STANDARD WAFER SWITCHES**

Standard size 1 1/2 wafer—silver-plated 5-amp contact, standard 1/2 spindle 2" long—with locking washer and nut.

No. of Poles	2 way	3 way	4 way	5 way	6 way	8 way	9 way	10 way	12 way
1 pole	33p	33p							
2 poles	33p	33p							
3 poles	33p	33p							
4 poles	33p	33p							
5 poles	33p	33p							
6 poles	33p	33p							
7 poles	33p	33p							
8 poles	33p	33p							
9 poles	33p	33p							
10 poles	33p	33p							
11 poles	33p	33p							
12 poles	33p	33p							

**HONEYWELL PROGRAMMER**

This is a drum type timing device, the drum being calibrated in equal divisions for switch purposes with trips which are infinitely adjustable for position. They are also arranged to allow 2 operations per switch per rotation. There are 15 changeover micro switches each of 10 amp type operated by the trips thus 15 circuits may be changed per revolution. Drive motor is mains operated 5 revs. per min. Some of the many uses of this timer are Machinery control, Boiler firing, Dispensing and Vending machines. Display lighting animated signs, Signalling etc. Price from Makers probably over £10 each. Special snip price £5.75 plus 25p post and ins. Don't miss this terrific bargain.



**THIS MONTH'S SNIP**

**ELECTRIC TIME SWITCH**

Made by Smiths these are A.C. mains operated. NOT CLOCKWORK. Ideal for mounting on rack or shelf or can be built into box with 13A socket. 2 completely adjustable time periods per 24 hours, 5 amp changeover contacts will switch circuit on or off during these periods. £2.50, post and ins. 23p. Additional time contacts 50p pair.

**COMPUTER TAPES**

2,400ft. of the best magnetic tape money can buy. Made by E.M.I. lin. wide, almost unbreakable and on a 104in. metal computer spool. Users have claimed successful results with video as well as sound recordings. £1 plus 33p post. Cassette to hold spool 50p extra.



**20 AMP ELECTRICAL PROGRAMMER**

Learn in your sleep! Have Radio playing and kettle boiling as you awake—switch on lights to ward off intruders—have warm house to come home to. All these and many other things you can do if you invest in an Electrical Programmer. Made by the famous Smiths Instrument Company. This is essentially a 230/240 volt mains operated clockwork and a 20 amp Switch, the switch-off time of which can be delayed up to 12 hours (continuously variable not stepped). Similarly the switch-on time can be delayed. This is a beautiful unit, size 5 1/2 x 3 1/2 x 2 1/2 in. deep. Metal encased, glass fronted with chrome surround. Offered at £2.40 plus 23p postage and insurance.



**INTEGRATED CIRCUITS**

A parcel of integrated circuits made by the famous Plessey Company. A once in a lifetime offer of Micro-electronic devices well below cost of manufacture. The parcel contains 5 ICs all new and perfect, first grade device definitely not sub-standard or seconds. The ICs are all single silicon chip General Purpose Amplifiers. Regular price of which is well over £1 each. Full circuit details of the ICs are included and in addition you will receive a list of 50 different ICs available at bargain prices 25p upwards with circuits and technical data of each. Complete parcel only £1 post paid or list and all technical data.

**4 AMP VARIAC CONTROLLERS**

With this you can vary the voltage applied to your circuit from zero to 270 volts without changing and the heat. One obvious application therefore is to dim lighting. Ex. equipment but little used—as good as new offered at approx. half price—£5 plus 63p post and ins.



**BARGAIN OF THE YEAR**

**MICROSONIC RADIOS**

7 transistor Key chain Radio in very pretty case, size 2 1/2 x 2 1/4 x 1 1/4 in.—complete with soft leather zipped bag. Specification: Circuit: 7 transistors superheterodyne Frequency range: 530 to 1600 Kc/s. Sensitivity: 5 mV/m. Intermediate frequency: 465 Kc/s. or 455 Kc/s. Power output: 40mW. Antenna: ferrite rod. Loudspeaker: Permanent magnet type. In transit from the East, these sets suffered slight corrosion as the batteries were left in, but when this corrosion is cleared away they should work perfectly—offered without guarantee except that they are new. £1.25 plus 13p post and insurance. Less batteries. Six for £7, post free. Rechargeable batteries 43p per pair.



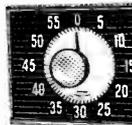
**ERGOTROL UNITS**

These units made by the Mullard Group are for operating and controlling d.c. Motors and equipment from A.C. mains. Thyristors are used and these supply a variable d.c. resulting in motor speed control and operating efficiency far superior to most other methods. The units are contained in wall mounting cabinets with front control panel on which are fuses—push buttons for on/off and the variable thyristor firing control. 4 models are available—all are brand new in makers cases: Model 2410 for up to 5 amps £17.50 Model 2411 for up to 10 amps £27.50 Model 2413 for up to 45 amps £47.50 Model 2415 for up to 80 amps £85.00 Note: 2415 is a floor mounting unit.



**1 HOUR MINUTE TIMER**

Made by famous Smiths company, these have a large clear dial, size 4 1/2 in. x 3 1/2 in., which can be set in minutes up to 1 hour. After preset period the bell rings. Ideal for processing, a memory jogger or, by adding simple lever, would operate micro-switch. £1.15.



**2kW FAN HEATER**

Three position switching to suit changes in the weather. Switch up for full heater (2kW), switch down for half heat (1kW), switch central blower cold for summer cooling—adjustable thermostat acts as auto-control and safety cut-out. Complete kit. £3.75. Post and ins. 38p.

**UNDER-FLOOR HEATING CABLE**

200ft. lengths, suitable for dissipating 1,000 watts at 80 volts. Join three in series to make a 240-volt mains-operated element of 3kW. Price £1 per length, 23p post on any quantity.

**3-CORE LEADS**

Heavy duty 23/36, average length 5ft. 50p per dozen lengths, plus 23p post and ins.

**CONSTRUCTORS' PARCEL**

1. Plessey miniature 2-gang tuning condenser with built-in trimmers and wave gang switch. 2. Ferrite slab aerial with coils to suit the above tuning condenser. 3. Circuit diagram giving all component values for 6-transistor circuit covering full medium wave and the long wave band around Radio 2. The three items for only 40p which is half of the price of the tuning condenser alone.

**MAINS RELAY** 200/250v. with 3 10 amp contacts. This is a very well made relay, which being very small only 1 1/2 x 1 x 1 in. approx., will fit into confined spaces. 63p each. £6.75 per dozen.

**HEARING AID AMPLIFIERS** 3 transistors and associated condensers and resistors on a little printed circuit board, the whole thing only about half as big as an Oxycube. If you are making miniature equipment then these may well be just what you are looking for. £1.75 each.

**LARGE PANEL MOUNTING MOVING COIL METERS**

Size 5 in. x 4 in. Centre zero 200-0-200 micro amp, made by Sangamo Weston. Regular price probably £5. Our price £3. Ditto but 100-0-100 £4.

**A.C. AMMETER**

0-5 amps., flush mounting, moving iron. Ex-equipment but guaranteed perfect. £1.50.

**CIRCUIT BOARDS**

Heavy copper on 3/32 paxolin sheet, ideal for making power packs, etc., as sheet is very strong and thick enough to allow copper to be cut away with hacksaw blade. 5 in. x 5 in. 8p each. 15 in. x 5 in. 23p each.

**SUB-MINIATURE MOVING COIL MICROPHONE**

as used in behind the ear deaf aids Acts also as earphone size only 1/2 in. x 1/2 in. Regular price probably £3 or more. Our price £1. Note these are ex-equipment but if not in perfect working order they will be exchanged.



**MAINS OPERATED CONTACTOR**

220/240v. 50 cycle solenoid with laminated core so very silent in operation. Closes 4 circuits each rated at 10 amps. Extremely well made by a German Electrical Company. Overall size 2 1/2 x 2 x 2 in. £1 each.

**SIEMERSTAT CONTROL SWITCH**

Combined on-off switch and "heat on" regulator intended for automatic temperature regulation of electric hot plates up to 3kW. Official rating 15A 200-250V A.C. size 2 1/2 x 2 in. deep. Single hole fixing 63p. Knob 23p extra.

**AUTO-ELECTRIC CAR AERIAL** with dashboard control switch—fully extendable to 40in. or fully retractable. Suitable for 12v positive or negative earth. Supplied complete with fitting instructions and ready wired dashboard switch. £6 plus 25p post and ins.



**TOGGLE SWITCH**

3 amp 250v. with fixing ring. 7 1/2p each 75p doz.



**MICRO SWITCH**

5 amp. changeover contacts, 9p each, 90p doz. 15 amp. on/off 10p each or £1.05 doz.



**MINIATURE EAR PIECE**

As used with imported pocket radios. 8p each 75p doz.



**15/20 AMP CONNECTORS**

Polythene insulated 12-way strip. 13p each £1.20 doz.



**13 AMP FUSED SWITCH**

Made by G.E.C. For connecting water heater etc., into 13 amp ring main. Flush type 18p each £1.50 doz. Metal boxes for surface mounting 8p each 75p doz.



**13 AMP SPUR UNIT**

By G.E.C. for connecting clock, etc., to ring main. Pull-out fuse. Flush mounting. Cream. 13p each: £1.20 doz.



**MAINS MOTOR**

Precision made—as used in record decks and tape recorders—ideal also for extractor fans, blower, heater, etc. New and perfect. Snip at 50p. Postage 15p for first one then 5p for each one ordered. 12 and over post free.



**MINIATURE WAFER SWITCHES**

2 pole, 2 way—4 pole, 2 way—3 pole, 3 way—4 pole, 3 way—2 pole, 4 way—3 pole, 4 way—2 pole, 6 way—1 pole, 12 way. All at 18p each, £1.80 dozen, your assortment.



**MINIATURE SLIDE SWITCH**

3 pole change-over. 15p each £1.50 doz. Heavy duty 250 watt Model, not Weller, but by a famous Italian maker. £4 plus 33p postage and insurance.



A New Service to Readers. A bulletin bringing news of new lines, special snips and "too few to advertise" lines will be posted to subscribers during first week of each month. The bulletin will be called "Advance Advert News" and the Subscription is 60p per year. Subscribers will also receive our completed 1971 catalogue when this is published.

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Also 102/3 Tamworth Road, Croydon



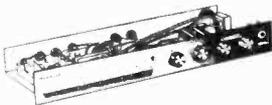
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## ENGLAND'S LEADING ELECTRONIC CENTRES

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### HENELEC SELF-POWERED PRE-AMPLIFIERS



IC STEREO



FET 154



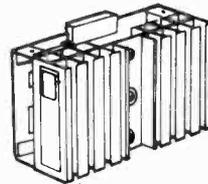
FET9/4

Brochure No. 25 on request

SLIM MODERN DESIGNS USING THE LATEST SILICON TRANSISTORS, FET's and IC's. DIN SOCKETS, ETC. fitted. PUSH-BUTTON SELECTION,  $\pm 20$ dB. Bass and treble boost and cut. All inputs provided plus TAPE RECORD and REPLAY. Specifically designed for use with PA25 and PA50 Amplifiers GOLD AND SILVER FINISH. Mains operated. Supplied with all plugs etc. ADJUSTABLE OUTPUT UP TO 1 VOLT. Simple mounting. Also suitable for use with Amplifier Models MPA 12/3 and MPA 12.15.

- ★ **FET9/4.** Mono with built-in mix. mixer. Accepts any ceramic or crystal cartridge. Plus tuner, tape, etc. Price **£12.50** p.p. 20p.
- ★ **FET154 STEREO.** Magnetic cart., input, tuner, tape, etc. Beautiful stereo sound. Price **£16.50** p.p. 25p.
- ★ **I.C. STEREO** All facilities plus headphone socket without amplifiers. Uses IC's, FET's etc. Price **£24.00** p.p. 30p

**SIMPLICITY TO MOUNT—EASY TO USE—DESIGNED FOR QUALITY, PERFORMANCE AND PRICE**



### LOOK AT THE SPECIFICATIONS!

25 WATT & 50 WATT RMS SILICON AMPLIFIERS

- At full power 0.3% distortion.
- At full power—1dB 11c/s to 40 kc/s.
- Response—1dB 11 c/s to 100 kc/s.
- Rise time 2  $\mu$  sec.
- Short circuit proof plus limiting cct.

**PA 25** 10 transistor all silicon differential input 400 mV sensitivity. 25 watts Rms into 8 ohms. Supplied with edge connector harness size 5" x 3" x 2".

**PA 50** 12 transistor version 50 watts Rms into 3 to 4 ohms. Size 5" x 3" x 4".

**MU 442.** Power supply for one or two PA 25 or one PA 50. PA 25 **£7.50** p.p. 15p. PA 50 **£9.50** p.p. 15p. **MU 442** **£6.00** p.p. 25p. All units. No soldering—just edge connectors and plugs.

### TEST EQUIPMENT

For Educational, Professional and Home Constructors



**AF105** 50k/volt multi-meter (illus.). Price **£8.50** p.p. 20p. Leather case **£1.42**

**200H** 20k/volt. Price **£3.87** p.p. 20p. Case **62p**

**500** 30k/volt multi-meter Price **£8.85** p.p. 20p. Leather case **£1.50**



**THL 33** 2k/volt. Price **£4.12** p.p. 15p. Leather case **£1.15**

**TE65** Valve voltmeter (illus.) **£17.50** p.p. 40p

**VM51** Transistorised AF/RF millivoltmeter. Price **£32.00** p.p. 40p

**TE22** Audio Generator. Price **£17.00** p.p. 35p.



**TE20D** RF generator (illus.). Price **£15.00** p.p. 35p

**TE23D** Matching audio generator. Price **£17.00** p.p. 35p

**TE15** Grid dip meter. Price **£12.50** p.p. 20p

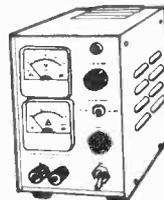


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\***CI-5** Scope. 3" tube 10 Mc/s PB. Price **£39.00** p.p. 50p

\***CI-16** Double beam scope. Price **£87.00** p.p. 50p

\* Leaflet No. 19 on request.



**RP40** (illus.) Variable 5-20v. 0.2 amps. Price **£25.50** p.p. 47p

**RP24** 12 volt  $\pm 3v$ . 0.2 amps. Price **£21.50** p.p. 47p

**RP124** Variable 0-24v. 1 amp. Price **£13.50** p.p. 37p

#### PANEL METERS

Complete range in stock. 38, 65 and 85 types plus large range Edge types also 240°-250° types. Latest Catalogue is a must for complete details.

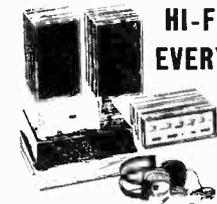
### BUILD THIS FM TUNER

also Decoder, tuning meter & power supply



5 MULLARD TRANSISTORS 300 kc/s BANDWIDTH. PRINTED CIRCUIT HIGH FIDELITY REPRODUCTION. MONO AND STEREO. A popular VHF FM Tuner for quality and reception of mono and stereo. There is no doubt about it—VHF FM gives the REAL sound. All parts sold separately. **TOTAL £6.97** p.p. 20p

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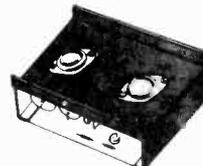
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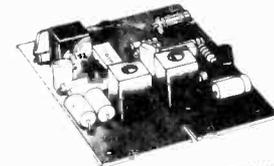


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  - PZ5 for Z30 ... **£3.97** or PZ6 for Z30 ... **£6.97**
  - PZ8 for Z50 ... **£5.97** Transformer ... **£2.25**
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Two transistor plus integrated circuit design. 9-12 volt operated, 50mV sensitivity, lamp output direct. Auto switching plus many other features. Size 2 1/2" x 2 1/4" x 1/8" Standard 0:1 connector or solder connections. Output 1 volt per channel. Price ready to use **£6.75** (Leaflet No. 7 on request).



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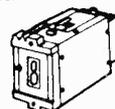
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  - 25,000 mfd 25 volt ... **75p**
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- At a fraction of normal price  
**MADE BY MALLORY, USA**



### E.A.C. DIGIVISOR mk. II

At a fraction of normal price. Moving Coil 0 to 9 Display. One inch character size. Light beam lens operated meter. Movement 500  $\mu$ A. Character lamp 6.3 volts. Also lamp for decimal point. Overall size: 4 1/2 x 1 1/2 x 2 1/2. Brand new. Price **£3.97**. Post 15p.



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**WITH VISCOUNT F.E.T. FIELD EFFECT TRANSISTORS AMPLIFIER**

This superb stereo system is a real price breakthrough. It comprises the VISCOUNT F.E.T. Mk I amplifier on which full details are given below, the famous Garrard SP 25 (including teak veneer base and transparent cover) with diamond cartridge or 2025 TC and the very successful DUO type 2 speakers.

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**WITH MK II amplifier and magnetic cartridge £48 plus £2.50 P&P**

## The Viscount F.E.T. Mk I £14.25 plus 37p P. & P.

**Specification:** Output per channel 10 watts r.m.s. into 3 ohms. Frequency bandwidth 20 Hz to 20 kHz ± 1 dB @ 1 watt.  
**Total distortion:** @ 1 kHz @ 9 watts 0.5%.  
**Input sensitivities:** CER. P.U. 100mV into 3 meg ohms. Tuner 100mV into 100K ohms. Tape 100mV into 100K ohms.

**Overload Factor:** Better than 26 dB.  
**Signal to noise ratio:** 70 dB on all inputs (with vol. max).  
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High fidelity transistor stereo amplifier employing field effect transistors. With this feature & accompanying guaranteed specifications below, the Viscount F.E.T. vastly surpasses amplifiers costing far more. Size: 12½" x 6" x 2½" in simulated teak case.

**BUILT & TESTED.**

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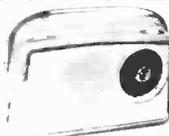
Specification same as Mk. I, but with the following inputs.

Mag. P.U. CER. P.U. Tuner. Spec. on Mag. P.U. 3mV @ 1 kHz input impedance 47K. Fully equalised to within ± 1 dB RIAA. Signal to noise ratio—65 dB (vol. max).



### Elegant Seven Mk 3 (350mW)

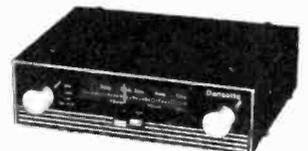
7 transistor fully-tunable M.W.-L.W. superhet portable Set of parts. Complete with all components, including ready etched and drilled printed circuit board—back printed for foolproof construction. MAINS POWER PACK KIT: 47p extra. Price **£5.25** plus 37p P. & P. Circuit 13p FREE WITH PARTS.



### The Dorset (600 mW)

7-transistor fully tunable M.W.-L.W. superhet portable—with baby alarm facility. Set of parts. The latest modusised and pre-alignment techniques makes this simple to build. Size: 12 x 8 x 3in. MAINS POWER PACK KIT: 47p extra. Price **£5.25** plus 13p P. & P. Circuit 13p FREE WITH PARTS.

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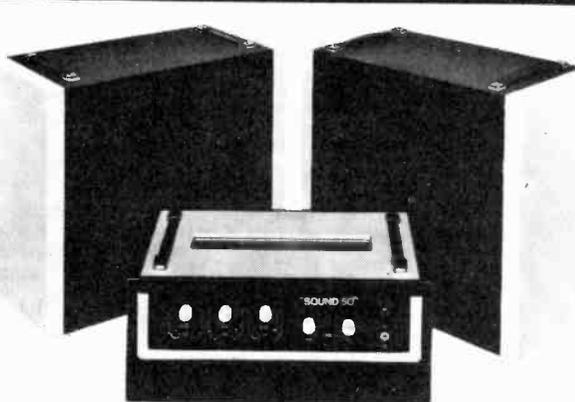
# SOUND 50

## SOUND 50 AMPLIFIER AND SPEAKER SYSTEM

The Sound Fifty valve amplifier and speakers are sturdily constructed with smart housings and thoroughly tested electronics. They are designed to last—to withstand the knocks and bumps of life on the road. Built for the small and medium sized gig, they are easy to handle and quick to set up and can be relied upon to come over with all the quality and power you need.

**Output Power:** 45 watts R.M.S. (Sine wave drive). **Frequency response:** -3 db points 30 Hz at 18 KHz. **Total distortion:** less than 2% at rated output. **Signal to noise ratio:** better than 60 db. **Speaker Impedance:** 3, 8 or 15 ohms. **Bass Control Range:** ±13 db at 60 Hz. **Treble Control Range:** ±12 db at 10 KHz. **Inputs:** 4 inputs at 5 mV into 470 K. Each pair of inputs controlled by separate volume control. 2 inputs at 200 mV into 470 K.

To protect the output valves, the incorporated fail safe circuit will enable the amplifier to be used at half power. **SPEAKERS:** Size 20" x 20" x 10" incorporating Baker's 12" heavy duty 25 watt high flux, quality loudspeaker with cast frame. Cabinets attractively finished in two tone colour scheme—Black and grey.



COMPLETE SYSTEM

**£50**  
plus £4 P & P

Amplifier £28.50 + £1 P & P.  
Speakers ea. £12.50 + £1.50 P & P.

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TOURISTE MK3  
CAR RADIO  
ALL TRANSISTOR

Beautifully designed to blend with the interiors of all cars. Permeability tuning and long wave loading coils ensures excellent tracking, sensitivity and selectivity on both wave bands. R.F. sensitivity at 1 MHz is better than 8 micro volts. Power output into 3 ohm speaker is 3 watts. Pre-aligned I.F. module and tuner together with comprehensive instructions guarantees success first time. 12 volts negative or positive earth. Size 7" x 2" x 4½" deep. **Originally sold completely built for £15.23**

SET OF PARTS  
**£6.30**  
Plus 37p P & P

Circuit diagram 13p. Free with parts. Speaker, baffle and fixing kit £1.25 extra plus 20p P & P.

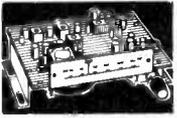
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**TRANSISTOR FM TUNER**



6 TRANSISTOR HIGH QUALITY TUNER. SIZE ONLY 6in. x 4in. x 2 1/2in. 3 I.F. stages. Double tuned discriminator, ample output to feed most amplifiers. Operates on 9 volt battery. Coverage 88-108 Mc/s. Really built ready for use. Fantastic value for money. £26 37 1/2. P. & P. 12 1/2p. STEREO MULTIPLEX ADAPTORS. £4 97 1/2.

**GOODMANS SPECIAL OFFERS!**

MAXAMP 30 Stereo Amplifier 15 + 15 watt r.m.s. with matching STEREO-MAX AM/FM Tuner. Total list price £136 52 OUR PRICE £89 THE PAIR Carriage £1.

**CRYSTAL CALIBRATORS NO. 10**



Small portable crystal controlled wavemeter. Size 7in. x 7 1/2in. x 4in. Frequency range 500 Kc/s-10 Mc/s (up to 30 Mc/s on harmonics). Calibrated dial. Power requirements 300 V.D.C. 15mA and 12 V.D.C. 0.5A. Excellent condition. £4 47 1/2. Carr. 37 1/2p.

**LELAND MODEL 27 BEAT FREQUENCY OSCILLATORS**

0-20 Kc/s. Output 5K or 500 ohms. 200/250 v. A.C. Offered in excellent condition. £12 50. Carriage 50p.

**CLASS D. WAVEMETERS**

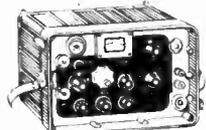


A crystal controlled heterodyne frequency meter covering 1.7-8 Mc/s. Operation on 6 v. D.C. Ideal for amateur use. Available in good used condition. £5 97 1/2. Carr. 37 1/2p. or brand new £7 97 1/2. Carr. 37 1/2p.

**B.C. 221 FREQUENCY METERS**

Latest release 125 KHz-20 MHz. Excellent condition. Fully tested and checked and complete with calibrator charts. £27 50 each. Carr. 50p.

**AM/FM SIGNAL GENERATORS**



Oscillator Test No. 2. A high quality precision instrument made for the Ministry by Airmecc. Frequency coverage 20-80 Mc/s. AM/FM. Incorporates precision dial, level meter, precision attenuator 1µV-100mV. Operation from 12 volt D.C. or 0/110/200/250 v. A.C. Size 12 x 8 1/2 x 9in. Supplied in brand new condition complete with all connectors. fully tested. £45. Carr. £1.

**AVO CT.39 ELECTRONIC MULTIMETERS**

High quality 97 range instrument which measures A.C. and D.C. Voltage, Current, Resistance and Power Output Ranges D.C. volts 250 mV-10,000v. (10 meg Ω-110 meg Ω input). D.C. current 10µA-25 amps. Ohms. 0-1,000 meg Ω A.C. volt 100mV-250V (with R.F. measuring head up to 250 Mc/s) A.C. current 10µA-25 amps. Power output 50 micro-watts-5 watts. Operation 0/110/200/250V. A.C. Supplied in perfect condition complete with circuit lead and R.F. probe. £25. Carr. 75p.

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High quality 10 valve receiver manufactured by Murphy. Coverage in 3 bands. 150-300 Kc/s. 500 Kc/s-1.5 Mc/s. 3.9-30.5 Mc/s. I.F. 500 Kc/s. Incorporates 2 R.F. and 3 I.F. stages, bandpass filter, noise limiter, crystal controlled B.F.O. calibrator I.F. output, etc. Built-in speaker, output for phono. Operation 150/230 volt A.C. Size 19 1/2 x 13 1/2 x 16in. Weight 114lb. Offered in good working condition. £22 50. carr. £1 50. With circuit diagrams. Also available B41 L.F. version of above. 15 Kc/s-700 Kc/s. £17 50. Carr. £1 50.

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**TO-3 PORTABLE OSCILLOSCOPE. 3" TUBE**



Y amp. Sensitivity. 1v p-p/CM. Bandwidth 1.5 cps-1.5 MHz. Input imp. 2 meg Ω. 25 PF. X amp sensitivity. 9v p-p/CM. bandwidth 1.5 cps-800 KHz. Input imp. 2 meg Ω. 20 PF. Time base. 5 ranges 10 cps-300 KHz. Synchronization. Internal/external. Illuminated scale. 230 x 240 v. A.C. Supplied brand new with handbook. £37 50. Carr. 50p.

**NEW PANEL METERS**

USED EXTENSIVELY BY INDUSTRY, GOVERNMENT DEPARTMENTS, EDUCATIONAL AUTHORITIES, ETC. LOW COST QUICK DELIVERY OVER 200 RANGES IN STOCK OTHER RANGES TO ORDER

**NEW "SEW" DESIGNS!**

CLEAR PLASTIC METERS BAKELITE PANEL METERS

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50µA	£3 47 1/2	50µA	£3 12 1/2
50-500µA	£3 37 1/2	50-500µA	£2 97 1/2
100µA	£3 37 1/2	100µA	£2 97 1/2
100-100µA	£3 25	100-100µA	£2 87 1/2
500µA	£3 12 1/2	500µA	£2 62 1/2
1mA	£2 97 1/2	1mA	£2 47 1/2
20V. D.C.	£2 97 1/2	20V. D.C.	£2 47 1/2
30V. D.C.	£2 97 1/2	30V. D.C.	£2 47 1/2
300V. D.C.	£2 97 1/2	300V. D.C.	£2 47 1/2
1 amp. D.C.	£2 97 1/2	1 amp. D.C.	£2 47 1/2
5 amp. D.C.	£2 97 1/2	5 amp. D.C.	£2 47 1/2
30V. A.C.	£2 97 1/2	30V. A.C.	£2 47 1/2
150V. D.C.	£2 60	150V. D.C.	£2 60
300V. D.C.	£2 60	300V. D.C.	£2 60
15V. A.C.	£2 60	15V. A.C.	£2 60
300V. A.C.	£2 60	300V. A.C.	£2 60
8 Meter 1mA	£2 87 1/2	8 Meter 1mA	£2 87 1/2
VU Meter	£3 60	VU Meter	£3 60
1 amp. A.C.*	£2 60	1 amp. A.C.*	£2 60
5 amp. A.C.*	£2 60	5 amp. A.C.*	£2 60
10 amp. A.C.*	£2 60	10 amp. A.C.*	£2 60
20 amp. A.C.*	£2 60	20 amp. A.C.*	£2 60
30 amp. A.C.*	£2 60	30 amp. A.C.*	£2 60

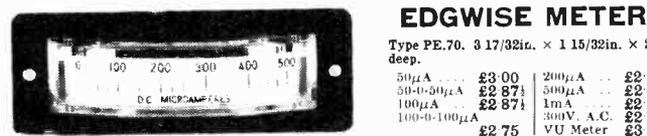
**"SEW" CLEAR PLASTIC METERS**

Type MR.85P. 4 1/2in. x 4 1/2in. fronts.		Type MR.38P. 1 21/32in. square fronts.	
10mA	£2 60	200µA	£1 37 1/2
50mA	£2 60	300µA	£1 37 1/2
100µA	£2 60	500µA	£1 37 1/2
300µA	£2 60	750µA	£1 37 1/2
1 amp.	£2 60	1 amp.	£1 37 1/2
5 amp.	£2 60	2 amp.	£1 37 1/2
15 amp.	£2 60	5 amp.	£1 37 1/2
30 amp.	£2 60	10 amp.	£1 37 1/2
20V. D.C.	£2 60	3V. D.C.	£1 37 1/2
30V. D.C.	£2 60	10V. D.C.	£1 37 1/2
150V. D.C.	£2 60	15V. D.C.	£1 37 1/2
300V. D.C.	£2 60	20V. D.C.	£1 37 1/2
15V. A.C.	£2 60	100V. D.C.	£1 37 1/2
300V. A.C.	£2 60	150V. D.C.	£1 37 1/2
8 Meter 1mA	£2 87 1/2	300V. D.C.	£1 37 1/2
VU Meter	£3 60	500V. D.C.	£1 37 1/2
1 amp. A.C.*	£2 60	500µA	£1 50
5 amp. A.C.*	£2 60	500-500µA	£1 37 1/2
10 amp. A.C.*	£2 60	1mA	£1 37 1/2
20 amp. A.C.*	£2 60	1-1mA	£1 37 1/2
30 amp. A.C.*	£2 60	5mA	£1 37 1/2
		10mA	£1 37 1/2
		50mA	£1 37 1/2
		100mA	£1 37 1/2
		150mA	£1 37 1/2

Type MR.52P. 2 1/2in. square fronts.		Type MR.45P. 2in. square fronts.	
50µA	£3 10	50µA	£2 25
50-50µA	£2 60	50-50µA	£2 10
100µA	£2 60	100µA	£2 10
100-100µA	£2 37 1/2	100-100µA	£1 87 1/2
500µA	£2 25	200µA	£1 87 1/2
1mA	£2 00	500µA	£1 60
5mA	£2 00	500-500µA	£1 50
10mA	£2 00	1mA	£1 50
50mA	£2 00	5mA	£1 50
100mA	£2 00	10mA	£1 50
500mA	£2 00	50mA	£1 50
1 amp.	£2 00	100mA	£1 50
5 amp.	£2 00	1 amp.	£1 50

Type MR.65P. 3 1/2in. x 3 1/2in. fronts.		"SEW" BAKELITE PANEL METERS	
50µA	£3 37 1/2	Type MR.65. 3 1/2in. square fronts.	
50-50µA	£2 75	50µA	£1 75
100µA	£2 75	1 amp.	£1 75
100-100µA	£2 60	5 amp.	£1 75
500µA	£2 10	15 amp.	£1 75
1mA	£2 10	30 amp.	£1 75
5mA	£2 10	50 amp.	£1 75
10mA	£2 10	5V. D.C.	£1 75
50mA	£2 10	10V. D.C.	£1 75
100mA	£2 10	20V. D.C.	£1 75
500mA	£2 10	50V. D.C.	£1 75
1 amp.	£2 10	150V. D.C.	£1 75
5 amp.	£2 10	300V. A.C.	£1 75
10 amp.	£2 10	50V. A.C.*	£1 75
15 amp.	£2 10	150V. A.C.*	£1 75
20 amp.	£2 10	300V. A.C.*	£1 75
30 amp.	£2 10	500mA A.C.*	£1 75
50 amp.	£2 10	1 amp. A.C.*	£1 75
5V. D.C.	£2 10	5 amp. A.C.*	£1 75
		10 amp. A.C.*	£1 75
		20 amp. A.C.*	£1 75
		30 amp. A.C.*	£1 75
		VU Meter	£3 10

\*MOVING IRON - ALL OTHERS MOVING COIL Please add postage



**EDGWISE METERS**

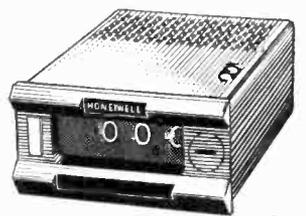
Type PE.70. 3 17/32in. x 1 15/32in. x 2 1/2in. deep.	
50µA	£3 00
50-50µA	£2 87 1/2
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2N1304	25p	BC107	12p	NKT473	25p
2N1305	25p	BC108	12p	NKT773	25p
2N1306	25p	BC109	12p	NKT10439	37p
2N1307	25p	BC113	25p	OA2	32p
2N1308	25p	BC116	40p	OA2	32p
2N1309	25p	BC125	55p	OA2	32p
2N1310	25p	BC126	55p	OA2	32p
2N1311	25p	BC127	55p	OA2	32p
2N1312	25p	BC128	55p	OA2	32p
2N1313	25p	BC129	55p	OA2	32p
2N1314	25p	BC130	55p	OA2	32p
2N1315	25p	BC131	55p	OA2	32p
2N1316	25p	BC132	55p	OA2	32p
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2N1328	25p	BC144	55p	OA2	32p
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2N1424	25p	BC240	55p	OA2	32p
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2N1481	25p	BC297	55p	OA2	32p
2N1482	25p	BC298	55p	OA2	32p
2N1483	25p	BC299	55p	OA2	32p
2N1484	25p	BC300	55p	OA2	32p
2N1485	25p	BC301	55p	OA2	32p
2N1486	25p	BC302	55p	OA2	32p
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**RUSSIAN C1-16 DOUBLE BEAM OSCILLOSCOPE**  
5 mc/s Pass Band. Separate Y1 and Y2 amplifiers. Rectangular 5 in. x 4 in. C.R.T. Calibrated triggered sweep from .2  $\mu$ sec. to 100 mill-sec. per cm. Free running time base 50 c/s-1 mc/s. Built-in time base calibrator and amplitude calibrator. Supplied complete with all accessories and instruction manual. £87 Carr. paid.



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1  $\mu$ /watt to 6 watts. £20. Carr. £1.



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Variable range 0-111 db. Connections. Unbalanced T and Bridge T. Impedance 600 ohms. Range (0.1 db x 10) + (1 db x 10) + 10 + 20 + 30 + 40 db. Frequency: DC to 200 KHZ (-3db). Accuracy: 0.05 db. + indication db x 0.01. Maximum input less than 4 watts (50 volts). Built in 800  $\Omega$  load resistance with internal/external switch. Brand new £27.50 P. & P. 25p.



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Sine 18-200,000 Hz; Square 18-50,000 Hz. Output max. +10 db (10 K ohms). Operation internal batteries. Attractive 2-tone case 7 1/2 in. x 5 in. x 2 in. Price £17.50 Carr. 17p.



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**VOLTAGE STABILISER TRANSFORMERS.** 180-260v. Input. Output 230v. Available 150w or 225w. £12.50. Carr. 25p.

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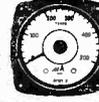
**MODEL 5025** 57 Ranges. Giant 5 1/2 in. Meter, Polarity Reverse Switch. Sensitivity: 50K/Volt D.C. 5K/Volt A.C. D.C. Volts: 125, 25, 1.25, 2.5, 5, 10, 25, 50, 125, 250, 500, 1,000V. A.C. Volts: 1.5, 3, 5, 10, 25, 50, 125, 250, 500, 1,000V. D.C. Current: 25, 50  $\mu$ A, 2.5, 5, 25, 50, 250, 500mA. 5, 10 amp. Resistance: 2K, 10K, 100K, 1MEG, 10 MEG. Decibels: -20 to +85 db £12.50 P. & P. 17p.



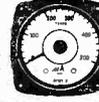
**FTC-401 TRANSISTOR TESTER**  
Full capabilities for measuring A, B and 1C0. NPN or PNP. Equally adaptable for checking diodes. Supplied complete with instructions, battery and leads. £6.97. P. & P. 15p.



**AVO CT471A MULTIMETER**  
Battery operated, fully transistorised. Sensitivity 100  $\mu$ Q/v. Measures A.C./T.C. voltages 12mV. to 1,200 V. A.C./D.C. current 15 $\mu$ A. to 1.2 Amp. Resistance 12 ohm to 120 m $\Omega$ . H.F. V.H.F. U.H.F. voltage with multiplier 4V. to 400V. up to 50 Mc/s. 40 mV. to 4V. up to 1,000 Mc/s. Offered in perfect condition. £55 each. Carr. 50p.



**270° WIDE ANGLE 1mA METERS**  
MW1-6 60mm. square £3.97 P. & P. extra  
MW1-8 80mm. square £4.97 P. & P. extra



**"YAMABISHI" VARIABLE VOLTAGE TRANSFORMERS**  
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**TMK MODEL TW-20CB FEATURES RESETTABLE OVERLOAD BUTTON.** Sensitivity: 20K  $\Omega$ /Volt D.C. 5K  $\Omega$ /Volt A.C. D.C. Volts: 0-0.5, 2.5, 10, 50, 250, 1,000V. A.C. Volts: 0-2.5, 10, 50, 250, 1,000V. D.C. Currents: 0-0.05, 0.5, 5, 50, 500mA. -10 amp. Resistance: 0-5K, 50K, 0-500K. 5 MEG. Decibels: -20 to +82db. £11.50 P. & P. 17p.



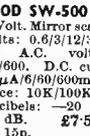
**MODEL AS-100D.** 100K  $\Omega$ /Volt 5 in. mirror scale. Built-in meter protection 0/3/12/60/120/300/600/1,200 v. D.C. 0/5/30/120/300/600 v. A.C. 0/10  $\mu$ A/5/60/300mA/12 Amp. 0/2K/200K/2M/200M. -20 to +17 db. £12.50 P. & P. 17p.



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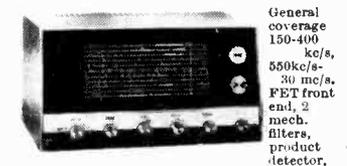

**UNR 30 RECEIVER**  
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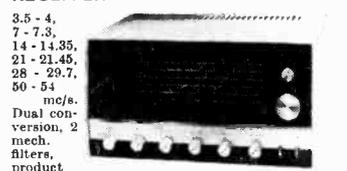
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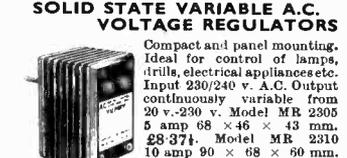
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CV4033 0-35	EA42 0-50	EF98 0-75	GZ30 0-50	PCF801 0-49	QV03/10 1-38	QV06-20 1-38	UABC80 0-33	2D21 0-33	6A44 0-20	6Q7G 0-30	30C17 0-80	866A 0-75	
CV4034 0-60	EA4806	EF183 0-33	GZ32 0-50	PCF802 0-49	QV03/20 1-38	QY3-125 1-38	UAF42 0-33	2E26 1-00	6A45 0-31	6Q7M 0-38	30F5 0-85	872A 2-88	
CV4045 0-50	EA91 0-98	EF184 0-35	GZ34 0-55	PCF806 0-49	QV04/15 5-25	R10 0-90	UBC41 0-48	2K25 8-00	6A86 0-30	68G7 0-38	30FL1 0-75	931A 3-63	
AR338 0-80	CV4048 0-83	EFBC3 0-43	EF960 0-50	HL41DD	QV06-40A 5-25	R17 0-40	UCH81 0-35	3A5 4-00	6A87 0-75	68J7M 0-35	30L15 0-85	954 0-26	
A231 0-50	CV4064 1-50	EF90 0-24	EL33 0-63	KT8 1-75	QV06-40A 5-00	R18 0-38	UCL82 0-38	3B24 1-45	6AT6 0-28	68L7GT 0-30	30L17 0-55	955 0-15	
BT19 3-00	CY30 0-63	EF90 0-38	EL34 0-63	KT8 1-75	QV06/40 5-00	R19 0-38	UCL83 0-58	3B240M 1-00	6B4G 1-00	68N7GT 0-30	30L19 0-75	964 2-00	
BT79 2-85	DAF91 0-23	EF983 0-45	EL36 0-46	KT61 1-13	QV06/40 4-30	RG3/1250 6-00	UL41 0-60	3B241M 5-50	6B4E 0-25	6V6G 0-28	30PL1 0-80	3651 0-38	
BT89 3-35	DAF99 0-38	EF989 0-33	EL38 1-25	KT66 1-50	QV5/10 3-50	RG5/500 1-05	UL84 0-30	3B241M 5-50	6B4E 0-25	6V6G 0-28	30PL13 0-93	3654 0-40	
CIC 1-00	DC900 1-00	EL41 0-55	EL41 0-55	KT97 2-55	QV5/10 3-50	S1M2 4-00	U07 1-05	3B28 2-00	6B4E 0-25	6V6G 0-28	30PL14 0-75	3672 0-35	
CBL31 0-80	DET3 50-00	EL42 0-58	EL42 0-58	KT81(708) 1-13	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6 0-45	3687 0-50	
CV330 0-75	DET19 0-33	EL41 0-45	EL41 0-45	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3691 1-25	
CV5 4-75	DET20 0-13	EL84 0-24	EL84 0-24	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3694 1-50	
CV74 4-00	DET22 5-00	EL85 0-39	EL85 0-39	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV82 2-50	DET23 5-50	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV315 4-00	DET24 2-50	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV350 5-50	DET25 0-75	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV370 15-00	DF91 0-20	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV372 3-25	DF96 0-38	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV404 6-00	DH63 0-30	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV408 2-50	DH77 0-25	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV428 2-25	DK92 0-39	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV429 17-50	DK91 0-30	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV450 1-25	DK92 0-45	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV1144 3-00	DK96 0-39	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV1385 7-00	DL66 1-25	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV1522 9-00	DL92 0-31	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV1528 2-25	DL94 0-34	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV2155 1-63	DL96 0-39	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV2306 17-50	DL810 1-25	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV2312 1-75	DL816 1-50	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV4003 0-50	DY86 0-30	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV4004 0-50	DY87 0-33	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV4006 0-40	DY89 0-33	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV4006 0-90	E88CC 0-60	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV4007 0-35	E180F 0-88	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV4014 0-35	E182CC 0-88	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV4015 0-50	E180F 0-88	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV4024 0-30	E810F 1-13	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV4025 0-35	EA18C80 1-50	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	
CV4031 0-35	EF92 0-33	EL86 0-41	EL86 0-41	KT88 1-70	QV5/20 0-28	S1M2 4-00	U07 1-05	3C24 3-00	6B4E 0-25	6V6G 0-28	35L6GT 0-50	3702 0-75	

Transistors		2N247	AD161	BCV72	GET875	NKT217	NKT718	OC24	OC45	OC78	OC82D	OC71	2N3710
18111 0-13	2G381 0-25	AD161 0-38	BCV72 0-18	GET875 0-25	NKT217 0-40	NKT718 0-25	OC24 0-50	OC45 0-15	OC78 0-20	OC82D 0-15	OC71 0-15	2N3710 0-13	
18113 0-15	2G382 0-30	AD161 0-38	BCV72 0-18	GET875 0-25	NKT217 0-40	NKT718 0-25	OC24 0-50	OC45 0-15	OC78 0-20	OC82D 0-15	OC71 0-15	2N3710 0-13	
18115 0-30	2G415 0-30	AD161 0-38	BCV72 0-18	GET875 0-25	NKT217 0-40	NKT718 0-25	OC24 0-50	OC45 0-15	OC78 0-20	OC82D 0-15	OC71 0-15	2N3710 0-13	
18121 0-13	2G416 0-33	AD161 0-38	BCV72 0-18	GET875 0-25	NKT217 0-40	NKT718 0-25	OC24 0-50	OC45 0-15	OC78 0-20	OC82D 0-15	OC71 0-15	2N3710 0-13	
2G210 0-63	2G417 0-33	AD161 0-38	BCV72 0-18	GET875 0-25	NKT217 0-40	NKT718 0-25	OC24 0-50	OC45 0-15	OC78 0-20	OC82D 0-15	OC71 0-15	2N3710 0-13	

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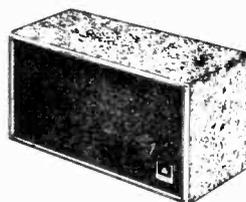
40361	55p	2N2905	44p	2N4291	15p	BC148	14p	BFX87	29p
40362	68p	2N2905A	47p	2N4292	15p	BC149	15p	BFX88	26p
2N696	20p	2N2924	20p	AC107	46p	BC153	19p	BFY50	23p
2N697	22p	2N2925	22p	AC126	20p	BC154	28p	BFY51	20p
2N706	12p	2N2926	11p	AC127	20p	BC157	19p	BFY52	23p
2N930	29p	2N3053	27p	AC128	20p	BC158	17p	BSX20	16p
2N1131	36p	2N3055	75p	AC153K	25p	BC159	18p	C407	17p
2N1132	40p	2N3702	13p	AC176	27p	BC167	13p	MC140	25p
2N1302	19p	2N3703	13p	ACY20	16p	BC168	11p	MPS6531	35p
2N1303	19p	2N3704	13p	ACY22	16p	BC169	13p	MPS6534	30p
2N1304	23p	2N3705	13p	AD140	56p	BC177	17p	NKT211	25p
2N1305	23p	2N3706	13p	AD142	56p	BC178	15p	NKT212	25p
2N1306	33p	2N3707	13p	AD149	60p	BC179	17p	NKT214	23p
2N1307	33p	2N3708	13p	AD161	40p	BC182L	13p	NKT274	18p
2N1308	36p	2N3709	13p	AD162	40p	BC183L	11p	NKT403	65p
2N1309	36p	2N3710	13p	AF114	30p	BC184L	13p	NKT405	79p
2N1613	23p	2N3711	13p	AF115	30p	BC212L	25p	OC71	29p
2N1711	26p	2N3819	35p	AF117	28p	BC213L	25p	OC81	25p
2N1893	54p	2N3904	35p	AF124	30p	BC214L	25p	OC81D	25p
2N2147	95p	2N3906	35p	AF127	28p	BCY70	19p	ZTX300	17p
2N2218	33p	2N4058	20p	AF139	48p	BCY71	33p	ZTX301	17p
2N2218A	43p	2N4059	20p	AF239	49p	BCY72	15p	ZTX302	22p
2N2219	38p	2N4060	20p	ASY26	27p	BF115	23p	ZTX303	22p
2N2219A	53p	2N4061	20p	ASY28	27p	BF167	27p	ZTX304	33p
2N2270	62p	2N4062	20p	BC107	14p	BF173	31p	ZTX304	25p
2N2369A	19p	2N4124	18p	BC108	12p	BF194	17p	ZTX501	25p
2N2483	35p	2N4126	27p	BC109	14p	BF195	18p	ZTX502	30p
2N2484	42p	2N4284	15p	BC125	15p	BFX29	31p	ZTX503	25p
2N2646	54p	2N4286	15p	BC126	22p	BFX84	25p	ZTX504	60p
2N2904A	42p	2N4289	15p	BC147	15p	BFX85	34p		

## PEAK SOUND PRODUCTS



ENGLEFIELD 12+12 AMPLIFIER

Stereo amplifier in modular kit form 12 watts RMS per channel into 15Ω £38.45  
Cabinet kit only £6. These prices nett.  
As reviewed in Hi Fi Sound and other important journals.



BAXANDALL SPEAKER SYSTEM

Designed by Peter Baxandall. Superb reproduction for its size. Handles 10 watts with ease. Uses ELAC 15Ω 59RM109 speaker unit. Kit £13.90 nett; built £19.40 nett.

## MAINLINE AMPLIFIER KITS

RCA/SGS designed main amplifier kits. Input sensitivity 500-700mV for full output into 8Ω.

Power	Kit price including components	Suitable unreg. power supply kit
12W	£8.40 nett	£4.60
25W	£9.50 nett	N/A
40W	£10.50 nett	£5.75
70W	£12.60 nett	£6.94

## RESISTORS

Code	Power	Tolerance	Range	Values available	1 to 9 (see note below)	10 to 99	100 up
C	1/20W	5%	82Ω-220KΩ	E12	7	6-5	6
C	1/8W	5%	4.7Ω-330KΩ	E24	1-5	0-8	0-7
C	1/4W	10%	4.7Ω-10MΩ	E12	1-5	0-8	0-7
C	1/2W	5%	4.7Ω-10MΩ	E24	1-2	1	0-9
C	1W	10%	4.7Ω-10MΩ	E12	2-5	2	1-9
MO	1/2W	2%	10Ω-1MΩ	E24	4	3-5	3
WW	1W	10% ± 1/20Ω	0.22Ω-3.9Ω	E12	7	7	6
WW	3W	5%	12Ω-10KΩ	E12	7	7	6
WW	7W	5%	12Ω-10KΩ	E12	9	9	8

Codes: C = carbon film, high stability, low noise.  
MO = metal oxide, Electroasil TR5, ultra low noise.  
WW = wire wound, Plessey.

### Values:

E12 denotes series: 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and their decades.  
E24 denotes series: as E12 plus 11, 13, 16, 20, 24, 30, 36, 43, 51, 62, 75, 91 and their decades.

**ZENER DIODES** 5% full range E24 values:  
400mW: 2.7V to 30V, 15p each; 1W: 6.8V. to 82V, 33p each; 1.5W: 4.7V to 75V, 60p each.  
Clip to increase 1.5W rating to 3 watts (type 266F), 4p.

**CARBON TRACK POTENTIOMETERS**, long spindles. Double wiper ensures minimum noise level.

Single gang linear 220Ω to 2.2MΩ, 12p; Single gang log, 4.7KΩ to 2.2MΩ, 12p; Dual gang linear, 4.7KΩ to 2.2MΩ, 42p; Dual gang log, 4.7KΩ to 2.2MΩ, 42p; Log/antilog, 10K, 47K, 1MΩ only 42p; Dual antilog, 10K only, 42p. Any type with 1/2A D.P. mains switch, extra 12p.  
Please note: only decades of 10, 22 and 47 are available within ranges quoted.

### CARBON SKELETON PRE-SETS

Small high quality, type PR, linear only: 100Ω, 220Ω, 470Ω, 1K, 2K, 4K, 10K, 22K, 47K, 100K, 220K, 470K, 1M, 2M, 5M, 10MΩ. Vertical or horizontal mounting, 5p each.

**COLVERN** 3 watt Wire-wound Potentiometers. 10Ω, 15Ω, 25Ω, 50Ω, 100Ω, 250Ω, 500Ω, 1K, 1.5K, 2.5K, 5K, 10K, 15K, 25K, 50K, 32p each.

**ENAMELLED COPPER WIRE** even No. SWG  
2 oz. reels: 16-22 SWG 25p; 24-30 SWG 30p;  
32, 34 SWG, 33p; 36-40 SWG, 35p.  
4 oz. reels: 16-22 SWG only 42p.

Prices are in pence each for quantities of the same ohmic value and power rating. NOT mixed values. (Ignore fractions on total value of resistor order.)

### TYGAN SPEAKER MATERIAL

7 designs, 36 x 27 in. sheets, £1.57 sheet.  
Pattern book, S.A.E. plus 3p stamp.

### MULLARD polyester C280 series

250V 20%; 0-01, 0-022, 0-033, 0-047 3p each; 0-068, 0-1, 4p each; 0-15, 4p; 0-22, 5p. 10%; 7p; 0-33, 0-47, 8p; 0-68, 12p; 1μF, 14p; 1-5μF, 21p; 2-2μF, 24p.

### MULLARD SUB-MIN ELECTROLYTICS

C426 range, axial lead 6p each  
Values (μF/V): 0-64/64; 1/40; 1-6/25; 2-5/16; 2-5/64; 4/10; 4/40; 5/64; 6-4/6-4; 6-4/25; 8/4; 8/40; 10/2-5; 10/16; 10/64; 12-5/25; 16/40; 20/16; 20/64; 25/6-4; 25/25; 32/4; 32/10; 32/40; 32/64; 40/16; 40/2-5; 50/6-4; 50/25; 50/40; 64/4; 64/10; 80/2-5; 80/16; 80/25; 100/6-4; 125/4; 125/10; 125/16; 160/2-5; 200/6-4; 200/10; 250/4; 320/2-5; 320/6-4; 400/4; 500/2-5.

### LARGE CAPACITORS

High ripple current types: 1000/25, 28p; 1000/50, 41p; 1000/100, 82p; 2000/25, 37p; 2000/50, 57p; 2000/100, £1.44; 2500/64, 77p; 2500/70, 98p; 5000/25, 62p; 5000/50, £1.20; 5000/100, £2.91; 10000/15, 85p; 10000/25, £1.22; 10000/50, £2.20.

### COMPONENT DISCOUNTS

10% on orders for components for £5 or more.  
15% on orders for components for £15 or more.  
(No discount on nett items.)

### POSTAGE AND PACKING

Free on orders over £2.  
Please add 10p if order is under £2.  
Overseas orders welcome: carriage and insurance charged at cost.

Note: U.K. cheques not in decimal currency cannot be accepted.

## 30 WATT BAILEY AMPLIFIER PARTS

Sensitivity 1.2V for full output into 8Ω.  
Transistors and PCB for one channel £6.40  
Transistors and PCBs for two channels £12.80  
Capacitors and resistors (metal oxide), £2.00 per channel.  
Complete unregulated power supply pack, £4.75

## INTEGRATED CIRCUITS

PLESSEY SL403A 3 watts into 7.5 ohms. Data book supplied FREE when two of these units are purchased. Price per unit, nett £2.10

**SINCLAIR IC.10** as advertised, complete with instructions and applications manual £2.95 nett.  
Components pack for stereo inc. transformer, controls, etc., £4.75 nett.

### S-DeCs PUT AN END TO BIRDS NESTING

Components just plug in—saves time—allows re-use of components. S-Dec (70 points), £1.00  
Complete T-Dec, may be temperature-cycled (208 points), £2.50  
Also μ-Decs and IC carriers.

### MEDIUM RANGE ELECTROLYTICS

Axial leads: 50/50, 9p; 100/25, 9p; 100/50, 13p; 250/25, 13p; 250/50, 19p; 500/25, 19p; 500/50, 21p; 1000/25, 20p; 1000/50, 30p; 2000/25, 30p; 2000/50 48p.

### SMALL ELECTROLYTICS

Axial leads: 4-7/10, 4-7/25, 5/50, 5p each; 10/10, 10/25, 10/50, 33/10, 50/10, 5p each; 25/25, 25/50, 47/25, 100/10, 220/10, 6p each.

### NEON INDICATOR LAMPS

all 200/250V. Square bezel, red only 19p  
Round, chrome bezel red, amber, clear 24p each

**TOGGLE SWITCHES**, 250V a.c. 1-5A.  
chrome dolly and chrome milled nut S.P.S.T. 19p, S.P.D.T. 25p D.P.D.T. 29p; S.P.D.T. centre off 20p

### WAVECHANGE SWITCHES

LONG SPINDLES 24p each  
1P 12W; 2P 6W; 3P 4W; 4P 3W  
SLIDER SWITCHES D.P.D.T. 15p each

# ELECTROVALUE

DEPT. WW.371, 28 ST. JUDES ROAD, ENGLEFIELD GREEN, EGHAM, SURREY,  
Hours: 9-5.30, 1.0 p.m. Saturdays. Phone: Egham 5533 (STD 0784-3) Telex 264475



**LOW COST ELECTRONIC & SCIENTIFIC**

**BRAND NEW MINIATURIZED AUTOMATIC STRIP CHART RECORDER**

by RUSTRAK of America. This recorder indicates the magnitude of applied currents or voltages by a continuous distortion-free line on pressure sensitive paper. Chart width 2 3/4 in. Chart speed 1/2 in. per min. Moving coil movement, scale calibrated 0-100 microamps. Int. resistance 4,600 ohms. Chart drive motor 12v. D.C. C/W handbook. Price £40. P. & P. 10/-.

**A BARGAIN IN NEW POWER SUPPLIES. AT LESS THAN HALF MANUFACTURERS PRICE**

O/P Voltage 7.5v.-9v. Max. load current 10 Amps. Max ripple on full load approx. 60mV. p.p. Threshold current, 10.5A. Overvolt protection. OUR PRICE £19.50

**HONEYWELL INCREMENTAL DIGITAL RECORDER MODEL 6200**

Records random or synchronous digit (binary) data on 7-track 1/2 inch tape in steps of 0.005 inch. Packing density 200 bit/inch. Offered in first class condition. This recorder has had very little use. Price c application.

**MOTORS**

**LOW TORQUE HYSTERESIS MOTOR MA23**

Ideal for instrument chart drives. Extremely quiet, useful in areas where ambient noise levels are low. High starting torque enable relative high inertia loads to be driven up to 6-oz/in. Available in the following speeds and ranges: 240V 50 Hz 1 1/2 r.p.m., 1/8 r.p.m., 1/12 r.p.m., 1/20 r.p.m., 1/60 r.p.m. 120V 50 Hz 1/6 r.p.m., 1/15 r.p.m., 1/10 r.p.m., 1/24 r.p.m., 1/3 r.p.m., 1/240 r.p.m., 1/300 r.p.m., 1/720 r.p.m., 1 r.p.m. M.P.10 Induction Motor. 120V 50 Hz 20 r.p.m. £1.50 P. & P. inclusive.

**CLUTCH MOTORS**

240V 50 Hz 1/12 r.p.m., 1/8 r.p.m., 1/3 r.p.m. 120V 50 Hz 1/2 r.p.m., 1/10 r.p.m., 1/6 r.p.m., 5/12 r.p.m., 4/11 r.p.m., 1 r.p.m., 2 r.p.m. 120V 60 Hz 1/5 r.p.m., 1 r.p.m. £1.50. P. & P. inclusive.

**REVERSIBLE MOTOR**

120V 60 Hz 1/10 r.p.m. D.C. Motor MD83. 28V 1/120 r.p.m., 1/60 r.p.m., 1/15 r.p.m., 1/12 r.p.m. £1.50. P. & P. inclusive.

**NEW LOW INERTIA INTEGRATING MOTORS**

Electro-Methods Model. 901 and 906 PL. Permanent magnet D.C. Motor. High sensitivity. Ideal for instrument-type servo mechanisms, light loads driving mechanical counters performing integration, or as small power generators. Will operate directly off a photo-cell or thermo couple, etc. 6V. Nominal. Typical parameters. Starting voltage (no load) 15 mV at 0.375 mA. Full load speed 1845 r.p.m. (approx.). Moment of Inertia of Armature 1.8 gr. cm/cm. Weight of Motor 300 gms (approx.). £15. P. & P. included.

**SPLIT-FIELD D.C. SERVO MOTOR**

Evershed and Vignoles Type. FAE 2/C/B, FB5A/A1/B, FEK25/CG/30, FB6A/P1/B, PAD6/G4/BD, FB5/A1, FE16/C. £13.50. P. & P. included.

**NEW D.C. STEPPING MOTOR**

"Slo-Syn." 14V 0.53A 50 oz in torque. BIFILAR Synchronous Motor. Stepping duty 200 steps/shaft revolution. Each step 1.8 degrees + 3% accuracy. Non-cumulative. Made by Superior Electric Co., U.S.A. £18.50. P. & P. included.

**E.H.T. GENERATOR, BRAND NEW D.C. CONVERTER MULLARD TYPE 1049**

Input 12V D.C. 0.3A. Output 1800V (Min) at 1 mA. 2500V (Min) on No Load. Full spec. and circuit provided. Encapsulated module L. 5in., W. 2 1/2in., H. 1 1/2in. £5.50. P. & P. included.

**MIDGET POWER RELAY** Type Mk 1 (OMRON)

230V 50 Hz Coil, 1 pole double throw. Unused. Faulty plating on frame. 5 for £1.50. P. & P. included.

**SYNCHRONOUS MOTORS**

Model S 71 r.p.m. and 1/60 r.p.m. Self starting complete with gearing shaft 1/2 in. dia. 1/2 in. long. 200/250V 50 Hz. New condition Ex-Equipment. £1.50. P. & P. included.

**D.C. TACHOGENERATOR**

Type 9c/106 16v. at 1000 r.p.m. Drive shaft dia. 3/16 in., 3/8 in. long. Price £18.50. P. & P. inclusive.

**R.F. ATTENUATOR MARCONI TF 1073A**

DC-150 MHz 1dB steps 75 Ohms. Double Screened construction. Tested and in VG condition. £25.

**ACTUATOR**

By English Electric. Type 4519 Mk. 1 D.C. Motor AE 1560 Mk. 1 28V 3A. 500 r.p.m. Intermittent rating. £18. P. & P. inclusive.

**ACCELEROMETERS**

Model LA 2.3C Potentiometric + or - 10G operating Voltage 30V. Nominal resistance 17.5K and Model LA 2.3C + or - 100G 34V. Rel 20 K. Price £26. P. & P. 5/-.

**TYPE SE 55/A Range + or - 1G £26. P. & P. 5/-.**

**TYPE F** by G.E.C. Up to 1,000 G. Ceramic type giving o/p of 23 mV. Supplied c/w technical leaflet. Weight 14.8 grammes. 2BA stud mounting. £3.15. P. & P. 3/-.

Many other types in stock

**COUNTERS**

Manufacturer	Type	No. of Digits	Impulses per sec.	Reset	Operating Volt	Current	Size	Ref.	Remarks
Sedeco	ATCEZ3E	3	10	M.	48V D.C.	48mA	4"L x 1" x 1"	C.2	
Sedeco	ATCEZ4E	4	25	M	60V D.C.	100mA	1 1/2" x 1" x 4"L	C.6	600 Ohm coil new 1000 Ohm coil used
Sedeco	ATCEP4E	4	10	E/12V D.C.	12V D.C.	120mA	4"L x 2 1/2" x 1 1/2"	C.5	New Used
Sedeco	ATCEP5E	5	25	E/24V D.C.	24V D.C.	240mA	4"L x 1 1/2" x 2 1/2"		New
Sedeco	ATCEZ5E	5	25		160V				Coil 100K. New
Sedeco	TIF5 PIEH	5	10	M	116V 50Hz		1 1/2" x 5 1/2" x 5 1/2"		2 banks of 5 digits each bank independent. Used
Sedeco	ITPB3	6	10	M. & E.	240V 50Hz				Print out—Totalling
Counting Instrument	1506	4	15		24V D.C.			C.3	Each digit independently set, counts down to zero operating main switch
"	429	4	15	E/240V 50Hz	24V D.C.			C.12	
"	120	6	15	E/24V D.C.	24V D.C.		3 1/2" x 3 1/2" x 1 1/2"		
"	101A	6		M.	48V D.C.		4" W x 2 1/2" x 2 1/2" L		Used
Veeder Root	BD134545	5							Mechanical operation. Ratchet reset Inverse Nos.
"	"	6		M.	160V D.C.				
"	B38	6		M.	48V D.C.				
"	"	6			110V D.C.				
"	"	6		M.	230V 50Hz				
"	"	6		M.	24V D.C.				
Hazler	"	6		M.	24V D.C.				500 Ohm coil. New
"	"	6		M/E	110V D.C.				1100 Ohm/800 Ohm. Used

Many other types of counters are available ranging from 3-6 with various supply voltages. Ring our Sales Office for full information.

**TEKTRONIX** Plug in Unit Type E—BRAND NEW. Price P. & P. 10/-. Also Type 80 £25

**HIGH SPEED IMPULSE COUNTER**

DAVIS WYNN and ANDREWS 4 in dial with pointer registering up to 100 plus a 4 digit counter mounted in dial. Uses an inverse air escapement. Coil resistance 100 ohms. 20V operation. £8. P. & P. 7/6.

**VIBRON ELECTROMETER**

This unit is a vibration condenser amplifier which is suitable for the measurement of small D.C. potentials covering the range of 1M-1V. This unit can also be used as high impedance null detector for the comparison of ionization currents of very high resistance. £89.50.

**NUMERICATORS**

End Reading	Quantity	Price Each (Less Base)	Price Base
GR10M/U (Clear)	1-3	(£1.40) 28/-	Bases (20p)
	4-10	(£1.35) 27/-	4/-
	11-25	(£1.30) 26/-	Each
	26-100	(£1.20) 24/-	

Side Reading

	Quantity	Price Each (Less Base)
XN3/FA 38 m/m lead (Amber)	1-3	(£1.15) 23/-
XN3/F 38 m/m lead (Red)	1-3	(£1.10) 22/-
XN3A/F 6 m/m lead (Red)	4-10	(£1.05) 21/-
XN3A 6 m/m lead (Clear)	11-25	(£1.05) 21/-
XN11/F 38 m/m lead (Red)	26-100	(£0.95) 19/-
XN23/FA 38 m/m lead (Amber)		

Post Free

**EICHNER 8 HOLE PUNCH**

No motor drive required. Solenoid operated equipment using 48V Reader £29.10.0; Punch £49.10.0. Carriage 25/-.

**7 HOLE NON PARITY TAPE PUNCH**

New condition.

**LOW SPEED 7 HOLE TAPE PUNCH**

60 characters per second by well-known manufacturer.

**TELETYPE 8 HOLE PAPER PUNCH BRPEII £260.**

Also available 5 hole punch BRPE2 as above. This model has interchangeable heads. Complete with spooler. Price £75.

**5/7 HOLE OPTICAL READER BY FERRANTI**

20 characters per second. £20.

(183) SIGNAL GENERATOR CT 480 SANDERS. Range 7-12 KHz. O/p. 0-±50V. Attenuation range -10 to +10 Price

**TRANSDUCER OSCILLATOR-AMPLIFIER-DEMODULATOR**

encapsulated unit for matching with S.E. Transducers. Su where space or adverse environmental conditions prevail. Su with a matching transducer a typical o/p is ± 3V into 50K Supply voltage 12v. D.C. Range of transducers available 0-750; 0-1000; 0-4000 psi. Price

**TRANSDUCER—New Resistive Bordon Tube Principle**

Transducer by K.D. Instrument. Model TD 216 0-2000 Ref. C. 6. Price

**TRANSDUCER NEW EX-GOVERNMENT DISPLACEMENT BR RESISTANCE STRAIN GAUGES** Range ± 1 mechanical placement equivalent to 0.3% resistive change. 3.5 + 3.5 K Model IT-2-31-35. Price

**OSCILLATOR**. High discrimination, by Marconi T.F. 1168, instrument suitable for H.F. Communication. Due to the discrimination makes it suitable for crystal filter response and Rx drive units. Frequency range 90-110 KHz. 2Hz discrimination. Crystal and Standardised centre frequency. Calibr accuracy ± 1%. Ref. I.5. Price

**RECORDERS 4 PEN OSCILLOGRAPHS SOUTHERN INSTRUMENTS M942C**. 4 Channel fitted with 4 speed gear boxes 1, 5, 25, 100 m.m. per sec. Frequency response 0-55 Hz, sensi 0/m.m./M.A. Price

**2 PEN OSCILLOGRAPH MR450** as per 4 Pen. Ref. I.2. Price PLUS CARB

**E.M.I.**

Portable L.F. Tape Recorder. Ex-service equipment consisting of Three Unit housed in transit cases (Tape Deck, Amplifier, 1 1/2 in. track speed 30 in., 15 in., 7 1/2 in. and 1 in. min. Price Many control facilities. This is a good quality recorder.

**ELECTRONIC BROKERS LTD**

**EQUIPMENT AND COMPONENTS**

**MEASURING INSTRUMENTS AND RECORDERS**

**MULTIMETER TYPE CT471B**

Fully transistorized multi-range instrument for measurement of voltage up to 1000 MHz (1500 MHz with reduced accuracy) and current up to 20 mA and D.C. Resistance A.C. voltage and current divided to 11 ranges.  
 C./D.C. Volts 12mV-1200V.  
 C./D.C. Current 12 micro A-1.2A.  
 C. Resistance 5 ranges 0.1 ohm-100 M ohm.  
 F. Voltages 5 range 40mV to 4V. battery powered. Offered in excellent condition. Tested before dispatch. Complete with handbook. £54. Carriage 10/-.

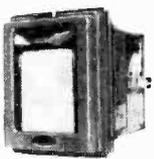


**ACSIMILE RECORDERS**

649 K 18 in. Chart Recorder. 1101 speed: 60, 90, 120 rev./min. maximum speed: 1 in./15/16 in.; 1 1/4 in. per min. Scanning rate: 1 line/in. Price £350. Completely overhauled + carriage

**SINGLE PEN RECORDER**

By Record Electrical (R3)  
 3 in. chart, sensitivity 1 mA. Coil res. 1.53k. Fully interchangeable gears available to make a wide range of chart speeds. 200/250V. Size: 8x11x6 in. Almost new—complete with chart and ink. List over £100. Our price £49 50



**PRECISION POTENTIOMETERS**

**TEN TURN 360° ROTATION BRAND NEW (Ref. C5)**

Res. Ohms	Linearity	Manufacturer	Model	Price
100/100/100	0.5	Beckman	A	£3 00
100	0.5	Beckman	A.S.	£3 00
200	0.5	Beckman	A	£3 00
500	0.1	Beckman	S	£3 50
500	0.1	Colvern	2501	£2 25
500	0.1	Foxes	PX4	£2 00
500	0.1	Colvern	2610	£2 50
500	0.1	Colvern	2610/11	£3 00
500	1.0	Relcon	HEL107-10	£2 25
1K	0.5	Relcon	HEL107-10	£2 25
2K	0.5	Beckman	SA1101	£3 00
2K	0.25	Beckman	7216	£3 00
2K	0.1	Reliance	GPM15	£2 00
2K	0.1	General Controls	GPA15/4	£2 00
5K	0.1	Relcon	07-10	£2 50
5K	0.1	Colvern	CLR2503	£3 00
10K	0.5	Beckman	A	£3 00
10K	0.1	Beckman X	A	£3 50
10K	0.1	Colvern	CLR26/1001	£3 50
15K	0.1	Colvern	CLR2402	£3 00
18K	0.1	Beckman	A	£3 00
25K	0.5	Hellpot	SA1337	£3 00
29K	0.05	Beckman	SA1244	£4 50
30K	0.1	Colvern	2402	£1 50
30K	0.1	Beckman	SA95C	£3 00
30K	0.1	Beckman	A.88	£3 50
30K	0.1	Beckman	SA1692	£3 00
30K	0.25	Beckman	SA1679	£2 25
30K	1.0	Colvern	2402/1	£1 50
50K	0.1	Reliance	07-10	£2 25
50K	0.1	Colvern	07-5	£2 25
50K	0.1	Colvern	2503	£2 25
50K	0.1	Foxes	PX4	£2 25
50K	0.5	Beckman	A	£3 00
50K	0.1	Beckman	A	£3 00
100K/100K	0.1	Ford	A	£5 00
100K	0.1	Beckman	A	£3 50
100K	0.5	Beckman	A	£3 00
100K	0.1	Colvern	2501	£2 25
100K	0.1	Colvern	2610	£2 50
298K	0.1	Beckman	SA3902	£3 50
300K	0.1	Beckman	A	£3 50

**THREE TURN 780° ROTATION**

100/100	0.5	Beckman	C	£3 00
100/100	0.1	Beckman	Type C	£3 00
300	0.1	Beckman	9303	£2 25
1K	0.1	Fox	PX2/H3	£2 25
10K	0.5	Beckman	C.88	£2 25
20K/20K	0.1	Beckman	C.8	£3 00
10K/10K	0.1	Beckman	C	£3 00
50K	0.5	Beckman	C.8	£1 75

**FIFTEEN TURN 5400° ROTATION**

25K/25K	10 watts	Beckman B	10	£6 50
46K/46K	10 watts	Beckman B	10	£6 50

**TWENTY TURN 7200° ROTATION**

1 Meg	General Controls	PXM130	£4 00
50K	Reliance		£2 00

**156 TURN 56160° ROTATION**

480	Kelvin Hughes	KTP0701	£9 50
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**FIVE TURN 1800° ROTATION**

200	Relcon	HEL107-05	£2 25
500	Colvern	CLR2505	£2 00
U1-5K	Colvern	CLR2605	£2 00

**FIVE-AND-A-HALF TURN**

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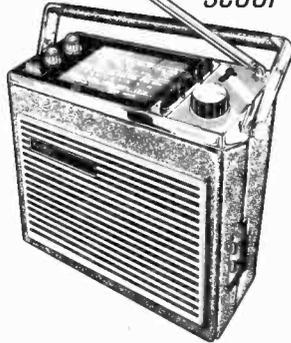
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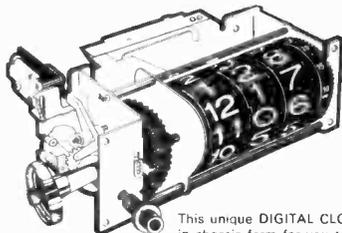
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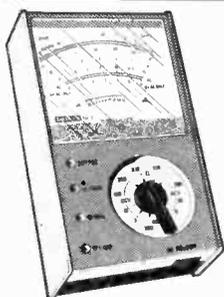
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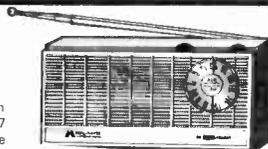
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BSY28	13p	OC28	40p
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Pri 200-220-240v. Sec. 250-0-250v. 50 M/A. 6.3v. Ia. 22/6 P. & P. 5/-.  
Pri 230v. 4.2v. Ia. 10/6 P. & P. 3/6.

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Pri. 10-0-200-220-240v. Sec. 2.5v 5a four times. 50/- Carr. 8/6.

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No.	Sec. Taps	Amps	Price	Carr.
1A	25-33-40-50	15	£10 10 0	12/6
1B	25-33-40-50	10	£7 12 6	9/6
1C	25-33-40-50	6	£6 15 0	9/6
1D	25-33-40-50	3	£4 0 0	7/6
2A	4-16-24-32	12	£7 2 6	8/6
2B	4-16-24-32	8	£5 7 6	8/6
2C	4-16-24-32	4	£3 12 6	7/6
2D	4-16-24-32	2	£2 7 6	5/-
3A*	25-30-35	40	£16 10 0	12/6
3B*	25-30-35	20	£10 5 0	10/6
3C	25-30-35	10	£7 5 0	8/6
3D	25-30-35	5	£4 2 6	7/6
3E	25-30-35	2	£3 2 6	7/6
4A*	12-20-24	30	£13 0 0	12/6
4B	12-20-24	20	£8 5 0	9/6
4C	12-20-24	10	£4 5 0	8/6
4D	12-20-24	5	£3 12 6	7/6
5A	3-12-18	30	£9 12 6	9/6
5B	3-12-18	20	£7 2 6	8/6
5C	3-12-18	10	£4 5 0	7/6
5D	3-12-18	5	£2 17 6	7/6
6A	48-56-60	1	£3 12 6	6/6
6B	48-56-60	1	£3 12 6	6/6
7A*	6-12	50	£10 7 6	10/6
7B	6-12	20	£6 2 6	8/6
7C	6-12	10	£3 17 6	7/6
7D	6-12	5	£2 15 0	6/6
8A	12-24	1	£1 12 6	6/6
9A	17-32	8	£6 6 0	6/6
10A*	9-15	2	£1 9 6	6/6
11A	6-3	15	£2 10 0	7/6
12A	30-25-0-25-30	2	£3 12 6	6/6

Note: By using the intermediate taps many other voltages can be obtained.  
Example: No. 1 ... 7-8-10-15-17-25-33-40-50v.  
No. 2 ... 4-8-12-16-20-24-32v.  
No. 5 ... 3-6-9-12-15-18v.

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2	150	4 lb	£2 12 6	6/6
3	300	6 1/2 lb	£3 12 6	6/6
4	500	8 1/2 lb	£5 2 6	8/6
5	1000	15 lb	£7 2 6	9/6
6	1500	25 lb	£9 15 0	10/6
7*	1750	28 lb	£14 15 0	12/6
8*	2250	30 lb	£17 17 6	15/-

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Also: 2203A, 2200A, 2202A.

Resolved Components Indicator VP 253/1a. Solartron Low Frequency Decade Oscillators. Solartron OS 103 and associated equipment. 2 Phase Low Frequency Oscillator, type Bo 567. Solartron. Solartron Synchro test set, type CT 428. Solartron AC Millivolt meter. Precision. Type VF 252.

**AERIAL CHANGE/OVER RELAYS** of current manufacture designed especially for mobile equipments, coil voltage 12 v., frequency up to 250 MHz at 50 watts. Small size only, 2 in. x 3/4 in. Offered brand new, boxed. Price 30/-. inc. P. & P.

**RECEIVERS COMMUNICATIONS**  
Marconi CR150. 2-60 MHz as new... £60  
Hallcrafters S27C 110-220 MHz... £40  
HRO Mx 500KHz-30MHz... £30  
Redifon R50M. 13KHz-32MHz... £95  
Reece Mace Double conversion 60KHz-31MHz... £60

**COAXIAL SWITCHES**  
American Manufacture

Suitable for aerial changeover and high frequency switching up to 1,000 MHz miniature Vacuum drawn type 110 vdc operation connections BNC and N types. Offered brand new, boxed. Price 65/-.

Hilger & Watts Microspin X Band Bridge. Type W957. Microspin Proton Head Frequency Meter. Type FAZ08. Microspin Modulator. Type FA 210. Microspin 1 cm Wave guide directional couplers, associated measuring equipment. High Voltage Klystron Power Supply Units. Type FA 80. Hilger & Watts Absorbance Converter, and many other items of interest offered. Brand new equipment.

**LEAD-ACID EQUIPMENT BATTERIES 10v 5AH.**

Transparent casing. Size 2 1/2 x 5 x 7 in. Offered brand new and boxed, 2 batteries per box, complete with links and full instructions. Can supply voltages in the range from 2-20 v. Price 45/-. incl. P. & P.

Burndet RF Plugs still available. These hard to find plugs are used on a multitude of equipment, especially Londez aerial c/o relays. Offered new ex. equipment. 2 for 10/-. inc. p.p.

Nife traction Batteries Nickel Iron. 1.2V per cell rated at 180 A.H. Sold in crates of three cells or crates of five cells. £4 per cell. Guaranteed best buy.

**BT91-500R THYRISTORS**  
500 PIV Max/rect. Current 16 amps. Guaranteed perfect. Price 25/- each.

**COLVERN HELICAL POTS**

1K ohms  
5K ohms  
10K ohms  
20K ohms  
30K ohms  
ALL TEN TURN  
PRICE 35/-

Wayne Kerr Impedance Bridge B521. Price £45.

Electronic Voltmeters for low level signal sources.

PYE High Impedance DC Amplifier for measurements better than 20 uV to 10 volts centre zero. Price £56.

Phillips GM 6010 1 mV FSD to 300 V in 12 ranges. Price £45.

Phillips PM 2520 1 mV FSD to 300 V in 12 ranges RMS voltmeter 10 Hz to 1 MHz. Price £45.

Dawe Model 616A transistorised Voltmeter 10 mV FSD to 300 volts. In 10 ranges. £27.

Levell Model TM2A transistor AC Voltmeter 1.5 mV FSD to 500 volts. £22. Solartron VF-252. AC millivoltmeter 1.5 mV for FSD to 15 V 30 M ohms impedance. Price £65.

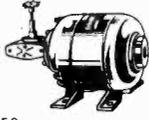
**H. W. SULLIVAN STANDARD AIR SPACED CONDENSERS**

Capacitance range 0 to 100 pf fully screened with engraved vernier subdivided into 100 equal divisions complete with vernier index and original manufacturers seal offered brand new, at only £25 each.

**P.F. RALFE** 10 CHAPEL ST. LONDON N.W.1  
Phone 01-723 8753

**GEARED MOTORS**

"Parvalux" Reversible 100 RPM Gearing Motor, Type S.D.14, 230/250v. A.C. 22 lb./in. spindle. 1st class condition. £7.50 each. P. & P. 50p. Also limited number only as above. Brand New. £12.50 each. P. & P. 50p.



**ELECTRIC CONTROL (CHICAGO).** Shaded pole 240v. 50 Hz. 110 rpm. 16 lb./in. £2.25. P. & P. 25p. 200 rpm 10 lb./in. £2.50. P. & P. 25p.

**MYCALEX.** Open frame, shaded pole motors. 240v. 50 Hz. 7 rpm. 28 lb./in. 80 rpm. 12 lb./in. £2.25 each. P. & P. 25p.

**SMITHS SYNCHRONOUS MOTORS.** 12 r.p.h. 240v., 50 Hz. 2 watts. 88p each. P. & P. 25p.

**KLAXON, HEAVY DUTY.** 240v. 50 Hz. 250 rpm Continuous rating. Torque 45 lb./in. Weight 36lbs. £18.50. P. & P. £1.50.

**"CROUZET" TYPE 965.** 115/240v. 50 Hz. 47/68 Watts. 50 rpm. Stoutly constructed. Size: 2 1/4" dia. x 3 1/2" long plus spindle 1 1/2" dia. Anti-clock. £2.75. P. & P. 25p.

**"TANSITOR" (U.S.A.) TANTALUM WET SINTERED ANODE POLARISED CAPACITORS.** DC size: 1 1/2" long x 3/8" dia. 200µF. 25v. DC size: 3/4" long x 1/4" dia. 180µF. 25v. DC size: 3/8" long x 1/4" dia. 150µF. 30v. DC size: 1" long x 3/8" dia. 2.5µF. 300v. DC size: 1 1/2" long x 3/8" dia. One wire each end. Also few only, Tansistor "MICRO-MODULE" capacitors 0.2 mfd. 15v. wire-ended, size: 1/2" dia. (disc). T.A.G. and Union Carbide 15 mfd. 10v. All types £1.25 per doz. (mixed or as required). Carriage paid.

**VINKOR POT CORE ASS. TYPE LA.2103.** Normal price £1.48. Our price 75p each. Special quote for quantity.

**AMPEX.** Dynamic stick microphone, high impedance, low noise. Offered well below makers price at £8.50. P. & P. 25p.

**Special offer of AMPEX professional tape heads, mu-metal shrouded.** (Designed for model AG20). Full track record, or playback, £4.50. Erase head £2.50. Set of 3 with mounting bracket and cover £10.50. Half track record or playback only, £4.50 each or £8.00 per pair with bracket and cover. Carriage paid.

**SYLVANIA CIRCUIT BREAKERS** gas filled providing a fast thermal response between 80° and 180°C. 10 amp. at 240v. continuous. Fault currents of 28 amps. at 120v. or 13 amp. at 240v. silver contacts. Supplied in any of the following opening temperatures: 90, 95, 100, 115, 120, 125, 130, 135, 140, 145, 150, 160, 170, 175. 3 for £1.00. £3.50 per dozen.

**"TEDDINGTON" CONTROLS THERMOSTAT TYPE TBB.** Adjustable between 75° and 120°C. Circuit cuts in again at 3° below cut-out setting. 42" capillary and sensor probe. The thermostat actuates a 15 amp. 250v. c/o switch. A second single pole on/off switch is incorporated in the adjustment mechanism. 88p. Carriage Paid.

**Painton Rotary Switch.** Type 72 (to P.O. spec. RC1416). 3 pole, 3 position, 2 bank. Offered at less than half normal price at £1.63. Carriage Paid.



**"GOYEN" PRESSURE SWITCH.** Incorporating differential adjustment between 2" and 12" water gauge (a max. of approx. 1/2 p.s.i.). A single pole change-over switch rated 15 amps. 250v. is actuated. Air inlet tube 3/8". On Projection 1/2". Overall size: dia. 3/8", depth 2" plus 3/8" (air tube). £1.25. Carriage Paid.

**THORN KEY SWITCH.** 3 change-over. Neat action, either locking or spring-return, as required determined by reversing fixing plate. Attractive plastic prestle. Available red, green, grey, cream. 60p each. Carriage paid.

**HONEYWELL (USA) Sub-miniature 2 bank panel mounting micro-switch, positive toggle action giving 2 change-overs. Size: 3/8" x 1/2" x 3/8". 63p each. Carriage paid.**

**"HONEYWELL" V3 Series.** Flush microswitch 10 amp. c/o. The side panel is insulated. End plate size: 2" x 1/2". £1.50 per doz. Carriage Paid.

**MARCONI SANDERS Micro-wave switch.** Type No. 6442. Maker's list price £75. Our price £7.10.0.



**BRAND NEW ALTERNATORS BY ENGLISH ELECTRIC.** All outputs are at 400 c.p.s. Type Input V. C.P.S. Ph.

1 220 50 3 } All these types give the same dual outputs as below

2 380/440 60 3 } V. Ph. V.A.

3 115 60 3 } 115 3 50

4 220 60 3 } 85 1 300

5 220 D.C. } 115 3 50

6 110 D.C. } 85 1 300

£30.00 each. Carriage extra

The following types each have 4 separate outputs (all at 400 c.p.s.).

7 380/440 50 3 } 115v. 28 W.; 115v. 250W; 20v. 6V; 28v. 250W;

8 110 D.C. } 115v. 28 W.; 85v. 250W; 20v. 6V; 115v. 250W.

9 24 D.C. } 115v. 28W; 115v. 250W; 20v. 6V; 28v. 250W.

10 110 D.C. } 115v. 28W; 115v. 250W; 28v. 250W; 20 v. 6V.

11 220 D.C. } 115v. 28W; 85v. 250W; 20v. 6V; 115v. 250W.

£42.50 each. Carriage extra

**WESGROVE VIDEO TAPE RECORDERS.** Unused but offered without guarantee to personal callers only at the extremely low price of £60.00 each. The following features are incorporated: Fixed heads (pre-heated reversible), speed 12 ft. per second, 1/2" twin-track tape will take 7,600 ft. triple play, 26 transistors (22 silicon), F.M. pulsed sound. Camera and mike inputs. 405/625. A real bargain for the enthusiast! Also available a few decks complete with heads £15.00 each. Also cameras £75.00 each (tested O.K.).

**MOTORS**



**AMPEX 7.5V. D.C. MOTOR.** This is an ultra-precision tape motor designed for use in the AMPEX model AG20 portable recorder. Torque 450GM/CM. Stall load at 500ma. Draws 60ma on run. 600 rpm ± 5% speed adjustment, internal AF/RF suppression. 1/2" dia. x 1" spindle, motor 3" dia. x 1 1/2". Original cost £16.50. Our price £4.25. P. & P. 25p. Large quantity available (special quotations). Mu-metal enclosure available 75p each.

**NEW HYSTERESIS MOTORS BY WALTER JONES.** Type 14050/12, 240v. 50 c/s 1500 rpm cont. rating, output 2.0 oz./in. Size: 3 1/2" x 2 1/2" x 2 1/2". Spindle 1" x 3/8". Weight 3 lb. Maker's price in region of £22.50 Our price £6.50 each. Carriage Paid.

**VACTRIC PRECISION D.C. MOTOR.** Type XO7P19. 10v. D.C. 0.66 amp. 8000 rpm. 30 gm/cm. Size 7. Original makers packing. Limited supply. £3.50 Carriage Paid.

**VACTRIC PRECISION D.C. MOTOR AND COUPLED GEAR HEAD.** Motor type 11P101, 28 volts, 5000 rpm, 120 gm/cm. Gear head type 15H102 ratio 300:1. Torque 10 lb./in. Makers packing. £14.50 Carriage Paid.

**MYCALEX MAINS.** Shaded pole, 1425 rpm. 3/8" spindle. 2 for £1.25 Carriage Paid.

**MAINS INDUCTION MOTOR.** Open frame, 1/2" spindle, weight 1/2 lb. Powerful. 88p each. P. & P. 12p

**E.M.I. PROFESSIONAL TAPE MOTOR.** 110/240 v. 50 Hz. 3000 rpm, reversible, silent running. 4 1/2" dia. x 4 1/2" long. Spindle 3/8" x 2". Weight 6 lbs. £3.50 each or £6.00 per pair. P. & P. 50p each.

Brand New "DISCUS" Centrifugal Blower by Watkins & Watson. 240v. 50 Hz. Powered by A.E.I. continuous rating 2850 rpm motor. Cowl diameter 10". Outlet flange 2" I.D. Coupling flange supplied. These superb precision units are ideally suited for Organ construction. Offered at approx. half makers price £15.50 Carriage £1.50

**PRECISION AND SERVO POTENTIOMETERS PRECISION LINE (USA).** Size 15. 300Ω ± 5% LIN. Continuous track plat. wipers set at 180°. £2.25 each. Carriage Paid.

**PENNY & GILES.** Size 15. 500 Ω. Type Q26201-72/1. Continuous track. £2.50 each. Carriage Paid.

**BECKMAN.** Type AS.506, 10 turn. Tol. ± 1%. LIN Tol. ± 0.7%. 40k. Long spindle. £2.00 each. Carriage Paid.

**S.T.C.** Type B330 CT. 2500 Ω. 2 1/2" dia. x 1 1/2". Completely copped encased. £1.25 each. Carriage paid.

**MARCONI SANDERS Micro-wave switch.** Type No. 6442. Maker's list price £75.00 Our price £7.50

**CRYSTAL OVENS G.E.C. Type QC940.** 6/12v., AC/DC, 75°C. Takes 2 1/2" min. crystals. Similar to above 12v. only by Snelgrove (Toronto). £2.75 each, carr. paid.

**BERCO.** Rotary rheostat. Type L25. 100 Ω. 25 watt. 1 1/2" dia. 1/2" spindle. 50p each. 13p Carriage.

**PAINTON BOURNS TRIMPOTS.** 1k, 2k, 2.5k, 5k, 10k, 20k, 50k, 500k. Other Trimmer pots in stock.

**RIL 10k. MORGANITE 1k. MEC 200 Ω (tubular) 50 Ω.** Any 3 for £1.10 carr. paid.

**"TEXAS"** Unmarked, Tested, TO5 Geranium general-purpose transistors. 24 for £1.00 P. & P. 13p. Large quantity available.

**CINEMA ENGINEERING Precision "Standard"** Wire Wound Resistors. Extremely high stability over very wide temperature range. 1/6 Watt 0.25% 30K, 75K 30p ea. 1/3 Watt 0.05% 9K, 10.02K, 50K, 200K, 60p ea. 0.1% 100K, 250K, 625K, 60p ea. 0.25% 477K, 60p ea. 0.5% 500K, 60p ea. 1% 500Ω, 850Ω, 3.770Ω, 3K, 4K, 5K, 10K, 15K, 50K, 90K, 375K, 450K, 60p ea. 1/3 Watt 0.05% 200Ω, 60p ea. 0.1% 9.65K, 14.6K, 15.33K, 500K, 800K, 1 meg, 60p ea. 0.5% 81K, 2.2 meg, 60p ea. 0.1% 20K, 1.35 meg, 1.5 meg, 2 meg, 3.3 meg, 60p ea. 1 Watt 0.05% 0.24959K. £1.00 ea. 0.1% 3.24K 1 meg, 3 meg, 4 meg, 3.75 meg, £1.00 ea. 1% 2.4 meg, 2.5 meg, 3.6 meg, £1.00 ea. 2 Watt 0.05% 5 meg, £1.50 ea. 0.1% 5.714 meg, 10 meg, £1.50 ea. 0.1% 2 meg, 2KM, £1.50 ea. 0.5% 5.9 meg, 10 meg, £1.50 ea. 1% 2K, 5K, 5 meg, 10 meg, £1.50 ea.

**RIL Type 2 ± 0.01% 6.666K £1.00 each.**

**RIL Type 9 ± 1% 560Ω 13p each.**

**ALMA ± 0.05% 50K 75p each.**

**ALMA ± 0.1% 141.46K 50p each.**

**SHALLCROSS ± 0.5% 3400Ω 30p each.**

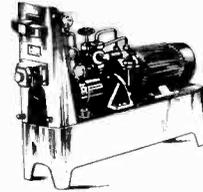
**ELECTRO-THERMAL PRECISTOR ± 0.1% 2.4K 50F each.**

**OXLEY P.T.F.E. BARB TERMINALS.** Lead thro' 7/8" or 3/4". Stand-Off 11/32" or 1/2". £2.75 box of 100 all types.

**HARWIN.** Tapped (6 Ba) high voltage "stand off" insulators, length 3/8" or 3/4", tapped (8 Ba) 3/8" long. £2.00 per 100. Carriage Paid.

**K.L.G. SEALED TERMINALS.** Type TLSI AA, overall length 1/2", box of 100, £1.00 Type TLSI BB, overall length, 1", box of 100, £1.50 Carriage Paid.

**VICKERS-SPERRY-RAND HYDRAULIC POWER UNIT.** This is a Pump Unit made for use in conjunction with a power ram. This equipment was originally designed for use with ships' steering but has many other applications. Further details on request. £95.00 Carr. extra.



**RELAYS**

Perspex enclosed, plug in, with base. Size 1 1/2" x 1 1/2" x 3/4" MQ 308 600Ω 24v. 4 c/o. 60p ea., £5.00 per doz. MQ 508 10,000Ω 100v. 4 c/o. 50p ea., £4.50 per doz. "ISKRA" 240 V.A.C. 3 c/o. 6 amp contacts. Size approx.: 1 1/2" x 1 1/2" x 1". 88p.

**SIEMENS** Miniature, plug in, Perspex cover, 1000 Ω 6/12v. 2 c/o. 3/4" x 1 1/2" x 1 1/2" high. Complete with base. 70p ea., £7.00 per doz.

**A.E.** Perspex enclosed, plug in, 50Ω 6v. 2 c/o. 63p ea. 470Ω 12v. 4 c/o. 73p ea. 2,780Ω 48v. 4 c/o. 73p ea. 1,260Ω 48v. 6 c/o. 83p ea.

**CLARE.** Sealed relay. Type RP3716G4. £1.25 ea.

**CLARE ELLIOTT.** Sub-min 675 Ω 24v. Type WJ 2 c/o. Similar to above. 340Ω 17.6v. 75p ea.

**MAGNETIC DEVICES.** Sub-min 24v. 2 c/o. 3/4" x 1 1/2" + 3/4". 75p ea.

**BOURNE.** Trimpot sub-miniature relay 18v. 1,000 Ω 1 amp. l c/o encapsulated 3/4" x 3/4" x 1 1/2" high. £1.25 ea.

**SIEMENS.** High speed type 89L. 1,700Ω + 1,700Ω, 63p ea.

**"B. & R."** 3 c/o. 10 amp. contacts (silver) operates on 2 volts D.C. Draws approx. 1 amp. Size: 2" x 1 1/2" x 1 1/2". £1.00.

**DIAMOND "H"** sealed relay. Type BR115CIT-IC 26v. 150 Ω 4 c/o encapsulated in heavy brass case glass sealed terminals. Robust. 75p ea.

**SCHRACK.** Octal base 24v. 2 HD c/o. Perspex enclosed, 63p.

**E.R.G.** 1,000 Ω 6v. DC. 1 make encapsulated reed type. Size: 3/4" x 3/4" x 1 1/2". 4 for £1.00.

**SANGAMO WESTON.** Moving coil relay 315 Ω 310µA, complete with base. 75p ea.

**S.T.C.** Midget sealed relay. Type 4190EC. 12v., 40mA 170 Ω. Single HD make. 53p ea.

**F.I.R.E.** Plug in relay, 115v., coil 50v. c.p.s., 3 heavy duty silver change-over contacts. Very robust. 63p ea.

**LATCH-MASTER.** Miniature relay 6, 12, 24v. DC. One make one break 5 amp contacts. Once current is applied relay remains latched until input polarity is reversed. 3/4" dia. x 3/8". Please state vertical or horizontal mount and voltage. Original cost £8.00, now offered at £1.63 ea.

**G.E.C.** Sealed relay. Type M 1492. 24v. 670 Ω. New condition but ex-equipment. £1.00 ea.

**HELLERMANN DEUTSCH.** Type L26F18. Latching relay. Latch coil 200 26v. DC. Reset 375 Ω 6 change-over switching. A truly superb relay. Measuring only 1 1/8" x 1" dia. £3.75 ea. Limited stock. All carriage paid.

**SCHRACK** Rotary Selector Relay RT304. 48v. coil (280 ohm). 48 positions, 4 sweep arms (4 pole 12 way). There are 2 secondary switches: (1) one c.o. H/duty contact set which changes over and back with each step; (2) two H/duty change-overs which change over on each 12th step and return on the following pulse. Size: 3 1/2" x 1 1/2" x 4 1/2" high. Also as above but 110v. (1,290 ohm coil). All new and in original maker's packing. £3.25. Carriage paid.

**ELECTROLYTIC CAPACITORS MULLARD.** 900µF 100v. heavy ripple screw terminals 1 1/2" dia. x 3 1/2", 70p ea., £6.00 per doz. 1,600µF 64v. 1 1/2" dia. x 3", 38p ea., £3.50 per doz. 10,000µF 10v. 1 1/2" dia. x 3", 38p ea., £3.50 per doz. 1,250µF 25v. 1" dia. x 2". 50p ea., £4.50 per doz.

**HUNTS** 1,000µF 50v. 1 1/2" dia. x 2", 25p ea., 10,000µF 6v. 1 1/2" dia. x 2", 30p ea., £3.00 per doz. 16µF 350v. 1 1/2" x 1 1/2" wire ends, £2.00 per doz. 32-32µF 275v. 1" dia. x 2", 38p ea. 100µF 100v. 1" dia. x 2", 25p ea.

**ERIE.** Ceramicon capacitor. Type CHV41P. 500 P.F. 30KV Size 1-5" dia. x 1-44" long. 50p ea. Carriage paid.

**MAINS 6 DIGIT COUNTER BY E.N.M. LTD.** Non-reset. Size: mounting plate 2" x 1 1/2". Unit size: 2 1/2" high x 1 1/2" x 1 1/2". £1.38.

**TIME ELAPSED REGISTER.** 24v. D.C. Has a 5 digit readout plus dial reading 1 hour (60 min. div.) metering. Total of 99,999 hrs. Non-reset sealed unit, chrome bezel, through panel mounting. Size 2 1/2" dia. x 3 3/4" overall. £3.25. Carriage paid.

**DEAC. RECHARGEABLE PERMA-SEAL** Nickel-Cadmium Batteries Type 900B. 1.22v. at 900 mA (10-hr. rate). Size 90 mm. x 13.5 mm. Weight 40 gr. Unused 63p ea. P. & P. 12p.



**"DECCO" MAINS SOLENOID.** Compact and very powerful. 16 lb. pull. 1" travel which can be increased to 1" by removing captive-end-plate. Overall size 2" x 2 1/2" x 2 1/2" high. £1.38. P. & P. 25p.

**American "POWERSTAT"** Variable Voltage Transformer. Input: 120v. 50/60 c.p.s. Output: 0-120v. at 2.25 amps. 1/2" spindle with alternative pre-set locking device. Size (approx.): 3" dia. x 2" long. First class condition. £2.00. Carriage paid.

**METERS**

**ERNEST TURNER 800µA METER.** 160 Ω movement, 2" case, elliptic plastic front. Green-Red-Green uncalibrated scale £1.50 each. Carriage Paid.



**MINIATURE B.P.L. 500-0-500 MICRO-AMMETER.** 1/8" dia. scale. Through panel mounting. Hermetically sealed. £1.63. Carriage paid.

**ERNEST TURNER 5" x 4" 0-1ma** scaled in 50 equal divisions, mirror scale, chrome escutcheon. Quality instrument. £4.25. Carriage Paid.

**5" x 4" 1000µA 1000 Ω.** Mirrored scale, few only. £4.75. Carriage Paid.

**"ATLAS" SUB-MINIATURE LAMPS (Capped).** —Ratings 5v. 60ma. 35 ± 25% Lumens. Life Expectancy 60,000 hours or at 6v. 70 ma. 75 ± 25% Lumens, 5,000 hours. Size: 9.1 x 3.1 mm. £1.50 per doz. £5.00 box of 50.

We welcome orders from established companies, educational depts., etc. (To cover invoicing costs minimum £2.50, please.) A discount of 10% may be deducted from all orders of £20.00 or over.

**ELECTRO-TECH SALES** BUSINESS HOURS: 264 PENTONVILLE ROAD, LONDON, N.1 9.30-6 (1 p.m. Sats.) (ONE MIN. FROM KINGS X STATION) Tel. 01-837 7401/2

# AUDIOTRINE A55 HIGH QUALITY STEREO SYSTEM

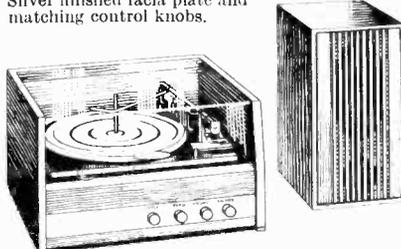
### 5 + 5 WATT OUTPUT

#### GARRARD 5200 CHANGER

with low mass pick-up arm and Stereo Cartridge. CONTROLS: TREBLE, BASS, VOLUME STEREO BALANCE.

Operation on 200-250 v. A.C. mains. Output rating I.H.F.M.

Luxurious Teak Veneer Finished Cabinets. Transparent plastic (tinted) cover included for main unit. Silver finished fascia plate and matching control knobs.



### PAIR OF LOUDSPEAKER UNITS

incorporating high flux 8 in. x 5 in. speaker. Size approx. 13 x 7 1/4 x 8 1/2 ins.

### PRICE COMPLETE ONLY

Carr. £1-25 **£42**  
Terms: Deposit £5.50 and 9 monthly payments £4.50 (Total £46).

# FANE 807 HIGH FIDELITY LOUDSPEAKER

A full range 8 in. 10 watt Unit for excellent sound quality in suitable enclosure. Roll P.V.C. cone surround and long throw voice coil to achieve very low fundamental resonance at 30 c.p.s. Tweeter cone is fitted to extend high tone response. Frequency range 25-15K Hz. Impedance 3Ω or 8-15 Ω. Cast Chassis. REMARKABLE VALUE.



**£3.50**

# AUDIOTRINE HIGH FIDELITY LOUDSPEAKERS

Heavy construction. Latest high efficiency ceramic magnets. Treated Cone surround or "L" indicates Roll Rubber surround. "D" indicates Tweeter Cone providing extended frequency range up to 15,000 c.p.s. Exceptional performance at low cost. Impedance 3 or 8-15 ohms.

WHEN ORDERING PLEASE STATE IMPEDANCE  
HF 102D 8" 8W £2.71 HF 120D 12" 15W £4.49  
HF 102D 10" 10W £3.40 HF 126 12" 15W £5.25  
HF 120 12" 15W £3.99 HF 126D 12" 15W £5.75

# FANE ULTRA HIGH POWER LOUDSPEAKERS

All power ratings are R.M.S. continuous. 2 years' guarantee. High flux ceramic magnets. Heavy cast chassis. ALL CARRIAGE FREE.

'POP' 100	'POP' 60	'POP' 50
18 in. 100 watt 14,000 gauss 8/15Ω	15 in. 60 watt 14,000 gauss 8/15Ω	12 in. 50 watt 13,000 gauss 15Ω
<b>£22.05</b>	<b>£12.90</b>	<b>£10.50</b>

Dep. £8 and 9 monthly payments £2 (Total £24).  
Dep. £3.30 and 9 monthly payments £1.30 (Total £15).  
Dep. £2 and 9 monthly payments £1.15 (Total £12.35).  
FOR BASS GUITAR OR ELECT. ORGAN, ETC.

# FANE LOUDSPEAKERS 'POP' 25/2

Dual cone 15Ω (for uses other than Bass Guitar or Electronic Organ. Or dep. £1 and 9 monthly payments 75p (Total £7.75). Carr. free.

# R.S.C. TA6 6 Watt High Fidelity Solid State Amplifier

200-250v. A.C. mains operated Frequency Response 30-20,000 c.p.s. -2dB. Harmonic Distortion 0.3% at 4,000 c.p.s. Separate Bass and Treble controls. 3 input sockets for Mike, Gram, Radio or Tape. Input selector switch. Output for 3-15 ohm speakers. Max. sensitivity 5mV. Output rating I.H.F.M. In fully enclosed enamelled case, approx. 9 1/2 x 2 1/2 x 5 1/2 in. Attractive brushed silver finish fascia plate 10 1/2 x 4 in. and matching knobs. Complete kit of parts with full wiring diagrams and instructions. Carr. 40p.  
**OR FACTORY BUILT WITH 12 months' g'tee. £9.45**

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1A5	0.25	6C9	0.73	6V7G	0.83	20P1	0.88	303	0.63	DM70	0.30	ECL82	0.33		
1A7GT	0.37	6C12	0.29	7B6	0.58	20P3	0.90	305	0.33	DM71	0.38	ECL83	0.52		
1B5	0.38	6C17	0.33	7B7	0.35	20P4	0.83	306	0.85	DW4/360	0.80	ECL84	0.60		
1D6	0.48	6C6DG	1.15	7C6	0.30	20P5	1.00	807	0.59		0.38	ECL85	0.55		
1FD1	0.35	6C16	0.38	7P8	0.68	25A6G	0.29	956	0.10	DY86/7	0.29	ECL86	0.40		
1FD9	0.22	6C16	0.43	7H7	0.28	25L6G	0.29	1821	0.53	DY802	0.48	EP22	0.63		
1G6	0.30	6C4V4	0.43	7R7	0.85	25V5	0.38	5763	0.50	E90P	1.20	EP76	0.38		
1H5GT	0.35	6D3	0.38	7V7	0.25	25V5G	0.43	6060	0.30	E90T	1.20	EP77A	0.35		
LL4	0.13	6B6	0.15	9B3V6	0.50	25Z4	0.30	7193	0.53	E88C	0.60	EP39	0.40		
LD5	0.30	6F1	0.63	9D7	0.78	25Z5	0.40	7475	0.70	E180F	0.95	EP40	0.50		
LLN5	0.40	6F6	0.63	10C1	1.25	25Z6G	0.43	A1834	1.00	E182CC1	1.13	EP41	0.50		
1N5GT	0.39	6F6G	0.95	10C2	1.00	30C1	0.30	A2134	0.98	E1148	0.53	EP42	0.33		
1R5	0.28	6F12	0.17	10C14	0.33	30C15	0.65	A3042	0.75	EA50	0.18	EP54	0.38		
1R4	0.24	6F13	0.33	10D1	0.50	30C17	0.80	AC044	1.18	EA76	0.85	EP71	0.33		
185	0.25	6F14	0.33	10F1	0.75	30C18	0.84	AC048	0.98	EAC80	0.33	EP80	0.23		
1U4	0.28	6F15	0.45	10F9	0.45	30F5	0.80	AC2PEND	EAC91	0.33	EP83	0.48			
1U5	0.48	6F18	0.45	10F18	0.35	30F11	0.84	0.98	EAF42	0.50	EP85	0.29			
2121	0.35	6F23	0.72	10L14	0.37	30P12	0.75	ACPEN	EB34	0.20	EP86	0.32			
3A4	0.20	6P24	0.68	10L1D1	0.53	30P12	0.80	ACPEN	(7)	EB41	0.50	EP89	0.25		
3A5	1.00	6P25	0.65	10P12	0.35	30P14	0.73	0.98	EB81	0.12	EP78	0.33			
3B7	0.25	6P26	0.29	10P13	0.65	30P14	0.32	AC/TH1	50	EB04	0.48	EP92	0.13		
3D6	0.19	6P28	0.70	10P14	1.10	30P15	0.84	AC/TP	0.98	EB08	0.33	EP97	0.65		
3Q4	0.38	6G6G	0.75	10P18	0.33	30P17	0.78	AL60	0.78	EB09	0.20	EP98	0.55		
3Q5GT	0.35	6H6GT	0.15	12A6	0.63	30P4MR	0.98	ARP3	0.35	EB09	0.30	EP183	0.30		
3B4	0.29	6V3G	0.19	12A0G	0.40	30P12	0.69	ATP4	0.12	EBP80	0.30	EP184	0.30		
3V4	0.32	6J6	0.18	12A0B	0.40	30P16	0.33	AZ1	0.40	EBP83	0.40	EP180	0.75		
4H4G	0.53	6J7G	0.24	12A0E	0.58	30P18	0.33	AZ31	0.46	EBP89	0.32	EP90	0.38		
5V4G	0.38	6J7GT	0.28	12A0F	0.23	30P19/30P4	AZ41	0.63	EB121	0.60	EK90	0.24			
5Y3GT	0.28	6K7G	0.10	12A17	0.19	0.60	B319	0.32	EC53	0.63	EL32	0.18			
5Z3	0.45	6K7GT	0.23	12A16	0.24	30P11	0.69	CL33	0.98	EC54	0.50	EL34	0.53		
5Z4G	0.35	6K6G	0.20	12A19	0.23	30P12	0.37	CV6	0.53	EC70	0.24	EL37	0.67		
630L2	0.58	6L1	0.98	12A0V	0.28	30P13	0.78	CV8	0.98	EC86	0.63	EL41	0.55		
6A8G	0.33	6L6GT	0.39	12A1X	0.23	30P14	0.75	CY1C	0.53	EC88	0.60	EL42	0.53		
6AC7	0.18	6L7GT	0.63	12A1Y	0.68	30P15	0.98	CY31	0.38	EC92	0.35	EL51	0.50		
6AG5	0.25	6L18	0.45	12B46	0.30	35A3	0.50	D63	0.25	ECC32	1.58	EL83	0.38		
6AK5	0.25	6L19	1.38	12B66	0.30	35A5	0.75	D77	0.12	ECC33	1.58	EL84	0.24		
6AK6	0.30	6L20	0.48	12B87	0.40	35D3	0.70	DAC32	0.25	ECC40	0.60	EL85	0.40		
6AL5	0.12	6N7GT	0.40	12E1	0.85	35L6GT	0.44	DAF91	0.22	ECC81	0.18	EL86	0.40		
6AM4	0.83	6P15	0.24	12T7GT	0.33	35W4	0.23	DAF96	0.35	ECC82	0.23	EL91	0.25		
6AM6	0.17	6P28	1.26	12K5	0.50	35Z4	0.50	DC990	1.00	ECC90	0.23	EL95	0.35		
6AQ5	0.28	6Q3G	0.30	12K7GT	0.34	35Z4GT	0.24	DD4	0.53	ECC84	0.30	EM34	0.90		
6AR6	1.00	6Q7GT	0.43	12K7GT	0.28	35Z5GT	0.30	DF33	0.39	ECC85	0.28	EM80	0.38		
6AT6	0.20	6R7G	0.35	12A7GT	0.40	50B6	0.35	DF91	0.14	ECC86	0.40	EM81	0.42		
6AU6	0.25	6R7	0.55	0.50	50C5	0.32	DF96	0.35	DM84	0.35	EM84	0.34			
6AV6	0.30	6A7GT	0.35	128C7	0.35	50D6GT	0.17	DF97	0.63	ECC189	0.48	EM87	0.38		
6B8G	0.13	68C7GT	0.33	128G7	0.23	50L6GT	0.45	DF98	0.30	ECC80	0.58	ET31	0.37		
6BA6	0.25	68V7	0.33	128H7	0.23	0.33	DH76	0.28	ECC807	1.35	EY81	0.35			
6BE6	0.24	68H7	0.53	128K7	0.23	0.77	0.53	DH77	0.20	ECC80	0.33	EY83	0.55		
6BE6	0.43	68J7GT	0.35	128L7	0.24	85A2	0.43	DH81	0.58	ECC82	0.33	EY84	0.50		
6B86	0.43	68K7GT	0.28	128Q7GT	0.85A3	0.40	DH101	1.25	ECC86	0.65	EY87	0.38			
6BQ5	0.24	68N7GT	0.28	0.50	90AG	0.38	DK32	0.37	ECC804	EY88	0.43	PAC80	0.35		
6PQ7A	0.38	68Q7	0.38	14H7	0.48	90AV	3.35	DK40	0.55	2.10	EY91	0.53	PC86	0.52	
6BR7	0.73	68T4T	0.60	0.33	90C1	1.70	DK91	0.28	ECC821	0.83	EZ35	0.25	PC88	0.52	
6BR8	0.63	6V6G	0.18	18A05	0.24	90CV	1.68	DK92	0.43	ECC835	0.29	EZ40	0.40		
6BS7	1.25	6U7G	0.53	19H1	2.00	90C1	0.80	DK96	0.37	ECH42	0.84	EZ41	0.43		
EZ80	0.23	PC800	0.38	PY81	0.27	UY85	0.29	and diodes	AF139	0.65	GD4	0.32	OC22	0.38	
EZ81	0.24	PC804	0.32	PY82	0.27	U10	0.45	IN1124	0.53	AF178	0.68	GD5	0.28	OC23	0.38
EZ90	0.22	PC805	0.33	PY83	0.29	U12/14	0.38	2N404	0.18	AF180	0.48	GD6	0.28	OC24	0.38
FW4	/500	PC808	0.48	PY88	0.34	U16	0.75	2N506	0.53	AF181	0.70	GD7	0.28	OC25	0.38
FW4/800	0.75	PC819	0.49	PY500	1.08	U18/20	0.75	2N2147	0.85	AF239	0.38	GD10	0.20	OC28	0.60
GZ37	0.75	PC805	0.64	PY800	0.38	U19	1.73	2N2297	0.23	ASV27	0.43	GD11	0.20	OC29	0.68
GZ30	0.35	PC806	0.78	PY801	0.34	U22	0.39	2N2309A	ASV28	0.38	GD12	0.20	OC35	0.32	
GZ32	0.45	PC808	0.64	PZ30	0.48	U25	0.65	2N3988	0.50	ASV29	0.50	GD14	0.50	OC36	0.43
GZ33	0.70	PCF80	0.30	QV03/10	0.26	0.58	2N3013	0.38	BI181	0.50	GD15	0.20	OC37	0.43	
GZ34	0.53	PCF82	0.33	0.30	U31	0.30	2N3033	0.33	BI182	0.50	GD16	0.20	OC41	0.50	
GZ37	0.75	PCF84	0.30	QV75/20	0.63	U33	1.48	2N3121	0.26	BI115	0.14	GT111	0.78	OC42	0.63
HAB080	0.45	PCF86	0.50	Q150/15	0.35	0.83	2N3703	0.19	BA116	0.25	GT113	0.20	OC43	1.18	
HL13C	0.20	PCF87	0.80	0.63	U37	1.75	2N3709	0.20	BA129	0.13	GT116	0.40	OC44	1.10	
HL23D	0.40	PCF200	0.67	QV04/7	0.63	U45	0.78	2N3806	0.10	BA130	0.10	GT118	0.20	OC45	1.13
HL41D	0.88	PCF800	0.65	R10	0.75	U47	0.85	2N3988	0.50	BOY10	0.45	GT119	0.20	OC46	1.15
HL42D	0.50	PCF801	0.35	R11	0.98	U48	0.59	28323	0.50	BOY12	0.50	GT120	0.38	OC47	1.13
HN309	1.37	PCF820	0.45	R16	1.75	U50	0.28	AA119	0.15	BOY33	0.20	GT347	0.43	OC70	1.13
HRK2	0.53	PCF805	0.64	R17	0.88	U76	0.24	AA120	0.15	BOY34	0.23	GT372	0.55	OC71	1.13
HVR2A	0.53	PCF806	0.64	R18	0.50	U78	0.22	AA129	0.15	BOY39	0.23	GT373	0.15	OC72	0.13
HVR2B	0.53	PCF808	0.73	R19	0.33	U107	0.92	AAZ13	0.18	BOY39	0.25	GT382	0.50	OC74	0.23
IW4/350	0.38	PCF812	0.75	R26	0.59	U153	0.27	AC107	0.15	BO107	0.13	GT387	0.23	OC75	0.13
IW4/500	0.38	PCF820	0.62	R32	0.38	U191	0.63	AC113	0.25	BO108	0.13	GT389	0.23	OC76	0.15
PCF82	0.37	RG1/240A	U192	0.27	AC114	0.40	BO113	0.25	BO130	0.23	OC77	0.27			
PCF83	0.50	U193	0.34	AC127	0.20	BO115	0.15	GT389	0.23	OC78	0.15				
PCF84	0.38	RA34	0.38	U251	0.73	AC128	0.20	BO116	0.25	GT389	0.23	OC78D	0.15		
PCF85	0.45	SP13C	0.63	U281	0.40	AC154	0.25	BO118	0.23	GT389	0.23	OC79	0.40		
PCF86	0.48	SP13C	0.63	U282	0.40	AC156	0.20	BO121	0.38	GT389	0.23	OC81	0.13		
PCF87	0.78	SP13C	0.63	U291	0.50	AC157	0.25	BO119	0.45	GT389	0.23	OC81D	0.18		
PCF88	0.25	PCF801	0.69	TH43B	0.50	U301	0.53	AC165	0.25	GT389	0.23	OC82	0.15		
PCF89	0.33	TE233	0.98	U329	0.27	AC167	0.25	BO159	0.25	GT389	0.23	OC82D	0.15		
PCF90	0.45	TP2620	0.98	U381	0.29	AC167	0.20	BO163	0.20	GT389	0.23	OC83	0.20		
PCD50	1.44	UAC80	0.33	U403	0.33	AC168	0.38	BO173	0.38	GT3	0.25	OC84	0.24		
PCN4D1	0.42	UAF42	0.52	U404	0.38	AC169	0.33	BO180	0.30						

**STANDARD GPO DIAL TELEPHONES** (black) with internal bell. 87p. P. & P. 25p. Two for £1 50. P. & P. 37p.

**TRANSISTORISED FIELD RATEMETER** type 1308A range 0.05 to 25 m/hr in 5 ranges size 12x34x74 ins. £10 each. P. & P. 50p.

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**DOSIMETER** 0-50R 0-150R and charger £2. P. & P. 7/8. Charger only 30/-, P. & P. 33p.

**PHOTOMULTIPLIERS**. EMI 6097X at £8 50 ea. 6097B—£5 ea.

**TRANSISTOR OSCILLATOR**. Variable frequency 40 c/s to 5 kc/s. 5 volt square wave o/p, for 6 to 12v DC input. Size 1 1/2 x 1 1/2 x 1 1/2 in. Not encapsulated. Brand new. Boxed. 57p ea.

**CRAMER TIMER** 28V DC Sweep 1/100th sec & sweep 60 secs. 4" dial. Remote control stop/start reset £6 50.

**RELAYS**  
G.E.C. Sealed Relays High Speed 24V. 2 make 2 break. 23p ea.  
S.I.C. sealed 2 pole c/o. 2,500 ohms. (okay 24v) 13p ea; 12v 35p ea.

**CARPENTERS** polarised Single pole c/o 20 and 65 ohm coil as new, complete with base 37p ea.  
Single pole c/o 14 ohm coil 33p ea; Single pole c/o 45 ohm coil 33p ea.

**POTENTIOMETERS**  
COLVERN Brand new. 50; 100; 250; 500 ohms; 1; 2.5; 5; 10; 25; 50k all at 13p ea. Special Brand new MORGANITE 2.5K; 250K; 500K 2.5 meg. 1" sealed. 17p ea.

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**INSTRUMENT** 3" Colvern. 5; 25 ohms 35p ea.

**BOURNE TRIM POTS**. 10; 20; 50; 100; 200; 250; 500 ohms; 1; 2.5; 5; 25K at 35p ea.

**ALMA** precision resistors 100K; 400K; 497K; 998K; 1 meg—0.1. 27p ea.; 3.25K—0.1. 20p ea.

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ERIE feed through ceramic 2200 pf—4p ea.  
Sub-min. TRIMMER 1/2 square. 8, 5pf. Brand new 13p ea.  
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E.H.T. 2 mfd 5 KV. Brand new £1 50 ea.  
E.H.T. 0.1 mfd 7 KV at 40p ea.; 0.1 mfd 5 kv at 35p ea.

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**STEP DOWN ISOLATING** trans. Standard 240V AC to 120V tapped 60-0-60 700W. Brand new. £5 ea.  
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**RACAL RA17K receivers £250**.  
Racal RA98A Automatic SSB adaptor for above. Brand new crate. £75.

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**BRAND NEW INSTRUMENTS HOUSING**. Size 8x6x7" deep. Comprising of anodised aluminium front and rear linked frame with recessed light blue front and rear panels. Detachable dark grey vinyl covered aluminium covers. Price £3 87 ea. P. & P. 25p.

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8½ x 5½ x 1/16 in. 2/6 sheet, 5 for 10/-  
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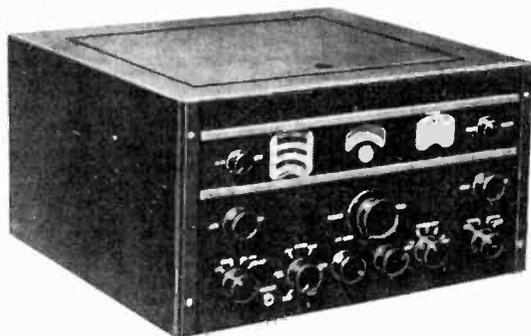
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**MARCONI SIGNAL GENERATOR TYPE TF-144G**: Freq. 85 Kc/s-25Mc/s in 8 ranges. Incremental: ± 1% at 1Mc/s. Output: continuously variable 1 microvolt to 1 volt. Output Impedance: 1 microvolt to 100 millivolts, 10 ohms 100mV - 1 volt - 52.5 ohms. Internal Modulation: 400c/s sinewave 75% depth. External Modulation: Direct or via internal amplifier. A.C. mains 200/250V, 40-100c/s. Consumption approx. 40 watts. Measurements 29 x 12½ x 10 in. New condition. £45 each, carr. £1-50.

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**SOLARTRON PULSE GENERATOR GP1101.2:** Period—2 microsecs to 100 msec; Pulse Duration—1 microsec to 100 msec; Delay time—1 microsec to 10 msec. All continuously variable in 5 ranges with fine control. Accuracy  $\pm 10\%$ . Pulse Amplitude—0.5V-100V. Accuracy  $\pm 10\%$  continuously variable in 4 ranges with fine control. Double Pulses; Pre-Pulse; Triggering; Square Wave Output; Squaring Amplifier. Input—100-250V, 50-60 c/s. New condition with Manual. Price: £85 each + £1.25 carr.

**USM-24C OSCILLOSCOPE:** 3 in. oscilloscope with 2c/s to 10Mc/s vertical response, and 8c/s to 800Kc/s horizontal response. Sensitivity 50 mv. rms/inch. Triggered sweep, built-in trigger pulses and markers. Mains input 115V, 50c/s. Complete with all leads, probes and circuit diagram. £42.50 each, carr. £2.

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**SIGNAL GENERATOR TYPE 902:** (P.R.D.). A portable, general-purpose, broadband, microwave signal generator designed for testing and maintenance of aircraft radio and radar receivers in the SHF band. The RF output level is regulated by a variable attenuator calibrated in dbm. The frequency dial is calibrated in Mc/s. Provision is made for external modulation. Power Supply—115V,  $\pm 10\%$  A.C., 50 c/s. Freq.—3650-7300 Mc/s. Internal Transmission—CW, Pulse, FM. External Transmission—Square Wave, Pulse. Power Output—0.2 milliwatts. Output Attenuator: -7 to -127 dbm. Load—50  $\Omega$ . Price: £135 each + £2 carr.

**TEST SET TS-147C:** Combined signal generator, frequency meter and power meter for 8500-9600 Mc/s. CW or FM signals of known freq. and power or measurement of same. Signal Generator: Output -7 to -85 dbm. Transmission—FM, PM, CW. Sweep Rate—0-6 Mc/s per microsec. Deviation—0-40 Mc/s per sec. Phase Range—3-50 microsec. Pulse Repetition Rate—2000 pulses per sec. RF Trigger for Sawtooth Sweep—5-500 watts peak. 0.2-6 microsec. duration, 0.5 microsec pulse rise time. Video Trigger for Sawtooth Sweep—Positive polarity, 10-50V peak. 0.5-20 microsec duration at 10% max. amplitude, less than 0.5 microsec rise time between 90% and 10% max. amplitude points. Frequency Meter: Freq. 8470-9360 Mc/s. Accuracy— $\pm 2.5$  Mc/s per sec. absolute,  $\pm 1.0$  Mc/s per sec. for freq. increments of less than 60 Mc/s relative,  $\pm 1.0$  Mc/s per sec. at 9310 Mc/s per sec. calibration point. Accuracy measured at 25° C and 60 humidity. Power Meter: Input: +7 to +30 dbm. Output -7 to -85 dbm. Price: £75 each + £1 carr.

**SIGNAL GENERATOR TS-418/URM49:** Covers 400-1000 Mc/s range. CW, Pulse or AM emission. Power Range—0-120 dbm. Price: £105 each + £1.25 carr.

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**CT.381 FREQUENCY SWEEP SIGNAL GENERATOR:** 85Kc/s-30Mc/s and response curve indicator with 6in. CRT tube and separate power supply. Fully stabilised. Price and further details on request.

**CANADIAN HEADSET ASSEMBLY:** Moving coil headphones 100 $\Omega$  with chamois leather earmuffs. Small hand microphone complete with switch and moving coil insert. New Condition. £1.75 each, post 25p.

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**TCS MODULATION TRANSFORMERS,** 20 watts, pr. 6,000 C.T., sec. 6,000 ohms. Price £1.25, post 25p.

**SOLENOID UNIT:** 230 v. A.C. input, 2 pole, 15 amp contacts, £2.50 each. post 30p.

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**OHMITE VARIABLE RESISTOR:** 5 ohms, 5 $\frac{1}{2}$  amps; or 2.6 ohms at 4 amps. Price (either type) £2 each, 25p post each.

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**MARCONI DEVIATION TEST SET TF-934:** 2.5-100Mc/s (can be extended up to 500Mc/s on Harmonics). Dev. Range 0-75Kc/s in modulation range 50c/s-15Kc/s. 100/250V. a.c. £45 each, £1.50 carr.

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ACV22	19p	CBV2	15p	NK780216	75p	2N698	30p
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AF116	25p	C20	15p	OA90	8p	2N1090	30p
AF117	25p	C22	15p	OA91	8p	2N1091	33p
AF118	44p	C24	15p	OA95	8p	2N1131	30p
AF124	25p	C27	15p	OA200	10p	2N1132	30p
AF126	17p	CP	15p	OC19	37p	2N1302	20p
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BC148	15p	NKT135	26p	OC45	15p	2N2369	17p
BC149	15p	NKT137	32p	OC71	15p	2N2369A	20p
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BC183	10p	NKT214	23p	OC81	23p	2N2905A	75p
BC183L	9p	NKT215	21p	OC81D	20p	2N2906	44p
BC184	15p	NKT216	46p	OC81Z	55p	2N2906A	54p
BC184L	15p	NKT217	50p	OC82	25p	2N2926 all colours	10p
BC212	17p	NKT218	25p	OC82D	15p	2N3053	25p
BC212L	12p	NKT219	25p	OC83	23p	2N3054	63p
BCY30	25p	NKT223	37p	OC84	25p	2N3055	75p
BCY31	48p	NKT224	25p	OC139	25p	2N3702	11p
BCY32	50p	NKT225	21p	OC140	35p	2N3702	11p
BCY33	20p	NKT229	29p	OC170	25p	2N3703	10p
BCY34	25p	NKT237	31p	OC171	30p	2N3704	11p
BCY38	30p	NKT238	19p	OC200	37p	2N3705	10p
BCY70	17p	NKT240	20p	OC201	47p	2N3706	9p
BCY71	17p	NKT240	20p	OC202	63p	2N3707	11p
BCY72	16p	NKT241	21p	OC203	37p	2N3708	7p
BD121	£1.10	NKT242	15p	OC204	40p	2N3709	9p
BD123	£1.10	NKT243	56p	OC205	65p	2N3710	9p
BD124	£1.03	NKT244	17p	OC206	75p	2N3711	9p
BDY20	£1.05	NKT245	17p	OC207	75p	2N3819	35p
BF115	25p	NKT261	21p	OCPT7/M	47p	2N3820	60p
BF163	40p	NKT262	19p	ORP12	50p	2N3826	30p
BF167	25p	NKT264	21p	ORP60	60p	2N4058	17p
BF173	30p	NKT271	18p	ORP61	40p	2N4060	20p
BF178	52p	NKT272	17p	P346A	19p	2N4061	20p
BF180	37p	NKT274	43p	ST140	15p	2N4062	20p
BF181	37p	NKT275	23p	ST141	20p	2N4284	15p
BF184	25p	NKT279A	12p	TD716	60p	2N4287	15p
BF185	25p	NKT281	29p	TIP31A	62p	2N4289	15p
BF194	17p	NKT302	87p	TIP32A	74p	2N4871	40p
BF195	15p	NKT304	79p	V405A	46p	3N84	£1.40
BF200	35p	NKT351	75p	ZTX10B	11p	3N128	69p
BFX13	25p	NKT401	71p	ZTX300	13p	3N140	76p
BFX29	31p	NKT403	65p	ZTX302	18p	3N141	73p
BFX84	26p	NKT404	60p	ZTX303	18p	3N152	86p
BFX85	34p	NKT405	79p	ZTX304	27p	40250	55p
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BFX87	30p	NKT420	£1.83	ZTX320	30p	40310	45p
BFX88	25p	NKT451	58p	ZTX330	18p	40312	48p
BFY50	23p	NKT452	54p	ZTX501	16p	40320	36p
BFY51	19p	NKT453	50p	ZTX502	20p	40360	43p
BFY52	20p	NKT603F	30p	ZTX503	17p	40361	48p
BFY53	16p	NKT613F	30p	ZTX504	40p	40362	58p
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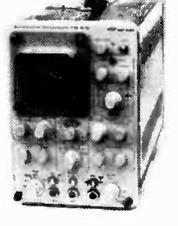
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2D21	0.35	6AT6	0.30	6S8C	0.35
2E24	2.55	6AU6	0.25	6S8D	0.35
2K25	8.00	6AV5GTA	0.92	6S8E	0.35
2X2	0.37	6AV6	0.30	6S8F	0.35
3A4	0.35	6AW8A	0.55	6S8G	0.35
3B4	0.60	6AX4GTB	0.62	6S8H	0.35
3B28	2.15	6AX5GT	0.62	6S8I	0.35
3B21	2.75	6AX6GT	0.62	6S8J	0.35
3D6	2.00	6B4G	1.05	6S8K	0.35
3D21A	2.00	6B4G	1.05	6S8L	0.35
3Q4	0.40	6B7	0.40	6S8M	0.35
3Q5GT	0.45	6B8G	0.20	6S8N	0.35
384	0.35	6BA6	0.25	6S8P	0.35
3V4	0.45	6BE6	0.30	6S8Q	0.35
4-125A	8.00	6BF5	0.80	6S8R	0.35
4-400A	16.00	6BF6	0.50	6S8S	0.35
4B2	4.00	6BH6	0.45	6S8T	0.35
4HA5	0.45	6BJ6	0.45	6S8U	0.35
4THA	0.45	6BK4B	1.20	6S8V	0.35
5AR4	0.60	6BK7A	0.55	6S8W	0.35
5B/254M	2.25	6BL7GTA	0.62	6S8X	0.35

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329A	1.90	AX50	2.25	E180G	1.25	ECL82	0.35	EL360	1.15	HBC91	0.30
329B	1.90	C1A	4.50	E180H	0.90	ECL83	0.65	EL803	1.00	HP93	0.35
329C	1.90	G1K	4.50	E280F	2.10	ECL84	0.55	EL821	0.55	HP94	0.30
329D	1.90	GBL1	0.90	E810F	2.90	ECL85	0.55	EL822	0.90	HK90	0.35
329E	1.90	GBL31	0.90	EAS2	2.00	ECL86	0.40	EL800	0.75	HL23	0.40
329F	1.90	GL4	0.80	EAS2	4.50	ECL87	0.40	EL805	0.50	HL23DD	0.40
329G	1.90	GL3	3.75	EAB30	1.50	EM34	0.90	EM34	0.90	HL23DD	0.40
329H	1.90	GL3	3.75	EAB30	1.50	EM71	0.75	EM71	0.75	HL23DD	0.40
329I	1.90	GL3	3.75	EAB30	1.50	EM80	0.40	EM80	0.40	HL23DD	0.40
329J	1.90	GL3	3.75	EAB30	1.50	EM81	0.90	EM81	0.90	HL23DD	0.40
329K	1.90	GL3	3.75	EAB30	1.50	EM84	0.25	EM84	0.25	HL23DD	0.40
329L	1.90	GL3	3.75	EAB30	1.50	EM85	1.00	EM85	1.00	HL23DD	0.40
329M	1.90	GL3	3.75	EAB30	1.50	EM87	0.55	EM87	0.55	HL23DD	0.40
329N	1.90	GL3	3.75	EAB30	1.50	EM88	0.55	EM88	0.55	HL23DD	0.40
329O	1.90	GL3	3.75	EAB30	1.50	EM89	0.55	EM89	0.55	HL23DD	0.40
329P	1.90	GL3	3.75	EAB30	1.50	EM90	0.55	EM90	0.55	HL23DD	0.40
329Q	1.90	GL3	3.75	EAB30	1.50	EM91	0.55	EM91	0.55	HL23DD	0.40
329R	1.90	GL3	3.75	EAB30	1.50	EM92	0.55	EM92	0.55	HL23DD	0.40
329S	1.90	GL3	3.75	EAB30	1.50	EM93	0.55	EM93	0.55	HL23DD	0.40
329T	1.90	GL3	3.75	EAB30	1.50	EM94	0.55	EM94	0.55	HL23DD	0.40
329U	1.90	GL3	3.75	EAB30	1.50	EM95	0.55	EM95	0.55	HL23DD	0.40
329V	1.90	GL3	3.75	EAB30	1.50	EM96	0.55	EM96	0.55	HL23DD	0.40
329W	1.90	GL3	3.75	EAB30	1.50	EM97	0.55	EM97	0.55	HL23DD	0.40
329X	1.90	GL3	3.75	EAB30	1.50	EM98	0.55	EM98	0.55	HL23DD	0.40
329Y	1.90	GL3	3.75	EAB30	1.50	EM99	0.55	EM99	0.55	HL23DD	0.40
329Z	1.90	GL3	3.75	EAB30	1.50	EM100	0.55	EM100	0.55	HL23DD	0.40

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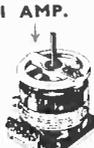
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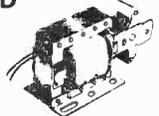
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**EXTREMELY POWERFUL SOLENOID** with approximately 14lb. pull, 1 inch travel. Fitted with mounting feet 4 inches long, 2 1/2 inches wide and 3 inches high. Price £2.00 including post & pkg.



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25 ohm coil, 24 v. D.C. operation. £5.88, plus 13p P. & P.

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3 banks of 11 positions, plus homing bank. 40 ohm coil 24-36 v. D.C. operation. Carefully removed from equipment and tested. £1.13, plus 13p P. & P.



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(NFW) Ceramic construction, winding embedded in Vitreous brush assembly designed for continuous duty. **AVAILABLE FROM STOCK IN THE FOLLOWING VALUES:**  
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185	6-12 4 c/o E-E	50p*	1250	24-36	4 c/o	63p*	
230	6-12 2 c/o	63p*	1250	36-45	6M	63p*	
280	6-12 2 c/o	73p*	2500	36-45	6M	63p*	
700	16-25 4M 2B	63p*	5800	80-85	4 c/o	50p*	
700	16-24 4 c/o	78p*	9000	40-70	2 c/o	50p*	
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(1) Coil ohms; (2) Working d.c. volts; (3) Contacts; (4) Price E-E Ex. Equipment. All Post Paid.

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## 200-250 v. 1 R.P.M. MOTOR

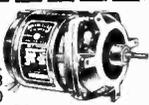
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Spindle length 1 3/16", diameter 1/4". Manufactured by SEC. Price £1.13 plus 18p p. & p.



200/250v. 1/2 RPM Motor (Mfg by Smith Price 75p inc. post)

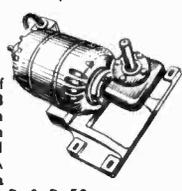
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The above two precision made U.S.A. motors are offered in 'as new' condition. Input voltage of motor 115v A.C. Supplied complete with transformer for 230/240v A.C. input  
Price, either type £3.15 plus 23p P. & P. or less transformer £2.13 plus 23p P. & P.  
These motors are ideal for rotating aerials, drawing curtains, display stands, vending machines etc. etc.



## PARVALUX TYPES DI9 230/250 VOLT AC REVERSIBLE GEARED MOTORS

30 r.p.m. 40 lb. ins. Position of drive spindle adjustable to 3 different angles. Mounted on substantial cast aluminium base. Ex-equipment. Tested and in first-class running order. A really powerful motor offered at a fraction of maker's price. £6.30, P. & P. 50p.



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## Electronics Maintenance Engineers

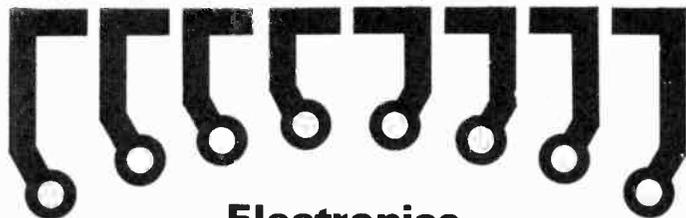
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Tel: 01-573 3888, Ext. 2523.**



### Electronics Maintenance Engineer

An engineer, possibly with Computer maintenance experience, is required to maintain and service the fastest radio paging system in the world. This unique equipment has recently been installed at the London Stock Exchange in the City of London. The man appointed will probably be educated to O.N.C. (electronics) or equivalent standard. Two years' experience of maintaining digital control equipment is desirable. The man must be capable of working on his own initiative and will probably be aged over 25 years. Starting salary will be in the region of £1,500 p.a. plus overtime.

### Electronics Engineers

Additional Maintenance Engineers are required in our Radio Paging and Public Address Maintenance Workshop. The men appointed will be required to repair and maintain miniaturised transistor equipment. Previous experience in fault finding or production testing digital equipment is desirable. C. & G. Inter-Telecomms. or Radio an advantage. One of the engineers will be required to take charge of the maintenance and repair of public address equipment.

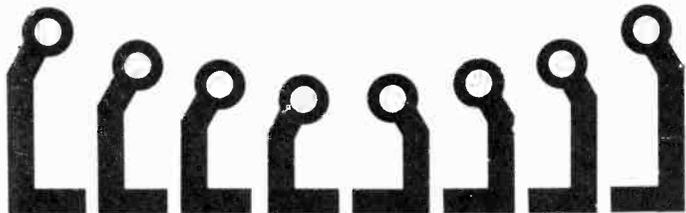
*All these vacancies are staff appointments and benefits include realistic and progressive salaries, 3 weeks holiday, sickness payment scheme and pension and life assurance schemes. For further details or an early interview, write or telephone me at this address:*

Mr. T. F. Sohl, Group Personnel Manager,



**SHIPTON AUTOMATION LTD**

**Shipton Group House, Oval Road,  
London, NW1 7DD.  
Tel: 01-485 4100. Ext. 331.**



### BRITISH RELAY

#### TELEVISION and RADIO DISTRIBUTION SYSTEMS

We are expanding our activities in the field of wired installations in hotels, both at home and overseas. For this,

### WE REQUIRE ENGINEERS

with the necessary specialist knowledge and experience, for duties which include:—

- SYSTEM PLANNING
- SCHEDULING and ESTIMATING
- INSTALLATION CONTROL
- COMMISSIONING

If you have experience which is relative to any aspects of this type of work, and would like information on staff vacancies, please apply to the address below.

*All enquiries will be treated in strict confidence.*

**THE GENERAL MANAGER,  
SPECIAL SERVICES DIVISION,  
British Relay House · 41 Streatham High Road ·  
London, S.W.16.  
Tel: 01-677 9681**

# There's a big future in EVR

We're building up the EVR production unit at Basildon. Currently we need:

## **SHIFT CONTROL ENGINEERS**

to operate video tape and sound transfer facilities. You should have had experience of equipment and staff control in television engineering, of video tape recording, telecine operation, telerecording and film characteristics. A good knowledge of optical and magnetic sound transfer and vision and sound mixing is also desirable.

## **VTR ENGINEERS**

with good working knowledge of 2" quadruplex video tape recorder operations and maintenance. An experience of 1" machines would also be useful. Telecine experience an added advantage.

## **ENGINEERS & OPERATORS for the Electron Beam Recorder**

to work on the only Electronic Beam Recorder in this country. Either VTR or Audio Engineers are invited to apply, or operators with electronic background used to working with complex equipment. Training will be given.

## **AUDIO ENGINEERS**

with experience in operating audio equipment to high quality reproduction standards.

Salary levels are attractive, and will depend on experience. All applicants must be prepared to work shifts. We'll help with removal expenses and we can help you to get rented accommodation in Basildon.

Please write or telephone for an application form, to: F. A. Harvey, The EVR Processing Station, Christopher Martin Road, Basildon, Essex. Telephone: Basildon 22800.



**EVR Partnership**

## The Government of ZAMBIA requires

# RADIO SPECIALIST

(Police Department)

# RADIO ENGINEERS

(Civil Aviation)

### Salary up to £2,590

- ★ Contract of 36 months    ★ Low Taxation
- ★ Subsidised Housing    ★ Education Allowances    ★ 25% Tax-free Gratuity
- ★ Appointment Grant of up to £200 payable in certain circumstances
- ★ Salary £2,310 to £2,590 according to experience

Duties will involve the maintenance and installation of police radio equipment throughout Zambia, travelling by road and air.

The equipment includes modern low and medium power H.F. equipment, S.S.B. equipment and V.H.F. equipment including multiplex links. Knowledge of maintenance of teleprinters, diesel and petrol generators preferred. Candidates, who will serve in the rank of Inspector of Police (non-uniformed), must have completed a five year apprenticeship or hold a service trade certificate or equivalent qualification and have at least six years post-qualification experience.

**Radio Specialist. Ref. M2Z/61274/WF**

Duties will involve the maintenance, overhaul and installation of ground terminal radio communication equipment and navigational aid at Airports and Flight Information Centres.

The equipment includes radar systems, H.F. and V.H.F. transmitters and receivers, I.L.S. and D.F. systems and tape recorders. Candidates, who should be under 55 years of age, should have practical experience and a knowledge of theoretical principles within this field.

In addition they should have attained one of the following—

- (i) completion of a 5 year apprenticeship
- (ii) a service trade certificate
- (iii) an I.C.A.O. certificate

or (iv) equivalent.

**Radio Engineers. Ref. M2Z/690315/WF**

Apply to **CROWN AGENTS, 'M' Division, 4 Millbank, London, S.W.1** for application form and further particulars stating name, age, brief details of qualifications and experience and quoting relevant reference number.

## WORK AS A RADIO TECHNICIAN ATTACHED TO SCOTLAND YARD

You'd be based at one of the Metropolitan Police Wireless Stations. Your job would be to maintain the portable VHF 2-way radios, tape recorders, radio transmitters and other electronic equipment which the Metropolitan Police must use to do their work efficiently.

We require a technical qualification such as the City & Guilds Intermediate (telecommunications) or equivalent.

Salary scale: £1,161 (age 21) rising by increases to £1,590 plus a London Weighting Allowance. Promotion to Telecommunications Technical Officer will bring you more.

For full details of this worthwhile and unusual job, write to:

**METROPOLITAN POLICE**  
**Room 733 (RT/WW), New Scotland Yard**  
**Broadway, London, SW1**  
 or telephone 01-230 1212 extension 2605

1046

## UNIVERSITY OF DURHAM

### DEPARTMENT OF APPLIED PHYSICS AND ELECTRONICS

### SENIOR DEMONSTRATOR/ EXPERIMENTAL OFFICER IN ELECTRONICS

Applications are invited for the post of Senior Demonstrator or Experimental Officer in Electronics. Applicants should have an interest in a wide variety of electronic circuits using modern semiconductor devices. They should have a degree or equivalent qualification, or relevant experience.

The person appointed will assist in the development of circuits for both electronics teaching and research and will, if appointed as a Senior Demonstrator, undertake laboratory supervision and some lecturing.

Salary on the scale £1,200 × £100—£1,900 (Senior Demonstrator), or £1,145 × £55—£1,310 × £65—£1,505 (Experimental Officer) with possibility of promotion to £1,540 × £80—£2,260 (Senior Experimental Officer). All scales under review.

Applications, stating names and addresses of three referees, by 22 February, to the Registrar and Secretary, Old Shire Hall, Durham, from whom further particulars may be obtained.

1060

# SALES ENGINEER

with exciting prospects

We are a fast-expanding electronics company with a turnover rising at 100% per year. Our specialised instruments have already won us a world reputation for performance and quality. New products and developing markets offer the man who joins us the chance to make a big contribution and see his rewards grow as we grow.

The right man for the job, which is based in the West, will ideally be under 30, preferably a physics graduate, ambitious and full of drive. Previous sales experience is not essential, as training facilities are available. Salary will start in the range £1,500 to £2,000, plus a company car and the opportunity for overseas travel. But to a young sales engineer with real potential, that's only the beginning.

first choice  
in signal  
recovery

## Brookdeal

Contact: **John Roberts, Sales Manager,**  
**Brookdeal Electronics Limited,**  
**Market Street, Bracknell, Berkshire.**  
Tel: Brackell 23931 (Day). Wargrave 2885 (Evenings)

## STAVELEY-SMITH CONTROLS LIMITED SERVICE DIVISION

68 GROSVENOR STREET, MANCHESTER M1 7EW

### VACANCIES FOR SERVICE ENGINEERS

**Marine Radio, Radar, Gyro-Compass & Engine Room Electronics**  
Applicants must have had experience in service of this equipment and ability to fault find and repair. Good basic theoretical knowledge essential and keen interest in the Marine World.

Required for London, Newcastle, Belfast, Hull, Glasgow, Swansea.

### Marine and Industrial Electrical and Automated Equipment

Applicants must have had experience in sophisticated automation and controls of the heavier type of electrical equipment, such as Ships Remote Bridge Controls of main engines, Protective Devices and Alarms, Data Loggers etc.

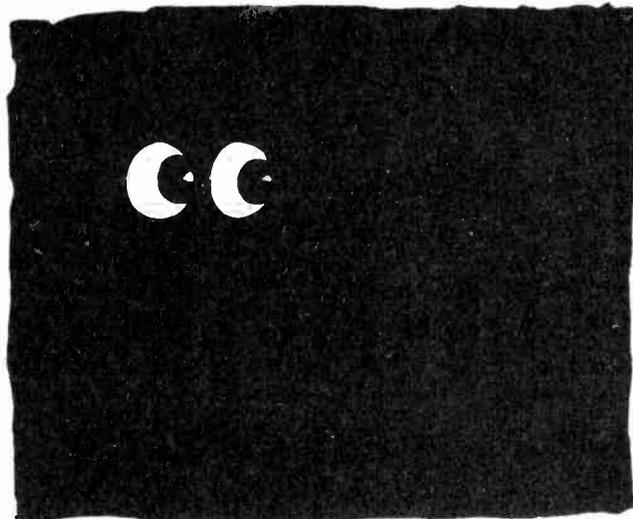
In Industry, Electronics and Automated Controls of heavier machines such as Machine Tools, Printing Equipment, Food Processing Machinery, Electric Fork Lift Trucks etc., require to be serviced and repaired. Required for London, Glasgow, Newcastle, Manchester.

### Electrical Instrument Mechanics

Applicants must have had experience in the rebuilding and repairing of all kinds of fine Instruments, recalibrations, scale writing etc. Work involved is very wide indeed. Multi range Instruments, Chart Recorders, Bridges and Switchboard Instruments. Required for London (City), and Manchester (Central). Applications in writing, giving full personal and technical background details, to The Manager, address as above.

1054

# Light engineering/ electronics and in the dark about computers?



Join us now as a Computer Service Engineer, and after six months' paid specialist training, you will be responsible for ensuring that our computers are in peak condition.

We are Britain's leading computer manufacturer; we give men who want a rewarding career an excellent basic salary while we train them in every aspect of customer engineering in the computer industry. You'll learn to deal with operational problems, and to use the most intricate machinery.

HNC or C&G in electronics engineering, a Forces' training in electronics, or similar qualifications, are your passport to our opportunities.

How far you progress is up to you—the experience you get will stand you in good stead for your future career development. You'll gain knowledge of new methods and techniques on the most sophisticated equipment.

To add to your basic salary, you can get generous overtime and shift rates. There is a special allowance for working in central London. You will be operating in a computer environment on customers' premises in conditions well above the average for industry.

Age: 21/35.

Locations: Reading, Bracknell, Middlesex, Hertfordshire, Surrey, Central London, Manchester, Kids Grove and Dublin.

Write giving brief details of your career, and quoting ref. WW668e to: A. E. Turner, International Computers Limited, 85/91 Upper Richmond Road, Putney, London SW15.

International Computers

ICL

# Straight talking electronics engineers

Listen to us for a few well-paid months, then with computer expertise added to your thorough understanding of general electronics, you'll be a well qualified Service Engineer Instructor.

We're looking for that rare ability to make others see exactly what you're getting at. We want people who know their stuff inside out—who can pass on practical information that trainees would otherwise take years of experience to acquire.

It will be your responsibility to make sure that when your pupils leave the Training Centre as computer service engineers, they're (almost) as good at their jobs as you are now at yours!

Some travelling will be involved in the UK, and possibly overseas, and during this time a salary premium is paid in addition to all normal expenses.

Most of you will be based at Letchworth in the pleasant Hertfordshire countryside, and only an hour's drive from London. Relocation expenses will be considered.

Please write, quoting ref WW665C to A. E. Turner, International Computers Limited, 85/91 Upper Richmond Road, Putney, London, SW15.

**International Computers**

**ICL**

Expanding firm of electronic equipment stockists and importers, seek a highly experienced man

## TO TAKE CHARGE AND DEVELOP NEW DEPARTMENT OF PASSIVE COMPONENTS

Excellent technical and commercial knowledge of capacitors and resistors necessary. The successful candidate will be expected to work on his own initiative and reward will be proportionate to results. Salary and commission by arrangement.

Please write to: **Z & I Aero Services Ltd.,  
44 Westbourne Grove,  
Bayswater, London, W.2**

giving short details of experience, position and present salary.

1069

## RADIO OPERATORS

There will be a number of vacancies in the Composite Signals Organisation for experienced Radio Operators in 1971 and subsequent years.

Specialist training courses lasting approximately 8 months are held at intervals. Applications are now invited for the course starting in September 1971.

### Salary Scales

During training with free accommodation provided at the Training School:

Age 21	£848 per annum
.. 22	£906 ..
.. 23	£943 ..
.. 24	£981 ..
.. 25 or over	£1,023 ..

On successful completion of course:

Age 21	£1,073 per annum
.. 22	£1,140 ..
.. 23	£1,207 ..
.. 24	£1,274 ..
.. 25 (highest age point)	£1,351 ..

then by 6 annual increments to a maximum of £1,835 per annum.

Excellent conditions and good prospects of promotion. Opportunities for service abroad.

Applicants must be United Kingdom residents, normally under 35 years of age at start of training course, and must have at least 2 years operating experience or PMG qualifications. Preference given to those who also have GCE 'O' level or similar qualification. Exceptionally well qualified candidates aged from 36-40 may also be considered.

Interviews will be arranged throughout 1971.

Application forms and further particulars from:

**Recruitment Officer, Government  
Communications Headquarters, Oakley,  
Priors Road, CHELTENHAM, Glos.,  
GL52 5AJ. Tel: Cheltenham 21491 Ext 2270**

92

## ST. OSYTH TRAINING COLLEGE CLACTON-ON-SEA

### QUALIFIED VISUAL AIDS TECHNICIAN

required as soon as possible with responsibility for care of audio-visual aids, C.C.T.V., photocopying and photographic equipment.

Salary: Technical grade 4 £1,272 — £1,515 according to qualifications and experience.

Further details and forms of application may be obtained from the Principal, to whom applications should be returned within 14 days of this advertisement.

1059

## ADM BUSINESS SYSTEMS LTD.

require

### SERVICE ENGINEERS

to cover their range of desk top electronic calculators. Applicants should have a sound knowledge of electronics or some previous experience of the repair of desk top calculators. Salary according to age and experience.

Applications giving full details of qualifications and experience to: R. Wardlaw, ADM Services Ltd., 64-66 King Street, Hammer-smith, London, W.6.

Telephone: 01-748 0211

1068

If you're a telecommunications man and match up to the qualifications below cut yourself into a slice of Britain's future



Become a

# Radio Technician

in the fast-growing world of Air Traffic Control

Please send me an application form and details of how I can join the fascinating world of Air Traffic Control Telecommunications.

Name .....

Address .....

Not applicable to residents outside the United Kingdom wwwt/£4

To: A J Edwards, C Eng, MIEE,  
The Adelphi, Room 705, John Adam Street, London WC2N 6BQ,  
marking your envelope 'Recruitment'

**Sending this coupon could be your first step to a job that's growing in importance every year.**

The National Air Traffic Control Service needs Radio Technicians to install and maintain the vital electronic aids that help control Britain's ever-increasing air traffic.

This is the kind of work that requires not only highly specialised technical skills but also a well developed sense of responsibility and candidates must be prepared to undergo a rigorous selection process. Those who succeed are assured a steadily developing career of unusual interest and challenge. Starting salary varies from £1044 (at 19) to £1373 (at 25 or over) : scale maximum £1590 (higher rates at Heathrow). There is a good annual leave allowance and a non-contributory pension for established staff.

You must be 19 or over, with at least one year's practical experience in telecommunications, ('ONC' or 'C and G' qualifications preferred).

## NATCS

National Air Traffic Control Service

# Radiomobile

BRITAIN'S CAR RADIO SPECIALISTS

Radiomobile is the Car Radio Division of Smiths Industries Limited, and holds the dominant position in the 'IN-Car Entertainment' market. The very rapid growth of this market has created requirements for many more Engineers at all levels. We are re-locating our Design Centre into modern premises at Hemel Hempstead, and the following appointments must be filled.

## ELECTRONIC DEVELOPMENT ENGINEERS

HEMEL HEMPSTEAD—HERTS

There are excellent career opportunities for Electronic Development Engineers at our new Design Centre. The ideal candidates will have a wide experience in the design of high quality AM and AM/FM radio receivers, possess the relevant Electronic Engineering qualifications and preferably be between 25 and 45. This is interesting work and the Engineer will be expected to be responsible for his design project right up to the manufacturing stage.

## SENIOR DRAUGHTSMEN

HEMEL HEMPSTEAD—HERTS

The Senior Draughtsmen will back up the work of our Development Engineers. Previous experience in the Electromechanical and Printed Circuit Board field is required. He should be qualified on O.N.C. (Mechanical) standard.

## ELECTRONIC TECHNICIANS

CRICKLEWOOD—LONDON

There are also excellent career opportunities for Electronic Technicians at our Cricklewood Factory. The work is concerned with development of our current radio products and Evaluation Engineering. Experience with radio receivers, tape playing equipment or electronic components would be an asset. The candidate should be qualified to O.N.C. (Electronics) standard. We would also like to hear from candidates studying for this qualification. Day release may be granted. Age preferably 21-40.

*These are monthly staff appointments and carry usual fringe benefits associated with a major company; including 18 days holiday this year.*

*All appointments carry attractive starting salaries which are reviewed annually.*

*Please write in confidence, telling us how you meet these requirements, giving details of your present position, experience, qualifications, age and salary to our Personnel Manager at the address below, or, if you prefer, write or telephone for an Application Form.*

**Miss I. S. Thom, Personnel Manager,  
Radiomobile Limited,**

**Goodwood Works, North Circular Road,  
London, N.W.2. 01-452 0171 EXT. 4340.**

# Airline Radio Technicians

BOAC require fully trained and highly skilled radio technicians to work on their modern jet aircraft for the repair and overhaul of radio/radar equipment at London Airport—Heathrow. A high standard of theoretical knowledge is essential and at least five years' experience in radio maintenance. An approved apprenticeship is desirable.

Pay is £28 15s. per week rising after three months satisfactory service to £30 6s. plus shift premium. Other benefits include an excellent pension scheme sports and social club and opportunities for holiday air travel.

Please write now with details stating training experience, and qualifications quoting reference WW/406 in your letter, to:

**Manager Selection Services, BOAC, PO Box 10, Hounslow, Middlesex.** or dial 01-759 5511, extension 3652, and ask for an application form.

1048



## WANTED

an enterprising and experienced

### ELECTRONIC TEST ENGINEER

to fit into a responsible position in our QUALITY CONTROL team and whose job it would be to:

- (a) Diagnose and clear faults on HI-FI and Audio equipment;
- (b) work from experience gained to optimise production techniques.

The successful applicant will work in the quality control department of a fast expanding company and must be of O.N.C. or equivalent standard.

Apply by letter or phone:

**Mr. Richard Monk**

**SINCLAIR RADIONICS LTD.**

**London Road, St. Ives, Huntingdonshire  
St. Ives 4311**

1049

*Based at Southampton, a pleasant part of Southern England, within easy reach of the Solent, New Forest and London.*

**RADIO  
TECHNICIAN  
(Conversion)**

**£1,461-£1,725 p.a.**

**SOUTHERNGAS**



This is a new position required in connection with Conversion activities where it is necessary constantly to re-survey sectors ahead of the Conversion Teams and Align V.H.F. and U.H.F. equipment. Negotiating site facilities and installing the equipment.

Applicants should have City and Guilds Final Certificate in an appropriate subject. They should have had formal training with a Telecommunications manufacturer or major user and subsequent operational planning experience totalling at least five years.

Salary within range shown according to ability and experience and qualifications.

Assistance with the cost of removal will be given. Application forms may be obtained quoting reference number P.575/4, from the Senior Personnel Officer, Southern Gas Board, 164 Above Bar, Southampton SO1 0DU, to whom they should be returned by 18th March, 1971.

An International Leader in the manufacture of professional sound mixing consoles for Broadcasting, T.V., and music recording studios, seek a

## SENIOR TEST ENGINEER

Must accept responsibility for projects during the test and studio commissioning stages and should be experienced in customer relations. Applicants must be of good personality and presentation, with the necessary expertise to carry out assignments competently.

A generous salary is offered in accordance with age, qualifications and experience. Assistance housing may be arranged.

**Apply to: Personnel Manager, Neve Electronic Laboratories Ltd., Melbourn, Nr. Royston, Herts. 1058**

## AUDIO TESTERS/ TROUBLE SHOOTERS

Required for interesting position in electro-musical equipment. Audio amplifiers of up to 100 watts. Echo Units (Copicat) S/S and valve, etc. Please phone in first place. WEM Ltd., 66 Offley Road, London, S.W.9. 735-6568. 937

## ENGINEERS

Have you considered a career in Technical Authorship? If you have sound experience in electronics, radar or computers and ability to write clear concise English, then we have vacancies as Technical Authors in the Home Counties and Midlands. Salaries range from £1,500 upwards with prospects of higher rewards. Box No. WW995.

## SITUATIONS VACANT

**A FULL-TIME** technical experienced salesman required for retail sales; write giving details of age, previous experience, salary required to—The Manager, Henry's Radio, Ltd., 303 Edgware Rd., London, W.2. [67]

**ARE YOU INTERESTED IN HI FI?** If so, and you have some experience of selling in the Retail Radio Trade, an excellent opportunity awaits you at Telesonic Ltd., 92 Tottenham Court Road, London, W.1. Tel. 01-387 7467/8. [21]

**DRAUGHTSMEN.** Mechanical and Electrical required by expanding electronics company specialising in lighting control and audio visual products. This position is salaried and gives ample opportunity for advancement. Please apply Electrosonics Ltd., 47 Old Woolwich Road, Greenwich, London, S.E.10. Tel. 858 4764. [22]

**HI FI/Tape Recorder Service Engineer** required. Telesonic Ltd. 01-387 7467. [1051]

**JUNIOR TECHNICIAN** (16-20) required by Psychology Department to assist in development, construction and maintenance of electronic equipment for use in teaching and research laboratories. Little routine work; good opportunities to exercise initiative; excellent holidays; day release. Salary within scale £653-£968. Apply, stating age, qualifications, experience (if any) to Administrative Assistant (P.T.), Birkbeck College, Malet Street, London, WC1E 7HX. [1066]

**MEN!** You can earn £50 p.w. Learn Computer Operating. Send for FREE brochure—London Computer Operations Training Centre, C.96, Oxford House, 9-15 Oxford Street, London, W.1. [1070]

**TECHNICIAN** required for Psychology Department Workshop at London School of Economics to work with two others on construction and testing of electronic and related equipment from design to finished article. Appropriate background would be craft apprenticeship or equivalent electronics workshop training and at least 3 years' experience. Knowledge of instrument making valuable. An unusual job giving the enthusiast an opportunity to widen his experience. Five-day week, 5-6 weeks holiday, salary £1,040-£1,408 according to qualifications, etc., plus £125 London allowance. Write or phone: Personnel Dept., L.S.E., Hough-ton Street, London WC2A 2AE, 01-405 7686. [1065]

**VITABOX** Bitone Major wanted. Model CN 343 or 344. Mr. Guy, tel. 021-474 3133. [1063]

## ARTICLES FOR SALE

**BUILD IT** in a DEWBOX quality plastics cabinet. 2 in. X 2 1/2 in. X any length. D.E.W. Ltd. (W), Ringwood Rd., FERNDOWN, Dorset. S.A.E. for leaflet. Write now—Right now. [76]

**COMPUTER BOARDS** with about 10 Silicon Transistors, mainly N.P.N. similar 2N706, 20 Silicon Diodes, Quality Resistors, Capacitors, etc. Some have Trimpots and Zeners. 17p each, 70p for 5. £2.50 for 25. LOGIC I.C.'s from 5p each on boards. MIXED COMPONENTS including Resistors, Capacitors, Diodes, I.C.'s, Transistors, some damaged but well worth 65p per lb or money back. THYRISTORS 2N1595, 50 P.I.V. 1A, 65p for 8 on board. All post paid. S.A.E. for list and all data. PAWSON, 114 South Street, Armdale, W. Lothian, Scotland. 1055

**MUSICAL MIRACLES.** Send S.A.E. for details of Cymbals and Drum Modules, versatile independent bass pedal unit for organs, pianos or solo, musical novelties, waa-waa kits (49/-). Also bargain components list reed switches etc. D.E.W. Ltd., 254 Ringwood Road, Ferndown, Dorset. [95]

**NEW CATALOGUE** No. 18, containing credit vouchers value 10/-, now available. Manufacturers' new and surplus electric and mechanical components, price 4/6, post free. Arthur Sallis Radio Control Ltd., 28 Gardner Street, Brighton, Sussex. [94]

**RELAYS,** contactors, timers. From cooking to co-ax. Foolsap S.A.E. for list please. Watsons, 7a Pier Street, Lee-on-Solent, Hants, PO 13 9LD. [1021]

**SINCLAIR PROJECT 60 OFFERS.** 2 x Z30 amplifiers, stereo 60 pre-amp, PZ5 power supply £18-15-0. Or with PZ6 power supply £20-15-0. 2 x Z50 amplifiers, stereo 60 pre-amp, PZ8 power supply £20-15-0. Transformer for PZ8 £3. Q16 loudspeaker £7-18-0. Project 60 FM tuner £20-15-0. OTHER OFFERS. S-DeCs 19/-, T-DeCs 42/-. Modern miniature meters, 1 1/2 in. square, similar to SEW 38P, 50 or 100 microamps 30/-. Sinclair Micromatic receivers, kit 44/-, assembled 54/-. Batteries 5/6 extra. PNP Silicon transistors 2S300 series, untested but at least 80% are good. 50 for 8/-, 100 for 14/-. Postage 7/6 on project 60 orders, 2/- on others. All goods are brand new. Money back if not satisfied. We regret that we are at present handling only mail order business. Swanley Electronics, Dept. WW4, 32 Goldsel Road, Swanley, Kent, BR8 8EZ. [1052]

**VACUUM pumps,** coating plant, pyrometers, recorders spectrophotometers/ovens, etc. Free catalogue. Barrett, 1 Mayo Road, Croydon, CRO 2QP, Surrey. Phone 01-684-9917. 1056

**VHF 80-180 MHz.** Integrated receiver, tuner, converter Kit. Remarkable results from single semiconductor. Comprehensive kit £4 post paid or send for free literature enclosing s.a.e. Johnsons (Radio) Worcester, WR1 2DT. [99]

**60 kc/s Rugby & 75 kc/s HBG** Neuchatel Radio Receivers. Signal and Audio outputs. Small compact units, £35. Toolex, 6 Warwick Close, Hertford (4856). [98]

*continued on page 111*

## "W.W." HI-FI KITS

★ **LINSLEY HOOD MODULAR PRE-AMP**  
July 1969 no-compromise design for the purist. Compactly built on Lektrokit. Layout details. Kit price from £7.5.0 (mono, mag.p.u.+2 I/P.s).

★ **LINSLEY HOOD SIMPLE PRE-AMP**  
Designer-approved PCB (marked component locations) gives excellent results with ceramic pick-up. Kit includes all parts as in May 1970 article plus front panel. Mono £6.5.0. Stereo £11.8.0 inc. p.p.

★ **BAILEY 30W AMPLIFIER (Nov. '68)**  
Mk. IV PCB has extra pre-set for quiescent current. Output capacitor and PCB mount directly and compactly on specially designed generous heat-sink.

★ **LINSLEY HOOD 15-20W AMPLIFIER**  
July 1970 latest and ultimate design. O/P capacitor, PCB, Tr3, 4 & 5 mount compactly onto heat-sink. Our kit personally tested and approved by the designer. Gain of O/P TR's > 100.

**POWER SUPPLIES** (simple and stab'd) available.

**HIGH QUALITY** components inc'g Mullard, Hunts, TCC capacitors, Plessey moulded pre-sets. O/P Tr's matched ±10% @ I<sub>c</sub>=1 amp.

**AFTER-SALES SERVICE** at reasonable cost.

**REPRINTS** of articles at 6/- per copy post free.

**DETAILED PRICE LISTS** at 1/- (Refundable with order).

**PERSONAL CALLERS WELCOME—BY APPOINTMENT. DESPATCH BY FIRST CLASS RETURN**

## A.1 FACTORS

72 Blake Road, Stapleford,  
Nottingham

Tel. Nottingham 46051 Giro No. 487 6008

(8 a.m.—10 p.m. 7 days/week)

We are a Polish company exporting high stability electronic components which have good mechanical characteristics and long life expectancy.

Valves

Electron Guns

TV Picture Tubes

Sub-assemblies

Tape Recorder Heads

We can offer production capacity and the ability to produce tape recorder heads to meet our customers' own specifications.

# Elektrim

EXPORTER:



Polish Foreign Trade Company for  
Electrical Equipment Ltd.  
Warszawa 1, Czackiego 15/17, Poland.  
Telegrams: ELEKTRIM-WARSZAWA,  
Phone: 26-62-71, Telex: 814351  
P.O. Box: 638

*If you are interested, please send for catalogues and quotations.*

WW—112 FOR FURTHER DETAILS

## Quality Parts for the discerning builder

**BAILEY PRE-AMPLIFIER** still offers lowest distortion level and best overload capability. Edge Connector Mounted Printed Circuit in Fibreglass or Paxolin material to choice. Highest quality parts including gain graded transistors.

**BAILEY 30w POWER AMPLIFIER.** Edge Connector Mounted Printed Circuit in Fibreglass or Paxolin material, size 4 1/2" X 2 1/2". This unit and the above Pre-amplifier can both be used in our new Metalwork Assembly.

**BAILEY 30w POWER SUPPLY.** We have now designed a Printed Circuit Board for the power supply, again intended to be used with our Metalwork, which also has edge connector mounting. Available in Fibreglass material only.

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**DOUBLE SIDED.** These cabinets will take rack panels both sides, that is back and front and are drilled and tapped all the way down every 1/2" for this purpose. They are fitted with "Instant" patent fully adjustable mounts which are vertically and horizontally adjustable—these allow the panels to be recessed when they are fitted with projecting components and it is desired to enclose them by doors.

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**PRICE £26.50 each (Carriage extra)**  
 Full length door £5 each extra

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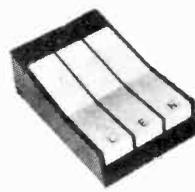
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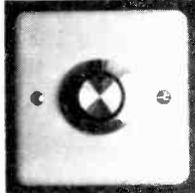
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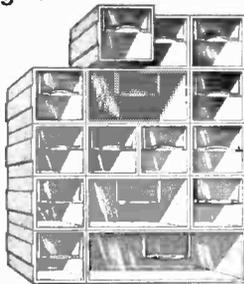
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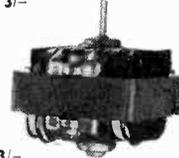


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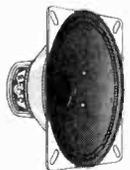
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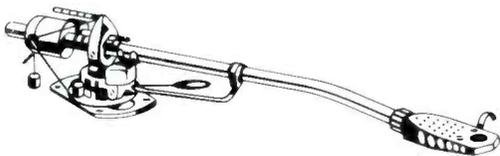
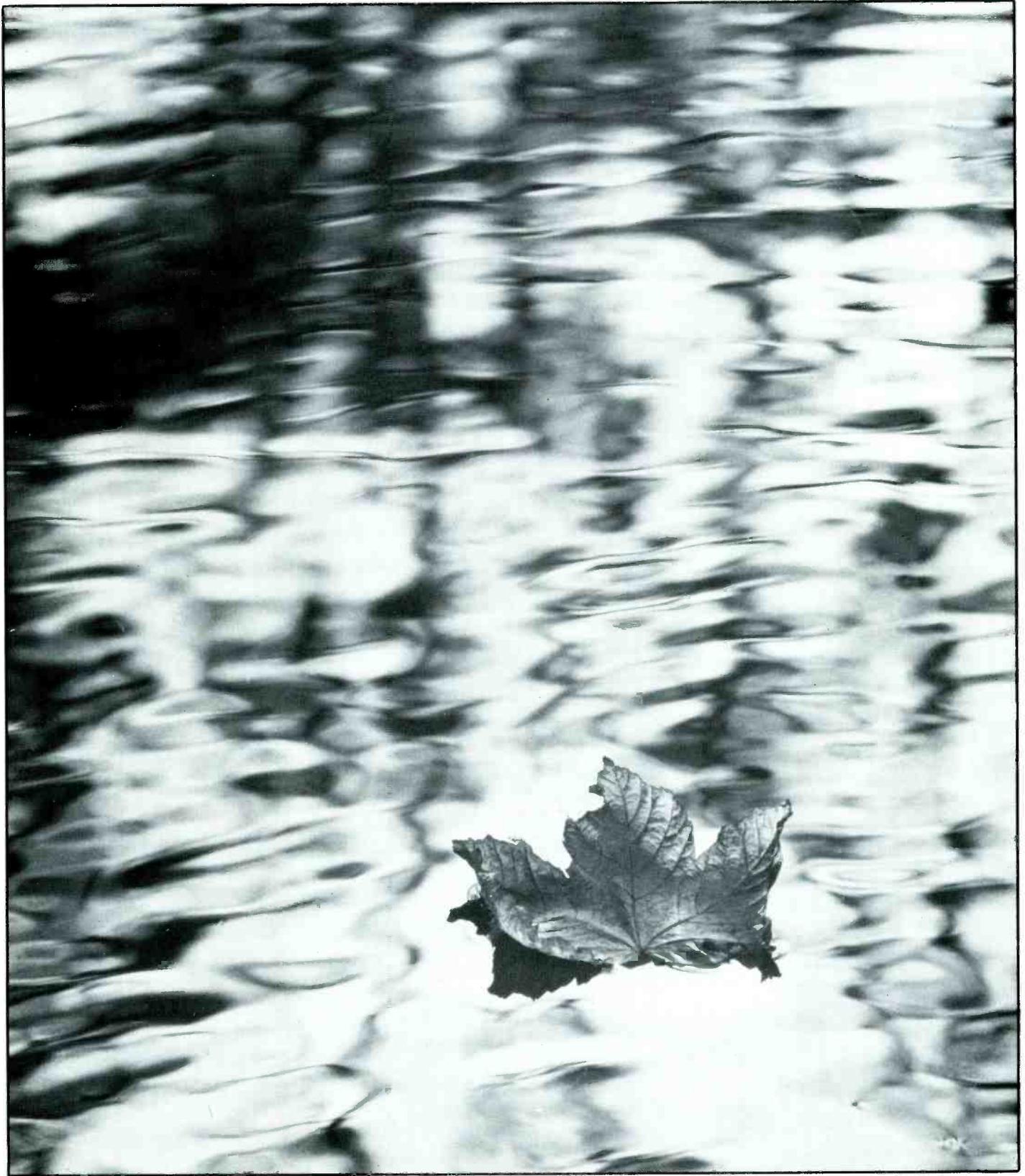
### INDEX TO ADVERTISERS

Appointments Vacant Advertisements appear on pages 100-106

	PAGE		PAGE		PAGE
A1 Factors	107	Garrard (Plessey Consumer Electronics Division)	31	Radford Laboratory Insts. Ltd.	42
Acoustical Mfg. Co., Ltd.	20	Goldring Mfg. Co. Ltd.	14, 35	Radio & TV Components Ltd.	74
Adcola Products, Ltd.	8	Grampian Reproducers Ltd.	110	Radio Components Specialists Ltd.	111
Advance Electronics Ltd.	36, 47			Radio Exchange Co. Ltd.	109
Amplivox Ltd.	61	Harris Electronics (London) Ltd.	55	Radiospares Ltd.	78
Ancom Ltd.	18	Harris, P.	109	Ralfe, P. F.	85
Anders Electronics, Ltd.	22, 34	Hart Electronics	107	Rank, Audio Visual Ltd.	12
Associated Automation Ltd.	4	Hatfield Instruments Ltd.	54	R.S.C. Hi-Fi Centres Ltd.	87
Associated Electronic Engineers Ltd.	8	Heath (Gloucester) Ltd.	19	R.S.T. Valves Ltd.	78
Audix B.B. Ltd.	46	Henrys Radio Ltd.	72, 73	Reslo Mikes	14
Aveley Electric Ltd.	52	Henson, R., Ltd.	109	Rola Celestion Ltd.	44
Avo Ltd.	10				
		I.C.S. Ltd.	82	Samsons (Electronics) Ltd.	84
Bantex Ltd.	22	I.M.O. (Electronics) Ltd.	35	Sankyo Seiki Mfg. Co.	12
Barr & Stroud Ltd.	53	Industrial Insts. Ltd.	10	S.D.S.A. (Int. Exhibition)	64
Batey, W., & Co.	32	Instructional Handbook Supplies	110	Scientific & Technical Services	108
Bentley Acoustical Corporation Ltd.	88	Integrex Ltd.	110	S.E. Laboratories (Eng.) Ltd.	62
Bentley, K. J.	110	Ivorvet Ltd.	111	Service Trading Co.	98, 99
B.I.E.T.	13			Shure Electronics Ltd.	60
Bi-Pak Semiconductors	69	J.E.F. Electronics	108	Sinclair Radionics Ltd.	66, 67, 68
Bi-Pre-Pak Ltd.	83			S.M.E. Ltd.	Cover iii
Black, J.	108	Keytronics	88	Smith, G. W. (Radio), Ltd.	75, 76, 77
Bourns (Trimpot) Ltd.	27	K.S.M. Electronics Ltd.	65	S.N.S. Communications Ltd.	50
Bradley, G. & E., Ltd.	37, 39			Smith, J., Ltd.	50
Brenell Eng. Co. Ltd.	52	Lasky's Radio Ltd.	70, 82	Sonex '71	65
Britec Ltd.	54	Lawson Tubes	110	Starman Tapes	110
Brooklands Plating Co. Ltd.	108	Leda Tapes	108	Stephens Electronics	91
Business Conferences & Exhibitions Ltd.	98	Ledon Instruments Ltd.	30	Sugden, A. R., & G. (Eng.) Ltd.	28
		Level Electronics Ltd.	15	Sugden, J. E., Ltd.	55
Carston Electronics Ltd.	28	Lexor Dis-boards Ltd.	78	Sutton Electronics Ltd.	108
Cesar Products Ltd. (Yukan)	108	Light Soldering Developments Ltd.	18		
Chiltmead Ltd.	89, 110, 112	Limrose Electronics	30	Taylor Electrical Instruments Ltd.	1
Colomor (Electronics) Ltd.	95	Linear Products Ltd.	28	Tektronix U.K. Ltd.	6, 43
Communication Accessories & Equipment Ltd.	22	Linstead Electronics	42	Telcon Metals Ltd.	27
Computer Sales & Service Ltd.	70	Lionmount & Co. Ltd.	55	Teleguipment Ltd.	56
Concorde Instrument Co.	108	Livingston Hire Ltd.	98	Teleradio, The Co. (Edmonton), Ltd.	110
		London Central Radio Stores	110	Telford Products Ltd.	24
D.E.W. Ltd.	108	L.S.T. Components Ltd.	94	Teonex Ltd.	29
Dabar Electronic Prods.	70	Lyons Instruments	50	Thorn Radio Valves & Tubes Ltd.	57
Deimos Ltd.	108			Tinsley, H., & Co. Ltd.	24
Diathane Ltd.	110	Marconi Instruments	45	Transradio Ltd.	23
Diotran Ltd.	64, 108	Marshall, A., & Sons (London) Ltd.	84, 90	Trio Corporation Ltd.	26
Douglas Electronic Industries Ltd.	109	McKnight Crystal Co.	108	Turner, Ernest, Electrical	30
Drake Transformers Ltd.	33	McMurdo Instrument Co. Ltd.	40		
		Mills, W.	92, 93	Ultra Electronics (Components) Ltd.	54
Eagle International Ltd.	16, 17	Milward, G. F.	96	Ultron	2
Edwards Scientific Insts. Ltd.	55	Modern Book Co.	107	United-Carr Supplies Ltd.	38
Electronic Brokers	80, 81, 110	Mullard Ltd.	49		
Electronics (Croydon) Ltd.	71	Multicore Solders Ltd.	Cover iv		
Electrosil Ltd.	63			Valradio Ltd.	18
Electro-Tech Sales	86	Nombrex Ltd.	55	Vitavox Ltd.	98
Electrovalue	79			Volfield Ltd.	23
Elektrim	107	Olympic Transformers Ltd.	32	Vortexion Ltd.	25
E.M.I. Electronics Ltd.	41	Osmabet Ltd.	109		
E.M.I. Tape Ltd.	48	Oxley Developments Co. Ltd.	44		
English Electric Valve Co. Ltd.	3, 5, 7, 9			Watts, Cecil E., Ltd.	108
Erie Electronics Ltd.	11, 21	Patrick & Kinnie	92	Wayne Kerr, The, Co. Ltd.	Cover ii
		P.C. Radio Ltd.	95	Webber, R. A., Ltd.	30
Farnell Instruments Ltd.	52	Pembridge College, The	65	Wel Components Ltd.	54
Ferroglyph, The, Co. Ltd.	59	Powertran Electronics	88	West Hyde Developments Ltd.	109
Firnor-Misilon Ltd.	44			West London Direct Supplies	78
Foulsham, W., & Co. Ltd.	111	Quality Electronics Ltd.	54	Wilkinson, L. (Croydon), Ltd.	84
Futuristic Aids Ltd.	53	Quarndon Electronics Ltd.	51		
Fyde Electronic Labs.	32	Quartz Crystal Co. Ltd.	110	Z. & I. Aero Services Ltd.	97

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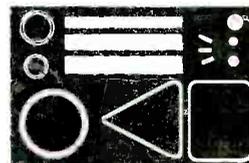
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