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37 Into the 'eighties

38 RADIO AND ELECTRONICS INTO THE 'EIGHTIES

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H.f. radio communication by R. F. E. Winn
Electronic measuring instruments by John L. Minck

61 News of the month
More v.h.f. broadcasting
Engineers want registration
Japanese make Prestel terminals

64 World of amateur radio

67 Practical parallel-tracking pickup arm — 2
by R. Cooper

73 Circuit ideas
Simple waveform generator
Amplitude modulator
Long duration timer

77 Letters to the editor
Sidebands as phasors
Digital filters
The Poynting vector

81 More on the scientific computer
by J. H. Adams

87 S.s.b. and f.m. tranceiver — 4
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<thead>
<tr>
<th>Model</th>
<th>Frequency</th>
<th>Accuracy</th>
<th>Sine Output</th>
<th>Distortion</th>
<th>Square Output</th>
<th>Sync Output</th>
<th>Sync Input</th>
<th>Meter Scales</th>
<th>Size &amp; Weight</th>
<th>Price</th>
</tr>
</thead>
<tbody>
<tr>
<td>TG200</td>
<td>1Hz to 1MHz in 12 ranges</td>
<td>±1.5% ±0.01Hz up to 100kHz</td>
<td>7V r.m.s. down to &lt;200µV with Rs = 6000</td>
<td>&lt;0.05% from 50Hz to 15kHz, &lt;0.1% from 10Hz to 50kHz, &lt;0.2% from 5Hz to 150kHz, &lt;1% at 1Hz and 1MHz</td>
<td>TG200D, DM &amp; DMP only, 7V peak down to &lt;200µV, rise time &lt;150nS, &lt;1V r.m.s. sine in phase with output, ±1% freq. lock range per volt r.m.s.</td>
<td>TG200M, DM &amp; DMP only, 0/2V, 0/7V &amp; 0/2V</td>
<td>TG200D, DM &amp; DMP only, 7V peak down to &lt;200µV</td>
<td>260 x 130 x 180mm, 4.3kg with batteries</td>
<td>£92</td>
<td></td>
</tr>
<tr>
<td>TG200D</td>
<td>3Hz to 300kHz in 5 decade ranges, increasing to ±3% at 300kHz</td>
<td>±2% ±0.1Hz to 100kHz</td>
<td>2.5V r.m.s. down to &lt;200µV</td>
<td>&lt;0.2% from 50Hz to 60kHz, &lt;1% from 10Hz to 200kHz, 2.5V peak down to &lt;200µV</td>
<td>2.5V r.m.s. sine, 2.5V r.m.s. sine, 0/2.5V &amp; -10/+10dB on TG152DM</td>
<td>TG152DM</td>
<td>TG152DM</td>
<td>260 x 130 x 180mm, 3.4kg with batteries</td>
<td>£99</td>
<td></td>
</tr>
<tr>
<td>TG200M</td>
<td>0.2Hz to 122MHz on four decade controls</td>
<td>±0.02Hz below 6Hz, ±0.3% from 6Hz to 100kHz, ±1% from 100kHz to 300kHz, ±3% above 300kHz</td>
<td>5V r.m.s. down to 30µV with Rs = 6000</td>
<td>&lt;0.15% from 15Hz to 15kHz, &lt;0.5% at 1.5Hz and 150kHz</td>
<td>2 Expanded voltage and -2/4dBm</td>
<td>260 x 180 x 180mm, 5.4kg</td>
<td>TG66B</td>
<td>Battery model £245</td>
<td></td>
<td></td>
</tr>
<tr>
<td>TG200DM</td>
<td>0.2Hz to 122MHz on four decade controls</td>
<td>±0.02Hz below 6Hz, ±0.3% from 6Hz to 100kHz, ±1% from 100kHz to 300kHz, ±3% above 300kHz</td>
<td>5V r.m.s. down to 30µV with Rs = 6000</td>
<td>&lt;0.15% from 15Hz to 15kHz, &lt;0.5% at 1.5Hz and 150kHz</td>
<td>2 Expanded voltage and -2/4dBm</td>
<td>260 x 180 x 180mm, 5.4kg</td>
<td>TG66A</td>
<td>Mains &amp; battery model £260</td>
<td></td>
<td></td>
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</tbody>
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<table>
<thead>
<tr>
<th>INPUT</th>
<th>OUTPUT</th>
</tr>
</thead>
<tbody>
<tr>
<td>100-125 volts or 200-250 volts</td>
<td>115 volts or 230 volts</td>
</tr>
<tr>
<td>FREQUENCY</td>
<td>FREQUENCY</td>
</tr>
<tr>
<td>45-65Hz</td>
<td>50Hz or 60Hz</td>
</tr>
<tr>
<td>STABILITY</td>
<td>VOLTAGE</td>
</tr>
<tr>
<td>Voltage</td>
<td>Frequency</td>
</tr>
<tr>
<td>±1% No load to full load</td>
<td>±0.01% No load to full load</td>
</tr>
<tr>
<td>POWER</td>
<td>DISTORTION</td>
</tr>
<tr>
<td>500VA or 250VA</td>
<td>2%</td>
</tr>
<tr>
<td>COOLING</td>
<td>DUTY</td>
</tr>
<tr>
<td>Fan Cooled</td>
<td>Continuous</td>
</tr>
<tr>
<td>DIMENSIONS</td>
<td>WEIGHT</td>
</tr>
<tr>
<td>432 x 162 x 508mm (17&quot; x 6&quot; x 20&quot;)</td>
<td>45 or 30Kg unpacked</td>
</tr>
<tr>
<td>CONSTRUCTION</td>
<td>TERMINATION</td>
</tr>
<tr>
<td>Cabinet or rack mounting</td>
<td>Cannon Connectors at rear of case</td>
</tr>
<tr>
<td>NATO CODIFIED</td>
<td>24V DC Inverter</td>
</tr>
<tr>
<td>24V DC Inverter</td>
<td></td>
</tr>
</tbody>
</table>

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<tr>
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<th>OUTPUT CONFIGURATIONS</th>
<th>PRICE*</th>
</tr>
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<tr>
<td>ICM7211IPL</td>
<td>HEXADECIMAL MULTIPLEXED 4-BIT</td>
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<td>ICM7211APIPL</td>
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<td>ICM7211MPIPL</td>
<td>HEXADECIMAL CODE B INTERF</td>
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<td>ICM7212IPL</td>
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<td>CODE B MICROPROCESSOR INTERFACE</td>
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<th>AD24</th>
<th>AD2412</th>
<th>ADV030</th>
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<td>8 amp</td>
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<td>16 amp</td>
<td>5 amp</td>
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<td>12</td>
<td>0 to 30</td>
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<td>PRICES</td>
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<tr>
<td>1 off - AD12/24</td>
<td>£68.50</td>
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<td>1 off - AD2412</td>
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<tr>
<td>4-Octave C-C</td>
<td>£32.20</td>
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<tr>
<td>5-Octave F-F</td>
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<thead>
<tr>
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<th>DESCRIPTION</th>
<th>PRICE</th>
</tr>
</thead>
<tbody>
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<td>LED</td>
<td>4 for 69p</td>
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<td>LED</td>
<td>2 for 48p</td>
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<td>276-034</td>
<td>LED</td>
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</tr>
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<td>276-142</td>
<td>Infra Red Emitter Detector Pair</td>
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<td>277-1003</td>
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<td>276-1373</td>
<td>Power Transistor Mounting Hardware</td>
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<td>276-1363</td>
<td>10 220 Heat Sink</td>
<td>60p</td>
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<tr>
<td>276-1364</td>
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Our front cover this month, introducing the articles "Radio and electronics into the 'eighties", symbolizes man's increasing involvement with his technology. This is a two-way process. The more devices and systems he produces the more he changes his environment and this reflects back on him by modifying his customs, institutions and general way of life. And it may go deeper than this. According to the early sociologist Durkheim, a person's knowledge of himself — his self-image — is created by the society in which he lives. Not only does he exist in society but society exists in him. So in modifying the material basis of society and hence social relations by technology, he continually changes his concept of himself as an individual and all the imagined needs or wants that arise out of this concept. No wonder that modern man in industrialized society seems such a restless, anxious and dissatisfied creature.

This two-way process is very intense when the technology is electronics, for here we are concerned with transmitting and transforming information, and ultimately, if not directly, this information causes human beings to think, feel and act. What seems to emerge from the developments described in the following articles is that the 1980s will see a further intensification of the links between the human being and his electronic systems. The systems will become even more closely matched to the input and output capabilities of the biological organism and will make even greater demands on it. It's not simply a case of more communication channels conveying more information in a given time, but a continuing increase in the refinement and variety of the information put in by and presented to the human beings.

Higher quality sound and visual images, and higher performance in radar systems and laboratory instruments, for example, all demand greater attention and discrimination. In broadcasting the addition of colour and text to television and stereophony to sound have already given us more to perceive and cognize, and electronic tricks in sound and vision synthesis are stretching these abilities to the edge of confusion. In radiocommunication, voice messages are being supplemented by digital data transmission, often on the same circuits, to make possible greater detail and accuracy. And now the general public can retrieve useful facts from data banks over the ordinary telephone lines.

Telecommunications are, of course, essential to organizations — especially large, far-flung organizations like multinational companies, airlines and political/military alliances — to enable them to respond quickly and appropriately to events in any part of their structure. Any message demands a decision, if only to ignore it, but with messages arriving quicker, and in ever greater quantity and detail, the mounting pressure on responsible people to be continually making decisions and deciding priorities is reaching inhuman proportions. Some individuals have found it too much and have left for a quieter life.

On the 50th anniversary of Bell Laboratories, the president, W. O. Baker, said of communications: "I see it also as a mission of importance involving great responsibility. Improving communications, more efficient and satisfying handling of information — these I deeply feel are essential to help solve economic and social problems and aid efforts to civilise the future". These are noble sentiments but it is already evident that we cannot solve such problems by technology alone. As humans we are limited in our powers to assimilate information and in our good will to act on it properly. Perhaps what we really need is less information and more wisdom.
Radio and electronics into the 'eighties

Intelsat V (above) the latest communications satellite, which will be launched at the turn of the year, marks dramatically the entry of radio and electronic technology into the 1980s, for it has double the communications capacity of its predecessor, Intelsat IVA. Equally important advances are being made in terrestrial radio and its related fields, and in the following pages we present articles by seven specialists who first look back at what has happened over the past decade and then project their thoughts and expectations into the 'eighties.

Land mobile radio

by W. M. Pannell, M.I.E.R.E. Pye Telecommunications Ltd

Technical progress in the electronics industry over the past decade has taken vast strides, with the land mobile radio sector certainly not lagging behind. The inevitable questions arise: What effect have all the changes in technique had on the mobile radio industry and its users? Which changes have made the biggest impact? And, what can we expect over the next decade?

Although the changes to the mobile and portable units, the fixed equipments and the peripherals have shown considerable innovation over the past ten years, many of the changes in technique have been brought about by the increasing complexity of overall system requirements.

One change that made a major impact on mobile radio in the UK, over a decade ago, was the decision to split the channel bandwidth at v.h.f. from 25 to 121/2 kHz. This resulted in some immediate relief in the search for extra spectrum and a marked reduction in co-channel interference. The change improved the utilization of channels for many types of user.

During the 1970s we also saw the increasing use of personal portables in all types of system. This is, of course, a logical progression in view of communication being needed between people rather than vehicles in most cases — the main exceptions being where interrogation of vehicle status is desired or where vehicles are the essential tool, for example fire engines.

It was at this point that the move towards miniaturization became an essential requirement in all types of equipment, not so much because of the need for smaller equipments, although in portable design this was naturally a fundamental requirement, but more to enable equipments of increased complexity and versatility to be designed for the more sophisticated systems without increasing the total volume of individual units. So an upsurge in the use of integrated circuits took place: the ubiquitous light bulb was replaced by light emitting diodes: l.e.d. followed by l.c.d. displays became a recognised means of presenting information; while conventional components became steadily smaller to keep up with the new techniques. At the same time, higher stability frequency sources and better i.f. filters became necessary in fixed, mobile and portable equipments as the need for higher performance developed.

Meanwhile, in the systems control field, processors began to take over many of the functions which had previously involved complicated manual operations. More facilities and information became available to the system controller, while, in the mobile, actions...
could, for example, be initiated from control or other designated points without the need for intervention by the mobile user.

Signalling. Signalling over radio gained considerable ground during the 1970s. Previously such requirements as selective calling were often considered to be refinements and were avoided where possible, usually on the grounds of cost and size. Solid-state techniques changed this view and selective calling units employing relays and often mechanical selectors gave way to units of but a fraction of the size and power consumption.

Unfortunately during this period the variations in signalling techniques increased in an alarming way, each manufacturer tending to develop his own form of coding with the result that compatibility became almost impossible. At present there is however a trend to standardise on a few of the better systems, mainly of the sequential tone variety. Even with the reduced number of variants, compatibility is still a problem and further standardisation would be advantageous.

A lot of work has been undertaken in recent years in digital signalling, generally of the order of 1200 bit/s. Various error detecting and correcting codes have and are being investigated to obtain higher coding efficiency and provide a good throughput of data. Such techniques may help in providing data communication at signal levels which in the past have been considered too low for error free data transmission. Digital signalling will undoubtedly be the answer to providing channel assignment switching, sophisticated selective calling, alarms, identity, printer drive, data display and many other uses. However, the low signal threshold achieved with tone signalling has yet to be equalled by any but very low speed digital signalling.

Microprocessors have enabled “intelligence” to be added to systems. The era of manual press-to-talk and the occasional channel change accompanied, where needed, by a selective call operating an electronic ‘door bell’ is now often superseded in the larger systems by intelligent switching functions where channel and routing procedures are performed automatically; hand shaking/identity routines are undertaken with complex control functions being processed, as well as many other technically complex operations. At the moment, microprocessors, although cheap, tend to be greedy in power consumption (n.m.o.s.). This may be improved in the near future by the use of c.m.o.s. and ultimately silicon on sapphire (s.o.s. m.o.s.). Microprocessors in portables where low consumption is critical may thus become practical.

Trunking. Trunking in land mobile systems is a technique which has grown during the past few years with the help of the microprocessor. While the full advantages of such systems in frequency spectrum economy have yet to be seen, undoubtedly first indications are favourable. The use of trunking, however, can raise an operational problem concerning the ownership of the base complex, and this may limit its use to definite types of system where single ownership or the radio common carrier type of operation prevails.

Quasi-synchronization. System techniques evolved during the 1970s included the use of a quasi-sync — a method whereby a number of transmitters carrying the same intelligent radiate simultaneously without interference in a number of overlapping areas. Although as early as 1946 J. R. Brinkley proposed the use of staggered carrier techniques, this method ultimately became unworkable as the channel bandwidth was reduced down to 12 kHz. At these narrow bandwidths much closer staggering, of the order of a few hertz, is required, so that a need arose for high stability, low noise oscillator sources. The technique of quasi-sync is generally applicable to a.m. and f.m. at frequencies up to 500 MHz although at v.h.f. the use of f.m. quasi-sync is subject to some reservations.

Frequency sources. The development of frequency synthesizers for mobile radio also shows signs of increasing in tempo as the need for greater frequency agility grows. Several designs have been announced using various custom built chips. It is just a matter of time before the cost of such devices is comparable with conventional crystals, even for one channel. Meanwhile frequency control has improved considerably by the use of a phase lock loop system and this is often standard on present day fixed receivers in the land mobile bands.

Modulation methods. Overshadowing many of the developments during the past few years has been the obvious rapidly diminishing spectrum space available for each new land mobile radio system. Much has been written on the,

This microprocessor controlled equipment generates and decodes selective calling tones. Providing alert, identification, status, alarm and other operating functions, it is compatible with all known selective calling systems.

Synthesizer board in the Pye M206X two-way radio can be supplied for anything from 16 to 128 channels.
subject and at the recent World Administrative Radio Conference in Geneva much was undoubtedly discussed. Even if, as a result of all the decisions made, extra spectrum is handed to mobile radio, the rate of growth is such that economies must be made. To this end techniques are already being investigated to achieve spectrum savings and further bandwidth splitting by the use of s.s.b. is but one method currently under review. Others include spread spectrum methods, stored speech and the virtual elimination of speech by the total use of data in those applications where standard forms of message predominate. The latter methods are still in the early stages of investigation, but the development of s.s.b. is quite advanced and shows considerable promise.

Cellular systems. Much has also been written on the use of small cell techniques in urban area radio systems. In the United States, where a lot of work has originated, several systems are being put into operation at 900MHz using this principle. Although the cells involved initially in these systems cannot really be described as 'small cell', the possibility of sub-division exists and will undoubtedly be the subject of further investigation. Small cell systems are necessarily oriented towards processor control if all the functions proposed are to be implemented. Cellular systems and trunking have a great deal in common in many design aspects.

Energy sources. In spite of the huge variety of systems which have been devised over the past decade, one common denominator remains — that of the energy source required to drive the equipments. Vehicle units are generally no problem, there being a ready source of d.c. in the vehicle. Portables are a different matter insofar as, although a battery of a suitable type is included in the assembly, this must be either replaced or recharged after a period of work. There has been no outstanding design change during the past ten years which has increased the portable battery capacity appreciably or reduced its size, so this is one aspect where changes are required.

In fixed equipment the tendency has been to use secondary batteries charged from sources of energy ranging from the public power supply through diesel generating sets, wind and water driven generators, thermal generators to solar cells. All methods have their place in providing power to radio equipment. With the present energy crisis, further work is indicated, not only to find means of providing power in relatively inaccessible places but to do so using the minimum resources at present in great demand.

The next ten years

In view of the vast changes which have taken place over the past decade one is tempted to forecast the future almost in terms of science fiction. It is not my intention to examine such possibilities but rather to consider the more down-to-earth developments of existing techniques.

Data will undoubtedly appear as one of the main contenders for optimising usage of the frequency spectrum. While speech will be with us for some considerable time, particularly in the simpler systems, the efforts being made in the data field must be recognised. For example although there is a lack of economically viable vocoders suitable for digital speech at the moment, they will undoubtedly appear. Alternatively, stored speech controlled by a digital bit stream could well be a relatively inexpensive method of spectrum conservation. Speech syntheisers driven directly by computers are also likely. Good speech quality at real time digital speeds of 2 or 3 kbit/s now appears probable in the next decade. Bubble memory techniques permitting occupancy time reduction are, even now, a possibility, with available bubble memories capable of $10^6$ bits/chip, one square centimetre in size, already available.

At present the rate of growth of data by digital methods is in excess of 20% per annum and is expected to maintain or even exceed this during the next ten years. Obviously the use of digital techniques, spread spectrum for example, provides a high degree of privacy and at the same time enables a high degree of large scale integration to be employed — all leading to smaller equipments and, one hopes, greater power economy.

The use of data processing methods to impart "intelligence" to a system is of course one of the most important aspects. Already microprocessors play a major role in the more sophisticated systems, as indeed they are beginning to do in many other areas of present day activity. The future holds an almost unlimited range of possibilities. Dynamic channel allocation, automatic transmitter power level adjustment to suit the propagation conditions and local interference level, automatic call routing, and many others are already in the pipeline, and every day sees a new requirement.

In spite of the digital revolution we must not forget the more conventional forms of mobile communications — forms which will undoubtedly remain in use for a long time, particularly in the simple system and in many of the overseas areas where sophistication is not necessarily needed at present. Here single sideband at frequencies up to at least 500 MHz could well provide all the channels needed until the end of the present century even in areas of international congestion — where, for economic reasons, several countries merge into a single overall area. It should also be emphasised that s.s.b. can also carry the simpler forms of data on equal terms with the more conventional a.m. and f.m. systems.

Portables will tend to become the more normal form of unit, although generally adaptable also for mobile use. Here again the use of data may modify the portable as we see it. For example, display methods may be incorporated to minimize standard speech messages. Key pads to send alpha-numeric messages will be of greater convenience than speech, in many cases, for example, in crowded environments where privacy is required. Similarly key pads will be used for routing the call.

The low efficiency of the portable antenna is another area for further development. However, it could well be that, rather than improving the ranges possible with portables, cell type systems will predominate and most fixed networks will consist of many low power stations closely spaced. Typically, if operation into the telephone is envisaged, the existing telephone call box could be used to locate individual fixed stations, the present physical spacing being close enough to permit very low power to be used. Available power and easy connection into the telephone system favours such an approach.

All these innovations will inevitably increase the complexity of the portable, requiring more compact packaging if only to maintain the same size. Work must be undertaken on battery design if sizes are to remain as at present or preferably reduced in volume, while the extra consumption of the ancillary equipments means that increased battery efficiency is a 'must'.

Two-way mobile data unit for use in a vehicle availability system.
possibly a packet of 'king' size cigarettes is about optimum, although the present day 'credit card' calculator seems to be popular, and this format could well be considered in future personal radio designs. The 'king' size package has already been achieved in many types of pager, but of course the battery requirement here is quite different as there is no heavy transmitter drain.

Methods of charging batteries, whether the batteries are small in size and number, or are the larger types feeding a fixed station, are important aspects requiring further attention. In many parts of the world solar energy is the obvious immediate answer for powers up to a maximum of 500 watts. If efficiency could be improved, many other types of station could benefit, quite often saving expendable fuel.

In suitable areas the wind is already utilized as a source of electrical power and work on optimizing the energy conversion has produced good results. The energy in water movement, whether wave motion, tidal changes or just flow, also offer large scope for investigation.

Without any doubt, the future of mobile radio looks exciting. We must however, keep a firm grip on future developments to ensure that they do not fall into 'nice to have' category, but perform a real service to the world. Improved communication, saving of energy and all the other advantages likely to accompany the microchip era will undoubtedly gain momentum as we move through the years towards the next century. It is up to the engineer to ensure that the steps taken follow an ordered path.

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*Broadcasting*

*by D. P. Leggett B.Sc., F.I.E.E.*

Engineering Information Department, BBC

One of the most striking features of the last decade has been the public appetite for high-quality audio. The 'hi-fi' was becoming a must in any modern household in the early 'seventies and by the end of the decade this had developed into 'quadrophony'. This movement has been led by the gramophone record, and experimental transmissions of quadraphony or surround-sound systems have been made. Although the majority of the radio audience still uses medium and long waves, the congestion and limited quality of reception on these bands has added further impetus to the swing towards v.h.f.

Another reflection of the healthy activity of radio in the last ten years has been the development of local and regional radio services. BBC Local Radio started in the late 'sixties, followed by Independent Local Radio in the early 'seventies. These did not bring new technical problems, but they did increase pressure on available frequency channels; indeed, we have now reached the point where the v.h.f. Band II is badly congested and frequencies have to be shared by programme services which really require channels to themselves.

Turning to television, the main areas of development in the past decade can be categorised as improvements in transmitted quality; extension of programme services; and improved facilities for programme makers. Improvement of picture quality is, of course, a continuing process as each generation of equipment succeeds the last, but one very obvious advance has been the spread of colour into the majority of all programmes with steady development in clarity, fidelity and consistency of colour picture generation and reproduction. Two other examples of technical quality improvement are worthy of mention: the introduction of almost distortion-free digital standard converters has brought significant quality improvements in the international exchange field; and the video noise reducer, a recent digital development, offers considerable benefits for programme material in general.

Programme services have been actively extended in the 'seventies. Notable developments have been the extension of U.H.F. transmitter coverage; the introduction of the electronic news presentation services, Ceefax and Oracle; increasing use of satellites for international exchange; computer-based subtitling services for the deaf and for foreign films; the simultaneous transmission (on radio) of stereo sound with selected television music programmes; and, in the home, the availability of video cassette recorders for catching programmes which would otherwise be missed.

Improved facilities for programme makers should, and do, result in a wider range of better programmes for the viewer. The decade has seen much progress, including improved videotape recorders with sophisticated editing systems; instant replay and slow motion facilities; really portable cameras and video recorders for electronic news gathering; full-facilities outside broadcast cameras requiring only a single coaxial cable; zoom lenses of increased range and aperture; digital timing correctors and synchronisers for automatic signal timing; and digital picture stores for special effects and graphics work.

What, then, is the zeitgeist which has characterised the 'seventies? I suggest it is the realisation that with
transistors, large-scale integration and computer techniques, technical solutions can be devised for most problems. Increasingly, as time goes on, it will be economic, political and social factors which determine the course and pace of development. The questions for the future will more often be “how much do we want and what can we afford?” rather than “is it technically feasible?”

The next ten years
You want ‘100 Best Tunes’ in the kitchen, so you pull out the telescopic aerial in your v.h.f. portable. For good results you need the aerial horizontal and angled for best reception; and in doing so you sweep three cups onto the floor! Then you find Radio 1 is taking its turn on the v.h.f. channel so you switch to medium wave. You find three or four stations transmitting serious music, so you pull out the telescopic aerial and angled for best reception; and in the room you can see the radio gain. You want ‘100 Best Tunes’ in the kitchen. You can hear Alan Keith’s voice, but with an exciting Frenchman in the background plus crackles from your neighbour’s electric drill. So there’s nothing for it but down to the pub again!

This points the way to some main tasks for the ‘eighties. We need more radio channels, signals which can be more easily received, and something to help us find the programme we want.

It is to be expected, following the World Administrative Radio Conference in Geneva, that more broadcasting channels will become available in the v.h.f. Band II. This will enable us to re-engineer the existing v.h.f. transmitting networks to avoid the necessity for sharing between BBC Radio 1 and Radio 2; to reduce the need for displacement of some Radio 3 and Radio 4 programmes by educational material; to place some Radio 3 and Radio 4 programmes in digital form. Although this may become the norm in the long-term future, current investment in conventional analogue systems is such that change to digital methods is not likely to be rapid.

Choosing a programme from the published schedules, selecting the right channel at the right time and tuning the receiver for optimum reception are becoming increasingly difficult for the average listener. Ideas are now developing for radio transmissions to carry coded identification signals inaudible to the listener but detectable by a suitable receiver. Given such codes, a receiver could be pre-programmed at the listener’s choice to search for any desired programme — or type of programmes such as news, light music — and switch on at the appropriate time without the need for any manipulation or control by the listener. Such coded signals could also be used for automatic control of cassette recorders and to carry time information for electronic clocks.

New radio services we can expect in the ‘eighties may include whatever form of surround-sound is finally agreed; and a dedicated channel of motoring information such as the BBC’s Carfax development.

At the programme origination end, digital sound recorders will fairly soon be with us and will offer quality good enough for multi-generation work with little need for the careful alignment and maintenance which analogue recorders demand. Digital sound mixing desks will also appear, together with computer control of complex mixdowns from multitrack recordings which is already a facility in some recording studios and television sound dubbing areas.

Television. Although the solution to many technical problems can be foreseen, there are in television one or two areas where we need to tell our inventors “go away and make a breakthrough!”

The limited sensitivity of colour cameras is a case in point. Existing sensors are already approaching the region where photon noise — arising from the quantum nature of light — becomes the limiting factor. No new sensor, however revolutionary, can cross this fundamental barrier nor can we foresee optical devices of manageable size which would gather in many more of the limited number photons emitted by an ill-lit scene. The apparently much greater sensitivity of the human eye/brain combination is achieved by physical and subjective processes which are not yet understood.

In another area, colour camera sensors and receiver display devices employ rather cumbersome three-colour superimposition techniques with attendant disadvantages in terms of size, complexity and cost. A single colour pick-up device is wanted with outputs directly related to hue and luminance and not needing for optical colour separation filtering: correspondingly a large area, flat display device is needed, responding to hue and luminance signals rather than relying on superimposition of three separate colour images. We must hope that the ‘eighties will see a breakthrough in this area also.

Turning to more foreseeable developments, work will continue through...
Prototype Carfax receiver module.

Teletext hard copy printer.

2Mbit television field store based on c.c.d. devices, as used in digital standards converter and digital noise reducer.

the decade to extend relay station coverage to yet smaller population groups in the UK, with community aerials and local wired distribution systems playing an important part. The fourth television channel will be with us and there may be increasing pressure for local television services. More channels will be needed and the u.h.f. bands may be extended to accommodate this; 405-line services on v.h.f. Bands I and III will be closed down and Band III at least is likely to be re-developed for extended, or new, television networks. Band I is not ideal for television and could be used for mobile services displaced from Band II and perhaps for the start of direct digital radio broadcasts. Television broadcasting via satellites — for direct reception at home or with local distribution from a number of ground stations — is being actively planned for some European countries, but seems less needed in the UK where conventional transmitter coverage is fairly comprehensive.

An alternative source of television programmes is the video cassette recorder. Already well launched in the 'seventies, its use for replay of pre-recorded material will become a significant factor in programme distribution in the 'eighties.

In the studios, programme makers will be looking for increased flexibility and reliability. These qualities are offered by digital techniques, by which signals may be stored, manipulated and passed between areas with little degradation or need for manual intervention. Already we have digital systems for special effects and graphics, standards conversion, noise reduction, source synchronisation, sound distribution, teletext services and numerous routing control functions. We can soon expect to see digital video recorders and editing systems, digital vision mixers and digital camera processing chains. Digital PAL coding will reduce very significantly the cross-colour effect which is perhaps the most obvious shortcoming of present-day colour television. For outside broadcasts we can look forward to compact cameras using highly integrated digital circuitry (and a single colour sensor?) with digital transmission via transportable satellite links into the network control centre.

The islands of digital operation now appearing in the chain will steadily be
merged during the 'eighties. Once a signal has been converted to digital form there are many good reasons for keeping it that way until final conversion at the transmitter to the PAL-coded analogue signal required by the domestic receiver.

For international exchange we shall find signals distributed in digital form, very possibly as luminance plus colour difference components; final coding into PAL, SECAM, etc. will be left to the individual customer countries. Accompanying sound will be digitally multiplexed with the vision signal, several sound channels being available for multilingual requirements. All this will require comprehensive national and international standardisation of digital coding methods, and much work in the 'eighties will be devoted to negotiation and argument on this front.

Teletext and similar services can clearly be expected to advance rapidly in the next ten years. The scope of the information provided can increase almost indefinitely, reasonably short access times being maintained by allocating an entire television channel to this purpose and by provision of further storage and processing in receivers.

High-resolution graphics, still and animated pictures of full television quality, and increasing sophisticated subtitling services will become available. Teletextware, the transmission via teletext of computer programmes, will greatly extend the variety of TV games and will provide the non-specialised computer services which increasingly we shall make use of in our domestic lives. Hard-copy printers will become available to give us permanent records of any desired teletext information and (though not perhaps in the 'eighties) this may become the medium by which we receive our copy of Wireless World.

As we move towards the 'nineties, we may see the first optical fibre data circuits run into private homes. In the longer term all radio, television, information and communications services will come to us 'on the fibre,' radiated transmissions being reserved for mobile applications where wireless communication is essential. Once we have our domestic wide-band circuits and high-quality large screen displays, the way will be clear for 'hi-fi' television on new standards. But it will not be in the 'eighties that we shall be closing down the 625-line services.

With TV receivers now in 97% of UK homes (70% colour) it's right and proper to consider television first. In the early 'seventies, the transition was being made from hybrid circuits with a mixture of valves and transistors to all solid-state. With moves in this direction, styling improvements were made possible to reduce the overall size of the average television cabinet and chassis engineering moved towards modular construction.

Ultrasonic remote controls made their appearance, and were quickly accepted only to be gradually replaced by quicker-acting infra-red control systems. Whilst ultrasonic controls were more than adequate for the typical viewer of the late 'seventies who wanted to send simple commands to his receiver, the introduction of infra-red microprocessor-controlled systems is particularly relevant to the customer requirements of the 'eighties when...
Teletext and Prestel are likely to be in widespread use.

However, both of these great British developments with their data display capabilities are still in their infancy and the lack of average consumer awareness about their existence and what the services offer is an indication that it is not enough for the engineers to apply their minds and develop such powerful means of communication. Marketing people must do more to promote their benefits.

Probably the product area of the 'seventies which will have the greatest impact in the 'eighties is domestic video, both cassette recorder and disc. The late 'seventies saw the introduction of domestic video cassette recorders not much larger than conventional audio cassette recorders and almost as easy to install and use. The early recorders (of any format) relied heavily on mechanical control functions but already we are beginning to see mechanical operations replaced by electronics and especially microprocessor controls, but more of this later. The audio scene saw one overriding development - the growth in importance of the conventional audio cassette, aided by the world-wide acceptance of a common standard. Ten years ago, the available cassette hardware and software was still regarded as something of a novelty and not a serious contender to the established position of the quality record player and audio disc or open reel recorder. Developments such as noise reduction systems, improved drive systems and record/replay heads, software developments improving overall performance standards (with first of all CrO₂ tape and more recently the introduction of metallic tapes) have elevated the performance of cassette equipment and cassettes of ten years ago to a replay medium generally accepted even in serious hi-fi circles. Certainly the public have also accepted the cassette. At the close of the 'seventies, UK homes owned more cassette playing equipment than disc playing.

The development of low price, good quality cassette mechanisms made the music centre a practical proposition and without doubt this particular item was the audio home entertainment product of the 'seventies. The audio cassette is also the common denominator amongst those other products that during the period had greatest appeal for the public. Cassette and radio cassette recorders now sell at an annual rate of more than 2-million units per annum in the UK. The biggest growth area in the late 'seventies was quality stereo radio cassettes with automatic programming facilities and even Dolby Noise Reduction.

Cassette-based products have been so successful because they have two overwhelming advantages over their disc counterparts; the cassette can be re-recorded and the machine is easily portable, satisfying today's demand for music on the move. In-car entertainment products have also adapted to the higher ownership levels of home based cassette equipment so that today it is possible to have better quality audio sound in a car than was was possible in most homes ten years ago.

But enough of the past; it seems that the 'eighties will see most of the colour televisions acquired during the 'seventies replaced by receivers which, on the outside, may look similar (apart from the reduced number of function controls) but on the inside will bear very little likeness. The modular chassis of the 'seventies will increasingly be replaced by single board chassis designed to optimize the availability of large scale integrated circuits (l.s.i.) and the application of microprocessors, remote control teletext and viewdata displays. The introduction of single board chassis will revolutionise not only product reliability but also the approach to servicing so that the service department of the 'eighties will look vastly different to that of the 'seventies. Today's cathode ray tube technology means that the television viewers of tomorrow will see demonstrably better pictures and data displays than have been seen to date.

Increasingly, TV receiver design will have to accommodate the requirements of home computers, video games etc. which are rapidly changing the nature of television from a passive piece of equipment capable of only showing programme material being broadcast by the BBC or IBA to a two-way, interactive display medium at the centre of a communications network. By the mid 'eighties, satellite broadcasting could become a reality, allowing the viewer a much wider choice of programme material. It is also reasonable to predict that voice-activated controls will begin to make their appearance, freeing the
viewer from the arduous task of having to press the control buttons of a hand-held remote unit!

But, as previously mentioned, the 'eighties will more than anything else be the decade of the widespread introduction of domestic video products. The VHS (Video Home System) format has quickly established itself as the best-selling video system in the world in all the major developed markets - the UK, Europe, USA and Japan - but despite this, other video formats are likely to be around for many years to come. The conventional format of the early video recorders is likely to change with the accent being on the portability of a recorder unit linked to a separate programmable TV tuner/timer which could be indispensable when satellite broadcasting is a reality. Indeed the situation could well arise that despite the increased leisure time available, video owners will be so busy recording programmes they will never have the time to replay them!

Already the introduction of the vidicon tube has made low-cost, good quality colour video cameras a reality. No one can doubt that the already high performance standards of today's products will be improved, real money prices will fall and the cameras themselves will weigh less and diminish in size. No wonder that with the arrival of electronic photography manufacturers around the world are getting out of the conventional cine 8 camera business as quickly as possible - they have seen the writing on the wall.

It is forecast that the ownership of domestic video cassette recorders will parallel the early growth of colour TV in the UK. By 1984 at least 7% of UK homes are expected to have acquired one. They will be used mainly for time-shift recording and the replay of home-made video movies at around £5 per hour, compared with £100 per hour plus for cine, the difference adding greatly to consumer appeal. The additional appeal of pre-recorded video cassette software will pale into insignificance when video disc players with their lost cost software become a reality. One thing is certain; the incompatibility of the various video disc standards that are likely to appear will be a much more serious factor than with the present ones surrounding video cassette recorders. The availability of disc software will be a critical factor on three counts:

a. without the appropriate software the disc player itself is useless.

b. questions related to the low cost production of video discs still have to be resolved.

c. material for reproduction on video disc is likely to be surrounded by a minefield of copyright issues which have still to be resolved.

However, the video disc player is likely to lead to the further demise of the conventional audio record player because despite the name "video disc," all video disc players give the capability of very much improved audio-only replay, making possible a signal-to-noise ratio in excess of 90dB through the use of PCM recording techniques. So looking ahead, any audio disc system that does not include a video replay mode is likely to find the going a bit tough.

So far no reference has been made to monochrome television receivers which, as the years pass, are likely to become increasingly less attractive as potential purchasers accept colour TV viewing as the norm. On the other hand it is not unreasonable to suggest that the youth of tomorrow will look at television in the same way that today they look at radio and the cassette. That is, they will want to take it with them wherever they go. Therefore (and with continuing miniaturization) today's combination TV products either with radio, or radio and cassette, are likely to become more and more popular. Audio products either mains-only, portable or "in-car" will become increasingly cassette-based as the youngsters of today become the purchasers of tomorrow. This is a generation to whom the cassette is not something new and the majority look upon their parents collection of 78, 33⅓ and 45 r.p.m. discs with the same degree of interest that Arthur Negus looks at 17th century...
Beyond the 'eighties?

Quite recently Ferguson had an experimental look at the home entertainment centre of the early 1990s. The result was a concept called "Total Television" which included in a domestic console unit, a VHS electronic cassette recorder, floppy disc machine, electronic audio cassette, Prestel/home computer keyboard and videophone with remote control of all viewing functions. The conventional c.r.t. was replaced by a wall-mounted flat screen to take account of the multiple screen viewing that might be a requirement of the future. A dream? Well apart from the sorting out of problems related to the flat screen the other features of the unit are either with us today or at least a large scale manufacturing possibility.

Only time will tell how close to reality the ideas of the late 'seventies will be at the end of the 'eighties.

Radio navigation and radar


The fields of radio navigation and radar cover a broad range of constantly changing techniques, and are influenced by advances in computers and military systems.

With both these topics, we are interested either in where we are, or where someone else is. Almost every permutation and combination of these alternatives has been investigated over the past fifty years or so.

In moving a vessel from A to B some basic form of dead reckoning and position plotting should be maintained and in ships in particular, traditional methods using the sextant, chronometer and compass are fundamental to good navigation. In the air, long-haul aircraft frequently rely on inertial navigation, again based upon the gyro, and indeed ships also use this type of navigational aid. However, we are here primarily concerned with radio aids and radar, and in very many ships, in aircraft and at airfields, the ubiquitous direction finder (d.f.) is used, and is sometimes the only form of aid. In fact, both radar and radio navigation can trace their ancestry back to the simple d.f.

The adoption of new equipment in civil aircraft and ships is inevitably limited by financial constraints; every piece of new hardware proposed for a ship or aircraft must be justified in terms of cost effectiveness. This means that adequate, well-proven techniques and systems tend to have a very long operational life. Nevertheless, if rapid, accurate position-fixing can shorten journeys and minimize delays, then in a period of increasing fuel costs, new equipment capable of providing this must become more readily acceptable.

Safety at sea and in the air is, of course, vitally important. At sea, minimum safety requirements are recommended by the International Maritime Consultative Organization (IMCO) primarily for vessels above 300 tons, although the country in which the ship is registered legislates for this in the UK, it is the responsibility of the Department of Trade. In the air, the equivalent authority is the International Civil Aviation Organization (ICAO).

Direction finding

Before dealing with some of the more recent developments in navigation aids, the current state of d.f. is worth examining. There are three major areas of common commercial usage, air-to-ground, ship-to-shore and ground-to-air. There are other military applications, but for general navigation the major advances have been in improving the equipment. A typical marine automatic direction finder, in common use, covers the m.f. beacons in the band 250-550 kHz and also operates on the international distress frequency of 2182 kHz. This equipment is as simple to use as a domestic receiver, gives automatic ambiguity resolution, the bearing of the station being read directly from a compass-type scale, typically to within ±1°. Because of the relatively short range of reliable bearings, ship navigation by d.f. is mainly confined to coastal waters; in the consumer field, many thousands of simple direction finders are in use in modest sailing boats and motor cruisers. The situation with airborne d.f. is similar to that for ships: most aircraft carry one and the accent is...
on automatic operation. The frequency band is typically 190 to 1800 kHz. The size of the antenna loops have been reduced and contained in streamlined bumps to reduce air drag. In many parts of the world a.d.f. is still the primary source of navigation information, which in areas with good reception can provide a bearing of \( \pm 1^\circ \).

Ground-based direction finders require only the minimum of a communication set in the aircraft to provide a position line, so that if all else fails, navigation assistance can still be provided. These direction finders mostly operate on v.h.f./u.h.f. and in order to minimize the bearing errors from all causes, antenna arrays are multielement, frequently wide aperture and automatic in operation, with direct-reading bearing presentation. Most locations can provide \( \pm 1^\circ \) accuracy on signals of reasonable strength.

A short-range navigational aid closely allied to d.f. is the v.h.f. omnirange (VOR) which, when associated with a distance-measuring equipment (DME), gives aircraft a precise location. The range limitations caused by operating at v.h.f./u.h.f. (108-118 MHz for VOR and 960-1215 MHz for DME) make this system unattractive for ships.

**Hyperbolic systems**

Measuring distances from known ground radio stations is a well-established navigational aid. Hyperbolic systems are so called because the position lines they provide from such measurements are hyperbolic curves. Referring to Fig. 2, if \( T_1 \), a transmitting station, emits a short pulse, and transmitter \( T_2 \) simultaneously emits a second pulse, then any receiver on line \( A-B \) will receive these pulses together. Positions at which one pulse is delayed by a given time with respect to the other lie on one of the hyperbolae. The association of a third transmitter would provide two position lines and therefore a fix.

One of the best known pulse systems is Loran 'C' which operates on a frequency of about 2 MHz and covers large areas of the Pacific, Atlantic and Europe. During the last war, a similar British system known as GEE operated at v.h.f. With a good ground-wave pulse, position accuracies of better than one mile in 100 miles are possible but, as with many long-range navigational aids, ionospheric sky-wave propagation can produce errors an order of magnitude larger, and considerable skill is needed to interpret results in adverse conditions. The Decca system, operating at around 100 kHz, also became established during the second world war. This uses c.w. signals and phase measurement to provide position lines and fixes. Very many ships and aircraft carry Decca, which has been considerably refined over the years to overcome propagation and ambiguity problems, so that automatic plotting on route maps is now generally in use, giving accuracies of fractions of a mile.

A system of increasing importance, which is designed to minimize range and propagation problems, is Omega. This operates on very low frequencies (v.l.f.)—typically 10-14 kHz—with interstation baselines of around 5,000 miles. The very low frequency provides long range, stable and predictable propagation characteristics and the large separation between stations means that position lines are almost parallel over very large areas. Omega is a c.w. phase-comparison system and is virtually the only radio navigation system that can be used by completely submerged submarines.

A typical marine Omega receiver incorporates four channels for continuous monitoring of four transmitters, each channel measuring the phase of the signal relative to an internal high stability reference oscillator. Phase difference can be measured to one-hundredth of a cycle, defined as centi-lanes. In use, the receiver is run continuously from leaving port, automatically logging the lanes. It takes about half an hour to cross one lane, and modern equipment provides direct
Fig. 3. Doppler navigation — airborne equipment — 1980 model AD660 compared with designs of the '50s (left) and '60s (right).

Fig. 4. Satellite navigation.

Terrain-reference navigation
The Doppler navigator provides an aircraft with means for measuring the frequency shift of a radio signal reflected from the ground. With no drift and for a radio beam transmitted at a forward angle \( \theta \) to the aircraft horizontal axis, the Doppler frequency shift is \( \frac{2V}{c} \cos \theta \) Hz. Thus, the Doppler shift can provide an accurate measure of the aircraft ground speed, \( V \).

If two beams are radiated downwards at an angle to the forward direction then it is possible to measure the sideways motion or drift of the aircraft. Note that the Doppler shift is also proportional to the cosine of the vertical angle of the beam, hence antenna systems must be horizontally stabilized or a further pair of beams arranged to point aft to provide a differential signal, independent of attitude.

The Doppler itself gives ground speed and drift angle; to determine location, accurate heading information must be provided to the navigation computer. Most Doppler systems operate at microwave frequencies around X-Band (3 cm) and are sufficiently refined to drive an automatic map reader, or feed an integrated navigation system. Overall accuracies of one or two per cent of distance flown can be expected.

Sonar Doppler operating on similar principles is increasingly used by larger ships, and mariners also use depth sounding to augment their position fixing, particularly near harbour.

Airborne radar systems giving very high azimuth resolution and known as synthetic aperture radar (SAR) can be used for navigation by map reading the high quality returns. The high resolution is obtained by simulating the radiation as from a wide aperture antenna by storing and recombining the individual signal elements from a small antenna as the aircraft carrying this small antenna moves along its track.

Similarly, by storing the height of the terrain along or adjacent to your own desired flight path, and comparing actual height from a radio altimeter, positional information may be obtained using correlation techniques.

Satellite navigation
NAVSTAR or Global Positioning System (GPS) is designed to give very accurate position and velocity information anywhere in the world. The full system is intended to include 24 satellites in three orbits, giving visibility of 6 to 11 satellites at 5° or more above the horizon from any location on the earth's surface.

The basic method of position fixing by means of satellites is similar to celestial navigation except that distance, rather than angle provides the basic data. Fig. 4 shows the essential components of NAVSTAR. The height of the satellite is accurately determined, the earth's radius is known and the range is measured by timing radio signals from the satellite. In three dimensions, the range line traces a circle upon the earth's surface giving an observer position line. Two such lines give a location fix, and three are needed.
for an aircraft to include its height. Signals are transmitted on two L-band frequencies, 1227 MHz and 1575 MHz, containing identification and the navigation data for the user to compute his position. This includes information on the status of the satellite, orbit details to enable the user to calculate the position of each satellite at the time of transmission, time corrections and propagation delay corrections.

High accuracy can only be achieved by precise synchronization of the satellite clocks with each other and the user clock error must be known or corrected; each space vehicle carries an atomic frequency standard which is corrected at least daily with a caesium clock at the master control ground station. In terms of accuracy one nanosecond of time error is equivalent to 0.3m range error.

The concept of navigation by satellite is simple. In practice however, for a worldwide system, a number of space vehicles must be maintained in accurate orbit, constantly updated for time and position. The user equipment includes a microwave antenna and receiver, together with a comprehensive navigation computer. Nevertheless, advances in microwave and microprocessor devices have made possible a range of receivers for ships, aircraft and missiles, and even a 10kg manpack, which will locate position to within about 10m. At present, GPS is in the validation phase I - about six satellites are in operation. Phase II is the period of development for military use, primarily in the USA, and this phase will end in 1982. True production of an operational system will take place between 1984 and 1987. Thus, one can expect that it will be the latter part of the 80s before NAVSTAR can be considered a truly universal worldwide navigational aid.

Radar systems

There is an enormous variety of radar equipments and techniques, ranging from small boat sets, to large ground military complexes. Radar is frequently used for navigation, especially by ships, but here I would like to discuss a few recent innovations affecting the big system design philosophies.

A simple, basic, airfield-based surveillance radar locates an aircraft by rotating a continuous train of pulses in a transmitted radio beam, narrow in azimuth, and measuring the time of flight of the pulses reflected from the aircraft. The aircraft position is usually displayed on a cathode ray tube or plan position indicator (p.p.i.) in the form of range and bearing from the radar antenna.

There have been considerable developments in radar techniques since the last war to help controllers cope with increased air traffic. Early improvements integrated computers and alpha/numeric labelling systems to automatically track and identify target returns. Extensive signal processing and moving target indication circuitry has overcome many problems of false returns and clutter obscuration. Perhaps two of the more recent major improvements in ground radar have been in the growth of secondary radar for air traffic control and the evolution of the 3-D radar for military use.

In hostile conditions the ability to observe enemy aircraft without their co-operation is obviously useful, but for aircraft which are both co-operating and controlled, the addition of a transponder confers useful advantages.

Secondary surveillance radar (s.s.r.) is similar to the military Identification Friend or Foe (i.f.f.) developed during the war to protect friendly aircraft. S.s.r. works by sending a radar pulse from an interrogating transmitter. This pulse is received aboard the aircraft by a transponder and retransmitted on a different frequency as a group of coded pulses, which include aircraft identity and a height reading from the aircraft's altimeter. The equipment is normally mounted on the primary radar and the signals from s.s.r. are either displayed directly on the radar p.p.i. for identification purposes or separately processed in the computer system.

The classic radar with the rotating beam will not provide height information; in fact, the beam shape is designed to cover as much vertical air space as possible. For height information, a separate vertically-scanning radar antenna was employed, usually controlled on demand. Continuing improvements in the design of microwave antennas and component design have enabled a new 3-D radar to be designed. Modern techniques enable such a system to be fully transportable and highly reliable; for example, the transmitter valve operates at 3.3MW to provide a 10,000h expected life. The operating wavelength of this particular system is 23cm, the range accuracy 0.05 nautical miles, azimuth accuracy 0.5 nautical miles in 100 and height accuracy 1,000ft at 100 nautical miles. It has many advanced facilities such as automatic plot extraction and tracking in three dimensions, and for military operation provides a range of electronic counter-counter-measure (e.c.c.m.) facilities including unrestricted frequency agility, random pulse staggering, pulse compression, chaff and clutter suppression and digital Doppler moving-target indication.

The future

The ideal radar gives all-weather, clutter-free operation and as much information as possible about aircraft in the air space of interest. This is true for both ground-based and aircraft systems, and similar criteria apply to ships' radars. The ideal navigation aid gives exact location under all operational conditions, is lightweight and simple to use. For both activities, of course, equipment needs to be highly reliable and cost-effective. The systems described so far represent the current,
state of development and undergo continuing refinement towards these objectives.

One must, however, differentiate between military and civil use. Co-operation-dependent systems, such as those based upon satellites or global transmitters, could well be vulnerable in times of national conflict. Probably the self-contained navaid is least open to this sort of criticism if high accuracy at reasonable cost can be sustained.

One can fairly safely predict that semiconductor microcircuit advances will continue to affect radar and range navigation developments in a very significant manner. Digital processing and storage are already leading to new concepts in system organization and complex error corrections not previously feasible.

Miniaturization of the newer solid-state, microwave power sources and other components leads to new applications. One example is location and control of road vehicles, increasingly important for large, commercial fleets or public utilities in these times of energy problems and rising fuel costs. The display shown in Fig. 5 us of part of the area of a map of London, where the characteristics of each road junction are stored in a computer in the boot of a car for automatic position fixing.

A further example is in radar developments which are making feasible static antenna arrays where each element of the array is effectively a miniature transmitter/receiver and the beam is electronically rotated or selected. One such system, known as bi-static, can use a separate transmitter as an illuminator, with several spaced receiving systems using multi-beam static arrays. Such a system could provide enhanced protection against noise, interference and signal distortion.

The US Air Force hopes to deploy a 600ft diameter radar in earth orbit by 1985, using the space shuttle. This could be used for tracking ships, aircraft, cruise missiles, inter-continental ballistic missiles and even armoured vehicles on the ground.

The author thanks the technical director, GEC-Marconi, for permission to publish this article.

Further Reading

Audio
by Adrian Hope

BACK IN the early winter of 1969 the Olympia Exhibition Hall played host to the International Audio and Photo-Cine fairs. Ten years ago, although burgeoning trade and public interest in sound reproduction had made Olympia a must in the post-war tradition of exhibiting equipment in the Russell, Washington and Waldorf hotels in London, there was still insufficient support to justify an audio-only show at Olympia. It soon changed of course as hi-fi became an essential domestic luxury. Now, ten years later, we have seen the rise to dizzy heights and fall into disfavour of Olympia as a hi-fi exhibition site. Indeed in many respects Olympia has been a barometer of hi-fi trade. After 1969 the Audio and Photo-Cine Fair became the Audio Festival and Fair and then the Home Entertainment Show. It was cancelled at the eleventh hour in 1976 and in 1977 drew only very disappointing crowds. Since then there hasn't been an Olympia audio exhibition.

The face of audio retailing has changed at least as much as the Olympia Exhibition Hall in the beginning of the 1970s most of the electronic shops in London's Tottenham Court and Charing Cross roads sold electronic components, along with construction kits and a smattering of ready-built audio equipment. Almost all had one characteristic in common: undisguised impatience with the average customer. It was, I suppose, understandable. There is little profit to be had from testing a valve or advising an amateur constructor on why a resistor has burned out. Soon one asks for a fuse, a resistor or a spare part could expect to be treated like a mad leper in all but a very few shops. Gradually the public became reconciled to the idea of buying equipment in a cardboard box from a shop assistant who might just as well have been selling washing powder or potatoes. The main culprit, some observers argued, was the end of resale price maintenance and the consequent declaration of a competitive price war. Shops selling at cut-to-the-bone prices could not hope to offer anything in the way of before and after sales service or advice. Some dealers stuck to higher prices but offered service into the bar-

gain. Inevitably some customers took advice from the high price dealer and then bought the recommended product at cut price in a cardboard box from a warehouse dealer. Between these extremes some dealers, both in London's golden mile and elsewhere in the UK where the golden mile image had spread, offered intelligent advice and reasonable service at a low price. Others offered neither service nor advice but at high price.

It was inevitable that the bubble would eventually burst. There comes a time, especially when money is short, when a householder with an adequate sound system will no longer go out once a year and buy a replacement. There comes a time when the public, working hard for their money, start to resent the need to junk relatively new equipment for the want of a single spare part that proves unobtainable, or at least an expensive nightmare to procure. It is no secret that now, at the end of the decade, the audio trade is in bad trouble. Spare cash now, and there is clearly less of it around, goes toward a video recorder or a second colour tv, not a new stereo amplifier, record turntable or cassette recorder to replace a perfectly adequate system which is still giving faithful service.

The Olympia barometer of hi-fi is not however to be taken as gospel. Although Olympia is no longer the site of an annual audio exhibition in London, other shows flourish. The sad truth is that Olympia now has a bad name in the audio world. Exhibitor firms have suffered once too often from what they euphemistically refer to as "union problems," but which in less euphemistic terms means spending many tens of thousands of pounds to exhibit and finding the stand unfinished on opening day. It's also a barn of a place, in many respects the unideal venue for audio demonstrations. But smaller shows in hotels in and around London have always left some exhibitors or visitors dissatisfied. One year in the mid-seventies there were two rival shows at two Heathrow hotels running in parallel. An autumn 1979 show in London was cancelled at the last minute through lack of trade support. Currently, perhaps rather curiously, the major UK show is the annual exhibition held at Harrogate in Yorkshire. The fact that so many of the trade, press and public are prepared to venture so far
Another phenomenon of the decade has been the rise, and occasional fall, of so many audio and hi-fi publications. At the beginning of the decade there were just two specialist hi-fi magazines. Both had a fairly staid outlook. Then the first of the breakaway "glossies" appeared followed by a string of several more. After various changes of ownership, a few bankruptcies, and several changes of title and direction the market now appears stable.

One theory is that the current misfortunes of the trade are partly due to the boom in hi-fi journalism. The argument is that enthusiasts, with limited money, are now content to read about new developments and leave buying them to someone else. Whereas magazines like Playboy and Penthouse work on the assumption that readers are interested mainly in vicarious thrills, the hi-fi industry has so far assumed that a stimulating article on audio will stimulate sales of the product. It appears stable.

The last decade has seen any number of new developments and offered, often foisted on the buying public. But a few have stood out head and shoulders from the rest either as a result of value which has been subsequently proven or because the passage of time has underlined their lack of consequence. But some ideas of consequence have failed, at least first time round. And some ideas of no consequence have succeeded, at least temporarily.

From a considered and selective recap on the technology seen in the 'seventies, likely trends for the 'eighties become clear.

The 1970s must surely go down in history as the decade in which surround sound didn't happen. In the late 'sixties engineers in the USA started to show interest in improving the reproduction of music in a relatively small domestic room by adding reverberation to simulate the sound of concert hall or large room. Early workers soon recognised that it was not sufficient merely to reproduce natural hall ambience, rather than simulate it at the reproduction stage.

The then-new breed of multitrack studio recorders provided the ideal tool to record ambience along with the main, front, sound stage. An eight-track tape cartridge or four-track tape-recorder provided the ideal medium for selling the resultant multichannel surround sound to the public. The record companies, forseeing a drastic drop in two-channel stereo disc sales, panicked. At the turn of the decade numerous engineers around the world beavered away to produce a multichannel surround sound disc that would also offer good stereo and mono.

Not to be outdone, the broadcasters addressed themselves to the same problem. At first there was excitement that the apparently impossible had been achieved; a quartet of loudspeakers around the room could be fed with four sets of signals derived from a two-channel stereo source. But as the inevitable trade-offs and compromises became better understood, thinking engineers became disillusioned. So did the public not so much because of the various system deficiencies, but because of the lack of standardisation between so many competitive systems.

With the benefit of hindsight we now know that lack of standardisation on any one system was probably the best thing that ever happened to domestic audio. If any one early 'seventies system had become a world standard we would now be stuck with it — and all its inherent inadequacies. But early in the 1970s surround sound reproduction (or quadraphonics as it became known when four loudspeakers in the four corners of a room became tradition), looked to the marketing men like potential big business. The 1972 Consumer Electronics Show in Chicago saw private discontent flare into public squabbles. While the manufacturers tried to produce reproduction equipment capable of playing any or all of the competitive systems then available or announced, the record companies hedged over which system to adopt. "They ought to be locked in a room and kept on bread and water until they come out with an agreement" said one frustrated manufacturer.

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*When broadcasters finally agree a surround format we might get multi-channel surround sound records from the industry again.*
At around this time a compromise offered by American engineer David Hafler started to find favour. This was the now familiar “Hafler circuit” which feeds a rear pair of loudspeakers with the difference information available across the outputs of a conventional stereo amplifier.

This simple connection provides signals for the rear, from almost any programme material. Readers of hi-fi magazines, puzzled over which quadraphonic system to buy, were repeatedly advised to compromise with a Hafler set up, at least temporarily until a standard was agreed. Even now, long after the quadraphonic bubble has burst, many enthusiasts retain a Hafler connection to feed rear loudspeakers because, especially with programme material recorded with a simple crossed pair of microphones, the results can be highly acceptable. There is now little doubt that every quadraphonic system marketed during the last decade is dead in its present form.

But the last years of the decade has seen the progressive acceptance of Ambisonics surround sound technology. This of course stems from the work of Michael Gerzon and Professor Peter Felligett.

It is also embraced, albeit at a fluctuating extent, by the BBC and IBA. The recent patent pool agreement between Ambisonics-NRDC, Nippon Columbia and Duane Cooper (joint holders of most of the crucial patents covering a hierarchical approach to Ambisonics. surround-sound technology) will almost certainly prove a significant influence in the next decade. In the USA, the Federal Communications Commission is currently debating, yet again, the future of surround-sound broadcasting. The signs are that the final FCC choice will be between Ambisonics and the CBS SQ system, or modern variants thereof. Until recently there has been a fair amount of interest from the Ambisonics faction. But now the IBA has raised a question mark over the validity of the hierarchical approach. Essentially the IBA argues that the best compromise is a three channel system, which offers good surround sound to listeners with a three-channel decoder, and good stereo and mono with existing equipment. This conflicts with the Ambisonics-NRDC approach which seeks to offer the surround-sound listener the choice of using either two or three channel (the third with or without limited bandwidth) reproduction equipment.

The IBA now describes the two approaches as “irreconcilable” so it is clear that if surround sound is to progress in the 'eighties past the laboratory stage the IBA, BBC and Ambisonics-NRDC engineers must reconcile their differences. This will require the cooperation of all parties in an intensive on-air transmission tests. Unfortunately the BBC and IBA have not been noted for their mutual cooperation and have instead appeared more inclined to generate competition even where none naturally exists. Although independency of technical research at the development stage is admirable and in the public interest, rivalry at the early stages of commercial development can only hamper the spread of a new technology. Witness the 'eighties past the laboratory stage the cooperation and have instead appeared not been noted for their mutual cooperation and have instead appeared.
that the future of one is dependent on the other. It was in 1972 that Philips first announced a video cassette recorder capable of recording colour TV pictures and sound on a cassette of half-inch tape. Although the original N1500 machine was intended for the industrial and educational market, by 1974 it was launched for — albeit limited — open sale to the general public. This started not only the domestic video revolution but also the inexorable move toward digital sound. Any recording system capable of handling the four or 5MHz necessary for colour video is more than capable of handling the bit stream necessary for stereo or multichannel sound in digital form. Moreover a decade of work into video reproduction from discs, which culminated in the USA test marketing launch of a practical video disc system by Philips-Magnavox in 1979, brings the digital audio disc a step closer. Philips has of course already shown the compact disc, or digital audio version of the Philips VLP video disc, and toward the end of 1979 announced a patents liaison with Sony. Sony had independently developed a laser-optical disc system similar to that proposed by Philips. With the union of Philips and Sony standardization of a laser-read optical video disc comes a step closer. Almost certainly the Philips-Sony union will bring agreement on a digital Compact Audio Disc smaller than the 30cm proposal made by Sony and larger than the 11.5cm diameter chosen by Philips for the compact disc. Very probably a digital "compact audio disc" of around 15cm will emerge from the union. But this will almost certainly not herald world standardization. JVC still sticks hard with its different, and quite incompatible, capacitance-read grooveless disc and RCA argues in favour of a grooved capacitance disc. Matsushita has proposed a grooved disc which is read by a mechanical pressure-sensitive stylus similar to that developed by Telefunken and Decca early in the decade and briefly marketed at the Teldec TeD video disc. It is now known that Teldec has a miniature digital audio disc version of TeD. This Teldec Mini Disc is ready to launch in Europe if and when the time is adjudged commercially right. Without doubt there are many bitter battles ahead before there can be world standardization on the digital audio disc. These battles will delay standardization and give impetus to the short term stop gaps such as metal tape. There is also a move toward 45rev/min long-playing analogue discs. It is argued that their higher rotational speed, coupled with the long playing time per side offered by computer-assisted cutting techniques, offer the analogue album a shot in the arm. Casual observers talk vaguely of some wholly new, as yet undreamed of, storage medium to replace the tape or disc. Without doubt it would be possible to encode programme material in holographic form. But the idea of a chip or memory, storing an hour of programme in solid state, must surely remain a dream for at least the next decade. Although high density memories with fast access time are available, a few moments calculation is sufficient to show that solid-state memories have a long way to go before they can offer the equivalent of an LP record in real time. Prophesies, especially in such fast-moving times, are always dangerous, but it seems a safe bet that for the next ten years sound and vision in the home will be stored on, and reproduced from, a moving strip of magnetic, capacitive or optical material or a rotating disc of similar characteristics.

The speed with which a new storage medium becomes a commercial success and gains acceptance as a household norm, will depend entirely on the behaviour of the companies involved in the development and promotion of such a new medium. Rapid agreement on digital encoding standards and storage techniques could bring a new record medium into the home within a couple of years. But behind the scenes squabbling, similar to that which killed off the quadraphonic fiasco this may not necessarily be a bad thing. Currently the signs are that the strong US and Japanese influences may impose on us world coding and sampling standards for digital sound reproduction which are tied to local TV standards. These could well prohibit or make expensively difficult, the exchange of recorded audio material between continents. Certainly it would be an appallingly retrogressive step. Moreover in their enthusiasm for a new generation of recording and reproduction techniques, engineers at laboratory level appear to have overlooked, or at least brushed to one side, the very real problems of mass producing high-density storage programme material in reliable quality as well as quantity. After one hundred years of analogue disc recording, there are still all too few record pressing plants capable of producing a respectable audio disc pressing. With track spacing between 50 and 100 times tighter in digital or video programme storage the importance of producing blemish-free pressings becomes paramount. The video and digital audio systems that succeed in the long run may well be the system for which it proves easiest to mass produce programme material.

Cassette recorders for the 'eighties will have bias and equalization for metal-particle tape but will the public pay the extra price?

H.f. radio communication
by R. F. E. Winn B.Sc.(Eng.), F.I.E.E. Racial Communications Ltd

Advances in component technology and new design concepts during the past decade, together with projected future developments, ensure that h.f. radio communications will retain importance well into the twenty-first century. In particular this is true of the maritime mobile service where satellite communication is still in its embryonic stage, in developing countries where the economies of h.f. point-to-point working with low traffic density are attractive, in defence (as a back-up if not always primary system), and in emergency use where air-transportable containerised stations can be rapidly deployed. As well as advances in technology in recent years there has been a better understanding of the vagaries of propagation. This has resulted in greater precision in predicting maximum usable frequencies over various paths during the 24-hour day at different seasons and during sun-spot cycles.

For medium and long-haul communication h.f. radio today is still an economic, efficient and reliable solution.

Receivers of the 1970s. The most significant technical changes have been in receiver design in which a number of ideas, coupled with newly available...
components, converged to provide by the early 1970s a completely new order of excellence in terms of overall performance and ease of operation. Before discussing the "breakthrough" of the 1970s it is helpful to look briefly at two previous generations of receivers.

In the immediate post-war years the most exciting development was the drift-cancelling technique known as the Wadley Loop. Although a tricky concept, demanding skilled mechanical as well as electrical design, it was successfully implemented in the now classic RA 17 receiver, made by my company, of which some thousands are still in daily use throughout the world. For the first time it had become possible to tune to a given frequency and leave the receiver unattended with reasonable confidence in its frequency stability over extended periods.

The next big challenge came in the 1960s with the change from thermionic valves to solid state devices. Early examples were heavily influenced by the previous valved designs, and although greater ingenuity was sometimes achieved they were little more than an exercise in re-engineering using transistors in place of valves. The advantages were reductions in weight, size and power consumption and an increase, at least in theory, in reliability. Overall performance, however, was disappointing and, in general, the best of the first generation of solid state receivers were inferior to the best of the valved sets. There was not even an advantage in price.

A parallel development in the 1960s was the frequency synthesizer, which generated a wide range of frequencies each with a stability equal to that of a single master crystal oscillator. This was seen as an elegant substitute for the often troublesome free-running local oscillator in superhet receivers and as a simpler solution to drift than the Wadley Loop. Unhappily the early synthesizers brought their own problems in the shape of unwanted intermodulation products generated by the internal mixers, adders and dividers. The advent of the digital synthesizer provided a cleaner output and today's units are capable of excellent spectral purity. The early synthesizers also suffered from the operational disadvantage in that frequency was selected through decade switches. Excellent if the exact frequency of a wanted signal was known, but hopeless for "searching". This problem was overcome later.

With so much new technology becoming available, engineers in this field came to the conclusion that a radical re-think on receiver design was overdue. Not only on how newly available technology and components could be implemented to advantage but also all aspects of performance and operation in modern conditions. The starting point was a statistical analysis of their occupancy of the h.f. frequency spectrum in terms of density and types of signals, their distribution and relative strengths, which would give a clearer indication of how a receiver needed to perform in order to use efficiently the 9,000 or so 3kHz channels available. An analysis was made by a computer in my company and, independently, a similar exercise was carried out by B. M. Sosin of Marconi Communications Systems.

It had been realised that the most significant limiting factor in receiver performance was linearity. Selectivity was as important as ever but the emphasis on front end sensitivity which had been a paramount feature of design for the past 50 years had come to the end of its usefulness and no further gains were necessary or indeed possible in this area.

It was found from the analysis and measurement that high powered broadcast and commercial stations were generating tens, in some cases hundreds, of millivolts at the antenna terminals when received on large collecting systems. The strong signals were generating a large number of intermodulation products strong enough to give the appearance of liveliness in the receiver yet masking weak wanted signals. What was required was a big increase in dynamic range together with extreme linearity, and the key to the problem of intermodulation products was to work out the linearity of previous receivers and to discover where the products were formed and at what level.

The first range of solid state receivers to incorporate the new principles in the 1970s was the RA 1770 series, of which the RA 1772 general purpose receiver will be discussed. The block diagram of this receiver (Fig. 1) shows it to be a straightforward double conversion superhet but with a number of novel features which provided a performance with respect to dynamic range, intermodulation products, reciprocal mixing, cross modulation, blocking and spurious response far superior to any other receiver then in production.

Fig. 1. Block diagram of the RA 1772 general purpose receiver.
The design sensitivity had indeed been necessary to convince ourselves that tests with a signal generator were there were far fewer signals. Repeated apparent lack of sensitivity because echoed by the first customer, were on the development models, later with the main gain in the second i.f. switching m.o.s.f.e.t. first mixer, only the potentially troublesome mechanical the front panel. This not only eliminated switching controlled by d.c. only from filters were selected through transistor fitted at the customers' choice. The rack of equipment. Provision was made had frequently resulted in a 6ft high case instead of extending facilities with complete receiving terminal in a single add-on adaptor units, which, in the past, could be disengaged electrically to hold the receiver on any particular frequency. The digital frequency readout, derived from the local oscillator, although at first disliked by operators accustomed to dial and pointer indicators, was necessary if the accuracy of the synthesizer was to be exploited operationally. No traditional mechanical analogue dial could achieve a resolution of 10Hz at 30MHz and even the most conservative of the old-time operational advantages.

Another innovation was to provide a complete receiving terminal in a single case instead of extending facilities with add-on adaptor units, which, in the past, had frequently resulted in a 6ft high rack of equipment. Provision was made for six internal filters which could be fitted at the customers' choice. These filters were selected through transistor switching controlled by d.c. only from the front panel. This not only eliminated the potentially troublesome mechanical switching of r.f. circuits from the front panel but also simplified remote control.

Although an earlier receiver had been developed using plug-in modules it was decided in the interests of economy to use conventional construction in the RA 1770 series but the physical configuration allows all circuits and components to be accessed by test gear for fault diagnosis while the receivers are in an operating condition. By the mid-1970s the series had been extended to include programmable and remote control receivers. The programmable set, in addition to continuous tuning at three selectable rates (10 Hz, 20 Hz or 1 kHz), had twelve programmable channels selected from a front panel switch.

The receiver for extended or full remote control is in two units, the receiver itself with blanked-off front panel except for local test facility, and an associated remote control unit with all the front panel controls. The receiver is triple conversion with the third i.f. at 100 kHz. Apart from a spin-wheel tuner and rotary controls for b.f.o. setting and i.f. and a.f. gain, all other functions on the remote control unit are selected by push-buttons. Control is exercised by a time-sharing data-multiplexing system which converts parallel control information into serial form for transmission over single wire lines. For extended control of all receiver functions three cable pairs are required. For full remote control over virtually any distance standard data modems are used on an associated remote control unit with blanked-off front panel.

The system enables complete receiving systems to be built in which a single operator with one remote control unit commands several remote receivers.

Transmitters of the 1970s. Transmitter development in the past decade has not been as spectacular as in receivers. The digital synthesizer came into more general use for frequency control in drive units and remote control systems provided flexible extended and fully remote control. The most dramatic development was a solid-state power amplifier delivering up to 1kW of power (Fig. 2). This presented a great technical challenge, the problem as with solid state receivers being the inherent non-linearity of bipolar transistors which demanded careful balance at every stage. No single device could produce significant output and my company's approach was to employ eight modules, each of 125W output with combiners summing through hybrid units to 250W, 500W and finally 1kW. The system had to survive a module failure which necessitated some complexity in design to provide protection over a large frequency range.

The advantages of the solid state design were mainly in reliability and ease of servicing. The 30V supply rail was non-lethal (although it is of course still possible to receive a serious r.f. burn from the antenna terminal). In terms of reliability there was adequate redundancy, failure of a module merely reducing total power output and any of the eight modules could be replaced or worked on without interruption of service. 500W and finally 1kW were on the same principle but with only four 125W modules was also produced.

For higher powers the valve remains supreme in terms of economy and efficiency. One 10 kW transmitter of the 1970s period, still in production, was solid state in the drive stages with air-cooled semiconductor devices in the power stages. Automatic tuning, servo-driven, gave a typical tuning time of 8 seconds with a maximum output of frequencies of 20 seconds. Automatic level control was provided and the power supply had automatic overload protection with automatic re-set which would not finally lock out the supply in...
the case of a transient fault until four unsuccessful attempts at reconnection had been made.

The next ten years

Both technical and economic gains are anticipated in the decade ahead and in fact are already being realised. The market is highly competitive and it is clear that design trends will be towards better specification and more facilities per unit cost.

A positive example is an m.f./h.f. receiver which made its public debut in London in October 1979. It is a joint Anglo-American development and substantial orders have already been received from the US Air Force. The receiver (Fig. 3) has the overall performance of its predecessors at a far lower price, achieved largely by more functions per integrated circuit and therefore a smaller number of components. It is a double conversion superhet with the first i.f. at 40.455 MHz and the second i.f. at 455 kHz. Frequency and receiver status displays are liquid crystal and all functions are push-button selected, control being through a microprocessor.

The important innovative advance is the synthesizer. In the RA 1772, described earlier, there were five circuit loops constructed on four printed circuit boards. In the new receiver a single loop synthesizer occupies only one board and as well as generating the local oscillator frequencies at intervals of 1 Hz (previously 10 Hz resolution) it also generates the b.f.o. output in 10 Hz steps. Because of the single loop design the new synthesizer has even greater spectral purity because all mixing has been eliminated and thus fewer frequencies are being generated. The unit is based on an I.S.i. m.o.s. chip developed by Racal Microelectronics Ltd which achieved 1 Hz resolution by synthesizing phase as well as frequency. The UK version has a 100-channel frequency store and an interface for a remote control system. The US version has IEEE 488 input/output interfaces as standard, but both versions can be adapted for other interfaces by software changes.

Fig. 3. Anglo-American m.f./h.f. receiver. This recently introduced model uses a microprocessor for control and a new synthesizer.
The synthesizer mentioned above is also employed in a military wide-band receiver where it is used to cover the h.f./v.h.f. spectrum continuously from 2MHz to 512MHz.

On the transmitter front the advances that one will see in the 1980s are less spectacular but none-the-less worthwhile. A second-generation 1kW solid state amplifier uses four 300 W modules which, allowing for losses in the com- biners, delivers a full 1kW to the radiating system. Linearity has been further improved so that for the first time the CCIR recommendations for intermodulation products have been met over the whole of the h.f. range.

Looking further ahead there are two great hopes. One is v.m.o.s. devices which could provide much greater linearity than current bipolar devices, and of greater efficiency. The second is the feed-forward or polar loop concept on which research is being conducted at Bath University. If successful, there is a promise of solid-state transmitters comparable in efficiency and linearity with current class AB vacuum tube amplifiers.

Of more immediate note the world demand for low-cost channelised transmitters continues unabated, and it is now becoming apparent that the conven- tional channelised drive unit may well be displaced by a programmable synthesizer on economic grounds. With modern technology a synthesizer is already comparable in cost with a 10-channel crystal drive unit.

Receiver performance has now reached a new plateau but the application of the microprocessor will provide considerable refinement, resulting in more "intelligent" units in both systems management through remote control and the receiver itself. For example, there is the self-adaptive receiver already realised which senses the type of signal it is receiving and automatically adjusts itself by minor frequency shift and selection of appropriate filters and demodulators to the transmission mode it is receiving without operator intervention. If on c.w. it would probably select the narrowest filter and adjust the b.f.o. frequency for a pleasant tone, and audio gain to a convenient level, for recording or operator con- venience. If s.s.b. is detected then the appropriate upper or lower sideband filter, and so on. The microprocessor will also be used for routine self- checking of sensitivity and other parameters.

The newer techniques pioneered on h.f. are already producing a spin-off at higher frequencies, particularly the concept of a high first i.f. which opens the door to broad band pre-mixer amplification. High stability v.h.f. syn- thesizers will also allow s.s.b. on v.h.f. and u.h.f., thus enabling more efficient use of the spectrum as has happened on h.f.

We may also expect new forms of modulation which will help overcome the inherent limitations of ionospheric propagation. There could be re-births such as the Piccolo system, where the advent of solid state circuitry has made the system economic enough to attract much wider application.

Work is currently being conducted on topics such as time encoded digital speech at 2.4 kilobit/s and, though presenting considerable technical dif- culties, few professionals doubt that such developments will eventually prove successful and further enhance communications at h.f.

Although for purposes of illustration the practical examples quoted are all from the author's own company, he gladly acknowledges parallel work in other countries which, through pro- fessional cross-fertilisation, will con- tinue to advance the art and science of h.f. radio.

**Electronic measuring instruments**

**by John L. Minch **Hewlett-Packard Company

Progress in instrumentation is a result of at least three driving forces: the on-rush of new system requirements such as fibre-optic communications and satellite technology, 'breakthroughs' in component technology, such as micro- processors or microwave, hybrid microcircuits; extensions and combinations of present instrumentation, such as the remarkably successful IEEE-488 interface bus for programmable systems. Very often, progress is really an intricate combination of all of the above. In so many cases successful instruments don't involve technology 'breakthroughs', but merely embody the right combination of customer requirements. With few exceptions, most of these requirements were already in place at the beginning of the decade. Digital, analogue, and microwave integrated circuit techniques' advanced substantially, but the primary technology was already there.

The 1970s

Dramatic progress did take place during the 'seventies. Probably the most important new developments were of logic analysers and logic design instru- ments. The earliest of these, typified by the HP 1601L introduced in 1973, was nothing more than a standard oscilloscope display with columns of Os and Is. An early serial data analyser, the HP 5000A, permitted diagnostics on long streams of data captured and displayed on rows of 1.e. ds. In the six years since, the progress in logic analysers and microprocessor design instruments has been nothing but breathtaking. And none too soon either, because relentless marketing pressure is pushing microprocessors well beyond the obvious applications in calculators and communications into appliances, toys, electric organs and motor cars. Design, qualification, production test, maintenance and service all need these measurement tools to work with microprocessors and digital circuitry.

One common theme of the 'seventies for most classes of instrument was that requirements moved two ways at once. Thus, the market called for smaller, more portable and less expensive models at the same time that other models went as far as technology would allow, with highly complex and powerful instruments and remarkably high price tags. An example of the former is the low-priced, digital voltmeter, while the high-priced example is the HP 3455A, a high-precision, system d.v.m.

Oscilloscopes handled higher frequencies and became both smaller and more portable, while others became much more powerful and complex, using microprocessors to measure digital time delay or rise times. Waveform, pulse and function genera- tors tended to go in only one direction — towards smaller and cheaper designs, but with remarkably strong specifications. It's amazing how much waveform performance can be packed in a small package these days. The more complex pulse-generator products usually were the word and coded-pulse instruments.
required by new digital communications technology and fibre-optics.

**R.f. and microwave.** R.f. and microwave instruments entered the 'seventies with great promise. In 1970, hybrid microcircuit technology and the design processes using scattering parameters were in place, ready to supply the building blocks; G.a.s.f.e.t. devices were coming. The results were truly astounding. The microprocessor has made the difference — about half the circuits in many microwave instruments are now digital and it comes as no surprise that about half of our microwave design teams are digital and software designers.

A typical result is a newly-introduced synthesized signal generator. The 10kHz-1280MHz signal spectral purity of this generator rivals the best cavity-type generator of previous years, but it is also fully programmable and frequency agile (500µs switching time). The real contribution of this very expensive generator is in the design of the front panel controls. The mostly digital keyboard communicates only to the microprocessor, which does all the circuit and signal control, making things extremely easy for the operator. For example, he can set up ten completely different front-panel signal conditions, store each, and recall them at the push of a button.

Another example of this "smart" type of microwave instrument is a recent 1500MHz spectrum analyser. Starting from power switch-on, the machine runs through 30 self-tests and draws its own graticules and titles, and provides powerful measurement routines which are far beyond usual manual testing. Self-tuning routines bring identified signals to the centre of the screen and read out frequency and amplitude digitally. Sweep speed, bandwidth and read out frequency and amplitude signals to the centre of the screen and the display will then show only new signals which show up later.

R.f. network analysis finishes the 'seventies with a typical instrument, covering 500 kHz to 1.3 GHz, which measures, calculates and displays complex impedance transfer functions, group delay, deviations from linear phase, etc. It's about all the design power an r.f design engineer needs.

**Fig. 3.** 110MHz spectrum analyser employs digital storage, a television type display and automatic operation to give accurate spectral information quickly and easily.

**Fig. 2.** Synthesized signal generator provides precision r.f. signals and, being bus-controllable, may be incorporated into a fully automatic test set up.

In instrumentation, the 'seventies brought one development which probably overshadows all other advances in instrument techniques — the IEEE-488 bus. Interestingly, the IEEE bus was not a technological breakthrough; it was really more of an organisational and political advance. A simple data party line allowing automatic control of instruments and resulting data computations has revolutionised measurements already: over 700 instruments and controllers from over 160 manufacturers throughout the world now operate on the bus. Engineers now think in terms of automatic measurements for labs and production and maintenance uses.

**Servicing.** Finally, in the late 1970s, a more coherent strategy for dealing with service and repair of digital circuits was emerging. Early attempts at field diagnosis and repair of 'digital' boards placed the emphasis on changing the board. When the total number of instruments in service was small and widely scattered, the organisation to make this feasible was difficult.

One solution gaining rapid acceptance now is a design strategy based on signature analysis of digital circuitry. Instruments with a high content of digital components are designed with a certain portion of the microprocessor set aside to be used in fault diagnosis. In that test mode, the instrument circuitry is forced through a switching procedure which causes each digital circuit node or pin on a digital logic pack to produce a sequential stream of 0s and 1s. That repetitive pattern is unique to that pin of a good instrument. Thus a signature analyser like the HP 5004 takes a bit stream as long as 216 bits and compresses it into a 4-digit alphanumeric display. Instruction manuals and test procedures are written to measure and assign a unique 4-digit signature number to every digital circuit pin. Technicians can quickly troubleshoot right down to a component level, picking out faulty i.c. packs with little trouble and alleviating the serious problem of stocking complete p.c. boards.

**The future**

Forecasting the future is always risky, but the clues to the next five years of instrumentation are already apparent from the most recent offerings.
Alternative digital methods will continue to invade analogue and r.f. techniques. For example, instead of a super-accurate, flat-frequency-response r.f. attenuator for use in signal generators, a signal generator will use a moderately-accurate but highly stable one: a highly-precise calibration table stored in memory then corrects the output signal. This is effective and inexpensive so long as there is already a microprocessor available.

It seems quite clear that analogue and radio-frequency circuit techniques will be further eroded by digital methods. As faster analogue-to-digital converter components come along, instruments will sample and convert signals to digital form forward in the measurement process. Output signals may be more commonly generated by digital waveform synthesizers. For example, oscilloscope sweeps would be much more accurate if generated digitally by a clock whose frequency was referred to a crystal standard.

Systems. Systems engineering will call for new initiatives in measurement which will create new instrument concepts. Communications systems are moving rapidly to digital modulations. Signal simulators will be needed for generating phase-shift-keyed modulations for satellite work as well as frequency agile signals for the new military communications and the cellular mobile telephone technology.

Fibre optics technology's on-rush into communications, in spite of its highly optimistic projections, has been underestimated: few people really see its impact clearly. The bandwidths of communication power to be unleashed by fibre optics will revolutionise not only the system business but will change instrumentation. Fibre optic data links can already link IEEE-488 bus instruments. Computer and terminal links as well as medical data transmission with no ground loops are just the beginning. These technologies will call for design and test equipment not yet envisaged. More importantly, they will call for new concepts in measurement.

The computer system technology will have memory and processors in every corner. Instrumentation will more than adapt: there is very heavy interaction between logic design instrumentation and the semiconductor revolution itself.

Fig. 4. Each pin of a digital i.c. pack has a unique 4-digit signature displayed and referenced in the repair manual, allowing diagnostics down to a component level.

Certainly, computer-aided design for assistance in lab. projects becomes common. Engineering productivity is the key: in the 'seventies, automatic test equipment found willing ears for production test and for lowering costs — it was easier to justify.

The 1980s must attack the design side of things. Technology moves so fast that any lab. project which lasts longer than three years is going to produce a product with old or obsolete technology. As a result, there will be a steady proliferation of IEEE-488 bus minisystems in laboratories. New instruments will appear with more operator-interactive controls and displays which interact, compute, correct and translate into your terms.

Complicated measurement procedures will be captured in software so the same tests can be re-run two weeks later. Suppose you run a particular test as you complete your circuit bread-board. Two weeks later, after modifications, you would like to recall the same procedure, set up all front panel settings as they were, run the test and compare the data to the previous test. This may sound a little like the HAL computer from the movie 2001, but it isn't; the technology to do that is here now in IEEE-488 bus systems. Now just contemplate individual instruments doing much of the same.

How will we maintain all this equipment? One computer maker recently proposed throwaway p.c. boards as a repair strategy; that might happen. Super-integration and high-reliability test programs could well give a substantial advantage in reliability. But the usual reaction to that is to pack even more complexity into the instrument functions, putting instrument reliability back where it started. Smaller, less costly, highly digital instruments will get more reliable. Larger, more complex, high priced instruments will hold their own on reliability. The most likely course will be a combination. With maintenance labour rates bound to increase, there may be some trends towards the throw-away-type repair on very low-priced instruments. In higher-priced equipment the instrument will contain more self-test and diagnostic capability, under control of its own microprocessor: that trend is already apparent. Then when the self-test has isolated problems to a given module or p.c. board, the digital signal analysers will take over.

Instruments in ten years will still consist of printed-circuit mother boards and plug-in modules. But p.c. board testing which has focused mostly on production functions may gravitate to maintenance depots where repair quantities can justify the cost. The new super-flexible automatic board-test systems are becoming attractive because of their remarkably low prices.

So, get ready for some technically exciting times. The surface has barely been scratched.
"Make way for engineers"—IERE president

The normal fabric of British life will have to be substantially changed, claims Professor William Gosling of the University of Bath, if we are to create an engineering profession adequate to the needs of our society. Giving his inaugural address as new president of the IERE, he said that we urgently need "an elite corps of engineers, particularly electronic engineers, who will be as able, perhaps abler, than any others in the world. To induce the most talented people to seek such a life, society will need to use the only inducements which have ever been known to work, namely honour, prestige and wealth. They will also need a good 'second division' of supporting engineers, of technician engineers and technicians. At each level of employment the appropriate rewards — tangible and intangible — to secure the quality and numbers to meet our social needs must be forthcoming. Such things are not achieved cheaply, but only by the diversion of resources in the appropriate direction. Since, the wealth of society cannot immediately increase, even with the most favourable industrial policies, we are faced with a stark logic. If we need better engineers, more able to facilitate the creation of wealth by industry, we must make that career more attractive to the ablest of our children. To do that the rewards must be markedly improved. But if the very best engineers grow richer, everybody else, including all the other engineers, the trade union members and the arts graduates, must for a time see their prosperity grow less rapidly than would otherwise have been the case. This is a high hurdle for us all to get over, particularly in a society largely run by a collusion of arts graduates and trade unions, which has developed a marked predilection for living on its seed corn."

In a reference to the Finniston inquiry into the engineering profession, Professor Gosling said that nothing that could conceivably come out of this will change overnight the whole status and remuneration of engineers. "Maybe if engineers could be organised into a tight and monolithic union, and if they exploited their power ruthlessly and without regard for others, a change of that magnitude could be achieved. So far, engineers have for the most part not shown that willingness to unite themselves, nor yet to their credit the extreme degree of ruthlessness and militancy. We may be sure that what they have not been prepared to organize themselves for and force from society, they will not be given unasked, from some kind of altruistic recognition of merit. We do not live in that kind of world."

Japanese see opportunity in Prestel

Only a month after Prestel, the Post Office's viewdata system, started as a full public service (December 1979 issue, p55), the Japanese firm Sony displayed in London some equipment it has specially developed and manufactured for this information retrieval service. Shown by Sony (UK) Ltd at the Professional Viewdata Exhibition in November, it consists of two 14-inch colour television terminals using the famous Trinitron tube (December 1971 issue, p.587), one with a simple keypad and the other with a full alpha-numeric keyboard. Editing will be possible on these terminals. The equipment was developed at Tokyo and at the Sony (UK) manufacturing plant at Bridgend, Wales, and is assembled at Bridgend.

Speaking of his company's involvement in Prestel, Mr Kazuo Imac, of the Commercial and Industrial Division, said: "As well as being the first Japanese company to develop Prestel equipment, we have considerable investment in viewdata technology and this Prestel equipment is only the first of many developments to come." It will be remarked that this Japanese company seems to show considerably more enthusiasm for the system than the television set manufacturers in the country where Prestel was born. The British set makers have been well behind schedule in supplying viewdata receivers ordered for the test service started in September 1978.

"Engineers want statutory registration"—survey

A survey has revealed that professional electrical and civil engineers are overwhelmingly in favour of a statutory registering authority for the professions. The survey, carried out by NOP Market Research Ltd for the Institution of Electrical Engineers, questioned IEE and ICE members on their attitudes towards their professions, standards, and the way qualified engineers were perceived by society. It found that 92 per cent of IEE members favoured registration while the figure for the Civils was 87 per cent. The registering authority should be responsible for the registration of professionally qualified engineers (said 92 per cent IEE, 93 per cent ICE) as well as exercising control over the standards of education, training and qualification (80 per cent IEE, 72 per cent ICE) and professional conduct and discipline (78 per cent IEE, 79 per cent ICE). Virtually all members questioned believed that the registering authority should have the right of sanction against an individual if professional standards were not maintained.

It should be compulsory for all professional engineers to become registered (said 58 per cent IEE and 65 per cent ICE). A further fifth thought registration should be compulsory above a certain level of responsibility. However, if registration wasn't made compulsory then 79 per cent (IEE). 71 per cent (ICE) said they would apply anyway.

Not only did the majority favour registration but 67 per cent of both institutions believed that work requiring a high degree of responsibility should only be undertaken by registered engineers. When it came to the way the profession was perceived by the public, 97 per cent (IEE), 98 per cent (ICE) stated that "the public have little knowledge of the engineering profession." On the question of pay, 91 per cent (IEE), 88 per cent (ICE) said that they believed they were paid less than others in similar professional occupations. An overwhelming majority stated that engineers had achieved a higher professional status abroad than in the UK. The questions were posted to a random sample comprising 4,400 corporate members of the IEE and 600 of the ICE, and the overall response rate was 52 per cent.

Japanese companies, Mullard Ltd, General Instruments, Texas Instruments and VG Electronics, demonstrated the British teletext/viewdata system in Tokyo on December 10 and 11. The object of the presentations was to show the advantages of the system's components and sub-assemblies to Japanese setmakers who undertake, or plan to undertake, the manufacture of suitably-adapted TV receivers in the UK or Europe. The presentations were organised by the British Overseas Trade Board. The Sony terminals mentioned above in fact use Mullard viewdata integrated circuits.

Arts competition

The Royal Society of Arts is including an audio-visual presentation in its 1979/80 Design Bursaries Competition, which this time will offer awards to the value of £20,000. In the audio-visual presentation section, students and young designers are given the opportunity to develop their technical skills and to apply their visual imagination to animating a sequence of ideas by means of lasers, holograms or any other audio-visual method. Further information may be obtained from the Royal Society of Arts, John Adam Street, Adelphi, London WC2N 6EZ.
Hospital paging using synthesized speech

A new microprocessor-controlled radio paging system, recently installed by Multitone Electric Company Ltd at Frenchay Hospital near Bristol, includes synthesized speech. Multitone's ACCESS 1800 paging terminal has enabled the hospital to organise several group alert sections of staff and considerably speed up the connection of one member of staff to another by telephone without using the switchboard staff.

ACCESS 1800 enables simultaneous calls to be made to as many as 12 team members in up to ten teams including the cardiac arrest team, a mobile resuscitation unit, and major accidents and fire teams. A member of staff can locate any receiver holder by simply dialling an access digit on any telephone, followed by the receiver number and the caller’s extension number. He may then hang up the phone. A “bleep” will be heard by the receiver holder who, upon pressing a button, will then hear a synthesized speech message giving the caller’s extension number. The switchboard is not involved in this at all. The cardiac arrest team can be alerted and mustered within seconds to a particular ward by a verbal message over their receivers. Similarly, the mobile resuscitation unit can usually be mobile in about 30 seconds from the origination of a call from the switchboard.

Thirty calls may be stacked in the computer’s memory and automatically processed in sequence, even when interrupted by a priority call. Any temporary change of receiver number, for staff on call, can be programmed into the memory, which will automatically call the alternative number when the original, unobtainable number is dialled. If one doctor is unobtainable, a second on-call doctor can be summoned automatically in his place. This call transfer system eliminates the need to inform all staff of the change of number when any receiver is exchanged.

Pseudo-direct satellite speculation

Mr Pat Hawker of the IBA, speaking as a ‘devil’s advocate’—his own words—at a meeting of the Society of Cable Television Engineers on October 16, posed the question “What would happen if a commercial company in Luxembourg were to use lower-power satellite positioned at 19° W (the orbital position allocated to Luxembourg) on the appropriate 12GHz channels and carrying a stream of bought-in programmes in the English language?” Speculating, he said, “Such transmissions would be picked up in the UK.”

A small number of enthusiasts, according to Mr Hawker, would undoubtedly be capable of making their own equipment to receive these transmissions and sell or give it away for community distribution. For good quality reception, he said, they would need efficient satellite receive-only terminals with — for 12GHz, possibly 1.5, 2 or at most 3 metre dish aerials and these, while requiring greater profile accuracy, would not necessarily be any more expensive than the 4.5 metre dishes used in the USA. According to a recent press report, he said, enthusiasts in North America had managed to receive tv from Westar and Satcom Systems, mainly to mining and timber camps. The report said that Canadian government officials had estimated that 50 unlicensed stations were involved, but their operators were not shut down because the government had difficulty in locating them and there was a genuine danger, according to an official, that the lumberjacks and miners would resist with force.

Reminding his audience that Radio Luxembourg had been carried on cable, Mr Hawker posed a second question, “Would British cable networks be permitted to distribute programmes from France, West Germany or Luxembourg?”

“It would need Home Office approval,” he said, “but as Erik Jurgens, chairman of the Netherlands Broadcasting Corporation has pointed out, there is Article 10 of the European Convention. This states: Everyone has the right to freedom of expression. This right shall include freedom to hold opinions and to receive and impart information and ideas without interference by public authority and regardless of frontiers. This Article shall not prevent States from requiring the licensing of broadcasting, television or cinema enterprises.” Mr Hawker suggested that such an Article posed the question: “The system of transmission used in most other countries would certainly cause interference, and shouldn’t be used in the UK. There are other systems (e.g. v.h.f./f.m.) that would be much less troublesome — but the problem of interference is undoubtedly important, and more research is needed to ensure that any chosen system would be satisfactory.”

CA for CB

The Consumers’ Association have come out in favour of introducing a citizens’ band radio service in the UK. In a one-page summary of the arguments for and against in the November issue of their magazine Which? they conclude: “Citizens Band radio in this country may not save many lives, nor may it be the best way of relaying traffic information. But it could provide an easy-to-use, relatively cheap method of communication that many people would find useful to have on occasions. We’d like to see it available here, if the problems of interference can be overcome.”

The Association maintains in fact that the possibility of interference with other electronic equipment is the only serious argument against the introduction of c.b.: “The system of transmission used in most other countries would certainly cause interference, and shouldn’t be used in the UK. There are other systems (e.g. v.h.f./f.m.) that would be much less troublesome — but the problem of interference is undoubtedly important, and more research is needed to ensure that any chosen system would be satisfactory.”

SERT move

German press considers higher frequencies for c.b.

Conditions on the 27MHz citizen's band are giving users cause for concern and every day there are new calls for better operating conditions. The German electronics journal, Funkschau, therefore carried out tests and compared some alternative bands to get acquainted with the advantages and disadvantages of each one as far as c.b. was concerned. Their findings showed that shifting c.b. into the v.h.f. or u.h.f. region could produce considerable advantages. It would cause much less interference to home-entertainment equipment, and the substantial increase in the channels which could be used would put an end to the present overcrowding.

Because special permission is required in West Germany to use frequencies around 900MHz, this band could not be included in the tests. Instead the 23cm amateur band (1295MHz), which has similar propagation characteristics, was considered, together with the 70cm (435MHz) band and the current 11m (27MHz) band. On the 11m band they found that there was always heavy interference from vehicles in country districts, further south and from industrial generators, while on v.h.f. and u.h.f. only noise could be heard. The tests were carried out using omnidirectional antennas with no gain and power levels of less than 1W.

For propagation comparisons the different types of terrain were considered. Munich was chosen as a heavily built-up municipality, the Upper- Bavarian lakes were used for propagation over areas of water, and the hilly country in the north of Munich enabled trials to be done over undulating terrain. As expected, the poorest ranges were observed in the 22cm band, and usable ranges could not be achieved until a station arrived at an exposed location. Penetration was good on this band and radio contact was not even lost when one station moved into a garage. In the city of Munich, the "phase wipeouts" from passing vehicles proves a great nuisance, and it was concluded that diversity reception could help in this case. It was the journal's experience that the 23cm band could only be of value for c.b. radio if repeater stations were set up on high buildings or mountains, and it would also be necessary to obtain approval for high-gain antennas.

US noise jammer simulator to be made by UK company

A contract, valued at more than $4 million, to build the US Navy a noise jammer simulator, has been awarded to Watkins-Johnson the Windsor-based electronics company. The order, which comes from the Naval Weapons Centre at Dahlgren, Virginia, gives the company the responsibility of designing, manufacturing, installing and activating a computer-controlled system capable of emulating hostile jamming environments. When completed in 1981, the simulator will be used at the Atlantic Fleet Weapons Training Facility to provide electronic counter-countermeasures training for Navy radar operators.

More v.h.f. broadcasting likely

The v.h.f. sound broadcasting band in Region 1, at present 87.5 MHz to 108 MHz, will almost certainly be extended upward to 104 MHz as a result of a decision at WARC 79, we understand. In Britain, for example, this will allow an extension of BBC and IBA local radio services, will avoid the necessity for sharing between BBC Radio 1 and Radio 2, and will reduce the need for some Radio 3 and Radio 4 programmes to be displaced by educational broadcasts (see article by D. F. Leggatt in this issue). To permit this extension of broadcasting, the police radio communications at present occupying 100-104 MHz will have to be moved elsewhere but it is not yet known what frequencies are likely to be used.

Apart from this loss, mobile radio in Region 1 has benefited overall from the decisions at WARC 79. At the time of going to press we understand that unofficial sources that this service will be allocated sections of the spectrum which it has not had the use of before. In Britain one of these sections could well be part of Band 3 (806-960 MHz) which is at present used for 405-line television broadcasting by both the BBC and IBA, but what happens here will in fact be an internal UK decision made by the Home Office. The BBC hint that the remainder of Band 1 could perhaps be used for the new direct digital radio broadcasts.

It seems there has been something of a conflict at WARC 79 between the USA and Canada over the allocations for services in the u.h.f. bands in Region 2. Because the heavily populated areas of Canada are close to the US border it is obviously necessary that the two countries use these bands in the same manner in an integrated way to avoid interference. Canada wants to use the u.h.f. bands exclusively for television broadcasting (the present exclusive allocation for this service being 470-890 MHz), partly because it has a large number of language groups to cater for both native peoples and immigrants, while the USA wants a more flexible arrangement in which they are shared with mobile radio. For example, the land mobile radio community in the USA recommended a co-equal mobile and broadcasting allocation between 470 and 806 MHz to provide flexibility in the international table of allocations and leave the domestic u.h.f. television allocations intact to the degree that is necessary. At the time of going to press we understand that the Canadian case is getting strong support from other delegations, but the issue is not yet settled.

Impulse buying by hi-fi customers

A consulting firm, Venture Development Corporation, from Massachusetts, claims that there is a link between the time spent by a customer selecting a radio set and the amount of money spent by the manufacturer. The Corporation says that hi-fi buyers sometimes have a lot in common with new car buyers in that they need a lot of information, they often price shop, and they frequently require substantial psychological support. At other times, it says, the hi-fi buyers behave like chewing gum buyers, needing very little time to make a brand selection and being completely pre-sold on a particular product. Price did not seem to be a critical factor as long as the merchandise was available.

The consulting firm compared the owners of systems costing $1400 or more with owners of systems costing less than $800, and found that 72.7% of the owners of high-priced systems spent at least a month selecting component brands, but only 37.2% of low-priced systems owners spent that long. Two factors accounted for this, according to the firm. Firstly, the larger the purchase, the more the people were willing to invest to guarantee an optional selection, and secondly, the more expensive systems had more features requiring consideration, making the final choice more complicated.

20.7% of the owners of systems worth less the $800 decided on their components within one day or less, and only 4.2% of the owners of high-priced systems were able to make a purchase in the same time. The Corporation claims that the implication for retailers is clear. They should not rush the sales of high-priced merchandise. Product literature, specification sheets and reprints of reviews should be readily available for customers to consider at their leisure, and the higher the price, the more information should be offered.

V.o.r. computer

Walter Freter, who is a member of the Munich gliding club and the Siemens (Munch) amateur electronics group, has developed an automatic v.h.f. omnirange (v.o.r.) receiver, using a microprocessor to calculate and display the required compass bearing. Normally, the pilot of an aircraft is required to look up the frequency of the selected v.o.r. beacon, tune his navigation receiver and set the omni-bearing selector, observing the left/right indications of the display and adjusting the heading to keep the needle centred.

Freter's design avoids all this by virtue of its programmed table of all European frequencies, and the power of its microprocessor to tune the navigation receiver to the beacon transmission. The processor will calculate the required compass course to fly, using the left/right information which would normally be displayed, and will show the continuously up-dated compass course on a numerical display on the control panel.

Siemens say that several manufacturers (not Siemens?) have shown interest in the equipment.
Past the peak?
By the time these words are published it seems likely that the peak of Solar Cycle 21 may have passed — although this will not be known for certainty until 1980. Long-distance paths on frequencies up to and above 50MHz reappeared in mid-October with many cross-band (50MHz/28MHz) amateur contacts between Europe and North America. The season appears to have opened on October 18 when American 50MHz signals were received in West Germany. The amateur station, G3SSO, operated by personnel at GCHQ, Cheltenham is thought to have been the first British station to make such a contact this autumn, working Canadian VE1AVX on October 19. RSGB advises that 28.875 - 28.895MHz has become established as the frequencies for cross-band s.s.b. operation with 50MHz North American stations.

The sunspot peak has been reached sooner than expected, although if the cycle follows the usual pattern, the decline will be considerably slower and several more seasons of 28MHz (and possibly 50MHz) long-distance bands and other "openings" appear likely. The past decade has shown once again the great difficulties experienced by radio physicists in accurately predicting, except in the short-term, the dates of maxima and minima and the level of maximum sunspot activity. Perhaps the most interesting new theories to emerge recently are those of Professor R. H. Dicke of Princeton University who believes that the cycles are accurately timed deep inside the sun by a form of magneto-fluid oscillator but take varying times for the magnetic fields to reach the surface; he also espouses the theory that the true solar cycle last 22 years with a reversal of magnetic field polarity at 11-year intervals.

The first G/YL
Miss Barbara Dunn, G6YL, who died recently, is generally believed to have been the first licensed 'YL' ('young lady') amateur operator in the UK and held her licence for over 50 years. Throughout the 1930s she was one of the small group of British 'YL' operators who were tremendously active on the long-distance bands and in pioneering both 28MHz and the old 56MHz bands. Even in 1937, ten years after she took out her licence, there were only five 'YL' amateurs in the UK: Nell Corry, G2YL; Constance Hall, G8LY (still licensed); A. J. Burns, GM2IA; G6SF; and Barbara Dunn — though these were joined soon afterwards by Catherine Myler, G3GH, who later was one of the very few amateurs to receive official recognition for their work as Voluntary Interceptors in the Radio Security Service.

Foxhunting
One of the aspects of amateur radio that continue to attract a small but faithful and enthusiastic following is the art of locating hidden stations by the use of direction-finding receivers. For many years the RSGB has organized a series of "qualifying events" leading to a "national final" based on transmissions in the 1.8MHz amateur band. For the qualifying events, competitors are expected to locate two different hidden transmitters within about a ten-mile radius of the starting point, but for the national final it is a question of finding three stations in a matter of a few hours. The 1979 winner, Eric Mollart of the Mid-Thames Club, took only just over two hours to do this, in spite of the many ingenious difficulties that tend to get built into the course as a result of past experiences. The technique which has been used at several events is to have an extremely long aerial which even when located may apparently lead nowhere. At Wolverhampton, in one of the 1979 qualifying events, for instance, one transmitter had several hundred yards of fine wire suspended in the trees as aerial, but with a final length tacked under the horizontal rails of a fence, eventually leading to gorse bushes in which the operator and his transmitter were concealed. The d/f bearings thus led the competitors only to a wooden fence with no sign of the concealed station.

A rather different form of 'foxhunting' using the 144MHz band, is also organized, for example, by the UK FM Group (London), though one gains the impression that care is taken to ensure that it can be combined with the objectives of the Campaign for Real Ale!

In brief
The USSR is planning to launch an RS3 amateur radio satellite during spring or summer 1980. King Hussein of Jordan (JY1 and G5ATM) recently met 45 members of the Radio Society of Harrow at a reception given by the Mayor .... Richard Thurlow, G3WW has become the third amateur in the world to obtain a CQDX award for working 100 different countries on slow-scan television (No. 1 was W8YEH, No. 2 G3IAD). Japan is now issuing amateur callsigns in the JM prefix series. The VHF Committee of the RSGB has recommended 146.500MHz as a "calling frequency" for amplitude-modulated transmissions.
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BRIEF SPECIFICATIONS MODEL 2035A & 2037A

<table>
<thead>
<tr>
<th>DC Volts</th>
<th>5 ranges 100 µV to 1000 V</th>
<th>0.1% ± 1 digit, 0.25% ± 1 digit</th>
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<tr>
<td>AC Volts</td>
<td>5 ranges 100 µV to 1000 V m</td>
<td>0.5% ± 1 digit, 1.0% ± 1 digit</td>
</tr>
<tr>
<td>DC Current</td>
<td>5 ranges 0.1 mA to 2.00A</td>
<td>0.25% ± 1 digit, 0.5% ± 1 digit</td>
</tr>
<tr>
<td>AC Current</td>
<td>9 ranges 0.1 mA to 2.00A</td>
<td>0.5% ± 1 digit, 1.0% ± 1 digit</td>
</tr>
<tr>
<td>High Ohms</td>
<td>6 ranges 0.1 Ω to 20 MΩ</td>
<td>0.2% ± 1 digit, 0.5% ± 1 digit</td>
</tr>
<tr>
<td>Low Ohms</td>
<td>6 ranges 0.1 Ω to 20 MΩ</td>
<td>0.2% ± 1 digit, 0.5% ± 1 digit</td>
</tr>
<tr>
<td>Temperature**</td>
<td>10 ranges -50°C to +150°C</td>
<td>1°C to 2.5°C</td>
</tr>
</tbody>
</table>

Input impedance: 10 MΩ + DC and 10 MΩ/100pF - ACV
Burden voltage: 100 mV at 1000 display
Over voltage protection: 1000 V (DC + AC peak)
Over current protection: 2x250 V fuse
Ohm overload protection: 250 V DC or AC peak
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Battery life (8V): 200 hours typical with alkaline battery
Weight: 11 Oz (310 gms) without battery.
Accesories supplied: Test leads
Temperature Co-ef: 0.1% /°C
Display: ½" (13 mm) Character, 3½ Digits Liquid crystal display with low battery indicator, and «—» sign
Case colour: Light grey with matching buttons.
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WIRELESS WORLD, JANUARY 1980

WWW - 057 FOR FURTHER DETAILS
Practical parallel-tracking pickup arm — 2

Optoelectronic servo control gives low-inertia, fail-safe operation

by Rod Cooper

Despite the many advantages of the parallel-tracking record deck, the high cost of owning one deters all but the well-heeled few. This prompted the design and construction of a pick-up arm and control system with simplicity of construction specifically in mind. By avoiding complex engineering it is possible to construct the design with non-specialized tools in about 40 hours and for a fraction of the cost of a commercial item.

WHilst ACCESS to a lathe makes construction quicker and easier, it is quite feasible to make all the parts with tools normally found in a small workshop. An electric drill and stand, some BA taps and dies and a selection of metal cutting files and saws are however essential.

Both the tracking arm and reference arms are made of thin-wall Duralumin tube, readily available from aeromodel shops. One end of the tracking arm is plugged with a tight fitting brass rod and glued into place with Araldite. This serves to strengthen the fragile tube where the vertical pivot goes through, and provides some degree of counterbalance.

Constructors will notice that the positions of horizontal and vertical pivots have been transposed, compared with the conventional arrangement. Having the vertical pivot on the tracking arm is not good practice on a conventional arm of course, but is permissible here because the tracking arm on a parallel-tracking machine does not swing on the pivot more than half a degree, whereas the conventional must swing through a wide angle. The change enables an unusual design of horizontal pivot to be used — one that allows the tracking arm assembly to be easily taken off for transport or adjustment without having to dismantle anything, and allows replacement without having to re-align it with the reference arm. There are other advantages to this design, namely: it is much easier to make than the usual spindle type, it is virtually friction-free, needs no lubrication, has no play due to bearing clearances and does not introduce play due to wear.

Avoiding play is important because the control system cannot distinguish between play and tracking error. It is for this reason too that the sliding platform is spring loaded, so that any running clearance in the track is taken up. Diagram 3 shows the horizontal pivot design. Two adjustable screwed pivot points rest on top of two support pillars, one in a slot and the other in a conical cup on the opposite side of the gimbal ring. The arrangement is quite stable, provided the two pivots are far enough apart.

The vertical pivot is straightforward. Adjustment for inclination is by means of the brass plate which forms the upper bearing, and which can be moved around on the flat top of the gimbal ring to the correct position.

The track in Fig. 4 can be cut with a small hack saw and then filed to the exact dimensions. It is worth spending some time ensuring the track is straight, as the whole concept depends on the reference arm maintaining a constant angle to the tracked radius of the record. Also, it is essential that the carriage slides without any hard spots. It is not necessary to produce a perfect fit, as a small amount of slack will be taken up by the spring-loading.

To reduce wear, a few drops of clock-oil (which has good non-gumming properties) can be applied to the vertical pivot, the lead screw and the running surfaces parallel track. Don’t use mineral oil sold as general-purpose or light machine oil because it thickens to a gum after a while.

The hinge pivot holder part 14 is soldered in position to the lower plate, part 11. The best way of doing this is to pre-solder both plate and holder; with a length of 6BA rod through both holders, position them the correct distance apart and place them on the plate, and gently heat the plate from below. It is then quite easy to move the two holders into the exact position while the solder is molten; excess solder will cause holders to float out of place, so use the bare minimum.

For the sake of simplicity, the counterweight on the prototype was made from a piece of lin diameter brass bar drilled through the centre and decoupled with a foam rubber insert. However, the comments by Randhawa on counterweights (WW April 1978 pages 63-8) should be noted by constructors as a better design is probably possible. The main requirement for the counterweight is that it should give neutral equilibrium with the chosen cartridge when the tracking arm is positioned about half way up the vertical pivot.

The photocell holder was filed from a piece of solid engineering-grade p.v.c. which is particularly easy to use, but
other reinforced or filled plastics such as Tufnol would probably be suitable. The two photodiodes were cemented to the holder with Araldite. An aluminium shim separated the diodes, this being necessary to prevent light from one diode reaching the other by reflections via the transparent sides of the BPW34. The size of the shim is not critical but for good light cut-off between the diodes it should project 15in or so all round.

A shroud was made from the same shim material to clip onto the holder. It is best if this is eventually fixed in place with Araldite when the system has been proved to work satisfactorily. Beer and soft drink cans are a good source of strong, thin aluminium. It is important that the weight of the holder and shroud is kept as low as possible to preserve the low inertia of the tracking arm.

Regarding the finish and appearance of the self-made metal parts, both polished brass and aluminium can be protected from tarnish by Letraset aerosol spray No. 101. This provides quite a tough, abrasion-resistant transparent film which is almost undetectable.

Fig. 4. Lower assembly comprised lead screw arrangements as shown, together with drive mechanism pictured in December issue.

Fig. 3. Improved design of upper assembly differs from author's original as shown in photographs.
Note that spigot on part 22 in Fig. 4 has projecting part filed to fit loosely in slider, part 19.
Wiring to the cartridge, opto-switch and filament bulb is made with 3x48swg Litz wire. There seems to be no readily available alternative to Litz wire which is flexible enough for the job. The cartridge and opto-switch wiring is carried inside the tubular tracking arm, exits near the vertical pivot and is firmly clipped to the back of the upper platform. From here the cartridge wiring is kept apart and carried in p.v.c. sleeving to a 16 pin dual in-line plug and socket on the plinth. The opto-switch wiring is combined with the wiring from the bulb and carried in separate p.v.c. sleeving to the socket. This arrangement gives a neat and symmetrical layout and helps prevent the lead-out wires from fouling the gimbals.

The T1½ filament bulb is the only commonly available bulb which will insert into the standard ¼in diameter tube. It should not be free to move when in place, and wrapping a small piece of adhesive tape round the plastic body of the bulb will make it a firm push fit. Insert so that the filament is vertical.

The cassette motor used in the prototype drew 80 mA on normal play, rising only a few milliams when running on full rated voltage, but drawing 500 mA when stalled. The output transistors need to be mounted on heat dissipators to avoid overheating when the motor is stalled; though stalling should never take place in theory, it is not unlikely during testing and setting up. Similarly, the short-circuit protection resistor in the BD35 collector circuit should be generously rated.

The relay used was a sensitive reed-switch type with a coil wound specifically for this circuit, but a standard 12V relay could be used in conjunction with a series ballast resistor. The 47kΩ adjustment potentiometer should be set so that in normal ambient light conditions and with the light slit off the face of the photodiodes, the relay will close. High ambient light conditions may swamp the diodes despite the shroud, and prevent the relay from closing. However this is never likely to occur if the unit is used sensibly, for example away from bright sunlight. A heavily-tinted or even light-tight cover on the record player is recommended.

The power supply for the turntable, servo motor and electronics is a 20V stabilized unit capable of giving 1A (my servo motor and electronics is a 20V design of the power supply is by no turntable required 350mA peak). As the design of the power supply is by no
Fig. 5. Assembly details of motor and 100 to one speed reduction (lower portion) are left to individual constructors. Upper assembly is detailed in drawings and Figs. 3 & 4.

Fig. 6. When properly adjusted a tracking error of 0.2° is corrected in half a second. A set square is needed for scribing reference lines on an aluminium template at right angles to radius line.

means critical it is left to the discretion of the constructor. On the prototype, which had the mains transformer bolted to the plinth, it was found that mechanical vibration was finding its way to the tracking arm to give 50Hz hum. Mounting the transformer on rubber grommets cured the problem, but it is perhaps a better solution to have a power supply unit which is separate from the plinth. At least one commercial unit has adopted this approach.

Setting up

With the tracking arm fully assembled with cartridge and counterweight, raise or lower the vertical pivot to produce neutral equilibrium. The horizontal pivots can also be adjusted to help produce equilibrium, and then set in place with Loctite thread-locking compound. With the cartridge resting on a discarded record, the level of the opto-switch is now adjusted to be in line with the light beam, by means of the spacing washer (Fig. 1, part 1), which may have to be filed down or added to in order to achieve this.

A template to check the accuracy of tracking is essential. A sheet of thin aluminium is cut to suit Fig. 6, the corners being checked against an engineer’s set-square. Find distance d, which will depend on cartridge position, with the template resting firmly against the front edge of the parallel track. Scribe a radius line at distance d parallel to the front edge of the template, left to right, and then using the set-square scribe several lines for reference purposes at right angles to this radius. Adjust the reference arm by means of the screws securing it to the upper platform so that it is parallel to one of the reference lines on the template. Track the arm fast forward and check that the reference arm remains parallel to the various other reference lines. If there is a discrepancy, the parallel track is not straight, and should be re-filed; fortunately the eye has very good perception of parallelism. When this is satisfactory, and with the opto-switch disconnected, play a record, setting the voltage to the servo motor so that the tracking arm keeps pace with the record, very approximately. Note this voltage.

Now connect the opto-switch and with the record stationary and the sliding platform disconnected from the lead screw, bring the tracking arm parallel to the reference arm. The meter reading should now correspond to that obtained with the opto-switch disconnected. If it is not then either the reference arm must be moved sideways to correct this (and then re-aligned of course) or the opto-switch must be moved in relation to the tracking arm.

As a final check, observe the tracking arm from above as it plays a record properly, and note the changes in meter reading as the servo-system corrects tracking errors. Now is the time to adjust the sensitivity by means of R4 and the maximum voltage to the motor (if necessary), by changing the 13V limiting Zener diode for a higher or lower value as required. The prototype was set to correct an error of 0.2 degrees in about 0.5 seconds, which I found to be adequate. The time taken depends not only on the sensitivity but on how hard one is prepared to drive the servo motor. The amount of noise and vibration generated is naturally small in motors designed for cassette decks, but in the prototype, which used a 6V motor, 5.5V was the optimum voltage, before noise from this motor overtook noise from the turntable motor.

S. G. Brown, F.R.S.

At the time of his death shortly after the end of the second world war Sidney George Brown F.R.S. had more than 1000 patents for inventions. These included the gyrocompass used by the Admiralty during the first world war, when they wanted to avoid adopting the American Sperry equipment; the tuned-reed headphones, which were so sensitive to weak signals that they were a standard issue for wireless operators; and a loudspeaker. Brown was the son of a family which had already won fame in the USA for proposing methods of preventing a repetition of the fire which destroyed much of Chicago in the eighteenth century.

Mr F. P. Thomson, biographer of A. D. Blumlein, is now preparing a biography of Brown. He would like to hear from people who knew the Brown family in the USA or worked for S. G. Brown or his company in Britain and who could give or lend papers, notes, photographs, etc. Mr Thomson’s address is 39 Church Road, Watford, Herts WD1 3PY.

Editorial writer for Wireless World

Wireless World needs a new person on its editorial staff. Technical experience in electronics and/or communications and an ability to write are essential. The work is varied and includes writing technical news reports and other material, attending meetings, exhibitions, press conferences and other events, some abroad, and editing contributed technical articles. A good deal of freedom will be given to a person who shows ability and responsibility. Preferred age range 25 to 35. Write to: The Editor, Wireless World, Dorset House, Stamford Street, London SE1 9LU.
C.m.o.s. compatible piezo sounder

Piezo electric sounders are efficient and reliable devices which contain a ceramic transducer and a switching transistor. Although the average current drain is 50mA, the sounder functions as a class C blocking oscillator where the current is pulsed with a peak of 800mA.

It is difficult to switch such a current directly with c.m.o.s. or t.t.l. and a switching transistor would need a wasteful 50mA or so of base current to ensure saturation. Although v.m.o.s. transistors need no drive current they are relatively expensive and have a significant saturation voltage. The simplest solution is a small thyristor which requires a maximum gate current of only 0.2mA. Because the anode current falls to zero between each pulse, the thyristor will turn off unless gate current is present. No gate to cathode resistor is required because a logic low output clamps the gate off.

C. Stephens
Woodbridge
Suffolk

Variable current-limiting supply

This simple power supply offers variable current limiting from 10mA to 3A by using the pass transistor to offset the $V_{be}$ of the protection transistor. Resistor $R_1$ can have any reasonable value and omitting $R_2$ allows unlimited maximum current. In the alternative circuit, $R_3$ and $D_1$ must be chosen for the maximum current required.

D. Rawson-Harris
Stockport
Cheshire

Thermistor replacement for oscillators

The R53 thermistor is often used in oscillator circuits to stabilize the output and reduce distortion. Unfortunately the device is reasonably expensive and intolerant of accidental power surges. This circuit provides a more stable output than the bridge driven rectifier previously published in Wireless World.

In the bipolar version the transistor and diodes can be any general purpose silicon types. The output level can be raised by connecting a Zener diode in series with the emitter. As the output of the oscillator is stabilized to 2.5V ± 5% it should be at least 3.5V r.m.s. before limiting.

If low distortion is important, a similar circuit with a f.e.t. can be used as shown. This does, however, require an oscillator output which at least equals $V_{ge}$ i.e. 8V r.m.s. for a 2N3820.

R. Dynan
London

Continued on page 94
Improved transistor tester

This transistor tester is based on a circuit by N E Thomas in the March 1977 issue of Wireless World. Any unknown bipolar transistor can be placed in the test socket and the transistor leads can be in any order. The ring of three oscillator produces a three-phase waveform which switches either two green and one red l.e.d. on for a n-p-n device or two red and one green for a p-n-p type. Other displays indicate a faulty device. By switching $S_1$ to the appropriate position, the base can be biased via the correct test socket switch. When this has been identified, increasing the base current by reducing the variable resistance turns the collector l.e.d. on first so all three leads are identified. Noting the position of the wiper and the brightness of the l.e.d. gives an indication of the transistors' gain.

M. Odyniec
Podlaska
Poland

12W class A power amplifier

Almost all of the published audio power amplifier designs have had outputs in excess of 30W. However, there are still many applications where a high quality amplifier with less output is needed.

This circuit uses a class A output stage with feedback control of the quiescent current. Two independent amplifiers throughout simplify the circuit and provide a 3 dB improvement in the signal to noise ratio. The necessary trimming of resistors $R_1$ to $R_4$ can be achieved by temporarily connecting them in a bridge arrangement. Specification of the prototype is shown below.

Power output into 8Ω: 12.5W
Frequency response: 5Hz to 225kHz
(-3dB)
Output slew rate: 10V/μs
Distortion: <0.02%
(5Hz to 20kHz, 0 to 10W)
Hum (ref. full power): -85dB
Noise excluding hum: -103dB
Stability: Unconditional
Output offset without nulling network: 15mV

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**VDU MODULE. £33.75**

- Display up to 4K memory (32 lines x 16 chars, with character generator; or 4096 spot positions in graphics mode) on UHF domestic TV. Eurocard-sized module includes UHF modulator, runs on single 5 V supply. Complete ASCII upper-case character set can be mixed with graphics.

**POWER SUPPLY. £6.10 inc. p & p.**

- Delivers 8 V at 600 mA from 220/240 V mains - sufficient to drive all modules shown here simultaneously. Sealed plastic case, BS-approved.

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HURRAH FOR TELETEXT

May I, as a television dealer, air my views concerning teletext, which seems to have dominated Letters to the Editor in recent issues?

I feel the first point I must make concerns the letter from Mr Williams in the October 1979 issue. He complains on the one hand that there are not enough pages, and then goes on to add that if there were, he would not have time to read them all. Spelling and punctuation errors, he says, occur frequently but in my opinion they do not occur as often as in some newspapers.

Regarding access time, it takes on average 12 seconds for a page to appear, a little longer on Oracle - not bad for a system that has to ride piggyback on a few borrowed lines. Teletext is not fading away as some people would have you believe. We dealers must take a lot of the blame for its slow start. My teletext customers are extremely pleased with their sets, which could be due to the fact that we spend over an hour demonstrating the full teletext facilities to them.

I keep wondering why some people wish to change the format of teletext. As far as I am concerned, it offers a very good and comprehensive service the way it is. Teletext sales are on the increase and I feel there is a healthy market developing for the future. So hands off our teletext service, it is the best healthy market developing for the future. So sales are on the increase and I feel there is a

SIDEBANDS AS PHASORS

The opening remarks of J. M. Osborne's excellent article "Sidetbands as Phasors" (September 1979) suggest that Ressel functions are necessary to show that the sidebands of a frequency modulated wave extend to infinity. This is not strictly true for their use is merely a mathematical convenience. The same result can be achieved using primarily traditional trigonometrical methods. A general expression for a frequency modulated wave (see Terman's "Electronic and Radio Engineering", page 588) is:

\[ e = \text{Asin}(\omega_c + \text{msin} \omega_t) \]

where \( \omega_c \) and \( \omega_t \) are \( 2\pi \times \) the carrier and \( 2\pi \times \) the modulation frequency respectively and \( m \) is the modulation index. This expression can be expanded using the well known "sine-sum" formula to:

\[ e = A\sin(\omega_c) \cos(m\sin \omega_t) + A\cos(\omega_c) \sin(m\sin \omega_t) \]

Thus the problem now turns on finding a simplification for the terms \( \cos(m\sin \omega_t) \) and \( \sin(m\sin \omega_t) \) and here we must depart into the realms of simple differentiation. Sine and cosine can each be expanded in series form (see, for example, Saxelby "A course in Practical Mathematics", page 221) so that:

\[ \sin x = x - \frac{x^3}{3!} + \frac{x^5}{5!} - \frac{x^7}{7!} + \ldots \]

and \( \cos x = 1 - \frac{x^2}{2!} + \frac{x^4}{4!} - \frac{x^6}{6!} + \ldots \]

Substituting \( m\sin \omega_t \) for \( x \) in these two series we arrive at two other series, one with odd powers of \( \sin \omega_t \) and the other with a zero frequency component and even powers of \( \sin \omega_t \). Each has related coefficients in powers of \( m \).

The individual terms of each series can be further expanded into fundamental and harmonic components of \( \omega_c \). The even indices will produce cosine terms of even harmonics and the odd indices harmonic sine terms, the highest harmonic in a particular term being equal to the order of the index.

For example:

\[ \sin^2 \omega_t = \frac{1}{2}(1 - \cos 2\omega_t) \]

and \( \sin 3\omega_t = \frac{1}{4}(3\sin \omega_t - \sin 3\omega_t) \)

It is now necessary to collect together terms of similar frequencies and to condensate their coefficients. We have to substitute these terms back into the original expansion where the cosine terms will be multiplied by \( \cos \omega_t \) and the sine terms by \( \sin \omega_t \). We are now on familiar ground where each term will resemble that of an a.m. wave. The terms will have the form:

\[ \cos(\omega_c + \text{msin} \omega_t) + \sin(\omega_c + \text{msin} \omega_t) \]

These are, of course, the infinite sidebands of the frequency modulated wave. The carrier term will result from the zero frequency component arising from the expansion of the even powers of \( \sin \omega_t \) and it should be noted that it will have an amplitude depending on a complex function of \( m \).

The method is laborious and it does not have the elegance of the more accepted method. However, it may appeal to students who have not progressed far with their mathematics - if they have the time and patience to pursue the complicated calculations. There may also be advantages when the modulating wave is not a simple sine or cosine function \( a_m \) for instance, in frequency shift telegraphy, although the mind boggles at the intricacy of the ensuing manipulations.

A similar expansion can also be used for showing the infinite extent of the sidebands when phase modulation is employed.

S. F. Brown
Post Office Telecommunications
Rugby Radio Station
Warwickshire

CORRECTIONS

In the second part of J. M. Osborne's article "Sidetbands as phasors" in the October issue, several errors occurred on page 68. In Appendices 1 and 2 for which we apologize to readers. In Appendix 1 the expression in the second line (for p.m. of carrier) should read:

\[ a \sin(2\pi t + 8\sin2\pi \omega t) \]

In Appendix 2 the first expression (for f.m. of carrier) should read:

\[ a \sin(2\pi t + \frac{\Delta f}{f} \sin \omega t) \]

and the second expression (seventh line) should read:

\[ a \sin(2\pi F + \frac{\Delta F}{F} \sin 2\pi ft) \]

Also in Appendix 2 the expression in the middle column of p. 68 for the maximum rate of swing in terms of frequency (11 lines from top of column) should read:

\[ 2\Delta F \approx 82\pi f \]

- Editor.

WHAT IS AN ELECTRON?

Neither Dr Theocharis nor Professor Jennison appears to understand the aim of modern physics (Letters, October). This is to discover and systematise useful descriptions of the natural universe as we observe it in experiment. Those descriptions are invariably mathematical and some of them are carefully bounded. Professor Jennison has proposed a model and the numbers will show whether or not it is useful. Particle-wave duality must be one of the classic paradoxes and it remains unresolved. Dr Theocharis thinks that most physicists actually believe in a real Jekyll and Hyde electron. Professor Jennison actually appears to do so - and that is his prerogative. Most modern scientists will be happy to leave these two to fight it out. Paradoxes arise through the inadequacy or incompleteness of mathematical descriptions but that does not itself invalidate those descriptions. One must simply tread carefully in making use of them.

D. A. Ross
Poynton
Cheshire

CITIZENS' BAND AND THE LAW

In November a correspondent criticised you for "supporting" the illegal use of c.b. radio, and his criticism was based on the belief that law-breaking is automatically wrong in any circumstances. Is law-breaking automatically wrong? Let us hear some eminent views.

J. J. Rousseau, 1762: "The inflexibility of the laws, which prevents them from bending to circumstances, may in certain cases make them injurious, and bring about in a time of crisis the ruin of the state."

Edmund Burke M P: "It is not what a lawyer tells me I may do, but what humanity, reason, and justice tell me I ought to do."

J. S. Mill, 1861: "There is no ethical creed which does not temper the rigidity of its laws by giving a certain latitude for accomodation to peculiarities of circumstances and it seems to be universally admitted that there may be unjust laws. and that law..."
DIGITAL FILTERS

It is with great interest that I have been following the Wireless World articles on digital filters ever since the original article by Rees. Having programmed the RC low-pass filter on my H-P calculator, I would like to draw attention to a problem that seems to have been overlooked concerning the testing of these algorithms.

As the algorithm is basically derived from the impulse response via the Laplace transform method, the user is tempted to test it by applying a unit step, and feel satisfied when the desired exponential response is obtained. However, the filter cannot operate meaningfully on any frequency above the Nyquist frequency, while any impulsive type of test signal contains a large proportion of its energy in its high frequencies. Thus the only acceptable test signal must be one containing no harmonics beyond a certain frequency.

When a sine wave was used to test the RC filter it was found to be phase advanced by an amount corresponding to half of one time increment. The amplitude error was 0.16% when there were 10 samples per cycle and the period was equal to RC. To correct the time error a sliding mean was applied. Each sample was weighted with the previous sample before being used (see Fig. 1). The sliding mean can be considered as another filter with a rectangular impulse response whose first frequency null falls upon the sampling frequency (see Fig. 2). The equivalent geometrical procedure is to interpolate the samples as shown in Fig. 1. Even so the procedure is not entirely satisfactory as odd multiples of the Nyquist frequency are only attenuated, not removed. The interpolated sine wave had negligible phase error but the amplitude error had increased to 3.5%.

The process is equivalent to using an almost ideal filter on the interpolated waveform and then sampling the output at the original sample rate. Presumably a more sophisticated pre-processor such as for example a filter with a Gaussian impulse response would reduce errors due to residual harmonics.

In conclusion, and as Ham2 points out, aliasing of the input signal is to be avoided if at all possible. Thus, at least for instrumental data there is no entirely satisfactory substitute for an analogue anti-aliasing filter to be applied before any digital processing. For synthetic test data, some digital pre-processing is needed to reduce unwanted harmonics. It seems that digital filters are not necessary as simple as has been implied in your articles.

W. Gray
Farnborough
Hants

References

COMMENT IS POLITICAL

I have read Wireless World for more than 25 years and paid for it out of my own pocket as, unlike many readers, I do not have the subscription paid by my company. During this period it has served me well and I shall be forever grateful for the technical help and guidance it has provided me with. There have also been delightful moments of humour which have helped to demonstrate that technical people can be human.

However, recently I have noticed a tendency to knock the establishment - whatever flavour it might be. I consider the inclusion of political rhetoric out of place in a journal of the calibre of Wireless World: your November editorial was particularly distasteful to me. I take Wireless World for many reasons but they do not include being subjected to the political bias of the editorial staff, both in editorials and general content.

Please, Mr Editor, can we return to an apolitical journal - crusades I can accept but political bias no.

J. Greenwood
Chelmsford
Essex

POUYTING VECTOR

Apparently many people find the concept of displacement current useful and some find it distasteful. Not being a member of either group I would normally be prepared to continue as a passive spectator of the fascinating correspondence which has been stimulated by the recent articles on the subject. After all, no-one is suggesting that $\varepsilon_0\alpha$ should be struck out from Maxwell’s equations, and presumably no-one is insisting that everyone must believe that there is any physical reality in a current which is said to flow in empty space where there is nothing to carry it (and nothing to be displaced). I would even leave it to others to point out that in Fig. 4 of “The history of displacement current” in your March issue the current $i$ will vary continuously between B and B', as is the way.
with transmission lines, so if you want a continuous "current" you do need a displacement current, not localised at B, but distributed along the length of the transmission.

However, the excellent iconoclasts Catt, Davidson and Walton have spurned me to action by their uncharacteristically unquestioning use of a concept/mathematical construct which is far less harmless than displacement current, namely the Poynting vector or "energy current" ExH. A single example will show what I mean. Suppose I take a battery and connect it to a lamp by a pair of good thick wires. Since the electric field is negligible inside the wires the Poynting vector is too. In fact the Poynting vector is mainly localised in the space surrounding and particularly between the wires. In other words, a correctly drawn conclusion that energy flows from the battery to the lamp. One could even, in principle, integrate the Poynting vector over a surface containing the battery or the lamp, but not both, and calculate correctly the rate at which energy flows from the battery to the lamp, but one would be allowing oneself to be blinded by one's own mathematics to deduce from the fact that the Poynting vector is indeed locally zero in the wires and is at a maximum between the wires that the energy flows mainly between the wires and not to any appreciable extent through the wires.

In case anyone does believe that even in this case the Poynting vector represents a physical energy flow I propose the following experiment. First, interpose a metal screen between the battery and the lamp, less than an inch from one of the wires, but fitting as closely as possible, so as not to leave more than the tiniest space for the Poynting vector to squeeze through. Note the effect (if any) on the amount of energy which gets to the lamp. Now take away the screen and make a break (just a little one, mind) in one of the wires. Again, note the effect on the amount of energy which gets to the lamp. Note the effect on the amount of energy which gets to the lamp. Again, note the effect on the amount of energy which gets to the lamp. After the break a long section of the wires, however short it may be (say one mile), creating a long section with very low characteristic impedance, transmits energy over its entire length (say one mile), creating a long section with very low characteristic impedance, transmission line reflection theory correctly tells us that energy flow from battery to lamp is delayed. More conventionally, this delay would be thought of as an RC time constant, the C being the narrow gap between conductor and screen for the very long distance. Referring to his sentence 3, once the tiny break is made, and energy current breaks (Heaviside called an obstructor) is made, energy current flows through the break and out into the vast space beyond. This space presents a rapidly increasing (characteristic) impedance, causing all the outgoing energy current to be reflected back through the break into the narrow channel through which energy was previously gliding calmly (at the speed of light) from the battery to the lamp. After the initial disturbance of the steady state caused by the breaking of the conductor (obstructor), the lines of energy current gradually, through the mechanism of reflections, settle down to a new pattern where energy (of the same amplitude as before the conductor was broken) flows out of the battery to the gap in the wire, there to be fully reflected back into the battery, in a "continual dance of energy" which Carter dismissed as absurd but CAM Consultants do not. (The Electromagnetic Field in its Engineering Aspects, by G. W. Carter, Longmans 1954, page 321.) If however the break is made when the conductor is extremely narrow (and long), it will take time for its existence to become apparent. Very traditionally, this very narrow, long gap in the conductor would be regarded as a capacitor. An RC time constant was envisaged, the transmission line of very low characteristic impedance.

Dealing with his third para. in a lighter vein, one is urged to suggest that it is the "phlogiston" in a balloon material which keeps it doing its job. The absurd theory that goods travelling in a railway system travel between the rails, or an obstruction across between the rails, nearly touching the rails; close enough to leave too little space for the train wheels to get through. This will prove that goods are really piped along inside the railway lines and it is absurd to think that the lines merely guide the flow of merchandise.

When all is said and done, however, the acid test is the question of whether the velocity of propagation of the energy (electric) current is a function of the characteristics μ, of the dielectric or of the conductor. When a seagull (or merely the reflection of a seagull) is flying above the surface of the water, does its speed depend on the nature of the air or of the water?

I. Cott, M. F. Davidson, D. S. Walton

"TRIVIAL" AMPLIFIER DESIGNS

I find it quite incredible that Wireless World, should see fit to publish yet another article describing amplification equipment for domestic sound reproduction, in which purely academic distortion levels are pursued virtually for their own sake. The author states that he designed the amplifier with a view to its being "competitive with current commercial designs." Can this really be an accurate aim? In my estimation and third harmonic distortion audibility threshold (even where skilled sound engineers and producers are concerned) is in the region of 0.1%. Given that this is so, then an amplifier which produces second and third harmonic distortion not in excess of 0.1% over its entire bandwidth should sound as good as one with 0.0002% second harmonic distortion, all other factors being equal — entrance slew rate limitations, overload effects, audibility threshold of high harmonics, et al.

A multitude of exotic schools of thought currently abound to extol the "sound" of polypropylene capacitors, special loudspeaker cables, diaphragm materials, etc., 'real time' amplification, 180V/μs slew rates, passive equalisation, minimal overall feedback, etc. I challenge Wireless World to seek out the truth of this mysticism, rather than present confused and confusing material. I wish to state that I in no way whatsoever wish to deprecate per se the designs presented by Douglas Self and B. J. Codd, but rather to suggest that whilst their engineering approaches are interesting, they are really grossly trivial in a world where the allowable second harmonic distortion on a studio tape machine is of the order of 3%, where 70% of record presences are defective and electromechanical transducers from the cutting head to the loudspeaker are as yet imperfect.

'To exemplify: I have recently built Douglas Self's Mk I advanced preamplifier design using TDA 1034N op-amps. Using horn-loaded loudspeakers and Cridom Electrika amplifiers in a tri-amplified configuration, I perceive no different results for my friends to say "Your equipment sounds different." The chances are high that your equipment sounds different.'
THERMIONIC DEVICES

I know of nothing more likely to start an argument between historians than that of Fleming's diode ushered in the thermionic "valve era..." (November 1979, p.94).

Dare I suggest that Edison's patent of 1884 (nothing to do with wireless of course) covered a most practical application of ther- mionics to the control of a generator? For all I know this may also have been the first thermionic closed-loop servo-mechanism to be described. But Edison was very busy inventing hundreds of other things, and can perhaps be excused for not applying his "so-called" effect to wireless, the phonograph, moving pictures etc. as well.

What is most puzzling is that Fleming was apparently so slow off the mark - a whole 20 years before the penny dropped! Of course he had been fairly busy around 1900 combining the more recent ideas of Tesla, Thomson and Marconi into the Pollock transmitter, a very substantial engineering task; and this may have diverted his mind from developments in Germany, such as Wehnelt's lime-coated thermionic filament also published in 1904 which was incorporated into the Braun-Wehnelt cathode ray tube of 1905. (The same Braun, of course, who later shared a Nobel prize with Marconi.)

In the event it must have been a little humilitating for Fleming that there was not more interest in his thermionic diode (though it may have stimulated the invention of the crystal detector). The reasons were that the carbournium detector was simpler and more rugged and the Marconi magnetic detector needed no battery. Thermionics really took off in a more obvious fashion about a decade later, with the advent of better vacua and other technical improvements. In fact it became important enough for litigation over rights; and though neither side seemed to emerge with much of value, the ruling did confirm Fleming's legal title to his (rather gassy) diode valve.

Desmond Thackeray
University of Surrey
Guildford

MICROPROCESSOR PERIPHERAL ICs

A problem exists in the design of circuits using the latest microprocessor peripheral i.c.s. I would like to suggest a solution which, although using one more pin of the package, would require little complication of the i.c.

The problem is evident when several peripheral interface to the same data bus, and this bus includes one or more sets of bi-directional bus buffers. In order to ensure that these buffers are always driving in the correct direction, the logic designer finds himself duplicating circuitry that must already exist inside the i.c. Some peripheral chips put data on the bus for up to one of three different reasons. To determine the direction of the relevant bus buffer, all these states must be decoded, and ORed together, along with similar lines from other peripheral chips on that section of the bus.

My suggestion is that a 'drivers active' function be brought out to a pin of each bus-interface peripheral i.e. Relevant bus buffers could be turned around by a simple OR of these few signals. Even greater simplicity could be achieved if the 'drivers active' lines were open-collector types, a wired-OR then being possible.

I feel sure that this line would also be useful in the debugging phase of microprocessor support circuitry where problems of bus contention and floating buses may have to be resolved.

PRE-AMPLIFIER WITH NO T.I.D.

Potential builders of the Miloslavskij passive de-emphasis preamplifier (August issue) might like to note that its RIAA network is grossly in error. Correct design formulae for passive de-emphasis can be found in the literature:

S. Lipshitz
University of Waterloo
Ontario, Canada

References


ELEMENT OR DIAMOND?

While experimenting in television during the "mechanical" period, I realised that the accepted theory of the "picture element", based on the chessboard idea, is a fallacy. I found that a continuously moving spot cannot resolve a picture detail as small as itself; it smudges along the traced line, generating a maximum frequency only two-thirds that calculated from an ST100 diagram, which involved 15 crossovers [Diagrams supplied.-Ed.]. The celebrated "ST100" offered plenty of scope for compulsive twiddlers, with two tuning capacitors, plug-in coils with variable coupling, filament rheostats and a cats whisker. Although it was an essentially simple reflex arrangement, Scott-Taggart showed real originality in circuit-diagram presentation. Scoring ordinary logic in layout, he produced bafflingly devious links.

One of the figures I have sent you is copied from an "ST100" diagram, which involved 15 crossed wires. The other is the same circuit, but as it would more commonly have been designed 50 years ago - with only three crossovers [Diagrams supplied.—Ed.]. The contrast speaks for itself.

C. Leslie Thomson
Kingston
Edinburgh, 16

RADIO AMATEUR INVALID AND BLIND CLUB

May I bring to your attention the change in the title, secretary and address of the Radio Amateur Invalid and Blind Club. Now celebrating its silver jubilee, the Club is formed of invalid and blind members interested in the hobby of amateur radio; their local representatives who undertake to help by visits, repairs and advice; and supporter members whose financial contributions enable help to be given. The sole condition of membership in any of the above categories is an annual subscription of £1 minimum for Radial the Club newsletter which is issued every six weeks.

F. E. Woolley (Mrs)
Hon. Secretary
9 Runnach Court
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JOHN SCOTT-TAGGART

Your brief, but nostalgic, obituary on John Scott-Taggart (p.35 October 1979) recorded his prowess as an engineer. In his earlier days he was also a formidable showman. From the mid-twenties to the early thirties, thousands of experimenters were persuaded that the 'ST' series of circuits had supernatural powers.

The celebrated 'ST100' offered plenty of scope for compulsive twiddlers, with two tuning capacitors, plug-in coils with variable coupling, filament rheostats and a cats whisker. Although it was an essentially simple reflex arrangement, Scott-Taggart showed real originality in circuit-diagram presentation. Scoring ordinary logic in layout, he produced bafflingly devious links.

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Addington Road
Surbiton
Surrey KT6 4TE
More on the scientific computer

Further details of the monitors

By J. H. Adams, M.Sc.

After publication of the scientific computer series (April to September 1979) there have been many requests for more information on the firmware. This article describes in more detail the machine code and BURP monitors in terms of hexadecimal machine code. Readers will need a hex print-out of the three p.r.o.m.s and the mnemonic to hex conversion tables published in the July 1979 issue of Wireless World.

Several readers have expressed incredulity at the thought of working directly in machine code rather than using assembly language mnemonics. However, the hex codes for 50 to 60 of the most regularly used operations can soon be learnt and, thanks to the logical distribution of codes to operations, many more follow from these. The once-in-a-megabyte ones such as IN D (C), ED 50 in hex, can be obtained from the conversion table. This does not rule out working in assembly language and using an assembler, or translating yourself, but in my experience the latter soon becomes tiresome and it is easier to write in hexadecimal.

When writing software it is useful to have a supply of the forms shown in Fig. 1. The instruction 18, a relative jump, should be pronounced one eight and not eighteen. Similarly, the second byte is one seven and definitely not seventeen. If you want to jump forward with a relative jump, simply make the jump byte the number of bytes (up to 7F) over which execution must move, in this case 17 — 1 row and 7 bytes, to reach the target byte FF. For a jump back to the same target from the second 18, calculate the jump forward code to the next byte immediately under the target, 02 in this case, and then jump up row by row, decrementing the higher order hex character, i.e. from 02, F2, E2. When using a jump back the byte must be in the range 80 to FD (FE and FF serve no useful purpose).

Machine code monitor

Both monitors follow the same basic sequence as illustrated in Fig. 2. With the machine code monitor the base address of the Z80 stack is set, the address for the top corner of the screen is loaded into the DE register pair which will have been pushed onto the stack, is exchanged with the contents of the HL register pair and then used as a pointer to that data before being exchanged back onto the stack, at the end of the routine, to cause a return to, in this case, 0010. The start procedure then clears the rest of the top line, resets the teletypewriter output flip-flop and, using the subroutine at 0355, reads in and encodes a command from the keyboard. As explained in table 1, only the first and last letters are important to the subroutine. Whilst this limits the number of possible combinations which will produce different codes, a byte by byte comparison with a look-up table comprising all of the commands would use far too much p.r.o.m. space. After this has been achieved (001A), a comparison is made and if the code is not FC (the entry code for RUN) executions jump over 0D bytes for a further comparison and so on until a match is found, whereupon a block of instructions is executed before operation returns to 0000 again.

<table>
<thead>
<tr>
<th>Address</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>0254</td>
<td>Sets tape interface tone to 2400Hz and then calls 255 long time delays — about 4 seconds.</td>
</tr>
<tr>
<td>0260</td>
<td>Transmits the byte in register A to the tape interface, preceded by a start bit and followed by two stop bits.</td>
</tr>
<tr>
<td>027F</td>
<td>Calls a new line and then prints the contents of HL on the teletypewriter.</td>
</tr>
<tr>
<td>028E</td>
<td>Formats the hex byte in register A for printing as two characters on the teletypewriter.</td>
</tr>
<tr>
<td>02EC</td>
<td>Prints a space on the teletypewriter.</td>
</tr>
<tr>
<td>02FD</td>
<td>Calls a new line on the teletypewriter.</td>
</tr>
<tr>
<td>0301</td>
<td>Prints the contents of the A register on the teletypewriter.</td>
</tr>
<tr>
<td>0317</td>
<td>List subroutine. Entered at 0317, the starting address must be loaded in from the keyboard. Entry at 0310 assumes the address to be at 1FF0 to 1. Entry at 0320 assumes that the address is already in HL.</td>
</tr>
<tr>
<td>0336</td>
<td>A programmable time delay. The computer loops through six E3s, a long exchange instruction which, if used in pairs, does nothing but use up time. The number of loops is set by the byte immediately following the CALL in the original program. Each loop lasts 64μs.</td>
</tr>
<tr>
<td>0346</td>
<td>Clears the top line and sets DE to 8000.</td>
</tr>
<tr>
<td>034E</td>
<td>Used to format results, as in FIND and COR, this rounds DE up to the next multiple of B.</td>
</tr>
<tr>
<td>0355</td>
<td>The algorithm for encoding input commands. Returns with last letter of the command minus the first letter in register A.</td>
</tr>
<tr>
<td>0372</td>
<td>The formatter used in LOAD and LIST in machine code language.</td>
</tr>
<tr>
<td>0393</td>
<td>Clears the v.d.u., leaving DE unaffected.</td>
</tr>
<tr>
<td>039F</td>
<td>Displays HL and a space. Used in LIST, LOAD, FIND, COR and in BURP lists.</td>
</tr>
<tr>
<td>03AA</td>
<td>Displays the contents of A as a two character hex byte.</td>
</tr>
<tr>
<td>03C4</td>
<td>Calls a new line on the v.d.u. and clears the remainder of the current one.</td>
</tr>
<tr>
<td>03CE</td>
<td>Displays the string of characters following the call in the program block up to byte 1D.</td>
</tr>
<tr>
<td>03DE</td>
<td>Loads HL from the keyboard.</td>
</tr>
<tr>
<td>03E7</td>
<td>Loads A with a hex byte from the keyboard.</td>
</tr>
<tr>
<td>03F6</td>
<td>Reads in a single keyboard character and, if a letter adds 8, then truncates to four bit binary (used as part of 03E7).</td>
</tr>
</tbody>
</table>

Table 1. Low level monitor subroutines.
An exception to this is for the code FC, the routine for which 001E jumps immediately to 0042. This avoids one of the subroutines which have to be located at particular points in the memory map. Several subroutines can be called by single byte instructions which are known in mnemonic form as RSTs. These were originally intended for use with the 8080 and the Z80’s “8080 mode” interrupt response which, after receiving the interrupt, calls for the interrupting device to place one or more instruction bytes onto the data bus for execution. Although this mode is not used, the single byte calls are a useful space-saver where a subroutine may be short and often needed. The subroutine which is avoided in this case at 0020 is called by byte E7 and produces a space on the v.d.u. at address 0026 is a jump to a subroutine which would require more than eight bytes. It is intended for use during the testing of machine-code programs and when its RST byte EF is inserted into the program by using an ALT, it will suspend the execution of the inserted instruction bytes onto the data bus and when its RST byte EF is avoided in this case at 0020 is space-saver where a subroutine may be used, the single byte calls are a useful instruction bytes onto the data bus for receiving the interrupt, calls for the execution of a subroutine which would require more instruction bytes. The sequence check that the 57109 is ready, outputs the instruction with the hold-off, waits for the ready to go off and then puts the hold on again.

The two interrupts also use fixed service routines. At 0038 is the maskable interrupt routine which reads in and stores number cruncher data using HL as a pointer. At 0066 the non-maskable interrupt’s routine services the keyboard, first checking if the computer is at a HALT byte (76) and reading in the keyboard if it is or resetting the computer if it is not (0068 is an example of a long relative jump). This particular software does not make use of the control characters available in ASCII except for the RETURN byte 0D, which it translates to 0D. Instead it blanks off the top three bits of any codes above 3F (mainly the letters) at 007C and moves lower and upper case codes into the area 00 to 1F. This compression of the ASCII code into six bits produces byte which are compatible with the v.d.u. character generator and this makes writing to the v.d.u., which occurs at many places in the monitors, a simple operation.

Before the service routine, the routines for the various operations in table 2 fit end to end to 0253, with the exception of some unprogrammed space at 0139. This space may be used by overprogramming the jump byte 011F-10 and the ten bytes as required. Note that the LIST (014A) routine is just a call to a subroutine at 0317 because an identical block of instructions are required as part of the ALT routine. As this is the last command code to be checked, the call is conditional on a match so that if the code is undefined, execution passes to 01A9 and a software reset.

### Table 1. BURP subroutines.

<table>
<thead>
<tr>
<th>Code</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>0000</td>
<td>Used in graph plotting. Converts a number stored in 1E00 to the nearest integral value. Negative values are put to zero.</td>
</tr>
<tr>
<td>002E</td>
<td>Displays a number formatted by 05A9 in 1E00 - F displaying E for OB,. for OA, a space for OF, - for OC and ASCII</td>
</tr>
<tr>
<td>01A6</td>
<td>Converts A to three digit denary and displays on v.d.u.</td>
</tr>
<tr>
<td>01CD</td>
<td>Inputs denary keyboard digits to binary in C.</td>
</tr>
<tr>
<td>016F</td>
<td>Prepares the store area specified by the contents of A using 0714 and then reads in a number from the keyboard, converting standard and</td>
</tr>
<tr>
<td>0226</td>
<td>handles the 57109 TR (branch) output which pulses low whenever one of the 57109 test instructions proves to be true. The subroutine starts</td>
</tr>
<tr>
<td>0203</td>
<td>The look-up table for the 57109 instructions.</td>
</tr>
<tr>
<td>0253</td>
<td>The list is terminated by FF.</td>
</tr>
<tr>
<td>046E</td>
<td>Repeats 042E for the string of 57109 instructions following the call in the main program. The list is terminated by FF.</td>
</tr>
<tr>
<td>04D4</td>
<td>Jumps over the next word in the program line. Used in FOR statements to miss STEP and UNTIL.</td>
</tr>
<tr>
<td>0460</td>
<td>Outputs the contents of the 57109 X register to locations 1FF4 - 1FFF and then reformats it into the location specified by the contents of</td>
</tr>
<tr>
<td>0452</td>
<td>The routine starting addresses.</td>
</tr>
<tr>
<td>0466</td>
<td>Graph plotting routine which scales the variables to be plotted to the screen matrix of 63 X 128. It divides the variable specified by</td>
</tr>
<tr>
<td>0458</td>
<td>after outputting to 1E00.</td>
</tr>
<tr>
<td>0468</td>
<td>Handles the 57109 RR (branch) output which pulses low whenever one of the 57109 test instructions proves to be true. The subroutine starts</td>
</tr>
<tr>
<td>058A</td>
<td>Prepares the store area specified by the contents of A using 0714 and then reads in a number from the keyboard, converting standard and</td>
</tr>
<tr>
<td>0688</td>
<td>the last procedure is jumped. Finally, the read in and masked byte which caused the exit from the parity checking loop, stored in register B as</td>
</tr>
<tr>
<td>0714</td>
<td>The look-up table for the 57109 instructions.</td>
</tr>
</tbody>
</table>

### Table 2. Machine code routine starting addresses.

<table>
<thead>
<tr>
<th>Code</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>002F</td>
<td>FILL</td>
</tr>
<tr>
<td>0099</td>
<td>LOAD</td>
</tr>
<tr>
<td>011E</td>
<td>ALPH</td>
</tr>
<tr>
<td>0152</td>
<td>FIND</td>
</tr>
<tr>
<td>01A6</td>
<td>LIST</td>
</tr>
<tr>
<td>0042</td>
<td>RUN</td>
</tr>
<tr>
<td>004D</td>
<td>MOV</td>
</tr>
<tr>
<td>007C</td>
<td>CTRL</td>
</tr>
<tr>
<td>0080</td>
<td>ALT</td>
</tr>
<tr>
<td>0084</td>
<td>COR</td>
</tr>
<tr>
<td>00B2</td>
<td>0120</td>
</tr>
<tr>
<td>0203</td>
<td>TAPE</td>
</tr>
<tr>
<td>022E</td>
<td>READ</td>
</tr>
</tbody>
</table>
Table 4. Format for storing and printing three variables.

<table>
<thead>
<tr>
<th>Table 4.</th>
</tr>
</thead>
<tbody>
<tr>
<td>005 LET A = 23.45</td>
</tr>
<tr>
<td>006 LET B = 0.00733</td>
</tr>
<tr>
<td>007 LET C = 3.45633</td>
</tr>
<tr>
<td>008 PRINT A</td>
</tr>
<tr>
<td>009 END</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Table 5. BURP routine starting addresses.</th>
</tr>
</thead>
<tbody>
<tr>
<td>083F DEL</td>
</tr>
<tr>
<td>0929 LOAD</td>
</tr>
<tr>
<td>092F GOTO</td>
</tr>
<tr>
<td>092B INPUT</td>
</tr>
<tr>
<td>092B WRITE</td>
</tr>
<tr>
<td>092B GOSUB</td>
</tr>
<tr>
<td>092B NEXT</td>
</tr>
</tbody>
</table>

From 0254 to 03FF are the subroutines listed in Table 1. When necessary, the subroutines PUSH registers to be used solely within the subroutine and then POP them back before the return so that no interference is caused to data within the main program. Most subroutines are self-contained but some, e.g. 02EC, jump on to others for their completion. As subroutines are sometimes called within subroutines, within subroutines etc., the stack storage area, which extends into the r/w.m. from 1FFD, should be left free to at least 1FC0 for the computer's use. Like C7, other space savers will be found in the subroutines, e.g. AF to clear the register A instead of 3E 00, which makes use of them. Details of the subroutines are given in Table 3. In BURP, program material is loaded from OCO on, the area 1E00 to 1EDF is used for the formatting of results to be printed and 1E10-F stores variable A and so on up to 1FB0-F which holds the FOR loop step. Table 4 shows the formatting used for the storage and printing of three different variables. Note that all results are stored scientifically to maintain eight digit accuracy. Although the MM57109 can operate in either mode, it is quicker to stay in the scientific mode and let the Z80 convert the results within the range 0.0001-99999999 to floating point for display.

At 0800 the stack pointer is set and DE is assigned as the screen pointer again. BURP is then displayed and the rest of the top line cleared. The mantissa digit count is set at 04 (0817) and the screen position reset to 8008 ready for the input of a command. 081E to 0823 is harmless nonsense and 0824 to 0837 resets the number cruncher by sending the operation 3F (NO OP) with the hold to the 57109 off, pausing for 8ms and then reapplying the hold. During this sequence the interrupt mode is set but as it is the masked one that is driven by the number cruncher, the somewhat capricious behaviour of the i.c. before it has run the reset has been taken over by the rest of the system. The i.c. is then given a master clear (2F) and switched to the scientific mode (22) by a multiple executive subroutine at 0446 (0832).

At 0838 another command encoder is called to read in a command from the keyboard. The algorithm used here is two times first plus last, so once again only two letters are required. However, this algorithm is capable of producing a far greater list of codes and therefore reduces the chance of two words deriving an identical one. As with the low level monitor, routines entered by recognition of this code ensue, see Table 5. The start of the last of these, the RUN command, reads in and encodes the line number input in the command and stores it in register C. The v.d.u. pointer is then set to 8040, the start of the second line, and C is decremented, pushed, popped, incremented and then pushed again. Four of these operations might seem to do nothing to C and on this occasion they do not. The total effect is to store the current line number on the stack. When the execution of a line is completed however, the next line number can be computed and saved by returning to 097F. After GOTOs, when A will hold the next line number, a pop to remove the old number followed by a jump to 0981 will load this as the next line to be executed. As all lines will terminate by jumping back to one of these locations (except for END which returns to 0800), to avoid absolute jumps (i.e. jumps to specific addresses), relative jumps to these two critical points are string out through the third param.

A line of BURP is stored as the hex byte ED, the line number in hex, the actual data in modified ASCII and then the byte IF to signify its end. The end of the memory block in use is signalled by the byte C0. With the commands ADD, DEL, DUMP, LIST and RUN involving line numbers, the memory block up to C0 and looks for ED followed by the line number in question. During a RUN the next word in the line is encoded using the two times first plus last algorithm (0983) and again, the routines for all of the commands are strung end to end and each is preceded by an immediate compare and a jump-on-not-zero (20 hex). The last command. HALT, compares at 080F and if a match is not made the computer jumps over the single byte 76 of the HALT routine and goes on to the next line by executing several relative jumps back to 097F. This explains why there is no routine for REM as it and any unrecognised first word on a line is just.

**Fig. 2. Basic operating sequence for both monitors.**
Table 6. New features of the improved firmware.

<table>
<thead>
<tr>
<th>General</th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>v.d.u. cursor on all modes.</td>
<td>RETURN available in graphics mode.</td>
</tr>
<tr>
<td>DEL deletes last character on all modes.</td>
<td>Interface for ASR or KSR teleprinter (as printer and/or punch).</td>
</tr>
</tbody>
</table>

**BUPR**

Extended IF statements. Any statement may be conditioned by IF.

Mathematical capability available in IF. FOR PRINT, WRITE, GRAPH and AXIS statements.

Printed strings in INPUT as well as PRINT statements.

Multiple statements — virtually unlimited numbers of statements may be written against a single line number.

This speeds execution and expands the effective statement capacity well beyond the 254 lines.

Extra maths functions:
- **ABS** makes current result positive
- **INT** blanks digits following decimal point
- **FRAC** blanks digits preceding decimal point
- **RND** places pseudo-random number into the MM57109

No need for LET at the start of LET-type lines.

'in a line, causes the computer to ignore the data following, up to the end of that line (alternative to REM).

**Hardware changes required**

The wiring of several spare keys.

The teleprinter interface shifted from D7, to D0, and 55V reduced to 5V.

**P.r.o.m. required**

Complete with the graph plotting firmware, this will still fit into three 2708 p.r.o.ms.

The 1980 conference has a four-part conference and exhibition, January 30 to February 1. Sponsored by Wireless World and associated electronics and computer journals, this annual event has grown in size to such an extent that it has had to be moved from its hotel venue to the Wembley Conference Centre (opening hours, 0930 to 1800 hours each day).

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<table>
<thead>
<tr>
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<th>DISPLAY, GAS FILLED, ETC.</th>
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</tbody>
</table>

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Two-metre s.s.b. and f.m. transceiver—4
Alignment procedure and operating notes

by G. R. B. Thornley, G2DAF

For satisfactory alignment the following test instruments will be required: a c.w. signal generator; an absorption wavemeter; an AVO Model 8 or equivalent; a diode probe valve-voltmeter; a digital frequency meter; and an audio oscillator.

It is advantageous to test and align as many units as possible before final assembly in the chassis, so the following instructions will be based on this method. Initially, each unit should be connected to a stabilized power supply, set to 12.7V, with a milliammeter in series to monitor the current drain and to ensure that there is no short circuit or fault condition on the circuit.

S.s.b. generator unit
Connect the power supply, still set to 12.7V, to the +12V TX terminal post on the s.s.b. generator board and wire an external 1-pole, 2-way switch in place of S12, with the pole connected to the power supply. Check that there is 9.1V feeding Tr1. Set the slider of R11 to mid position and connect the diode probe of the valve-voltmeter to the test point TP. Adjust the core of L3 for maximum carrier output — this will be in the range 0.3 to 0.5V r.m.s. Operate the temporary switch S13 to select crystals XL1 and XL2 in turn, and ensure that they are both oscillating at approximately equal amplitude.

Remove the valve-voltmeter probe and connect the digital frequency meter via a 5pF series capacitor to the test point TP. Switch to the i.f.s. crystal and adjust C30 until the crystal is on exactly 10,700kHz to the “IF. in” terminal post. Transfer the valve-voltmeter probe to the “I.F. out” terminal post (output side of C32). Connect a microphone to the “Mic” terminal post and adjust R16 for maximum gain. If all is well, a whistle into the microphone will produce an s.s.b. signal and will deflect the pointer of the valve-voltmeter to approximately 0.25V r.m.s.

Connect an 8-ohm loudspeaker to the circuit, transfer the 12.7V supply to the +12V amplifier terminal post and adjust R15 for exactly 6.35V at the junction of R65 and R66. Open circuit the wire link between the test point TP and the ground plane, and connect the AVO, on the 1,000mA range, in lieu. Adjust R65 for a quiescent Tr13, Tr14 collector current of 20mA. Set the audio signal generator to 1.5kHz and zero output, and connect it to the “A in” terminal post (connection to C65). Advance the audio generator output to 100mV r.m.s., while watching the AVO reading, which should increase to 250-300mA. A clean undistorted note, at full volume, should be heard from the loudspeaker. Reduce the audio drive to about 100mA collector current and swing the audio generator output frequency from 300 to 3,000Hz. The sound amplitude should remain approximately constant and without distortion at any frequency. Remove the AVO and reconnect the link (Note that R65 is soldered across D13 on the etched side of the p.c.b.).

Temporarily bridge the “A out” terminal post of the demodulator (junction of R66 and R63) and connect it to the “A in” terminal post of the audio amplifier using screened cable. Connect the 12.7V power supply to the +12V RX terminal post, check that the source rail is at 3.3V and set the a.g.c. rail to 5.5V by adjusting R65. Set the wiper arm of the balancing potentiometer R65 to mid position, connect the signal generator, set to exactly 10,700kHz to the “IF. in” terminal post (input to C65) and advance the r.f. output until a 1.5kHz tone can be heard from the loudspeaker. Adjust the cores of L13, L14 and L15, for maximum output while progressively reducing the signal generator output to avoid overloading the demodulator and the audio stages.

Make a screened-cable link from C65 to the drain of Tr15 on the underside of the p.c.b. and temporarily connect R65 and R63 to a 1mA-movement S-meter. With no signal generator input, set the S-meter to zero by adjusting R65. This will alter the a.g.c.-line potential because R65 and R63 interact, so it will be necessary to reset R65. Repeat the two adjustments until the S-meter reads zero and the a.g.c. reads 5.5V. Set the signal generator output to 10mV and adjust the core of L13 for maximum S-meter reading. Reduce the signal generator output to 100μV. If all is well the meter should give about an S9 reading. When the transceiver is completed, R66, which controls the S-meter sensitivity, can be set to obtain an S9 reading for a 50μV two-metre-band signal.

Reduce the signal generator output to zero, and the S-meter should return to zero. If it does not do this, it means that the carrier oscillator output is leaking into the i.f. amplifier. Connect C65 to one side of the balanced-modulator potentialmeter, R65 and adjust R64 and C65 in turn to balance the modulator and obtain a zero indication on the S-meter. If adjusting C65 does not improve the balance, remove the link and connect C65 to the other side of R65. While making these adjustments ensure that the correct h.s.b. crystal (10,685.5kHz) is switched into operation. If balance cannot be fully obtained and C65 is at full capacity, wire a 25pF ceramic capacitor across C65 on the underside of the p.c.b. and readjust C65.

F.m. generator unit
Connect a 100μA f.s.d. S-meter to the SM terminal post of the f.m. generator board. Turn the i.f. gain control, R45, to
maximum, and inject exactly 10,700kHz from the signal generator into the "F.M. in" terminal post, at a level that starts to deflect the S-meter. (Note that the meter will read approximately 50pA with no signal input.) Adjust the cores of L14 and L15 to obtain maximum S-meter reading. At the same time as the tuned circuits are brought onto resonance, reduce the signal generator output to avoid overloading the i.f. stages.

Set the signal generator input to obtain a S-meter deflection of three-quarters full scale and connect the digital frequency meter in parallel with the signal generator output to avoid overloading the i.f. stages.

Set the signal generator input to 10,700kHz and carefully adjust C111 until the AVO reads 50µA and make a note of the frequency. Repeat for 100µA and 150µA and note these frequencies too. Go back to the 0µA reading and reverse the AVO connecting leads. Check that the meter is indicating the wavemeter set to 62.5MHz. Set the slider of R117 for "Mod out". Set the signal generator output to avoid overloading the i.f. stages.

Phase-lock v.c.o. unit

The alignment instructions for the phase-lock v.c.o. unit assume that the three p.c.b.s and the MC7805 regulator have been assembled in the screening box, and the LED indicator D10 connected to C26 and C29. All interconnections should be made, and supply and switching terminal posts wired to the appropriate box via 1,000pF feed-through capacitors. Measure the output voltage of the MC7805 regulator and ensure that this is 5.0V.

With a soldered link, short circuit TP1 on the v.c.o. p.c.b. to the groundplane in order to disable the oscillator Tr30. Apply the signal generator output to TP1 and connect the valve-voltmeter probe to "RF out" terminal post. Set the signal generator to 134.3MHz and adjust the core of L24 for maximum r.f. output. Transfer the valve-voltmeter probe to "V.C.O. out" terminal post and adjust core of L25 for maximum r.f. output.

Wire the microphone to "Microphone in", and high impedance headphones to "Mod out". Set the slider of R117 for maximum audio gain. Speak into the microphone, and if all is well this should produce low-level crisp, clean audio in the headphones.

Connect the d.f.m. to test point TP3, and with trimmers C117 and C118 trim each crystal as near as possible to the required frequencies 125,000kHz and 126,000kHz. Note that crystals for amateur use are normally supplied to a frequency tolerance of ±0.005% and it may not be possible to pull XL5 and XL6 completely on to the required frequency. Finally operate S2 a number of times, and ensure that both crystals operate without hesitation and without frequency jumping. Remove the d.f.m. and connect the signal generator, set to 9,300kHz to test point TP4, and the valve-voltmeter probe to "I.F. out". Adjust cores of L24 and L25 for maximum r.f. output.

With the short-circuit link from TP, and the AVO should now read 0.85V. With the external switch S2, select the 125MHz crystal and connect the signal generator, on 9.3MHz and 500mV r.f. output, to "V.F.O. in". Screw the core of L21 completely into the winding. The AVO will now read 4.9V. Slowly unscrew the core of L21 until the AVO indication drops from 4.9V to 2.9V. At this point the indicating LED will light. The loop is now locked.

Operate the external switch S2 to select the 126MHz crystal. The AVO should now read 4.5V and the LED should remain lit. Select the 125MHz crystal and tune the signal generator to 8.3MHz. The AVO should now read 1.6V with the LED illuminated. Switch to the 126MHz crystal and the AVO should read 2.9V with the LED illuminated.

It will be noted that with the 126MHz crystal selected and the v.f.o. (signal generator) input of 9.3MHz, the loop control voltage is 4.5V falling to 2.9V with a v.f.o. input of 8.3MHz. Swing the signal generator across the 1MHz tuning range and the control voltage will follow in step, within the above limits. Select the 125MHz crystal and repeat. The control voltage will follow in step, within the limits of 2.9V to 1.6V.

As a final check of reliable phase-lock loop operation, short circuit the "I.F. in" terminal post to chassis earth. This should cause the AVO reading to

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**Note:** The above text is a transcription of a technical document related to electronics and frequency modulation, focusing on alignment instructions and crystal discriminator measurements. The document includes diagrams and equations for different frequency points and crystal resonances. The text is dense with technical terms and requires a good understanding of electronics to comprehend thoroughly. The provided text is a comprehensive guide for setting up and testing a phase-lock v.c.o. unit, including instructions for crystal selection, frequency tuning, and operating checks. The document aims to ensure that the equipment operates within specified frequency ranges and error margins.
change to 4.9V and the l.e.d. to cease illumination - loop unlocked. Immediately the short circuit is removed, the AVO should revert to its original reading and the l.e.d. should illuminate - loop locked. Switch the 12.7V power supply on and off a number of times, and check that the loop always locks reliably from switch on, at any 8.3 to 9.3MHz input frequency.

For reliable operation the v.f.o. input should be not less than 500mV r.m.s. The i.f. input at "I.F. in" will only appear when the loop is locked, and this, measured with the valve-voltmeter diode probe, will be in the range 0.6 to 1.2V r.m.s., depending on the v.c.o. operating frequency (133.3 to 135.3MHz).

Note that it is important that the v.f.o. input drives Tr39 and the i.f. input drives Tr46 as shown. If these input connections are reversed the MC4044P phase detector will be disabled and the loop will not lock.

V.c.o. amplifier unit
Connect the signal generator set to 134.3MHz to "V.C.O. in", and the valve-voltmeter probe to "Out RX".
Adjust cores of L30 and L31 to obtain maximum r.f. output. Transfer valve-voltmeter probe to "Out TX" and check that both readings are approximately the same. The measured output should be in the range 500 to 700mV r.m.s.

V.f.o. unit
These alignment instructions assume that a 100:1 ratio gear drive is being used (i.e. 50:1 for 180 degrees rotation of C222) and that 40 turns of the tuning knob will change the v.f.o. by 1,000kHz, equal to 25kHz per turn.
Fully mesh the vanes of C222 and mark a reference point on the drum dial. Turn the tuning knob two complete turns clockwise. Mark a calibration point on the drum dial and number 0. This is 0kHz and is the start of the tuning drum scale. Now turn the tuning knob 40 complete turns, mark the calibration point on the drum dial and number 1,000. This is 1,000kHz and is the end of the v.f.o. tuning range.
Unscrew the cores of L33 and L34 so that they are outside the windings. Check that there is 8.5V feeding Tr45, Tr46, and Tr47. Connect the "V.F.O. out" terminal to the d.f.m. and with the dial at 0kHz adjust the dust core of L33 for an output frequency of 8,300kHz. Turn the drum dial to 1,000kHz and adjust C222 for 9,300kHz. These two adjustments interact with each other, and must be repeated until the d.f.m. readout is correct at each end of the tuning range. Once this has been achieved the drum dial can be calibrated each 100kHz with main divisions, and every 25kHz for intermediate divisions. Finally the tuning knob circumference is divided into 25 equal sections and numbered 0 to 24 so as to provide a calibration mark every 1kHz.
Disconnect the d.f.m. and replace with the valve-voltmeter probe and measure the r.f. output at 8,300kHz and 9,300kHz. The two readings should be approximately equal and in the range 0.9 to 1V r.m.s. (unloaded value). Set the v.f.o. output to 9,300kHz and screw in the cores of the low-pass filter L33 and L34 equally until the valve-voltmeter reading just begins to reduce. At this point unscrew each core by one turn. Alignment has been undertaken without any biasing potential on D31. When in normal operation with R190 connected to the "Calibrate" control, the mean potential on D31 will be about 2V and this will reduce the capacitance by approximately 10pF. The v.f.o. can be brought back to correct calibration by re-adjusting C222.

Receiver converter unit
Because a second signal generator is required for the heterodyning input (133.3 to 135.3MHz) to the receiver converter unit and the transmitter converter unit, it is at this stage an advantage to complete the construction by installing and wiring all units and panel controls in the main chassis - with the exception of the power amplifier.
Connect the valve-voltmeter probe to the "HET in" terminal and check that...
the input level is 500 to 700mV r.m.s. Set slider of R31 to mid position, and tuning dial to 144.9MHz. Couple 100mV output from signal generator via a 2 turn link, to L38 and adjust output transceiver tuning knob until a 1.5kHz tone can be heard from the loudspeaker. Adjust cores of L4c and L4d for maximum S-meter reading. Transfer the link to L39 and adjust the transceiver dial to 144.9MHz. Select 100mV output slider of R211 to mid position, and tuning the input level is 500 to 700mV r.m.s. Set the slider of R216 to mid position. Adjust C242 and C237 for maximum meter reading. As each circuit is brought into resonance reduce the signal generator output to avoid overflowing the following stages.

Re-set R31 as necessary to give equal voltages at source connection of Tr51 and Tr52.

Transmit converter unit

Fit a TO-5 clip-on heat sink to Tr5a and bend the vanes as necessary to clear the screening can of L52. Check that the emitter potential is 0.15V indicating a collector current of 15mA. This is not critical and can be in the range 10 to 20mA. If outside these limits it will be necessary to withdraw the p.c.b. and adjust the value of R52.

Set the transceiver tuning dial to 145MHz. Connect the valve-voltmeter probe to “HET in”, and check that the input level is in the range 500 to 700V r.m.s. Set the slider of R51 to mid position. Connect 750hm dummy load to “RF out” via two feet of coaxial cable, with the valve-voltmeter probe in parallel with the 750hm load. Set the dual cores of L4c and L4d so that each core is just level with the top of the screening can. Connect the signal generator, set to 145MHz, to test point TP5. Operate the “press-to-talk” switch and adjust trimmers C276, C277, C288 and C282 for maximum output. Unscrew cores of L2b and L2c for maximum output. Connect a 1.5kHz audio tone into the junction of L66 and C312, with the valve-voltmeter diode probe in parallel with the 750hm load. Wire a suitable ammeter in series with the 20V supply. Connect a 20V supply to the +20V line, and adjust R232 to obtain Tr57 collector current of 10mA. Reconnect the link between C288 and C289.

Unscrew the link between C203 and C214. Connect stabilised 20V supply to C230 with the milliammeter in series and adjust value of R52 to obtain Tr58 collector current of 40mA. Connect a 20V supply to the +20V terminal with the milliammeter in series. Adjust value of R51 to obtain Tr59 collector current of 90mA. Reconnect the link between C208 and C214.

Assemble the amplifier in the die-cast screening box, install in the main chassis, and complete all connections. Connect a 750hm dummy load via a two foot length of coaxial cable to the junction of L6b and C152. With the valve-voltmeter diode probe in parallel with the 750hm load. Wire a suitable ammeter in series with the 20V supply. Connect a 1.5kHz audio tone into the “MIC” socket via a 40mA attenuator. Set the output of the audio generator to zero and operate the “press-to-talk” switch. Tr58 and Tr59 should be drawing the combined quiescent collector current of 130mA.

Power amplifier

On the power amplifier, first check that the damping resistors R33b and R33a have been wired across the r.f.cs. to the bases of Tr58 and Tr59. Unsolder the link between C288 and C289 and replace with a milliammeter wired to extension leads. Connect the +12.7V supply to the +12V terminal. Adjust value of R232 to obtain Tr57 collector current of 10mA. Reconnect the link between C288 and C289.

Unscrew the link between C203 and C214. Connect stabilised 20V supply to C230 with the milliammeter in series and adjust value of R52 to obtain Tr58 collector current of 40mA. Connect a 20V supply to the +20V terminal with the milliammeter in series. Adjust value of R51 to obtain Tr59 collector current of 90mA. Reconnect the link between C208 and C214. Assemble the amplifier in the die-cast screening box, install in the main chassis, and complete all connections.

Connect a 750hm dummy load via a two foot length of coaxial cable to the junction of L6b and C152, with the valve-voltmeter diode probe in parallel with the 750hm load. Wire a suitable ammeter in series with the 20V supply. Connect a 1.5kHz audio tone into the “MIC” socket via a 40mA attenuator. Set the output of the audio generator to zero and operate the “press-to-talk” switch. Tr58 and Tr59 should be drawing the combined quiescent collector current of 130mA.

Dust core locking

It is most important that all the dust cores are an interference fit in the former and will hold their settings, and the material used must hold the core firmly but must not become solid, in case re-adjustment should be necessary at some future date. Before commencing alignment it is recommended that the screwed threads of each core and former are smeared with zinc ointment (obtainable from any chemist). The author has used this method for many years without any problems.

Operating notes

It is worth noting that the transmit output from the f.m. generator unit is a

<table>
<thead>
<tr>
<th>Test procedure</th>
<th>A.c. Line (volts)</th>
<th>Output Audio relative that at 10V input</th>
<th>Signal Input dB relative</th>
</tr>
</thead>
<tbody>
<tr>
<td>1. Signal generator on 10, 700kHz connected &quot;1F in&quot; terminal post.</td>
<td>4.4</td>
<td>20</td>
<td>0.5</td>
</tr>
<tr>
<td>2. A.g.c. a.c. 80Hz on 100mA c.c. range.</td>
<td>3.9</td>
<td>27</td>
<td>10</td>
</tr>
<tr>
<td>3. Audio output. AVO 8 on 100mA a.c. range in series with loudspeaker.</td>
<td>3.5</td>
<td>30</td>
<td>100,000</td>
</tr>
<tr>
<td>4. Source rail. 3.3 volts (2.7V BZY88 zener).</td>
<td>3.2</td>
<td>33</td>
<td>800</td>
</tr>
<tr>
<td>5. R4a set at mid position, 110 ohms.</td>
<td>2.9</td>
<td>36</td>
<td>100,000</td>
</tr>
</tbody>
</table>

It will be noted that the change in audio output is within 2dB for a change in r.f. input of 60dB and within 5dB for a change in i.f. input of 80dB. This represents very acceptable receiver r.f. performance.
c.w. carrier and the frequency modulation on the final 144 to 146MHz signal is derived from the v.f.o. Deviation is controlled by the microphone amplifier gain control potentiometer $R_{19}$ (on the f.m. generator p.c.b.), and, in the absence of a deviation meter, this can be set to accepted amateur band requirements by 'on-the-air' reports. The "CALIBRATE" control — nominally set at the mid position — will provide the required reference bias of 2 volts for the varicap diode in the v.f.o. unit.

For a final check on s.s.b. carrier attenuation, connect the "Aerial" output socket to a 75ohm dummy load with the diode probe of the valve-voltmeter in parallel across the load. Set the valve-voltmeter to the 1.5 volt range and remove the microphone from its socket. Operate the "press-to-talk" switch, and if there is a reading on the valve-voltmeter this denotes carrier leakage. Carefully re-balance the transmit modulator on the s.s.b. generator p.c.b. by adjusting $R_{11}$ and $C_{18}$ in step, until there is zero reading on the valve-voltmeter.

For the c.w. operator, transmission is conveniently effected by keying an outboard transistorised 1kHz audio oscillator fed into the microphone input socket. Both the receiver converter unit, and the transmitter power amplifier will work equally well into a 50ohm aerial system.

Modifications
As a result of more than two years "on-the-air" experience, two modifications have been incorporated to improve the s.s.b. operating convenience. These are as follows:

1. Wire a 10µF 10V capacitor across the end pins of $R_{2}$ on the printed circuit side of the s.s.b. generator p.c.b. This delays the gate 2 potential of $Tr_{3}$ and $Tr_{4}$ and prevents the transmission of a small "splash" of carrier caused by the switching transient on relay $RL_{1}$ changes over from "receive" to "transmit".

2. Relay $RL_{2}$ has a spare set of contacts which can be used to speed up the receiver a.g.c. recovery time, for those operators who like fast "break-in" operation. Connect the pole (pin 12) to chassis earth and the by-pass contact (pin 13) to chassis earth via a 47µF 25V capacitor. With a length of PVC-covered wire routed along the fold of the chassis rear apron, connect pin 13 to gate 2 of the a.g.c. amplifier $Tr_{7}$ (junction of $R_{2}$ and $R_{7}$ on the etched side of the p.c.b.) This modification shortens down $Tr_{7}$'s gate-2 potential to zero when transmitting, and prevents the switching transient feeding from the 10.7MHz i.f. amplifier into the a.g.c. system at high level.

Conclusion
This transceiver has been designed to provide a high level of performance on both transmit and receive, together with a high standard of reliability and convenience of operation.

For the f.m.-only operator, construction can be greatly simplified by omitting the s.s.b. generator unit. Repeater operation on any channel in the 145 to 146MHz section of the band can be provided by installing two crystals 300kHz apart, in the phase-lock unit. (That is, 63.0MHz and 62.7MHz giving heterodyne frequencies of 126.0MHz and 125.4MHz.) The switching lines can be taken to a spare set of contacts on the change-over relay $RL_{1}$, so that 126.0MHz is selected on "receive" and 125.4MHz on "transmit" for normal repeater operation. If reverse repeater operation is also required, it is only necessary to add a panel-operated, 2-pole 2-way switch and wire this so that the crystal switching lines can be reversed.

Because there is ample information in textbooks and other literature on stabilized power supplies, detailed constructional details have not been given. The two units used by the author incorporate simple series stabilization using BDY20 transistors with the usual BC108 and BYZ88 reference diode, and have proved to be entirely satisfactory. All prospective constructors are strongly advised to use — with the exception of the surplus S.T.C. 445-LQU 901B FM filter specified — only first class new guaranteed components and transistors.

Notes on Part 3. Component suffixes for $L_{1}$ to $L_{4}$ in Fig. 11 are incorrect and should read respectively: 53, 54, 55, 60, 57, 56, 59, 62, 61, 58, 63, 64, 65 and 66. $C_{19}$ in line four of p78 should read $C_{18}$. Fourth line of last column on p79 should read "die-cast box are mounted vertically to at either end of the chassis platform, and the squelch unit is mounted vertically on the rear panel." Caption to Fig. 16 on p80 refers to $Tr_{3a}$ and $Tr_{3b}$ and not $Tr_{7a}$ and $Tr_{7b}$ as shown. Component suffixes for $C_{19}$ to $C_{24}$ in Fig. 17 are incorrect and should read respectively: 200, 206, 203, 204 and 193. A table of d.c. voltage checks for this transceiver will be made available on request.

Books Received
Manual of Avionics, by Brian Kendal, is said by the publishers to enable the layman to acquire a working knowledge of radio nav aids, but to have as its primary aim the detailed analysis of electronics in civil aviation for the professional reader. The author, however, maintains that he has steered a middle course between the elementary and the mathematical analysis.

The book is certainly of interest to the layman, and is written at this level: it will probably not be of great help to the professional for the reasons given in the author's introduction — it is simply not possible to perform the tasks set in the book. At the layman's level, it is extremely detailed, comprehensive and authoritative, if one bears in mind that the 'avionics' of the title is restricted to communications and navigational aids, including radar.

A short historical chapter, which manages to cover everything from Clerk Maxwell to cavity magnetrons in 26 pages, is followed by seven chapters on air traffic management, radio telephony and direction-finding, short-range nav aids and radio landing systems, radar, and the hyperbolic systems and Doppler navigation.

For anyone interested in gaining a fairly superficial (in professional terms) idea of the control and navigation of civil aircraft, the book can be highly recommended for its comprehensiveness and authority: the author is Senior Air Traffic Engineer of the Civil Aviation Authority. It is published by Granada Publishing, PO Box 9, Frogmore, St. Albans, Herts. at £10.

A Window in the Sky, by A. T. Lawton, is concerned with the possibilities opened up for astronomers by the use of equipment outside our atmosphere. In contrast to many works on astronomy, the book is not only immensely detailed and factual, it is also a "good read." Mr Lawton puts the case for extra-terrestrial instruments, discusses the techniques for putting them there and examines several possible 'sites' in space. When all the equipment is in place, there is then the problem of what to investigate and, after a detour into the physics of integrated circuits and optical and radio telescopes, the rest of the book is a survey of some of the astronomical phenomena already known and others only guessed at. The book is published in hardback by David and Charles, Brunel House, Newton Abbot, Devon, at £8.50.
Astables: Logic gate circuits

by Peter Williams, Ph.D. Paisley College of Technology

A widely quoted astable circuit using inverters from the c.m.o.s. logic family is shown, using one capacitor and one resistor. A modification using a second resistor \( R_s \) is also well-known but \( R_s \) plays no part in the frequency control; rather it isolates the protective diodes at the inverter input from the voltage step applied via the capacitor, thereby protecting the input and preventing the diodes from conducting heavily and disturbing the frequency. Because only passive components are needed the circuit seems not to conform to any of types I to V (December issue). It does, however, contain a differentiator as in type IV and though the amplifier gain is much less the behaviour should be similar in this respect. The other amplifier has an inverting gain of relatively small magnitude and this corresponds to the see-saw amplifier. The other amplifier is much less the behaviour should be similar in this respect. The other amplifier has an inverting gain of relatively small magnitude and this corresponds to the see-saw amplifier of type IV. Hence this apparently new circuit is in fact type IV whether the inverters be c.m.o.s., t.t.l. or e.c.l.

Another common form of astable circuit quoted in the literature uses three inverters and a single capacitor with no passive resistors. It is sometimes described in terms of a three-phase oscillator. Such circuits are used as sinusoidal oscillators with 60° phase-shift per stage and with feedback or attenuation to limit the gain of each stage such that oscillation is not excessive. The present circuit is then argued to be a development of this with one external capacitor to define a longer time constant and hence lower the frequency. It is not then clear how the other inverters contribute to the response and the circuit certainly seems quite different from types I to V. It is unwise to press arguments based on sinusoidal response too hard when applied to switching behaviour and vice versa. The absence of a passive resistor does not mean that the circuits have no resistance. The output slope resistance of a c.m.o.s. inverter is quite high and the maximum current may be limited to < 1 mA. Hence to compare the circuit with one based on op.amps it has to be visualized with a resistor at each output.

There is a simple change that suggests a different interpretation of the circuit and allows it to be classified as a known type. The circuit is simply redrawn with the capacitor appearing to shunt two of the cascaded inverters rather than one. This involves no actual change since the capacitor is still connected across the single inverter — it is merely a changed appearance. The two cascaded inverters are equivalent to a single high-gain, non-inverting stage and, adding a resistor at the output of the first stage to represent its output resistance, the circuit is shown to be functionally identical with type V. An inverting amplifier of finite gain drives a non-inverting amplifier with capacitive feedback via a resistive path. It is important to try re-arranging unfamiliar or difficult circuits to see if various sub-sections become recognizable. Many circuit diagrams have a layout that suits the whims of a designer or the convenience of a draughtsman; they have to be made to serve the understanding of the user.

Other apparently more complex astable circuits can sometimes be simplified readily. In the circuit shown the cascaded inverters become equivalent to either a high gain inverting or non-inverting amplifier depending on whether an odd or even number of inverters is employed. Once this is noted, then this circuit is obviously a type V astable again. As in the previous circuit the external resistor offers a considerable advantage — the resulting time constant can be very large and hence the frequency can be very low while using only a small value of capacitance. If the resistor is omitted the frequency also becomes strongly dependent on supply voltage via the variation in output resistance of the individual devices composing the inverter. The multiple delays in the cascaded inverters limit the upper frequency of oscillation but the high gain makes lower frequencies less dependent on parameter variations. Such circuits are not recommended for stable frequency clock generators, a task normally performed by crystal-controlled oscillators.

Astables can also be devised that use only a single active circuit and correspond to types I and II. In some logic families Schmitt circuits are already available often with more than one input. These add the AND function to the switching action. The circuit with the unused inputs inhibited behaves like an operational amplifier with series positive feedback and the signal applied to the inverting input, i.e. when the output is returned to the input via an RC section it becomes a type I astable. When the output is positive the capacitor charges until it reaches the upper threshold voltage, switching the output to zero and discharging the capacitor back toward the lower threshold. The op.amp. and potential divider in type II comprise a non-inverting amplifier of finite gain. If the combination is replaced by a non-inverting logic buffer an astable action should again result. The missing factor is that the circuit must have a quiescent state in the capacitor's absence that brings it into the linear region. A grounded resistor is not valid for a logic gate, and is here replaced by a potentiometer. When set in the linear region oscillations commence — an additional series resistor can be used to set the frequency.
Astables: Logic gate circuits

THEORY

Both gates must enter their linear region for the loop gain to reach unity and initiate regenerative feedback. If these regions correspond to a small range of input voltages centred on $V_5/2$ the analysis is simple. For low-gain inverters both the waveforms and frequencies are less precise. It is assumed that input conduction is avoided (or minimized) as shown.

Under these conditions the outputs are anti-phase square waves with the transitions occurring as the differentiator input passes through $V_5/2$. On the positive going step this input is driven up to $V/2 + V_s = 3V_s/2$. At that instant the other end of the resistor is taken down to zero. Hence $V_1 = -3V_s/2$ while $V_2 = -V_s/2$

$$t_2 - t_1 = \tau \log_3 1.1 \tau$$

The second part of the cycle has the differentiator input driven to $V_2/2 - V_s = -V_2/2$ while the other end of the resistor rises to $V_s$. Hence $V_1 = 3V_s/2$, $V_2 = V_s/2$ giving an identical time interval.

Hence $T = 2\tau \log_3 2 = 2.2\tau$

If the circuit is interpreted as a phase-shift circuit using analysis as for a sinusoidal response, invalid results are obtained.

The modified form of the circuit has an inverter with a voltage-gain $>1$. Hence its output is saturated for most of the timing cycle, and though type V in structure, a modified analysis is required. Again the thresholds are assumed to be close to $V_2/2$ and the CR junction is driven to $3V_s/2$ and $-V_s/2$ on the transitions.

This leads to comparable values of period and frequency, viz $T = 2.2\tau$

Second-order effects are important at high frequencies where gate delays modify the response. In each case an additional large value resistor should be added in series with any gate/inverter input subject to voltage steps going outside the supply lines.

The first-order response is identical with that of the previous circuit. The Schmitt trigger is assumed to have upper and lower threshold voltages $V_u$ and $V_l$. The time for the rising ramp is

$$t_2 - t_1 = \tau \log_3 \frac{V_2}{V_1} = \tau \log_3 \frac{V_2 - V_l}{V_s - V_u}$$

and for the falling ramp $\tau \log_3 \frac{V_2 - V_u}{V_s - V_l}$

The period is $T = \tau \log_3 \left( \frac{V_2 - V_l}{V_s - V_u} \right) + \log_3 \frac{V_2}{V_s}$

$$T = T \log_3 \left( \frac{V_2 - V_l}{V_s - V_u} \right) + \tau \log_3 \left( \frac{V_2}{V_s} \right)$$

But for symmetrically placed thresholds

$$T = \tau \log_3 \left( \frac{V_2 - V_l}{V_s - V_u} \right) + \tau \log_3 \left( \frac{V_2}{V_s} \right) = 2\tau \log_3 \left( \frac{V_2}{V_s} \right)$$

EXAMPLES

1. The c.m.o.s. astable has $R = 100\,k\Omega$ and is required to oscillate at 10kHz. Assuming that $R_2$ is large enough to avoid conduction choose a suitable value of capacitance stating any assumptions.

The threshold of c.m.o.s inverters is normally within the range 45 to 55% $V_s$. It is convenient to take the threshold as $V_s/2$.

To check the effect of the variable threshold, assume each inverter switches at 0.45$V_s$

$$V_1 = V_1 + 0.45V_s$$

First time interval

$$t_1 = \tau \log_3 \left( \frac{3V_s}{2V_s} \right)$$

Second time interval

$$t_2 = \tau \log_3 \left( \frac{3V_s}{2V_s} \right)$$

This compares with a value of 2.197 for the symmetrical case if $\log_3$ is evaluated more accurately i.e. on changing the threshold by 5% of supply (or 10% of its initial value) the mark-space ratio changes from 1:1 to 1:1.12 a change of 13%, though the frequency changes by only 0.4%.

2. An astable is constructed with a c.m.o.s Schmitt circuit having upper and lower thresholds of 3$V_s$ and 6.5$V_s$ at a supply voltage of 10$V_s$. Estimate the frequency of oscillation with an RC section having $T = 500\mu s$.

The second part of the cycle has

$$V_1 = -1.55V_s$$

$$V_2 = -0.55V_s$$

First time interval

$$t_1 = \tau \log_3 \left( \frac{1.55}{0.55} \right) = 1.170\tau$$

Second time interval

$$t_2 = 2\tau \log_3 \left( \frac{1.55}{0.55} \right)$$

This result can be obtained from the general case above by substitution as in the analysis opposite.
Circuit Ideas continued

Amplitude modulator
With a 555 connected in the astable mode the timing capacitor charges and discharges between $V_{H} = 2V_{cc}/3$ and $V_{L} = V_{cc}/3$. By simultaneously increasing or decreasing $V_{H}$ to $V_{L}$ symmetrically about $V_{cc}/2$, amplitude modulation can be achieved. Resistor $R_{x}$ is a compromise between excessive drop under d.c. conditions and loading of op-amp $A_{1}$.

A. D. Teckchandani
Faridabad
India

Simple waveform generator
For audio frequencies this waveform generator offers several advantages over the usual Wien bridge circuit. No amplitude stabilization is required, there are no spasmodic interruptions to the output when switching range, and a range of 10:1 is easily achieved with a standard twin-gang potentiometer.

The integrator $T_1, T_2$, the emitter follower and the Schmitt trigger $T_6, T_3$ produce a triangular waveform at the collector of $T_2$. This output is of constant amplitude throughout the frequency range due to fixed triggering points. The triangular waveform also feeds a second integrator $T_6, T_3$, which produces a good sine wave of constant amplitude. The audio range is easily covered by three pairs of capacitors and the three outputs can be taken selectively to a single emitter follower.

F. V. Goodfellow
Southampton

Long duration timer
The two oscillators constructed from a 556 have periods $T_1 + t_1$ and $T_2 + t_2$, where the outputs of the oscillators are high during $T_1$ and $T_2$ and low during $t_1$ and $t_2$. Also, $t_1$ is much smaller than $T_1$ and $t_2$ is much smaller than $T_2$, but $T_1$ and $T_2$ are almost, but not quite, equal. When the supply is connected the oscillators start simultaneously and there is a long duration before the low periods of the oscillators overlap. When this occurs a short low pulse is produced by the 7400. The maximum interval between the pulses can be estimated as follows. Let $t_1 = t_2 = t$ and let $T_1 = T_2$. It then takes $T_1/t$ periods of the slow oscillator to overlap at the low duration. Therefore, the time delay $T$ is $T_1, T_2/t$ and can be very long. For example, if $t$ is 50μs and $T_1, T_2$ is 18 min, $T$ is 778 years. In the practical circuit with a 556 or two 555s, such long periods are not possible because the well known current spike, caused when the output of a 555 goes high, triggers the other oscillator into a low state before its high period has been completed. However, the new 355 timer should produce better results.

O. B. Hellman
Turku
Finland
Solenoid-operated cassette units

Typical applications of two new solenoid-operated cassette mechanisms, the Symot models LW 104 and YME 1006, include remote data acquisition, automatic annunciation, and processing activities in security systems. The LW 104 has been designed for use with continuous loop cassettes and is manufactured in corrosion-resistant plastic with a close-fitting translucent dust cover. The control solenoid, which operates on either 6V or 12V d.c., pulls on the pinch wheel and head assembly. The standard motor is an electronically-regulated type with an external circuit. YME 1006 is an all-metal skeleton mechanism for use with either continuous loop or conventional compact cassettes. Three forms are available — play only, record/replay with rewound facility and record/replay with cue and review facility. A (specially compounded) rubber capstan pinch roller permits permanent tape engagement without damage or roller indentation. Mono tape heads are fitted as standard and motors are mechanically regulated at 6V or 9V d.c. Symot Ltd, 22a Reading Rd, Henley-on-Thames, Oxfordshire RG9 1AG.

WW 301

Diagnostic engine tester

Diagnosis of engine timing and faults in the electrical system of petrol engines is the function of the SD-80 ignition tester manufactured by Albol Electronic and Mechanical Products. The unit is supplied from a 12V battery and the makers claim that, by its use, savings of about 10% can be made on petrol costs, although we assume that this presupposes that the engine is already operating below par. Functions covered by the tester include engine revs, ignition angle (with respect to t.d.c.), contact breaker make angle (dwell), battery voltage, h.t. voltage, plus two resistance checking ranges. The unit also powers a stroscopic lamp for advance/retard measurement and dimensions are 250 x 310 x 170mm at a weight of 4.8kg (2.21b). Price is £198 plus v.a.t. and a six-month guarantee is provided. Albol Electronic and Mechanical Products Ltd, 3 Crown St, London SE5.

WW 302

7-segment i.e.d. display

Each of the seven segments of the Highland Electronics 31-019 i.e.d. display can be illuminated separately and the unit can be panel-mounted in a single 16mm diameter round hole. Terminations are provided on a miniature p.c.b., which is an integral part of the unit's construction and extends in a vertical plane from the moulded body of the display. The terminal print on the board aligns with a standard 7-way d.i.l. socket with 2.54mm terminal spacing. Alternatively, the unit may be hard-wired. Ten connections are provided, one for each segment, one for the decimal point and two commoned negative supply terminals. The display will operate on voltages between 1.7 and 2.7V (d.c.), with each segment and the decimal point drawing 15mA continuous, 80mA pulse, for 1ms at max. voltage. The display provides, apart from numerals, upper case letters ACFHJLPUY and lower case letters bceghinory. Highland Electronics, 8 Old Steine, Brighton, East Sussex BN1 1EJ.

WW 303

Pocket frequency meter

Mobile communications applications are the areas of use which Electroplan quotes for the Labgear CM7044 portable frequency meter. This instrument covers the range 10MHz to 500MHz and it is powered by rechargeable batteries. A small antenna (with b.n.c. fitting) is provided enabling measurement of transmissions to be made without disturbing the transmitter or making internal connections. Readings are presented on a seven-segment i.e.d. display in two ranges — 10 to 50MHz and 50 to 500MHz. Electroplan Ltd, PO Box 19, Orchard Road, Royston, Herts SG8 5HJ.

WW 304

Radial component pre-former

An automatically fed machine, capable of forming and cropping up to 5000 components (radial capacitors and transistors) an hour is now available from Elite Engineering Ltd. The design of the machine allows the cropping and forming of components to the same form even where their bodies are different, without changing the tooling, although interchangeable tooling permits most different transistors to be cropped and formed for insertion in p.c. boards. Radial lead capacitors can be hopper fed if necessary or hand fed on to a belt if an especially difficult form is required. Demonstrations of the machine can be arranged or sample components sent to the makers for forming on standard
tools. Peter J. W. Noble, Elite Engineering Ltd, Unit 3, Saltern Lane, Fareham, Hants PO16 0TD.

**WW 305**

**Power supply and nicad charger**

Producing an output of 13.8V d.c. at 750mA for amateur radio transceiver operation and a second output at 45mA, constant current, for recharging nickel-cadmium batteries, the Lar Modules PS1200, permits trans-

mission from the base station while recharging is taking place. The transceiver output supply is regulated and all switching is automatic. Protection circuits are included and output 2 (charger) is at negative ground. LAP Modules Ltd, 27 Cookridge St, Leeds, LS2 3AG.

**WW 306**

**R.f.i. sealing paste**

Described as "extremely fine in texture, consisting of a high concentration of pure silver particles in silicone resin" by the makers, Emerson and Cumming (UK) Ltd, Eccoshield SX is a conductive, non-hardening sealant and gasketing material for use as an r.f. shield. Volume resistivity of the paste is less than 0.005-ohm and it can be used at temperatures from -70°F to +400°F (-56°C to +204°C) with no adverse effects. The paste's consistency can be changed by thinning with toluene and the manufacturer quotes its use on cover plates of conduit junction boxes, to replace knitted metal gaskets and on bolt threads where it can help to assure continuous electrical contact and to prevent corrosion. The claim is also made that structures sealed with Eccoshield have a measured insertion loss in excess of 100dB.

**WW 307**

**Mains socket tester**

Constructed in the form of a 13A mains plug top, a socket tester with a visual display which indicates a variety of fault conditions in a domestic mains supply is available from Galatrek. The makers say that when the tester is plugged into a socket (any form, including 5A or 15A round pin, these are connected by a length of cable) the neon display indicates "correct," "live fault," "no earth," "live/neutral reversed," "neutral fault," and "live/earth reversed." The tester costs £4.50 including v.a.t. and a 3-phase remote tester is also available at £8.95 inc. v.a.t. Galatrek, Scotland St, Lanrwst, Gwynedd, LL26 0AL, North Wales.

**WW 308**

**Tape head demagnetizer**

Demagnetization of tape heads without the need to withdraw the demagnetizing yoke away from the head at a constant speed is the claim made by TDK for its battery-operated electronic head demagnetizer, type No. HD11. The defluxing operation can be carried out in Is, and the yoke is adjustable to settings of 15° and 30° from the horizontal. The design of the unit also makes it possible to carry out defluxing of heads on many older models of tape recorder, some of which are difficult in terms of head access. TDK Tape Distributor (UK) Ltd, 11th Floor, Pembroke House, Wellesley Rd, Croydon, Surrey.

**WW 309**

**Auto transformers**

A range of transformers intended for the adaptation of modernized equipment which has been imported from the US is now available from F. H. Radford Ltd. This comprises a series of single phase auto transformers for either 240 or 220V supply, this input being transformed to 115V, by means of a single connection change. Four basic models are available as 500, 1000, 2000 and 3000VA, each of which is equipped with two American 15A 3-pin outlets and a 3-core output lead. F. H. Radford Ltd, 38 Charlotte St, London WIP 1HP.

**WW 310**

**Magazine storage rack**

A collapsible frame moulded from polythene and held together by four metal tubes constitutes the Multi-file magazine storage rack. The frame is designed to hold up to 24 issues of a fairly bulky A4 publication (such as Wireless World) although a few more can be squeezed in if required. Each magazine is fitted with two clips which pinch at either end of the spine, and located at the centre spread — these must be fitted carefully to avoid tearing — and the journal is then hung by these polythene spikes from broadcast f.m. circuits or d.c. motors. In order to maintain the 19kHz pilot tone during blanking periods, a signal generated by a car's ignition circuits or d.c. motors. In order to maintain the 19kHz pilot tone during blanking periods, a signal derived from the decoder v.c.o. is added to the input signal for a period determined by the setting of externally-controlled time constants. This method ensures that the blanking process does not impair the quality of the output signal. Further information for alternative applications is available from the distributor and the one-off price of the i.c. is £2.53 excluding v.a.t. Ambit International, 200 North Service Rd, Brentwood, Essex CM14 4SG.

**WW 311**

**Long scale panel meter**

Applications requiring higher than usual accuracy are quoted by Bach-Simpson (UK) for its new range of panel meters featuring a 250° pointer deflection angle. These meters, specified as 2123L for d.c. and 2143L for a.c. (rectified) are self-shielded, permanent magnet moving-coil instruments with non-magnetic pivots and spring-backed jewels; zero adjustment is via the front pivot. The facia dimensions of these meters are identical to the Simpson "Century" range of 3½ in panel meters. Bach-Simpson (UK) Ltd, Trenant Estate, Wadebridge, Cornwall, PL27 6HD.

**WW 312**

**Noise blanking chip**

Designed for the removal of noise spikes from broadcast f.m. com- posite signals before decoding, the Toko KB456 is claimed by the UK distributor, Ambit Inter-
ternational, to be capable of providing an improvement of approximately 25 to 30dB on the unblanked signal to noise ratio. This i.c. is specifically intended for the removal of short duration impulse noise such as that generated by a car's ignition circuits or d.c. motors. In order to maintain the 19kHz pilot tone during blanking periods, a signal derived from the decoder v.c.o. is added to the input signal for a period determined by the setting of externally-controlled time constants. This method ensures that the blanking process does not impair the quality of the output signal. Further information for alternative applications is available from the distributor and the one-off price of the i.c. is £2.53 excluding v.a.t. Ambit International, 200 North Service Rd, Brentwood, Essex CM14 4SG.
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<td>AMD 9511</td>
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**ACORN......**

S100 at NEWBEAR

**SPECTRONICS**

**UV Eprom-Erasing Lamp**

PE14* Erases up to 6 chips. Takes approx. 19 mins. **£56.00**

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---

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**20 MODELS AVAILABLE INCLUDING LED VERSIONS AND TALKING READOUTS**

<table>
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<tr>
<th>Model</th>
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<td>Crystal oven, 3 parts 10*</td>
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**RCS ELECTRONICS, WOLSELEY ROAD, ASHFORD, MIDDX. ASHFORD 53661**

**SUPPLIERS TO:** Ministry of Defence, G.P.O., B.B.C., N.P.L., Government Depts., Crystal Manufacturers and Electronic Laboratories world-wide

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VISIT OUR SHOP AT: 3 BALDOW ST, WARE, HERTF.  
TEL: 0920 3182. TELEX: 878611

**BI-PAK**

### TRANSISTORS

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### ALL PRICES INCLUDE VAT: ADD 35p POST PER ORDER

JUST QUOTE YOUR ACCESS OR BARCLAYCARD NO.
NRDC-AMBIOSONIC UHJ

SURROUND SOUND DECODER

The first ever kit specially produced by Integrex for this British NRDC backed surround sound system which is the result of 7 years’ research by the Ambisonic team. W.W. July, Aug. ’77.

The unit is designed to decode not only UHJ but virtually all other ‘quadrophonic’ systems (Not CD4), including the new BBC HJ 10 input selections.

The decoder is linear throughout and does not rely on listener fatiguing logic enhancement techniques. Both 2 or 3 input signals and 4 or 6 output signals are provided in this most versatile unit. Complete with mains power supply, wooden cabinet, panel, knobs, etc.

Complete kit, including licence fee £49.50 + VAT
or ready built and tested £67.50 + VAT

NEW S5050A STEREO AMP

50 watts rms-channel. 0.015% THD. S/N 90 dB, Mag/n 80 dB.
Output device rating 360w per channel
Tone cancel switch. 2 tape monitor switches.
Metal case—comprehensive heatsinks
Complete kit only £63.90 + VAT.

INTRUDER 1 Mk. 2 RADAR ALARM

With Home Office Type approval

The original 'Wireless World' published Intruder 1 has been re-designed by Integrex to incorporate several new features, along with improved performance. The kit is even easier to build. The internal audible alarm turns off after approximately 40 seconds and the unit re-arms. 240V ac mains or 12V battery operated. Disguised as a hard-backed book. Detection range up to 45 feet.

Complete kit £49.50 plus VAT.

Wireless World Dolby noise reducer

Trademark of Dolby Laboratories Inc.

Feature:
- switching for both encoding (low-level h.f. compression) and decoding
- a switchable t.m. stereo multiplex and bias filter
- provision for decoding Dolby f.m. radio transmissions (as in USA).
- no equipment needed for alignment.
- suitability for both open-reel and cassette tape machines.
- check tape switch for encoded monitoring in three-head machines.

Also available ready built and tested

Calibration tapes are available for open-reel use and for cassette (specify which)

Single channel plug-in Dolby PROCESSOR BOARDS (92 x 87mm) with gold plated contacts and all components

Please add VAT @ 15%

We guarantee full after-sales technical and servicing facilities on all our kits, have you checked that these services are available from other suppliers?

INTEGREX LTD.
A high-quality push-button FM Varicap Stereo Tuner combined with a 24W r.m.s. per channel Stereo Amplifier.

Brief Spec. Amplifier: Low field Toroidal transformer, Mag. input, Tape In/Out facility (for noise reduction unit, etc.), THD less than 0.1% at 20W into 8 ohms. Power on/off FET transient protection. All sockets, fuses, etc., are PC mounted for ease of assembly. Tuner section uses 3302 FET module requiring no RF alignment, ceramic IF, INTERSTATION MUTE, and phase-locked IC stereo decoder. LED tuning and stereo indicators. Tuning range 88–104MHz. 30dB mono S/N @ 1.2V. THD 0.3%. Pre-decoder ‘birdy’ filter. PRICE: £59.95 + VAT

NELSON-JONES MK.2 STEREO FM TUNER KIT
Price: £69.95 + VAT

A very high performance tuner with dual gate MOSFET RF and Mixer front end, triple gang varicap tuning, and dual ceramic filter/dual IC IF amp.  

Brief Spec. Tuning range 88–104MHz. 20dB mono quieting @ 0.75μV. Image rejection — 70dB. IF rejection — 85dB. THD typically 0.4%. IC stabilized PSU and LED tuning indicators. Push-button tuning and AFC unit. Choice of either mono or stereo with a choice of stereo decoders.

Mono £36.40 + VAT
With ICPL Decoder £40.67 + VAT
With Portus-Haywood Decoder £44.20 + VAT

STEREO MODULE TUNER KIT
A low-cost Stereo Tuner based on the 3302 FET RF module requiring no alignment. The IF comprises a ceramic filter and high-performance IC Variable INTERSTATION MUTE. PLL stereo decoder IC. Pre-decoder ‘birdy’ filter. Push-button tuning

PRICE: Stereo £33.95 + VAT

S-2020A AMPLIFIER KIT
Developed in our laboratories from the highly successful ‘TEXAN’ design. PC mounting potentiometers, switches, sockets and fuses are used for ease of assembly and to minimize wiring. Power on/off FET transient protection.

PRICE: £35.95 + VAT

BASIC NELSON-JONES TUNER KIT £15.70 + VAT
BASIC MODULE TUNER KIT (stereo) £18.50 + VAT
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EURO VHF FM TUNERSET 7252

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WIRELESS WORLD, JANUARY 1980

Specially reduced prices for ready-built Teletext Decoders... from only £160. Send SAE for details and current list.

Kits and PCBs are now available for the Ultrasonic Remote Control unit as described in recent issues of W.W. Kit includes printed-through-hole "Board 4" Kit £26.62 total.

Components necessary to build the complete decoder. A reprint of the series of articles is complete decoder. Components and installation instructions.

Heatsink and Screwdriver £5.29, + £1.73. Specially reduced prices for ready-built Teletext Decoders... also available.

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Simply ahead...

ILP'S NEW GENERATION OF HIGH

I.L.P. modular units comprise five power amplifiers, pre-amp which is compatible with the whole range, and the necessary power supply units. The amplifiers are housed and sealed within heatsinks all of which will stand up to prolonged working under maximum operating conditions.

With I.L.P. performance standards and quality already so well established, any advances in I.L.P. design are bound to be of outstanding importance and this is exactly what we have achieved in our new generation of modular units. I.L.P. professional design principles remain — the completely adequate heatsinks, protected sealed circuitry, rugged construction and excellent performance. These have stood the test of time far longer than normally expected from ordinary commercial modules. So we have concentrated on improvements whereby our products will meet even more stringent demands such, for example, as those revealed by vastly improved pick-ups, tuners, loudspeakers, etc., all of which can prove merciless to an indifferent amplifier system. I.L.P. modules are for laboratory and other specialised applications too.

PRODUCTS OF THE WORLD’S FOREMOST SPECIALISTS IN ELECTRONIC MODULAR DESIGN

AVAILABLE ALSO FROM A NUMBER OF SELECTED STOCKISTS
and staying there

PERFORMANCE MODULAR UNITS

HY5 PRE-AMPLIFIER

VALUES OF COMPONENTS FOR CONNECTING TO HY5

Volume - 10K / log.
Bass/Treble - 100K / linear.
Balance - 5K / linear.

The HY5 pre-amp is compatible with all I.L.P, amplifiers and P.S.U.'s. It is contained within a single pack 50 x 40 x 15 mm. and provides multi-function equalisation for Magnetic/Ceramic/Tuner/Mic and Aux (Tape) inputs, all with high overload margins. Active tone control circuits; 500 mV out. Distortion at 1KHz-0.01%. Special strips are provided for connecting external pots and switching systems as required. Two HY5's connect easily in stereo. With easy to follow instructions.

£4.64 + 74p VAT

THE POWER AMPLIFIERS

<table>
<thead>
<tr>
<th>Model</th>
<th>Output Power</th>
<th>Distortion Typical at 1KHz</th>
<th>Minimum Signal/Noise Ratio</th>
<th>Power Supply Voltage</th>
<th>Size in mm</th>
<th>Weight in gms</th>
<th>Price + V.A.T.</th>
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<tr>
<td>HY30</td>
<td>15 W</td>
<td>0.02%</td>
<td>80dB</td>
<td>-200 to +20</td>
<td>105x50x25</td>
<td>155</td>
<td>£6.34 + 95p</td>
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<td>HY50</td>
<td>30 W</td>
<td>0.02%</td>
<td>90dB</td>
<td>-250 to +25</td>
<td>105x50x25</td>
<td>155</td>
<td>£7.24 + 10p</td>
</tr>
<tr>
<td>HY120</td>
<td>60 W</td>
<td>0.01%</td>
<td>100dB</td>
<td>-350 to +35</td>
<td>114x50x85</td>
<td>575</td>
<td>£15.20 + 22p</td>
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<td>HY200</td>
<td>120 W</td>
<td>0.01%</td>
<td>100dB</td>
<td>-450 to +45</td>
<td>114x50x85</td>
<td>575</td>
<td>£18.44 + 27p</td>
</tr>
<tr>
<td>HY400</td>
<td>240 W</td>
<td>0.01%</td>
<td>100dB</td>
<td>-450 to +45</td>
<td>114x100x85</td>
<td>1.15Kg</td>
<td>£27.68 + 45p</td>
</tr>
</tbody>
</table>

Load impedance - all models 4 - 16.11 - input sensitivity - all models 500 mV - Input impedance - all models 100K / log - Frequency response - all models 10Hz - 45Hz - 3dB

THE POWER SUPPLY UNITS

I.L.P. Power Supply Units are designed specifically for use with our power amplifiers and are in two basic forms - one with circuit panel mounted on conventionally styled transformer, the other with toroidal transformer, having half the weight and height of conventional laminated types.

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WIRELESS WORLD, JANUARY 1980

109
AN INVITATION TO

Communications 80, the fifth in a series of international expositions dealing with the applications of telecommunications equipment and systems, particularly in the areas of data and business communications which are being created by the converging technologies of computing and telecommunications.

Communications 80 will attract visitors from all over the world (from 69 countries at the last event in 1978) who will be coming to see the latest developments in communications technology displayed by leading international manufacturers. Many of the visitors will also attend the integral conference, organised by the Institute of Electrical Engineers in association with the Electronic Engineering Association and the Telecommunications Engineering and Manufacturing Association.

Communications 80, the world's leading international exposition in the field, is actively supported by the International Telecommunication Union - the world telecommunications authority representing 153 governments; the British government, through the Home Office, the British Post Office, Cable and Wireless Ltd; and the two main UK trade associations - the Electronic Engineering Association and the Telecommunications Engineering and Manufacturing Association.

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1000mF 12V 17p; 2000mF 50V 35p; 5000mF 12V 42p

500mF 50V 65p; 1000mF 12V 17p; 2000mF 50V 35p;

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Large ceramic mag. 50-16,000 c/s.

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For 61/2in speaker and tweeter

For 13x8in or 8in speaker

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EAC. mains 200/250V Leaflet F.A.C.

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5 watts 8 ohms 5 watts 8 ohms 5 watts 8 ohms 5 watts 8 ohms 5 watts 8 ohms

50 to 14,000 cps. 10 watts. 4 ohm

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9V, 3 amp £4.00

250W 30V. 1 1/2 amp £3.60

25-0-25V Zany £4.50

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IC 300: Direct IFFM printed circuit board £6.55 + £0.85 VAT.

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FM/FM radiowaves, stereo details structure in its advertising.

Commodities

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## INTEGRATED CIRCUITS

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DISPLAY ELECTRONICS

Would like to wish all their customers and business associates a Very Merry Christmas and Prosperous New Year.
NO COMPETITION

The superb 3.77 is the only choice in compact professional recorders.

Who says?
Hundreds of satisfied professional users — Broadcast authorities, studios, record companies, universities etc etc.

What makes it the best?
The 3.77 provides more performance and features for your £ than any other model. Like 3 speeds, flat metal facia with excellent editing facilities, 100% variable speed control, logic control with motion sensing, line-up oscillator.

An ITA Product.

1-7 Harewood Avenue, Marylebone Road, London NW1. Tel: 01-724 2497. Telex: 21879

WW—890 FOR FURTHER DETAILS
Polyskop SWOB I. E450.
IT I 101 RC oscillators £65.
20WAY JACK SOCKET STRIPS. 3 pole
PYE RESISTANCE BOXES

TIP42C
0.25
0.25
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0.27
0.38

252
17
17
70
59

0.44
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ARROW HART

TRIALS

TEKTRONIX 515A Oscilloscope
AIRMEC Display oscilloscope. 4 beam.

BRUEL & KJOER Frequency analyser 2105
SOLARTRON LM 1420.2. DVM. 6 ranges to 1KV.

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**OLIVETTI PRINTER & KEYBOARD type Te 300**

with PUNCH & READER. Upper case ASCII with V24 Interface. 240 volt operation

£125 each

**TELETYPES KSR33**

Upper case ASCII with 20MA Loop. This isa printer with keyboard (no Punch or Reader on this model)

£225 each

**BRUHL & KJER EQUIPMENT**

AUDIO FREQUENCY SPECTRO METRE type 2112 £175 ea.

BEAT FREQUENCY OSCILLATOR type 1013 £140

BEAT FREQUENCY OSCILLATOR type 1014 £140

BEAT FREQUENCY OSCILLATOR type 1024 £140

AUTOMATIC VIBRATION EXCITOR CONTROL type 1018 £90

AUTOMATIC VIBRATION EXCITOR CONTROL type 1019 £90

AUTOMATIC VIBRATION EXCITOR CONTROL type 1016 £90

**TRANSISTOR INVERTER 115V 50/60 Hz INPUT**

These run at 20kHz. They can be modified to be a switching power supply or to provide EHT for VDU, Oscilloscopes, etc. or the output core could be rewound to provide any voltage/current within the units rating. As supplied they have multiple outputs. A schematic is for VDU, Oscilloscopes, etc. or the output core could be rewound to provide any

£125 each

**CROWN replacement MOTOR for IBM GOLF BALL TYPWRITERS.**

115v 50/380 1380. £6.50 each P&P £1.50

**علومات**

**INFRA RED IMAGE CONVERTER type 9606 (CV 144)**

1 1/2" aperture. Requires single low current 3KV to 6KV supply, and is individually boxed. With leads.

£12.50 each P&P 75p

Infra Red Lamps also advertised

**HONEYWELL YOu**

1920 Character Upper Case ASCII. With edit and block transmission. Limited quantity with data. **NEW LOW PRICE £200 each**

**POLARAD SPECTRUM ANALYSER**

5" Display. These are supplied with STU 2 plug-in. 1 to 4.5GHz

£125 each

**MARCONI SPECTRUM ANALYSER Type TF1094**

This gigantic but superb analyser covers from 100KHz to 30MHz with a 6Hz resolution. 5" display. Complete with trolley.

£75 each

**STEPMING MOTORS**

6/12 pinoption with additional where the motor occurs. Can be used as a tacho. Diagram supplied. Well actually work on 5 volts. 12/24 recommended.

£1.50 each P&P 75p or 5 for £5 P&P £1.50.

**CRYSTALS**

12th turning left past Reading Technical College in Kings Road then first right - look on right for door with "Spoked Wheel"

Minimum order £3 value of goods. P&P or carriage and VAT at 15% on total must be added to all orders.

CALLERS VERY WELCOME STRICTLY BETWEEN 9am-1pm and 2-5pm Monday to Saturday inc.

BARCLAYCARD (VISA) and ACCESS accepted. Official orders welcome

**CHILTHEAD**

NORWOOD ROAD, READING

TELEPHONE NO. 669656

(2nd turning left past Reading Technical College in King’s Road then first right — look on right for door with “Spoked Wheel”)
Our catalogue contains small metal enclosures for every application including the attractive new G range cases, with unique integrated chassis and sloping visor front and the inexpensive kit-form Veropak. We’ve also got circuit boards, accessories, module frames and plastic boxes—all to the highest standard to give your equipment the quality you demand. Send 40p to cover post and packing and the catalogue’s yours.

VERO ELECTRONICS LTD RETAIL DEPT.
Industrial Estate, Chandler’s Ford,
Hampshire S05 3ZR
Tel: (04215) 62829

Wireless World wishes to apologise to all parties concerned for any inconvenience caused by the publication in the December 1979 issue, of an advertisement purportedly on behalf of Nevenco Ltd. This was published due solely to an error on the part of Wireless World and not as the result of an order by any advertiser.

FOTOLAK
POSITIVE LIGHT SENSITIVE AEROSOL LACQUER

Enables YOU to produce perfect printed circuits in minutes!
Method: Spray cleaned board with lacquer. When dry, place positive master of required circuit on now sensitized surface. Expose to daylight, develop and etch. Any number of exact copies can of course be made from one master. Widely used in industry for prototype work.

FOTOLAK
£2.00
Developer 30p
Ferric Chloride 50p
Pre-coated 1/16 Fibre-glass board
204mm x 114mm £1.50
204mm x 228mm £3.00
408mm x 228mm £6.00
467mm x 305mm £9.00
Plain Copper-clad Fibre-glass
Approx. 1.8mm thick sq. ft. £2.00
Approx. 2.00mm thick sq. ft. £1.50
Approx. 1.00mm thick sq. ft. £1.75
Clear Acetate Sheet for making master: 260mm x 260mm 12p

POSTAGE AND PACKING 65p PER ORDER. VAT 15% ON TOTAL

G. F. MILWARD ELECTRONIC COMPONENTS LIMITED
369 Alum Rock Road, Birmingham B8 3DR. Telephone: 021-327 2339
8K ON BOARD MEMORY!
5K RAM, 3K ROM or 4K RAM, 4K ROM (link selectable). Kit supplied with 3K RAM, 3K ROM. System expandable for up to 32K memory.

2 KEYBOARDS!
56 Key alphanumeric keyboard for entering high level language plus 16 key Hex pad for easy entry of machine code.

GRAPHICS!
64 character graphics option — includes transistor symbols! Only £1.82 extra!

MEMORY MAPPED
High resolution VDU circuitry using discrete TTL for extra flexibility. Has its own 2K memory to give 32 lines for 64 characters.

KANSAS CITY
Low error rate tape interface.

COMPLETE KIT
Cabinet Size 19.0" x 15.7" x 3.3". Television by courtesy of Rumbelows Ltd, price £58.62

POWERTRAN COMPUTERS
POWERTRAN COMPUTERS
(POWERTRAN ELECTRONICS)
PORTWAY INDUSTRIAL ESTATE ANDOVER
HANTS SP10 3NN
(0264) 64455


The kit for this outstandingly practical design by John Adams being published in a series of articles in Wireless World really is complete! Included in the PSI COMP 80 scientific computer kit is a professionally finished cabinet, fibre-glass double sided, plated-through-hole printed circuit board. 2 keyboards PCB mounted for ease of construction, IC sockets, high reliability metal oxide resistors, power supply using custom designed toroidal transformer. 2K Basic and 1K monitor in EPROMS and, of course, wire, nuts, bolts, etc.

PSI COMP 80 Memory Expansion System
Expansion up to 32K all inside the computer's own cabinet.
By carefully thought-out engineering a mother board with buffers and its own power supply (powered by the computer's transformer) enables up to 3 8K RAM or 8K ROM boards to be fitted neatly inside the computer cabinet. Connections to the mother board from the main board expansion socket is made via a ribbon cable.

Mother Board:
Fibre glass double sided plated through hole P.C.B. 8.7" x 3.0" set of all components including all brackets, fixing parts and ribbon cable with socket to connect to expansion plug: £39.90

8K Static RAM Board:
Fibre glass double sided plated through hole P.C.B. 5.6" x 4.8". £12.50
Set of components including IC sockets, plug, and socket but excluding RAMs: £11.20
2114L RAM (16 required) Complete set of board, components, 16 RAMs: £89.50

8K ROM board:
Fibre glass double sided plated through hole P.C.B. 5.6" x 4.8". £12.40
Set of components including IC sockets, plug, and socket but excluding ROMs: £10.70
2708 ROM (8 required) Complete set of board, components, 8 ROMs: £78.50

Roppy Disk, PROM programmer and printer interface coming shortly!

Value Added Tax not included in prices

PRICE STABILITY: Order with confidence. Irrespective of any price changes we will honour all prices in this advertisement until December 31st 1979. If this month's advertisement is mentioned with your order Errors and VAT rate changes excluded.

EXPORT ORDERS: No VAT. Postage charged at actual cost plus 50p handling and documentation.

U.K. ORDERS: Subject to 15% surcharge for VAT. No charge is made for carriage. Or current rate is changed.

SECURICOR DELIVERY: For this optional service U.K. mainland only add £2.50 VAT included per kit.

UK Carriage FREE
**TERMINALS**

**EXTEL MATRIX PRINTERS**
- Optically coupled RS-232 interface
- Correspondence-quality upper / lower case
- Integral paper tape reader and punch
- Operates as stand-alone typewriter
- Selectic / EBCDIC coded
- £425 plus VAT

**IEL Model 1051**
- IBM GOLFBALL Typewriter
- RS232/V24 Interface
- £150 plus VAT

**PRINTERS**
- Matrix
- £150 plus VAT

**NEWNES TECHNICAL BOOKS FOR THE '80S**

**COMPUTER APPRECIATION,** 86 High Street, Betchlingey, Redhill, Surrey RH1 4PA
Tel: Godstone (0883) 843221

**Now you can get on-card dual output power supplies from Vero Systems — in five versions:**
- DUAL 5 Volts
- DUAL 12 Volts
- DUAL 15 Volts
- MIXED 5 and 12 Volts
- MIXED 5 and 15 Volts

The cards are designed to Eurocard standard size (100 x 164mm) to fit straight into your card or case frame.

**ORDER CODE**
- DUAL 5V: 89-2660K
- DUAL 12V: 89-2671K
- DUAL 15V: 89-2673K
- MIXED 5 and 12V: 89-9017K
- MIXED 5 and 15V: 89-9018K

**Each supply is fully regulated with over voltage current and thermal protection, input voltage 110/220v 230/240v AC and both outputs are fully isolated from each other but may be connected to give different power rail configurations. The cards are supplied fully tested each one complete with 64-way indirect connector plug, card handle and connection chart.**
YOUR LAST CHANCE to obtain Wireless World Circards. We still have some copies of the original Wireless World circuit cards, even though the companion bound volumes Circuit Designs 1 & 2* are out of print. Fill the gaps in your circuit files with these sets of 5 x 8in. (127 x 204mm) cards in plastic wallets — and at 1976 prices!

These unique circuit cards normally contain descriptions and performance data of 10 tested circuits, together with ideas for modifying them to suit special needs.

*The two out-of-print volumes contained sets 1 to 10 and 11 to 20 of Circards.

To: General Sales Department, IPC Electrical-Electronic Press Ltd., Room CP34, Dorset House, Stamford Street, London SE1 9LU.

Please send me the following sets of Circards:

1 Basic active filters 2 Switching circuits, comparators and Schmitts 3 Waveform generators 4 AC measurements 5 Audio circuits 6 Constant current circuits 7 Power amplifiers 8 Astable circuits 9 Optoelectronics 10

£2 each, £18 for ten, inclusive.

I enclose cheque/money order for £

Make cheques payable to IPC Business Press Ltd.

Name

Address

Company registered in England. Registered address, Dorset House, Stamford Street, SE1 9LU, England. Registered Number 677128
ELECTRO-TECH COMPONENTS LTD.
364 EDGWARE ROAD, LONDON, W.2. TEL: 01-723 5667

JVC-VICTOR HIGH FIDELITY STEREO CASSETTE TRANSPORT MECHANISM

ELECTRO-TECH COMPONENTS have secured a very large quantity of cassette transport mechanisms, equipped with all the latest improvements, as well as "SEN-ALLOY" type 1.5 micron record/replay heads, and solenoid-controlled auto-stop action. These were manufactured by JVC/VICTOR of Japan to specification of TANDEM OF NORWAY, for inclusion in a cassette deck costing over £280. This mechanism alone would normally cost over £50.

FEATURES:
- Close-tolerance, high-quality, top loading transport
- "SEN-Alloy" (SA type) R/P head
- Solenoid driven auto-stop circuit
- Electronic head cleaning device
- Air damped "soft" cassette eject
- Digital microswitches for switching
- Pre-aligned heads and calibrated motor speed regulator built in
- Three-digit tape position counter
- Six function keyboard controls: "Record", "Rewind", "Forward", "Play", "Stop/Eject", "Pause"
- PCB connectors and cables attached
- High mass balanced flywheel with permanent lubrication
- Full specifications for motors, heads, and switches available on request.

Price of above unit £14.95

Plus £1 P&P VAT Inc.

Regular readers of WIRELESS WORLD will know of the original LINSLEY-HOOD CASSETTE DECK design, published in May 1978. Subsequent articles by Mr. Linsley-Hood have confirmed that the design far exceeded his original expectations, so much so that he published a number of improvements, modifications, and additional features to the original design, which are now incorporated in our.

★ CASSETTE DECK KIT BASED ON DESIGN OF MR. LINSLEY-HOOD ★

We have developed an outstanding stereo cassette kit with the aid of Mr. Linsley-Hood, to complement the improved specification and latest important advances in cassette electronics since the original design was published.

Included in the kit are two fibreglass PCB's, drilled and plated for immediate assembly, two VU meters, Dual LED Peak Meters, Variable Bias system, Power Supply, over 10 micro-circuit IC's for the most up-to-date performance, as well as monitoring amplifier, test and calibration cassette, etc.

Price of Kit (without transport mech.) £15.95 plus £1.00 P&P VAT Inc.

Also available: A custom-designed case for the Kit, this is a fully screened enclosure, sloping panel, satin anodised, wood end panels, professional finish.

Price of Case £9.75 plus £1.00 P&P VAT inc.

HERE IT IS! THE BRAND NEW 8022A HAND HELD DMM

Consider the following features:
- 6 resistance ranges from 200 ohms to 60 meg.
- 8 current ranges from 2mA-2A
- 6 conductor ranges from 2mS-200nS.

£122

Cassette and Insurance £3.00

Even more sophisticated is the 8020A. Identical in most respects to the 8022A but in addition incorporates a conductance range from 2mS-200nS.

£122

Cassette and insurance £3.00

A handsome soft carrying case is available for the 8020A and 8022A at £7.

Trade and Export Enquiries Invited

IN THE COLUMN OF SPECIALS

WIRELESS WORLD, JANUARY 1980

FULLY AUTOMATIC ELECTRONIC MULTITESTER

THE 8022A HAND HELD DMM

This model incorporates all the features of the 8020A but in addition has:
- A peak hold switch which can be used in AC or DC for voltage and current functions.
- Audible continuity testing and level detection for sensing logic levels.
- A temperature (°C) range for use with a thermocouple.

£135

Cassette and insurance £3

8000A AND 8012A BENCH MODEL D.M.M.s

The 8000A is the genuine product, featuring digital display with more functions and features than ever offered for such a low price. The 8012A, has identical characteristics, but is scaled down in size and cost.

The 8000A and 8012A have 6 conductance ranges from 3m – 750V.

The 8012A has the following features:
- Three additional resistance ranges.
- Three additional current ranges.
- Three additional voltage ranges.

£230.00 each

Plus £1 P&P VAT Inc.

 lesbian & gay health prevention

LOW COST, AUTORANGING MULTI-FUNCTION COUNTER

- Accurately in both frequency and period measurement modes.
- Wide frequency range – 0 Hz to 80 KHz.
- High sensitivity: 25 Hz, typically 15 Hz.
- Digital display with leading zero suppression, automatic annunciator and push switches.
- Autoscaling in all gain ranges, all function switches.
- Four manually selectable gate times providing resolution of 0.1 Hz.
- True counting to 10^6 events with overflow indicator.
- Digital output, compatible with analogue 1-5mV low pass filter and attenuator.
- Optional parallel digital output with decimal point and led illuminator.
- Traditional high quality finish.

£175

Cassette and Insurance £3

Please add 15% VAT to all orders

WELCOME CALLERS WELCOME

We are open 9 a.m.-6 p.m. Monday-Saturday.

Carrying a very large selection of electronic components and electro-mechanical items. Special quotations on quantities.

IT 1/2 20,000OV AC/DC 0-10, 0-5, 0-2.5, 0-1K, 0-500, 0-50V
DC 0-100A, 0-0.5A, 0-50 mA. 0-250, 0-50, 0-10, 0-2.5, 0-5, 0-1 uA
Power supply - 0.1, 0.25, 0.5, 1, 2.5A, 5, 10, 20, 50W.

£10.95

Y7202 MK

AC/DC 0-1000 0-500 0-100 0-50, 0-10, 0-5V
DC 0-100A, 0-0.5A, 0-50 mA. 0-250, 0-50, 0-10, 0-2.5, 0-5, 0-1 uA
Power supply - 0.1, 0.25, 0.5, 1, 2.5A, 5, 10, 20, 50W.

£10.95

Trade and Export Enquiries Invited
ELECTRONIC KITS OF DISTINCTION FROM POWERTRAN

DE LUXE EASY TO BUILD LINSLEY-HOOD 75W STEREO AMPLIFIER £99.30 + VAT

This easy to build version of our world-wide acclaimed 75W amplifier kit based upon circuit boards interconnected with gold plated contacts resulting in minimal wiring and construction delightfully straightforward. The design was published in Hi-Fi News and Record Review and features include rumble filter, variable scratch filter, versatile tone controls and tape monitoring whilst distortion is less than 0.01%.

WIRELESS WORLD FM TUNER £70.20 + VAT

A pre-aligned front-end module makes this Wireless World published design very simple to construct and adjust without special instruments. Features include an excellent a.m. rejection push-button station selection as well as infinitely variable tuning and a phase locked loop stereo decoder incorporating active filters for ‘birdy’ suppression.

LINSLEY-HOOD CASSETTE DECK £79.60 + VAT

This design published in Wireless World, although straightforward and relatively low cost provides a very high standard of performance. There are separate record and replay amplifiers and switchable equalisation together with a choice of bias levels are also provided. The mechanism is the Goldring-Lenco CRV with electronic speed control.

TRANSCENDENT 2000 SINGLE BOARD SYNTHESIZER

As featured in Electronics Today International

The kit includes fully finished metalwork, fully assembled solid task cabinet, filter sweep pedal, professional quality components (all resistors either 2% metal oxide or 1/2% metal film) and it really is complete — right down to the last nut and bolt and last piece of wire! There is even a 13A plug in the kit — you need buy absolutely no more parts before plugging in and making great music! Virtually all the components are on the one professional quality glass PCB printed with component locations. All the controls mount directly on the main board, all connections to the board are made with connector plugs and construction is so simple it can be built easily in a few evenings by almost anyone capable of neat soldering! When finished you will possess a synthesizer comparable in performance and quality with ready built units selling for between £500 and £700.

COMPLETE KIT ONLY £168.50 + VAT!

Comprehensive handbook supplied with all complete kits! This fully describes construction and tells you how to set up your synthesizer with nothing more than a multi-meter and a pair of ears!

CHROMATHEQUE 5000 5-CHANNEL LIGHTING EFFECTS SYSTEM

This versatile system featured as a constructional article in ELECTRONICS TODAY INTERNATIONAL has 5 frequency channels with individual level controls on each channel. Control of the lights is comprehensive to say the least. You can run the unit as a straightforward sound-to-light or have it strobe all the lights at a speed dependent upon music level or front panel control setting or use the internal digital circuitry which produces some superb random and sequencing effects. Each channel handles up to 500W and as the kit is a single board design wiring is minimal and construction very straightforward.

COMPLETE KIT ONLY £49.50 + VAT!

Complete kit includes fully finished metalwork, fibreglass PCB's, controls, wire, etc. — Complete right down to the last nut and bolt!

MrA200 100W MIXER/AMPLIFIER

Featured as a constructional article in Electronics Today International the MPA 200 is an exceptionally low-priced but professionally finished general purpose, rugged, high power amplifier which has an adaptable range of inputs such as disc, microphone, guitar etc. There are 3 wide-range tone controls and a master volume control. Mechanically the design is simplicity in the extreme with minimal wiring making construction very straightforward. Kit includes fully finished metalwork, fibreglass PCB's, controls, wire, etc. — Complete right down to the last nut and bolt!

COMPLETE KIT ONLY £49.90 + VAT!

All kits also available as separate packs (e.g. P.C.B. component sets, hardware sets, etc.). Prices in FREE CATALOGUE.
T20+20 AND T30+30 20W, 30W AMPLIFIERS

**SPECIAL PRICES FOR COMPLETE KITS**

- T20+20 KIT PRICE £33.10 + VAT
- T30+30 KIT PRICE £38.40 + VAT

**SOLD AS COMPLETE KITS ONLY**

- T20+20 deliver 20W rms per channel of true Hi-Fi at exceptionally low cost. The easy-to-build design is based on a Toroidal transformer and new amplifier circuitry. This unit matches well with the T30+30.

**WE’VE MOVED! NEW FACTORY UP! PRICES DOWN!**

**DIGITALLY CONTROLLED, TOUCH SENSITIVE, POLYPHONIC, MULTI-VOICE SYNTHESIZER**

The Transcendent DPX is a really versatile new 5 octave keyboard instrument. There are two audio outputs which can be used simultaneously. The overall effect of this is similar to that of several acoustic instruments playing the same piece of music. The ensemble circuitry can be switched in with either string or metal tone. Although the DPX is an advanced design using a very large amount of circuitry, much of it very sophisticated, the kit is mechanically extremely simple, very straightforward to assemble and contains many features which can be varied by the user.

**COMPLETE KIT ONLY £299.00 + VAT**

- Complete kit only includes power supply, keyboard, interface socket, synthesizer board, button board, on-off switch, variable delay control.

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<th>Price</th>
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<td>SCLUMBERGER-SOLARTRON 5½ digit Digital Multimeter A243</td>
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<td>4½ digit D.M. M. 7050</td>
<td>£350</td>
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<td>D.M.M (Microprocessor configured, serviced 7065)</td>
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<td>OSCILLOSCOPES</td>
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<td>Storage Scope OS2200</td>
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<td>30MHz Dual Trace DCDU 150</td>
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<td>75MHz Dual Trace 4100</td>
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<td>HEWLETT PACKARD 500KHz High Sensitivity 130C</td>
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<td>7MHz Dual Trace 1707B</td>
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<td>T.D.R. System 140A + 1414A</td>
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<td>5MHz Battery Miniscop PM3010</td>
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<td>15MHz Portable Dual Trace PM3212</td>
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<td>X1 Probe Kit EB80</td>
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<td>SUPPLEMENTARY</td>
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<td>RECORDERS</td>
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<td>BRUSH Multipoint B Channel Chart Recorder</td>
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<td>SHANDON SOUTHERN</td>
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<td>6 Channel Recorder 10-650</td>
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<td>YOKOGAWA</td>
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<td>2 Channel Chart Recorder 3047 £530</td>
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<tr>
<td>3003 Sweeper Main Frame c/w</td>
<td>£750</td>
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<td>3302, 3331, 3341, 3351, 3360 and 3370 modules. Frequency range: 0-300MHz sweep width 0-100% of the range 0-62dB with 0.1dB attenuation in 10dB steps. Power supplies: 0/5V with 0.1% stability. Internal detector. £1,150</td>
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<td>1365 Lin Log Sweep Function Generator, 0-2Hz</td>
<td>£275</td>
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<td>2Hz-10V 500 Hz. Sine and triangle. Sweep time 10yrs 10000s</td>
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<td>SOUND LEVEL METERS</td>
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<td>BRUEL &amp; KJAER</td>
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<td>Sound Level Meter 2203</td>
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<td>Portable Sound Level Meter, 1993</td>
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<td>Channel Logic Analyser 1650</td>
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<td>True R.M.S. Voltmeter 933</td>
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<td>AM/FM Mod. Meter 1785</td>
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<td>Power Meter 432A + 475</td>
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<td>Power Meter 330A + 475</td>
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<tr>
<td>Functional Generator PM 521</td>
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<tr>
<td>Sine, square, triangle, single shot with</td>
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<td>variable phase, 0-10V with 0.1% stability.</td>
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<td>MARCONI INSTRUMENTS</td>
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<td>Function Generator, Up to 500MHz £1200</td>
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<td>2003 Sweeper Main Frame, 0-300MHz 650£</td>
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<td>Pattern Generator PM521</td>
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<td>AM Multimeter PM2454B</td>
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<td>AM Multimeter PM3501</td>
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<td>AM Multimeter PM2607</td>
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<td>AM Multimeter PM2622</td>
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<td>ELECTRONIC BROKERS</td>
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<td>£275</td>
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The table above lists various test equipment and their prices. The prices are in British pounds (£).
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- Programmable Cold Junction Compensation
- Complete with Adjustments
- Platinum R/T Stability for C.J.C.
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Tel. 727 5841 Telex 261306

SPECIAL OFFER OF BRAND NEW USSR MADE MULTIMETERS

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<th>U4315</th>
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<td>20,000 o.p.v.</td>
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<td>Sensitivity A.C.</td>
<td>2,000 o.p.v.</td>
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<td>D.C. Current</td>
<td>60µA-1.5A</td>
<td>50µA-2.5A</td>
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<td>A.C. Current</td>
<td>0.6mA-1.5A</td>
<td>0.5mA-2.5A</td>
</tr>
<tr>
<td>D.C. Volts</td>
<td>75mV-600V</td>
<td>75mV-1000V</td>
</tr>
<tr>
<td>A.C. Volts</td>
<td>15V-600V</td>
<td>1V-1000V</td>
</tr>
<tr>
<td>Resistance</td>
<td>1k-1M</td>
<td>20k-50k</td>
</tr>
<tr>
<td>Capacity</td>
<td>0.5µF</td>
<td>0.5µF</td>
</tr>
<tr>
<td>Accuracy</td>
<td>1.5% D.C.</td>
<td>2.5% D.C.</td>
</tr>
<tr>
<td>Price complete with pressed steel carrying case and test leads</td>
<td>£10.50</td>
<td>£10.50</td>
</tr>
<tr>
<td>Packing and postage</td>
<td>£1.50</td>
<td>£1.50</td>
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<table>
<thead>
<tr>
<th>TYPE</th>
<th>U4324</th>
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<tbody>
<tr>
<td>D.C. Current</td>
<td>0.06-0.6-60-600mA-4.3A</td>
</tr>
<tr>
<td>A.C. Current</td>
<td>0.3-3-300mA-3A</td>
</tr>
<tr>
<td>D.C. Voltage</td>
<td>0.6-1.2-12-30-60-120-500-1200V</td>
</tr>
<tr>
<td>A.C. Voltage</td>
<td>3.6-15-60-150-300-600-900V</td>
</tr>
<tr>
<td>Resistance</td>
<td>500(1)-5(5)-500k(4)</td>
</tr>
<tr>
<td>Accuracy</td>
<td>0.5% D.C., 2.5% A.C., 4% (of F.S.D.)</td>
</tr>
<tr>
<td>PRICE</td>
<td>£9.50</td>
</tr>
<tr>
<td>Packing and postage</td>
<td>£1.20</td>
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<table>
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<tr>
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<tbody>
<tr>
<td>COMBINED WITH SPOT FREQUENCY OSCILLATOR</td>
<td></td>
</tr>
<tr>
<td>Sensitivity</td>
<td>20.000µV/V</td>
</tr>
<tr>
<td>Voltage ranges</td>
<td>2.5-1000V A.C./D.C.</td>
</tr>
<tr>
<td>Current ranges</td>
<td>0.05-500mA D.C. only</td>
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<tr>
<td>Resistance</td>
<td>5/1MQ</td>
</tr>
<tr>
<td>Accuracy</td>
<td>5% F.S.D.</td>
</tr>
<tr>
<td>Oscillator output</td>
<td>1kHz 50/50 squarewave</td>
</tr>
<tr>
<td>Frequency</td>
<td>485kHz sine wave</td>
</tr>
<tr>
<td>PRICE, in carrying case, complete with leads and manual</td>
<td>£8.00</td>
</tr>
<tr>
<td>Packing and postage</td>
<td>£1.00</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>TYPE</th>
<th>U4341</th>
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<tbody>
<tr>
<td>COMBINED MULTIMETER AND TRANSISTOR TESTER</td>
<td></td>
</tr>
<tr>
<td>Sensitivity</td>
<td>16:700µV/V D.C. , 3.300µV/A.C.</td>
</tr>
<tr>
<td>Current</td>
<td>0.06-0.6-6-60-600mA D.C. , 0.3-3-30-300mA A.C.</td>
</tr>
<tr>
<td>Voltage</td>
<td>0.3-5.5-30-150-300-900V D.C.</td>
</tr>
<tr>
<td>Resistance</td>
<td>1.5-7.5-30-150-300-750V A.C.</td>
</tr>
<tr>
<td>Transistors</td>
<td>Collector cut-off current 60A max</td>
</tr>
<tr>
<td>D.C. current gain 10.350 in two ranges</td>
<td></td>
</tr>
<tr>
<td>PRICE, complete with steel carrying case, test lead, battery and instruction manual</td>
<td>£9.50</td>
</tr>
<tr>
<td>Packing and postage</td>
<td>£1.50</td>
</tr>
</tbody>
</table>
ELECTRONICS TEST ENGINEERS

We need your skills to stay true to type

equivalent. you could build a great career with us. A knowledge of analogue circuitry would be an added advantage. The work is deeply interesting and stimulating—and never routine. Staff facilities include superb working conditions, sick pay scheme, a subsidised canteen and relocation expenses where appropriate. And salary structures are highly competitive. Posts are open to both men and women. For full details, write or telephone to the Personnel Department, Linotype-Paul Limited, Runnings Road, Cheltenham. Tel: Cheltenham 45001.

Linotype-Paul
AMPEx

AMPEx Corporation, a world leader in analogue and digital data recording technology, has been designated the official supplier of video recording and magnetic tape products to the 1980 Moscow Olympics. Early in 1980 the Group’s Training Department in Reading will need an additional

INSTRUCTOR

IN BROADCAST TELEVISION COLOUR CAMERAS AND VIDEO TAPE RECORDERS

This is an opportunity to join a company in the forefront of technological innovation in a position involving contact with engineers from all over the world and some overseas travel.

The essential qualifications are:

* experience as, or personality to become, an expert instructor training engineers of many nationalities.
* sound knowledge of advanced electronics, particularly in the broadcast television field.
* sound knowledge of foreign language would be useful.

An attractive salary and benefits package is offered.

Please telephone Clive Legg on Reading 85200, Ampex Great Britain Limited, Acre Road, Reading, Berks.

ANTENNA SALES ENGINEER

Unusual opportunity for introducing Kathrein FM, TV and communication transmitting antennas to UK customers and to increase sales of Spiner and Kabelmetal products in the same market.

The job entails calling on existing customers throughout the UK, developing new customers, the preparation of quotations and tenders and assisting customers with their technical problems.

The successful candidate will be over 25 and preferably have good sales ability, suitable experience and qualifications. A good salary and an above average car will be offered. Four weeks’ holiday per annum and a non-contributory pension scheme complete the package.

Please apply in writing, marked confidential, to:

The Managing Director

Hayden Laboratories Limited

HAYDEN

Foreign and Commonwealth Office

Telecommunications Officers

in London and at Hanslope Park, Milton Keynes, for work in the installation, modification, maintenance and operation of HF, VHF, UHF and microwave receivers, associated test equipment, recorders, telephone and teleprinter equipment, electronic ancillary apparatus (some using analogue and digital techniques), voice frequency telegraph and other specialised equipment.

Candidates must have served an apprenticeship or have had equivalent training. They should normally have 3 years’ relevant experience, and hold ONC in Engineering (with pass in Electrical Engineering ‘A’) or Applied Physics or TEC/SCOTEC certificate or equivalent qualification in a relevant subject. Ex-Service personnel who have had suitable training and at least 3 years’ appropriate service (as Staff Sergeant or equivalent) will also be considered.

Salary: £4,575-£6,100; London £780 more. Starting salary may be above the minimum for those with more relevant experience. Promotion prospects. Non-contributory pension scheme.

For further details and an application form (to be returned by 17 January, 1980), write to Civil Service Commission, Alencon Link, Basingstoke, Hants RG21 1JB, or telephone Basingstoke (0256) 68551 (answering service operates outside office hours). Please quote T/5274.
**Career Opportunities in Audio Electronics**

**Dolby Laboratories**

The UK operation of this international name in audio electronics manufactures a comprehensive range of professional noise reduction systems which is employed world-wide in the broadcasting, recording and film industries. Dramatic increase in world demand has stimulated the company's development, creating the following exciting career opportunities.

**Application Consultants** c. £9,000

Reporting to the International Marketing Director, the prime responsibility will be the provision of a full technical consultancy to professional users. Major activities will include advice on specifications and equipment compatibility in cinemas and studios; training installation and service technicians; distributor and end-user liaison; field servicing and trouble-shooting operational problems; and sound consultancy during film dubbing.

Candidates are likely to have a broad-based audio background ideally including practical experience in electronics, as well as professional recording and mixing. Essential personal qualities include the ability to work with considerable autonomy and flexibility to high professional standards. World-wide travel is involved for which a working knowledge of a European language would be an advantage. Ref AA57/7146/WW.

**Production Engineers**

*(Electromechanical & Electronic)* c. £7,000

Reporting to the Production Director, the principal responsibilities of these posts will include the introduction of new products to line production; production improvements/trouble-shooting; modification control; and liaison with the California-based R & D team. The electromechanical engineer will have prime responsibility for all mechanical aspects of production, with major emphasis on assembly processes; jig, fixture and tool design; and packaging. The electronics engineer will have responsibility for defining test procedures and for the design, development, specification, and/or procurement of test equipment. An analogue background is desirable.

Candidates, probably in their mid-20s to 30s, will be of graduate or equivalent status, and should be able to demonstrate an ability to produce reliable, cost-effective solutions. Considerable autonomy is offered; experience gained in a small-company environment would be an advantage. Ref TE61/7147/WW.

**Inspection Supervisor** c. £7,000

Reporting to the QA Manager, the Supervisor will assume full responsibility for inspection of 'in-house' assembly operations. Key tasks will be the motivation, control, training and development of the inspection team, and the preparation and analysis of inspection reports and quality investigations to improve both quality standards and cost-effective production. This post is likely to appeal to young electronics engineers (from age 23 years) who seek a stepping stone into line management. The attractive salaries will be supplemented by competitive benefits which include relocation assistance. Location: London SW9.

Initial interviews are conducted by PA Consultants. No details are divulged to clients without prior permission. Please send brief career details or write for an application form; quoting the appropriate reference number on both your letter and envelope, and advise us if you have recently made any other applications to PA Personnel Services.

---

**King's College, London**

**Electronic Technician**

For interesting work in busy Physics Research Department including construction, repair and maintenance of equipment. Experience in integrated circuits and digital electronics desirable.

Good conditions. 5-weeks' annual holiday. Superannuation scheme. Interest-free loans for annual rail season tickets. Salary on scale £4,480 p.a. to £5,100 p.a. inclusive (under review).

Apply in writing with full details to: The Head Clerk (Ref. 221743/WW), King's College, London, Strand WC2R 2LS.

**PA Personnel Services**

Hyde Park House, 6th Knightridge, London SW1X 7LE. Tel: 01-215 6006 Telex: 27874
AMPEX

BROADCAST VTR ENGINEERS

FOR MIDDLE EAST AND AFRICA BASED IN ATHENS

We seek HNC calibre Electronics Engineers or those with equivalent experience, to whom product training will be given. They will be required to travel and work independently and to join our highly professional team serving this area from its Regional Office in Athens.

Salaries reflect the demanding nature of the job. Assistance with relocation, rent, education expenses will be given. Pension, medical expenses and insurance.

Write fully to Don Cameron, AMPEX, P.O. Box 45, Halandri, Athens, Greece, or for application form from Clive Legg, Ampex Great Britain Ltd., Acre Road, Reading, Berks. on Reading 85200.

The Group parent company, Ampex Corporation, has been designated the official supplier of video recording and magnetic tape products to the 1980 Moscow Olympics.

---

Electronic Engineers – What you want, where you want!

TJB Electrotechnical Personnel Services is a specialised appointments service for electrical and electronic engineers. We have clients throughout the UK who urgently need technical staff at all levels from Junior Technician to Senior Management. Vacancies exist in all branches of electronics and allied disciplines - right through from design to marketing - at salary levels from around £4000 to £8000 p.a.

If you wish to make the most of your qualifications and experience and move another rung or two up the ladder we will be pleased to help you. All applications are treated in strict confidence and there is no danger of your present employer (or other companies you specify) being made aware of your application.

TJB ELECTROTECHNICAL PERSONNEL SERVICES, 12 Mount Ephraim, Tunbridge Wells, Kent. TN4 8AS.

Tel: 0892 39388

Please send me a TJB Appointments Registration form:

Name ..................................................
Address ..................................................
How to get second interviews without having first ones, you have to cut a few corners.

All too often, first interviews are unnecessary. You provide a mass of information for the second or third time. You're screened by comparatively junior people. And you have to invent some excuse for being away from your own job at an inconvenient time. Second interviews are when it all happens. You meet the decision-makers and you know they're interested. Lansdowne can save you from wasteful first interviews. Just fill in and send us this coupon and you will receive our ‘First Interview’ form. And, because we have access to the opportunities in over 3,000 companies, large and small, we can match you with the situations that might suit you.

The employer will then get in touch with you directly and invite you to what is, in effect, a second interview. From then on, it's up to you. As you'd expect from Britain's most professionally respected register, we maintain total confidentiality throughout. And you can specify those companies to which you do not want your particulars sent. Cutting corners could save you a great deal of time. Why not cut a few right now?

Lansdowne Appointments Register, Design House, The Mall, London W5 5LS. Tel: 01-579 2282 (24 hour answering service).

Our clients would like to meet men and women, aged 20-40 years, earning between £4,000 and £8,000, from any of the following areas — (please tick where appropriate).

☐ Service Engineers  ☐ Audio Engineers  ☐ Technicians
☐ Test Engineers  ☐ Sales Engineers

Name

Address

Lansdowne Appointments Register, Design House, The Mall, London W5 5LS. Tel: 01-579 2282. (24 hour answering service).
RADIO OFFICERS

If your trade or training involves radio operating, you qualify to be considered for a Radio Officer post with the Composite Signals Organisation.

A number of vacancies will be available in 1980/81 for suitably qualified candidates to be appointed as Trainee Radio Officers. Candidates must have had at least 2 years’ radio operating experience or hold a PMG, MPT or MRGC certificate, or expect to obtain this shortly.

On successful completion of 40 weeks’ specialist training, appointees move to the Radio Office Grade.

Salary Scales:

<table>
<thead>
<tr>
<th>Trainee Radio Officer</th>
<th>Radio Officer</th>
</tr>
</thead>
<tbody>
<tr>
<td>Age 19 £3271</td>
<td>Age 19 £3961</td>
</tr>
<tr>
<td>Age 20 £3382</td>
<td>Age 20 £4107</td>
</tr>
<tr>
<td>Age 21 £3485</td>
<td>Age 21 £4243</td>
</tr>
<tr>
<td>Age 22 £3611</td>
<td>Age 22 £4359</td>
</tr>
<tr>
<td>Age 23 £3685</td>
<td>Age 23 £4571</td>
</tr>
<tr>
<td>Age 24 £3767</td>
<td>Age 24 £4854</td>
</tr>
<tr>
<td>Age 25+ £3856</td>
<td>Age 25+ £5166</td>
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</tbody>
</table>

then by 5 annual increments to £6981 inclusive of shift working and Saturday, Sunday days.

For further details telephone Cheltenham 21491 Ext. 2269, or write to the address below.

GCHQ Recruitment Office
Government Communications Headquarters
Oakley, Priors Road, Cheltenham GL52 5AJ

TELEVISION PROJECTS ENGINEERS

We have vacancies in our expanding Projects Section for Junior and Intermediate engineers. Responsibilities cover all stages of custom-built vision/audio switching system manufacture from customer liaison through design, production and test to final acceptance.

The positions offer the chance for energetic engineers with initiative to join a vision/audio switching system manufacture from customer liaison through to many professional TV broadcasters in the UK and Europe. A certain amount of travel here and abroad could be involved.

In particular this opportunity would suit engineers possessing some experience in electronic testing wishing to expand their horizons and gain experience in television broadcast systems.

In addition to a good salary the company offers profit-sharing and non-contributory pension schemes, free BUPA membership, a friendly environment in rural settings and excellent career prospects.

For more details contact David Steel at:

pro-bel LIMITED
TELEPHONE BRACKNELL (0341) 56869/56960

MARTIN-BAKER (ENGINEERING) CO. LTD.
has a vacancy for an

ELECTRONIC TECHNICIAN

AT CHALGROVE AIRFIELD, OXFORD

The successful applicant will be required to assist small team, on commissioning and operation of telemetry and instrumentation systems for ejection seat trials.

QUALIFICATIONS — Ability to make prototype units from rough drawings and test to specifications using standard test equipment. Knowledge and experience of U.H.F. Trans/Recs., tape recorders and logic systems. (Gained as a radio amateur perhaps).

Salary range £5500–£5700 per annum. Weekly paid 40-hour week. 22 days’ holiday per year, non-contributory pension scheme after five years.


Editorial writer for Wireless World

Wireless World needs a new person on its editorial staff. Technical experience in electronics and/or communications and an ability to write are essential. The work is varied and includes writing technical news reports and other material, attending meetings, exhibitions, press conferences and other events, some abroad, and editing contributed technical articles. A good deal of freedom will be given to a person who shows ability and responsibility. Preferred age range 25 to 35.

Write to: The Editor
WIRELESS WORLD
Dorset House, Stamford Street
London SE1 9LU

TECHNOMARK
Engineering and Technical Recruitment
11 Westbourne Grove
London W2 01229 9239

APPointments in
ELECTRONICS
£5 - £10,000

Missiles — Medical
Computers — Medical
Radar — COMMS
Hardware — Software

For free expert advice and immediate action on salary and career improvement, phone or write to: Mike Gemmell BSc.

ANDROMICA (T.V.) LTD.
34 Rockingham Road
Uxbridge, Middelx
Tel. Uxbridge 57971

VIDEO ENGINEERS

Experienced Video Engineers are required for important work, mainly in the field of high security systems. Some work on short contracts is available in the Middle East, North Africa etc, if required, but not mandatory. A company car, pension scheme and generous salary can be expected but loyalty and a determination to do the job well are necessary. We are looking for Engineers who expect to earn £4,000 - £7,000.

Please apply to:
ANDROMICA (T.V.) LTD.
34 Rockingham Road
Uxbridge, Middlesex
Tel. Uxbridge 57971
HNC Level Engineers

(Electrical or Electronic)

Train for the future as a
Broadcast Transmission Engineer

Through our network of over 500 transmission stations the IBA is responsible for the transmission of all Independent Television and Local Radio services. With a steadily increasing number of stations, the preparations for the fourth television channel and more local radio stations now underway we are taking on increased responsibilities.

We take great pride in the fact that our system is one of the best in the world and great importance is placed on maintaining the efficiency of the service. To do this we have teams of highly trained and experienced engineers all over the country.

Internal promotions and continued expansion have created a number of opportunities for H.N.C. or H.T.C. or equivalent level engineers (male or female) to train for a challenging future. Our carefully devised training programme, which will commence this summer, can lead to a recognised Diploma and combines theoretical study and practical training. This comprehensive training is a step beyond traditional learning and gives a grounding in broadcast engineering that is second to none. Naturally, course fees, accommodation and meals will be paid during the course. A full driving licence is required, but if you do not already have one, we will assist you by arranging and paying for instruction.

On the satisfactory completion of the training programme, your salary will be £5,880 per annum and then rise annually to £7,280 per annum, with further progression to £8,202 per annum. (During the training period you will receive a salary of up to £4,700 per annum, depending upon experience.) At higher levels it will be up to you to demonstrate your ability as promotions are based on internal competition - all of our Regional engineering managers started their careers at transmitting stations.

Employment benefits include Free Life Assurance and Personal Accident Schemes, a Contributory Pension Scheme, generous relocation expenses and subsidised mortgage facilities.

Please write or telephone Mike Wright for a fully illustrated information package and application form, at IBA, Crawley Court, Winchester, Hampshire SO21 2QA. Telephone: Winchester 822574.
Appointments

**DESIGN ENGINEER**

Thorn Consumer Electronics Limited, leading manufacturers of television and audio equipment in the U.K., wish to appoint an experienced Design Engineer for their Research and Engineering centre at Enfield.

The successful applicant will join a team investigating new ideas and systems for the television industry and should have a degree or equivalent, with at least two years in television design, with some digital design experience, and be preferably under 35 years of age.

The ability to work on his/her own initiative, liaising with internal development departments and outside suppliers, is essential.

Please apply in writing, stating age, experience and qualifications to:

The Personnel Manager, (DE/WWW),

**THORN CONSUMER ELECTRONICS LTD.**
Great Cambridge Road, Enfield, Middlesex, EN1 1UL.

---

**JUNIOR DEVELOPMENT ENGINEERS**

**ELECTRONICS**

John Player and Sons, a leading manufacturer of tobacco products, offers the following opportunities to young electronics engineers to gain valuable practical experience in industrial electronics.

Vacancies exist for work in the Machinery Evaluation Section where new generation cigarette making and packing machines are undergoing pre-production trials. These machines are equipped with increasing numbers of modern electronic control circuits and include microprocessors.

The successful applicants will undergo a period of familiarisation, look after specific machines during the evaluation period, be involved in the development of special features as well as devising evaluation aids and ultimately in the training of others in the maintenance of these machines on the production floor.

We are looking for men or women who are qualified to HNC or equivalent, and have 2 years’ experience in one or more of the following areas:

- electronic control and logic circuits
- process control systems
- microprocessors

A knowledge of the tobacco industry is not essential.

We offer a starting salary of £5,500 per annum together with other benefits including relocation assistance where applicable.

Application forms can be obtained by phoning Nottingham (STD 0602) 787711 Extension 345 or writing to:

Lorna Blayney

**JOHN PLAYER AND SONS**

Nottingham NG7 5PY

---

Manufacturers of professional film and video equipment now need the following staff:

**ELECTRONICS DESIGNER**

An engineer with some experience is required to join a small design team working on a variety of projects. Fields of interest include logic, analogue and power control circuits. The level of work would suit a Graduate or someone with relevant design experience.

**ELECTRONICS TECHNICIANS**

There are vacancies for test personnel for fault finding and general testing of PCB’s and equipment. Some experience of logic and analogue circuits is essential.

The above vacancies are suitable for men or women. If you are interested in either of them please telephone Nigel Gardiner on 01-543 3131, or come along and see us.

**PAG GROUP**

565 KINGSTON ROAD, RAYNES PARK
LONDON, SW20

---

**GUERNSEYMEN**

come home, we need you here!

We have vacancies for, **ELECTRONICS ENGINEERS** and a **DRAUGHTSMAN**

We are forming a Product Development group within our company here in Guernsey which will be involved in the introduction, appraisal, and design of new products aimed at our European Markets.

We are in the business of manufacturing data communications equipment including sophisticated microprocessor-based monitoring and test equipment. We have immediate vacancies for Engineers with experience in one or more of the following areas:

- Systems, Analogue, Software, and digital design.

We also have a vacancy for a Draughtsman with electronics experience.

Applicants, who must have Guernsey residential qualifications are invited to write to the Personnel Manager giving details of experience and qualifications.

---

**ROHDE & SCHWARZ**

Independent concern represented in 80 countries

**SENIOR TEST AND CALIBRATION ENGINEERS**

With a background in RF and microwave experience, in analogue, digital techniques, logic and microprocessor controlled ATE also vacancies exist for

**TEST & CALIBRATION ENGINEERS**

with knowledge of one or more of the above techniques.

We offer an exceptional salary, performance related bonus scheme, training abroad, prospects of promotion, a wide variety of work, a happy atmosphere, a non-contributory pension scheme and subsidised restaurant.

Please write or phone to:

Mr. Z. Eres (Technical Manager) extension 43.

Electronic Instruments & Communications Equipment

aveley electric LTD

Roebuck Road
Chesington
Surrey KT9 1LP

01-397 8771

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**ITA EXPANSION**

We need more high-calibre engineers conversant with current recording equipment. Applicants must be able to assume responsibility in return for an attractive salary and secure future.

Apply: Chief Engineer
ITA, 1-7 Harewood Avenue
Marylebone Road
London, N.W.1
01-724 2497

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**CAPITAL APPTS.**

**FREE LISTS**

**OF DESIGN/DEVELOPMENT** and **Test Jobs**

Permanent and Contract

To £6,500

01-543 3131
day: 636 9059 eve

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**Dyatech DATA COMMUNICATIONS LTD**

Place du Commerce, Bouet, St Peter Port, Guernsey
Telephone 0481 26475
**SOUTHERN ELECTRICITY**
Littlewick Green, Maidenhead

**SECOND ENGINEER**
(Telecommunications)

**CHIEF ENGINEER’S DEPARTMENT**
**HEAD OFFICE**

**Applications**

**SALARY WITHIN THE RANGE £6,830-£8,955 PER ANNUM**

Applications are invited for the above post in the Technical Services Section of the Chief Engineer’s Department.

The successful applicant will be part of a team engaged in the design, commissioning, and subsequent maintenance of telecommunications systems throughout the Southern Electricity Board, and must be able to spend periods away from Head Office when carrying out these duties.

Schemes in progress include telecontrol, data communications, medium capacity microwave links, multi-channel line circuits and radio and line telephony systems. Applicants should have had experience in some of this work and preferably in possession of suitable technical qualifications.

The successful candidate will be required to drive a motor vehicle which may be either a private car or a Board-owned car. Appropriate relocation assistance will be provided.

Applications on forms obtainable from the Secretary, Southern Electricity, Southern Electricity House, Littlewick Green, Maidenhead, Berks., SL6 3QB, and returned to him quoting 76/79 by not later than January 11, 1980.

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**FIELD ELECTRONICS ENGINEERS**

Gardline Surveys are a leading Hydrographic and Geophysical Survey Company providing shipping, offshore positioning and site investigation services to oil companies and other clients.

Due to continuing expansion we have vacancies for the following personnel:

**SEISMIC ENGINEERS**—with a strong electronics background, a familiarity with digital acquisition systems and preferably with marine or shallow marine operations.

**UNDERWATER SYSTEMS ENGINEERS**—with a sound background in electronics and an aptitude for practical work and fault finding. Gardline operates a variety of equipment including Huntex Deep Tow Boomer, E. G. and G. Sidescan Sonars, Magnetometers, Sparkers, etc. Experience with one or more of these systems is desirable but not essential.

**POSITIONING ENGINEERS**—with experience in the field of survey vessel navigation or oil rig positioning. Gardline operates a variety of positioning systems including Satellite Navigation, 2KHZ Systems, Syledis and Trisponder. A computer and track plotter are usually used in conjunction with the above equipment. Familiarity with digital techniques and the ability to fault-find desk top calculators would be an advantage.

Whilst formal qualifications are an advantage, experience and the ability to work effectively in a field environment is considered to be of prime importance. We expect our engineers to be adaptable and willing to learn to use systems that they are not familiar with at present.

Employment will be based at Great Yarmouth or if required Aberdeen. Operations are primarily North Sea based but there are good prospects of overseas employment through our branch offices in Houston and Sharjah (U.A.E.).

Salary is fully negotiable and with sea pay is likely to be around £8,000.

There is a company pension scheme and 4 weeks’ annual leave plus roster leave accrued whilst at sea.

Applicants should write or telephone The Technical Manager, Gardline Surveys, Oilmar House, Admiralty Road, Great Yarmouth, Norfolk. Tel: Great Yarmouth (0493) 50723.
HOLLAND

Holland, the most ‘English’ country in continental Europe offers you high salaries and excellent opportunities for advancement.

If you have the following background you could earn around £13,000 p.a. on a long-term contract in Holland.

We have an immediate need for:

Technical Authors and/or Instructors
with either an electronics, radar/sonar or weaponry background.

Contact Norma Baxter on 01-952 8092 or evenings between 6pm and 8pm on 01-207 1725.

The Howard Organisation enjoys an international reputation and you are invited to benefit from our experience and success.

We have an immediate need for:

Senior Electronic Technician (MALE OR FEMALE)

£4,317-£4,770

For the Media Resources Centre, Glyn House, Church Street, Ewell. To carry out on-site service/repair work to electronic equipment used for teaching deaf children (VHF radio microphones, speech trainers, group hearing aids, audiometers, etc). To remove from site and repair in Ewell workshop those items best serviced by bench work. You will be expected to travel from school to school and school to base in your own vehicle, for which Casual User car allowance will be paid. You will be expected to diagnose and repair the special equipment as necessary, working alone in schools.

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Application form from Media Resources Centre, Tel. 01-393 0208.

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